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March 23, 1984

Ministry of Energy, Mines & Petroleum Resources 617 Government Street Victoria, B.C. V8V 1X4

Attention: Mr. P. Hagen

Coal Administrator

Dear Sir:

Enclosed please find our report on the Telkwa Project.

This report has been prepared by Mr. D. Handy and Mr. S. Cameron, both of whom are employed by Crows Nest Resources Limited as geologists.

Mr. D. Handy, Honours B.Sc., graduated in Geology from the University of Waterloo in 1977. Prior to his graduation, Mr. Handy worked as an assistant for two geotechnical companies and after graduation as a geologist for a major company in Saskatchewan. Mr. Handy has been employed by Crows Nest Resources Limited as a Project Geologist since 1979.

Mr. S.Cameron, B.Sc., in Geology graduated from the University of Calgary in 1981. Prior to graduation Mr. Cameron worked as an assistant for a major exploration company in the North West Territories. He also worked for Crows Nest Resources Limited as a geological assistant in 1980. Mr. Cameron has been employed by Crows Nest Resources Limited as a Geologist since May 1981.

In my opinion, all of these personnel are fully qualified, by training and experience to prepare this report and this account of work done under their direct supervision.

Yours very truly,

H.G. Rushton

Vice President - Development

Enclosure

1.0 Summary

The Telkwa Project is contained within 38 B.C. Coal Licences covering 9713 hectares and 5 Freehold Lots covering 1295 hectares. Shell Canada Resources Limited holds 13 of the 38 Licences and 2 of the 5 Freehold Lots under option agreements. The remainder of the licences are held by Shell Canada Resources Limited and the other 3 Freehold Lots are owned by SCRL. Crows Nest Resources Limited, which is a wholly owned subsidiary of SCRL is the operator of the project.

The Telkwa licences lie in close proximity to the Canadian National Railway and are 360 km by road east of the port of Prince Rupert. Existing infrastructure, the proximity of a coal handling port and the good quality of the coal make Telkwa an attractive project.

Early Cretaceous sedimentary rocks of the Skeena Group contain significant thicknesses (single seams up to 7.6 metres, aggregate seam thicknesses of up to 30 metres) of low ash, high grade, medium to high volatile bituminous coal amenable to thermal use.

Lack of outcrop exposure has necessitated that CNRL undertake an intensive drilling program since 1979 to delineate the deposit. Stratigraphic and structural interpretation of the Telkwa deposit is based largely on drill core data accompanied by a comprehensive suite of downhole geophysical logs.

The 1983 summer and winter drilling programs were undertaken to further delineate the East and West Goathorn areas of the deposit, and to verify structural and stratigraphic interpretations made on the basis of 1982 and previous drilling programs.

The 1983 exploration program included the construction of 4.8 km of new access road. Sixty-nine NQ diamond drill holes and four six inch diameter core holes were completed. A 1.76 km length seismic refraction survey was conducted to delineate depth to bedrock in problem areas at West Goathorn. A test pit was excavated to enable bulk samples of seams 2 to 10 to be obtained for washability tests. Geological and geotechnical data was also gathered from this excavation. Four six inch diameter core holes were drilled to provide further bulk samples of the seams from the north and south ends of the deposit.

The 1983 exploration program further defined the Goathorn Creek reserve area of low ratio coal indicated by the 1982 drilling program. The presence of Seam 1 at surface mineable depths was found at the north end of the deposit. This area must be drilled further to fully define the extent of this additional reserve.

The total field expenditure for 1983 was \$2,019,500. Of this total \$854,100 is being applied to the coal licences covered by this report. The remainder was spent on Freehold land owned by Shell Canada Resources Limited.

2.0 Introduction

2.1 Location and Access

Enclosure 1-1: Index Map

Enclosure 1-2: Access Map

The Telkwa Project is located 15 km south of the town of Smithers in West Central British Columbia; Coast Land District 5,NTS Map Sheet 93L/11. The coal licences lie north of the Telkwa River and east of Pine Creek and south of the Telkwa River along Goathorn Creek and Cabinet Creek. The center of the licence block is situated at N. Lat 54°35'/N. Long 127° 8'. Smithers is 360 km from the port of Prince Rupert along the CNR line and Highway 16. The Telkwa Project is 10 km from this rail line and mostly accessible by good gravel road.

2.2 Tenure

The Telkwa Project licences are subdivided into three groups: Telkwa North, Telkwa South and Bulkley Valley Coal Limited Option.

Such a subdivision is necessary for land tenure purposes.

GROUP NUMBER	LICENCE NUMBERS		
327	4271, 4272 , 4274-4281, 4283, 5305-5307, 6040		
325	4260-4262, 4264, 4265, 4267, 4269, 4270, 4282, 5389		
Bulkley Valley Coal Limited Option 221	3709, 3710, 3875-3885		

All licences are operated by Crows Nest Resources Limited. All licences are held by Shell Canada Resources Limited with the exception of those optioned from Bulkley Valley Coal Limited.

In addition, Shell Canada Resources Limited owns 3 freehold lots and options 2 freehold lots (Whalen Option) which are also included as part of the Telkwa Project.

Appendix 1 of this report contains a "Coal Land Disposition Map".

Appendix 2 contains a tabulation of "B.C. Coal Land Tenure Standing" for each group of licences being renewed.

3.0 Regional Geology

Mesozoic successor basins developed in the Intermontane Belt between the Columbian and Pacific Orogens in the B.C. Cordillera. These deeply subsiding troughs usually had both marine and fresh water depositional environments. Fresh water lakes could have developed in areas of poor drainage and provided sites for thick peat accumulation. Coal bearing clastic sequences also accumulated in areas of dip-slip and strike-slip faulting in the troughs.

The Skeena Group successor basin is filled with interbedded marine and non-marine sedimentary and volcanic strata. This assemblage was deposited on the folded and faulted terrane of the Bowser Lake and older groups such as the Hazelton. Sediments of the Skeena Group are distinguishable from the Bowser Lake and Hazelton sediments by the presence of fine detrital muscovite. "In the Late Jurassic to Early Cretaceous, prior to deposition of the Skeena Group sediments, the Hazelton Group underwent a period of uplift, deformation and erosion. During the Mid Early Cretaceous, the sea readvanced from the west, in the area of Skeena Valley, inundating the non-marine, Late Lower Cretaceous coal basins such as Telkwa and Lake Kathlyn. The sediments of the Skeena Group were derived from an uplifted Pinchi-belt - Columbian Orogen. They were deposited in a southwesterly direction, across the Skeena Arch, which apparently had little influence on the shape of the basin receiving the Skeena Clastics". 1

1 Tipper H.W. and Richards T.A., Jurassic Stratigraphy and History of North Central British Columbia, 1976, page 7.

Tipper and Richards (1976) have taken Sutherland Brown's (1960) subdivision from the Hazelton Group and applied it to the Skeena Group as follows: The Brian Boru Formation for the Early Cretaceous volcanics and the Red Rose Formation for the Late Jurassic to Early Cretaceous sediments.

4.0 Telkwa Geology

4.1 Stratigraphy

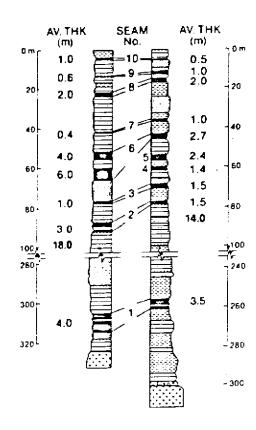
Figure 1: Telkwa Type Stratigraphic Section

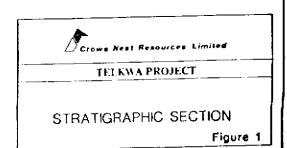
The rocks of the Telkwa coal field consist of interbedded marine and non-marine sedimentary and volcanic strata of the Skeena Group. The sediments include a predominance of mudstone and siltstone with minor sandstone and shale, a basal conglomerate and coal. Volcanics are grey to green basaltic to rhyolitic breccias, tuffs and flows. The Hazelton volcanics are usually weathered to a deep reddish-purple at their contact with the overlying Skeena sediments. Porphyritic Tertiary intrusive rocks in the form of dykes and sills have been found over the property. A large intrusive plug forms a nonconformable contact with the Skeena sediments north of the Telkwa River. In the Telkwa area recent erosion has removed the coal-bearing sediments from the higher ridges leaving all or part of the sedimentary sequence preserved in topographic lows. Outcrops are usually found in stream valleys which have cut through the glacial drift cover. Few exposures occur away from the creeks until the higher ridges are reached and invariable these are volcanics of the Hazelton Group. The Skeena-Hazelton contact over most of the area is drift covered and heavily timbered making accurate delineation of the areal extent of the coal bearing sediments very difficult.

STRATIGRAPHIC SECTION

WEST GOATHORN

EAST GOATHORN





- 7 -

The Skeena Group stratigraphic section varies in thickness over the Telkwa area but probably does not exceed 500 metres. Laterally, individual beds can pinch out rapidly including coal beds as evidenced by drill hole TW82D-238.

A palynological study on two drill cores representing the Telkwa stratigraphic section indicates clastic deposition started in Neocomian times in a marine depositional environment. A marine regression occurred resulting in a fluvial flood plain environment with the deposition of Seam #1 or the #1 coal zone. The study indicates the rocks between Seam #1 and the upper coal zone were deposited in mainly a shallow, lower energy marine environment with the occasional regression/transgression cycle occurring. The upper coal zone from Seam #2 to #7 is believed to have been deposited in a deltaic environment supporting swamp and/or marsh vegetation.

The upper 3 seams #8,#9 and #10 appear to have been deposited in a coastal region periodically subjected to tidal incursions. Above Seam #10 the study shows an upland depositional environment in a fluvial regime indicating a major marine regression near the end of the Lower Cretaceous in Telkwa area. The Telkwa sediments exhibit numerous soft sediment deformation structures including rip up clasts, micro slump faults and load casts. Heavily bioturbated zones are common. Thin bentonitic clay layers (1 to 5 cm thick) are present at certain locations in several of the coal horizons. X-ray defraction indicates these clays to be kaolinitic in composition and not mixed layer "swelling clays".

4.2 <u>Coal Stratigraphy</u>

At least 14 individual coal seams exist in the Telkwa deposit.

Within the Goathorn Creek area 10 major correlatable seams have been identified. These are numbered 1 to 10 going stratigraphically up section. Average aggregate thickness of the upper 9 seams at Goathorn East (east of Goathorn Creek) is 14 metres. The upper 9 seams range individually from a thickness of 0.5 to 2.5 metres on average. West of Goathorn Creek individual coal intersections of up to 7.6 metres have been drilled. Seams #4 and #5 pinch out laterally in the Goathorn East area and are not present at Goathorn West. The remaining 7 seams thicken westward and average an aggregate thickness of 18 metres at Goathorn West. A distinct marker horizon occurs beneath Seam #2 on the gamma ray logs. This geophysical signature has been used as a datum line for seam correlation over the entire property. Seam #1 is situated some 100 to 150 metres below the gamma marker and averages 3.5 m in thickness over the property. Over the property individual coal seams develop splits, thickness changes over short lateral distances, and the seams exhibit an extremely undulating nature. These inconsistencies will require a very flexible approach to mining and coal preparation.

4.3 Structure

In the Goathorn Creek area, north-south to north/west-south/east trending normal and reverse faults have divided the property into several structural fault blocks. The majority of these faults have been interpreted from drilling data, stratum contours and air photo interpreted lineaments. These faults occur as zones with imbricates and splays as evidenced by coal seam repeats in some drill holes. Most of the faults are believed to be high angle (ie: dips greater than 75°). While some appear to originate in basement volcanics this is not necessarily the rule. The test pit excavation uncovered a number of small scale offsets (in the order of a few metres). These were not detected by closed space drilling (30 metres). A high frequency of faults of this nature can be expected throughout the property. Over the Goathorn East area, the beds strike from 345° to 025° and dip to the east within a 10° to 35° range.

The Goathorn West area shows a predominance of northwest - southeast trending normal faults as well as a shallow east-west trending syncline toward the northern end. Generally the west strata maintain a strike of 330° with dips to the north in the 10° to 30° range.

5.0 Summary of Previous Work

- 1979 1:10000 scale geological mapping
 - bulldozer trenching
 - road upgrading
 - rotary drilling (4 holes)
 - coal sampled and analyzed
 - drill site reclamation
- 1980 no exploration
- 1981 1:10000 scale geological mapping
 - 1:5000 scale geological mapping
 - road upgrading
 - bulldozer trenching
 - rotary drilling (7 holes)
 - diamond drilling (1 hole)
 - coal sampled and analyzed
 - drill site reclamation
 - geodetic location survey
 - geophysical survey EM37
 - 1:5000 scale topographical maps constructed

- 1982 1:5000 scale geological mapping
 - backhoe trenching
 - road construction and upgrading
 - rotary drilling
 - diamond drilling
 - coal sampled and analysed
 - geophysical surveys EM37
 - seismic refraction
 - proton magnetometer
 - geotechnical studies piezometer installation
 - soil sampling
 - core logging
 - 1:5000 scale topographical maps constructed
 - 1:1000 scale topographical maps constructed
 - 1:2000 scale topographical maps constructed
 - road and drill site reclamation

6.0 Work done in 1983

- 1:1000 scale geological mapping (test pit)
- road construction
- diamond drilling-NQ and 6 inch diameter
- coal sampled and analysed
- seismic refraction survey
- geotechnical studies piezometer installation
 - core logging
- test pit excavated
- 219 tonnes of coal bulk sampled from seven seams
- road and drill site reclamation
- test pit reclamation

The stratigraphic section was mapped in the test pit excavation.

A total of 4.8 km of new road was constructed, 1.6 km on Freehold Land, 3.2 km on licences covered by this report.

69 NQ diamond drill holes were completed on the property during 1983 for a total of 8175 metres. 39 of the diamond drill holes (5656 metres) are situated on licences covered by this report. The remaining holes are located on Freehold lots. All drill core has been lithologically logged. Selected core holes have been geotechnically logged in detail. CNRL's drill core storage facility is located at the site of Bulkley Valley Collieries Limited.

Four 6 inch diameter core holes were completed for a total of 403 metres.

One of the four holes was collared on a licence covered by this report for

a total of 142 metres. The other 3 holes were drilled on Freehold lots. Coal samples were sent to Birtley Laboratories in Calgary for analyses.

A test pit was excavated on Freehold land and from this pit 219 tonnes of coal from Seams #2, #3, #6, #7, #8, #9 and #10 was shipped to Birtley Laboratories for washability tests.

All pertinent drill holes and roads were surveyed. Additional 1:15000 scale air photos were taken as well as a set of true color photographs at a scale of 1:40000. Present 1:2000 and 1:5000 contour maps were updated and a new set of 1:5000 orthophotos was constructed.

1.76 km of seismic refraction was conducted on licences covered by this report.

12 Piezometers were installed in holes on both East and West Goathorn.

Packer permeability tests were performed on 4 of the piezometer locations.

All disturbances including new roads, drill sites and the test pit were recontoured and seeded.

The total cost of the 1983 exploration work was \$2,019,500. Of this figure, \$854,100 is being applied to the licences reported herein.

Appendix 3 contains a copy of the Application to Extend Term of Licence which gives a detailed account of the amount and nature of expenditures applied to the three licence groups.

7.0 Test Pit

The test pit was excavated to obtain bulk coal samples from each of the upper 9 coal seams at Goathorn East for pilot plant washability tests and ultimately engineering design of a coal preparation plant. In addition, geotechnical data related to pit wall stability, hydrology, and mining equipment was gathered from this exercise.

7.1 Geology

Eleven NQ diamond holes were drilled on an east west line at a spacing of from 90 to 30 metres to determine to subcrop elevation and the structural geometry of Seams #2 to #10. Coal quality tests were performed to determine if the subcrop of each seam was oxidized.

Drilling indicated that Seam #4 and #5 pinched out laterally, therefore these seams were not sampled in the test pit. Enclosures 1-16 and 1-17 contain the test pit geological map and cross-section with bulk sample locations and test pit cross-section.

7.2 Equipment Used

One 631C Scraper

Two 631D Scrapers

One D8 Crawler Tractor

Two D9 Crawler Tractors

One Hydraulic Excavator

Reclamation work was done with a farm tractor, skidder and a small crawler tractor.

Coal bulk samples were shipped to Birtley Coal and Mineral Testing Limited in Calgary via 5 ton unit containers, 2 end dump gravel trucks and one belly dump gravel truck.

The duration of the test pit excavation from top soil removal to reclamation was from the end of June to the end of September.

Approximately 145,000 cubic metres of material were moved, 40,000 cubic metres were rehandle material.

Seams #2,#3, #6, #7, #8, #9, #10 were all bulk sampled for a total of 219 tonnes. The pilot plant washability tests on these samples are ongoing at present. The engineering assessment of this data will be completed by August 1984.

7.3 Mining and Geotechnical Observations

Scrapers and crawler tractors appear to be a viable mining method at Telkwa. Approximately 10% of the interburden rock was difficult to rip with a D9 and may require blasting in a full scale mining operation.

Backfilling the pit indicated an 8-10% swell factor can be anticipated.

The coal was very hard with clean hanging wall/footwall separations. In a practical mining situation dilution will be more significant than that experienced in the test pit. Factors influencing mining dilution will be the high frequency of small scale faults, the undulating nature of the seams and mining thin seams (0.30m to .50m) or split seams such as Seam #3.

Surface run-off was controlled by a small containment pond. Ground water flow was evident at several coal footwall contacts. An indepth hydrological study is presently underway.

Pit slope stability was extremely good, however the test pit excavation was at deepest in the order of 20 metres. Individual benches should stand well in excess of 45 degrees when mining down dip. A detailed engineering study is in progress to determine actual stability.

8.0 Mineability and Reserves

8.1 Goathorn Creek Area

The Goathorn Creek area of the Telkwa Project is the most attractive location for low-ratio open pit mineable coal. The upper 7 to 9 coal seams generally maintain thicknesses of 0.5 metres or greater and total 14 to 18 metres of aggregate coal thickness in 85 to 100 metres of stratigraphic section. A significant amount of Seam 1 should be mineable at the north end of the Goathorn East area and in the area of hole TW82D-239 in Goathorn West. Goathorn East contains probably 90% of the mineable reserves in the Goathorn Creek area. Glacial fluvial erosion has removed much of the reserves in the Goathorn West area.

Using an aggregate coal thickness of seams greater than 0.3 metres per hole multiplied by an area of influence of half the distance to each adjacent hole results in an insitu reserve of 50 million tonnes for the Goathorn Creek area.

Seam 1 was not included in this calculation. Assigning a specific gravity of 1.5 g/cc to the coal results in an overburden ratio of less than 10:1 bank cubic metres waste per tonne coal. These reserves should be classified as proven. This reserve was calculated after the 1982 field season. At the time of writing of this report an updated reserve calculation using the 1983 drilling has not been completed. This work will be finished by the summer of 1984.

9.0 Coal Quality

The 1983 quality program involved obtaining samples from "NQ" core holes, large diameter core holes (6 inch or 15.24cm) and bulk samples from a test pit located in the Goathorn East project area.

Coal core samples were obtained from 69 NQ diamond drill holes. In addition 4 large diameter (15.24cm) diamond holes were cored. The objective of the large diameter core program was to obtain samples of Seam #4 and #5 for washability purposes since these seams were not present in the test pit.

A secondary objective was to obtain samples to the north and south of the test pit in order to determine if any variation in washability characteristics occur across the property. Analytical results of the large diameter core are not available at the time of writing this report.

Incremental analysis on a per hole basis can be found in Appendix 6.

Quality on a seam by seam and on an overall weighted average basis for Goathorn East and Goathorn West follows in Tables 1 through 6.

A total of 14 bulk samples were extracted from the test pit through an entire section of Seam #2 to Seam #10 with the exception of Seams #4 and #5, both of which pinched out just east of the test pit. These samples will be used to determine the washability characteristics of each seam which in conjunction with mining criteria will be used to make up a number of blends for pilot plant processing. Combustion tests will be performed on the clean coal from the pilot plant products. No results are available at this time.

The Telkwa coal is ranked as High Volatile "A" Bituminous by ASTM standards. Analytical results from core hole data show it to be a prime thermal coal product with heating values in excess of 7000 kcal/kg at approximately 10 percent ash. Yields at this ash level are upward of 75% with average volatiles of 28 % and a sulphur content of approximately 1 to 1.2 percent. The Hardgrove grindability index is in the range of 60 to 62. Initial testing on selected samples show fluidity to be quite low although the possibility of producing metallurgical coal on a batch basis will be investigated. Rheological test results, ultimate analysis, ash analysis and ash fusion temperatures of samples from core hole TW81D-112 can be found in appendix 6. Ash fusion temperatures performed on samples from core hole TW81D-112 are all in excess of 2200°F.

Appendix 6 also contains data from preliminary washability tests performed on two small diameter (NQ) core samples. The results indicate that clean separations can be expected at high specific gravities resulting in a high yield, low ash product.

TABLE 1

RAW COAL QUALITY

GOATHORN EAST

BASIS - AIR DRIED RAW COAL

DATE: MARCH 13, 1984

SEAM	RESIDUAL MOISTURE	ASH	VOLATILES	FIXED CARBON	CALORIFIC VALUE	SULPHUR	AVERAGE THICK. (m)
1	.84	23.94	24.73	51.32	6285	1.25	5.21
2	1.09	24.22	25.37	47.56	6059	1.16	2.49
3	.99	25.14	24.10	46.20	5764	1.79	2.02
4	1.02	17.60	26.80	53.54	6528	1.55	1.54
5	1.16	17.29	25.59	54.34	6586	.90	2.33
6	1.21	20.13	25.28	51.04	6258	1.27	3.35
7	1.14	18.50	26.24	51.21	6378	2.15	1.52
8	1.21	16.74	26.44	54.43	6671	1.98	2.16
9	1.06	16.03	30.02	50.92	6896	2.86	1.01
10	1.06	17.46	28.00	50.02	6693	3.00	.81

TABLE 2
WASHED COAL QUALITY
GOATHORN EAST

DATE: MARCH 13, 1984

BASIS - AIR DRIED WASHED AT 1.6, 1.7, 1.8 S.G.

AVER. RESIDUAL FIXED CALORIFIC THICK SEAM MOISTURE ASH **VOLATILES** CARBON VALUE **SUL PHUR** FS1 YIELD (m) 1 1.11 12.83 27.36 58.68 7127 .85 3.5 72.01 5.21 2 1.95 11.93 27.42 57.68 7102 .81 1.0 74.31 2.49 3 1.75 12.43 27.37 58.44 7097 1.22 1.0 73.62 2.02 1.60 9.05 4 28.78 60.56 7332 .96 2.0 77.96 1.54 2.03 5 8.38 27.82 61.77 7398 .65 1.0 80.83 2,33 6 2.05 9.19 28.49 60.27 7291 .88 1.0 79.57 3.35 7 1.73 9.70 29.01 59.56 7295 1.32 1.5 81.60 1.52 8 1.85 9.42 28.72 60.02 7311 1.15 1.0 83.99 2.16 9 1,32 8.80 33.13 56.75 7499 1.75 1.5 83.22 1.01 10 1.38 10.45 31.19 56.98 7328 2.07 2.0 83.70 .81

TABLE 3

RAW COAL QUALITY

GOATHORN WEST

BASIS - AIR DRIED RAW COAL

DATE: MARCH 13, 1984

SEAM	RESIDUAL MOISTURE	ASH	VOLATILES	FIXED CARBON	CALORIFIC VALUE	SULPHUR	AVERAGE THICK. (m)
1	.89	28.13	24.09	46.83	5581	1.93	4.73
2	1.26	18.25	23.51	54.42	6282	1.44	2.95
3	.97	24.25	22.73	50.15	5831	1.56	1.38
6	1.38	14.00	-	•	-	.68	4.53
6U	.98	16.83	25.83	56.35	6688	1.60	4.09
6L	1.43	11.30	27.02	60.65	7212	1.15	6.36
7	1.18	15.63	23.57	52.14	6088	2.91	1.24
8	1.14	16.55	22.27	59.53	6651	1.39	2.67
9	1.16	20.05	24.58	51.35	6036	4.12	1.07
10	1.06	27.79	23.99	47.16	5627	3.87	1.18

TABLE 4
WASHED COAL QUALITY
GOATHORN WEST

BASIS - AIR DRIED WASHED AT 1.6, 1.7, 1.8 S.G.

DATE: MARCH 13, 1984

SEAM	RESIDUAL MOISTURE	ASH	VOLATILES	FIXED CARBON	CALORFIC VALUE	SULPHUR	FSI	YIELD	AVER. THICK (m)
1	.96	12.77	27.03	59.24	7128	1.20	3.5	61.51	4.73
2	1.99	9.78	25.57	63.05	7304	1.01	1.0	80.38	2.95
3	1.23	11.04	25.03	64.07	7251	1.13	1.5	67.17	1.38
6	3.04	6.72	25.36	64.89	7371	.68	-	85.39	4.53
6U	1.44	6.20	27.67	64.69	7623	.98	2.5	79.96	4.09
6L	1.87	6.52	27.54	64.07	7472	.83	2.5	91.20	6.36
7	1.78	6.16	26.19	65.87	7499	1.39	.5	82.10	1.24
8	1.49	10.03	24.16	64.33	7192	1.17	1.0	81.53	2.67
9	1.01	9.08	26.02	63.90	7379	2.51	1.0	72.28	1.07
10	1.30	9.77	26.28	62.66	7307	2.53	2.0	63.00	1.18

TABLE 5

TELKWA PROJECT

GOATHORN EAST OVERALL QUALITY

	FLOAT 1.6 to 1.8 S.G.	RAW
VOLATILES	28.16	25.42
ASH	10.73	21.34
RESIDUAL MOISTURE	1.76	1.08
FIXED CARBON	59.14	50.59
CALORIFIC VALUE (kcal/kg)	7219	6264
YIELD	77.35	-
FSI	1.5	-
SULPHUR	1.00	1.52
AVERAGE THICKNESS(m)	2.24	2.24

TABLE 6

TELKWA PROJECT

GOATHORN WEST OVERALL QUALITY

	FLOAT 1.6 to 1.7 S.G.	RAW
VOLATILES	26.51	24.39
ASH	10.04	21.19
RESIDUAL MOISTURE	1.43	1.09
FIXED CARBON	62.16	51.80
CALORIFIC VALUE (kcal/kg)	7289	6104
YIELD	73.65	-
FSI	2.5	-
SULPHUR	1.15	1.76
AVERAGE THICKNESS (m)	2.71	2.71

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TELKWA PROJECT

SSESSMENT REPORT

N.T.S. Map Sheet

93L/11

Lat./Long

54° 35'/127° 8'

Coal Licences

Group 327

4271, 4272

4274 - 4281 4283, 6040

5305 - 5307

Group 325

4260 - 4262 4264, 4265

4267, 4269

4270, 4282

5839

Bulkley Valley Coal Ltd. Option

3709, 3710 3875 - 3885

Group 221

Shell Canada Resources Ltd.

Licences Held by -

Crows Nest Resources Limited

Exploration Period -

May - September 1983

December 1983

Report Date -

Operated by -

March 1984

Project Members -

Dave Handy

Steve Cameron

Project Geologist Geologist

Jim Eisenman

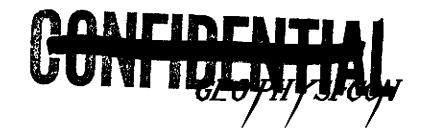
Geol. Technologist Field Coordinator

Robert Aiello

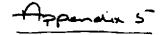
TELKWA PROJECT

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SEISMIC SURVEYS TELKWA COAL PROJECT, B.C. SUMMER 1983



Prepared For

CROWS NEST RESOURCES LTD.
CALGARY, ALBERTA

Prepared By

GEO-PHYSI-CON CO. LTD. CALGARY, ALBERTA

August 1983 C83-21

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GEO-PHYSI-CON

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1.0 INTRODUCTION

This report presents the results of geophysical surveys carried out for Crows Nest Resources by Geo-Physi-Con Co. Ltd.

The location of the survey was at Crows Nest Resources, Telkwa
Coal Project, just outside of Telkwa B.C., shown in Figure 1.

The area is characterized by coal bearing sedimentary rock lying over volcanic basement and under a highly variable thickness of overburden. The survey objectives were:

- to map the thickness of overburden (depth to sedimentary rocks using refraction seismic methods),
- ii) to map coal seams using reflection seismic methods in a test pit located on the east side of Grothorn Creek, and
- iii) to determine depth and rippability of bedrock using refraction seismic in the test pit.

The survey is requested and authorized by Dave Handy of Crows Nest Resources Ltd. under Purchase Order 22371.

2.0 LOGISTICS AND DATA ACQUISITION

The seismic surveys were carried out between July 11 and 15, 1983 by a four-man crew. The crew included a project geophysicist, senior technician and two field helpers from Geo-Physi-Con Co. Ltd.

The crew lodged at commercial facilities in Smithers, B.C. and traveled daily to the survey site. Two trucks were rented from Budget Rentals in Smithers. Explosives and storage magazines were obtained through Free Spirit Adventures, also located in Smithers. The survey line locations are shown in Figure 2.

A seismic spread of 12 geophones was used with either 5, 20 or 40 metre spacing between geophones. In Table 1 is a list of line numbers, geophone separation, seismic method employed and length of line.

TABLE 1

Line	Geophone Spacing	Seismic Method	Length
West 4	40 m	Refraction	880 m
West 6	20 m	Refraction	880 m
Test Pit	5 m	Refraction and reflection	275 m

Compression type seismic waves were generated with explosives placed in shallow (<0.5 metre) holes for geophone spacing of 20 m and 40 m. For the 5 m spacing, those waves were generated by a hammer striking a metal plate.

The seismic data was recorded using a GeoMetrics
ES1210-F 12 channel signal enhancement seismograph. The manufacturer's specifications for this instrument are included in Appendix
A. For seismic spreads having a geophone spacing of 20 m or 40 m, arrivals were recorded from shot locations 20 m and 220 m from the end of the cable as well as from one to three interior shots. The purpose of the end shots was to obtain arrivals refracted from

bedrock at most geophones. The purpose of the interior shots was to provide control in the variation in overburden velocity. For geophone spacing of 5 m, arrivals were recorded at either end of the cable as well as one interior shot. A typical shooting arrangement is illustrated in Figure 3.

Relative elevations were determined using a hand inclinometer and distance using the geophone cable. True elevations were then determined using topographic base maps supplied by Crows Nest Resources Ltd.

3.0 DATA PROCESSING

In seismic surveys the data obtained consists of travel times of compressional waves, from source (explosive charges) to detectors (surface geophones). The paths of the seismic waves are illustrated in Figure 4.

3.1 Refraction Seismic

The depth to bedrock is calculated by the delay time method. An example of this method for a simple two-layer case is

shown in Figure 5. A plot is first made of the difference in arrival times at the same geophone from shots offset from the ends of the cable spread. The geophones which record arrivals from teh bedrock will generate a straight line with little scatter; the slope of the line is $2/V_2$ (Figure 5). Points which do not fall on this line indicate that the paths of at least one of the waves did not refract from the bedrock. The advantage of this procedure is that the difference plot allows i) the identification of geophones recording arrivals refracted from the bedrock, and ii) the calculation of a true bedrock velocity that takes into account irregular dipping surfaces.

Next, the delay times defined in Figure 5 are computed for each geophone having arrivals from the same refractor. The delay time is directly proportional to the layer thickness, so that the depth can be calculated beneath each geophone (Figure 5). The time distance graphs for each spread are included in Appendix B.

3.2 Reflection Seismic

The reflection seismic was interpreted using the X-squared T-squared analysis. This method has been graphically illustrated in Figure 6. In the interpretation the arrival times

are squared along with the corresponding offset distance. These are then plotted on the X-squared T-squared coordinate system. A best fit straight line is drawn through the points and the velocity determined by taking the square root of the inverse of the slope of the line. The intercept of the line is T_0^2 . Using all of this information, depths can be determined using the equations in Figure 6.

3.3 Determination of Rippability

The seismic velocity of rock relates to its competency and strength. The Caterpillar Company has established a relation between rippability with hydraulic rippers mounted on various Caterpillar tractors and seismic wave velocity. The chart for the D9H Caterpillar tractor is reproduced in Figure 7. This chart was compiled from experience with ripping on an open face (grade rock).

It should be stated that velocity is only one factor determining ease of excavation. Other factors which may affect the excavation are i) the ability of the ripper to penetrate the rock ii) the amount of space and grade for the cut. Clearly, the

classification is subject to modification due to local conditions but is probably a reasonable estimate.

Since the exact rock type is not known for each site, an average was taken from the rippabilities of all the sedimentary rocks listed in the chart and classified in the following manner.

- a) <2500 m/sec rippable
- b) 2500 3000 m/sec marginally rippable
- c) 3000 m/sec nonrippable

4.0 RESULTS

The seismic program was planned to i) determine the depth to coal bearing sedimentary sequences by refraction seismic method ii) to map coal seams in a test pit using reflection seismic and iii) to determine depth and rippability of rock in the test pit using refraction seismic.

4.1 West 4

The depth to bedrock profile from the interpretation of the refraction seismic is shown in Figure 8. Two seismic spreads

using a 40 m geophone spacing were surveyed for a total length of 880 m. This line was an extension of Line West 4 of the 1982 seismic program.

The bedrock profile shows that a three-layer section is present along the entire line. The first layer has a velocity of 850 m/sec and represents overburden. The second layer ranges in velocity from 1920 m/sec to 2200 m/sec. This is representative of more dense materials which may or may not be saturated. The bedrock velocity was 3920 m/sec and is representative of competent sedimentary rocks. From station 0 to 500, rock occurs between 130 and 180 m. For the remainder of the line bedrock of this velocity was not detected with the shooting arrangements available so the depth to bedrock has been inferred. The depth to rock here was calculated to be from 180 m to 206 m. There is a drill hole close by which did not reach rock after drilling over 125 m.

4.2 West 6

There were 4 seismic spreads surveyed with a geophone spacing of 20 m along this line. The profiling in this area was not continuous due to the fact that the road was not straight.

The location of Spread 1 is shown in Figure 2. The interpreted section from the refraction seismic data is shown in Figure 9. The section was interpreted using a three-layer model. The first layer had a velocity of 950 m/sec and is representative of overburden type materials. The second layer had a velocity of 1810 m/sec and probably represents materials more dense than the first layer which may or may not be saturated. The third layer had a velocity of 2620 and represents bedrock type materials. The depth to this layer ranged from about 90 m to 105 m.

The location of Spread 2 is shown in Figure 2. The interpreted section from the refraction seismic data is shown in Figure 10. The section was interpreted using a three-layer model. The first layer had a velocity of 870 m/sec and is representative of overburden type materials. The second layer had a velocity of 1860 m/sec and probably represents materials more dense than the first layer. The third layer had a velocity of 2600 and has been interpreted to represent bedrock type materials. The rock becomes much shallower compared to Spread 1 with depths of between 35 m and 45 m being calculated.

The location of Spreads 3 and 4 are shown in Figure 2. These two spreads were joined and the results of the refraction seismic interpretation shown in Figure 11.

There are two drill holes located along this portion of line. The first drill hole (DH 209) was located at Station 40 and reported overburden thickness at 7.5 m. The second drill hole (DH 107) was located at Station 280 and reported overburden thickness at 7.0 m.

The depth to bedrock has been determined using a three-layer model along the entire line. The first layer had a velocity of between 700 and 750 m/sec and is representative of overburden type materials. The second layer had a velocity of 1930 m/sec and represents more dense materials which may or may not be saturated. The third layer had a velocity of between 3500 and 3530 m/sec and is representative of competent sedimentary rocks. From Station 0 to 240 the depth to rock is fairly shallow with depths of between 35 m and 50 m. Along the remainder of the line, rock becomes much deeper with depths of over 80 m being calculated at Station 460.

The results of the refraction seismic do not match the drill hole results along the line. A possible explanation for this is that the rock layer has been weathered and has the same velocity as the second layer (~1930 m/sec). Therefore, there is no velocity contrast between layers, making it impossible for refraction seismic to distinguish between layers. If this were

the case, then drilling has not reached the competent rock (~ 3500 m/sec).

It is felt that if the rock has similar velocities to the second layer it is a localized phenomena. The reason for this is the fact that drill holes located within 150 m of the seismic line (DH 267, DH 228 and DH 230) reported depths of 34 m, 49 m and over 30 m, respectively. These depths correspond to depths calculated by refraction seismic along this line.

4.3 East Test Pit

At this site two seismic methods were employed using a 5 m geophone spacing. First, refraction seismic was done to determine depth to rock and the rippability of that rock and second, using reflection seismic to determine coal seams in the subsurface.

The results of these surveys are shown in Figure 12. The depth to rock has been determined using a two-layer model. The first layer velocities ranged from 210 to 580 m/sec and are representative of overburden velocities. The second layer ranged from 2000 to 3330 m/sec and is representative of rock. The rock is quite shallow with depths of between 1 m and 3 m. In Figure 12 is shown the rippability of these rock zones.

The reflection seismic was able to locate a reflectors along portions of the survey line shown in Figure 12. The first occurs between Stations 0 and 65 at a depth of between 50 m and 55 m. The second between Stations 140 and 170 at a depth of between 35 m and 40 m and the third from station 230 and 300 at a depth of between 45 m and 50 m.

5.0 CONCLUSIONS

Since there is a marked difference between overburden and bedrock velocity, it was possible to determine depth to bedrock using refraction seismic techniques. Along line West 6, Spreads 3 and 4, there is disagreement between depth to rock as reported in drill holes and those calculated by refraction seismic. A possible explanation is that the rock in this case is weathered with similar velocities as the overburden (~1930 m/sec). This would result in there being no velocity contrast between layers, making it impossible for refraction seismic to distinguish between layers. If this is the case, drilling has not reached the more competent rock layer (~3500 m/sec).

From the velocities obtained through the analysis of the refraction seismic data it was also possible to determine rippability of rock at the test pit. This was done by comparing the

velocities to the Caterpillar Company's "Performance Rippability Charts" for sedimentary rocks of a D9 Ripper. Clearly, the Caterpillar Rippability Charts are subject to modification due to local conditions but they are probably a reasonable estimate.

The reflection seismic had limited success in locating reflectors at depth in the test pit area.

THE ASSOCIATION OF PROFESSIONAL ENGINEERS, GEOLOGISTS and GEOPHYSICISTS OF ALBERTA PERMIT NUMBER P 2802

Geo Physi Con Co. Ltd.

Calgary, Alberta July 1983 C83-21 Respectfully submitted,

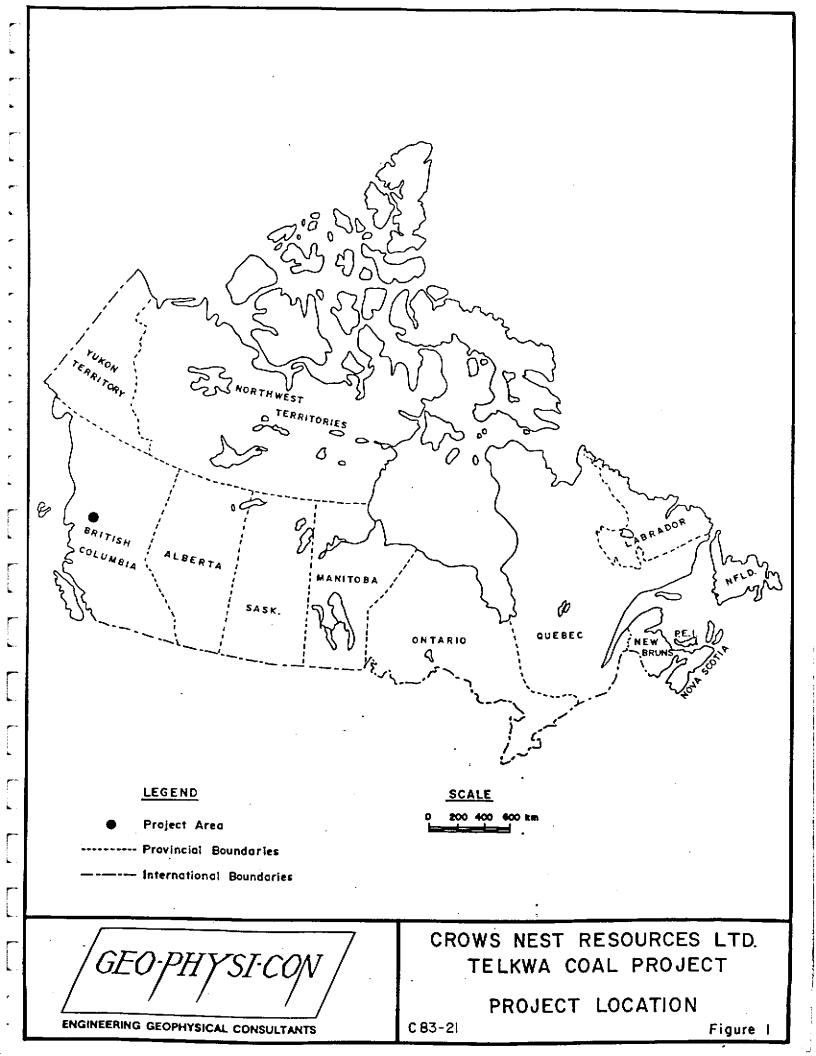
GEO-PHYSI-CON CO. LTD.

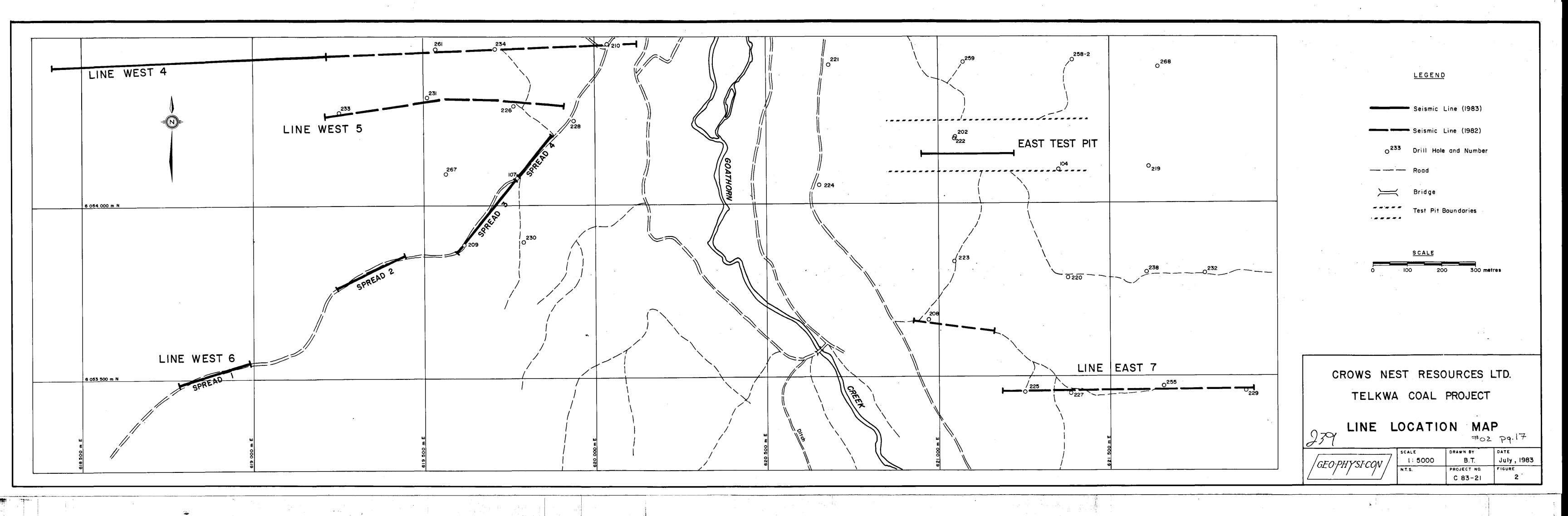
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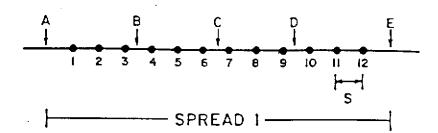
Michael Pesowski, B.Sc., Project Geophysicist

Per: midal Pank

T. Sartorelli, P.Eng., Senior Geophysicist







LEGEND

- Geophone location
- Shot locations
- A Normal shot
- B Normal centreline shot
- E Reverse shot
- D Reverse centreline shot
- C Centreline shot
- S Geophone spacing

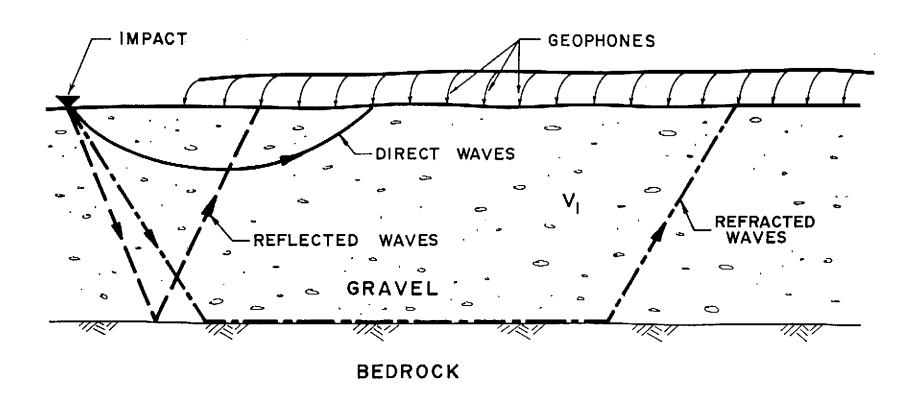
GEO-PHYSI-CON

ENGINEERING GEOPHYSICAL CONSULTANTS

SHOT AND GEOPHONE LAYOUT SINGLE SPREAD CROWS NEST RESOURCES LTD.

CB3-217

Figure 3



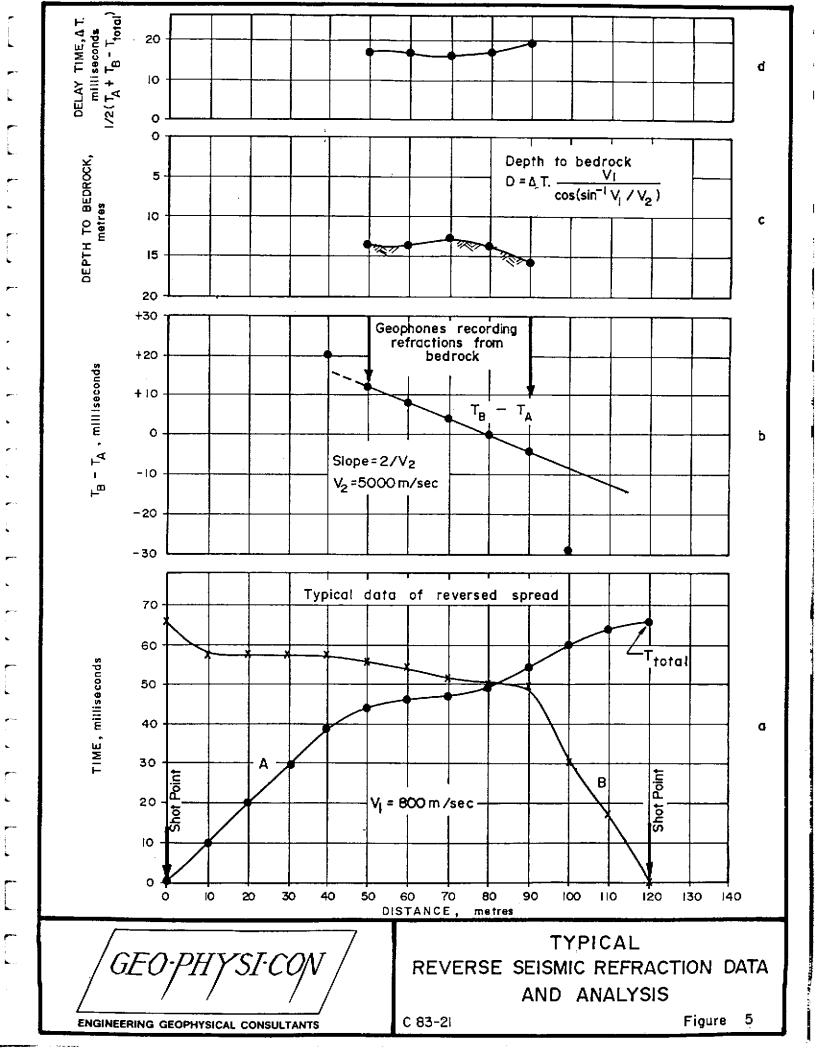
 $V_2 > V_1$

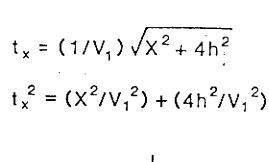
GEO-PHYSI-CON ENGINEERING GEOPHYSICAL CONSULTANTS

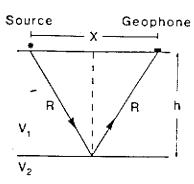
PATHS OF SEISMIC WAVES

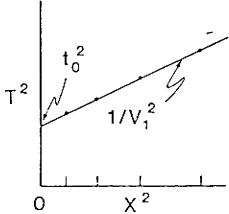
C 83-21

Figure 4









$$V_1 = \sqrt{1/(\text{Slope of line})}$$
where $V_1 = \text{velocity of medium}$

$$h = \sqrt{(t_0^2 V_1^2)/4} = (t_0 V_1)/2$$
where h = depth to reflector at X = 0

FROM: An Introduction to the Utilization of the Shallow or Engineering Seismic Reflection Methods R. Lankstrom, M. Lankstrom, 1981

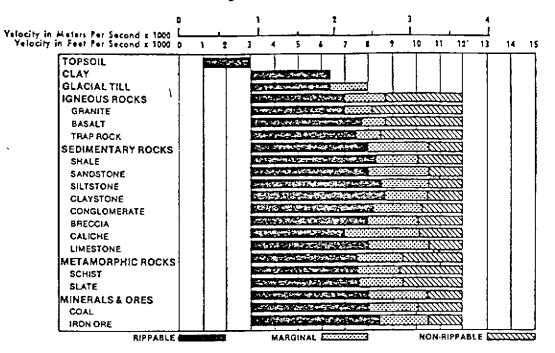
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CROWS NEST RESOURCES LTD.

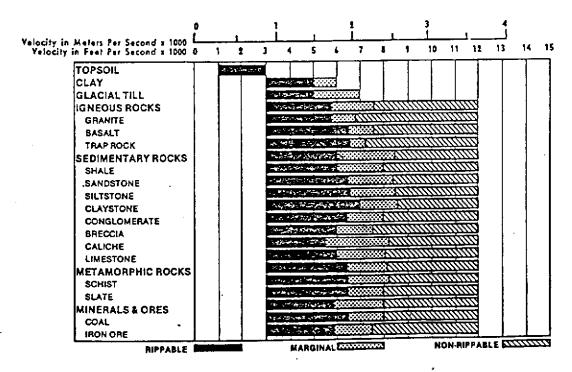
TELKWA COAL PROJECT

X² - T² ANALYSIS

D9H RIPPER PERFORMANCE ESTIMATED BY SEISMIC WAVE VELOCITIES Multi or Single Shank No. 9 Series D Ripper



D8K RIPPER PERFORMANCE ESTIMATED BY SEISMIC WAVE VELOCITIES Multi and Single Shank No. 8 Series D Ripper



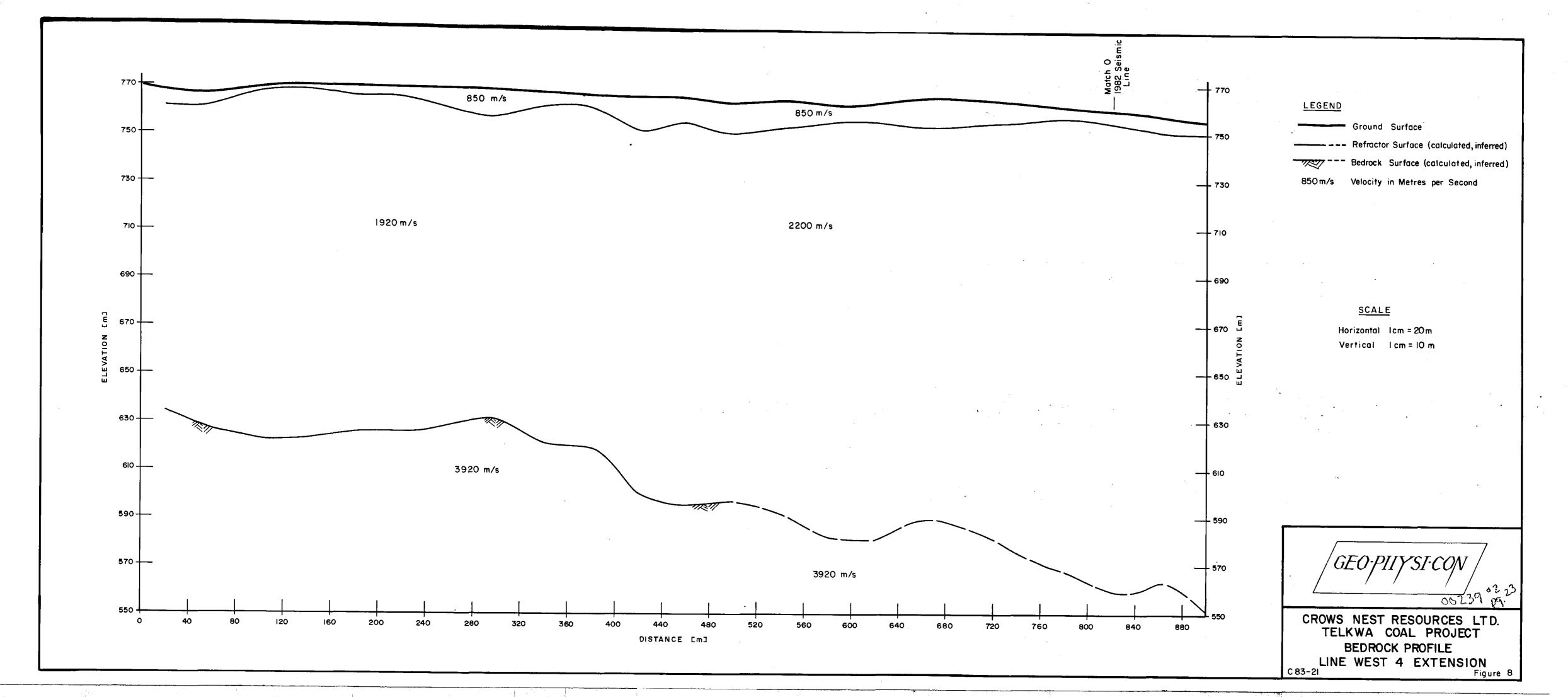
Reference: from Catipiller Performance Handbook

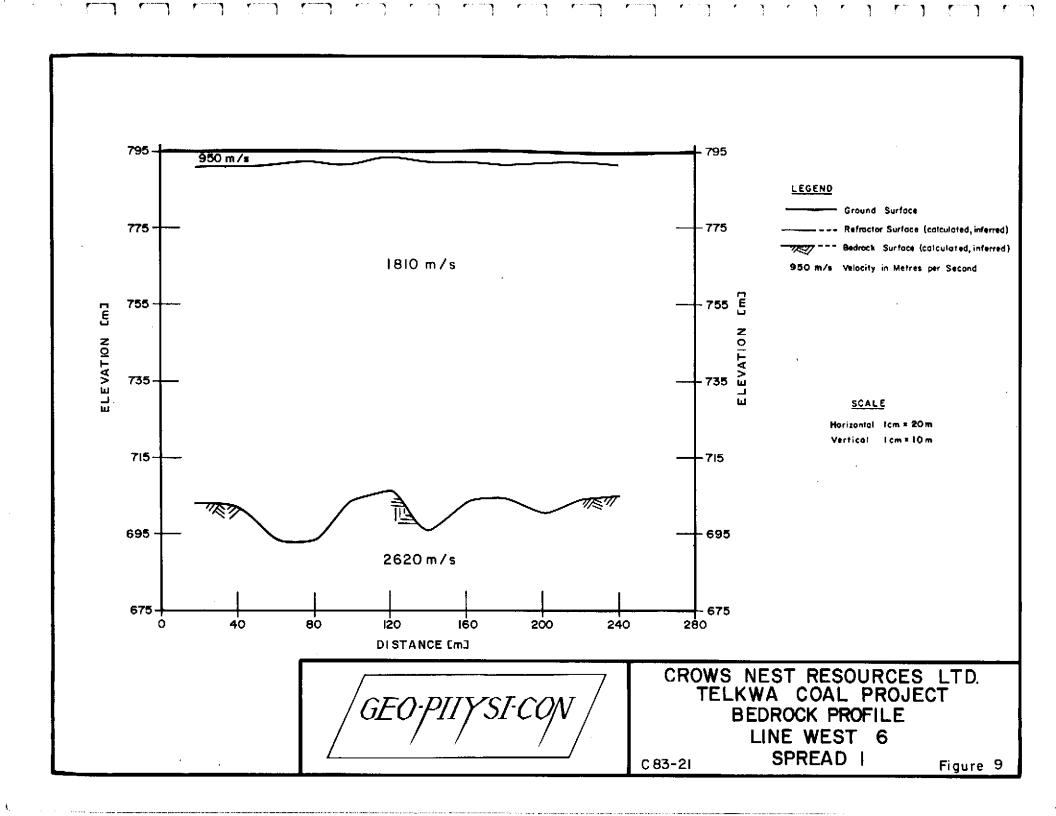
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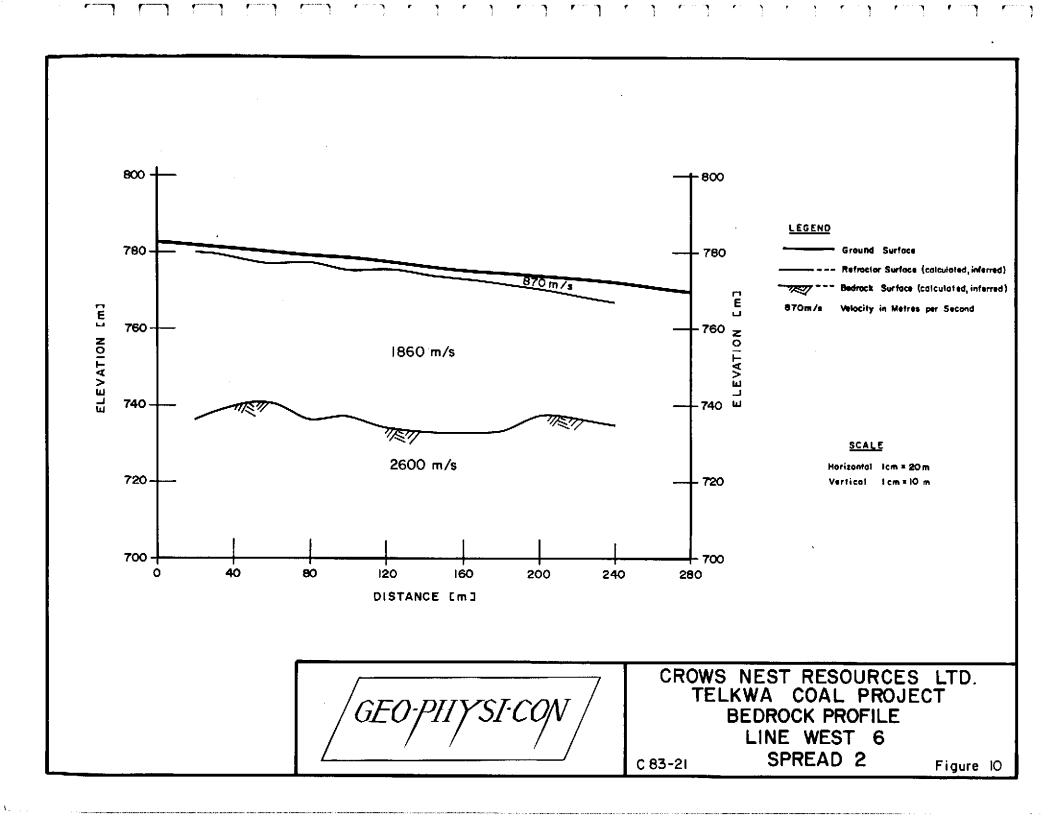
RIPPABILITY OF BEDROCK

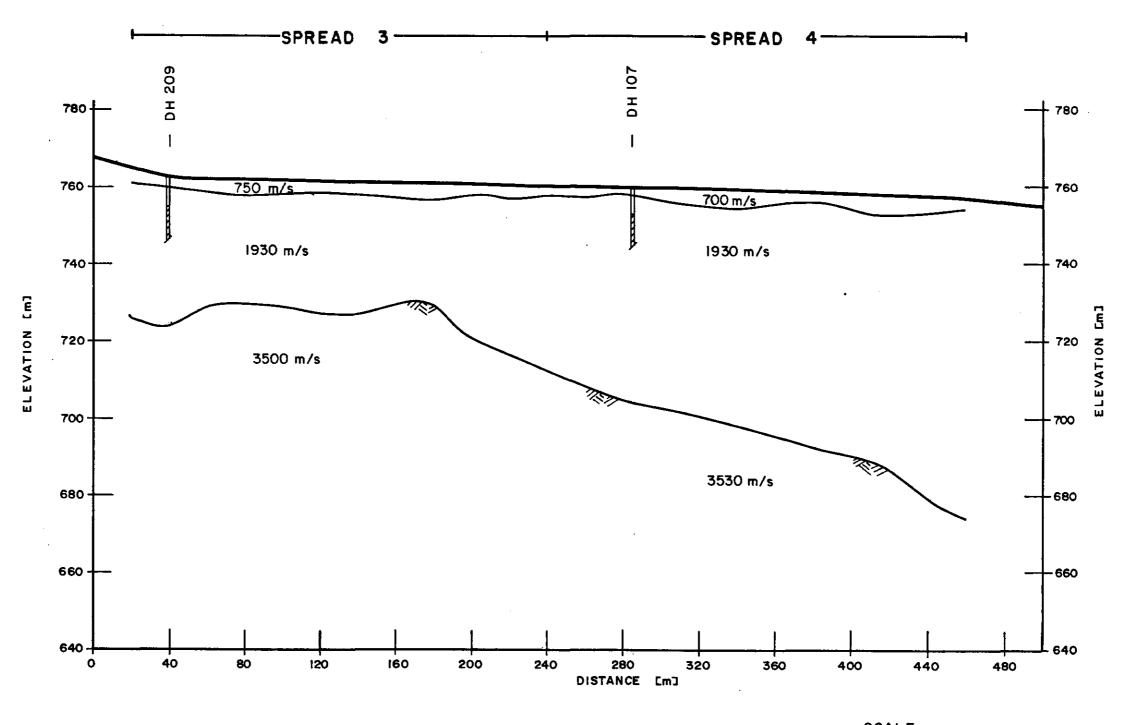
C83-21

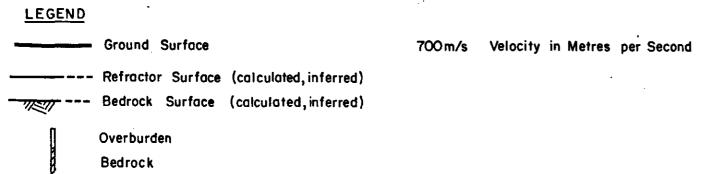
Figure 7











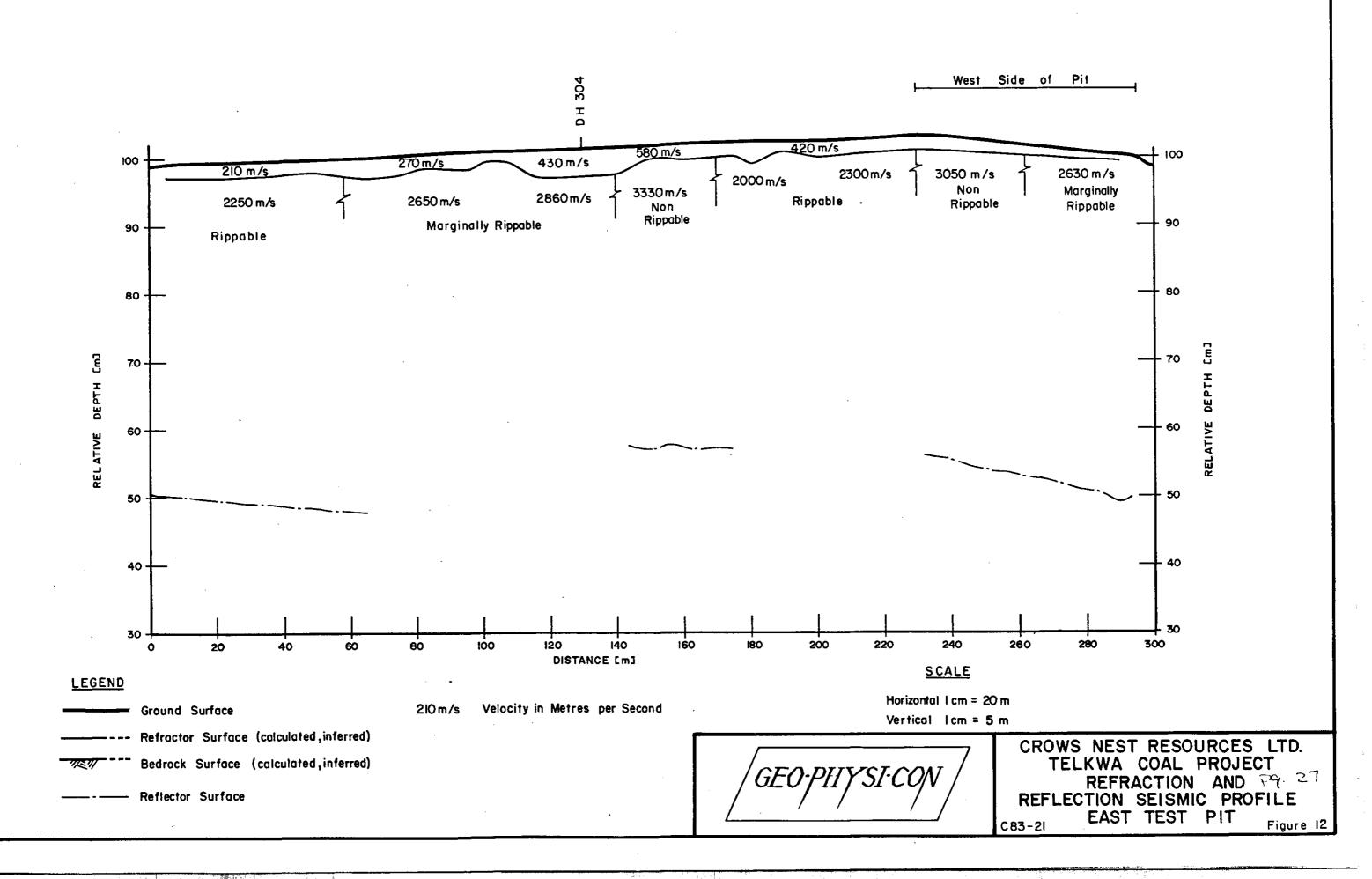
<u>SCALE</u>

Horizontal Icm = 20 m

Vertical Icm = 10 m

GEO-PHYSI-CON

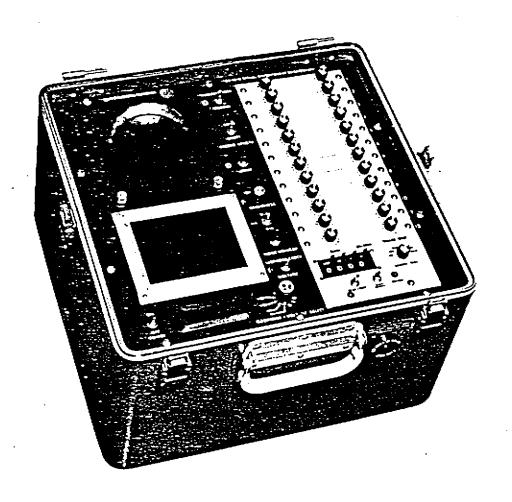
CROWS NEST RESOURCES LTD.
TELKWA COAL PROJECT
BEDROCK PROFILE 79.26
LINE WEST 6
C83-21 SPREADS 3 and 4 Figure II



geoMetrics/nimbus

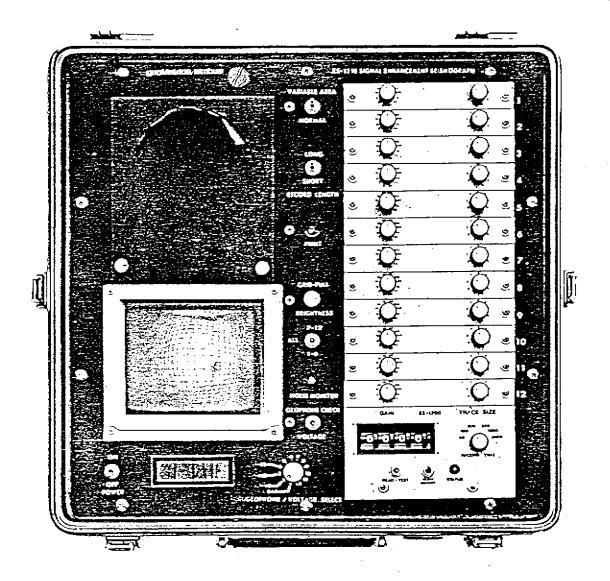
MULTICHANNEL SIGNAL ENHANCEMENT SEISMOGRAPH MODEL ES-1210

Preliminary Data Sheet



- * Signal enhancement for greater sensitivity, improved waveform definition, and more accurate time measurements. Operates under high noise conditions and surveys to greater depths without explosives.
- * Multichannel oscillograph provides permanent records on high-contrast, sunlight proof, reproducible paper with wiggle trace or variable area format.
- * Daylight-visible CRT monitor displays the signal stored in memory.
- * Compact, lightweight and portable. Ruggedly packaged in weatherproof case.
- * Optional digital magnetic tape recorder for computer compatible data storage.

The Nimbus ES-1210 Multichannel Signal Enhancement Seismograph is unique in its combination of CRT display, signal enhancement and oscillograph recording in a single small field instrument. Simple to use yet powerful in performance, this new instrument is ideally suited for all shallow geologic investigations for mining, construction and geologic exploration.



CONTROLS AND FEATURES

Amplifier (input) GAIN is controlled by a 12-position switch, selectable from relative gain of 1 to 5000 in steps of 1-2-5-10 etc. Each amplifier has a 10 bit by 1024 sample memory which stores the digitized signal. Playback gain is controlled over a 20 to 1 range by the TRACE SIZE control. Pulling up the trace size control freezes the memory on that particular channel so that it will not further enhance or erase, thus saving the data while allowing operation on the other channels. Playback or display are not affected by memory freeze.

Enhancement control electronics include the RECORD LENGTH control, which selects total time of the record among 50, 100, 200, 500, 1000 or 2000 milliseconds. The record DELAY postpones the start of the record up to 9.999 seconds in one milliseconds increments, allowing you to look later in time, delete unnecessary leading portions of the signal, and maintain faster sampling rates for later events. CLEAR MEMORY controls erases the data stored in the memory. An interlock is provided (both READ and CLEAR must be used) to prevent accidental erasure of valid data. TEST provides a start command to take a record in lieu of hammer switch or blaster.

Signal enhancement is a term used to describe the stacking process used in the ES-1210. The seismic signals for each hammer blow or shot are digitized and stored in a computer-like memory in the instrument. Unlike conventional analog seismographs, the record is not made at the instant of the hammer impact or explosion. Instead, it is held indefinitely and printed at the operator's convenience. If the impact or explosion is repeated, the seismograph will add the new signal and the old one, storing the sum back in the memory. As this process is repeated, the signal will grow larger and larger, thus enhancing its appearance on the display or oscillograph record. Seismic noise in the earth, which provides the most significant limitation in depth penetration, is random and does not add in the signal enhancement process at the same rate that the true signal does. As a result, surveys can be performed to about three times the depth that could be realized without enhancement using an equivalent energy source.

Signal enhancement is also a significant improvement in making shear wave velocity measurements. These types of surveys are important because of the dynamic parameters of foundations can be calculated from shear wave velocities, liquid saturation can be discriminated from other conditions with equivalent P-wave velocities, and shear strength can be estimated. The most reliable shear wave studies are made with mechanical sources, which means that signal enhancement is often a requirement.

Signal enhancement provides other, less obvious advantages, even when using explosive sources. Since the playback gain of the signal stored in memory is adjustable, there is less guess work involved in getting good records. Multiple copies can be made without reshooting the blast. Since the frequency response is not limited by galvanometers and paper speed, a higher time resolution is available, an important factor when working in high-velocity materials.

The signal stored in the memory is displayed on the built-in CRT monitor, and the display will have the same appearance as the paper record. A paper record can be made as often as necessary, at will, without disturbing the data stored in memory. The trace size control can be changed to optimize the record for an application. The gain may be set high for sharp breaks on the P-wave arrivals, and a hard copy made. Then the gain can be turned down for better shear waves or reflections and another copy made.

Both the CRT and oscillograph record in conventional wiggle trace and variable area. A wiggle trace record, like that of a conventional seismograph, would be selected for refraction and shear wave studies. Variable area recording (often seen on examples of petroleum reflection records) is best for reflection because that presentation emphasizes coherent events and resembles geologic structure.

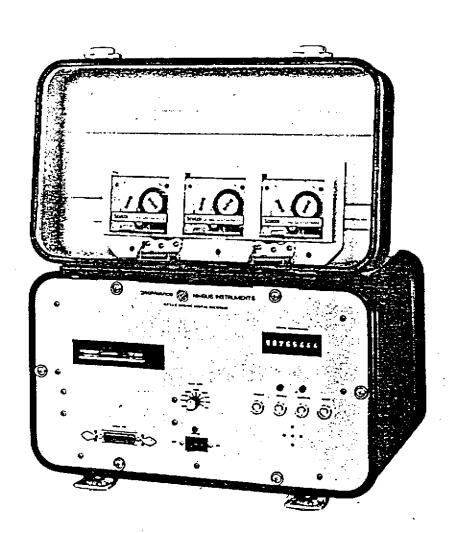
The CRT display is especially important in three other situations. When working in areas with significant background noise, the display gives an instant observation of the signal quality so that it is immediately known whether to repeat impacts, freeze specific channels, or erase and start over. The other use is in shallow reflections. The instant examination of all the channels simultaneously is important in recognizing these events in the record. The third use of the CRT display is in gain selection. With the NOISE MONITOR switch depressed real time signals are shown on the CRT and the gain setting for each channel can be chosen appropriately.

The CRT display is five inches (13 cm) diagonal measurement. It displays all 12 channels simultaneously or switch selected combinations of six channels as desired. It has a special light filter to allow direct viewing in sunlight without special hoods. The bezel will fit standard oscilloscope cameras so that photographs may be made of the display if desired. Timing lines may be superimposed on the CRT at will by pulling up on the BRIGHTNESS control. The timing line intervals vary, depending on the record length, so that appropriate resolution and clarity is maintained.

A digital voltmeter is provided to measure the battery voltage, internal power voltages, and individual geophone resistances. The NOISE MONITOR, when selected, couples the amplified geophone signals to the CRT display. This allows monitoring the instantaneous background noise so that records may be made during quiet periods.

The data stored in the memory may be accessed externally. An optional digital tape recorder, the G-724S, is available to provide computer compatible storage of the data. The G-724S will store 10 full records (120 channels) in a reduced resolution, 8-bit format, or you can store 5 records (60 channels) in the full 10-bit format. The G-724S serves as its own playback device, outputting the data in an RS-232 format which is directly interfaceable to most computers including desk top models.

G-724S Digital Recorder



Nimbus ES-1210

SPECIFICATIONS

Basic refraction and reflection system includes: 12-channel exploration seismograph, 12-volt battery pack, 110/220 volt charger, power cord, hammer switch, and instruction manual.

Signal Enhancement:

samples, digitizes, and stores signal in a random access memory. Repeated signals are added while random noise is cancelled or limited.

10 bits by 1024 words on each channel.

Sample Interval:

switch selectable 50, 100, 200, 500, 1000, or 2000 microseconds

Record Length:

Memory Size:

switch selectable 50, 100, 200, 500, 1000, or 2000 milliseconds

CRT Display:

5" diagonal measurement CRT, daylight visible without hoods, switch selectable time lines, camera compatible, and displays wiggle trace or variable area record display.

Oscillograph:

permanent record of all 12 channels simultaneously on 4" wide electrosensitive paper. Record will not fade in light, and reproduces on copying machines.

Noise Monitor:

ambient vibrations displayed on CRT allowing timing of energy source during quiescent periods and the optimization of gain adjustments.

Timing:

crystal controlled, .01% accurate, time lines are switch selectable on CRT and high or low resolution on oscillographic record.

Precision Delay:

postpones start of record up to 9.999 seconds in one millisecond increments.

Digital Meter:

indicates battery voltage, geophone resistance on each channel power supply voltages.

Digital Output:

a panel connector to allow digital recording of signal stored in memory on optional digital recorder Model G-724S.

Record Initiation:

by contact closure, saturated NPN transistor, or negative 5-volt pulse.

Standard Size/Weight: (seismograph)

14 X 15 X 15 inches (36 X 38 X 40 cm) lid closed

38 pounds (17 kg)

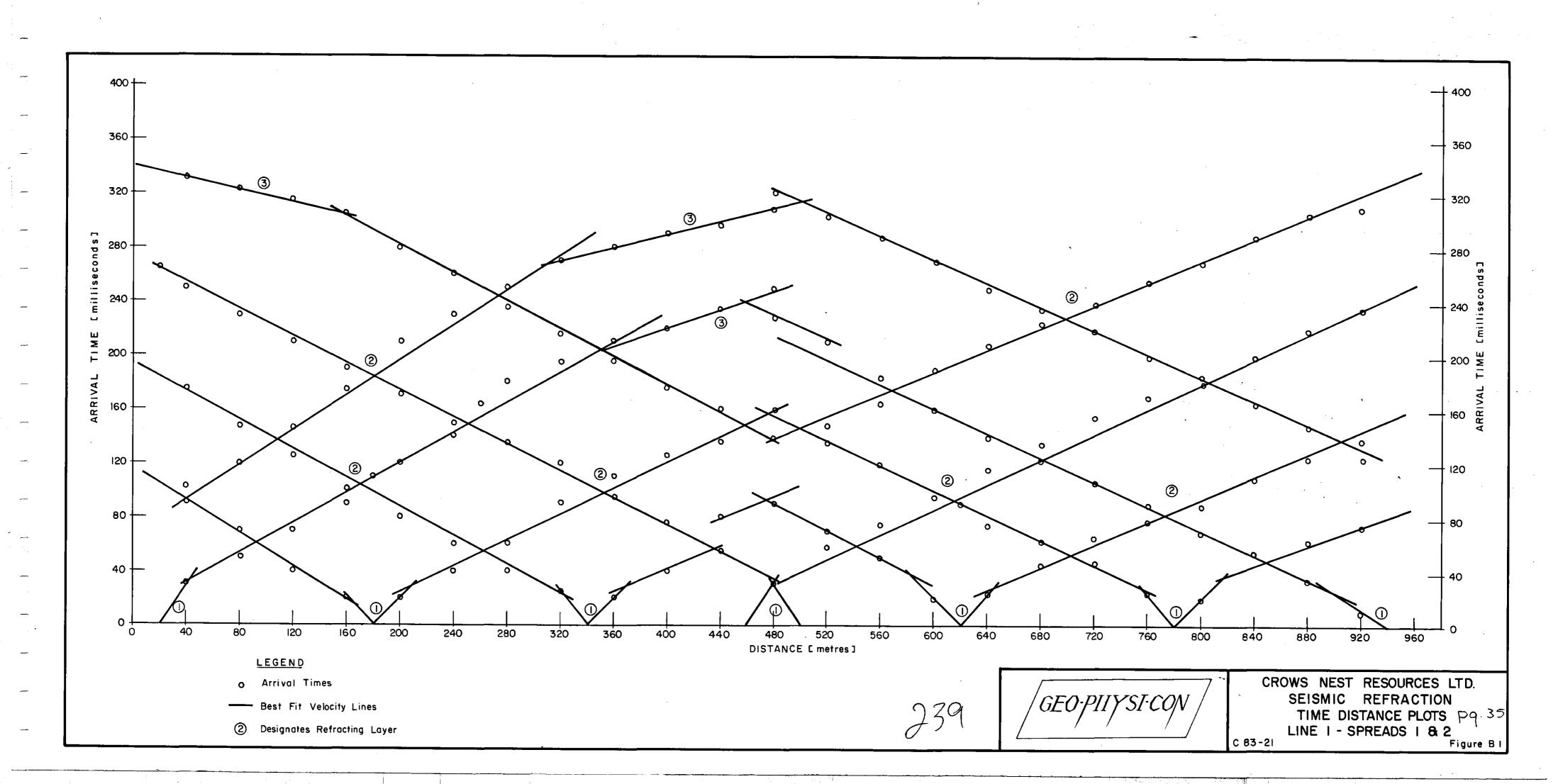
Power Requirements:

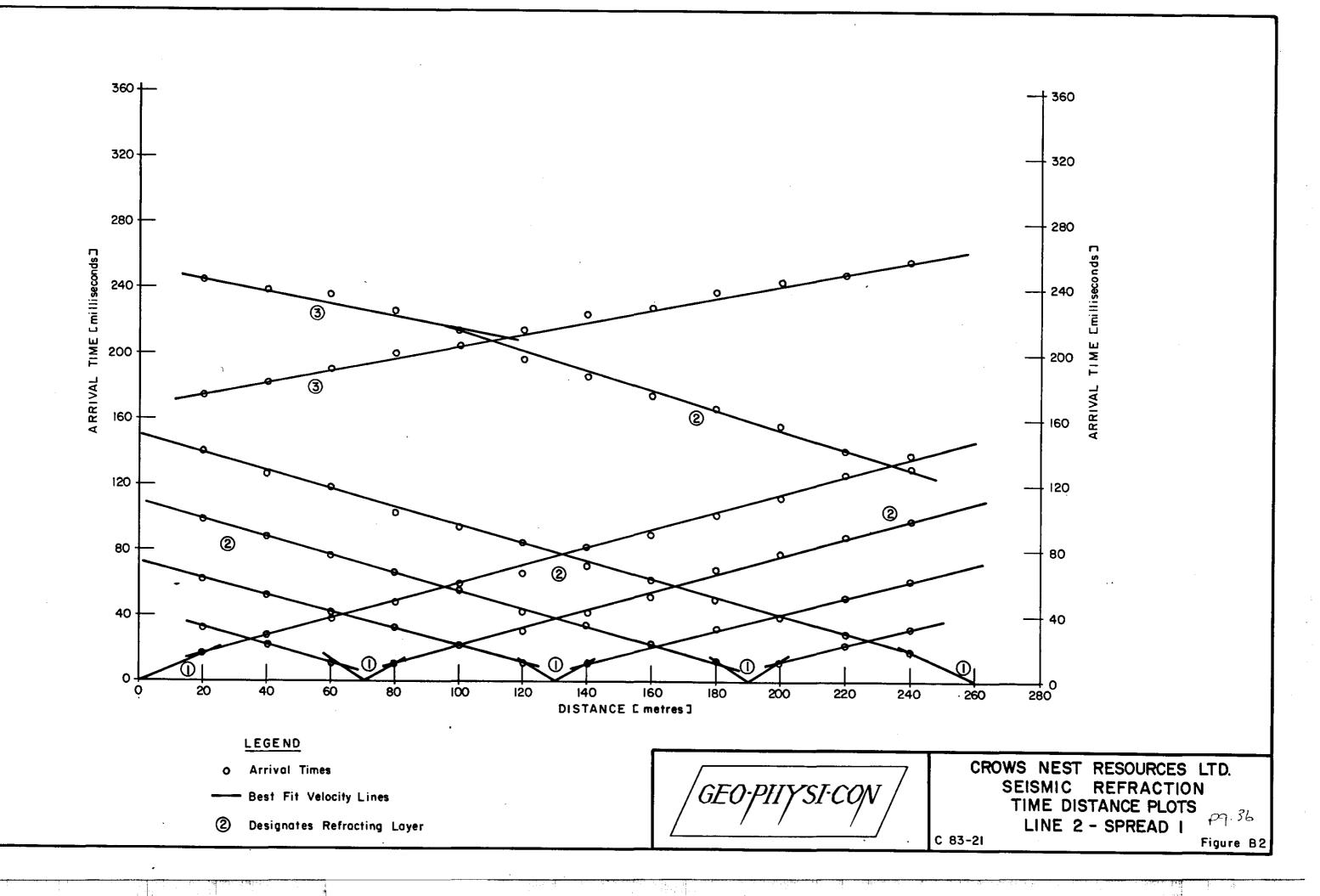
12 volts, 3.5 amperes

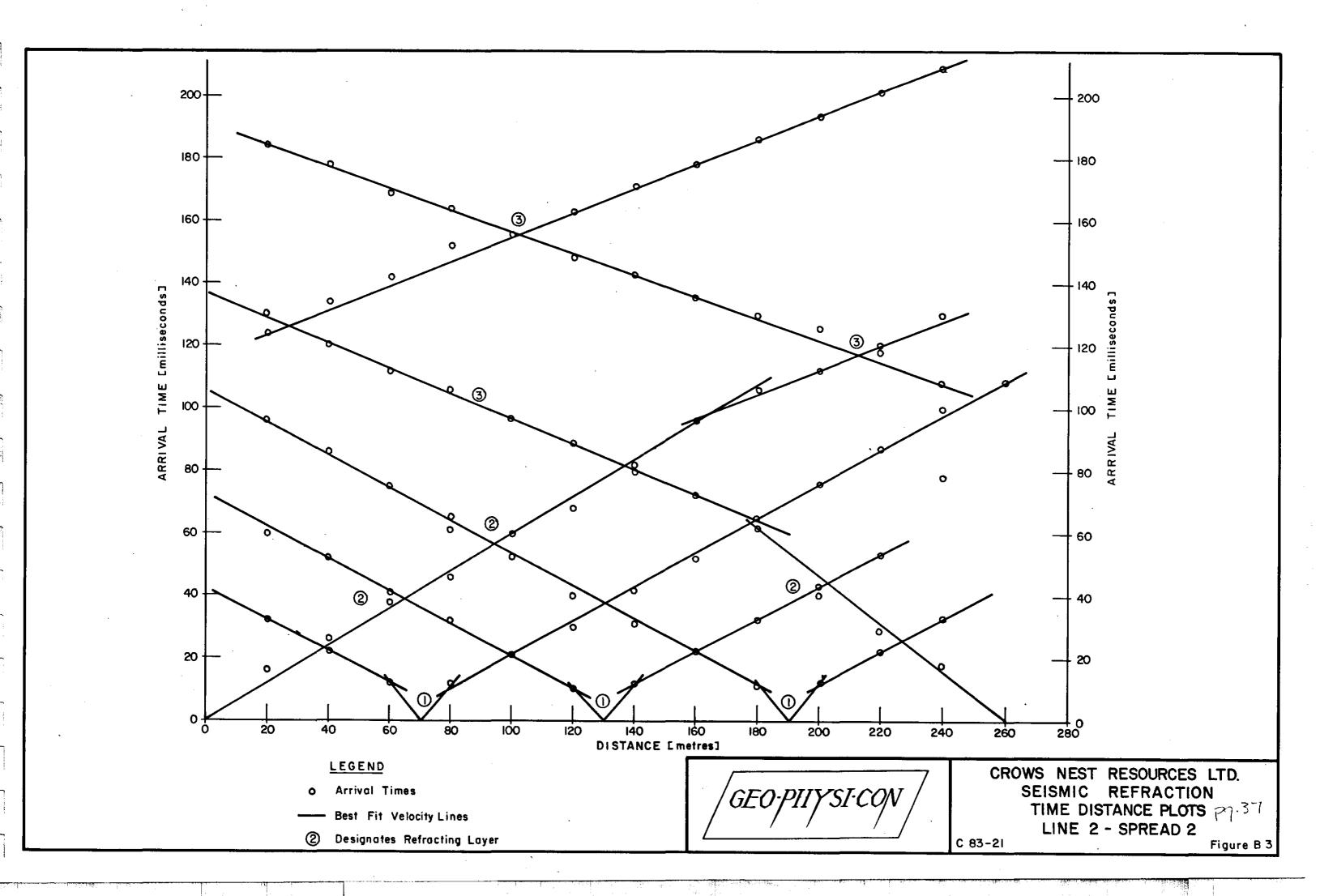
Seismograph Case:

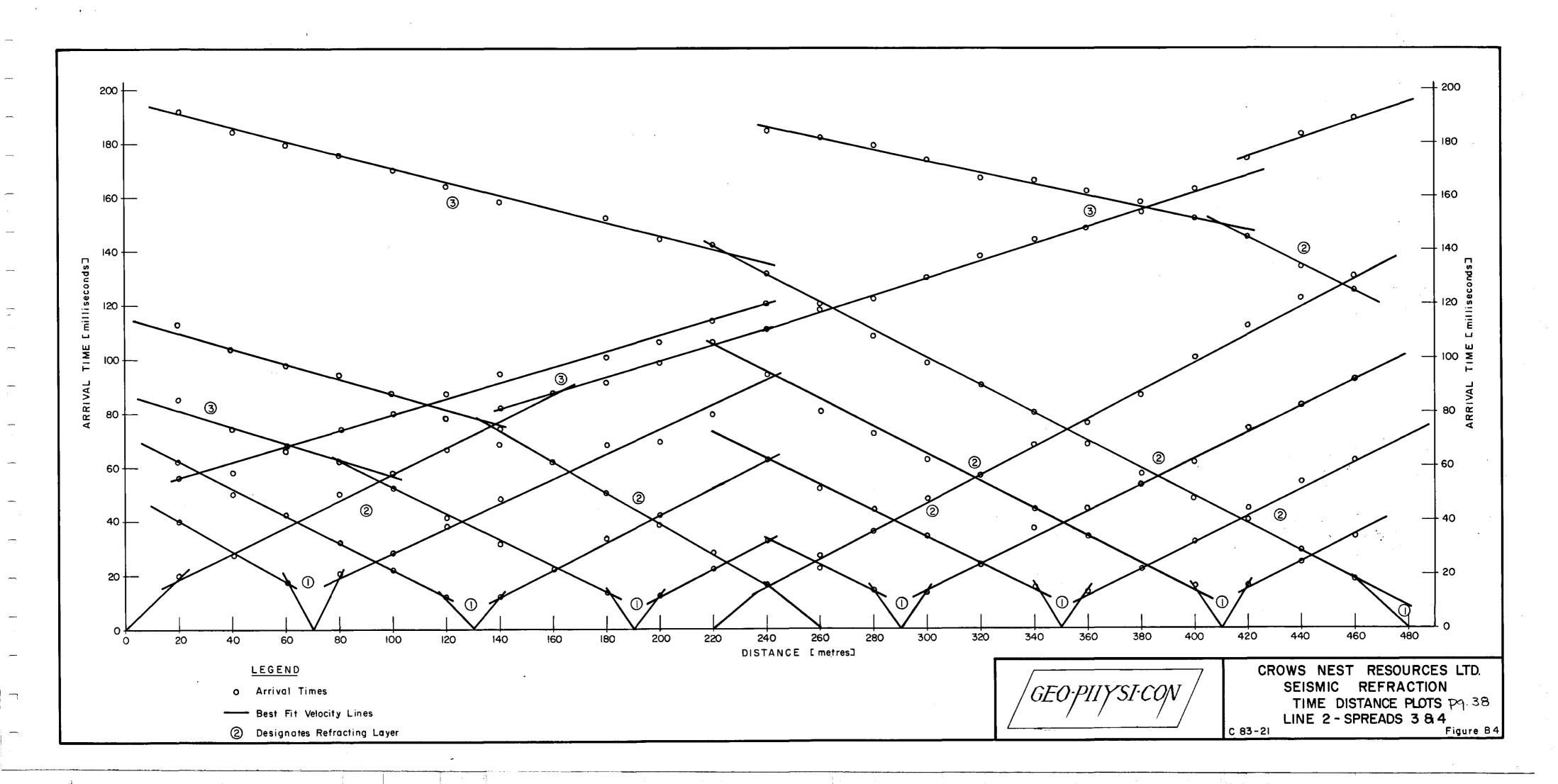
Heavy duty aluminum with lid and water tight seal.

GEOMETRICS, INC. 295 JAVA DRIVE SUNNYVALE, CA. 94086 U.S.A. TEL: (408) 734-4516 CABLE: "GEOMETRICS"









CONFIDENTIAL

GEOTECHNICAL CORE LOGS

LOCATION = TW83D-301

START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY		JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
4.57	32.8	.0	COAL						**	
	-		NTRK							
5.79	49.2	.0	COAL			6.			6.	
			MDST	15.	2.	4,			21.	
			NTRK			7.			21.	
8.23	52.5	6.2	MDST	19.	1.	1.	····		21.	
			SLTS		1.	• •			1.	
11.28	26.9	. 🗘	COAL	3.		35.			38.	
			MDST	6.		30.			36.	
14.33	92.6	25.9	COAL	8.	1.	23.			32.	
			MDST	12.	5.				17.	
16.76	85.2		COAL	5.	3.				8.	
17.37	85.6	56.4		3.	1.				4.	
			SLTS	19.	7.	3.	1-16-F		29.	
20.42	100.0		SLTS	24.	4.	10.			38.	
23.47	59.4	14.3	SLTS		4.	['] 75.			79,	
25.91	103.9		SLTS	31.	5.	20.			56.	
28.96	85.2	35.8		18.	7.	10.			. 35 .	
31.39	91.Q	63.9		10.	3.				13,	
32.61	99.6	45.6	COAL	21.	5.	70.			96.	
			MDST	13.	3.				16.	
			SLTS	´ 6 .		,			6.	
35.20	90.2	17.4	COAL	18.	1.	16.			35.	
			MDST	12.	15.	14.			41.	
38.25	101.6		MDST	25.	4.	11.		4.	44.	
41.30	102.5	40.0	COAL	7.	1.	2.			10.	
44 50	20.0	_	MDST			28.		20.	48.	
44.50	30.3		MDST			30.			30.	
46.48	53.3	.0	COAL			20.		<u></u>	20.	
47.70	97.5	04.4	MDST	6.	_			1.	7.	
50.90	97.5 95.1	34.1		16.	5.	27.			48	
53.95		59.3		3.		8.			11.	
57.00	97.4	61.3				9.		·	9.	1
60.05	99.0	77.4 72.0				27.			27	
63.09	101.3 100.0	72.0 56.4				17.			17.	
66.14	95.1		MDST			21.			21.	
99.14	99. l	73.8	SLTS			9.	··•	 	9.	
			SNDS			10.			10.	
69.19	100.3	92 A	SLTS	16.		10.			10.	
00.10	100.3	62.0	3613	10.		4.			20.	

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CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT Fractures	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
3.05	41.3	0.	NTRK			*				
····			SLTS	4.	1.	· · · · · · · · · · · · · · · · · · ·			5.	
5.18	87.5	40.3	SLTS	13.	10.				23.	
8.23	34.4	. 0	COAL	5.	2.				7.	
			NTRK						,.	
9.45	42.6	.0	COAL	6.	2.				8.	
10.06	73.6	16.5		3.					3.	
			OTHR		4.				4.	
10.97	94.1	20.3	CDAL	5.					5.	
			SLTS	15.	14.				29.	
14.02	90.1	73.6	SLTS	14.	7.	10.			31.	
17.1 6	94.5	54.7	MDST	7.	6.	3.			16.	
			SLTS	9.	10.				19.	
20.27	90.6	72.5	MDST							
			SLTS	15.	6.	. 8.			29.	
23.47	100.3	53.1	COAL	7.		10.			17,	
			MDST			11.			11.	
			SLTS	12.	4.				16.	
26.52	99.3	22.6	COAL	9.		8.			17.	
			MDST			34.			34.	
29.57	99.2	57.2								
			MDST	12.	7.				19.	
32.00	76.0	33.6					1			
			MDST	3.	15.	t.			19.	5
35.66	95.1	42.3	MDST	5.	2.	20.			27.	
38.71	99.7	78.0	MDST			, 13.			13.	
41.76	101.0	93.8	MDST			13.			13.	
44.81	94.1	77.6	MDST			10.			10.	

START OF CORE RUN	RECOVERY PERCENT	Ř.Q.D.	LITHOLOGY	BEDDING Fractures	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
7.62	7.1	٥.	SLTS			4.			4	
11.28	95.1	60.7	SLTS	6.	•				6.	· ~ · · · · · · · · · · · · · · · · · ·
11.89	96.7	40.0	COAL	4.	1.				5.	
12.19	89.3	48.6	COAL	12.	2.				14.	
			MDST	7.		2.			9.	
14.33	85.5	36.8	COAL	5.	1.			***	6.	
			MDST	48.	5.	3.			56.	
17.37	60. Q	6.6	MDST NTRK			21.			21.	
20.42	15.1	.0	MDST	6.	3.	**********			9.	
23.47	68.9	28.5	MDST	16.		13.			29.	
26.52	106.6	27.9	COAL	4.	4.	6.			14.	
			MDST			1			1.	
			SLTS	1.	3.	· · ·	······································		4.	
27.74	89.6	51.4	COAL	14.	7.				21.	
29.57	93.4	61.2	COAL	10.	6.				16.	
			MDST	9.	4.				13.	
32.61	91.8	78.4	SLTS	16.	9.	10.			35.	
35.66	94.1	76.1	SLTS	12.	9.	10			31.	
38.71	88.5	41.3	SLTS	12.	15.	4.			31.	
41.76	95.1	35,4	MDST			41.			41.	
44.81	75.7	41.4	MDST			43.	***************************************		43.	
47.85	83.3	50.2	MDST			21.			21.	

START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
5.18	62.0	.0		9.		15.			24.	
			MDST			21.			21.	
			SLTS			15.			15.	
7.92	67.2	. 0	COAL	6.	1.	10.			17.	
8.53	88.5	19.7	COAL	9.					9.	
9.14	101.4	67.3	COAL	7.			" "		7.	
			SLTS	12.	2.	1,	•		15.	
11.28	97.0	50.8	SNDS	10.	10.	7.			27.	
14.33	100.3	64.1	SNDS	10.	6.	8.			24.	
17.37	99.0	40.3	SLTS	22.	8.				30.	
			SŅDS	6.	1.				7.	
20.42	86.2	48.9	SLTS	13.		4.			17.	
			SNDS	6.	1.	25.			32.	
23.47	99.3	54.8	COAL	2.	4.				6.	
			SNDS	21.	7.	6,			34.	
26.52	94.9	35.Q	CDAL	6.	1.	•			7.	
			MDST	7,					7.	
27.89	85.7	41.1	CDAL		5.				5.	
			MDST	6.	2.				8.	
29.57	95.7	29.9	COAL	2.	2.				4,	
	•		MDST	31.	5.	3.			39.	
32.61	96.7	13.8	MDST			127.	"		127,	
35.66	82.0	21.3	COAL	5.	2.	2.			9.	
			MDST		3.	22.			25.	
38.71	68.Q	28.7	COAL	19.	5				24.	
39.93	92.3	46.4	COAL	7.	1.	1.			9.	
			MDST	9.	2.				11.	
41.76	83.6	20.3	MDST	26.	5.	33.			64.	
44.81	100.3	26.3	MDST			33.			33.	
47.85	79.3	44.6	· MDST			60.		7	60.	
50.90	101.6	31.1	MDST			48.			48.	
53.95	103.3	43.0	MDST			43.			43.	
57.00	93.4	70.8	MDST	10.	2.		•		12.	
			SNDS	3.	2.	8.	-		13.	

START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL Fractures	
. 55	100.0	.0	OTHR	· · · · · · · · · · · · · · · · · · ·		10.			10.	
		_	SLTS	9.	4.	15.			28.	
14.33	-1.0		NDAT							
14.93	14.8	.0	MDST			5.			5.	
			OTHR			. 40. 5.			40.	
16.76	23.4	10.0	COAL	3.	2.	5.		30.	40.	
17.37	40.Q	16.1				30.			30.	
			MDST		•	31.			31.	
20.42	88.5	36.4	MDST	9.	3.	9.			21.	
			SNDS			14.			14.	
23.47	4.9	.0	NTRK							
26.53	75.0	.0	MDST			59.			59.	
			NTRK							
29.57	5Q.Q	. 0	NTRK							
30.33	51.3	.0	MDST			14.			14.	
32.61	43.6	11.3	MDST			42.			42.	
35.3 6	92.7	60.3	COAL	10.		5.			15.	
			MDST	9,	1.	10.			20.	
			SNDS		2.	20.			22.	
38.53	83.2	38.2	COAL							
			MDST	8.					8.	
			SNDS	10.	4.				14.	
41.15	97.2	68.1	MDST		3.	23.			26.	
44.35	87.3	70.4	COAL							
			MDST			14.			14.	
47.73	93.2	38 3	COAL	30.	4.	1.		•••	35.	
50 84	95.8	41.2	COAL	21.		• •			21.	
			MDST	7.					7	
53.95	95.1	82.3	MDST	16.	3.				19.	

										
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY		JOINT FRACTURES		MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
8.23	59.2	.0	SNDS	4.					4.	
9.75	31.5	.0	COAL			8.	· · · · · · · · · · · · · · · · · · ·		ē.	
10.67	59.6		COAL			7.			7.	
			NTRK							
12.80	54.9	.0	SLTS	10.		10.			20.	
14.02	44.9	.0		10.		50.			60.	
16.45	66.1	10.4		13.	2.	36.			51.	
19.81	37.9		SLTS	10.		30.			40.	
23.16	37.6		COAL			60.			60.	
			SLTS	ā.	3.	30.	·····		41.	
26.52	98.4	42.6	COAL	2.			•		2.	
	•	,	MDST	17,	7.	•			24.	
			SNDS	5.	2.				7.	
29.57	90.1	10.5		11.	2,	45.			58.	
20.07			MDST	12.	1.	15.		5.	33.	
32.61	88.5	.n	COAL	13.	3.	20.		J .	36.	
V2.141	00.0		MDST	30.	1.	11.		1.	43.	
35.66	75.7	8 8	MDST	32.	37.	30.		6.	105.	
00.00	,	0.0	OTHR	OE.	07.			٠.	,00:	
38.71	66.6	0	COAL	17.	6.				23.	
30.71	00.0	.0	MDST	5.	٠.				5.	
	·		SNDS	7.					7.	
41.76	101.0	٥	SNDS	25.	7.	15.			47.	
44.81	97.0		SNDS	23.	7.	24.		20.	74.	
47.85	95.4		SLTS	20.	3.	6.		20.	9.	
47.00	30.4	31.1	SNDS	25.	5.	12.			42.	1.78 t - 0.72444.7-E - 1.48
50.90	101.0	50 2	NDAT	23.	1.	1			1.	
50.90	101.0	30.2	NTRK							
			SLTS	5.	1.				6.	
			SNDS	15.	3.	50.			68.	
53.95	101.0	64.5		24.	1.	50. 5.				
57,00	90.8	64.6	SNDS COAL	16.	1.	10.			30. 26.	
37.00	3U.0	41.3	SLTS	10.	1.	10.			1.	
			SNDS	9.	3.		•		12.	
60.05	89.1	16.4	COAL	9.	3. 1.					
60.05	09.1	10.4		9.	1.	34.			10.	
E2 00	04.6	^	MDST MDST			34. 15.		6.	. 34.	
63.09	91.6 77.0	.0	COAL	9.	1.	15.		<u> </u>	<u>21.</u> 16.	
65.84	11.0	.0			1. 5.	= -				
co es	50 6	~	MDST	11.		28.			44.	
68.88	59.6	.0	COAL	14.	1.	12.		E ^	27.	
71.00	67.7		MDST	8.	<u>2</u> .			53.	63.	
71.63	81.7	33.3	COAL	7.					8.	
75 00	00.7	25 4	MOST	22.	5.				27.	
75.29	99.7	08.4	MDST	19.	1.				20.	
			NDAT	· · · · · · · · · · · · · · · · · · ·	<u> </u>	6.			7.	
78.33	98.0	14.4	NDAT	23.	2.				25.	•

LOCATION - TW83D-307

				LUCAT	10N - 18830	1-307				•
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY		JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	···
6.40	97.3	.0	MDST	15.	5.			••••	20	
			OTHR		<u>-</u> -	10.			20. 10.	
8.23	90.5	.0	MDST			28.			28.	
11.28	70.7		MDST			42.			42.	
14.32	83.9		MDST			5.			5.	
			SNDS			54.			54.	
20.42	96.7	21.3	COAL	7.		10.			17.	
			SLTS	12.	2.	•			14.	
			SNDS			17.			17.	
23.47	100.0	.0	CDAL	2.		3.			5.	
			SNDS	35.	3.	4.			42.	
26.52	88.5	10.2	SNDS	31.	3.	43.		1.	70.	
29.56	77.9	32.4	MDST			5.		30.	35.	
			SNDS	8.	2.	10.		3.	23.	
32.00	88.7	.0	COAL	6.		5.			11.	
			MDST	12.	1.				13.	
			SLTS	9.		3.		1.	13.	
34.42	71.0		COAL			25.			25.	
34.75	86.7	.0	CDAL			25.			25.	
35.05	92.2	۰.0	COAL	12.		1.			13.	
			MDST			70.			70.	
37.49	80.6		COAL	9.		4.			13.	
37.60	78.3		COAL	9.		15.			24.	
38.40	93.5		COAL	8.					8.	
38.71	52.5		COAL		1.	9			1.	
39.32	97.7	0	COAL	7.		10.			17.	
			SLTS	25.	2.				27.	
41.45	98.7		MDST	42.	5.				47.	
44.50	100.3	9.5	MDST	23.	3.	8.			34.	
			SNDS	10.	2.				12.	
47.55	99.3	35.4	SLTS	29.	4.	4.			37.	
			SNDS	2.					2.	
50.59	88.9	12.8	MDST	22.	<u>4.</u>	23.			49.	
50.04	00.5	_	SLTS	3.	3.	3.			9.	
53.64	96.7	.0	COAL	2.	•				2.	
54.65	67.4		MDST	20.				9.	29.	
54.86	67.4		COAL	6.	· · · · · · · · · · · · · · · · · · ·	15.			21.	
55.32	100.0	.0	CDAL		_	32.			32.	
E6 50	80.0	^	MDST	9.	3.	2.		100.	114.	
56.59	83.6	.0	SLTS	8.	3.				11.	
E0 E0	77-7		SNDS	6.	6.				12.	
58.52	77.0	.0	CBSH	5.			2.		7.	
E0 40	60.5	_	COAL		1.	45.			46.	
59.13	62.3	.0	CBSH			3.			3.	
. 60 74	46 4		COAL							
59.74	45.7	.0	CBSH			1.			1.	

START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
59.74	45.7	.0	COAL			50.			50.	
60.20	56.8	.0	COAL	25.	1.	200.			226.	
			MDST	13.	1. '	3.		100.	117.	
62.79	98.7	.0	MDST		2.	28.		99.	129.	
65.84	99.3	34.5	MDST	4,		2.		4.	10.	
68.88	93.4	56.4	MDST	31.	1.	3.		8.	43.	
71.93	81.6	26.6	COAL	22.		3.			25.	
			MDST	14.		6.		10.	30.	
74.98	75.0	.0	COAL	19.	1.	10.			30.	
			MDST			3.			3.	
			NTRK					100.	100.	
77.42	69.7	.0	COAL	10.				25.	35.	
			MDST	11.	3.			53.	67.	
	•		NTRK					1.	i.	
79.86	76.2	16.4	COAL	5.					5.	
			MDST	11.			•	6.	17.	
81.08	86.9	10.9	MDST	6.				31.	37.	<u> </u>
			SNDS	20.	7.	20.			47.	
83.82	89.0	6.3	COAL	4.		15.			19.	
			MDST			•		50.	50.	
			SNDS	25.	6.				31.	
87.17	23.0	.0	COAL					1020.	1020.	
90.22	100.0	٥.	COAL	35.		•			35.	
			MDST	20.	3.				23.	
91.13	88.3	.0	COAL	7.		6.			13.	
			MDST	4.		10.		57.	71.	
93.27	77.0	۰.	COAL	4.		25.			29.	·
			MDST	15.		13.		5.	33.	
96.32	101.3	27.0	MDST	16,	3.				19.	
			SLTS	28.	3.				31.	
99.36	87.7	34.4		49.	15.	14.		3Q.	108.	
105.46	100.0	27.9	MDST			12.		14.	26.	
108.51	100.0	52.5	MDST			16.			16.	

				LOCAT	ION = TW83D	-308				
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY		JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
11.28	6.6	.0	NTRK			25.			25.	
12.80	50.0	.0	SNDS			, 63.			63.	
14.32	77.2	_	SLTS	10.		, 63.				
15.24	110.0		COAL	3.	٥				10.	
13.24	110.0	70.0	SLTS	3.	2.				5.	
15.54	98.9	78.7							3.	
15.54	38.9	38.3		8.	1.				9.	
			MDST	_		25.			25.	
45 55			SLTS	7.	4.	2.			13.	
<u>17.37</u>	96.7	20.3	SNDS	25.	3.	32.			60.	
20.42	86.3	10.9	CBSH			5.			5.	
			MDST	29.		1.			30.	
			SNDS	2.		-			2.	
22.25	101.6		COAL	9.	2.				11.	
22.86	86,5	.0	CDAL	14.	3.				17.	
			MDST	27.		16.			43.	
25.60	124.6	77.O	COAL	8.					8.	
26.21	87.0	37.0	COAL	6.					6.	
26.67	103.3	63.9	CDAL	8.					8.	
. 27.28	93.9	50.9	COAL	7.	1.				8.	
			MDST	15.	. 1.				16.	
29.56	96.1	40.0	MDST	33.	1.	1.			35.	
32.61	95.7	52.1	MDST	27.	2.	iż.			41.	
35.66	100.0	16.4		10.	1.	, _ ,			11.	•
			SLTS	31.	3.	37.			71.	
38.71	93.8	0	MDST	16.	2.	10.			28.	
	20.0	<u>.</u>	SLTS	17.		8.				
41.76	97.4	32.6		42.	6.	†.			30.	
44.80	88.5	23.0			5. 5.				49.	
-		_	_	22.		16.			43.	
47.85	108.7		CDAL	16.	3.				19.	· ·
48.77	68,1	11.7	COAL	3.	1.				4.	
			MDST	7.				57.	64.	
50.90	90.2	10.2	COAL	16.	11.				27.	
			MDST	22.	<u>5.</u>				2 7.	
53.95	99.Q	. 0	-	45.	5.				50.	
57.00	88.5	17.4		4.					4.	
			MDST	15.	2.			50.	67.	
			SNDS	10.	5.	3.			18.	
60.04	88.3	. 0	COAL	10.	1.	1.			12.	
			MDST	5.			1.	50.	56.	
60.81	55.3	12.4	COAL	16.	4.	17.			37.	
63.09	60.0	.0	COAL	2.	3.			25.	30.	
			MDST	100.	3.			103.	206.	
			NTRK					.00.	200.	
66.14	74.4	.0	MDST	15.				16.	31,	
00.17	, , , , ¬	. 0	NTRK					10.	31,	
69.19	37.7		MDST	50.				23.	73.	
J. 15	31.7	.0	D.J. i	50.				∠3.	15.	

LOCATION = TW83D-308

TART OF ORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
72.24	65.Q	-0	COAL					25.	25.	
, 2.2.			MDST	25.				22.	47.	
74.07	63.6	- 0	CDAL	4.				64,	68.	
75.28	51.6	.0	COAL	2.				21.	23.	
75.90	86.4	.0	CDAL	2.				50.	52.	
			MDST					17.	17.	
78.33	58.7	11,1	COAL	2.				15.	17.	
			MD\$T			5.		9.	14.	
81.38	80.0	,0	COAL	3.					3.	
			MDST	15.				60.	75.	
			SNDS	22.					22.	
84.43	92.1	43.3	COAL	15.	2.	10.			27.	
			MDST	16.	2.				18.	
87.48	99.0	56.9	COAL	6.					6.	
			MDST	23.					23.	
90.52	98.0	63.3	MDST	32.					32.	

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START OF	RECOVERY	R.Q.D.	LITHOLOGY	BEDDING	JÖÏNŤ	UNCLASSIFIED	MINDR FAULT	FAULT ZONE	TOTAL	
CORE RUN	PERCENT				FRACTURES		FRACTURES	FRACTURES	FRACTURES	
8.84	79.1	.0	COAL	6.		6.			12.	
			MDST			7.			7.	
9.75	69.3	.0	COAL	5.	1_	6.			12.	
			MDST			33.			33.	
11.28	73.8	.0	COAL	Э.	1.				4.	
			MD\$T	4.	1.	9.			14.	
13.11	82.6	.0	COAL	3.		8.			11.	
			MDST	4.	1.	7.			12.	
14.32	46.8	.0.	MDST	3					3.	
			NTRK							
14.94	37.9		MDST	18.	2.	25.			45.	
17.37	33.5		MDST	15.	3.	8.			2 6 .	
20.12	73.3	14.0	COAL	4.	 				6.	
			MDST	31.	4.	251.			286.	
24.69	82.9		COAL	8.	3.				11.	
25.45	61.5		CDAL	12.	2.	15.			29.	
26.36	77.6	.0	COAL	8.	3,	10.			21.	
28 50	60.6		MD5T	5 .	8.				14.	
28.50	69.6		COAL	7.	2.				9.	
28.96	95.6	42.5	COAL	4.	2.	_			6.	
			MDST SLTS	8	ā.	5.			13.	
32.16	00 =	59.1		12.		30.			45.	
35.51	92.5 91.2		SLTS SLTS	24. 32.	2. 9.	20. 6.			46.	
38.71	96.7		SLTS	25.	9. 5.	300.			47.	
40.54	95.9	54.1	SNDS	9.		10.			330. 21.	
41.76	77. 6	45.1	SNDS	16,	2.	10.			28.	
44.80	88.9		COAL	10.	2.	10.			12.	
77100	00.0		SNDS	7.					7.	
46.33	91.4	40.8	COAL	6.	4.				10.	
-0.00	3,,,	-0.0	MDST	š.	2.	6.			16.	
47.85	79.4	-0	COAL	10.	5.				15.	
		- •	MDST	5.	6 .				11.	
49.99	98.6	33.8	CDAL	3.	1.				4.	
			MDST	14.	7.				21.	
52.121	90.7	32.2		14.	4.	25.			43.	
53.95	92.3	42.1	MDST	15.	1.	59.			75.	
55.78	40.2	.0	COAL	2.		3.			5.	
			MDST	2.		40.			42.	
57.00	11.2	.0	COAL			50.			50.	
60.04	74.2	.0		4.	1				5.	
60.66	68.7	. 0		6.	4.	32.			42.	
			MDST	8.	1.	25.		25.	59.	
62.48	84.6	15.4	MDST			102.			102.	
			SLTS	33.	8.	20.			61.	
65.99	92.8	.0	MDST			18.			18	

				LOCAT	ION = TW830	1-310				
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES		MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
9,14	83.6	.0	COAL	4.	1.				5.	
			SLTS	6,	1.	· · · · · · · · · · · · · · · · ·			7.	
9.75	63.9	.0	COAL	8.		20.			28.	
10.36	70.5	22.5		15.	3.	45.			63.	
12.80	97.4	28.9	SNDS	21.	1.	13.			35.	
14.32	85.2	۰.0	MDST	16.	8.	35.			59.	
			SNDS	5.	1.	10.			16.	
17.37	80.3	45.9	CDAL	2.					2.	
			MDST	3.	1.				4.	
17.98	71.1		COAL	4.	2.				6.	
18.74	85,8	.0	CDAL	4.	3.	15.	•		22.	
20.42	83.6	^	MDST COAL	18. 3.	2.	20.			40.	
20.42	63.5	<u></u>	MDST						3. 6.	
21.03	100.0	. 0		6.		25.			31,	
21.49	82.2	48.9		5.		25.			5.	
21.94	88.5	54.1	COAL	3.	2.				5. 5.	
22.55	148.4	67.7	COAL	8.					8.	
22.86	70.5		COAL	3.					3.	
			MDST	19.	4.	25.			48.	
25.66	83.6	43.0	MDS1	12.			10.		22.	
			SNDS	11.	3.	10.			24.	
25.91	71.8	38.1		25.	1.	9.			35.	
29.56	99.7	49.8	MDST	7,	•	3.			10.	
			SLTS	6.	3.				9.	
			SND5	14.	_				.14.	
32.61	91.5		SNDS	20.	3.	7 .			30.	
38.71	96.1	46.9	COAL	7.					7.	
42.06	00.4	77 0	MDST	25. 5.	4.	9.		20.	58.	
42.06	98.4 98.6	-	CDAL CDAL	ວ. 8.	1.	6.			5.	
42.07	50.0	12.2	MDST	4.	18.	υ,	25.		15. 47.	
44.80	85.8	40.7	_	9.	1.	14.	25.		24.	
47.00		70.1	SNDS	12,		2.			14.	
47.55	90.2	.0	COAL	14.	4.	۷.			18.	
,,	33.2		MDST	9.	5.	17.			31.	
49.38	91.4	.0	COAL	13.	ž.	12.			27.	
			MDST			11.			11,	
50.90	68.O	.0	COAL	15.				212.	227.	
52.12	30.6	.0	COAL	6.	2.	50.		6.	64.	
53.95	85.6	.0	COAL	<u>4</u> .		25.			30.	
			MDST	8.	4.	31.			43.	
_			SNDS	11.	5.	7.			23.	
57.00	91.8		SNDS	31.	22.	6.			59.	
60.04	101.6			32.	22.				54.	
63.09	76.7	.0	SNDS	24.	Ž,	30.			56.	

LOCATION = TW83D-310

TART DF DRE RUN	RECOVERY PERCENT	Ŕ,Q,Ď,	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
66.14	97.4	13.4	SLTS	14	2.				16.	
			SND\$	28.	3.	4.			35.	
69.19	40.3	.0	MDST	6.		200.		1.	207.	
			SNDS	7.	3.	34.			44.	
72.24	90.0	.0	COAL	10.	3.	2.			15.	
72.54	82.1	.0	MDST	39.	5.	65.	· · · · · · · · · · · · · · · · · · ·	6.	115.	
75.28	68.9	. 0	COAL	6.					6.	
			MDST	34.	7.			4.	45.	
78.33	24.6	.0	COAL					500.	500.	
79.55	76.5	9.3	COAL	25.	4.				29.	
			MOST	7.				26.	33.	
81.38	101.0	43.3	COAL	1.					1.	
			MDST	36.	1.				37.	
84.43	103.0	63.9	MDST	28.	Ž.		• •		30.	
87.48	98.7	92.1	MDST	16.					16.	

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LOCATION = TW83D-311

START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LÍTHÖLÖĞŸ	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
					·					
3.05	55.4	.0	SLTS	10.	1	16.			27.	
5.18	69.8	7.5	SND\$	35,	3,	9.			47.	
8.23	70.1	.0	MDST	9.		42.			51.	
			SNDS	15.	2.	4,			21.	
10.67	60.7	. 0	MDST	9.	3.	50.			62.	
11.89	75.4	.0	COAL	9.		5.			14.	
12.50	83.0	. 0	COAL	5.	1.				6.	
			MDST	31.	2.				33.	
14.32	33,6	.0	COAL	4.	3.	10.			17.	
15,54	27.9	.0	COAL	12.	2.	8.			22.	
17.37	19.1	.0	CDAL	9.	1.	15.			25.	
19.20	54.1	.0	COAL	4.	6.	15.			25.	
			MDST	6.				7.	13,	
20.42	86.2	23.0	MDST	36.	3.	24.			63.	

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START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
4.27	92,3	.0	DTHR	~~~~~~		10.	*		10.	
			SLTS	iā.	4.	101			17.	
5.18	40.3	5.9	SLTS	14.	i -	10.			25.	
8.23	30.5	.0	SNDS	10.	3.	15.			28.	
11.28	36.1	.0	SLTS	13.	4.	101.			114.	
14.33	45.1	. 0	SLTS	13.					13.	
16.15	38.5	.0	SLTS	4,		50.			54.	
17.37	41.3	4.9	CDAL	5,	1.				6.	
			MDST	9.	t.				10.	
		· ·	SLT5	<u>9</u> .					9.	
20.42	92.5	4.9	COAL	6.	3.				9.	
			MDST	34.	15.	10.			59.	
23.47	98.4	34.4	COAL	4,	1.				5.	
			MDST	37.	4.				41.	
26.52	87.9	.0	COAL	10.	1.				11.	
			MDST	38.	12.				50.	
29.57	34.8	. 0	MDST	16,	7.	25.			48.	
32.61	94.8	17.4	COAL	1.					1.	
			MDST	34.	5.	3.			42.	
35.66	93.1	28.9	MDST	27.	4.	13.			44.	
38.71	95.7	22.0	MDST	20.	2.	22.			44.	
41.76	94.2	22.0	MDST			33.			33.	
44.81	91.4	22.7	MDST			29.			29.	
47.85	87.2	27.2	MDST			27.			27.	
50.90	99.3	31.8	MDST			60.			60.	
53.95	109.9	17.9	MDST			81.			81.	
56.69	93.5	35.6	MDST			42.			42.	
			SNDS			3.			3.	

LOCATION = TW83D-313

				LOCAT	.ION = 1M83C	0-313				
START OF CORE RUN		R.O.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TÓTÁL FRACTURES	
6.70	38.7	.0	COAL	6.		6.			12.	
7.32	56.7	.0		6	1.	4.			11.	
7.92	60.8	Ö.	CDAL	6.	1.				7.	
			MD5T			36.			36.	
9.45	75.4	.0	COAL	4.		10.			14.	
			MDST			7,			7.	
10.06	77.0	٠.0	COAL	10.	1.	. 25.			36.	
10.67	68.9	.0	COAL	10.		7.			17.	
11.28	50.7	.0	COAL	6.	1.				7.	
			MDST	7.	4.	53.			64.	
14.32	32.8	.0	MDST	14.	1.	49.			64.	
17.37	96.1	.0	COAL	2.		6.			8.	
			MDST	8.	5.	15.			28.	
18.14	58.8	.0	COAL	10.	1.	31.	•		42.	
20.42	83.6	4.3	COAL	6.	4.				10.	
			MDST			45.			45.	
			SND\$	10.	1.				11.	
23.47	92.1	25.2	SNDS	19.	8.	10.			37.	
26.52	94.1	18.7	SNDS	14.	7.	6.			27.	
29.56	82.3	20.7	MDST			59.			59.	
			SNDS	9.	4.	5.			18.	
32.61	104.6	.0	MDST			20.			20.	
			SNDS	9.		25.			34.	
35.66	28.2	.0	COAL	5.		10.			15.	
			MDST			112.			112.	
38.71	16.4	.0	-					103.	103.	
40.54	91.8	.0				19.			19.	
41.76	36.7	.0	COAL	2					2.	
			MDST			25,		46.	71.	
44.80	24.2		MDST			25.			25.	
45.42	21.7		COAL			25.			25.	
46.02	30. 6	.0	COAL		•					
			MDST			<u>6</u> .			<u>6</u> .	
47.85	94.1		MDST			24.			24.	
50.90	98.0	.0	COAL			20.			20.	
	_		MDST			18.			18.	
52.42	43.8	.0	· COAL	3.	1	20.			24.	
		_	MDST			10.			10.	
53,95	64.8	.0	COAL	6.		2.		10.	18.	
		_	MDST			1 <u>1</u> .	•		11.	
55.17	79.8		COAL	12.	5.	3.			20.	
57.00	95.4	32.6	COAL	7.	2.				9.	
			MDST	2.		6.			8.	
		~~ .	SLTS	11.		6 .			17.	
60.04	99.7	/3.4	SLTS	16.					17.	
			SNDS	8.	1.	3.			12.	

START OF CORE RUN		R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	· ·-
5.18	12.1	.0	SLTS	11.	******	25.			36.	
8.23	9.8	.0	SLTS	9.		30.			39.	
11.28	20.7	.0	SLTS	13.		100.			113,	
14.32	33.1	.0	SNDS	7.	3.	29.			39.	
17.37	91.0	.0	SLTS	1.	2.	10.			13.	
			SNDS	3.	2.				5.	
19.81	12.5	.0	SLTS		1.	25.			26.	
23.16	22.0	.0	NTRK							
26.21	25.9	.0	MDST			23.			23,	
29.26	48.4	,0	MDST			28.			28.	
31.39	18.0	. 0	SLTS							
32.61	66.2	.0	COAL	1.	2.	15.			18.	
			MDST	3.	11.	10.			24.	
			SLTS	1.	·				1.	
35.66	45.9	.0	MDST	2.		39.			41.	
38.71	58.2	.0	COAL			б.			6.	
			MDST					30.	30.	
39.62	75.7	.0	COVE			21.			21.	
			MDST					14.	14.	
41.76	80.6	.0	COAL	25.	1,				26.	
			MDST		2.	72.		10.	84.	
44.80	83.9	.0	COAL	3.					3.	
			MDST			23.			23.	
45.42	40.7	.0	COAL	7.		10.			17.	
			MDST			46.			46.	
47.85	62.Q	.0	COAL	10.					10.	
1			MDST			6.			6.	
48.77	45.9	.0		10.	7.	10.			27.	
49.99	67.Q	.0	COAL	9,	1.	11.			21.	
50.90	44.6	.0	COAL	3.	1.			30.	34.	
51.82	69.5	. 0						31.	31.	
			MDST			4.		15,	19.	
53.95	97.0	.0	MDST	8.	7.	3.			18.	

LOCATION = TW83D-315

				LUCAI	1014 - 14036	-313				
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY		JOINT FRACTURES		MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
9.45	83.6	- 0	MD5T	5.	3.	15.	· · · · · · · · · · · · · · · · · · ·		23	
11.28	67.8	20.8	MDST	3.		60.			63.	
13.11	69.0	.0	MDST	5.	8.	6.			19.	
15.24	90.6	.0		4.	4.				13.	
17.37	98.4	26.9	MDST	6.	3.	16.			25.	
20.42	85.2	13.4	MDST			. 24.			24.	
23.47	100.0	.0				44.			44.	
26.52	90.5	5.9		1,		17.			18.	
29.56	79.0	<u>.o</u>				49.			49.	
32.31	86.2	.0	_	18.	6.	62.			86.	
35.51	64.7	4.7	SLTS	32.	16.	53.			101.	
			SNDS	1.					1.	
38.71	62.7	10.2	SLTS	11.	1.	28.			40.	
<u> </u>		_	SNDS	7.	3.	20.			30.	
41.15	97.7		SNDS	23.	2.	, 3 .			28.	
44.20	131.7	26.7	COAL	1.		•			1.	
			SND5	15,		<u>3</u> . 6.			18.	
44.80	92.5	.0		4.		6.			10.	
			MDST	27.	6.			15.	48.	
47.85	95.1		MDST	46.	7.				53.	
50.90	99.3	15.1	<u> </u>	46.	12.				58.	
53.95	88.2	٥.		2.	2.				4.	
		_	MDST	32.	₿.				40.	
56.24	66.7		COAL	10.	3.	50.			63.	
56.84	97.6	5.2	COAL	4.	3.				7.	
			MDST	10.	1.		•		11.	
		_	SLTS	29.	15.	10.			54.	
59.74	87.6	.0	SLTS	28.	10.	6.			44.	
			SNDS	9.		25.			34.	
62,48	54.7	.0	MDST		_					
04.04		_	SNDS	11.	2.				13.	•
64.01	24.6	.0	COAL							
		· -	MDST				****			
64.14	82.Ö		COAL	14	2.				16.	
64.62	61.5	.0	COAL	1.		20.			21.	
		_	MDST			,				
65.53	18.0	<u>. o</u>						30.	30.	
65.53 66.75 69.19	99.2	13.9		_3.	_				3.	
			MDST	21.	8.				29.	
60 40	54.5	45.5	SLIS	12.	3.				15.	
	91.8	43.3	MDST	9	<u>_1.</u>				10.	
70.04	400 5	40.4	SLTS	11,	6.	15.			32.	
	100.7	43.1		29.	9.				38.	
75.28 78.33	99.0	15.1				46.			46.	
78.33	92.8	23.3	MDST			45.			45.	

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CT107 CC										
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LÍTHOLOGÝ		JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
5.18	91.0	6.6	SLTS			24.			24.	
	51.0		SNDS			10.		·····	10.	
7.62	85.5	23.0	SLTS			25.			25.	
			SNDS			28.			28.	
11.28	84.9	7.9	CDAL	12.		3.			15.	
			SLTS	14.					14.	·
12.80	92.8	.0	SLTS	23.	2.				25.	
14.32	95.7	.0	SNDS	46.	6.	3.	•		55.	
17.37	81.0	.0	MDST	9.	1.	20.			30.	
			SNDS	22.	5.				27.	
20.42	32.2	. 0		13.		31.			44.	
22.56	105.3	.0	COAL	5.					5.	
			MDST	24.	1,				25.	
24.08	61.3	22.6	COAL	9.	3.				12.	
25.76	88.2	38.2		8.	2.	11.			21.	
26.52	92.5	. 0	COAL	4.	3.				7.	
			SLŢŞ	38.	1.				39.	
29.56	91.5	.0	SLTS	43.	4.	1.			48.	
			SNDS	10.	1.				11_	
32.61	98.7		SLTS	63.	1.				64.	
35.66	94.1	<u>19.3</u>		41.	4.				45.	
38.71	98.4	20.7		44.	1.	31.			76.	
41.76	8,19	3.9	COAL	1.		8.			9.	
			MDST	20.					20.	
			SLTS	29.	<u></u>	6.			36.	
44.80	98.7	.0		45.	1.	6.			52.	
47.85	90.8	19.6	COAL	4.					4.	
40.00	120.0		MDST	16. 4.					16.	
49.38 49.68	120.0	.0		8.	3.				7.	
50.14	96.1		COAL CDAL	8. 4.	2.				10.	
30.14	50.1	13.1	MDST	4. 41.	3.	. 25.			4.	
53.19	96.7	24 0	COAL	4.	1.	. 25,			69.	
33.13	,30.7	34.3	SLTS	11.		ē.			5.	
			SNDS	6.		0.			17.	
54.71	87.3	9.7	COAL	8.	1.	•			6.	
24.71	07.0	0.7	MDST	17.	3.			5.	9.	
57.00	113.3	.0		'5.	3.			<u>ə.</u>	2 <u>5</u> . 8.	
57.30	92.3	-	CBSH	21.	1.			20.	42.	
_,	uz.u	22.0	COAL	4.				20.	42.	
			MDST	24.					4. 24.	
57.30	113.1	26.8	COAL	3.					2 4 .	
. = . = .			MDST	37.	3.				40.	
C 1 E 7	82.0	37.7	COAL	7.	1.				8.	
61,57										
61,57 62.18	123.3	.0		6.		•			6.	

TART OF ORE RUN	RECOVERY PERCENT	R.Q.U.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
62.48	93.1	32.5	MDST	43.	2.				45.	•
65.68	90.9	51.6	MDST	29.					29.	· · · ·
68.88	109.0	67.2	COAL	3.					3.	
			MDST	10.					10.	
70.10	104.9	. 0	COAL	19.					19.	
70.71	68.5	.0	COAL	10.		16,			26.	
71.63	60.0	.0	COAL	6.		6.			12.	
71.93	94.1	.0	COAL	8.					8.	
72.24	83.3	.0	COAL	4.		10.			14.	
72.54	95.7	.0	COAL	9.	•	3.			12.	
			MDST	3.		•			3.	
73.00	97.4	.0		3.					3.	
			MDST	17.					17.	
73.76	78.9	38.2	COAL	11.					11.	
74.52	89.5	.0	COAL	17.	1.	2.			20.	
			NDAT			4.			4.	
75.28	96.4	68.9	COAL							
			MDST	10,					10.	
			NDAT	13.					13.	
			SLTS	10.	1.				11.	
78.33	97.4	60.7	SLTS	10.	_ 1	<u> </u>			12.	
			SNDS	16.					16.	
81.38	98.4	42.3	SNDS	37.	1.	30.			68.	
84.43	87.9	35.4	SNDS	24.	10.	5.			39.	

LOCATION	= TW8	:3D-317
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				LOCAT	ION = TW83D	-317				
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY		JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
3.35	39.9	. 0	SLTS	2.	6.				8.	
5.18	50.8	.0	SLTS	5.		15.			20.	
6.40	29.9	.0	SI.TS	1.	1.	10.			12.	
7.47	23.1	.0	SLTS	7.	7.	20.			34.	
11.28	21.7	.0	SLTS			50.			50.	
14.32	97.7		SNDS	51	16.	1.			68.	
17.37	60.0		SLTS	12	3.				15.	
			SNDS	22.	4.				26.	
20.42	94.8	23.3	SLTS			44.			44.	
23.47	96.7	74.4				$\frac{30}{10}$			30.	
26.52	94.4		SLTS	21.	1.				22.	
29.56	94.1		ŠLTŠ	19.	11.				30.	
32.61	95.7	16.4	SLTS	16	24.	3			43.	
35.66	85.6		SLTS	28	10.				38.	
38,71	93.8		SLTS	22.	13.	16.			51.	
41.76	99.3		SLTS	22.	5.	,				
44.80	77.0		SLIS	11.	9.		25.		27. 4 5.	
47.85	96.4		SLTS	12.	11.	44.			45. 67.	
50.90	75.7		SLTS	23.	12.					
53.95	32.8			23.	12.	. 15.		=0	50.	
			SLTS	_				50.	50.	
55.17	83.6	.0	COAL	5.		1.			6.	
	7- 4	_	SLTS	10.	8.	10.			28.	
56.39	75.4	.0	COAL	4	2.				6.	
			MDST	13.	3.	16.			32.	
			SNDS			50.			50.	
59.44	98.6		SNDS	8.	2.	22.	25.		57.	
61.57	88.8	.0	SNDS	10.	13.	3.			26.	
63.09	98.4	40.3	SLTS	4.	2.				6.	
			SNDS	19.	5.				24.	
66.14	89.2	7.9	MDST	16.	6.	50.			72.	
			SLTS	15.	4.				19.	•
69.19	66.0	.0	MDST	23.	4.	30.			57.	
71.63	86.1		CBSH	5.					5.	
			MDST	17.	3.				20.	
72.85	59.0	.0	CBSH	2.					2.	
			COAL			25.			25.	
			MDST			14.			14.	
74.07	26.7	.0	COAL			15.			15.	
74.52	85.0	. 0	COAL			25.			25.	
			MDST	45.	7.	25.			77.	
			SLTS	17.	9.				26.	
77.72	78.7	.0	MDST	32.	5.	15.			52.	
		-	SNDS	20.	1.	25.			46.	•
80.77	100.0	. 0	SNDS	61.	4.	25.			90.	
83.82	92.5		SNDS	28.	8.	30.			66.	
			COAL		-					

LOCATION = TW83D-317

START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTÀL FRACTURES	
87.17	98.7	20.9	SLTS		8.	3.			11.	
88.70	87.9	. 0	COAL			10.			10.	-
			MDST	16.	11.	25.			52.	
90.52	79.2	.0	COAL	4.		5.	`		9.	
			MDST	8,	5.	25.			38.	
92.35	57.4	.0	CBSH							
			COAL	3.		5.			8.	
			MDST	6.					6.	
			NDAT		2.				2.	
93.57	97.7	.0	NDAT	56.	14.				70.	
96.62	85.9	.0	COAL			5.			5.	
			MDST	34.	8.	50.			92.	
			SNDS	3.	4.				7.	
99.67	69.2	.0	MDST			75.			75.	
100.58	52.2	.0	MDST			18.			18.	
101.50	79.5	.0	MDST	21.		†5.			36.	
102.72	84.9	-0	COAL	29.	2.	5.			36.	
			MOST	18.	2.	34.			54.	
			SLTS			19.			19.	
105.76	100.3	.0	SLTS			47.			47.	

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				LOCAT	ION = TW830	-318				
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY		JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
11.28	3.9	.0	OTHR		*					
14.32	40.7	8.9	SLTS	10.	4.				14.	
17.37	94.8	44.3	SNDS	14.	11.				25.	
20.42	98.4	52.8	SLTS	19.	3.				25. 22.	
23.47	94.4		SLTS	11.	9.				20.	
	011.7		SNDS	13.	2.				15.	
26.52	90.5	67.1		23.	4. -					
29.56	97.0		MDST	7.					23.	
20100	37.0	12.0	SLTS	25.	1.	7.			7.	
			SNDS	20.	- -	1.			33.	
32.61	51. 6	17.5		14.		10.			2.	
35.36	106.5		SLTS	19.					24.	
38.10	97.0	67.2		17.	4.	40.			' 63.	
41, 15	97.7	<u></u>			3.	15.			35.	
44.20	99.0			19.		3.			22.	
		82.6	SNDS	14.	4.				18.	
47.20	85.1	24.7		8.		18.			26.	
50.60	100.0		SLIS	17.	10.				27.	
53.64	99.3	59.7	SLTS			. 22.			22.	
56.69	100.0	43.0	SLTS	9.	9.				18.	
			SNDS	4	3.	3.			10.	
59.74	92.8	85.3	SLTS	9.					9.	
			SNDS	7.	1.				8.	
62.94	92.5	78.4	SNDS	12.		1.			13.	
66.14	102.3	94.4	SLTS	5.					5.	
			SNDS	7.					7 -	
69.19	99.3	53.8	SLTS	4.	•		 -		4.	·····
			SNDS	15 <i>.</i>	4.				19.	
72.24	97.7	80.0	SNDS	14.	1.				15.	
75.28	98.4	81.3	SLTS	20.	4.				24.	
78.33	97.4	88.9	SLTS	17.					17.	
81.38	99.3	86.2	SLTS	7.					7.	
			SNDS	9.	4.				13.	
84.43	101.0	86.9	SNDS	14.	2.				16.	
87.48	95.3	68.6	COAL	5.		· · · · · · · · · · · · · · · · · · ·			5.	
			MDST	7.					7.	
			SLTS	4.		•			4.	
			SNDS	2.		,			2.	
90.22	73.9	-0	COAL	4.		28.			32.	
90.68	59.8	21.3		11.	2.	20.			13.	
91,90	82.0		CDAL	7.					7.	
92.51	89.6		CBSH	5.	1.				7. 6.	
			CDAL	14.		25.			39.	
93.57	72.1	O	COAL	10.	3.	10.			23.	
94.18	44.3		COAL	, ,	٠.	50.				
94.79	63.9		COAL	5.		25.			50.	
- · · · · ·			CBSH			~Q.			30.	

LOCATION = TW83D-318

		FAULT ZONE FRACTURES	MINOR FAULT FRACTURES	UNCLASSIFIED FRACTURES	JOINT FRACTURES	BEDDING FRACTURES	LITHOLOGY	R.Q.D.	RECOVERY PERCENT	START OF CORE RUN
	2.					2.	COAL	58.2	87.7	95.40
	5.		** *			5.	MDST			
	11.					11.	CBSH	33.6	108.4	96.62
	4 -					4.	COAL			
	16.			1 _		15.	COAL	32.3	85.9	97.69
	6.				1.	5.	MDST			
	31.				15.	16.	MDST	53.9	99.3	99.67
	7.					7.	SNDS			
	4.					<u>4</u>	COAL	61.0	100.0	102.71
	8.					8,	MDST			
	11.					1 <u>1</u> .		42.9	94.5	103.94
	5.			_		5.	COAL			
	5.			<u> </u>		·	MDST			105 75
	2.				_	2.	COAL	45.9	89.2	105.76
	26.				4.	22.	MDST		0+ 6	100 01
	4.					4.	=	81.0	91.8	108.81
· · · · · · · · · · · · · · · · · · ·	. 1. 6,	1.		· -	·············	5.	COAL			
	1 <u>1</u> .			5.		6,	MDST SLTS			
	5.					5.	SNDS			
].				5.	6.	5LT5	80.3	100.0	111,86
	11.				3.	5.	SNDS	30.3	100.0	
	5. 19.				4.	7. 15.	•	76.4	101.0	114.91

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START OF	RECUVERY	R.D.D.	LITHOLOGY	BEDDING	JOINT	UNCLASSIFIED	MINOR FAILET	FALLET ZONE	TOTAL	•
CORE RUN						FRACTURES	FRACTURES	FRACTURES	FRACTURES	
6.10	100.0		CDAL .	5.		20		·	25.	
6.40	69.6	.0	COAL	2.					2 -	
			SLTS	13.	5,	40.			58.	
8.08	35.6		SNDS	12.	3.	30.			45.	
10.97	58.3	,0	COAL	3.	2.	10.		· · · 	15.	
			NTRK							
13.56	CE C	^	SLTS	8.	5.	50.			63.	
14.17	65.6 54.0		COAL	8.	1.	21.			30.	
14.17	51.9		COAL	<u>5</u> .	2.				8.	
16.00	67.7		MDST	6.	4.	5.			15.	
16.61	67.2		COAL	8.	1.	15.			24.	
	32.6		COAL	5.		5.			10.	
17.07	47.5		CDAL			10.			12.	
17.68	91.6	21.9	CDAL	6.	1.	_			7.	
00.40	A+ 1		MDST	29.	2.	3.			34.	
20.42	97.1	13.9		33,	9.				42.	
23.16	89.2	20.7	MDST	15.	2.				17.	
			SNDS	22.	2.				24.	
26.21	97.0	12.5	SLTS	15.	2.	5.			22.	
		_	SNDS	24.	2.	3.			29.	
29.26	88.2		SLTS	12.	5.	<u>3.</u>			20.	
32.61	69.5	.0	MDST	10.	2.	9.			21.	
			SLTS	9.	9.	3.			21.	
35.36	87.5	43.1	COAL	2.		4.			₲.	
			MDST	23.	5.				28.	
38.40	91.8		COAL	8.	4.				12.	
39.01	95.3	.0	COAL	5.	1 -				ნ.	
			MDST	14.	11.				25.	
41.15	62.6		MDST	10.	3.	8.			21.	
42.06	72.1	.0	COAL	11.	1.				12.	
			MDST	13.		12.		17.	42.	
44.35	61.7	.0	COAL	2.				15.	17.	
			MDST	16.	6.			25.	47.	
45.42	56.6		MDST	28.	1,	51.			BQ.	
47.40	54.0		MDST	25.	2.	20.			47.	
50.90	63.5		MDST	. 18 .	6.				24.	
53.34	32.8	.0	COAL							
			MDST	6.	2.				8.	
55.78	39.3	.0	COAL	2.		10.		15.	27.	
			MDST	9.	1.				10.	
57 91	59.8		COAL	8.				100.	108.	
58.83	71.9	. 0	COAL	14.		52.			66.	
60.04	95.9	24.6	COAL	11.	6.				17.	
61.26	103.8	19.7	COAL	6.					6.	
			MDST	21.	6.	2.			29. 28.	
63.09	98.4	66 2	MDST	23.	<u> </u>					

					TON = TW83D	-319				
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	FRACTURES	FAULT ZONE FRACTURES		
66.14	95.4	48.5	MDST	24.	3.				27.	
69.19 72.24	99.7 98.7	38.4 6.3	MDST	21.	8.	10.		· · · · · · · · · · · · · · · · · · ·	39,	
75.28	93.4	31.8	MDST			29. 30.			29. 30.	
										
										
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LOCATION = TW83D-320

START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY		JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
3.35	52.7	.0	MDST			30.			30.	
8.23	7.8	. 0				25.			25.	
10.67	84.2		MDST			22.			22.	
13.71	93.4		MDST			122.			122.	
16.76	86.0	.0	MDST			21.			21.	
20.12	89.0		MDST	****		12.			12.	
		· -	SNDS	6.		15.			21.	
23.47	97.4	81.3	SLTS	5.	1.				7.	
			SNDS	7.	4.				11.	
26.52	98.4	19.4	SLTS	45.	7.				52.	
29.56	90.2		SLTS	10.	13.				23.	
32.61	101.3		SLTS	25.	11.				36.	
35.66	97.4		SLTS	25.		1.			32.	
38.71	98.0		SLTS	28.	$-\frac{5}{7}$			· · ·	35.	
41.76	90.1		MDST	20.	1.				21.	
44.80	90.2		MDST	10.	5.				15.	
47.85	102.0		MDST	11.		8.			19.	
50.90	90.5	11.5				33.			33.	
53.95	100.0		MDST			26.			26.	
57.00	90.8		MDST	12.	8.	20.			20.	
60.04	94.1		MDST	21.	4.				25. 25.	
63.09	96.4		MOST	11.		3.			14.	
66.14	97.5	61.1		11.	6.	J.			17.	
68.58	92.8		MDST	15.	7.	1.			23.	
71.78	86.9	8.3		34.	11.				45,	
74.68	98.7		MDST	4.	2.			10.	16.	
			SLTS	16.	2.	5.		10.	23.	
			SNDS	12.	1.	24.			37.	
77.72	82.2	.0	SLTS	5.	4.	- 1.			9.	
			SNDS	14.	10.	1.			25.	
81.38	64.1	.0	SNDS	12	12.	4.			28.	
84.42	97.7		COAL	7.		7.			7.	
-			MDST	7.				25.	32.	
			SLTS	<u>.</u>				<u> 20</u> .	9.	
87.02	110.9	٠.0	COAL	2.	4.				5. 6.	
87.48	93.4		COAL	4.	2.	51.		15.	72.	
_	•	*	MDST	• •		J. ()		50.	50.	
88.39	88.0	.0	CBSH		2.				3.	
	· -	- -	MDST	• •		14,			14.	
89.31	70.2	.0	CBSH	4.	1.	,,			5.	
•	· -	. •	MDST	• •	• •	23.			23.	
90.52	96.1	.0		25.	9.		4		34.	
93.57	97.8		CBSH	10.	2.				12.	
	- · · -	, 0	COAL	4	٠.				4.	
			MDST	7,		17.			4. 17.	
94.49	81.7	. ō				42.		200.	242	

20.00 x 0.00 x 0.00 T+40.00

START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
96.62	62.0	.0	COAL							
			MDST	3.					3.	
99.67	6 5.9	.0	COAL							
			MDST	13.					13.	
100.58	<u>55.9</u>		COAL	3.					3.	
			MDST	10.					10.	
102.71	62.0	4.6	SNDS	46.	6.				52.	
105.7 6	99.0	10.5	SNDS	38.	7.				45.	
108.81	98.0		SNDS	41.	23.				64.	
111.86	89.5	17.7	SNDS	43.	3.	3.			49.	
114.91	99.0	23.6	CDAL	6.	1.				7.	
			MDST			5.			5.	
			SNDS	32.	3.				35.	
117.96	92.1	10.9	COAL	26.	3.	1.			30.	
			MDST	28.	1.				29.	
121.00	96.4	.0	MDST	40.	7.				47.	
124.05	101.3	. 0	COAL	7.		25,			32.	
			MDST	50.	4.				54.	
127.10	73.8	4.3	CBSH	5.					5.	
			COAL	11.	3.	40.			54.	
			MDST	17.		3.			20.	
130.15	86.6	22.6	CBSH	23.	10.	16.			49.	
			COAL	10.					10.	
			I GN			1.			1.	
133.20	102.0	13.5	MDST	13.					13.	
			SLTS	28.	1.	3.			32.	
136,24	100.0	23.6	NDAT		1.	3.			4.	
			SLTS	40	2.				42.	
139.29	95.4	26.6	MDST	30.					30.	
			NDAT		2.				2.	
142.34	99.0		NDAT	24.	7.	3.			34.	
145.39	85.6	11.8	NDAT			23.			23.	

				LUCAT	ION = 1883D	0-321			-	
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY		JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
4.57	52.5	.0	MDST							
7.01	126.2	16.4	SNDS	15.	1.				16.	
8.23	90.2	28.2	SNDS	21.	, -	35.			56.	
11.28	90.5	28.3	SNDS	28.	4.	0.5.			32.	
14.32	90.8		SLTS	19.	2.				21.	
			SNDS	13.	1.				14.	
17.37	97.4	21.6		34.	3.				37.	
20.42	97.4	14.1		28,	8.				36.	
23.47	100.0	24.6	MDST	19.	11.				30.	
26.52	97.0	30.9		17.	10.				27.	
29.56	95.7	39.0	MDST	26.	2.	6.			34.	
32.61	100.0	28.2		17.	4.	11.			32.	
35.66	89.2	-0		6.	20.	, , •			26.	
38.71	98.0	16.1		4.	34.	50.			88.	
41.76	97.0	39.1		22.	5.	1.	•		28.	
44.80	99.3	48.5	SLTS	23.	9.				32.	
47.85	97.7	52.5	SLTS	20.	8.				28.	
50.90	98.0	37.0	SLTS	21.	8.	3,			32.	
53.95	99.0	37.4	SLTS	22.	10.	• • • • • • • • • • • • • • • • • • • •			32.	
57.00	95.4		SLTS	23.	15.	6.			44.	
60.04	98.0	.0	MDST	29.	19.	10.			58.	
63.09	94.1	44.9	MDST	23,	6.				29.	
55.14	101.0	35.4	MDST	27.	7.	20.			54.	
69.19	89.5	58.7		18.	7.	20.			25.	
72.24	100.0	41.8		27.	7.	2.			36.	
75.28	100.7	31,8		45.	3.	3.			51.	
78.33	97.4	3.6		2.		٠.			2.	
			MDST			84.			84.	
			SNDS	1.	3.	11.			15.	
81.38	82.6	13.4		4	19.				23.	
			MDST	16.	1.				17,	
			SNDS	13.	5.				18.	
84.43	58.0	18.4		3.	10.				13.	
			SLTS	2.	` <u>``</u>			200.	205.	
			SNDS	17.	7.			200.	203.	
87.48	70.5	.0	COAL	3.	6.	15.			24.	
88.70	48.9	9.9	COAL	7.	1.	. 50.			58.	
			NTRK		<u>`</u>				30.	
			OTHR			10.			10.	
90.52	80.3	.0		6.	2.	10.			8.	
_	· -	• •	MDST	39.	12.	100.			151.	
93.57	85.6	10.2	COAL	6.	2.	10.			18.	
70.01	· -		MDST	~ .		32.			32.	
93.97			10001							
90.01			•	30.	1.	VZ.				
96.62	97.0	9.2	SLTS	30. 48.	1. 2.	31.			31. 81.	

					LOCAT	ION = TW830	1-321				
	START OF CORE RUN		R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JDINT FRACTURES		FRACTURES	FAULT ZONE FRACTURES	FRACTURES	
	102.72 105.76 108.81 111.86 114.91 117.96. 121.00	102.3 96.7 100.0 89.2 100.3 98.4 99.7	26.9 .0 9.5 56.4 62.2	MDST MDST MDST MDST SLTS SLTS SLTS SLTS	42. 36. 69. 27. 22. 29.	8. 2. 3.	2. 2. 22. 5.			52. 38. 74. 22. 32. 22. 29.	
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					ION = IM83D					
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLŌGY		JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
7.01	92.6	٠. ٥	SLTS			. 15.			15.	
8.23	96.4	.0	SLTS			42.			42.	
11.28	96.1	.0				38.			38.	
14.32	91.1		SLTS			58.			58.	
17.37	94.8		SLTS			31.			31.	
20.42	95.1		MDST			75.			75.	
			SLTS		21.	,			21.	
23.47	83,6	.0	MDST			37.			37.	
26.52	75.8		MDST	6.	18.	1.			25.	
28.96	100.7	.0		3.	8.	69.			80.	
32.00	97.4	.0	_			43.			43.	
35.05	86.9	.0	MDST			50.			50.	
38.10	56.1	.0	MDST	2.	2.	13.			17.	
41.15	84.3	.0				56.			56.	
44.20	101.3	.0	MDST			32.			32.	
47.24	89.2	.0		4.	6.	34.			44.	
50.29	98.4	.0	MDST			16.			16.	
			NDAT						2.	
			SLTS	13.					13.	
53.34	94.4	.0	NDAT	20.	5.	. 2.			27.	
			SLTS			20.			20.	
56.39	88.7	.0	SLTS	8.	10.				18.	
59.13	90.1	.0	SLTS	5.	2.	. 10.			17.	
60.04	98.0	13.4	MDST	24.	9.				33.	
63.09	85.2	٠,٥	MDST	23.	5.				28.	
66.14	95.4	10.2	MDST	10.	8.	5.			23.	
69.19	100.7	4.9		28.	4.	10.			42.	
72.24	94.7	4.6	MDST			50.			50.	
75.28	91.8	.0				102.			102.	
78.33	98.4	.0				33.			33.	
81.38	51.5	.0	MDST	1.	1.	107.			109.	
84.43	81.6	.0	MDST			16.			16.	•
87.48	95.7	36.5	MDST			22.	•	•	22.	
90.52	96.4	9.5	MDST			42.			42.	
93.57	99.0					48.			48.	
96.62	101.6	35 <i>.1</i>				25.			25.	
99.67	95.7		SLTS	11,	12.				23.	
102.72			SLTS			27.			27.	
105.76	99.3	15.7		7.	4.	17.			28.	
108.81	62.0	.0	COAL	1.		30.			31.	
			MDST			10.			10.	
			SLTS	6.					6.	
109.73		.0		4.		. 30.			34.	
110.95	53.8	.0	COAL	2.	1.	, 50.			53.	
	142 1	= ·	SLIS	8.				·	8.	
111.86	98.4	32.5	SLĪS	8.	6.				14.	

LOCATION = TW83D-322

				LOCAT	ION = TW83D	-322				
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LÍTHÖLÓGŸ	BEDDING FRACTURES		UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
114,91	97.7	41.6	SLTS	10.	13.				23.	
117.96	91.1	.0				22.			22.	
121.00	101.0	.0	SLTS	6.	11.	38.			55.	
124.05	100.0	12.8	SLTS	21.	20.				41.	
127.10	95.4		SLTS	17.	6.	9.	50.		82.	
			SNDS	22.	†.	4.			27.	
130.15	65.6	.0	SLTS	8.	4.				12,	
133.20	93.5	11.0	COAL	2.	f	2.			5.	
			SLTS	15.	3.	5.			23.	
134.72	60.7	19.7	COAL	2.	7.				9.	
135.33	55.7	.0	CDAL	2.	6.				8.	
135.94	70.8	.0	CB5H	7.	6.	25.			38.	•
			COAL			10.			10.	
		•	MDST	2.		15.			17.	
137.31	93.9	. 0	SNDS	21.	10.	15.			46.	
139.29	101.3	5.6	SNDS	39.	5.		•		44.	
142.34	96.1	.0	SNDS	54.	5.				59.	
145.39	101.6	15.8	SNDS	36.	3.				39.	
148.43	92.1	4.3	CBSH	1.					1.	
			COAL			6.			6.	
			SNDS	4 6 .	Э,				49.	
151.48	100.0	10.3	COAL	5.	1.	. 10.			16.	
			MDST	12.	3.	,			15.	
152.55	95.6	23.4	CBSH	1.					1.	
			COAL	8.	3.	2.			13.	
			MDST			12.			12.	
153.92	95.0	.0	CBSH			6 ,			6.	
			CDAL	8.	4.				12.	
			MDST	24.	2.	81,			107.	
157, 12	96.6	11.2	CBSH	10.					10.	
			COAL	3.		100.			103.	
			MDST	39.	4.				43.	
160.32	86.2	0	CBSH	3.					3.	
			MDST	20.	18.				38.	
163.07	67.2	.0	COAL	11.					11.	
163.68	107.9	32.9	COAL	8.	1.				9.	
164.44	86.9	. 0	CBSH	14.					14.	
			COAL	14.	3.				17.	
165.66	98.2	.0	CBSH	4.					4.	
			COAL	3.	17.				20.	
			MDST	21.					21.	
167.33	97.5	.0	MDST	10.	8.	12.			30.	
			SLTS	5.	18,				24.	
169.77	98.7	8.2	SLTS	26.		8.	5.		39.	
172.82	96.7		SLTS			28.			28.	
175.87	101.6	44.3	SLTS			21.			21.	

CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES		MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
5.18	77.0	.0	MDST			500.			500.	
0.10			NTRK			300.			300.	
8.23	85.2	.0				537.			537.	
11.28	95.4	.0	MDST			544.			544.	
14.32	79.7	.0	MDST	12.	1.	532.			545.	
17.37	75.4	.0	MDST	: ' '		43.			43.	
20.42	62.3	.0	MDST			321.			321.	
23.47	74.5	.0				529.			529.	•
26.21	97.0	.0	MDST			551.			551.	
29.26	83.2		MDST			559.			559.	
32.00	72.8	4.3	MDST			149.			149.	
35.05	104.9	٠.٥	MDST			125.			125.	
35.66	105.2	.0	COAL			100.			100.	
····		•	MDST NTRK			552.			552.	
38.56	29.9	.0	COAL			200.			200.	
40.23	14.8	.0				20.			20.	
40.84	6.5	.0				. 3.			3.	
41.76	54.6	. 0	COAL			500.			500.	
43.59	62.0	.0	COAL			500.			500.	
44.80	68.9	.0	COAL	2.	3.	50.			55.	
			SLTS	48.		43.			91,	
47.85	25.2	.0	CBSH	5.		2.			7.	
			COAL	2.	1.				3.	
			SLTS	2.		25.			27.	
49.99	100.0	.0	COAL			100.			100.	
			MDST			530.			530.	
51.51	101.2	.0	COAL							
			NTRK							
			SLTS	24.	21.	114,			159.	
53,95	95.5	.0	COAL			20.			20.	
			SLTS	39.	12.				51.	
			SNDS	4.					4 -	
56.84	89.6	15.6	COAL	4.	Э.	10.	•		17.	
			SLTS	15.	4.	•			19.	
57.61	97.1	.0	COAL	1.	Э.				4.	
			MDST			253.			253.	
			SLTS	8.	5.				13.	
60.04	101.3	.0	MDST	. –		257.			257.	
			SLTS	17.	9.				26.	
63.09	97.4	.0	CBSH	11,	<u> </u>				12.	
			COAL	13.	1.				14.	
		_	MDST	16.	4.	12.			32.	
64.62	75.8		COAL	3.		100.			103.	
65.53	102.2	5.1	CBSH	· · · · · · - · · · · · · · 		25.			25.	
			COAL	2.		100.			102.	

LOCATION = TW83D-323

START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLDGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
65.53	102.2	5.1	MDST			48.			48.	
68.27	101.0	.0	COAL	4.	2.	30.			36.	
			MDST			12.			12.	
			SLTS	35.	5.	200.			240.	
71.32	96.4	.0	SLTS			152.			152.	
74.37	85.1	.0	SLTS			151,		••	151.	
77.72	99.0	4.9	SLTS			62.			62.	
80.77	94.1	.0	SLTS			95.			95.	
83.97	89.7	6.3	SLTS			32.			32.	
87.17	98.4	7.5	SLTS			55.			55.	
90.22	102.0	.0	SLTS			41.			41.	
93.27	95.4	7.5	SLTS			42.			42.	
96.32	94.4	10.5	SLTS			34.			34.	
99.36	85.3	3.7	5LT5			46.		· · · · · · · · · · · · · · · · · · ·	46.	
102.56	97.2	. 0	SLTS			68.			68.	
105,76	98.2	.0	SLTS			123.			123.	
108.51	97.0	10.8	SLT5			. 18.			18.	
111.56	97.0	6.9	SLTS	3.	7.	19.			29.	
114.60	94.8	43.0	SLTS	23.	4.				27.	
117.65	92.8	17.0	SLTS	18.	4.	17.			39.	•
120.70	90.2	27.9	SLTS			19.		0	19.	
123.75	98.4	.0	SLTS			82.			82.	
126.80	97.0	.0	SLTS			53.			53.	
129.94	88.4	٥.	SLTS			51.			51.	
133.20	92.2		SLT5			46.			46.	
135.64	94.7	27.3	ŠLTS			. 15.			15.	
			SNDS			13.			13.	
138.68	91.0	4.9	SNDS			66.			66.	
141.12	95.1	5.2	SLTS			26.			26.	
			SNDS	1.	4 .	5.			10.	

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		1		LUCAT	IUN = (#83D	1-324				
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY		JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZÖNE FRACTURES	TOTAL FRACTURES	
4.00	100.0	.0	SNDS			20.			20.	
4.12	60.0	Ö		4.	2.				6.	
4.42	33.3		CDAL	• •		25.			25.	
4.72	26,7		COAL	3.	1.	25.			29.	
5.79	54.1		COAL	٥.	1.	100.			100.	
6.40	56.8		CBSH	ā.		100.			14.	
0.10	50.0	.0	MDST	3.		500.			503.	
8.23	82.2	0	. COAL	7.		100.			107.	
0.20	02.2	. •	MDST	13.	3.	59.			75.	
10.36	101.0		SLTS	14.	<u> </u>				14.	
10.00	101.0	.0	SNDS	43.	7.	3.			53.	
13.41	89.0	0	SNDS	32.	4.	3. 4.	•			
16.76	92.8	.0		64.	4.	4.			40. 64.	
19.96	77.9	. 0		21.	5.	·				
21.18	59.0		OTHR	21.	IJ.				26.	
21.79	95.8		SLTS	10	7.				25	
21.79	95.6	.0	SNDS	18. 30.					25.	
23.47	115.0				7.	3.			40.	
23.47	115.0	.0	COAL	5.	7.	_			12.	
25 50	00.0	_	SNDS	33.		3.			36.	
25.60	88.0	.0	COAL	6.		7.	50.		63.	
			SLTS	32.					45.	
27.43	66.7	.0	COAL	10.	5.	30.			45.	
		_	MDST	16.		35.			51.	
28.96	97.5	.0	MDST	14.	_				14.	
			SLTS	47.	7.	101.			155.	
32.16	96.3	. 0	COAL	9,	2.	20.			31.	
			MDST			40.		200.	240.	
			SLTS	19.	1 -				20.	
35.36	17.8	.0		2.		3.			5.	
35.81	101.3	.0		18.	1.	40.			59.	
36.57	73.8	.0	COAL	2.		3.			5.	•
			MDST	16.					16.	
			SLTS	23.	5.				28.	
38.71	112.4	6.9	MDST	25.	,	25.			50.	
			SLTS	35.	4.	· 4 .			43.	
41.45	88.1	.0	MDST			93.			93.	
44.80	100.0	- O	MDST			49.			49.	
		•	SLTS			54.			54.	
47.85	90.2	.0	SLTS			87.			87.	
50.90	99.0		SLTS			84.			84.	
53.95	96.7		SLTS			67.			67.	
			SNDS			9.			911	

LOCATION = TW83D-325

START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHULOGY		JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FRACTURES	TOTAL FRACTURES	
6.40	94.5	7.7	SNDS	18.		6.			24.	
8.23	50.5	. 0	SNDS	11.		55.			66.	
11.28	74.6	-	COAL	4.	1.	4.			9.	
	. , , ,		SLTS	17.	2.	••			19.	
12.50	24.2	.0	COAL	6.		25.			31.	
14.32	91.8		COAL	1.						
			SLTS		3.	10.			13.	
14.93	19.7	.0	CDAL	4.	1.	20,			25.	
•			MDST	2.		10.			12.	
17.37	64.3	4.6	COAL	2.		20.			22.	
			MDST	22.	9.	45.			76.	
20.42	94.4	.0	MDST	12.	5.	100.			117.	
22.56	30.9	14.5	COAL	2.					2.	
			MDST	2.	1.				3.	
24.08	84.0	.0	MDST	3.					3.	
			SNDS	16.	9.				25.	
26.52	84.7	6.9	MDST	13,	1.	100.			114.	
			SNDS	10.	5.				15.	
29.26	94.4	33.4		16.	6.	3.			25.	
32.31	100.6	12.2	COAL	6.		20.			26.	
			MDST	12.	2.				14.	
			SLTS	11.	2.				13.	
			SNDS	8.	2.	25.			35.	
35.66	89.8		SLTS	18.	8.				26.	
38.71	100.0		SLTS	32.		<u>1.</u>			41.	
41.76	98.7	.0	COAL	4.		. 1.			5.	
		_	SLTS	39.	8.	1.			. 48.	
44.80	102.5	-0	COAL			10.			10.	
			MDST			51.			51.	
47.55	98.7	.0	COAL	7.	1.				8.	
		_	MDST	_		36.			36.	
50.60	95.9		COAL	9.		21.			30.	
51.82	92.0	. 0	COAL	7		12.			19.	
	400.0	_	MDST			25.			25.	
53.95	100.0		MDST			89.			89.	
57.00	86.5		SLTS			46.			46.	
60.04	99.3		SLTS			42.			42.	
63.09	98.4	4.9	SLTS			56.			56,	

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LOCATION = TW83D-326

START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FRACTURES 5	TÖTÁL FRACTURES	
7,32	82.4	.0	SLTS			20.			26.	
8.23	19.7		SLTS	<u>6.</u> 9.		34.			43.	
10.97	86.9		SLTS	42.	9.	11.			62.	
14.02	100.8		SLT\$	20.	4.	30.			54.	
			SNDS	9.	11.				20.	
16.46	91.3	26.6	SLTS	9.		11.			20.	
			SNDS	27.	8.	2.			37.	
19.81	101.6	49.5	SLTS	28.	11.				39.	
22.86	96.4	32.8	MDST	29.	2.				31.	
			SLTS	2.	•••				2.	
25.91	101.6	35.4	MDST	31.	2.	3.			36.	
28.96	101.0	29.9	MDST	33.	4.	30.	•		67.	
32.00	96.4	23.9	MDST	41.	17.				58.	
35.05	100.0	23.5	MDST	24.			12.		38.	
36.88	45.9	٠٥.	CDAL		2.	25.			. 27.	
37.49	66,4	.0	COAL			15.			15.	
			MDST	19.					19.	
38.71	89.6	18.6	COAL	1.		26.			27.	
			MDST	15.	4.	20.			39.	
40.54	95.9	6.6	COAL	2.	13.	20.			35.	
			MDST	28.	4.	20.			52.	
			SLTS	4.	3.				7.	
44.20	88.2	31.6	SLTS	15.	4.	26.			45.	
			SNDS	16.	2.	5.			23.	
47.24	148.4		COAL	9,		6.			15.	
47.55	91.0	12.8	CBSH	11.					11.	
			COAL	4.	1.	60.			65.	
			MDST	16.	2.				18.	
50.90	97.4		SLTS	17.	9.				26.	
53.64	99.3	54.6	MDST	13.		30.			43.	
			SLTS	12.	4.				16.	
56.70	102.0	28.9	-	26.	4.	33.			63.	
59.74	95.9	16.6				68.			68.	
62.94	97.5	77.5				19.			19.	
66.14	100.3		SLTS			25.			25.	
69.19	97.7		SLTS			26.			26.	
72.24	100.7	80.3				15.			15.	
75.28	97.7		SLTS			16.			16.	
78.33	100.0	69.5	SLTS			15.			15.	
		- -	SNDS	1.	2.	. =			3.	
81.38	97,4	71.5	SLTS			16.			16.	
			SNDS	4.	2.				6.	

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CTABL DE	DECOVERY									
ORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
9.45	82.0	.0	SLTS	18.		50.			68.	
11.28	75.7	.0	SLTS	30.		53.		÷ • • •	83.	
14.32	82.0		SLTS	42.	8.	00.			50.	
17.37	94.3		SLTS	19.	2.	50.			71.	
19.81	66.9	.0		33.	4.	28.			65.	
23.47	39.3	.6.		25.		50.			75.	
26.52	13.2	.0		20.		50.			50.	
29.56	55.7		OTHR			, 100.				
20.00	55.7	.0	SLTS	18.		50.			100.	
32.61	61.7		OTHR	12.		75.			68.	
32.01	01.7	.0	SLTS	8.	2				87.	
35.04	59.7	^			2.	10.			20.	
35.66	22.0		OTHR DTHR	7.		3 m			7.	
				7.		15.		· · · · · · · ·	22.	
37.48	26.2	4 . 1		11.		15.			26.	
41.45			OTHR	2.	_				2.	
41.15	101.6		MDST	25.	2.	13.			40.	
44.20	57.3		MDST	13.	4.	26.			43.	
46.33	99.3	10.5	MDST	11.	6.				17.	
			SLTS	6.	1.				7.	
47.85	76.5	14.2	SLTS	16.	2.	67.			85 <i>.</i>	
49.68	65.6	.0	MDST	26.		150.			176.	
52.73	106.6	.0	MDST	50.	б.	25.			81.	
54.56	6 2.4	.0	COAL	4.	2.				6.	
			SLTS	22.	4.	10.			36.	
56.69	89.5	18.4	CBSH	13.		10.			23.	
	•		COAL	5.	8.				<u> </u>	
			NTRK							
			SLTS	28.	2.	25.			55.	
59.74	104.3	9.2	SLTS	53.	8.	3.			64.	
62.79	23.9		SNOS	7.		18.			25.	
64.92	79.7		SLTS	5.		100.			105.	
5 7. GE	,		SNDS	7.		2.			9.	
66.45	58.6	0	COAL	8.	1.	٤.			9. 9.	
00,40			SLTS	4,	····	30.			34.	
67.97	83.6	0	SLTS	5.		. 25.				
68.58	81.6		SLTS	11.		23. 50.			30.	
70.10	26.2		SLTS	11.		50. 50.			61.	
71.93	and the second s					50.			50.	
11.93	21.5	. 0	NTRK	-						
75 00	46.6	_	SLTS	5.		20.			25.	
75.28	18.9	. 0	COAL	2.					. 2.	
			NTRK							
			OTHR	_						
78.03	101.6	15.7	CBSH	1.					1,	
			COAL	6	5.	10.			21.	
			MDST	12.					13.	
			SLIS	27.	1.				28.	

LOCATION = TW83D-327

START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JÖİNT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
81.08	95.6	49.4	SLTS	30.	5.				35.	
84.28	95.9	15.3	SLTS	44.	1.				45.	
87.48	102.0	. 0	SLTS	54.	1.				55.	
90.52	96.1	21.3	MDST	40.	5.				45.	
93.57	100.7	٠.	MDST	44.	3.	3.			50.	
96.62	99.0	10.8	MDST	21.		2.			23.	
			SLTS			50.			50.	
99.67	98.4	.0	MDST			11.			11.	
			SLTS			26.			26.	

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START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY		JOINT FRACTURES	,UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
4.88	78.7	.0	COAL	8.	12,				20.	
5.49	62.3	.õ.	COAL	4.		10.			14.	
6.10	56.6	_	CBSH	5.		20.			25.	
			CDAL	9.		20.			29.	
			MDST			10.			10.	
7.92	67.2	ō	COAL	6.	4.	20.			30.	
7.52	07.2	-0	MDST	9.	1.	10.				
9.14	79.4	^	COAL	2.	1 -	10.			20.	
5, 1 4	75.4	.0		29.					2.	
11.28	28.4		MDST			······································			<u> 29.</u>	
11.20	28.4	.0	COAL	5.	-				5.	
40 74	40.5	^	MDST	10.	3.				13.	
13.71	40.5	.0	MDST		_	10.			10.	
			SLTS	26.	4.				30.	
15.24	34.3	. 0	SLTS	32.	4.				36.	
17.37	83.8		SLTS	26.	6.	4.			36.	
19.66	98.4	.0	SLTS	5.					5.	
			SNDS	37.	3.				40.	
22.71	91.3	11.8	SNDS	35.		55.			90.	
26.52	96.7	21.7	SNDS	29.	5.	12.			46.	
28.96	96.4	17.3	CB2H	2.		3.			5.	
			COAL	3.	2.		•		5.	
			MDST	12.	3.				15.	
			SNDS	22.	6.				28.	
32,61	89.7	29.0	CBSH	3.	4.				7.	
			CDAL	10.	3,				13.	
33,68	98.4	. 0	CBSH	3.	771				3.	
***		• •	CDAL	3.	3,	20.			26.	
			MDST	13.	٧.	20.			13.	
34.90	68.9	10.7	COAL	4.		15.			19.	
07.50		10.1	MDST	9.	2.	13.				
36.12	97.6	6 6	COAL	4.	۷.				11.	
30.12	97.0	0.0			9.				4,	
37.79	55.4	0	MDST	17. 4.					26.	
38.71		·· <u>-·</u> \footing	SLTS		<u>5.</u>				9.	
38.71	133.0	.0	CBSH	6.	3.				9.	
			COAL	8.					8.	
			MDST	4.					4.	
			SLTS	4.	3.				7.	
39.62	85.5	.0	COAL			150.			150.	
			MDST			54.			54,	
44.65	71.9	.0	COAL			15.	•		15.	
			MDST			54.			54.	
44.80	88.9	51.8	MDST	13.	1.				14.	
			SLTS	11.	1.	1.			13.	
47.85	94.4	17.4	SLTS	37.	3.	2.			42.	
50.90	101.6		SLTS	30.	4.				34.	
53.95	93.4		SLTS			2.			2.	

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ART OF	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
57.00	98.0	43.1	MDST	33.	1,	6.			40.	
60.04	95.7	17.4	MDST			48.		· · · · · · · · · · · · · · · · · · ·	48.	
			SLTS			4.			4.	
63.09	103.6	19.7	SLTS			50.			50.	
66.14	100.3	39.7	SLTS			37.			37.	
69.19	99.3	14.5	SLTS			24.			24.	
72.24	96.4	16.4	SLTS			62.			62.	
75.28	100.0	24.6	SLTS			39.			39.	
78.33	98.7	20.7	SLTS			51.			51.	
			SNDS	3.	3.	5.			11.	
81.38	101.0	17.4	SLTS			39.			39.	
84.43	101.0	11.8	SLTS			81.			81.	

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LOCATION = TW83D-329

								5 5 5	DECOVERY.	TIDE OF
	TOTAL FRACTURES	FAULT ZONE FRACTURES	FRACTURES	UNCLASSIFIED FRACTURES	JOINT FRACTURES		LITHOLOGY	R.Q.D.	RECOVERY PERCENT	DRE RUN
	86.			21.	8.	57.	SLTS	.0	95.1	7.62
esse =	62.			20.	5.	37.	SLTS		72.3	10.67
	72.			, 20. · 25.	9,	38.	SLTS		82.3	13.41
				51.	8.	39.	SLTS		74.1	16.46
	98.			31, 4.	8.	73.	SLTS		80.3	19.51
	85.			4.	6.		SLTS		95.4	23.47
	97.				0. 14.	78.	SLTS		102.0	26.52
	92.								89.5	29.56
	86.				12.	74.	SLTS		89.5 98.7	32.61
	89.			1.	12.	76.	SLTS			
	94.				13.	81.	SLTS		100.7	35.66
	88.			15.	18.	55.	SLTS		88.2	38.71
	68.				9.	59.	MDST		100.7	41.76
	103.			103.			MDST		85.9	44.80
	10.			6.	1 -	3.	CBSH	.0	102.5	47.85
	3.				2.	1.	CDAL			
	10.			10.			MDST			
	24.			24.			SNDS			
	3.					3.	CBSH	4.6	100.3	50.29
	6.				4.	2.	COAL		•	
	39.				7.	32.	SLTS			
	1 6 .				3.	13.	SNDS			
	10.					10.	CBSH	.0	89.3	53.34
	9.			5.	3.	1.	COAL			
	18.			1.	2.	15.	SNDS			
	20.		1.	10.	7.	2.		26.2	90.2	54.56
	26.			26.		· · · · · · · · · · · · · · · · ·	MDST	LUIL	V V V L	
	11.			20.	2.	9,	COAL	n	100.0	55.78
	9.				4.	5.		10.6	95.0	56.39
	9. 45.				٦.	45.	SLIS	10.0	50.0	20.05
						63.	SLTS		100.0	59.59
	68.			5.	4.	64.	SLTS		96.9	62.64
	73.			3. 4.		61.	SLIS		103.6	65.84
	66.				1.					
	67.			1.	8.	58.	SLTS		92.6	68.88
	31.				4.	27.	SLTS	-0	94.7	72.24
	34.				8.	26.	SNDS	_		
	11.				2.	9.	COAL	.0	52.5	75.28
	29.				1.	28.	MDST			
	50.			50.			OTHR			
	2.					2.	COAL	3.6	103.6	77.72
	13.					13.	MDST			
	58.			12.	1	45.	SLTS			
	4.					4.	CBSH	16.4	99.0	80.77
	3.					3.	CDAL			
	48.			10.	5.	33.	SLTS			
	5.			ı	1.	4.	SNDS			
	2.	 .				2.	CBSH		88.9	83.83

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				LOCAT	ION = TW83D	-329				
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY		JOINT FRACTURES		MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
83.83	88.9	.0	COAL	12.	7.				19	
84.73	69.7	.0	COAL	11.	15.	20.			19. 46.	
85.95	81.0	. 0	MDST	, - •		46.	5.		51.	
87,48	67.1	5.3		39.	5.		٠.		44.	
89.76	101.3	14.4	SLTS	37.	14.	4.			55.	
92.81	77.7	6.8		25.	8.				33.	
	, ,	0.0	MDST	16.	5.				21.	
			SLTS	2	2.				4.	
96.62	72.3	0	MDST	20.	15.	22.			57.	
98.75	100.7		COAL	7.		20.			27.	
	,		MDST	. •		26.			26,	
			SNDS	21.	4.	6.			31.	
101.80	43.5	0	COAL	3.	₹,	15.			18.	
			SNDS	<u>5.</u>		13.			5.	
102.72	100.0	.0		10.	3.				9. 13.	
103.33	93.0		COAL	11.	9.	20				
103.33	55.0	7.0	MDST	11.	5 .	20.			40.	
			SLIS	23.	3.	10.				
105.76	91.7			23. 7.					26.	
105.76	91.7	.0	COAL		3.	6 0.			70.	
400.05	400.0		SLTS	51.	4 -	1.			56.	
108.05	100.3	()	COAL	2.					2.	
			MDST		_	7.			7.	
444.40	AF A	20.1	SLTS	39.	9.	_			48.	
111.10	95.0	29.1	CBSH			5.			5.	
			MDST	· · · · · · · · · · · · · · · · · · ·		3.			3.	
			SLTS	25.	7.				32.	
114.30	96.7	23.5	COAL	23.	5.	10.			38.	
440 40			SLTS	5.		10.			15.	
116_13	83.6	18.0	COAL	3.	1.				4.	
			MDST			19.			19.	
117.96	92.1	30.6	CBSH	10.					10.	
			CDAL	3.		5.			8.	
			MDST	11.	3.	14.			28.	
			NDAT		2.	10.			12.	
121.00	88.5	.0	COAL	5.		10.			15.	
			MDST	16.	3.	3.		8.	30.	
			SNDS	4.	2.				6.	
123.44	96.7		SLTS	11.	9.	4.			24.	
125.27	100.0		SLTS	23.	4.	3.			30.	
127.10	94.4		SNDS	27.	14.		1.		42.	
130.15	103.9	14.5	SNDS	33.	15.				48.	
133.19	96.1	20.7	SNDS	32.	5.				37.	
136.24	96.1	8.5	MDST			39.			39.	
			SLTS	9.					9.	
139.29	102.0	.0	COAL	19.	3.	22.			44.	
			MDST	5.	1.				6.	

START OF	RECOVERY	R.Q.D.	LITHOLOGY		JOINT	UNCLASSIFIED		FAULT ZONE	TOTAL	
CORE RUN	PERCENT			FRACTURES	FRACTURES	FRACTURES	FRACTURES	FRACTURES	FRACTURES	
139,29	102.0	.0	SLTS	40.	3.				43.	
142.34	77.4	3.9	ČBSH	5.	2				7.	
	,,,,,	2.5	COAL	12.		5.			17.	
			MDST			43.			43.	
145.39	113.4	20.7	-	43.	3.				45. 46.	
148.44	47.4	4.3	CBSH	18.	3.	25.			46.	
			MDST			18.			18.	
			SLTS	2.		,			2.	
151,48	82.0	. 0	CB2H	4.		25.			29.	
			MDST			32.			32.	
			OTHR						52 .	
153.31	90.2	32.8	CBSH	2.					2.	
			COAL	5.	1.	10.			16.	
			MDST			11.			11,	
154.53	100.0	4.3	CBSH	9.	1.	1.	•		11.	
			MDST			42.			42.	
157.58	99.7	4.3	MDST			28.			28.	
160.63	81.0	7.9	MDST	22.	2.				24.	
163.68	102.0	39.8	MDST	2.	7.	17.			26.	
166.72	101.0	31.8	MDST	24.	3.				27.	
169.77	100.3	16.7	MDST	8.	2.	28.			38.	
172.82	88.9	43.0	MDST			31.			31.	
175.87	102.3	38.7	MDST			18.			18.	
			SLTS			29.			29,	
178.92	102.3	56.1	SLTS			26.			26.	
181.96	105.1	63.6	SLTS			24.			24.	
184.10	99.3	50.5	SLTS			20.			20.	
187.15	123.0	100.0	SLTS			5.			5.	
187.76	100.0	37.8	SLTS			34.			34.	
190.80	100.7	72.5	SNDS	3.		14.			17,	

LOCATION = TW83D-330

				LUCAT	ION = TW83D	1-330				
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY		JOINT FRACTURES	· UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	· ··· ·
7.01	57.3	11.7	SLTS	18.					18,	
8.23	99.0		SLTS	53.	3.	· 			56.	
11.28	96.4		SLTS	46.	9.				, 5 5.	
14,32	104.9		SLTS	27.	1.				28	
15.54	82.5		SLTS	24.	' -	1.				
17,37	98.5		SLTS	45.	2.		·		<u>25</u> . 47,	
20.12	93.4		SLTS	57.	2.	1.				
22.86	98.7		SLTS	64.		١.			60.	
25.91	96.1			04.	11.				75.	
28.96			SLTS		_	41.			41.	
32.00	98.4		SLTS	40.	4.	2.			46.	
	95.7		SLTS	58.	3.				61.	
35.05	101.3		SLTS	68.	2.	1.			71.	
<u> 38. 10</u>	96.7		SLT5	41.	8.	2.			51.	
41.15	97.0		SLTS	55.	3.	3.			61.	
44.50	97.7		SLTS	42.	2.				44.	
47.55	94.4	4.1	NDAT		2.				2.	
			SLTS	41.	3.				44.	
50.75	89.1	.0	SLTS	64.	3,			-· · · · · · · · · · · · · · · · · · ·	67.	
53.95	113.9	.0	SLTS	23.		28.			51,	•
56.39	92.5	.0	SNDS	44.	3.				47.	
59.74	99.7		CBSH	23.	3.				26.	
			5ND5	42.	1.				43.	
62.79	96.7	4.9	SNDS	35.	1.		L		36.	
65.84	99.7	28.3		38.	1.	2.				
68.88	63.3	3.9		32.	3.	2.			41.	
71.93	98.0	24.6		16.	8.				35.	
74.98	100.0	46.9		10.	7.				24.	
78.03	90.7		SNDS	13.					8.	
81.38	91.1				15. 6.	1.			29.	
			SNDS	39.		, <u>1.</u>			46.	
84.43	99.0		SNDS	37.	7.	20.			64.	
87.48	101.0		SNDS	36.	4.	2.			42.	
90.52	84.3	.0	CBSH	16.		50.			66.	
			COAL	3.		50.			_ 53.	
			MDST			15.			15.	
			SLTS	15.		2.			17.	
			SNDS	15.	2.				17.	
96.62	95.1	.0	MDST	35.		10.		100.	145.	
			SNOS	4.					4.	
98.62	96.7	4.9	MDST			11.			11.	
			SLTS			45.			45.	
			SNDS	9.					9.	
99.67	92.8	. o	MDST			18.			18.	
•	_	. •	SLTS			61.			61.	
102.72	99.3	6.3	MDST			46.	25.		71.	
		٠.٠	SLTS			6.	20.			
105.76	97.4	29 5	MDSŤ			44				
100.70	<i>31</i> ₁ 4	25.5	MU 3 I			44.			44.	

ORE RUN	PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
108.81	95.4	4.3	MDST			53.				
111.86	94.8	8.9	MDST			36.			53. 36.	
114,91	101.0	4.6	SLTS MDST SLTS			29. 41. 8.			29. 41.	
117.76	93.4	.0	MDST			34.	25.		<u>8.</u> 59.	-
121.00	98.0	45.9	SNDS SNDS	24.	12.	14. 1.			14. 37.	
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LOCATION = TW83D-331

				COURT	1014 - 1 #650	331				
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLÖĞY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
11.28	30.7	.0	SLTS	18.	2.				20.	
14.02	95.5	. ō		43.	14.				57.	
17.37	79.4	.0	SLTS	14.		200.			214.	
19.51	96.7	.o		51.	1.	52.			104.	
22.55	57.4	.0	SLTS	54.	11.	1.			66.	
25.60	82.1	20.7	ŠI.TŠ	38.		75.		·	113.	
29.56	96.7	9.5	SLTS	39.	8.	25.			72.	
32.61	95.7	27.9	SLTS	34.	4.	1.			39.	
35.66	96.4	36.1		35.	3.				38.	
38.71	92.5	8.9		40.	6.	ā.			49.	
41.76	97.0	13.8		27.		10.			37.	
			SNDS	21.	6.				27.	
44.80	93.4	15.7	SLTS	34.	13.				47.	
47.85	82.0	9.8	SLTS	25.	ġ.				34.	
50.90	93.4		MDST	8.	1.				9.	
		-	SLTS	21.	4.				25.	
52.42	129.4	.0	COAL		• •	50.			50.	
			MDST	<u>3</u> .		75.			78.	
53.95	68.9	.0	COAL	4.	5.	20.			29.	
		•	MDST	2.					2.	
54.56	67.2	.0				50.			50.	
55.17	90.2	29.5	SLTS	7.	3,				10.	
55.78	95.1		SLTS	20.	6.				26.	
57.00	95.7		SLTS	37.	7.	. 7.			51.	
60.04	98.4	17.4		34.	7.	5,			46.	
63.09	98.0		SLTS	12.	5.				17.	
1			SNDS	19.	2.				21.	
66.14	99.0	37.0	SLTS	31.	1.	4.			36.	•
			SNDS	2,	• •	10.			12.	
69.19	96.7	28.5	MDST	10.					10.	
			SLTS	24.	1.	2.			27.	
72.24	91.8	62.3		8.	• •				27. 8.	
72.85	104.9	26.2		10.	2.				12.	
72 45	83.5	36.3			4.	•			6.	
73.40			MDST	5.	, -				5.	
			SLT5	16.	1.				17.	
75.28	101.6	49.2	SLTS	35.		10.			45.	
78.33	112.0	74 9	COAL	3.					3.	
		3	SLT5	15.	3.				18.	
75.28 78.33 80.16 81.08	41.3	٥	COAL	5.	٥.	25.			30.	
81.08	41.8	.0		J.		100.			100.	
	101.6	27.9	COAL	6.	1.	25.			32.	
82.60	92.9	.0		32.	3.	25. 25.			60.	
81.99 82.60 84.43	95.1		MDST	20.	2.	23.				
57.75	- J 1	55.5	SLTS	19.	1.				22.	
87.48	89.7	54 0	COAL	5.					<u>20</u> .	
37.46	55.7	57.0	JUAL	5.					5.	

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START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
87.48	89.7	54.0	SLTS	14.	3.	•			17.	
89.61	78.3	13.0	COAL	14.	<u>2</u> .	25.			41.	
90.53	100.3	16.8		8.	4.	20.			12.	
			MDST			45.			45.	
93.57	99.6	13.1		5.				25	30.	
			MDST			35.		2 <u>5 .</u> 25 .	60.	
96.01	99.7	11.1	COAL	2.	1.	50.		20.	53.	
			MDST	3.	2.				5.	
			SLTS	32.	8.				40.	
99.06	65.6	16.9	COAL			20.				
			5LTS	8.	11.	•			19.	
100.89	72.1	21.9	CBSH			5.			5.	
			COAL	3.	4.				7.	
			MDST	11.	4.				15.	
102.72	98.7	32.6	, SLTS	33.	6.	8.			47.	
105.76	85.9		COAL	21.	3.	20.			44.	
			SLTS	15.	8.				23.	
108.66	63.6	.0	COAL	3.	3.	104.	1		110.	
109.73	95.3	12.2	COAL	6.	2.				8.	
			MDST	33.	3.				36.	
111.86	87.9	13.4		46.	6.	7.			59.	
114.91	96.1	42.3	MDST	14.		20.			37,	
			SLTS	15.		10.			25.	
117.96	108.0	38.3	CBSH	2.					2.	
			COAL	3.		200.			203.	
			MDST	12.	4.				16.	
			SLTS	18.	3.				21.	
120.70	83.6	3.0	COAL	30.	14.	30.			74.	
			MDST	17.	12.	37.			66.	
124.05	92.5	19.0	MDST			11.			11.	
			SNDS	18.	29.	55.			102.	
127.10	99.0	58.0		33.	16.	11.			60.	
130.15	90.2	28.2	SNDS	30.	6.	48.			84.	
133.20	93.7	13.8	COAL	5.	1.	10.	·		16.	
			MDST	45,	4.				49.	
136.24	96.4	59.0		14.	4.				18.	
			MDST			29.			29.	
139.29	92.8	9.5	-			35.		50.	85.	
142.34	95.7	4.3	_	10.	3.	33.			46.	
			SLTS	19.	9.				28.	
145.39	64.1	11.6		17.	2.	40.			59.	
			MDST	16.		22.			38.	
			SNDS	4.					4.	
148.59	123.4	7.0	COAL	4.					4.	
			MDST	21.	<u>8.</u>				29.	
			SLTS	12.	Ž.				14.	

START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIËD FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
151.03	94.4	26.9	COAL	3.					3.	
			MDST	20.					20.	
			SLTS	12.	1.				13.	
154.23	25.4	. 0	COAL	14.		20.			34.	
155.45	18.7	.0	COAL	4.	1.	5.			10,	
156.36	73.8	12.3	COAL			20.			20.	
			MDST	9.	6.				15.	
157.58	100.0	56.7	MDST	16.	2.	,			18.	
			SNDS	8.					8.	
160.63	91.8	80.0	SLTS	7.	1.	1.			9.	
			SND5	3.		4.			7.	
163.68	95.4	40.1	CDAL	6.					6.	
			MDST	16.	2.	5.			23.	
			SLTS	6.	2.				8.	
166.72	99.3	30.5	CDAL	4.	1.	5.			10.	
•			MDST	5,					5.	
			SLTS	20.	1.	4.			25.	
169.77	96.7	21,6	SLTS	24.	10.				34.	
172.82	101.0	32.5	SLTS	40.	4.				44.	
175.87	102.3	19.7	SLTS	44.	2.				46.	
178.91	92.7	23.6	SLTS	15.					15.	
180.14	90.5	6.9	MDST	9.	1.	12.			22.	
183.18	89.8	4.9	MDST			33.			33.	
186,23	92.8	7.2	MDST			31.			31.	

START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLÖĞY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
18,59	91.5	.0	MDST							
20.12	96.7	12.3		11.		65.	 -		65.	
20.12	30.7	12.3	SNDS	17.	2. 2.	10.			13.	
22.55	96.4	27 4	SLTS	25.	6.	10.			29.	
22.00	30.4	27.4	SNDS	7.	2.	10.			41. 9.	
25,91	103.0	5.7	SLTS		7.					
28.55	100.7	4.3	SLTS	24.	9.				36. 33.	
31.70	93,1		SLTS	28.	6.					
		20.2	SNDS	20.	٠.	6.			34. 6.	
34.75	101.0	34 9	SNDS	·		28.			28.	
37.79	99.0		SNDS			47.			47.	
40.84	99.0		SLTS	10.	4.	71.			47. 85.	
43.89	99.Q		SLTŠ	27.	14.	, , ,			85. 41.	
46.94	93.1		SLTS	28.	3.	10.			41.	
50,29	97.7	12.1	SLTS	36,	11.	10.			41. 48.	
53.34	99.3		ŠLTŠ	31.	13.	١.			44.	
56.39	98.0	16.7	SLTS	35.	2.	22.			44. 59.	
59.74	99.0	7.5	SLIS	28.	5 .	2.			39.	
62.79	100.0	23.3	SLTS	34.	12.	25.				
65.94	101.6	4.6	MDST	J7.	12.	48.	•		71.	
68.88	89.9		MDST			23,			48.	
30.00		22.0	SNDS	8.	3.	10.			<u>23</u> .	
72.24	49.2	6.0	MDST	6.	o.	10.				
, 2.24	73.2	0.0	SNDS	٠.		106.			6.	
74.07	62.0	0	SLTS	18.		100.			106.	
75.28	96.7	21.6	SLTS	46.	5.				<u>18.</u> 51.	
78.33	101.3		SLTS	36.	10.	20.				
,0.00	101.0		SNDS	5.	10.	20.			66. 5.	
81.38	87.2	13.1		1						
			MDST	8.		120.			1.	
			SNDS	14.	4.	120.			128.	
84.12	22.6	.0	COAL	14.		10.			18. 10.	
84.43	94.8	5.6	MDST			43.			43.	·
<u> </u>			SLTS	17.	5.				22.	
			SNDS	13.	1.				22. 14.	
86.56	97.8	29.3		13.	1.				14.	
87.48	100.0		MDST	13.					13.	
		- 	SLTS	2 i .					21.	
			SNDS	24.	5.				29.	
90.52	100.0	٠.٥	COAL		<u>-</u> .	15.			15.	
			MDST	8.		75.			8.	
90.83	37.7		COAL	2.		·· · · · · · · · · · · · · · · · · · ·		50.	52.	
		. 0	SNDS	4.				50.	⊒ <i>z.</i> 4.	
91.44	88.2	.0	MDST	4.	1.				5.	
		•	SLTS	23.	3.				26.	
			SNDS	8.					<u> </u>	

				LOCAT	IDN = TW83D	-332				
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
92.96	-1.0	.0	COAL							
93.27	95.4	.0	MDST	34.	4.			10.	48.	
94.79	102.7	19.7	SNDS	17.	9.	20.			46.	
96,62	77.9	.0	MDST				•	100.	100.	
		_	SNDS	13.					13.	
97.84	41.0	.0	COAL			100.			100.	
98,45	32.3	.0	COAL			20.			20.	
98.76	91.2	.0	COAL			10.			10.	
			SLT5	14.	5.				19.	
99.67	98.7	17.7		44.	5.				49.	
			SNDS		1,				1.	
102.72	83.2	6 9	SLTS	38.	7.		15.		60.	
	00.2	0.0	SNDS	10.			13,		10.	
105.76	109.B		COAL			· 2.			2.	
100.10	105.0	- 0	SLTS	59.	5.					
108.51	26.7	0	CDAL	33.	J.	. 50. 15.			114.	
108.81	26.2	.0							15.	
109.42	69.6	.0		20.		50.			50.	
103.42	09.0	.0				20			20.	
			COAL	5.	3.	20.			28.	
440.04		_	MDST	3.				50.	53.	
110.34	62.6					15.			15.	
			SLTS	8.				25.	33.	
444.05		_	SNDS	9.					9.	
111.25	23.0		COAL			15.			15.	
111.86	73.8	.0				50.			50.	
112.47	94.7	6.6		28.	4.			100.	132.	
		_	SNDS			3.			3.	
114.91	88.0	.0	SLTS	23.	2.				25.	
			SNDS	9.		25.			34.	
117.65	70.6	.0		3.		20.			23.	
			MDST	8.		100.	100.		208.	
			SNDS	8.					8.	
119.18	54.9	Q	COAL	2.		2.	100.		104.	
120.09	16.5	.0	COAL			50.			50.	
121.00	96.7	.0	SNDS	61.	5.				66.	
124.05	96.1	.0	SND5	28.	6.		20.		54.	
127.10	88.5	15.4	SNDS	21.	20.				41.	
130.15	93.7	19.4	SNDS	37.	5.				42.	
133.19	98.0	32.5	SNDS	41.	3.				44.	
136.24	92.8	45.6	SNDS	34.	7.				41.	
139,29	45.9	.0	MDST					500.	500.	•
			SNDS	24.	7,	30.			61.	
142.31	94.4	5.9	MDST			19.		700.	719.	
			SNDS			13.			13.	
145.39	102.3	46.9				27.			27.	
148.44	101.0	51.3		8.					4	

				LOCAT	ION = TW83D	-332				
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FRACTURES	FRACTURES	
151.48	95.4	14.8		3.				100.	103.	
154.53	96.4	8.9	SNDS COAL MDST SLTS	29. 9.	8.	5. 100.			37. 5. 100. 13.	
157.58	90.8	13.4	SNDS SLTS SNDS	44. 2. 54.	6. 4.		1.		50. 3. 58.	
160.63	92.8	26.2	SNDS	39.		10.		-	65.	<u> </u>
										
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				LOCAT	ION = TW83D	-333			
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL Fractures
10.67	100.3	, 0	SLTS	46.	5.				51.
13.72	53.4	. ō	MOST	28.	1.	-···			29.
17.37	114.5	. 0	MDST	28.	4.				32.
19.51	84.8	.0	MDST	39.	1.	2.			42.
23.47	102.3	4.9	MDST	52.	1.	3.			56.
26,52	98.0	9.9	MDST	45.	2.	•			47.
29.56	99.7	12.8	•	34.	2.				36.
			SLTS	15.					15.
32.61	98.4	.0		18.	8.	•			26.
		·	SNDS	25.	18.	• • • • • • • • • • • • • • • • • • • •			43.
35.66	93.8	. 0	CDAL	5.	4.				9.
	00.0		MDST	33.	8.				41.
			SLTS	15.	4.				•
			SNDS	5.	4.	<u> </u>			19.
38.71	90.8	21.5		39.	7.	4.			9.
41.76	107.4		COAL	16.		400			46.
41.70	107.4	23.0			2.	100.			118.
44.20	95.6	····	MDST	21.	<u>9</u> .				30
_		5.9		43.	5.	_			48.
47.40	89.8	8.8	CBSH	8.	_	1.			9.
40 77	50.0	40.0	COAL	13.	2.	3.			18.
48.77	53.8	19.8		<u> </u>	2.				4.
49.68	82.8	18.9	COAL	2.		3.			5.
			MDST	10.	1.	1.			12.
			SLTS	7.		1,			8.
50.90	72.5		SLTS	32.	5.				37.
53.95	93.4	17.7		41.	6.		15.		62.
57.00	99.7	8.6	SLTS	22.	5.				27.
			SNDS	26.	4.				30.
60.04	148.4	11.5		33.	2.	1.			36.
61.26	80.3	. 0	SLTS	31.	6.				37,
63.09	94.5	14.3	COAL	3.		2.			5.
			MDST	5.	2.				7.
			\$LT\$	8.	1.				9.
64.00	90.2	.0	MOST	18.		3.			21.
			SLTS	11.	5.				16.
65.84	87.4	6.6	COAL	9.	5.				15.
			MDST	21.	6.		25.		52.
67.66	105.9	7.8	COAL	5.	<u>3</u> .				8,
			MDST	28.	5. 5.				34.
69.19	99.3	8.5	MDST	11.	4.				15.
02.72		0.0	SLTS	29.	10,				39.
72.24	105.7	75. 7	CDAL	Ž.	10.				2.
12.27	100.1	55.1	St.TS	16.	2.				
			SNDS	13.	3.				18.
74.68	69.7	^	CDAL		J.				16.
				10.				100.	110.
75.90	80.0	.0	CDAL	5.				100.	105.

				LOCAT	ION = TM83D	-333				
	RECOVERY PERCENT	R.Q.D.	ĹÍTHÖLÖĞŸ	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
76.50	101.6	.0	COAL	18.	3.				21.	
77.72	68.5	. 0	COAL.	5.	1.				6.	
78. 6 4	104.4		COAL	5.					5.	
			MDST	29.			1.		30.	
			SLTS	9.	1.				10.	
80.47	74.6	. 0	COAL	10.	5.				15.	
81.69	81.4		COAL	16.	4.				20.	
			MDST	6.	1.				7.	
83.52	94.2	9.1	CBSH	6.	1.		3.		10.	-
			MDST	17.	3.				20.	
84.73	95.3	.0	COAL	10.	5 .				16.	
			MDST	3.	1.				4.	
			SLTS	22,	5.				27.	
87.48	96.7	29.6	SLTS	11.	3.				14.	
	•		SNDS	9.	8.				17.	
90.52	102.0	. 0	SLTS	37.	7.				44.	
• • •			SNDS	12.	8.				20.	
93.57	92.8	19.7	ŠLTS	53.	7.				60.	
96.62	101.8		COAL	14,	1.	2.			17.	
00.02	,01.0		MDST	39.	1.	4 -			40.	
99.36	100.3	40.1		41.	2.				43.	•
102.41	100.0	30.5		20.					22.	
.02.	,,,,,	00.0	SNDS	12,	3.				15.	
105.46	101.1	0	COAL	3	٥.				3.	
			SNDS	9,	8.				17.	
106.38	92.6	.0		32.	13.				45.	
108.81	97.4		CBSH	1.	10.				49.	
,	• • • • • • • • • • • • • • • • • • • •	,2.0	COAL	э.	1.				4.	
			MDST	43.	6.		30.		4. 79.	
111.86	97.4	20.3		11,	4.					
171100	07.1	23.0	SLTS	26.	6.	4.			36.	
114.91	116.4	45 9	COAL	Lo.	٠.	7,			ათ.	
		,0.0	SLTS	5.	5.				10.	
115.52	88.9	12.7		1.					1.	
	****	,	COAL	12.	7.				19.	
			MDST	'	· ·	18.			18.	
117.96	98.6	. 0	MOST			33.	•		33.	
			SLTS			18.	· -		18.	
120.09	88.5	n	COAL	2.		10.			18.	
			MDST	٤,		33.			2. 33.	
121.92	81.2	15.5	CDAL	17.	2.	1_				
			MDST		<u></u>		30.		20. 30.	
124.05	98.0	54.1					30. 30.		30. 30.	
	55.0	V,	SNDS	29.	10.		30.		30. 39.	
127.10	99.3	٥	SNDS	49.	12,				62. 60.	
			01700	23 .	14.	•	1		n 2	

START OF	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
133.20	95.7	7.2	SNDS	19.	19.				38.	
136.24	97.7	3.6	SNDS	44.	3.				47.	
139.29	92.5	4.9	SNDS	58.	10.				68.	
142.34	100.7	.0	SNDS	61.	7.				68.	
145.39	92.8	.0	SNDS	39.	12.				51.	
148.44	99.7	Ō	CBSH	7.		·		······································	7.	
			COAL	26.	3.	101.			130.	
			MDST			229.			229,	
			SNDS	16.	2.				18.	
151.48	79.0	. 0	CB2H	7.				• • • • • • • • • • • • • • • • • • • •	7.	
			COAL	З.		100.			103.	
			MDST	42.	10.	34.			86.	
154.53	92.2	. 0	CBSH			29.			29.	
			COAL			150.			150.	
			MDST	31.	1.	109.	25.		166.	
156.97	93.8	12.8	SLTS	44.	1.	1.			46.	
160.17	98. <u>1</u>	3.7	SLTS	55.	1 <u>2.</u> 8.				67.	
163.37	100.0	.0	SLTS	56.	8.	2.			66.	
166.42	95.7	.0	MDST			54.			54.	
169.47	99.7	12.1	MDST			19.			19.	
			SLTS			44.			44.	
172.52	101.6	7.9	SLTS			46.			46.	
175.56	98.1	30.0	SLTS			56.			56.	
178.76	91.6	9.4	SLTS			73.			73.	
181.96	100.0	6.9	SLTS			61.			61.	
185.01	85.9	25.9	SLTS			49.			49.	
			SNDS			17.			17.	

LOCATION = TW83D-334

START OF	RECOVERY	R.Q.D.	LITHOLOGY		JOINT	UNCLASSIFIED			TOTÁL	
CORE RUN	PERCENT			FRACTURES	FRACTURES	FRACTURES	FRACTURES	FRACTURES	FRACTURES	
10.36	75.0	.0	SNDS	12.		10.			22.	
11.28	97.7	.0	COAL	19.	6.	11.			36.	
			SLTS	36.	4.				40.	
			SNDS	15.		8.			23.	
14.32	89.8	.0	COAL	3.					Э,	
			SLTS	44.	10.	3.			57 <i>.</i>	
17.37	103.3	5.6	NTRK							
			SLTS	44.	4 .				48.	
			SNDS	8.	3.	2.			13.	
20.42	28.4	.0	SNDS	3.	2.	50.			55.	
22.25	104.1	-0		23.	7.	3.			33.	
23.47	98.7	.0	SLTS	41.	1.				42.	
			SNDS	20.	2.	1.			23.	
26.52	92.1	.0	COAL	13.		51.		200.	264.	
			MDST	35.		10.			45.	
			SLTS	26.	2.				28.	
29.56	83.6		COAL	44.		252.			296.	
32.61	102.0		SLTS	53.	1.	20.			74.	
35.66	98.4	13.8	SLTS	42.	6.	1.			49.	
38.71	98.0	0 0	SNDS	4.					4.	
30.71	98.0	8,9	SLTS SNDS	15.	3.				18.	
41.76	101.0	40.0	SLTS	34.	2.				36.	
44.80	98.0			58.	3.	6.			67 .	
44.80	98.0	.0	SLTS SNDS	40. 6.	7.				47.	
47.85	99.7		SLTS	28.					6.	
47.85	55.7	.0	SNDS	4.	6. 5.				34.	
50.90	98.0	ធឲ	SLTS	36.	3.				9.	
5 3.95	95.1		MDST	63.	3.				39. 66.	
57.00	96.4	30.3	CBSH	4.					4.	
37.00	₩. ¬	50.5	COAL	3.	14.	10.				
			MDST	18.	1-9.	10.			27. 18.	
60.04	100.7	. 0	CBSH	3.					3.	
			COAL	3.	1.				4.	
			MDST	8.	19.				27.	
63.09	97.7	.0			,	31.			31.	
66.14	95.7	.0				31.			31.	
69.19	101.6	· · · · · · · · ·	MDST	-		9.			9.	
		_	5LT5	23.	17,	<u>.</u> .			40.	
			SNDS	11.	4.				15.	
75.28	94.1	15.1	COAL	• • •	• •	10.			10.	
			SLTS	14.	20.				34.	
78.33	89.2	4.9	COAL	7.	2.	110.			119.	
			MDST	6.	3.	-			9.	
			SLTS	9.	6.	13.			28.	
81.38	86.7	18.2	COAL	2.	1,	10.			13.	

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				LOCAT	ION = TW830	-334				·
	RECOVERY PERCENT	Ř.Ö.Ö.	LITHOLOGY	BEDDING FRACTURES	FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FRACTURES	FRACTURES	·· · · · · · · · · · · · · · · · · · ·
81.38	86.7		SLTS	9.	8.		*****			
84.43			SLTS	26.	6.				17. 32.	
87.48			SNDS	12.	7.				32. 19.	
90.53		24.9	SNDS	19.	13.				32.	
93.57	94.1	28.9	SNDS	14.	9.				23.	
96.62	83.6	15.0	St.TS	10.	4.	20.		*****	34.	
			SNDS	5.					5.	
98.75	91.1	25.6	MDST	11.		13.			24.	}
			SLTS	4.					4.	İ
101.80			MDST	7.	•	25.	90.		122.	
104.85	93.4	28.5	MDST	15.		6.	50.		71.	
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				LUCAI	ION = IMB3D	-335				
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY		JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
3.96	73.8	.0	SLTS	8.		50.	****		58.	
5.18	61.5		SLTS	24.	5.	50.				
7.62	77.9		SLTS	13.	J .	50.			63.	
8.84	90.2		SNDS	13.		30. 34.			34.	
11.28	77.3		COAL	6.		20.			26.	
	77.3		SLTS	18.		27.	·- · · · - 		45.	
			SNDS	17.		27. 20.			45. 37.	
14.32	83.9	0	COAL	10.	2.	1.			13.	
14.42	00.5	.0	SLTS	49.	2.	200.			251.	
			SNDS	49.		50.			<u>251.</u> 50.	=
17.37	87.5	22.0	COAL	26.	5.	50. 15.				
17.37	\$1.3	23.0	MDST	28. 28.	3.	15.			46.	
20.42	95.7	_	COAL	26. 8.					31.	
20.42	90.1		SLTS		2.	1.			11,	
23.47	00.4	2.0		63.	4.				67.	
	93.1		SLTS	67.	4.	-			71.	
26.52	96.4		SLTS	75.	2.	2.			79,	
29.56	100.3		SLTS	74.	2.				76.	
32.61	92.1		SLTS	63.	<u>1</u> ,				68.	
35.66	101.0	.0	SLTS	41.	5.	50.			96.	
			SNDS	22.		6.			28.	
38.71	98.Q	12.1	COAL	3.					3.	
			SLTS	48.	3.				51.	
41.76	85.9	4.6	COAL	18.	5.				23.	
			MDST			14.			14.	
			SLTS	20.		3.			23.	
44.80	95.4	25.9	COAL	1.	2.				3.	
			SLT\$	35.					35.	
			SNDS	12.		3.			15.	
47.85	82.0	.0	CBSH	<u>5.</u>					5.	
			COAL	25.	3.	151.			179.	
			MDST	25.			,		25.	
50.90	99.0	10.5	MDST	67.	9.	2.			78.	
53.95	98.4	34.8	COAL	3.	2.				5.	
			MDST	26.					26.	
			SLTS	18.	1.	1.			20,	
57.00	87.8	22.4	CDAL	15.		12.			27.	
			SLTS	29.	4.	•	1.		34.	
60.04	88.2	8.5	COAL	18.	4.	15.			37.	
			MDST	3.			6.		9.	
61.57	94.1	٥.	CBSH	5.			٥.		5.	
	- , -		CDAL	16.	1.				17.	
			MDST		· · · · · · · · · · · · · · · · · · ·	18.			18.	
63.09	97.0	16.7	CBSH	9.		10.			9.	
-5.50	٠٠		COAL	14.	3.				17.	
					J.					
			MDST	33.					33.	

LOCATION = TWB3D-335

ULT FAULT ZONE TOTAL S FRACTURES FRACTURES
38.
36.
21.
15.
25.
37.
40.
43.
8.
78.
8.
100. 103.
25, 63.
9.
100, 103.
7.
56.
20.
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23.
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50. 64.
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15. 35.
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15. 43.
11.
52.
48.
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29.

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				LUCAT	ION = TW83D	334				
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES		FAULT ZONE FRACTURES	TOTAL FRACTURES	
8.23	85.2	.0	SLTS			38.			38.	
11.28	87.6	. o				128.			128.	
14.02	98.4		SLTS			131.			131.	
17.07	83.6		5LT5			21.			21.	
17.68	82.1		SLTS			49.			49.	
20.42	105.7	·····	SLTS			29.	· -···		29.	
21.64	60.1		SLTS			31.			31.	
23.47	95.1		SLTS			32.			32.	
26.52	92.1		SLTS			51.			51.	
29.56	90.2		SLTS			Ť <u>.</u>			19.	
32.61	93.4	•	SLTS			39.			39.	
35.66	94.4		SLTS			30.			30.	
38.71	92.1		SLTS			15.			15.	
	22.1		SNDS			32.			32.	
41.76	97.4	15.5	SNDS			33.				
44.80	95.1		SLTS						33.	
44.60	55.1	.0	SNDS			45.			45.	
47.85	96.1								10.	
			SLTS			52.			52.	
50.90	88.5		SLTS	F.6		70.			70.	
53.95	91.8		SLTS	56.	15.	3.	50.		124.	
57.00	78.3	.0	COAL						15.	
			MDST		_	22.			22.	
		_	SLTS	22.	3.	50.			75.	
60.04	66.2	.0	COAL	1.	5.	43.			49.	
			MDST			61.	75.		136.	
63.09	96.7	.0	SLTS	9.	2.				11.	
			SNDS	35.					35.	
66.14	13.1		MDST				25.		25.	
66.75	91.0	19.7	CBSH			<u> </u>			5.	
			CDAL	19.	1.	50.			70.	
			MDST			15.			15.	
			SLTS	11.		•			11.	
69.19	93.4		MDST			15.			15.	
69.80	98.4	41.0	COAL	3.					3.	
	•		MDST	7.	2.				9.	•
70.41	88.5	.0	COAL	5.					5.	
			MDST			33.			33.	
			SLTS	12.	3.				15,	
72.24	95.7	9.2	SLTS	6 5.	4.				69.	
75.28	104.3		SLTS	50.	1.	2.			53.	
81.38	99.0	.0	SLTS	47.	4.	_ 28.			79.	
84.43	98.4		MDST			32.			32	
		-	SLTS			46,			46.	
B7.48	100.0	.0	SLTS			36.			36.	
· · · · · -			SNDS			36.			36.	
90.52	100.0	õ	ŠNDS			63.			63.	

•				LOCAT	10N = TW83D	-33 6				
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY		JOINT FRACTURES		MINOR FAULT FRACTURES	FRACTURES	FRACTURES	
93.57	99.0	7.9	SNDS			56.			56.	
96.62	100.7	13.1	SNDS			64.			64.	
99.67	96.7		SNDS			35.			35.	
102.11	97.7		SNDS	27.	2.	26.			55.	
105.16 108.70	97.4	33.2	SNDS SNDS	31.	1-	20.			52.	
108.70	97.4	8.9	2140.2			57.			57,	
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START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY		JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
7.32	96.7	.0	SLTS	17.	3.				20.	
7.92	79.8	.0	SLTS	71.					74.	
11.28	52.6	•	CBSH		٠.				74.	
	02.0		MDST	12.					12.	
			SLTS	8.		1.			9.	
13.41	83.6		MDST	17.					11.	
		. •	SLTS	41	3.				44.	
16.46	78.7	. 0	COAL		٠.				4.4.	
,	, = , .		SLTS	45.	1.				46.	
18.29	82.2	. 0		27.		2.			29.	
19.81	90.1		SLTS	49,	3,				52.	
23.16	79.5		SLTS	34.	1.				35.	
25.60	90.7		CBSH	3.	• •	200.			203.	
			SLTS	35.					35.	
27.74	85.7	- 0	CBSH			. 32.			32.	
			SLTS			16.			16.	
29.56	98.4	0	OTHR			45.			45.	
32.61	99.3	ŏ.	ÖTHR			102.			102.	
35.66	101.0		OTHR			52.			52.	
38.71	114.8	.0				11.			11.	
39.32	93.9	.ŏ	OTHR			47.			47.	
41.76	96.7	.0	OTHR			52.			52.	
. 44.80	99.3	5.9	SNDS	47.	4.	1.			52.	
47.85	97.4		OTHR	7, ,	⊸.	22.			22.	
.,,,,,,	07.7	,	SNDS	3.	3.	20.			26.	
50.95	iōi.ō	.0	DTHR		<u> </u>	39.			39.	
53.95	95.7	.0	DTHR			48.			48.	
57.00	102.6	. 0	OTHR			. 46.			46.	
60.04	99.3	.0	OTHR			. 48. 48.			48. 48.	
63.09	99.3		OTHR			39.			39.	
66.14	96.1	.0	SNDS			77.			39. 77.	
69.19	99.7	8.9		38.	11.	1.				
72.24	90.1		OTHR	30.	11.	36.			50. 36.	
			SNDS	9.	4.	2.		·		
75.28	92.8	^	OTHR	٦,	7.	65.				
78.33	95.4		SLTS			65. 66.			65.	
81.31	100.3	.0				76.			66. 76	
84,43	92.5		CBSH						76. 50.	
07.73	Ve., J	.0	MDST			27.		50.	77.	
			SLTS			27. 45.		50.	//. 45.	
87,48	86.2	/3	CBSH			40.		EO		
07.40	o∪, <u>*</u>		CDAL			3.		50.	50.	
			MDST					400	3.	
89.00	82.2	_	COAL			36.		100.	136.	
99.00	02.2	.0	MDST					20.	20.	
			1 COM					100.	100.	

START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FÄULT ZÖNE FRACTURES	TOTAL FRACTURES	
90.52	83.6	.0	CBSH					200	200.	
			COAL					525.	525.	
			MDST			66.		100.	166.	
			SLTS			10.			10.	
93.57	96.4	16.7	CBSH	1.		4.			5.	
			COAL	9.					9.	
			MDST			29.			29.	
			SLTS	28.	6.				34.	
96.62	100.3	37.0	SLTS	39.	2 -				41.	
99.67	99.O	21.3	MDST	39.	5.	1.			45.	
102.72	97.1	29.2	MDST			43.			43.	
105.46	95.1	18.4	MDST			47.			47.	
108.51	100.7	14.1	MDST			10.			10.	
			SLTS			52.			52.	
111.56	102.3	53.0	SLTS			35.			35.	
114.60	96.1	52.5	SLTS			29.			29.	
117.65	102.0	49.8	SLTS			60.			60.	
120.70	87.5	48.2	SLTS			43.			43.	

.0	SLTS SLTS SLTS SLTS SLTS SLTS SLTS SLTS	30. 105. 113. 107. 78.	1. 3. 11. 6.	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES 32. 108.	
.0	SLTS SLTS SLTS SLTS SLTS SLTS	30. 105. 113. 107. 78.	3. 11. 6. 11.					
.0 .0 .0 .0 .0	SLTS SLTS SLTS SLTS SLTS SLTS	105. 113. 107. 78.	11. 6. 11.	,				
.0 .0 .0 .0 .0	SLTS SLTS SLTS SLTS SLTS	113. 107. 78.	11. 6. 11.				100.	
.0 .0 .0	SLTS SLTS SLTS SLTS	107. 78.	6. 11.				124.	
.0	SLTS SLTS SLTS	78.	11.				113.	
.0 .0 .0	SLTS SLTS			3.			92.	
.0	SLTS		6.				81.	
. 0		79.	8.	2.	50.		139.	
		81	2.		50.		83.	
ч								
3.5		<i>*</i>	•	4				•
		20	١.		•			
16 /								
10.4	****				· · · · · · · · · · · · · · · · · · ·			
			^	29.	50.			
99.9		17.	2.					
32.2								
			_	5.				
		14.	3.					
				-				
. 0								
						50.		
_		55.	8.					
				•••		999,	1005.	
							63.	
			4.				84.	
.0							38.	
		33.	6.	20.			59.	
٠٥						999.	999.	
	SNDS	37.	5.				42.	
.0	GOUG					999.	999.	
-0	GOUG					999.	999.	
.0	GOUG					750.	750.	
	SNDS	8.		1.				
-0	SNDS	46.	1.					
.0	SLTS	57.	1.	1.				
	SNDS	32.	5.					
.0	COAL					50		
		Ä	·	20		200.		
0			1.4					
		0 1.	14.	1.		05		
10.3		En	A			25.		
. ^		32.				1100		
	16.4 32.2 .0 .0 .0 .0 .0 .0 .0 .0	.O GOUG SNDS .O SNDS .O SLTS	5.9 COAL 2. SLTS 38. 16.4 COAL 2. SLTS 39. SNDS 17. 32.2 CBSH COAL SLTS SNDS 140 SLTS SNDS 550 MDST SLTS SNDS 550 SLTS 6. 4.2 SLTS 590 SLTS 770 SLTS 180 SLTS 180 SLTS 330 GOUG SNDS 370 GOUG SNDS 370 GOUG SNDS 370 GOUG SNDS 460 SLTS 570 SLTS 570 SLTS 570 GOUG SNDS 460 SLTS 570 SLTS 570 SLTS 570 GOUG SNDS 460 SLTS 570 COAL GOUG SLTS 570 SLTS 57.	5.9 COAL 2. SLTS 31. SNDS 38. 16.4 COAL 2. SLTS 39. SNDS 17. 2. 32.2 CBSH COAL SLTS SNDS 14. 3	5.9 COAL 2. SLTS 38. 9. 16.4 COAL 2. 4. SLTS 39. 29. SNDS 17. 2. 32.2 CBSH 14. COAL 100. SLTS 5. SNDS 14. 3. .0 SLTS 50. .0 MDST 9. SLTS 50. 9. .0 SLTS 25. .0 SLTS 6. 4.2 SLTS 59. 3. 1. .0 SLTS 77. 4. 3. .0 SLTS 18. 20. .0 SLTS 33. 6. 20. .0 GOUG 5. 5. 1. 1. .0 GOUG 5. 5. 5. 20. .0 GOUG 5. 5. 5. 20. .0 GOUG 5. 5. 5. 5. .0 <t< td=""><td> S. COAL SLTS SL</td><td>5.9 CDAL 2. 1.</td><td>5.9 CDAL 2. \$1. 1. 2. \$1. 1. 2. \$47. 16.4 CDAL 2. 4. 6. \$1.5 \$1. 6. \$1.5 \$1.5 39. 29. \$50. \$118. \$19. \$18. \$19. \$18. \$19. \$19. \$19. \$19. \$19. \$118. \$19. \$19. \$118. \$19. \$19. \$118. \$19. \$19. \$19. \$19. \$19. \$19. \$19. \$19. \$100. <t< td=""></t<></td></t<>	S. COAL SLTS SL	5.9 CDAL 2. 1.	5.9 CDAL 2. \$1. 1. 2. \$1. 1. 2. \$47. 16.4 CDAL 2. 4. 6. \$1.5 \$1. 6. \$1.5 \$1.5 39. 29. \$50. \$118. \$19. \$18. \$19. \$18. \$19. \$19. \$19. \$19. \$19. \$118. \$19. \$19. \$118. \$19. \$19. \$118. \$19. \$19. \$19. \$19. \$19. \$19. \$19. \$19. \$100. <t< td=""></t<>

START OF	RECOVERY	$\bar{R}, \bar{Q}, \bar{D}$.	LITHOLOGY	BEDDING	JOINT	UNCLASSIFIED	MINOR FAULT	FAULT ZONE	TOTAL	
ORE RUN	PERCENT			FRACTURES		FRACTURES	FRACTURES	FRACTURES	FRACTURES	
78,33	96.4	.0	NTRK			,				
81.38	82.5	.0	SNDS	36.	4.				40.	
84.12	99.3	.0	SLTS	19.	29.				48.	
B7.17	96.4	.0	SLTS	38.	11.				49.	
90.22	95.2	.0	SLTS					999.	999.	
93.57	101.3	ö.	SLTS	61.	2.				63.	
96.62	96.7	10.2	SLTS	50.					50.	
99.67	98.7	14.1	SLTS	42.	1.	1.			44.	
102.72	95.4		SLTS	63.	8.			50.	121.	
105.76	101.6	-0	SLTS	56.	16.	1.			73.	
108.81	101.3		SLTS	49.	9.				58.	
111.86	97.4		SLTS	36.	10.				46.	
114.91	93.1	8.9	SLTS	16.	15.	14,		20.	65.	
117.96	93 1		SLTS			52.			52.	
121.01	101.0		SLTS			52. 68.			58.	
124.05	91,1		SLTS			55.			55.	
127.10	96.4		SLTS			47.			47.	
130.15	89.5		COAL					25.	25.	
100.15	05.5	.0	GOUG					999.	999.	
132.44	67.7	0	COAL	6.	3.	1.				
134,11	87.3		COAL	Ο.	٥.	1.		999.	1009.	
134,11	01.3		SLTS	35.		·		200.	200.	
136.24	98.0	22.0			13.	2.			50.	
			SLTS	55.	9.				64.	
139.29	101.0	8.2	SLTS	1.	4.	1.			_6.	
142.34	91.5		SNDS SLTS	49.	8.				57.	
142.34		8.2		53.	5.			15.	73.	
145.39	82.3	.0	COAL	12.	1.	_		150.	163.	
			MDST	3.		6.			9.	
			SLTS					200	200,	
148.44	96.1	38.5	MDST	8.	2.				10.	
			SNDS	39.	4.	1.			44.	
151.48	73.4	4.3	COAL					300.	300.	
			MDST	53.	6_	20.			79.	
			SNDS	3.					3.	
154.53	94.8	.0	COAL	1.	2.	50.			53.	
			SLTS	43.	22.	10.			75.	
157.58	97.7	.0	SLTS	41.	5.				46.	
			SNDS	28.	3.				31.	
160.63	13.1		OTHR							
163.68	90.2	.0	SNDS	56.	10.				66.	
166.12	100.7	. <u>Q</u>		17.	11.	5.			33.	
169.16	101.6	, ō	CBSH					20.	20.	
			COAL	6.	3.	20.		50.	79.	
			MDST			100.			100.	
			SLTS	9.	2.				11.	
			\$ND5	13.	10.				23.	

	TOTAL FRACTURES	FAULT ZONE FRACTURES	MINOR FAULT FRACTURES	UNCLASSIFIED FRACTURES	JOINT FRACTURES		LITHOLOGY	R.Q.D.	RECOVERY PERCENT	START OF CORE RUN
	40.				2.	38.	CBSH	5.8	94.5	172.21
	27.		10.	•••	5.	12.	COAL			
	50.	50.					MDST			
	15.				3.	12.	COAL	.0	114.2	174.96
	78.	50.		28.			MDST			
	5.					5.	COAL	17.B	91.3	176.17
	243.			200.	6.	37.	MDST			
	42.				4.	38.	MDST	22.4	100.3	178.92
	53.			2.	9.	42.	SLTS			
	64,			·· · · · · · · · · · · ·	7.	57,	MDST	٥.	99.0	181.96
	16.			10.		6.		-0	102.5	185.01
	76.			31.	2.	43.	MDST			
	38. 17.			· 1.	4.	33.	COAL	4.9	79.3	187.45
	17.				1.	16.	MDST			
	102.			100.		2.	CBSH	4.9	93.4	190.50
	14.			•	3.	11.	COAL			
	57.			28.		29.	MDST			
			·—				NTRK			
	10.					10.	COAL	15.3	88.5	193.55
•	39.			39.			MDST			
	4.					4.		39.0	97.3	195.38
	43.			25.	6.	12.	MDST			
	42.				1.	41.	SLTS	23.9	100.7	197.20
	43.			1.		42.	SLTS	53.1	100.7	200.25
	41.					41.	MDST	50.8	99.7	203.30
	46.			46.			MDST	31.8	95.1	206.35
	59.			59.			MDST	14.8	103.0	209.40
	51,			51.			MDST	15.7	92.8	212.44

START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	-
8.23	92.8	61.6	SNDS	30.	1.	20.				
11.28	78.6	7.2	MDST	16.	<u> </u>	46.		 	51.	
11.20	70.0	1.2	SNDS	17.					62.	
14.32	65.4	0	COAL	10.		20. 4.			37.	
14.02	05.4	.0	MDST	10,	2.	_			14.	
16.46	48.5	5.1				85. 21.				
10.40	-0.5	J., 1	SNDS	17.	3.	30.				
19.20	78.7	0	MDST	17.	3.	50. 58.			50.	
22.25	41.4	.0				56.		60.	58.	
23.12	76.6	6.0			· · · · · · · · · · · · · · · · · · ·	30.			60. 33.	 · .
25.60	91.8	23.0	SNDS	6.		56.		J.	62.	
28.65	75.4		COAL	3.		4.				
20.00	, , , ,	, . 5	MDST	26.		4.		40.	7.	
			SNDS	9.	9.			40	66. 18.	
31.70	87.2	46.6	SNDS	30,	7.					
35.05	90.2	36.3	SNDS	30.	7.	15.			37. 52.	
38.71	86.9	11.7		3 0.	, .	(3.			52.	
			MDST	6.	· · · · - · · · · · · · · · · · · · · ·	40.			46.	
			SLTS	25.		10.			46. 35.	
40.84	90.2	21.3		20.	2.	60.			35. 82.	
			MDST	15.		40.			55.	
			SNDS	5.	4.		·· =	 -	9.	
43.28	98.4	.0	GOUG	٠.					9.	
		_	MDST	13.		2.	3.		18.	
44,50	38.8	.0	COAL	5.		50.	٥.		55.	
			LC							
46.02	92.9	.0	SLTS	15,		20.		f6.	51.	
47.85	88.5		GOUG					10.	31.	•
			SLTS			8.			8.	
50.90	100.0	.0	MDST						 -	
			SLTS	12.					12.	
53.95	79.8	.0	SLTS	6.		60.			56.	
55.78	106.6	.0	SLTS	10.	5.	40.			55.	
57.00	97.0	13.2	SNDS	33.	2.	19.			54.	
60.04	93.4	11.1	SLTS	56.	17.	70.			143.	
63.09	93.4	.0	COAL							
			MDST	18.	3.	51.			72.	
63.70	92.9	.0	COAL	50.	10.	80.			140.	
65.53	93.9	.0	COAL	15.	3.	, ,			18.	
			MDST	34.	2.	20.			56.	
67.66	86.9	.0	MDST	26.	12.	20.			58.	
69.19	98.7	.0	MDST	86.		61.			147.	
72.23	98.4	.0	MDST	76.	10.	32.			118.	
75.28	28.7	. 0				80.	•		80.	
77.72	105.1	.0.	MDST	10.					10.	

LOCATION = TW83D-339

ORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURÉS	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
79,86	92.1	.0	MDST			50.		50.	100.	
81.38	89.2	3.9	COAL	8.					8.	
			MDST			57.			57.	
			NTRK							
84,43	95.1	. 0	MDST			68.			68.	
			SNDS			65.		20.	85.	
87.48	96.7	10.9	SND\$	35.	18.	40.		25.	118.	
90.52	101.6	. 0	COAL	1.	1.				2.	
			GOUG							•
			MDST	45.	7.	132.			184.	
			NTRK							
			SNDS			10.			10.	
93.57	91.8	7.9	MDST	55.		<u>25.</u>		50.	130,	
96.62	97.7	.0	MDST			98.			98.	
99.67	109.3	.0	MDST	15.	10.	100.			125.	
101.50	72.1	.0	MDST			15.			15.	
102.72	105.3		MDST			80.			80.	
104.24	98.7	19.7	MDST			39.			39.	
105.76	91.8	4.6	MDST			70.		45.	115.	
108.81	91.8	4.9	MDST			90.		80.	170.	

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LOCATION = TW83D-342

START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLDGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
6,10	76.5	. 0	MDST			37.			37.	
8.23	98.4	-0	MDST			68.			68.	
11.28	100.3	.0	MDST			90.			90.	
14.32	92.5	. 0	MDST			. 156.			156.	
17.37	95.1	.0	MDST			115.			115.	
20.42	98.4	7.2	MDST			177.			177,	
23.47	99.7	.0	MDST			109.			109.	
26.52	92.2	.0	MDST			140.			140.	
28.96	88.8	.0				122.			122.	
32.00	85.2	.0	<u></u>			294.			294.	
35.05	101.6	.o.				300.			300.	
38.10	101.6	.0	SLTS			110.			110.	
41.15	87.5		COAL	15.	20.	30.			65.	
			MDST			16.			16.	•
			SLTS			80.			80.	
44.35	103.3	3.9	COAL			17.			17.	
			SLTS	45.	35.	17.			97.	
47.40	90.6	7.8	SLTS	63.	1.	40.			104.	
			SNDS			20.			20.	
50.60	98.7	6.6	MDST	30.		32.			62.	
			SNDS	50.	5.	30.			85.	
53.64	82.1	.0	MDST	80,	i.				81.	•
57.00	71.0	.0	COAL	13.		60.			73.	
			MDST	10.	4.			8.	22.	
58.83	97.5	9,9	COAL	6.	2.				8.	
			MOST	40.		100.			140.	
60.04	103.3	.0	COAL	25.	5.	160.			190.	
			MDST			91.			91,	
62.79	65.8	9.9	COAL	25.	12.				37.	
64.31	88.5	8.7	COAL	10.	4.				14.	
			MDST	60.	8.	40.			108.	
66.14	95.7	.0	MDST	90.	29.	1.			120.	
69.19	101.6	.0	MDST	160.		148.			308.	
			SNDS	2.					2.	
72.28	92.1	.0	COAL	10.	15.			50.	75.	
			SNDS	20.	6.				26.	
74.52	104.2	. 0		50.		200.		155.	405.	
77.11	100.0	.0		200.				80.	280.	
80.16	84.4		MDST	22.	З.				25.	
81.38	102.2	73.0	COAL	16.	3.	20.			39.	
			MDST	18.					18.	
82.75	78.7		COAL	20.	16,	10.			46.	
83.97	78.4	.0	COAL	25.	8.	60.			93.	
I			MDST			5.			5.	
85.50	81.2					165.			165.	
87.47	97.8	.0	MDST		28.	40.			68.	

START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
89.31	56,6	.0	COAL	6.	5.	100.			111.	
90.37	95.O	4.4	COAL	10.	3.	20.			33.	•
			MDST			73.			73.	
			SNDS	34.					34.	
93.57	100.0	10.8	SNDS	52.	10.	50.			112.	
96.62	95.9	11.1	CDAL	10.		200.			210.	
			MDST	40.		20.			60.	
			SNDS	30.	10.	30.			70.	
99.06	101.0	4.9	COAL	81.	1.				82.	
			MDST	5.		42.			47.	
102.11	101.3	9.9	MDST	57.	10.	30.			97.	
105.15	89.6	4.5	MDST	60.	10.	1.			71.	
108.51	101.3	.0	MDST	70.	15.	20.			105.	
111.57	99.0	.0	MDST	:		120,			120.	
114.60	99.3	. 0	MDST			55.			55.	
			SLTS			8.			8.	
117,65	86.6	6.0	-		-				148.	
121.00	101.6	3.9	SLTS			47.			47.	
124.05	94.4	4.9	SLTS			152.			152.	
127.10	96.1	13.1	SLTS			86.			86.	

				LOCAT	TION = TW83D	-343		
START OF CORE RUN		R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE TOTAL FRACTURES FRACTURES
9.45	80.9	28 4	SLTS	16.	4.			20.
11.28	92.8	5.3		44,	7.			51.
14.32	98.0		SLTS	62.	8.	2.		72.
17.37	98.0		SLTS	57.	4.	- .		61.
20.42	96.4		SLTS	60.	7.	2.		69.
23.47	101.6		SLTS	5i.	6.	2.		59.
26.52	100.0		SLTS	39.	9.	۷.		48.
29.56	83.0		SLTS	54.	4.	1.		69.
32.61	73.0		SLTS	7.	2.	33.		42.
35.Q5	100.3		SLTS			4.		76.
38.10	95.7		SLTS	63.	9.	4. 39.	00	
							20.	59.
41.15	96.7		SLTS			96.		96.
42.20	89.8		SLTS	57.	14.			73.
47.24	100.7	21.3	SLTS	43.	7.	1.		51.
50.29	83.9	15.7	SLT5	48.	1.			49.
_			SNDS			· 9.		9.
53.34	96.2		<u>SNDS</u>			89.		89.
57.00	95.7	.0				107.		<u>,</u> 107 .
60.04	89.2		SNDS	58.	5.	42.		105.
63.09	97.0		SNDS	50.	5.	1.		56.
66.14	101.6		SNDS	25.	3.			28
69.19	94.7	30.3	SLTS	23.	8.			31.
			SNDS	14.	1.			15,
72.23	91.8	9.5	COAL	5.	2.	20.		27.
			MDST			39.		39.
			SLTS	40.	2.			42.
75.28	94.4	6.1	COAL	9.	2.	15.		2ნ.
			MDST			28.		28.
77.42	101.1	34.1	COAL	13.	2.			1 5.
78.33	96.7	15.7	COAL	9.	2.			11.
			SLTS	39.	4.			43.
81.38	94.1	11.1	SLTS	36.	9.			45.
84.43	92.5		SLTS	55.	2.			57.
			5NDS	13.				13.
87.48	91.5	15 4	MDST	7.	2.			9.
07.40	01.0	٠٠	5ND5	54.	4.			58.
90.52	60.1	0	COAL	8.	٦.		75.	83.
90.32	00.1	.0	NTRK	٠				03.
			SNDS	5.	1.	25.		24
91.44	62.9	_	CB5H	5. B.	1.	25.		31.
21.44	02.9	.0	-	8.		5.0		8.
			COAL			20.		20.
00	00 F	_	MDST	29.	3.		-	32.
93.57	82.5	.0	COAL		3.		5.	B .
			MDST		3.	1		3.
95.40	90.2	29.5	CBSH	5.				5.
			COAL	8.	3.			11.

LOCAT	TON	= †	M83D	- 34	13
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START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY		JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
96.62	94.8	11 2	CBSH	4.					4.	
30.02	34.0	11.0	COAL	16.	3.				19.	
•			NTRK	10.	3.				15.	
			SLTS	25.	1.		25.		51.	
98.75	66.8	18.7		21.	3.	2.	201		26.	
100.89	133.9		SLTŠ	41.	10.	 			51.	
102.72	93.4		COAL	14.	6.	25.			45.	
103.94	90.7	39.0	COAL	14.	5.		20.		39.	
			MDST	9.					9.	
105.76	86.9	.0	COAL	2.	2.		15.		19.	
			MDST	53.					53.	
107.29	65.8	.0	COAL	9.	4.				13.	
			MDST	8.					8.	
108.81	93,1	20.0	SLTS	11.	2.				†3.	
			SNDS	24.	4.	3.			31.	
111.56	102.3		SNDS	46.	6.	•			52.	
114,60	100.3	38.7	SNDS	51.	10.				61.	
117.65	100.3	10.8	SLTS	48.	10.				58.	
			SND5	6 .					6.	
120.70	101.3		SLTS	49.	8.				57.	
123.75	85.8	4.7	COAL	10.	1.				11.	
			MDST			70.			70.	
100 10	05.4		SLTS			•				
126.49	95.1	22.6	COAL	8.	9.	1.			18.	
129.54	104.0		MDST			54			54.	
132.59	101.0 90.1	.0		4.	1.	67.			67.	
132.39	90.1	.0	COAL	4.	1.	,			5.	
134,11	75.1	0	MDST MDST			40. 53.			40. 53.	
136.24	108.2		COAL			15.		·	15.	
130.24	108.2	.0	MDST			49.			49.	•
138.07	76.2	0	MDST			36.			49. 36.	
139.29	92.8		COAL	17.	1,	10.			28.	
135.25			MDST	21.		12.			33.	
142.34	89.5	13 B	CDAL	10.	2.	10.			22.	
142.04	03.0	,5.6	MDST	11,	4	48.			59.	
			SLTS	25		40.			25.	
145.39	95.7	15.7		87.	· · · · · · · · · · · · · · · · · ·	i			96.	
148.44	99.3	24.7		48.	3.	',			51.	
151.48	98.0		SLTS	39.	3.	•			42.	
154.53	100.3		SLTS	15.	٥.	28.			43.	
157.58	99.3	10.2	รี่เริ่	141		51.			51.	
160.63	95.7	4.3	SLTS			62.			62.	
163.68	88.2	20.7				51.			51.	
166.72	100.7	48.5				36.			36.	
169.77	100.0	50 7	ŠNDŠ	···		25.			25.	

				LOCAT	ION = TW83E	-344				
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	<u>-</u>
10.36	87.0	.0	SLTS	12.		50.			62.	
11.28	87.6	·	SLTS	47.	9.	3.	·········	· · · · · · · · · · · · · · · · · · ·	59.	
14.02	79.2		SLTS	27.	15.	٥.			42.	
15.85	87.8		ŠLTŠ		,,,	44.			44.	
19,20	100.3	11.1				61.			61.	
22.25	83.6	-0	SLTS			60.			60.	
25,00	98.4		SLTS	36.	12.	14.			62.	
28.04	83.6		SLTS	31.	9.				40.	
30.18	88.1		SLTS	36.	6.	3.			45.	
32.61	63.3	9.8		33.	5.				38.	
35.66	28.2		SLTS	16.	3.				19.	
38.71	195.4		SLTS	86.	9.				95.	
40.23	91.5		SLTS	36.	5.				41.	
41.76	242.9	16.5	SLIS	38.	10.				48.	
42.67	95.3		SLTS	31.	11.				42.	
44.81	90.1		SLTS	75.	5.				80.	
47.85	97.7		SLTS	63.	2.	3.			68.	
50.90	98.0	. ŏ		73.	5.	4.			82.	
53.95	98.7	5.2		10.	5.	92.			92.	
57.00	99.0	28.9	SNDS	44.	6.	J2.			50.	
60.04	95.9		CDAL	7.	٥.	15.			22.	
30.01			SLTS	63.	8.	51.		· · · · · · · · · · · · · · · · · · ·	122.	
62.48	90.6	0	CDAL	1.	2.	10.			13.	
32.10	55.5		SLTS	31.	11.	100.			142.	
64.92	86.3	0	CDAL	٥,,	,,,	50.			50.	
	30.0		SLTS	37.	4.				41.	
66.75	67.2	. 0	SLTS	28.	2.	1.			31.	
	*		SNDS	3.		• •			3.	
69.19	91.8	19.7		28.	7.	11.			46.	
72.24	88.2	3.9	SNDS	56.	5.	5.			66.	
75.29	96.1		COAL	1.	~.	2.			3.	
		, 5	SLTS	16.	3.	50.			69.	
			SNDS	32.	9.	00.			41.	
78.33	97.7	. 0	SLTS	71.	21.				92.	
81.38	98.9		SLTS	40.	4.				44.	
		_	SNDS	35.	3.				38.	
84.12	73.2	. 0	COAL	7.	٥.	26.			33.	
			MDST	23.		4.			27.	
85.95 87.48 90.53 93.57	73.2	15.7	-	10.	4.				14.	
87.48	91.1	.0		66.	7.	45.			118.	
90.53	80.3	.0						500.	500.	
93.57	95.6		COAL					250.	250.	
	~~,0		\$LT\$	23.	3.	3.		250.	250. 29.	
95.40	34.9	.0	COAL		۷,	50.		100.	150.	
	~	••	GOUG			50.		500.	500.	
98.15	71.7	. 0	COAL	ĕ.	Ž.	2.			12.	
				٠,	~ .	2.			14.	

LOCATION = TW83D-344

TART OF ORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY		JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
98.75	82.0	.0	COAL		1.	3.			4.	
			GOUG					100.	100.	
			SLTS	13.	2.				15.	
100.58	100.9	.0	SLTS							
			SNDS	22.	8.				30.	
102.72	98.0	.0	SNDS	33.	5.	4.			42.	
105.77	98.0	٠.0	\$NDS	45.	8.		•		53.	
108.81	98.7	.0	GDUG					20.	20.	
			SNDS	34.	4.	1.			39.	
111.86	164.5	.0	COAL	2.					2.	
			GOUG					100.	100.	
112.17	86.0	22.3	COAL	5.	8.				13.	
			MDST			100.			100.	
113.38	82.4	.0	COAL	2.	1.				3.	
			SLTS	43.	4.				47 -	
114.91	96.1	.0	CBSH	5.		•			5.	
			COAL	3.	2.				5.	
			MOST			42.			42.	
			SLTS	46.	5.				51.	
117.96	51.3	٠.٥	COAL	1.	12.	15.			28.	
			MDST	5.		25.	25.		55.	
119.48	85.4	.0	CBSH	8.			• • • • • • • • • • • • • • • • • • • •	•	8.	
			COAL	7.	1.	1.			9.	
			MDST			79.			79.	
122.83	79.5	.0	COAL	10.	1.,	. 1.			12.	
			MDST	-		22.			22.	
124.05	97.4	.0	SLTS	81.	10.				91.	
127.10	98.0		SLTS	80.	3.	3.			86.	
130.15	101.6		MDST	74.	9.				83.	
133.20	95.7		- MDST			48.			48.	
136.25	96.7		GOUG			• • •		500.	500.	
			MDST			7.			7.	
139.29	99.7	Ó,	SLTS			77.	v		77.	
142.34	101.6		SLTS			70.			70.	
145.39	97.7		SLTS			62.	•		62.	

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START OF CORE RUN	RECOVERY * PERCENT	R.Q.D.	LITHOLOGY		JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINDR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
26.52	78.9	٥.	SLTS							
28.04	19.7	. 0	SLTS							
28.65	48.9	.0	COAL							
			SLTS	11.					11,	
29.57	57.6		SLTS			1 <u>5</u> .			15.	
32.00	90.2	18.9	SLTS	14.		3.			17.	
			SNDS	9.					9.	
34.44	75.4		SLTS	3.					3.	
37.49	100.0		SLTS	9.	3.	1.			13.	
38.71	29.5	.0	COAL	_		10.			10.	
		_	SLTS	3.					з.	
39.32	82.0	.0	COAL		_	_				
			SLTS	26.	3.	3.			32.	
41.76	85.8	39.3	COAL	9.					9.	
		_	SLTS	11.					11.	
43.59	47.5	.0	COAL	2.		50.			52.	
		🛫	MDST			4.			4.	
44.81	77.3	.0	CDAL	3.		10.			13.	
4			SLTS	6.		_			6.	
47.85	80.7	26.6	COAL		_	2.			2.	
	72.1		SLTS	12,	8.				20.	
50.90	72.1	19.7	CBSH	4.					4.	
			COAL			30.			30.	
50.40	24.2		SLTS			4.			4.	
52.12	91.3		COAL			25.			25.	
			SLTS	10.		11.			21.	
53.95	92.8		SLTS	7.		3.			10.	
55.47	82.6		SLTS	24.	4.				28.	
58.52	44,9	. 0	COAL			50. 7.			5 <u>0</u> .	
. 50 50	54.0		SLTS			/-			7.	
59.59	64.8	.0	COAL	6.		15.			21.	
60.50	103.3	25.0	MDST COAL	13.		11.	00		11.	
61.42	92.7								50.	
01.42	92.7	.0		7.	2.	51.			60.	
60 70	07.4	٠.	SLTS	7.	2.	1.			10.	
62.79	97.4	9.8	SLTS	36.	5.				43.	
65.84	90.5 94.3		MDST			13.			13.	
68.27			MDST	00		19.			19.	
70.71	101.3		SLTS	29.	2.	1.			32.	
72.24	98.0		SLTS	28.	4.	1.			33.	
75.29	95.6	.0	COAL	14.		3.			14.	
76.20	400.0	^	SLTS						4.	
76.20	109.9	.0	CDAL	6.		35 .	0.5		41.	
77 11	66.6	_	SLTS	16.	4.		25,		45.	
77.1 <u>1</u>	66.6	.0	COAL	11.	· · · · · · · · · · · · · · · · · · ·	25.			36.	
			MDST	8.	1.	13.			22.	

START OF RECOVERY R.Q.D. LITHOLOGY BEDDING JOINT UNCLASSIFIED MINOR FAULT FAULT ZONE TOT FRACTURES FRACTURES	CTURES 10. 10. 20. 23. 1. 4. 20. 29. 3. 1. 120. 176. 4. 12. 7.
81.38 83.6 4.6 CBSH 10. 10. 10. MDST 4. 1. 18. 84.43 100.4 42.0 MDST 1. 0THR 4. 13. 87.17 84.3 18.4 MDST 29. SLTS 2. 1. SNDS 1. 90.22 112.7 22.1 MDST 120. 92.66 92.5 34.1 MDST 120. 95.86 76.8 .0 CBSH 4.	10. 20. 23. 1. 4. 20. 29. 3. 1. 120. 176. 4. 12. 7.
81.38 83.6 4.6 CBSH 10. 10. 10. 10. MDST 4. 1. 18. 84.43 100.4 42.0 MDST 1. 0THR 4. 13. 87.17 84.3 18.4 MDST 29. SLTS 2. 1. SNDS 1. 90.22 112.7 22.1 MDST 120. 92.66 92.5 34.1 MDST 120. 95.86 76.8 .0 CBSH 4.	10. 20. 23. 1. 4. 20. 29. 3. 1. 120. 176. 4. 12. 7.
MDST 4. 1. 18. 84.43 100.4 42.0 MDST 1. OTHR 4. 5NDS 3. 4. 13. 87.17 84.3 18.4 MDST 29. SLTS 2. 1. 90.22 112.7 22.1 MDST 120. 92.66 92.5 34.1 MDST 176. 95.86 76.8 .0 CBSH 4.	20. 23. 1. 4. 20. 29. 3. 1. 120. 176. 4. 12. 7.
MDST 4. 1. 18. 84.43 100.4 42.0 MDST 1. OTHR 4. 5NDS 3. 4. 13. 87.17 84.3 18.4 MDST 29. SLTS 2. 1. 90.22 112.7 22.1 MDST 120. 92.66 92.5 34.1 MDST 176. 95.86 76.8 .0 CBSH 4.	23. 1. 4. 20. 29. 3. 1. 120. 176. 4. 12. 7.
84.43 100.4 42.0 MDST	4. 20. 29. 3. 1. 120. 176. 4. 12.
OTHR 5NDS 3. 4. 13. 87.17 84.3 18.4 MDST 29. SLTS 2. 1. 90.22 112.7 22.1 MDST 120. 92.66 92.5 34.1 MDST 176. 95.86 76.8 .0 CBSH 4.	20. 29. 3. 1. 120. 176. 4. 12. 7.
87.17 84.3 18.4 MDST 29. SLTS 2. 1. SNDS 1. 90.22 112.7 22.1 MDST 120. 92.66 92.5 34.1 MDST 176. 95.86 76.8 .0 CBSH 4.	29. 3. 1. 120. 176. 4. 12. 7.
SLTS 2. 1. SNDS 1. 90.22 112.7 22.1 MDST 120. 92.66 92.5 34.1 MDST 176. 95.86 76.8 .0 CBSH 4.	29. 3. 1. 120. 176. 4. 12. 7.
SNDS 1. 90.22 112.7 22.1 MDST 120. 92.66 92.5 34.1 MDST 176. 95.86 76.8 .0 CBSH 4.	3. 1. 120. 176. 4. 12. 7.
90.22 112.7 22.1 MDST 120. 92.66 92.5 34.1 MDST 176. 95.86 76.8 .0 CBSH 4.	1. 120. 176. <u>4.</u> 12. 7.
92.66 92.5 34.1 MDST 176. 95.86 76.8 .0 CBSH 4.	176.
95.86 76.8 .0 CBSH 4.	12. 7.
	12. 7.
COAL 4. 3. 5.	7.
MDST 7.	
97.54 115.5 28.6 CBSH 2.	2.
MDST 6. 25,	31,
99.67 72.4 24.3 COAL 3. 2. 10.	15.
MDST 9. 1.	10.
101.19 81.9 .O COAL 17. 2. 1,	20.
102.57 90.0 32.5 CDAL 5,	5.
MDST 25. 25.	50.
105.46 90.6 .O CBSH 6. 1.	7.
MDST 21.	21.
107.59 41.6 .0 COAL 50.	50.
MDST	
108.36 94.4 62.3 CB\$H 1,	1.
COAL 8. 1.	9.
SLTS 26.	26.
111.57 86.1 47.0 CB5H 5. 10.	15.
SLTS 15.	15.
113.08 84.7 46.4 CBSH 15. 15.	30.
SLTS 7.	7.
114.91 91.5 29.8 CBSH 7.	7.
MDST 37.	3 <u>7</u> .
OTHR 5.	5 .
MDST 37. OTHR 5. SLTS 1.	1
	_1.
117.96 89.8 33.6 OTHR 28. 120.40 97.7 44.4 SLTS 6. 15. SNDS 6. 1. 4. 123.44 93.2 12.5 CBSH 37. MDST 36. 50. SLTS 2. 4. 126.80 88.5 26.6 MDST 88.	28.
120.40 97.7 44.4 SLTS 6. 15.	21.
SNDS 6. 1. 4. 123.44 93.2 12.5 CBSH 37.	11.
123.44 93.2 12.5 CBSH 37. MDST 36. 50.	37.
MDST 36. 50. SLTS 2. 4.	86.
SLTS 2. 4. 126,80 88.5 26.6 MDST 88.	6.
126.80 88.5 26.6 MDST 88. 129.84 91.1 47.3 MDST 12.	88.
12.04 01.1 47.0 MOST 12.	12.

				LOCAT	ION = TW83D	-345				
START OF CORE RUN	RECOVERY PERCENT		LITHOLOGY	FRACTURES		UNCLASSIFIED FRACTURES	FRACTURES	FRACTURES	FRACTURES	
129.84	91.1	47.3	OTHR			13,			13.	
133.20	102.0	70.2	TUFF TUFF			5. 20.			5. 20.	
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			·····				<u></u>			
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START DF	RECOVERY	R.O.D.	LITHOLOGY			UNCLASSIFIED		FAULT ZONE	TOTAL	
CORE RUN	PERCENT			FRACTURES	FRACTURES	FRACTURES	FRACTURES	FRACTURES	FRACTURES	
21.34	100.0	29.7	SLTS	3.		6.	,		9.	
23.16	89.1	7.1	SLTS	18.	1.	11.			30.	
25.00	101.7	.0	SLTS	6.	3.	7.			16.	
25.60	74.3	6.5	COAL	19.	4.	3.			26.	
			DTHR							
27.74	95.6	25.3		14.					14.	
28.65	72.1	.0		7.	4.			50.	61.	
29.87	74.7		COAL	13.		•			13.	
30.78	59.0	.0	COAL	<u></u>		10.		50.	67.	
			MDST	48.					48.	
32.00	97.8	13.0		12.	1.				13.	
			MDST			6.			6.	
32.92	84.9		MDST	13.		5 9.			72.	
34.44	59.Q	22.1	COAL	5.					5.	
			MDST	5.	2.				7.	
35.66	95.4	.0	MDST	21.	2.	1.	20.		44.	
37.18	82.4	37.3	MDST	10.			-		10.	
38.71	103.3	21.3	MDST	13.					iš.	
39,32	83.1	34.4	MDST	11.	2.				13.	
41.15	85.2	32.8	COAL		1.				1.	
			MDST	10.					10.	
42.37	54.6	.0		12	3.	51,			66.	
44.20	78.9	.o.		3.	3.	20.			26.	
		· -	MDST	8.	٠.	20.			8.	
			SLTS	10.	1.	5.			16.	
47.24	91.1	40.0		19.	2.				28.	
50.29	100.3		CDAL	5.	ā.	30.			38.	
			MDST	17.	٧.	11.			28.	
			SLTS	, , ,		8.			28. 8.	
53.34	92.1	4.3	SLTS			44.			44.	
56.39	101.0	17.0	SLTS			42.				
59.44	99.0	17.0	SLTS			42. 63.			42.	
62.48	92.9	17.6	MDST	23.	20.	4.			63.	
65.84	99.0	10.5	MOST	23.	20.	44.			47-	
68.84	98.7	21.7				44. 19.			44.	
90.04	50.7	21.7	SLTS						19.	
71.92	93.5	20 6	SLTS			20.			20.	
75.28	90.5	40.3				39.			39.	
78.33	102.0	-	SLTS		•	30.			30.	
81.38	104.6					29. 50			29.	
81.38	99.7		SLTS			53.			53.	
			SLTS			35.			35.	
87.48	92.8		SLTS			50.			50.	
90.52	104.4	49.5	SLTS			30.			30.	
00.00			SNDS			11.			11.	
93.27	91.8		SNDS			43.			43.	
96.32	97.0	34.2	SND5			35.			35.	

				LOCAT	ION = TW830)-347				
START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	FRACTURES	FRACTURES		···
99.36	84.9	12.5	SLTS			45. 48.			45.	
102.41	97.4	15.7	SLTS			48.			48.	
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START OF CORE RUN	RÉCOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
7.62	65.6	.0	SLTS			23.			23.	
9.45	30.6	.0	SLTS			20.			20.	
11.28	32.1	. 0	SNDS	23.		•			23.	
14.33	89.5	.0	SNDS	53.	4.	4.			61.	
17.37	53.6	. 0	CDAL			20.			20.	
			MDST	29.	2.				31.	
			SNDS	5.	2.				7.	
19.20	78.2	.0	CDAL	8.		73.			81.	
			SNDS	40.	6.	Э.			49.	
21.95	100.0	٠.٥	SNDS	35.	4.				39.	
23.47	35.0	.0	CDAL			100.			100.	
			MDST			- 7.			7.	
25.30	35.2	.0	MDST			11.			11.	
26.52	45.9	.0	COAL					500.	500.	
			MDST			5.			5.	
27.74	72.6	.0	COAL	4,		2.		50.	5 6 .	
			MDST	22.		35.			57.	
			SLTS	97.	11.				108.	
32.16	83.6	.0	SLTS	85.	2.	1.			88.	
35.51	119.3	.0	SLTS	75.	12.				87.	
38.10	100.3	4.9	MDST		•	47.			47.	
			SLTS	31.	4.				35.	
41,45	70.5	28.9	MDST			32.			32.	
44.81	17.8		SLTS			26.			26.	
47.85	244.3	95.9	SLTS			49.			49.	
49.07	163.9	114.8	SLT5			22.			22.	

LOCATION = TW83D-353

START OF	RECOVERY	R.Q.D.	LITHOLOGY	BEDDING	JOINT	UNCLASSIFIED	MINOR FAULT	FALL T ZONE	TOTAL	
CORE RUN	PERCENT			FRACTURES		FRACTURES	FRACTURES	FRACTURES	FRACTURES	
6.70	71.9	.0	SLTS	5.	2.				7.	
8.23	60.7	.0	SLTS	6.	3.	1.			10.	
			SNDS	29.	1.				30.	
11.28	99.3	23.7	SNDS	42.	2.				44.	
14.32	94.7	6.1	SLTS	16.	2.				18,	
			SNDS	29.	2.	1.			32.	
16.76	4.3	.0	COAL			10.			10.	
17.22	93,4	.0	COAL			50.			50.	
			SLTS	7.					7.	
			SNDS	40.	5.		·		45.	
19.96	89.4	25.9		46.	t.	3.			50.	
23.16	100.0	38.7		33,	2.				35.	
26.21	101.0	19_3	SLTS	43.					43.	
			SNDS	7.	-			····	7,	
29.2 6	92.2	.0	SLTS	78.	4.				82.	
32.46	96.5	-0	MDST	62.		18.			80,	•
35.05	77.0	51.9	COAL	18.	4.				22.	
36.88	93.5	. 0	COAL	11.	2,			···	13.	
			MDST			4.			4.	
			SLTS	11.					11.	
38.56	93.1	3.7	SLTS	53.					53.	
41.76	100.0	.0	SNDS	69.	2.	2.			73.	
44.80	98.4	10.5	SNDS	45.	2.	1.			48.	
47.85	101.3	23.9	SNDS	54.		. 3,			57.	
50.90	69.3	.0	SNDS	37.		•			37.	
53.64	96.1	.0	CBSH	15.	1.				16.	
			MDST	19.	1.				20.	
			SLTS	22.		1.			23.	
56.39	105.6	7.5	MDST	61.					61,	
59.44	93.3	38.3	COAL	5.	6.	1.			12.	
60.04	93.4	4.9	COAL		3.				3.	
			MDST	84.					84.	
63.09	90.8	23.9		10.	1.	10. 26.			21.	
			MDST	27.		26.		-	53.	
			SLTS	2.					2.	
			SNDS	6.					6.	
66.14	89.4	4.4	CBSH	6.	4.				10.	
			COAL	9.	<u> </u>	10.			21.	
			MDST			61.			61.	
68.88	99.0	٠.				83.			83.	
71.93	134.8	53.3	COAL	10.	3.				13.	
			MDST			15.			15.	· · · · · · · · · · · · · · · · · · ·
72.85	96.7	11.1	MDST	37.		12.			49.	
75.28	100.7	24.6	COAL	3.			•		3.	
			MDST	60.	2.				62.	
78.33	95.7	16.4	COAL	29.	5.	1.			35.	

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LOCATION = TW83D-353

START OF CORE RUN	RECOVERY PERCENT	R.Q.D.	LITHOLOGY	BEDDING FRACTURES	JOINT FRACTURES	UNCLASSIFIED FRACTURES	MINOR FAULT FRACTURES	FAULT ZONE FRACTURES	TOTAL FRACTURES	
78.33	95.7	16.4	MDST	22.	1.				23.	
81.38	93.4	19.3	CBSH	3.					3.	
			COAL	22.	9.				31.	
			MDST			30.			30.	
84.43	82.3	12.1	COAL	3,					3.	
			MDST	25.		5.			30.	
			SLTS	17.	1.				18.	
87.48	100.3	45.4		42.	5.	3.			50.	
90.52	103.0	15.1		16.					16,	
			SNDS	48.	1.				49.	
93.57	102.0	18.4	SLTS	33.	7.	4.			44.	
			SNDS	24.		•			24.	
96.62	100.0		SLTS	78.	6.				84.	
99.67	87.6	4.0	CDAL	6.	1.	500.			507.	
			MDST	3.	1.				4.	
			SLTS		6.				6.	
			SNDS	19.	1 .				20.	
102.41	81.Q	۰.	COAL	8.	3.	1.			12.	
			SLTS	21.	1.	1.			23.	
103.78	78.3	5.6	COAL	1.			1.		2.	
			MDST			66.		50.	116.	
105.76	30.4	.0	COAL							
			SLTS							
106.68	40.9		COAL	24.	1.				25 <i>.</i>	
111.86	100.0	47.5	COAL	9.					9	
112.47	82.0	٥.	COAL	16.					16.	
			MDST	_		51.			51.	
114.30	101.0		SLTS	56.	3.	1.			60.	
117.35	103.0	14.1		53	5.	3.			61.	
120.40	102.0	50.3	MDST	39.	1.	•	- 2-111-11-12-1		40.	
123.44	95.1	11.1	MDST	28.	2.	30.			60.	
126.49	102.3	44.6	MDST			51.			51.	
129.54	92.2		SLTS			73.			73.	
132.89	103.3	11.5	SLTS			43.			43.	
135.94	100.3	51.1				43.			43.	
138.99	89.0	23.3	SLTS			65.			65,	

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CONFIDENTIAL COAL ANALYSES

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	TW81R-	107													
	SEAM	TOP	BOT	SAMPLE	ATYP	5G 	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
_	Na .	20.62	28.23	11-17	RAW	.00	.00	12.18	1.22	.00	.00	.00	.00	.00	
1	6	20.62 131.16	28.23 133.17	11-17 18+19	WASH Raw	1.60 -00	81.00 .00	6.80 16.48	1.87	26.36 .00	64.97	7307.00	. 52	.00	
	-1	131,16	133.17	18+19	WASH	1.60	68.00	7.03	1.52	26.03	.00 65.42	.00 7599.00	1.39	2.50	
~	1	134.35 134.35	139.00 139.00		RAW Wash	.00 1,60	.00 48.00	30.78 11.96	. 66 1 . 05	.00 25.99	.00	.00 7586.00	.00 .97	.00 3.00	
-	0	160.90	161.30	23+24	RAW	.00	. 00	32.99	. 90	.00	.00	.00	.00	.00	
	0	160.90	161.30	23+24	WASH	1.60	53.00	11.91	. 70	29.21	58.18	7308.00	1.07	3.50	
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	TW81R-	112													
Ĺ	SEAM	TOP	BOT	SAMPLE	ATYP	\$G	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	F\$I	
J	70	98.00	98.60	1+2	RAW	.00	.00	21.37	1.09	.00	.00	, 00	.00	.00	
	40	98.00	98.60	1+2	WASH	1.60	77.00	12.14	.90	30.50	56.46	7037.00	1.78	1.50	
	<u> </u>	104.60	105.40	3+4	RAW	.00	.00	16.62	. 98	.00	.00	.00	.00	.00	Ì
-1	9	104.60	105.40	3+4	WASH	1.60	80.00	9.05	.77	33.61	56.57	7418.00	2.44	1.50	
~[8 8	107.10	109.00	5+6	RAW	.00	.00	14.58	1.07	.00	.00	.00	.00	.00	j
_]	8	107 - 10	109.00	5+6	WASH	1.60	82.00	8.29	.98	30.28	60.45	7430.00	1.35	1.00	1
	×7	127.70	128.70	7+8	RAW	.00	.00	15.07	.99	. 00	.00	.00	.00	.00	ţ
	• 7	127.70	128.70	7+8	WASH	1.60	88.00	8.02	1.04	30.63	60.31	7498.00	1.36	3.00	
1	6	134.30	136.90	9+10	RAW	.00	.00	11.10	1.04	. 00	.00	.00	.00	.00	
_	6	134.30	136.90	9+10	WASH	1.60	79.00	6.19	2.09	28.57	63.15	7544.00	. 75	1.00	ļ
	-5	145.10	147.60	11+12	RAW	-00	.00	15.84	1.15	.00	.00	.00	.00	.00	İ
	- 5	145.10	147.60	11+12	WASH	1.60	88.00	6.09	1.57	29.24	63.10	7611.00	. 56	1.50	
-		151.75	153.20	13+14	RAW	.00	.00	8.35	1.12	.00	.00	.00	. 00	.00	İ
		151.75	153.20	13+14	WASH	1.60	91.00	5.33	1.72	29.11	63.84	7663.00	. 98	1.50	
	3	160.10	161.60	15+16	RAW	.00	.00	25.85	. 90	.00	.00	.00	.00	.00	
_	3	160,10	161.60	15+16	WASH	1.60	65.00	5.24	1.45	29.67	63.64	7908.00	. 70	1.50	
_]	.2	168.40	170.10	17+18	RAW	. 00	.00	14.65	. 98	.00	.00	.00	.00	.00	
7	2	168.40	170.10	17+18	WASH	1.60	85.00	5.62	1.40	29.95	63.03	7673.00	. 53	1.00	
7	5	192.50	194.80	19+20	RAW	. 00	. 00	42.54	.80	.00	.00		.00	.00	
	- 5	192.50	194.BQ	19+20	WASH	1.60	47.00	9.73	1.19	27.94	61.14	7416.00	1.16	1.00	
+	- 4	202.20	203.40	21+22	RAW	.00	. 00	14.25	,82	.00	.00	.00	.00	.00	
-	. 4	202.20	203.40	21+22	WASH	1.60	83.00	10.31	.1.21	27.58	60.90	7318.00	1.07	1.00	1
J	-3	209.10	209.80	23+24	RAW	. 00	.00	31.97	. 73	.00	.00		.00	.00	
1	3	209.10	209.80	23+24	WASH	1.60	63.00	16.49	.86	28.63	54.02	6911.00	1.67	1.00	
~	, 3	210.40	212.25	25+26	RAW	.00	.00	21.92	. 74	. 00	.00	.00	. 00	. 00	ĺ
_	- 3	210.40	212.25	25+26	WASH	1.60	77.00	9.29	1.01	29.25	60.45	7513.00	.83	3.00	
	<u>~2</u>	217.65	218.55	27+28	RAW	.00	.00	13,47	.92	. 00	.00	.00	.00	. 00	
٦	2	217.65	218.55	27+28	WASH	1.60	80.00	6.19	1.17	28.87	63.77	7786.00	.64	1.50	
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	TW82D-2 SEAM	TOP		SAMPLE		SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
7	`1 O	129.40 129.40 141.70	134.56 134.56 142.60 142.60	57 57 58	RAW WASH RAW WASH	.00 1,60 .00	.00	20.60 16.36 38.27 18.62	.72 1.01 .67	24.46 24.70 23.31 25.17	57.93 37.75	6464.00 6918.00 4706.00	.00	-1.00 3.00 -1.00	
		141.70	142.00		WASH	1.60	48.00	18.62	1.01	25.17	55.20	6586.00	. 00	1.50	
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PAGE 8 TW82D-204 SEAM TOP BOT SAMPLE ATYP SG YIELD ASH RESMOIST VOL CARB KCAL SULF FSI 193.24 194.70 22 RAW .00 .00 22.05 .73 27.79 49.43 6250.00 .00 -1.00 193.24 194.70 22 WASH 1.60 71.00 7.66 1.10 31.86 59.38 7427.00 .00 5.50 210.60 213.05 23 RAW .00 .00 9.52 . 78 28.12 61.58 7339,00 .00 -1.00 210.60 213.05 23 WASH 1.60 89.00 5.27 1.18 28.89 64.66 7690.00 .00 2.00 319.10 321.20 24 RAW .00 28.93 .00 16.34 .91 53.82 6609.00 .00 -1.00 319.10 321.20 24 WASH 1.60 78.00 8.97 -.98 29.21 60.84 7433.00 .00 3.00

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	PAGE	9														
1	TUDO	D-208🏞														
- 1	SEAM		вот	SAMPLE	ATYP	60	VIELD	A = 1.1	DEGUOTOT	Va.	0					
				JAMPLE	A11P	SG	YIELD	A5H	RESMOIST	VOL	CARB	KCAL	SULF	FSI		
\equiv	6	6.34	9.58	356	RAW	.00	.00	44.72	. 90	20.49	33.89	4116.00	.84	-1.00		
~	6	6.34	9.58	356	WASH	.00	.00	7.46	1.14	29.05		7476.00	. 65	2.50		
	6	10.68	11.28	355	RAW	.00	.00	19.41	. 99	29.74		6393.00	2.97	-1.00		
_	6	10.68	11.28	355	WASH	.00	.00	10.52	. 96	_30.56		7306.00	2.04	2.50		
	3	25.68	26.10		RAW	.00	.00	11.23	. 87	30.15		17244.00	2,13	-1.00		
-	3	25.68	26.10	354	WASH	.00	.00	8.68	. 82	30.03		7505.00	1.74	5.00		
	3	26.50 26.50	27.08	353	RAW	.00_	.00	15.06	. 92	25.43		\6883.00	2.67	-1.00		
	2	26.50 31.56	27.08 31.90	353 351	WASH RAW	.00	.00	10.40	1.04	26.29			1.69	1.00		
	2	31.56	31.90		WASH	. 00 . 00	.00	28.34 13.40	1.40 1.13	23.57		4793.00	2.62	-1.00		
	2	32.84	33.50		RAW	.00	.00	28.04	1.13	30.46 27.79	55.01	7109.00 .5462.00	1,59	3.50		
L	2	32.84	33.50		WASH	.00	.00	10.63	1.90	29.03		7182.00	.81	1-00 1.50		
		-> 132.01	137.12		RAW	.00	.00	17.93	.55	26.96		• 6644.00	.00	-1.00 🧲		
	1	132.01	137.12	05	WASH	1.60	75.00	9.75	.97,	24.70		7443.00	.00	4.00		
ļ	1	~ 217.30	223.50		RAW	.00	.00	14.78	.79	26.02	58.41		.00	-1-00		
- 1	1	217.30	223.50		WASH	1.60	79.00	8.59	.87	26.85	63.69	7556.00	.00	4.50		
	1	224.44	224.82		RAW	.00	.00	25.90	. 78	24.66		5813.00	.00	- 1 ₋ QO		
	1	224.44 225.71	224.82	14	WASH	1.60	65.00	12.34	. 98	26.40	60.28		. 00	4.50		
	1	225.71	227.08 227.08		WASH	.00	-00 73,00	17.56	. 87	26.00	55.57		.00	-1.00		
	1	233.41	234.41	13	RAW	1.60 .00	.00	10.17 35.18	. 90 . 69	27.23 22.11	61.70	7398.00	.00	5.50		
	ì	233.41	234.41		WASH	1.60	78.00	18.57	. 86	24.86	41.81 55.71		.00	-1.00		
ı			20		WA 211	1.00	75.00	10.51	. 60	24.00	55.71	6613.00	.00	3.50		
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SEAM	TOP	BOT	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
				~										-
1	18.08	21.95	42-45	RAW	.00	.00	41.13	. 55	18.36	39.96	4640.00	.00	-1.00	
1	¯18.Q8	21.95	45	WASH	1.60	33.00	12.09	.71	22.61	64.59	7471.00	.00	6.00	
<u>† </u>	31.00	32.00		RAW	.00	.00	42.85	. 56	18.73	37.86	4316.00	.00	-1.00	
1	₹31.00	32.00	46	WASH	1.60	27.00	14.60	1.01	21.87	62.52	7135.00	.00	5.00	
1	243.00	45.00	47	RAW	.00	.00	52.96	85	17.49	28.70	3312.00	.00	-1.00	
1	_43.00	45.00	47	WASH	- 1,60	15.00	14,25	. 99	23.25	61.51	7169.00	.00	7.50	
1	48.76	50.00	48	RAW	.00	.00	61.91	.82	14.90	22.37	2354.00	.00	-1.00	
1	≺48.76	50.00	48	WASH	1.60	11.00	16.82	1.01	22.42	59.75	6935.00	.00	7.50	

Printed on the Xerox 9700 E.P.S

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TW82D-:	214												
SEAM	TOP	BOT	SAMPLE	ATYP	ŞG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI
					- -		~						
	178.57	179.40	51	RAW	.00	. 00	12.02	. 80	30.52	56.66	7354.00	.00	-1.00
t	178.57	179.40	51	WASH	1.60	87.00	7.48	.99	31.35	60.18	7770.00	.00	4.00
	188.28	190.76	52	RAW	.00	.00	35.09	. 67	21.20	43.04	5122.00	.00	-1.00
	188.28	190.76	52	WASH	1.60	57.QQ	9.79	.66	26.58	62.97	7493.00	.00	3.00
i	224,50	228.40	53	RAW	.00	.00	18.94	.51	26.26	54.29	> 6695.00	.00	-1.00
	224.50	228.40	53	WASH	1.60	74.00	6.22	. 67	30.06	63.05	7900.00	.00	5.50
	236.52	241.25	54	RAW	.00	.00	17.95	.63	27.05	54.37	6614.00	.00	-1.00
	236.52	241.25	54	WASH	1.60	68.00	9.83	. 56	27.72	61.89	7507.00	.00	4.50
	244.88	245.68	55	RAW	- 00	.00	17.08	.59	27.02	55.31	36686.00 36686.00 36686.00 36686.00	.00	-1.00
	244.88	245.68	55	WASH	1.60	80.00	9.09	. 55	29.01	61.35	7479.00	.00	4.50
!	246.74	249.18	56	RAW	- 00	.00	33.87	.72	22.80	42.61	` 5061.00	.00	-1.00
,	246.74	249,18	56	WASH	1.60	56.00	10.75	1.06	24.85	63.34	7352.00	.00	1.50

Printed on the Xerox 9700 E.P.S

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SEAM	TOP	BOT	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	123	
7	19.91	21.05	08	RAW	.00	.00	10.61	1.04	27.92	60.43 73	159.00	.00	-1.00	
7	19.91	21.05	08	WASH	1.60	90.00	6.50	1.05	29.03	63.42 77	15.00	.00	2.00	
6	21.64	25.55	09	RAW	.00	.00	18.36	1.05	27.10	53.49 > 65	00.80	.00	-1.00	
6	21.64	25.55	09	WASH	1.60	72.00	6.86	1.21	28.30	63.63 76	53.00	.00	2.50	
5	27.66	29.50	10	RAW	-00	.00	12.12	. 98	28.67	58.23 71	60.00	.00	-1.00	
5	27.66	29.50	10	WASH	1.60	86.00	6.66	1.05	29.01	63.28 76	81.00	.00	3.50	
4	36.12	37.18	11	RAW	.00	- 00	10.09	.91	26.88	62.12 73	58.00	.00	-1.00	
4	36.12	37.18	11	WASH	1.60	91.00	8.25	1.11	26.49	64.15 75	26.00	.00	1.50	
2	48.17	52.13	12	RAW	. 00	.00	24.94	.86	24.43	49.77 > 60	00.88	.00	-1.00	
2	48.17	52.13	12	WASH	1.60	66.00	10.01	1.38	27.38	61.23 74	119.00	.00	3.00	

Printed on the Xerox 9700 E.P.

	!18 TOP	BOT	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB KCAL		FSI
	35.15	35.72	15	RAW	.00	.00	20.60	. 87	23.89	54.64 6407.00	.00	-1.00
	35.15	35.72	15	WASH	1.60	71.00	13.95	1.01	25.71	59.33 7018.00		1.00
	46.95	48.37	16	RAW	.00	. 00	9.03	.91	25.77	64.29 >7430.00		-1.00
	46.95	48.37		WASH	1.60	90.00	5.91	.96	27.69	65.44 7702.00		2.00
	49.56 49.56	50.08 50.08		RAW Wash	.00	.00	21.00	. 73	26.84	51.43 6378.00		-1.00
	52.82	54.56		RAW	1.60	68.00 .00	12.29 10.15	. 69 . 74	30.38 27.98	56.64 7249.00 61.13 7349.00		6.50
-	52.82	54.56	18	WASH	1.60	91.00	8.41	.77	28.53	62.29 7527.00		- 1 - 00 2 - 50
	59.93	61.32		RAW	.00	.00	10.58	.75	26.88	61.79 7373.00		-1.00
	59.93	61.32	19	WASH	1.60	89.00	8.36	.96	27.31	63.37 7567.00		2.00
	62.08	62.66		RAW	.00	.00	19.05	.65	26.00	54.30 >6603.00		-1.00
	62.08	62.66		WASH	1.60	73.00	10.72	. 63	27.29	61.36 7387.00	.00	3.50
	72.48	76.01		RAW	.00	.00	16.97	. 65	25.57	56.81 \6737.00	.00	-1.00
	72.48	76.01	21	WASH	1.60	76.00	9.53	1.03	26.41	63.03 7424.00	. 00	2.50
												
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EAM	TOP	ВОТ	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB KCAL	SULF	FSI
5 -	118.86	119.12	20	RAW	-00	.00	41.60	.79	21.60	36.01 4527.00	1.35	-1.00
5 5	118.86	119.12	20	WASH	1.60	46.00	18.62	1.19	26.08	54.11 6629.00	1.29	1.00
7 5	120.16	120.76	21	RAW	.00	.00	56.12	.74	16.96	26.18 >3165.00	. 28	-1.00
	120.16	120.76	21	WASH	1.60	30.00	15.44	1.33	26.70	56.53 6883.00	. 52	1.00
	123.43	124.46	22	RAW	.00	.00	27.33	.73	26.40	45.54 ~5682.00	.62	-1.00
ļ	123.43	124.46	22	WASH	1.60	61.00	13.70	1.90	27.78	56.62 6966.00	. 62	1.00
<u> </u>	139.39	139.85	23	RAW	.00	.00	24.37	. 60	27.04	47.99 ~6099.00	3.07	-1.00
}	139.39	139.85	23	WASH	1.60	59.00	11.69	.88	29.Q8	58.35 7288.00	1.88	1.00
3	141.39	142.42	24	RAW	.00	.00	15.79	. 61	27.12	56.48 - 6803.00	.86	-1.00
3	141.39	142.42	24	WASH	1.60	79.00	9.21	1.19	27.28	62.32 7443.00	.70	1.00
}	144.55	144.92	25	RAW	.00	.00	33.46	.55	27.16	38.83 \4884.00	1.85	-1.00
)	144.55	144.92	25	WASH	1.60	34.00	17.00	1.17	26.30	55.53 6768.00	1.38	1.00
)	148.78	149.11	26	RAW	.00	.00	36.85	. 54	24.24	38.37 34971.00	1.27	-1.00
)	148.78	149.11	26	WASH	1.60	55.00	18.89	. 88	28.60	53.39 6662.00	1.42	1.00
	151.15	152.10	27	RAW	.00	.00	14.71	. 45	29.30	55.54 6860.00	. 66	-1.00
	151.15	152.10	27	WASH	1.60	82.00	8.34	. 85	29.45	61.36 7524.00	.60	2.50
<u> </u>	152.57	153.68	28	RAW	.00	.00	24.47	. 65	24.67	50.21 \ 6051.00	. 50	-1.00
2	152.57	153.68	28	WASH	1.60	72.00	12.99	1.05	27.10	58.86 7074.00	.53	1.50
	154.82	155.34	29	RAW	.00	.00	17.88	.50	28.72	52.90 6621.00	2.89	-1.00
!	154.82	155.34	29	WASH	1.60	78.00	10.71	. 98	29,44	58.87 7330.00	1.26	2.50
	275.50	277.19	30	RAW	.00	.00	13.61	. 59	28.48	57.32 7128.00	1,50	-1.00
l	275.50	277.19	30	WASH	1.60	83.00	9.67	. 92	29.26	60.15 7530.00	.77	5.00
	280.27	282.07	31@32	RAW	.00	.00	12.04	. 43	27.87	59.66 7303.00	1.00	-1.00
	280.27	282.07	31032	WASH	1.60	87.00	8.83	:80	28.34	62.03 7562.00	4.79	4.50
†	282.54	282.78	33	RAW	.00	.00	24.82	. 45	27.40	47.33 5880.00	. 90	-1.00
7	282.54	282.78	33	WASH	1.60	60.00	9.96	.62	28.75	60.67 7409.00	.60	3,50
1	283.49	284.34	34	RAW	.00	.00	16.63	.50	28.49	54.38 6805.00	.61	-1.00
1	283.49	284.34	34	WASH	1.60	63.00	8.46	.61	29.83	61.10 7604.00	. 93	6.00

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SEAM	TOP	BOT	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOŁ	CARB KCAL	SULF	FSI	
10	33.00	33.86	01	RAW	.00	.00	19.80	1.52	28.47	50.21 6422.00	2.05	-1.00	
10	33.00	33.86	01	WASH	1.60	74.00	7.62	. 99	32.77	58.62 7594.00	3.19	4.00	
9	42.35	43.22	02	RAW	.00	. 00	10.12	1.35	32.87	55.66 >7386.00	2.42	-1.00	
9	42.35	43.22	02	WASH	1.60	90.00	7.46	. 99	35.Q5	56.50 7645.00	2.31	7.00	
8	44.45	46.69	03	RAW	.00	.00	14.40	1.08	28.22	56.30 6924.00	1.27	~1.00	
8	44.45	46.69	03	WASH	1.60	80.00	6.97	1.29	29.67	62.07 7628.00	. 96	2.00	
7	67.05	68.34	04	RAW	_00	.00	18.15	1.22	28.10	52.53 >6631.00	1.63	-1.00	
7	67.05	68.34	04	WASH	1.60	78.00	9.11	1.05	31.45	58.39 7473.00	1.73	3.50	
6	71.86	74.19	05	RAW	.00	.00	40.54	1.47	20.18	37.81 74566.00	.83	-1.00	
6	71.86	74.19	05	WASH	1.60	52.00	8.63	1.14	28.86	61.37 7475.00	4.48	2.00	
6	75.00	75.54	06	RAW	.00	.00	11.26	1.10	30.15	57.49 >7277.00	2.00	-1.00	
6	75.00	75.54	06	WASH	1.60	83.00	6.72	1.02	32.00	60.26 7714.00	. 48	2.50	
2	82.14	83.95	Q7	RAW	.00	.00	11.67	1.30	27.84	59.19 > 7072.00	.48	-1.00	
2	82.14	83.95	07	WASH	1.60	86.00	7.51	1.16	28.71	62.62 7568.00	1.80	2.00	
2	85.29	86.30	08	RAW	00	.00	22.02	1.26	24.04	52.68 76165.00	1.07	-1.00	
2	85,29	86.30	08	WASH	1.60	68.00	11.06	1.29	26.65	61.00 7184.00	.61	1.00	
1	231.20	235.44	09	RAW	.00	.00	19.15	.78	26.89	53.18 76576.00	1.43	-1.00	
1	231.20	235,44	09	WASH	1.60	71.00	7.72	. 77	29.74	61.77 7708.00	. 91	6.00	
1	236.12	237.22	10	RAW	.00	.00	16.43	1.10	27.15	55.32 >6770.00	.37	-1.00	
1	236.12	237.22	10	WASH	1.60	78.00	7.97	. 78	29.52	61.73 7655.00	. 41	7.50	
1	242.80	243.85	11	RAW	.00	.00	39.71	1.13	20.43	38.73 4544.00	. 20	-1.00	
1	242.80	243.85	11	WASH	1.60	35.00	19.47	.85	23.93	55.75 6532.00	. 28	2.00	

Target on the Xarax 9700 E.P.

1 2 2 2 2 2 2	96.44 96.44 02.70 02.70 10.25 10.25 18.60	200.92 200.92 203.10 203.10 212.16 212.16 219.10	63 64 65 65	RAW Wash Raw Wash Raw	.00 1.60 .00	.00	14.82	1.21	26.62		6969.00	3.36	-1.00	
2 2 2 2 2	02.70 02.70 10.25 10.25 18.60	203.10 203.10 212.16 212.16 219.10	64 64 65 65	WASH RAW WASH RAW	1.60 .00	84.00 .00	7.16							
2 2 2 2	02.70 10.25 10.25 18.60	203.10 212.16 212.16 219.10	64 65 65	WASH RAW	1.60			. • .	27.91		7712.00	1.75	4.50	
2 2 2	10.25 10.25 18.60	212.16 212.16 219.10	65 65	RAW			26.48	. 95	26.67		►5841.00	5.24	-1.00	
2	10.25 18.60	212.16 219.10	65		00	66.00 .00	16,59 24.91	. 70	28.38		6867.00	1.03	6.50	
	18,60		66	WASH	.00 1.60	65.00	11.12	1,16 ,93	25.18 27.08		5894.00 7302.00	. 35 . 40	-1.00 4.00	
	18.60	219.10		RAW	.00	.00	30.12	. 99	23.75		►5385,00	.53	-1.00	
			66	WASH	1.60	58.00	13.86	. 89	25.55	59.70	7050.00	. 56	3.00	
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SEAM	TOP	BOT	SAMPLE	ATYP	5G	YIELD	ASH	RESMOIST	VOL	CARB KCAL	5ULF	FSI	
,	16.60	17.66	12	RAW	.00	.00	16.45	1.38	27.57	54.60 36675.00	1.83	-1.00	
,	16.60	17.66	12	WASH	1.60	76.00	9.38	1.38	29.65	59.59 7351.00	1.42	2.50	
7	23.78	24.43	13	RAW	.00	.00	15.94	1,25	25.95	56.86 6730.00	4.38	-1.00	
,	23.78	24.43	13	WASH	1.60	77.00	9.49	1.19	28.04	61.28 7346.00	2.38	1.00	
	25.70	27.24	14	RAW	.00	.00	6.67	1.17	28.94	63.22 7598.00	1.07	-1.00	
,	25.70	27.24	14	WASH	1.60	90.00	5.52	1.35	29.80	63.33 7676.00	. 96	1.50	
	34.17	37.14	15	RAW	.00	.00	15.57	1.54	25.96	56.93 6738.00	. 57	-1.00	
i	34,17	37.14	15	WASH	1.60	84.00	7.51	1.71	28.87	51.91 743B.QQ	.52	2.00	
5	37.84	39.64	16	RAW	.00	.00	6.94	1.06	29.37	62.63 \$7573.00	. 8 1	-1.00	MISSIM
;	37.84	39.64	16	WASH	1.60	92.00	4.63	1.27	29.64	64.46 7769.00	.83	2.00	14(100).5
}	56.70	57.12	17	RAW	.00	. 00	16.60	1, 12	27.19	55.09 6752.00	2.92	-1.00	from L
3	56.70	57.12	17	WASH	1.60	81.00	10.99	1.51	27.91	59,59 7245.00	2.07	1.50	The half
}	58.09	59.25	18	RAW	.00	.00	15.11	1.28	26.95	56.66 6801.00	1.62	-1.00	da
}	58.09	59.25	18	WASH	1.60	82.00	9.38	1.46	26.77	62.39 7348.00	1.03	1.50	
2	67.14	69.99	19	RAW	.00	.00	23.60	. 90	24.88	50.62 6065.00	.51	-1.00	
	67.14	69.99	19	WASH	1.60	73.00	9.59	1.25	27.09	62.07 7407.00	45	1.00	

TOP	Bat	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB KCAL	544.5	FSI	
 							_ <u>KEJMBIJI</u>		CARD KCAL	SULF		
18.94	22.27	47	RAW	.00	.00	40.03	1, 19	23,19	35.59 4544.00	1.86	-1.00	
18,94	22.27	47	WASH	1.60	52.00	8.50	1.51	29.98	60.01 7447.00	1.52	1.50	
 44.96	45.36	48	RAW	.00	.00	31.94	.91	33.19	33.96 \4684.00	2.30	-1.00	
44.96	45.36	48	WASH	1.60	46.00	11.66	1.48	28.86	58 00 7214.00	1.58	2.50	
46.00	47.92	49	RAW	.00	.00	25.99	1.20	23.51	49.30 \ 5866.00	1.56	-1.00	
46.00	47.92	49	WASH	1.60	68.00	10.99	1.79	25.64	61.58 7203.00	1.05	1.00	
 48.33	49.22	50	RAW	.00	.00	39.84	. 99	25.82	33.35 \4306.00	2.35	-1.00	
48.33	49.22	50	WASH	1.60	43.00	10.37	1.44	27.02	61.17 7283.00	1.12	1.00	
53.76	54.22	51	RAW	.00	.00	39.19	. 92	22.70	37.19 4765.00	3.41	-1.00	
53.76	54.22	51	WASH	1.60	.00	18.42	1.37	26.89	53 32 6667 00	1.91	1.00	
 55.95	56.60	52	RAW	.00	.00	31.56	. 93	28.41	39.10 34906.00	. 58	-1.00	
55.95	56.60	52	WASH	1.60	48.00	12.02	1.62	27.79	58.57 7121.00	. 52	1.00	 .
57.08	57.40	53	RAW	.00	.00	17.41	.99	26.65	54.95 >6598.00	. 82	-1.00	
57.08	57.40	53	WASH	1.60	81.00	10.39	1.39	27.13	61.09 7295.00	.71	1.00	
 154.92	157.16	54	RAW	. 00	.00	11.21	. 84	28.31	59.64 7293.00	1.58	-1.00	
154.92	157.16	54	WASH	1.60	88.00	7.17	. 98	29.04	62.81 7680.00	- 86	5.00	
157.34	160.46	55	RAW	.00	.00	21.11	. 93	26.46	51.50 6348.00	.76	-1.00	
157.34	160.46	55	WASH	1.60	72.00	10.60	.71	28.87	59.82 7367.00	. 52	5.00	
 163.05	163.94	56	RAW		.00	19.57	1.41	27.87	51.15 6364.00	.42	~1.00	
163.05	163.94	56	WASH	1.60	72.00	9.32	1.19	29.55	59.94 7475.00	. 36	6.50	

32D-	225								,					
M 	TOP	<u>BOT</u>	SAMPLE	ATYP	SG 	AIÈFD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	·
	13.62	14.10	35	RAW	.00	.00	18.72	1.11	 28.94	51.23	6615.00	2.30	-1.00	
	13.62	14.10	35	WASH	1.60	74.00	9.64	. 98	31.43	57.95	7479.00	1.44	4.50	
	14.55	15.81	36	RAW	.00	.00	17.77	1.22	24.47	56.54	6627.00	2.81	-1.00	
	14.55	15.81	36	WASH	1.60	80.00	10.23	1.48	25.84	62.45	7302.00	.84	1.00	
	16.59	16.88	37	RAW	. 00	- 00	27.90	1.12	25.80	45.18	5592.00	3.08	-1.00	
	16.59	16.88	37	WASH	1.60	59.00	9.93	1,11	26.87	62.09	7374.00	1.23	1.00	
	22.28	22.78	38	RAW	. 00	<u> </u>	36.30	. 98	24.49	38.23	5050.00	10.28	-1.00	
	22.28	22.78	38	WASH	1.60	51.00	19.91	1.03	28.13	50.93	6577.00	1.90	1.00	
	24.37	25.22	39	RAW	.00	.00	14.72	1.38	30.40	53.50	6897.00	1.44	-1.00	
	24.37	25.22	39	WASH	1.60	82.00	7.71	1.84	30.89	59.56	7541.00	. 98	3.50	
	26.64	28.84	40	RAW	. 00	.00	41.39	1.34	23.20	34.07	4460.00	4,99	-1.00	
	26.64	28.84	40	WASH	1.60	43.00	13.08	1.19	30.02	55.71	7145.00	1.64	2.50	
	29.64 29.64	33.07 33.07		RAW	.00	.00	28.34	. 74	24.93	45.99	5650.00	1.76	-1.00	
	29.64 33.68	34,27		WASH	1.60	63.00	9.48	1.06	28.56	60.90	7421.00	. 63	1.00	
	33.68		42	RAW WASH	.00	.00	19.50	1.15	26.68	52.67	6323.00	1.19	-1.00	
	190.65	192.77		RAW	1.60	73.00	9.16	1.66	26.24	62.94	7406.00	. 83	1.00	
	190.65	192.77	-	WASH	.00 1.60	.00	9.48	1.06	28.31	61.15	7464.00	. 56	-1.00	
	193.01	194.34		RAW	.00	89.00 .00	6.54 20.85	1.31 .78	28.25	63,90	7762.00	. 53	4.00	
	193.01	194.34		WASH	1.60	67.00	10.78	1.20	27.66 28.87	50.71 59.15	6415.00	2.49	-1.00	
	271.76	273.86		RAW	-00	.00	12.26	.80	27.89	59.15 59.05	7432.00 7219.00	1.33	3.50	
	271.76	273.86		WASH	1.60	85.00	6.53	1,13	27.59	64.75	7822.00	1.88 .88	-1.00	
	274,14	274.46		RAW	.00	.00	17.16	.72	30.02	52.10	6398.00	.73	4.00 -1.00	
	274.14	274.46		WASH	1.60	76.00	6.51	1.37	27.65	64.47		.74	4.00	
							3.0,	1.27	21.00	04.47	7740.00	. 74	4.00	
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AM	226 TOP		SAMPLE	ATYP	SG	YIELD		RESMOIST	VOL	CARB		SULF	FSI	
	145.12 145.12 149.53	147.76 147.76 154.36	67-69 67-69	RAW Wash Raw	.00 1.60 .00	.00.83.00	14.29 8.21 34.93	.57 .59	26.28 26.61 23.15	64.59	6999.00 7569.00 4974.00	2.71 1.37 .81	 -1.00 3.50 -1.00	
	149.53 157.62 157.62	154.36 158.12 158.12	70 - 71	WASH RAW WASH	1.60 .00 1.60	49.00 .00 40.00	14.26 37.97 14,32	.87 1.01 .64	27.45 22.98 26.13	57.42 38.04	6945.00 4468.00 6948.00	. 83 . 36	5.50 -1.00 4.50	
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SEAM	TOP	BOT SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL.	CARB	KCAL	SULF	FSI	
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6	10.86	11.27 • 76	RAW	.00	.00	15.67	1.40	29.35	53.58	6877.00	3.21	-1.00	
6	10.86	11.27 76	WASH	1.60	84.00	11.43	1.20	31.47	55,90	7279.00	3.11	3.00	
5	22.62	25.51 78	RAW	.00	.00	14.36	. 75	28.30		6936.00	. 45	-1.00	
5	22.62	25.51 78	WASH	1.60	81.00	6.27	1.21	30.48	62.04	7655.00	.51	2.00	
5	26.06	27.13 79	RAW	.00	.00	20.45	1.45	25,76	52.34	6400.00	2.18	-1.00	
5	26.06	27.13 79	WASH	1.60	79.00	9.34	1.37	29.82	59.47	7393.00	1.15	1.00	
4	29.23	29.74 `80	RAW	. 00	.00	9.43	1.21	31.44	57.92	7323.00	1.39	-1.00	
4	29.23	29.74 80	WASH	1.60	84.00	2.88	1.44	32.05	63.63	7974.00	.61	2.00	
2	61.16	61.51 81	RAW	.00	.00	26.01	1.05	31.66	41.28	5646.00	2.75	-1.00	
2	61.16	61.51 81	WASH	1.60	65.00	15.23	1.08	29.50	54,19	6996.00	.70	2.50	
1	218.24	220.12 -82	RAW		.00	11.55	1.00	28.49	58.96	7313.00	1.41	-1.00	
1	218.24	220.12 82	WASH	1.60	88.00	8.58	1.30	28.84	61.28	7560.00	1.06	6.00	
†	221.70	227.83 🦜 83	RAW	.00	.00	20.61	. 95	26.10	52.34	6446.00	2.24	-1.00	
†	221.70	227.83 83	WASH	1.60	72.00	9.44	1.11	29.31	60.14	7493.00	1.24	5.00	
1	228.28	228.62 *84	RAW	.00	.00	36.07	. 95	22.50	40.48	4970.00	.47	-1.00	
[1	228.28	228.62 84	WASH	1.60	46.00	11.01	1.28	27.51	60.20	7353.00	.69	6.00	
 1	229.44	230.67 >85	RAW	. 00	. 00	18.29	1.08	26.18	54.45	6521.00	.40	-1.00	
1	229.44	230.67 85	WASH	1.60	72.00	8.51	1.32	24.82	65.35	7547.00	. 42	5.50	
1	236.56	<u>237.10 86</u>	RAW	.00	.00	45.03	1.17	19.73	34.07	4106.00	. 26	-1.00	
] 1	236.56	237.10 86	WASH	1.60	28.00	17.57	1.43	26.97	54.03	6711.00	. 40	4.00	

TW82D-	-229												
SEAM	TOP	BOT SAMPLE	ATYP	\$G	YIELD	ASH	RESMDIST	VOL	CARB	KCAL	SULF	F\$I	
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8	78.60	79.20 250	RAW	.00	.00	14.22	. 76	30.98	54.04	7051.00	3.61	-1.00	
8	78.60	79.20 250	WASH	1.60	85.00	9.19	1.09	31.85	57.87	7494.00	2.26	3.50	
7	85.99	87.13 \ 251	RAW	.00	.00	14.38	1.07	29.37	55,18	7014.00	2.87	-1,00	
7	85.99	87.13 251	WASH	1.60	83.00	7.24	1.12	31.87	59.77	7644.00	1,77	3.00	
6	92.67	94.88 \252	RAW	.00	.00	13.17	1.05	27.29	58.49	7101.00	4.12	-1.00	
6	92.67	94.88 252	WASH	1.60	84.00	7.67	1.21	28.90	62.22	7587.00	1.58	1.00	
6	97.56	97.94 253	RAW	.00	00	6.67	1.05	30.74	61.54	7722.00	1.70	-1.00	
6	97.56	97.94 253	WASH	1 - 6 Q	92.00	4.03	1.22	32.23	62.52	7926.00	1.35	2.00	
6	98.18	99.43 \ 254	RAW	.00	.00	17.17	. 92	27.90	54.01	6685.00	3.10	-1.00	
6	98.18	99.43 254	WASH	1.60	79.00	7.22	1.52	29.23	62.03	7540.00	.91	1.00	-
5	105.06	107.90 255	RAW	.00	.00	18.34	1.06	25.49	55.11	6554.00	. 49	-1.00	
5	105.06	107.90 255	WASH	1.60	77.00	7.71	1.40	28.79	62.10	7509.00	.59	1.00	
5	109.26	109.55 256	RAW	.00	.00	19.92	.91	27.44	51.73	6415.00	1.96	-1.00	
5	109.26	109.55 256	WASH	1.60	79.00	8.88	1.23	30.26	59.63	7439.00	1.27	1.50	
5	109.76	110.08 257	RAW	. 00	.00	11.72	1.00	27.61	<u>59</u> .67	7232.00	1.14	-1.00	
5	109.76	110.08 257	WASH	1.60	93.00	9.99	1.05	29.38	59.58	7391.00	. 95	2.50	
5	122.39	123.74 > 258	RAW	.00	.00	13.31	1.02	26.98	58.69	7059.00	1.20	-1.00	
5	122.39	123.74 258	WASH	1.60	86.00	9.70	1.29	27.24	61.77	7388.00	.00	1.00	
5	123.93	126.48 260	RAW	.00	.00	29.25	. 79	23.64	46.32	5576.00	1.42	-1.00	
5	123.93	126.48 260	WASH	1.60	64.00	11.03	1.35	26.46	61.16	7253.00	. 78	1.00	
4	131.36	132.55 ~261	RAW	.00	.00	18.57	. 90	28.13	52.40	6637,00	1.42	-1.00	
4	131.36	132.55 261	WASH	1.60	84.00	11.62	1.26	29.91	57.21	7263.00	1.26	3.00	
3	142.47	144.79 ~262	RAW	. 00	.00	31.55	. 85	23.46	44 . 14	5415.00	3.87	-1.00	
	142.47	144.79 262	WASH	1,60	50.00	15.78	1.24	26.99	55.99	6854.00	2.04	1.00	
2 2	145.76 145.76	146.78 \ 263 146.78 \ 263	RAW	.00	.00	25.12	.81	25.35	48.72	6032.00	1.37	-1.00	
5	162.29	163.32 264	WASH	1.60	62.00	7.37	1.25	28.70	62.68	7612.00	1.27	2.00	
5	162.29	163.32 264	RAW WASH	.00	.00	16.02	.88	25.54	57.56	6794.00	1.39	-1.00	
5	163.64	163.95 * 265	RAW	1.60	79.00	10.19	1.18	26.21	62.42	7345.00	1.14	1.00	
5	163.64	163.95 265	WASH	1.60	-00	20.66	.87	23.58	54.89	6380.00	1.56	-1.00	
4	170.77	171.30 - 266	RAW	.00	77.00 .00	11.20 29.68	1.29 .72	25.14	62.37	7214.00	1.37	1.50	
4	170.77	171.30 266	WASH	1.60	64.00	14.21	. 92	24.88	44.72	5450.00	- 48	-1.00	
1 4	173.27	174.89 267	RAW	.00	.00	12.27	.86	27.47	57.40	6954.00	.52	1.50	
4	173.27	174.89 267	WASH	1.60	81.00	3.97	1.36	27.14	59.73 64.99	7123.00	. 49	-1.00	
3	182.59	183.14 - 268	RAW	-00	.00	23.08	, .97	25.20	50.75	7120.00	. 53	1.50	
3	182.59	183.14 268	WASH	1.60	71.00	13.10	1,13	26.84	58.93	6151.00 7091.00	. 81	-1.00	
3	183.70	184.36 270	RAW	.00	.00	62.74	. 82	15.76	20.68		. 62	1.00	
3	183.70	184.36 270	WASH	1.60	20.00	15.42	1.00	25.87	57.71	2286.00 6904.00	.58	-1.00	
3	184.51	184.88 ~ 271	RAW	.00	.00	87.84	.79	8.49	2.88	.00	. 67 . 15	1.00 -1.00	
3	184.51	184.88 271	WASH	1.60	-00	.00	.00	.00	.00	.00	.00	-1.00	
3	184.88	186.30 - 272	RAW	.00	.00	53.34	.61	18.26	27.79	3457.00	.62	-1.00	
3	184.88	186.30 272	WASH	1,60	33.00	16.91	1.18	25.86	56.05	6797.00	.73	1.00	
2	188.50	189.56 - 273	RAW	.00	.00	14.31	.61	28.74	56.34	6920.00	. 73	-1.00	
2	188.50	189.56 273	WASH	1.60	80.00	8.41	1,04	28.92	61.63	7525.00	.53	2.50	
2	190.14	190.90 274	RAW	.00	.00	36.62	. 64	21.36	41.38	4934.00	. 32	-1.00	
2	190.14	190.90 274	WASH	1.60	49.00	15.41	1.15	25.08	58.36	6907.00	. 43	1.00	
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TW82D-	-231												
SEAM	TOP	BOT SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
10	97.79	98.97 🔪 292	RAW	.00	.00	28.34	1.30	24.54	45.82 553	29.00	3.96	-1.00	
10	97.79	98.97 292	WASH	1.60	64.00	9.28	1.29	27.24		30.00	2.37	1.50	
9	105.58	105.90 293	RAW	.00	.00	24.80	1.48	22.79		77.00	6 84	-1.00	
9	105.58	105.90 293	WASH	1.60	63.00	11.20	1.05	24.66		55.00	3.89	1.00	
9	106.60	107.24 ~294	RAW	- 00	.00	20.99	1.12	25.59		93.00	1.08	-1.00	
9	106,60	107.24 294	WASH	1.60	69.00	8.94	1.41	25.27		94.00	1.05	2.00	
9	109.71	110.24 295	RAW	- 00	.00	20.94	1.20	25.66		98.00	3.47	-1.00	
9	109.71	110.24 295	WASH	1.60	67.00	7.06	1.22	26.36		49.00	2.25	1.50	
8	115.57	117.56 ~ 296	RAW	.00	.00	17.04	1.24	21.82		52.00	1.07	-1.00	
8	115,57	117.56 296	WASH	1.60	81.00	11.36	1.23	23.35		25.00	1.10	1.00	
17	135.01	135.44 ~297	RAW	. 00	.00	26.92	1.21	23.56		03.00	5.05	-1.00	
7	135.01	135.44 297	WASH	1.60	60.00	8.74	1.10	25.91		31.00	2.83	2.50	
6U	144.99	148.22 -298	RAW	.00	. 00	15.53	1.03	24.74		51.00	1.37	-1.00	
en	144,99	148.22 298	WASH	1.60	82.00	6.47	1.47	27.06	65.00 75	78.00	.94	1.50	
6U	148.62	149.34 - 299	RAW	.00	.00	19.46	1.05	21.37	58.12 642	22.00	.55	-1.00	
6U	148.62	149,34 299	WASH	1.60	79.00	9.34	1.52	23.05		99.00	. 59	1.00	
3	166.17	167.14 301	RAW	.00	. 00	11.32	1.10	22.89	64.69 729	58.00	1.03	-1.00	
3	166.17	167.14 301	WASH	1.60	86.00	7.40	1.27	23.66	67.67 75	77.00	.80	1.00	
3	169.28	170.23 - 302	RAW	.00	.00	49.00	1.04	17.96	32.00 375	54.00	2.58	-1.00	
3	169.28	170.23 302	WASH	1.60	26,00	17.29	.81	24.74	57.16 679	59.00	1.31	4.00	
3	170.89	171.16 > 303	RAW	.00	.00	30.08	.96	21.33	47.63 546	69.00	1.80	-1.00	
3	170.89	171.16 303	WASH	1.60	65.00	14.13	. 80	22.67		79.00	1.29	2.00	
2	176.74	178,90 ~ 304	RAW	.00	.00	28.63	.98	21.53		43.00	1.52	-1.00	
2	176.74	178.90 304	WASH	1.60	68.00	9.16	. 79	25.36		62.00	1.41	2.50	
2	179.83	180.26 ~305	RAW	.00	.00	38.84	.74	19.61		21.00	.54	-1.00	
2	179.83	180.26 305	WASH	1.60	45.00	13.62	. 86	24.20	61.32 70	18.00	. 70	1.00	
2	181.01	182.11 -306	RAW	.00	.00	11.13	1.03	24.23	63.61 718	82.00	. 60	-1.00	
2	181.01	182.11 306	WASH	1.60	89.00	8.18	1.47	24.54	65.81 749	98.00	.77	1.50	
1	305.76	306.68 -307	RAW	.00	.00	19.69	.89	26.44	52.98 670	00.00	3.95	-1.00	
1	305.76	306.68 307	WASH	1.60	76.QQ	11.13	. 69	28.67	59.51 753	36.00	1.80	5.00	
1 1	306.98	307.99 -308	RAW	.00	.00	43.44	.89	20.43	35.24 438	80.00	2.31	-1.00	
!	306.98	307.99 308	WASH	1.60	27.00	14.87	. 75	26,59	57.79 71	76.00	. 95	3.50	
!	309.64	310.45 >309	RAW	.00	.00	44.49	. 9 1	22.25	32.35 43	19.00	3.59	-1-00	
1	309.64	310.45 309	WASH	1.60	42.00	17.56	. 59	30.44	51.41 696	64.00	2.29	6.50	
1	313.98	314.98 ~ 310	RAW	.00	. 00	38.15	.85	21.54	39,46 483	20.00	2.69	-1.00	
1	313.98	314.98 310	WASH	1.60	40.00	18,14	. 70	28.21		09.00	1.62	6.00	
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AGE	28												
TW82D- Seam	232 TOP	BOT SAMPLE	ATYP	60	WIFLE	4.511	DERMOTAT						
		BUI SAMPLE	- ALTP	SG	YIELD	ASH	RESMOIST	VOL_	CARB	KCAL	SULF	FSI	
3	10.99	12.73 > 133	RAW	.00	.00	13.80	1.23	28.08	56.89	6967.00	1.48	-1.00	
- 3	10,99	12.73 133	WASH	1,60	82.00	8.73	1.29	29.17	60.81	7390.00	1,11	1.00	
7	31.95	32.34 \134	RAW	.00	.00	34.57	.88	23.96	40.59	5128,00	5.83	-1.00	
7	31.95	32.34 134	WASH	1.60	59.00	7.04	1.48	31.36		7570.00	1.41	4.00	
7	46.04	48.10 \135	RAW	.00	.00	19.75	.91	26.67	52.67	6392.00	2.19	-1.00	
7	46.04	48.10 135	WASH	1.60	77.00	9.55	1.55	29.19	59.71	7323.00	1.56	1.50	
5	52.60	55.72 \136	RAW	.00	.00	44.94	.92	20.09	34.05	4176.00	. 59	-1.00	
3	52,60	55.72 136	WASH	1.60	43.00	6.83	1.47	29,22	62.48	7605.00	. 53	1.00	
3	58.24	58.65 >137	RAW	.00	.00	19.25	. 99	28.28	51.48	6282.00	1.86	-1.00	
5	58.24	58.65 137	WASH	1.60	75.00	10.96	1.47	27.56	60.01	7238.00	1.12	1.00	
5	60.35	62.40 138	RAW	.00	.00	15.36	1.20	27.54	55.90	6835.00	1.39	-1.00	
,	60.35	62.40 138	WASH	1.60	82.00	4.87	1.38	30.54	63.21	7761.00	1.13	3.50	
١,	73.24	74.36 ~ 139	RAW	.00	00	22.03	1.02	27.03	49.92	6305.00	4.11	-1.00	
ļ	73.24	74.36 139	WASH	1.60	66.00	10.18	1.19	31.07	57.56	7339.00	2.92	4.00	
<u> </u>	90.73	94 . 44 🥆 140	RAW	.00	.00	27.43	1,40	24,10	47.07	5723.00	1.85	-1.00	
	90.73	94.44 140	WASH	1.60	60.00	7,48	1.43	28.61	62.48	7539.00	. 75	2.00	
2	97.07	97.72 ~141	RAW	- 00	.00	39.52	. 89	20.79	38.80	4611.00	.38	-1.00	
<u>!</u>	97.07	97.72 141	WASH	1.60	60.00	6.91	1,56	27.60	63.93	7517.00	. 46	2.00	
	152.70	153.15 -142	RAW	.00	-00	24,34	.78	28.90	45,98	5980.00	5.86	-1.00	
	152,70	153.15 142	WA5H	1.60	61.00	7.39	. 99	32.66	58.96	7622.00	1.87	6.50	
	154.51	157.24 - 143	RAW	. 00	.00	14.10	. 97	27.39	57.54	6995.00	1.62	-1-00	
	154.51	157.24 143	WASH	1.60	83.00	6,92	1.21	28.05	63,82	7663.00	.92	2.00	
	171.15	172.56 -144	RAW	.00	.00	48.34	1.02	18,94	31.70	3890.00	1, 15	-1.00	
	171.15	172.56 144	WASH	1.60	46.00	9.73	1,15	28.22	60.90	7429.00	1.31		
	178.25	178.59 145	RAW	.00	.00	13.43	1.09	'28.83	56.65	7156.00	1.65	-1.00	
	178.25	178.59 145	WASH	1.60	86.00	6.24	. 89	30.71	62.16	7790.00	1,23	3.50	
	178.90	179.62 146	RAW	.00	.00	20.39	1.11	24.89	53.61	6354.00	1.83	-1.00	
	178.90	179.62 146	WASH	1.60	75.00	11,19	. 98	26.07	6i.76_	7271.00	1.00	1.00	
	179.62	179.97 🔪 147	RAW	- 00	.00	54.09	1.00	17.89	27.02	3338.00	2.27	~1.00	
	179.62	179.97 147	WASH	1.60	32.00	20.73	. 89	26.01	52.37	6450.00	1.08	1.00	
	179.97	181.79 - 148	RAW	.00	.00	7.39	1.10	27.55	63.96	7614.00	. 79	-1.00	
	179.97	181.79 148	WASH	1.60	86.00	4.58	1.33	27.98	66.11	7860.00	.67	1.50	
	290.67	290.92 ~149	RAW	.00	.00	33.06	. 76	26.98	39.20	5315.00	1.78	-1.00	
	290.67	290.92 [149	WASH	1.60	58.00	11.05	, 62	28.00	60.34	7395.00	1.59	3.50	
	291.15	292.28 150	RAW	.00	.00	24.12	. 75	24.10	51.03	6089.00	1.81	-1.00	
	291.15	292.28 150	WASH	1.60	76.00	13.47	. 96	25.07	60.50	7095.00	1.45	2.00	
	306.55	307.05 151	RAW	.00	.00	44.12	. 76	19.91	35.21	4199.00	.30	-1.00	
,	306.55	307.05 151	WASH	1.60	29.00	17.37	. 84	25.96	55.83	6735.00	36	5.50	
	346.95	347.30 152	RAW	.00	.00	44.66	. 88	21.38	33.08	4034.00	. 60	-1.00	
	346.95	347.30 152	WASH	1.60	30.00	17.63	. 99	27.09	54.29	6693.00	42	7.50	
	347.85	348.35 ~153	RAW	.00	.00	57.67	1.00	18.80	22.53	2677.00	. 20	-1.00	
•	347.85	348.35 153	WASH	1.60	18.00	11.40	1.05	27.04 1	60.51	7275.00	. 53	7.00	
<u> </u>	349.Q3	349.30 154	RAW	.00	.00	45.98	1.02	21.80	31.20	3878 00	.42	-1.00	
3	349.03	349.30 154	WASH	1.60	32.00	16.69	.97	27.69	54.65	6795.00	.61	4.50	
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SEAM	TOP	BOT SAMPLE	ATYP	SG 	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
6L	21.76	28.40 108	RAW	.00	.00	9.08	1.14	29.82	59.96	7466.00	1.64	-1-00	
6U 6U	21.76 29.89	28,40 108 36,16 \ 109	WASH RAW	1.60 .00	91.00	5.46 16.54	1.49 .96	31.10 27.50	61.95 55.00	7704.00 6752.00	1.09 2.06	6.00 -1.00	
6U 4	29.89 44.50	36.16 109	WASH	1.60	79.00	5.35	1.42	29.31	63.92	7720.00	1.05	3.00	
4	44.50	45.48 →110 45.48 110	RAW Wash	.00 1.60	.00 82.00	15.64 7.40	.94 1.83	24.04 25.31	59.38 65.46	6 878 .00 7 530 .00	1.67 1.11	-1.00 1.50	
4	46.60 46.60	47.04 111 47.04 111	WASH	1.60	62.00	$\frac{26.95}{14.54}$. 86	21.07	51.12	5806.00	2.31	-1.00	
3	57.86	58.24 ~ 112	RAW	.00	.00	14.54 31.83	1.61 .78	21.83 24.49	62.02 42.90	6894.00 5329.00	1.84 1.91	1,00 -1.00	
3 2	57.86 62.08	58,24 112 66,78 113	WASH Raw	1.60 .00	59.00 .00	12.45 19.89	1.24 1.39	27.97 .00	58.34	7146.00	1.98	2.00	
2	62.08	66.78 113	WASH	1.70	87.40	11.24	3.37	25.96	61.50	.00 7223.00	1.08	.00 3	-
1 1	178.30 178.30	180.36 ~114 180.36 114	RAW Wash	.00 1.60	.00 76.00	17.06 7.57	.77 1.08	25.32 26.08	56.85 65.27	6740.00 7630.00	2.08 1.15	-1.00 T 2.50	
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SEAM	TOP	BOT SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
Q	116.38	117.40 456	RAW	.00	.00	52.78	. 60	16.79	29.83	3388.00	2.82	-1.00	
Q	116.38	117.40 456	WASH	1.60	28.00	12.85	1.36	24.96	60.83	6974.00	.95	1.50	
6	134.92	135.65 ~457	WASH	1.60	91.00	5.06	1.59	27.39	65.96	7622.00	. 55	1.50	
6	134.92	135.65 457	RAW	.00	.00	13.23	1.37	25.50	59.90	6934.00	.87	-1.00	
6	136.07	137.44 ~458	RAW	.00	.00	29.05	1.06	23.43	46.46	5518.00	3.33	-1.00	
6	136.07	137.44 '458	WASH	1.60	60.00	11.53	1.13	28.02	59.32	7137.00	2.01	1.00	
Q	154.68	155.12 > 459	RAW	.00	.00	42.16	.74	29.62	27.48	3831.00	1.55	-1.00	
Q	154.68	155.12 459	WASH	1,60	26.00	19.26	.93	28.42	51.39	6616.00	2.04	3.00	
3	155.27	157.43 - 460	RAW	.00	.00	62.89	.97	15.71	20.43	2274.00	1.68	-1.00	
3	155.27	157.43 460	WASH	1,60	20.00	16.75	1.24	28.66	53.35	6741.00	1.10		
3	167.96	168.16 -461	RAW	.00	.00	37.02	.81	23.95	38.22	4940.00	-	2.00	
3	167.96	168.16 461	WASH	1.60	45.00	19.06	.89	27.45	52.60	6659.00	6.00 2.93	-1.00	
. 3	168.61	169.32 462	RAW	.00	.00	27.52	.74	26.08	45.66	5585.00		1.50	
3	168.61	169.32 462	WASH	1.60	68.00	14.29	1.23	26.90	57.58	6940.00	.76	-1.00	
3	169.56	169.94 #463	RAW	.00	.00	25,71	.72	22.53	51.04	5945.00	. 94	1.00	
. 3	169.56	169.94 (463	WASH	1.60	71.00	14.85	1.22	23.44	60.49	6907.00	38	-1.00	
. 2	173.40	174.24 464	RAW	- 00	.00	28.93	.75	22.50	47.82	5622.00	. 5 1	1.50	
. 2	173.40	174.24 464	WASH	1.60	69.00	15.66	1.49	24.35			. 45	-1.00	
. 2	174.68	175.02 465	RAW	-00	.00	36.92	.73	24.35	58.50	6825.00	- 46	1.00	
2	174.68	175.02 465	WASH	1.60	55.00	20.82	1.19		39.36	4855.00	57	-1.00	
. 2	175.64	176.20 466	RAW	-00	.00	38.73		24.45	53.54	6415.00	. 57	1.00	
2	175.64	176,20 466	WASH	1.60			.96	19.50	40.81	4629.00	5.23	-1.00	
		,,0,20 400	110 MH	1.00	47.00	15.47	.96	24.96	58.61	6843.00	2.45	1.00	

PAGE 31 TW82D-236 BOT SAMPLE ATYP TOP CARB SEAM SG YIELD ASH RESMOIST VOL SULF KCAL 150.73 151.38 286 RAW .00 .00 42.95 . 80 25.72 30.53 3826.00 3.52 1.00 150.73 151.38 286 WASH 1.60 30.00 10.74 27.06 4.00 1.11 61.09 7335.00 1.27 153.23 155.05 287 RAW .00 .00 56.30 .89 17.96 24.85 2989.00 2.51 1.50 153.23 155.05 WASH 1.60 23.00 14.02 1.14 27.43 57.41 6958.00 1.31 4.50

₩82D-: EAM 	TOP	BOT 123.22	SAMPLE	ATYP RAW	SG .00	YIELD 	ASH 17.55	RESMOIST .88	VOL 27.59	CARB	KCAL 6563.00	SULF .76	FSI -1.00	.
	22.42 422.42 123.59 123.59	123.22 124.59 124.59	173 174	WASH RAW WASH	1.60	79.00 .00 65.00	7.58 27.13 13.33	1.29 1.00 1.04	28.43 22.97 26.06	62.70 48.90	7520.00 5788.00 7025.00	.70 .61 .79	1.00\ -1.0Q\	
	124.97 124.97 125.49 125.49	125.31 125.31 126.05 126.05	175 175 176	RAW Wash	.00 1.60 .00	.00 73.00 .00 .00	13.33 24.56 15.92 11.42 8.84	.96 1.33 1.06	24.62 25.65 26.30 26.92	49.86 57.10 61.22	5931.00 6779.00 7212.00 7430.00	.72 .65 1.31	-1.00 1.00 -1.00	
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TW82D- SEAM	TOP	BOT SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
			7.7.7				KEJMOIJI		CARD	NOAL		F 31	
1	40.76	42.94 321	RAW	- 00	.00	12.97	1.02	28.23	57.78	7161,00	1.89	-1.00	
1	40.76	42.94 321	WASH	1.60	83.00	6.28	. 85	29.86	63.01	7750.00	1.44	4.00	
1	43.99	45.74 322	RAW	.00	-00	21.86	.93	27.57	49.64	6298.00	3.44	-1.00	
1	43.99	45.74 322	WASH	1.60	74.00	11.99	. 75	31.35	55.91	7304.00	2.46	6.50	
1	47.63	48.07 323	RAW	.00	.00	25.89	. 93	27,42	45.76	5908.00	1.03	-1.00	
1	47.63	48.Q7 323	WASH	1.60	68.00	16.00	. 94	29.52	53.54	6860.00	. 29	6.50	
1	49.14	50.46 > 324	RAW	.00	.00	19.12	1.31	26.47	53.10	6509.00	. 45	-1.00	
1	49.14	50.46 324	WA5H	1.60	84.00	13.85	1.28	27.57	57.20	7004.00	.46	4.00	
Q	56.56	57.14 325	RAW	.00	.00	36.32	1.13	22.57	39.98	4839.00	.36	-1.00	
Q	56.56	57.14 325	WASH	1.60	48.00	16.74	1.17	26.24	55.85	6734.00	. 48	1.50	
Q	89.75	90.19 > 326	RAW	.00	.00	42.82	1.05	27.50	28.63	3574.00	62	-1.00	
Ō	89.75	90.19 326	WASH	1.60	29 00	14.70	1.05	28 37	55.80	6890.00	. 93	6.50	

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SEAM	TOP	BOT SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
5	8.80	8.96 \87	RAW	.00	.00	50.09	. 85	24.47	24.59	.00	.41	- 00	
5	10.82	11.10~88	RAW	.00	. 00	15.30	1.12	27.90	55.68	6903.00	1,14	-1,00	
5	10.82	11.10 \88	WASH	1.60	88.00	11.18	1.09	27.63	60.10	7274.00	. 95	1.00	
7	12.04	12.24 89	RAW	-00	.00	23.78	1.24	24.30	50.68	6070.00	4.20	-1.00	
Ç	12.04	12.24 89	WASH	1.60	73.00	12.90	1.25	26.14	59.71	7065.00	1.37	1.00	
4	15.27	15.55 🦜 90	RAW	.00	- 00	31.51	. 89	33.20	34.40	4738.00	1.81	-1.00	
4	15.27	15.55 90	WASH	1.60	32.00	11.08	1.06	29.61	58.25	7262.00	1.64	1.00	
4	16.70	16.90 > 91	RAW	.00	. 00	35.92	1.37	24.58	38.13	4813.00	4.02	-1.00	
4	16.70	16.90 91	WASH	1.60	45.00	13.52	1.20	27.63	57.65	6995.00	3.17	1.00	
3	28.14	30.82 -92-94	RAW	.00	.00	25.88	. 99	28.12	45.01	5593.00	. 85	-1.00	
5	28.14	30.82 92-94	WASH	1.60	59.00	7.80	1.60	27.31	63.29	7455.00	. 74	1.00	
2	31.06	31.90 95	RAW	.00	.00	25.42	1.34	24.45	48.79	5810.00	. 52	-1.00	
2	31.06	31.90 95	WASH	1.60	70.00	13.77	1.38	25.52	59.33	6936.00	. 38	1.00	
2	32.68	32.96 ~ 96	RAW	.00	.00	31.34	1.17	27.15	40.34	4921.00	.50	- f - 00	
2	32.68	32.96 96	WASH	1.60	41.00	17.62	1.34	26.38	54.66	6565.00	. 54	1.00	
2	34.56	35.Q8 97	RAW	.00	.00	17.44	1.10	27.03	54.43	6559.00	1.32	-1.00	
2	34.56	35.Q 8 9 7	WASH	1.60	86.00	10.62	1.40	25.93	62.05	7278.00	. 99	1.00	

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	PAGE	37														
	TW82D SEAM	-242 TOP	вот	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL (~	SULF	FSI		
	1 1 1 1 1	111.51 111.51 117.42 117.42 118.54	112.00 112.00 117.88 117.88 118.84 118.84	288 288 289 289 290 290	RAW WASH RAW WASH RAW WASH	.00 1.60 .00	.00 53.00 .00 37.00	32.21 12.00 39.51 17.20 51.77	1.00 1.35 1.22 1.45	26.14 27.80 22.67 27.92 20.75	40.65 58.85 36.60 53.43 26.37	50.00 7087.00 4492.00	.42 .56 .21 .32	FSI 1.00 3.00 1.50 3.50 .50	1/2	D
	ς Ο	126.69	127.05 127.05	291	RAW WASH	1.60 .00 1.60	18.00 .00 27.00	18.57 42.63 16.39	1.52 1.18 1.64	26.35 23.44 26.31	53.56 32.75 55.66		.33 .37 .59	3.50 1,20 2.50		· ·
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	18.96 18.96 36.10	20.18 98 20.18 98	RAW WASH	.00 1.60	.00	17.25	1.43	26.33					
	18.96	20.18 98				17.25	1.43						
			WASH			~ ~~			54.99	6601.00	2.07	-1.00	
	30.10		C 4 1.4		80.00	8.98	1.43	27.79	61.80	7372.00	1.45	1.00	
	20.40	37.64 100	RAW	.00	.00	13.45	1.41	27.42	57.72	6968.00	. 54	-1.00	
	36.10	37.64 100	WASH	1.60	84.00	5.62	1.47	29.29	63.62	7681.00	. 56	2.00	
	38.14	38.96 101	RAW	.00	.00	19.20	1.19	26.10	53.51	6495.00	2 20	-1-00	
	38.14	38.96 101	WASH	1.60	78.00	11.64	1.35	27.80	59.21	7223.00	. 78	1.00	
	39.52	40.28 102	RAW	.00	00	22.20	1.15	24.22	52.43	6257.00	1.79	-1.00	
	39.52	40.28 102	WASH	1.60	72.00	12.63	1.42	26.83	59.12	7101.00	1.27	1.00	
	43.88	44.39 103	RAW	.00	.00	9.95	1.12	30.55	58.38	7414.00	1.67	-1.00	
	43.88	44.39 103	WASH	1.60	85.00	6.54	1.03	32.00	60.43	7728.00	1.53	2.50	
	62.76	64.68 104	RAW	. 00	.00	45.78	1.06	20.96	32.20	3993.00	. 93	~1.00	
	62.76	64.68 104	WASH	1.60	42.00	8.34	1.42	28.52	61.72	7481.00	. 82	1.00	,
	65.62	66.35 ~105	RAW	.00	.00	31.52	1.12	23,99	43.37	5232.00	. 57	-1.00	
	65.62	66.35 105	WASH	1.60	58.00	12.56	1.19	26.69	59.56	7065.00	. 58	1.00	
	67.74	68.00 ~ 106	RAW	.00	.00	35.68	.98	25.74	37.60	4623.00	.72	-1.00	
	67.74	68.00 106	WASH	1.60	45.00	21.03	1.30	25.60	52.07	6359.00	. 61	1.00	
	68.65	69.26 >107	RAW	.00	.00	19.93	1.13	25.41	53.53	6412.00	3.11	-1.00	
	68.65	69.26 107	WASH	1.60	77.00	11.60	1.18	25.99	71,67	7176.00	1.15	1.00	

TW820-	245											
SEAM	TOP	BOT SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI .
10	41.67	42.42 ~115	RAW	.00	.00	22.91	1.19	27.37	48.53	6160.00	3.22	-1.00
10	41.67	42.42 115	WASH	1.60	75.00	9.92	1.23	31.47	57.38	7367.00	2.18	1.50
10	49.72	50.73 116	RAW	.00	.00	13.97	. 95	32.72	52.36	7044.00	3.75	-1.00
10	49.72	50.73 116	WASH	1.60	76.00	6.90	1.22	34.87	57.01	7703.00	2.17	4.50
9	63.71	64.70 117	RAW	.00	.00	11.83	. 87	34.37	52.93	7267.00	2.24	-1.00
9 .	63.71	64.70 117	WASH	1.60	87.00	6.29	1.08	36.97	55.66	7790.00	1.69	7.00
3 wp	66.55	67.74 7118	RAW	, 00	.00	11.85	. 85	33.12	54.18	7239.00	2.07	-1.00
9 '-	00.55	67.74 < 118	WASH	1.60	84.00	6.92	1.23	35.21	56.64	7690.00	1.67	6.00
8	69.88	72.16 119	RAW	.00	.00	9.97	. 92	30.24	58.87	7331.00	2.11	-1.00
8	69.88	72.16 119	WASH	1.60	90.00	6.91	1.24	30.66	61,19	7642.00	1.47	1.00
8	76.64	78.99 120	RAW	.00	.00	15.14	. 74	28.83	55.29	6848.00	1.83	-1.00
8	76.64	78.99 120	WASH	1.60	80.00	7.28	1,13	29.56	62.03	7591.00	1.08	1.50
7	118.55	119.76 >121	RAW	.00	.00	16.86	.85	28.57	53.72	6774.00	2.58	-1.00
7	118.55	119.76 121	WASH	1.60	76.00	7.06	1.28	30.47	61.18	7675.00	1.76	3,50
5	125.51	125.78 -122	RAW	.00	.00	13.15	.73	30.13	_55.99	7142.00	1.59	-1.00
6	125.51	125.78 122	WASH	1.60	79.00	4.97	1.07	31.80	62.16	7868.00	1.25	2.00
6	125.11	128.32 -123	RAW	.00	.00	12.33	. 6 2	27.87	59.18	7115.00	. 69	-1.00
6	126.11	128.32 123	WASH	1.60	86.00	7.55	1.40	27.46	63.59	7537.00	. 66	1.00
3	149.60	149.95 7124	RAW	.00	.00	42.12	. 85	23.41	33.62	4530.00	2.31	-1.00
3	149.60	149.95 124	WASH	1.60	39.00	17.39	.84	29.97	51.80	6907.00	1.47	6.00
3	151.31	152.55 125	RAW	.00	.00	13.35	. 70	27.30	58.65	7072.00	. 95	-1.00
3	151.31	152.55 125	WASH	1.60	85.00	8.71	1.11	27.33	62.85	7545.00	. 79	1.00
3	153.39	154.29 ~126	RAW	.00	.00	37.11	.90	22.64	39.35	4906.00	2.24	-1.00
3	153.39	154.29 126	WASH	1.60	50.00	9.91	. 93	28.30	60.86	7453.00	1.09	1.00
2	157.55	158.03 -127	RAW	.00	. 00	29.98	. 65	27.30	42.07	5602.00	2.28	-1.00
2	157.55	158.03 _ 127	WASH	1.60	62.00	15.92	. 82	29.57	53.69	6987.00	1.73	2.50
2	158.36	162.74 -128	RAW		.00	28.29	1.02	26.31	44.38	5622.00	. 86	-1.00
2	158.36	162.74 128	WASH	1.60	60.QO	6.96	1.05	29.84	62.15	7671.00	. 68	2.50
2	163.41	163.99 ~ 129	RAW	.00	.00	37.71	.71	24.47	37.11	4691,00	. 98	-1.00
2	163.41	163.99 129	WASH	1.60	47.00	14.06	. 92	27.66	57.36	7020.00	. 62	2.00
2	165.32	165.72 >130	RAW	.00	. 00	63.46	. 75	19.76	16.03	2214.00	. 58	-1.00
2	165,32	165.72 130	WASH	1.60	13.00	21.49	1.08	29.12	48.31	6395.00	. 84	6.50
2	166.40	166.90 131	RAW	.00	.00	17.79	. 76	26.69	54.76	6719.00	1.37	-1.00
2	166.40	166.90 131	WASH	1.60	83.00	12.56	1.05	27.11	59.28	7157.00	1.03	1.00
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Printed on the Xenex 9700 8.P.S

W82D-: EAM	TOP		SAMPLE		SG	YIELD		RESMOIST	VOL	CARB	KCAL	SULF	FSI	
	79.24	82.22	~ 357	RAW	- 00	.00	18.04	. 72	25.74		6485.00	1.26	-1.00	
	79.24 88.63	82.22 91.67		WASH RAW	1.60 .00	75.00 .00	9.60 22.25	1.25 .63	25.57 27.53	63.58 49.59	7358.00 6038.00	1.10 1.21	1.00 -1.00	
	88.63	91.67	358	WASH	1.60	69.00	9.90	1.38	28.13	60.59	7311.00	1.32	2.50	
	94.68 94.68	96.75 96.75		RAW Wash	.00 1.60	.00 46.00	36.90 11.03	. 74 1.05	28.12 26.76		4539.00 7262.00	2.32 1.43	-1.00 2.50	
	101.58	102.10	360	RAW	. 00	- 00	35.93	. 86	19.62	43.59	5064.00	. 46	-1.00	
	101.68 105.20	102.10	360 361	WASH RAW	1.60	45.00	20.41 39.38	1.23 .71	22.94 23.78	55.42 36.42	6420.00 4413.00	, 54 . 68	1.50 -1.00	
	105.20	105.91		WASH	1.60	43.00	15.27	1.04	25.74		6958.00	.70	2.50	
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TW82D-	-247						•						
SEAM	TOP	BOT SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
10	115.16	115.80 204	RAW	- 00	.00	15.02	. 85	31.03	53.10	6952.00	2.50	-1.00	
10	115.16	115.80 204	WASH	1.60	86.00	10.03	1.07	30.75	58.15	7454.00	2.12	1.50	
9	120.55	121.56 205	RAW	. 00	. 00	13.48	1.00	32.33	53.19	7126.00	2.74	-1.00	
9	120.55	121.56 205	WASH	1.60	83.00	7.59	1.29	33.17	57.95	7633.00	1.79	5.00	
8	123.30	124.12 206	RAW	.00	.00	17.23	. 88	30.74	51.15	6494.00	1.95	-1.00	
8	123.30	124.12 206	WASH	1.60	73.00	5.91	1.34	30.38	62.37	7743.00	1.19	3.50	
7	145.04	146.31 207	RAW	.00	.00	18.89	. 87	27.45	52.79	6491.00	2.49	-1.00	
7	145.04	146.31 207	WASH	1.60	77.00	8.30	1.30	28.54	61.86	7484.00	1.39	2.50	
6	154.06	157.12 208	RAW	.00	.00	18.84	. 70	25.60	54.86	6469.00	. 68	-1.00	
6	154.06	157.12 208	WASH	1.60	81.00	7.72	1.24	27.72	63.32	7511.00	. 74	1.00	
Q	182.27	182.61 209	RAW	.00	- 00	20.84	. 75	24.31	54.10	6492.00	3.35	-1.00	
Q	182.27	182.61 209	WASH	1.60	79.00	11.53	1.20	25.21	62.06	7324.00	1.66	1.00	
3	191.25	191.84 ~210	RAW	.00	.00	38.84	. BQ	26.34	34.02	4541.00	5.50	-1.00	
3	191.25	191.84 210	WASH	1.60	37.00	14.65	1.09	27.85	56.41	7012.00	3.54	1.00	
3	193.29	194.20 211	RAW	.00	.00	21.15	.86	25.05	52.94	6339.00	. 76	-1.00	
3	193.29	194.20 211	WASH	1.60	75.00	10.39	1.10	26.61	61.90	7375.00	. 65	1.00	
3	194.98	196.53 7212	RAW	.00	.00	12.10	.82	27.16	59.92	7218.00	1.67	-1.00	
3	194.98	196.53 212	WASH	1.60	89.00	8.63	1.00	26.71	63.66	7539.00	1.03	1.00	
3	199.44	199.84 213	RAW	.00	.00	31.32	.58	30.23	36.87	4913.00	1.57	-1.00	
3	199.44	199.84 213	WASH	1.60	46.00	12.60	1.01	28.20	58.19	7238.00	1.31	1.00	
2	203.73	204.38 214	RAW	.00	.00	24.12	. 62	27.39	47.87	6135.00	. 92	-1.00	
2	203.73	204.38 214	WASH	1.60	78.00	14.82	. 94	28.74	55.50	7065.00	1.51	1.00	
2	204.78	206.43 215	RAW	.00	.00	19.84	. 78	27.75	51.63	6488.00	. 93	-1.00	
2	204.78	206.43 215	WASH	1.60	77.00	8.69	1.02	29.52	60.77	7562.00	.89	3.50	
2	207.94	208.36 216	RAW	.00	.00	33.52	.80	22.82	42.86	5173.00	. 40	-1.00	
2	207.94	208.36 216	WASH	1.60	56.00	14.49	1.01	26.40	58.10	6995.00	.40	1.50	
Q	211.80	212.10 217	RAW	.00	.00	35,19	. 85	21.43	42.53	4980.00	. 53	-1.00	
Ö	211.80	212.10 217	WASH	1.60	56.00	17.34	1.05	24.09	55.52	6784.00	.65	1.00	

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SEAM	TOP	BOT SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
10	151.95	152.45 311	RAW	.00	.00	29.77	1.53	25,24	43.46	5500.00	3.16	-1.00	ł
10	151.95	152,45 311	WASH	1.60	61.00	12.81	. 88	29.13	57.18	7098.00	2.01	1.00	i
9	156.74	157.66 \ 312	RAW	. 00	.00	16.40	.90	29.18	53.52	6904.00	5.79	-1.00	Į.
9	156.74	157.66 312	WASH	1.60	80.00	8.63	. 60	33.37	57.40	7612.00	2.21	4.00	
8	161.38	163.29 \313	RAW	.00	. 00	11.55	1.02	28.84	58.59	7232.00	1.84	-1.00	į
8	161.38	163.29 313	WASH	1.60	87.00	6.32	.71	29.95	63.02	7718.00	1.49	1.50	·
7	180.50	181.97 ~314	RAW	.00	.00	16.65	1.04	29.00	53.31	6745.00	2.07	-1.00	
7	180.50	181.97 314	WASH	1.60	78.00	8.52	. 57	30.96	59.95	7577.00	1.67	5.00	
6	189.94	192.20 >315	RAW	.00	.00	12.31	. 92	27.07	59.70	7108.00	. 64	-1.00	
6	189.94	192.20 315	WASH	1.60	86.00	7.17	1.53	27.83	63.47	7571.00	. 55	1.50	
6	192.91	193.84 ~316	RAW	.00	. 00	12.93	.91	27,75	58.41	7166.00	1.11	-1.00	
6	192.91	193.84 316	WASH	1.60	89.00	9.78	1.37	28.21	60.64	7421.00	1.03	2.00	
6	194.58	195.21 317	RAW	.00	.00	11.57	. 85	28.30	59.28	7239.00	1.22	-1.00	
6	194,58	195.21 317	WASH	1.60	53.00	5.10	1.34	28.80	64.76	7824.00	1.18	1.00	
3	212.78	214.83 \318	RAW	.00	.00	27.29	95	23.13	48.63	5806.00	1.47	-1,00	
3	212.78	214.83 318	WASH	1.60	72.00	10.28	1.56	26.17	61.99	7358.00	1.05	1.00	
2	220.13	221.17 \319	RAW	.00	.00	24.98	. 66	27.37	46.99	5961.00	1.90	-1.00	
2	220.13	221.17 319	WASH	1.60	70,00	12.86	1.12	28.56	57.46	7197.00	1.49	3.50	
2	228.91	229.55 - 320	RAW	.00	.00	43.52	.91	19.31	36.26	4348.00	.00	-1.00	
2	228.91	229.55 320	WASH	1.60	42.00	14.07	1.30	24.08	60.55	7041.00	1.13	1.00	
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TW82D-	250											
5EAM_	TOP	BOT SAMPLE	ATYP	\$G	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI
									~			
8	36.18	36. 5 6 336	RAW	.00	.00	11.25	1.22	26.38	61.15	7143.00	. 55	-1.00 > / ^/_
8	36.18	36.56 336	WASH	.00	-00	3.77	1.87	27.84	66.52	7776.00	.51	2.00) / D
7	52.42	52.88 > 177	RAW	.00	.00	30.51	1.00	29.53	38.96	4780.00	. 67	-1.00
7	52.42	52.88 177	WASH	1.60	50.00	9.36	1.14	27.33	62.17	7360.00	. 61	1.00
Į Q	69.62	70.02 🥆 178	RAW	.00	.00	44.56	. 96	21.09	33.39	4046.00	2.08	-1.00
Q	69.62	70.02 178	WASH	1.60	46.00	9.92	1.02	26.75	62.31	7359.00	1.74	2.50
6	74.43	76.30 `179	RAW	.00	.00	11.42	1.04	25.39	62.15	7093.00	. 50	-1.00
6	74.43	76.30 179	WASH	1.60	83.00	5.52	1.45	25.61	67.42	7653.00	. 50	2.00
5	83.96	86.15 ~180	RAW	.00	. 00	14.39	. 90	25.42	59.29	6888.00	. 39	-1.00
5	83.96	86.15 180	WASH	1,60	80.00	7.00	1.40	26.65	64.95	7549.00	. 56	1.50
_4	90.06	91.26 \181	RAW	.00	.00	14.82	. 95	24.90	59.33	6930.00	7.45	-1.00
4	90.06	91.26 181	WASH	1.60	74 00	4.98	1.17	27.77	66.08	7790.00	1.30	2.50
3	106.01	107.01 182	RAW	.00	.00	16.89	. 79	24.83	57.49	6779.00	1.37	-1.00
3	106.01	107.01 182	WASH	1.60	84.00	10.89	. 95	26.04	62.12	7326.00	. 86	1.00
3	107.35	107.90 183	RAW	.00	.00	16.89	. 76	25.36	56.99	6729.00	1.41	-1.00
3	107.35	107.90 183	WASH	1.60	83.00	10.56	. 77	25.47	63.20	7375.00	1.28	1.00
2	118.57	119.27 > 184	RAW	.00	.00	26.66	. 85	23.53	48.96	5929.00	2.86	-1-00
2	118.57	119.27 184	WASH	1.60	77.00	17.64	. 78	24.76	56.82	6772.00	2.65	1.00
2	120.37	120.68 ~185	RAW	.00	.00	33.71	.75	21.90	43.64	5200.00	. 51	~1.00
2	120.37	120.68 185	WASH	1.60	58.00	11.07	1.00	25.80	62.13	7294.00	. 61	2.50
2	121.90	122.36 →185A	RAW	-00	-00	40.27	. 65	27.15	31.93	4065.00	. 49	-1.00
] 2	121.90	122.36 185A	WASH	1.60	41.00	16.66	1.39	26.36	55.59	6757.00	. 74	2.00
Q	126.69	127.09 ~186	RAW	.00	.00	54.89	. 80	17.63	26.68	.00	. 33	.00

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SEAM	TOP	BOT SAMPL	E ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI
10	64.96	65,51 - 383	RAW	.00	- 00	24.28	. 84	29.15	45.73	5922.00	4.90	-1.00
0	64.96	65.51 383	WASH	1,60	63.00	8.70	. 85	30.62	59.83	8039.00	1.86	1.50
}	77.44	79.88 > 384	RAW	.00	.00	9.36	. 95	29.59	60.10	7438.00	3.04	-1.00
	77.44	79.88 384	WASH	1.60	89.00	5.24	. 90	29.90	63.96	7789.00	. 92	1.50
	100.60	101.68 >385	RAW	.00	.00	21.36	. 79	26.57	51.28	6326.00	2.36	-1.00
	100.60	101.68 385	WASH	1.60	74.00	8.97		29.10	61.16	7466.00	1.65	2.00
i	107.18	107.42 - 386	RAW	.00	.00	11.95	, 66	29.32	58.07	7299.00	3,84	-1.00
	~ 107 . 18	107.42 386>	WASH	1.60	82.00	5.24	.64	32.10	62.02	7866.00	1.70	4.00
	- 107.86	110.32 387	RAW	.00	.00	11.16	1.16	27.06	60.62	7179.00	.72	-1.00
	107.86	110.32 387		1.60	84.00	5.89	.91	28.13	65.07	7669.00	. 6 5	1.00
i	117.72	119.53 388	D RAW	.00	.00	11.59	1.02	27.91	59.48	7233.00	. 49	-1.00
·	117.72	119.53 388	WASH	1.60	86.00	5.32	.83	29.50	64.35	7785.00	. 51	2.00
	120.89	121.65 >389	RAW	.00	.00	14.38	.92	28.39	56.31	7060.00	1.87	-1.00
	120.89	121.65 389	WASH	1.60	84.00	6.46	. 77	31.16	61.61	7775.00	1.44	3.50
	121.65	121.84 390	RAW	, 00	.00	59.48	.77	17.43	22.32	2986.00	2.12	-1.00
	121.65	121.84 390	WASH	1.60	17.00	20.03	. 75	29.37	49.85	6564.00	1.97	5.00
	121.84	122.64 ~ 391	RAW	.00	.00	7.47	. 79	29.64	62.10	7657.00	1.28	-1.00
	121.84	122.64 391	WASH	1.60	93.00	5.03	. 58	31.43	62.96	7871.00	1.18	3.00
}	128.74	129,69 >392	RAW	.00	.00	20.83	.77	27.50	50.90	6251.00	2.15	-1.00
	128.74	129.69 392	WASH	1.60	67.00	10.53	.96	27.41	61.10	7378.00	1.30	1.00
	131.08	131.97 -393	RAW	.00	.00	42.03	. 79	22.44	34.74	4364.00	4.18	-1,00
	131.08	131.97 393	WASH	1.60	40.00	10.48	.82	28.03	60.67	7398.00	2.20	1.00
	134.12	135.80 ~ 394	RAW	.00	.00	40.21	. 55	23.10	36.14	4596.00	2.92	-1.00
1	134.12	135.80 394	WASH	1.60	47.00	15.08	. 84	29.06	55.02	7013.00	1.71	1.00
	267.65	269.36 -395	RAW	. 00	.00	16.79	.69	26.62	55.90	6806.00	. 66	-1.00
	267.65	269.36 395	WASH	1.60	81.00	10.66	. 53	27.08	61.73	7407.00	. 66	5.00
	275.61	277.88 - 396	RAW	.00	.00	23.39	.51	25.39	50.71	6267.00	1.59	-1.00
	275.61	277.88 396	WASH	1.60	68.00	10.84	. 41	28.77	59.98	7432.00	1.05	7.00
	280.04	280.84 - 397	RAW	.00	.00	19.73	.74	28.32	51.21	6466.00	. 32	-1.00
	280.04	280.84 397	WASH	1.60	77.00	11.25	. 52	28.49	59.74	7420.00	. 37	3.50
	284.75	285.40 398	RAW	.00	.00	56.39	. 70	17.51	25.40	3018.00	. 13	-1.00
	284.75	285,40 398	WASH	1.60	17.00	15.94	.56	25.87	57 63	6912.00	. 29	3.50

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TW820	0-252													
SEAM	TOP	BOT	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
9	106.19	106.88	155	RAW	.00	.00	18.55	1,11	24.49	55.85	6570.00	1.96	-1.00	
9	∼ 106 . 19	106.88	155	WASH	1.60	75.00	9.69	1.12	26.67	62.52	7427.00	1.77	2.00	
8	109.25	111.01	156	RAW	.00	.00	11.34	1.10	24.70	62.86	7208.00	1.21	-1.00	
8	~109.25	111.01	156	WASH	1.60	86.00	7.81	1.28	25.90	65.Q1	7544.00	1.11	1.50	
7	120.70	121.42	157	RAW	.00	.00	21.38	. 90	24.95	52.77	6301.00	5.24	-1.00	
7	120.70	121.42	157	WASH	1.60	66.00	7.29	1.28	26.21	65.22	7624.00	1.89	2.50	
6	126.08	127.47	158	RAW	.00	.00	12.79	1.02	25.66	60.53	7084,00	2.21	-1.00	
6	126.08	127.47	158	WASH	1.60	82.00	6.15	1.31	27.35	65.19	7678.00	1.29	2.50	
5	~~ 134.08	135.62	159	RAW	.00	.00	16.71	. 88	25.40	57.01	6580.00	. 48	-1.00	
5	134.08	135.62	159	WASH	1.60	81.00	9.09	1.58	24.98	64.35	7346.00	. 50	1.50	
, 3 —	155.80	156.14	160	RAW	.00	.00	73.98	1.01	11.05	13.96	1345.00	. 19	-1.00	
2	1 66, 12	166.73	161	RAW	.00	- 00	39.37	. 65	20.88	39.10	7498.00	1.96	-1.00	
2	166.12	166.73	161	WASH	1.60	39.00	15.47	.88	23.62	60.03	6930.00	1.04	1.00	
1	341.60	342.20	162	RAW	.00	.00	62.07	. 58	15.43	21.92	2368.00	. 15	-1.00	
1	346,12	346.48	163	RAW	. 00	.00	38.32	.61	20.00	41.17	4759.00	.26	-1.00	
1	346.12	34 6 .48	163	WASH	1.60	40.00	23.40	. 38	20.14	56.08	6426.00	. 32	1.50	
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and on the Xarox 9700 E.P.S

SEAM	TOP	BOT SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KÇAL	SULF	FSI
									CARD	NUAL	30LF	
,	36.83	37.86 224	RAW	.00	.00	15.21	. 70	28.29	55.80	6876.00	2.86	-1.00
c	36.83	37.86 \224	WASH	1.60	79.00	9.52	1.09	28.15	61.24	7450.00	1.45	2.00
Q	51.20	51.58 ~225	RAW	.00	.00	30.58	.80	23.57	45.05	5429.00	2.63	-1.00
)	51,20	51.58 225	WASH	1.60	58.00	16.98	1.11	24.60	57.31	6755.00	1.11	1,00
)	54.12	54.57 > 226	RAW	.00	.00	37.35	1,00	23.92	37.73	4788.00	1.56	-1.00
)	54.12	54.57 \226	WASH	1.60	47.00	18.24	. 96	28.41	52.39	6673.00	1.67	5.50
))	55.45	55.79 - 228	RAW	.00	.00	57.43	.54	18.86	23.17	2845.00	.39	-1.00
)	55.45	55.79 228	WASH	1.60	26.00	17.48	, 95	27.58	53.99	6676.00	. 96	5.50
)	73.65	73.99 229	RAW	.00	.00	32.70	.89	22.36	44.05	5210.00	1.72	-1,00
)	73.65	73.99 229	WASH	1.60	51.00	17.98	1.03	23.40	57.59	6624.00	1.05	1.00
)	77.46	77.88 230	RAW	.00	.00	37.06	, 98	22.68	39.28	4734.00	6.18	-1,00
)	77.46	77.88 230	WASH	1.60	44.00	12.80	1.30	25.43	60.47	7090.00	2.23	1.00
0	213.72	214.46 233	RAW	.00	- 00	26.31	.73	22.41	50.55	6027.00	2.96	-1.00
Ю	213.72	214.46 233	WASH	1.60	74.00	18 - 10	. 89	24.02	56.99	6788.00	1.96	1.50
<u> </u>	227,91	229.91 ~231	RAW	- 00	.00	16.17	1.07	23.01	59.75	6787.00	2.55	-1.00
3	227.91	229.91 7 231	WASH	1.60	79.00	8.81	, 99	25.03	65.17	7478.00	1.20	1.50
7	248.07	249.34 234	RAW	.00	.00	18.96	.80	22.30	57.94	6598.00	1.69	-1.00
,	248.07	249.34 234	WASH	1.60	78.00	7.56	.79	24.69	66.96	7663.00	1.68	3.00
<u> </u>	256.46	260.42 235	RAW	. 00	- 00	9.93	.84	23.23	66.00	7399.00	. 65	-1.00
3	256.46	260.42 235	WASH	1.60	89,00	5.15	1.49	24.53	68.83	7797.00	. 59	1.50
)	269.60	269.96 236	RAW	.00	.00	10.35	. 71	22.64	66.30	7418.00	2.15	-1.00
)	269.60	269.96 - 236	WASH	1.60	88.00	6.08	1.06	23.27	69.59	7783.00	1.42	1.00
5	278.20	280.02 > 238	RAW	.00	.00	18.89	.87	22.09	58.15	6603.00	1.29	-1.00
5	278.20	280.02 238	WASH	1.60	81.00	10.60	1.55	22.83	65.02	7338.00	. 73	1,50
4	283.37	285.13 -237	RAW	.00	.00	31.45	.72	20.68	47.15	5468.00	2.45	-1.00
4	283.37	285.13 * 237	WASH	1.60	62.00	15.47	1.22	23.37	59.94	7008.00	1.55	2.00
<u> </u>	286.72	287 . 11 > 239	RAW	.00	00	49.56	. 70	18.08	31.66	3740.00	1.31	-1,00
)	286.72	287.11 239	WASH	1.60	29.00	16.18	1.02	23.45	59.35	6956.00	1.06	2.00
3	299.74	301.97 - 240	RAW	.00	.00	24.15	.79	22.49	52.57	6175.00	. 99	-1.00
3	299.74	301.97 ~240	WASH	1.60	70.00	10,30	. 98	24.38	64.34	7505.00	1.72	1.50
<u>2</u>	306.64	308.38 -241	RAW	.00		24.77	. 77	23.33	51.13	6086.00	1.68	-1.00
2	306.64	308.38 ~241	WA5H	1.60	73.00	13.25	. 80	25.55	60.40	7252.00	1.52	3.00

SEAM	TOP	BOT	SAMPLE	ATYP	5G	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
10	137.44	137.94	242	RAW	.00	.00	23.10	1.60	25.47	49.83	6016.00	2.51	-1.00	
10	137.44	137.94		WASH	1.60	69.00	13,79	1,42	27.19	57.60	6929.00	1,23	1.50	
<u> </u>	151.00	153.30		RAW	.00	.00	24.14	1.26	25.94	48.66	5874.00	.23	-1.00	
В	151.00	153.30	243	WASH	1.60	65.00	12.79	1.29	28.03	57.89	7010.00	1.18	1.50	·
Ç	156.24	156.74	~244	RAW	.00	.00	43.19	1.13	18.86	36.82	4348.00	.84	-1.00	
Q	156.24	156.74	-244	WASH	1.60	47.00	20.34	1,19	24.51	53.96	6369.00	. 85	1.50	
6	175.80	176.42	~245	RAW	.00	.00	13.05	. 92	30.65	55.38	7016.00	1.51	-1.00	
6	175.80	176.42	245	WASH	1.60	90.00	8.99	1.00	30.83	59.18	7417.00	1.37	1.50	
5	177.64	178.08		RAW	.00	.00	39.65	. 70	22.50	37.15	4585.00	1.80	-1.00	
5	177.64	178.08		WASH	1.60	50.00	18.60	1.16	26.80	53,44	6528.00	1.19	1.00	
6 .	179.80	180.51		RAW	.00	.00	30.54	.82	26.29	42.35	5316.00	3.67	-1.00	
6	179.80	180.51		WASH	1.60	50.00	12.62	1.05	27.36	58.97	7071.00	1.45	1.00	
6	181.76	182.90		RAW	.00	.00	17.73	. 85	25.64	55.78	6581.00	. 56	-1.00	
5	181.76	182.90		WASH	1.60	80.00	9.05	1.39	26.75	62.81	7335.00	. 56	2.00	
2	199.90	200.68		RAW	.00	. 00	22.43	. 92	25.48	51.17	6201.00	1.79	-1.00	
2	199.90	200.68	249	WASH	1.60	79.00	15.69	. 99	26.56	56.76	6855,00	1.65	1.00	

SEAM	TOP	BOT SAMPLE	ATYP	SG	YIELD	A SH	RESMOIST	val.	CARB	KCAL	SULF	FSI	
													· · · · · · · · · · · · · · · · · · ·
7	107.35	108.56~ 187	RAW	.00	.00	14.21	.80	28.01	56.98	7027.00	2.31	-1.00	
7	107.35	108.56 ~ 187	WASH	1.60	86.00	8.10	1.07	29.71	61,12	7552.00	1.33	3.00	
6	114.27	115.21 ~188	RAW	.00	. 00	29.11	.64	23.51	45.74	5697.00	3.90	-1.00	
6	114.27	115.21 \ 188	WASH	1.60	70.00	5.21	1.17	29.65	63.97	7807.00	. 92	1.50	
5	120.61	121.44 189	RAW	.00	.00	27.22	. 89	23.13	48.76	5820.00	.76	-1.00	
5	120.61	121.44 ~ 189	WASH	1.60	67.00	12.97	1.10	26.70	59.23	7106.00	. 45	1.00	
4	123.69	124.88 >190	RAW	.00	.00	9.92	.86	30.35	58.87	7478.00	. 97	-1.00	
4	123.69	124.88 ~190	WASH	1.60	89.00	5.90	1.05	30.62	62.43	7805.00	.86	2.50	·
Q	127.14	127.49 ~191	RAW	.00	.00	53.57	. 54	20.60	25.29	3353,00	1.45	-1.00	
0	127.14	127.49 🦰 191	WASH	1.60	21.00	21.61	1.02	27.06	50.31	6384.00	1.44	1.00	
3	131.42	131.96 🔭 192	RAW	.00	- 00	35.58	. 50	25.62	38.30	5091.00	3.20	-1.00	
3	131.42	131.96 ~ 192	WASH	1.60	49.00	17.12	. 75	27.86	54.27	6838.00	1.81	1.50	
3	137.64	139.41 🕶 193	RAW	.00	.00	22.55	. 58	26.88	49.99	6136.00	. 84	-1.00	
3	137.64	139.41 > 193	WASH	1.60	79.00	10.41	.87	28.76	59.96	7365.00	. 73	3.00	
3	139.76	140.48 - 194	RAW	.00	.00	29.25	.83	23.51	46.41	5612,00	.58	-1.00	
3	139.76	140.48 ~ 194	WASH	1.60	67.00	13.79	. 95	26.35	58.91	7034.00	.64	1.50	
2	140.85	141.20 ~ 195	RAW	.00	.00	29.66	. 79	25.12	44.43	5475.00	.7 7	-1.00	
2	140.85	141.20 🕶 195	WASH	1.60	65.00	18.28	. 84	26.09	54.79	6587.00	. 65	2.00	
2	142.08	142.52 ~196	RAW	.00	.00	16.06	. 67	26.64	56,63	6825.00	1.12	-1-00	
2	142.08	142.52 ~196	WASH	1.60	88.00	11.90	.83	26.33	60.94	7232.00	. 95	i.00	

8 157.61 160.51 197 RAW .00 .00 32.87 1.13 19.84 46.16 5274.00 .34 1.50 157.61 160.51 197 WASH 1.60 78.00 16.57 1.50 22.48 59.45 6696.00 .41 1.50 150 202.58 203.92 198 RAW .00 .00 37.82 1.05 19.32 41.81 4699.00 60 1.50 150 202.58 203.92 198 WASH 1.60 53.00 10.95 1.79 23.36 63.90 7165.00 .59 2.00 150 206.68 207.00 199 RAW .00 .00 30.59 1.07 21.31 47.03 5452.00 .52 1.50 150 206.68 207.00 199 WASH 1.60 68.00 17.95 1.43 23.58 57.04 6577.00 .42 1.50 150 206.68 207.00 199 WASH 1.60 68.00 17.95 1.43 23.58 57.04 6577.00 .42 1.50 150 206.68 207.00 199 WASH 1.60 68.00 17.95 1.43 23.58 57.04 6577.00 .42 1.50 150 206.68 207.00 150 200 RAW .00 .00 32.87 1.13 19.94 46.16 5274.00 .34 1.50 150 20.76 211.29 200 RAW .00 .00 32.87 1.13 19.94 46.16 5274.00 .34 1.50 150 20.76 211.29 200 WASH 1.60 64.00 16.57 1.50 22.48 59.45 6696.00 .41 1.50 150 20.46 211.69 212.08 201 RAW .00 .00 34.14 1.07 20.46 44.33 5113.00 .40 2.00 150 20.46 211.69 212.08 201 RAW .00 .00 34.14 1.07 20.46 44.33 5113.00 .40 2.00 150 20.46 210.76 211.29 200 RAW .00 .00 .00 34.14 1.07 20.46 44.33 5113.00 .40 2.00 2.00 20.6		₽ŞI			CARB	VOL	RESMOIST	ASH	YIELD	SG	ATYP	SAMPLE	BOT	TOP	SEAM
8 157.61 160.51 197 RAW .OO .OO 32.87 1.13 19.84 46.16 5274.0O .34 1.50 157.61 160.51 197 WASH 1.60 78.0O 16.57 1.50 22.48 59.45 6696.0O .41 1.50 150 202.58 203.92 198 RAW .OO .OO 37.82 1.05 19.32 41.81 4699.0O - 6O 1.50 150 202.58 203.92 198 WASH 1.60 53.0O 10.95 1.79 23.36 63.90 7165.0O .59 2.0O 206.68 207.0O 199 RAW .OO .OO 30.59 1.07 21.31 47.03 5452.0O .52 1.50 206.68 207.0O 199 WASH 1.60 68.0O 17.95 1.43 23.58 57.04 6577.0O .42 1.50 150 210.76 211.29 200 RAW .OO .OO 32.87 1.13 19.94 46.16 5274.0O .34 1.50 150 210.76 211.29 200 WASH 1.60 64.0O 16.57 1.50 22.48 59.45 6696.0O .41 1.50 150 211.69 212.08 201 RAW .OO .OO 34.14 1.07 20.46 44.33 5113.0O .40 2.00 150 211.69 212.08 201 RAW .OO .OO 34.14 1.07 20.46 44.33 5113.0O .40 2.00 150 211.69 212.08 201 RAW .OO .OO 34.14 1.07 20.46 44.33 5113.0O .40 2.00 150 211.69 212.08 201 RAW .OO .OO 34.14 1.07 20.46 44.33 5113.0O .40 2.00 150 211.69 212.08 201 RAW .OO .OO .OO 34.14 1.07 20.46 44.33 5113.0O .40 2.00 150 211.69 212.08 201 RAW .OO .OO .OO .OO .OO .OO .OO .OO .OO .O				KCAL		·····-	KESMOISI			· · · · · · · · · · · · · · · · · · ·					
8							1 12				DAW	197	160 51	157 61	r a
6 202.58 203.92 198 RAW .00 .00 37.82 1.05 19.32 41.81 4699.00 - 60 1.50 6 202.58 203.92 198 WASH 1.60 53.00 10.95 1.79 23.36 63.90 7165.00 .59 2.00 206.68 207.00 199 RAW .00 .00 30.59 1.07 21.31 47.03 5452.00 .52 1.50 206.68 207.00 199 WASH 1.60 68.00 17.95 1.43 23.58 57.04 6577.00 .42 1.50 70 210.76 211.29 200 RAW .00 .00 32.87 1.13 19.94 46.16 5274.00 .34 1.50 9 210.76 211.29 200 WASH 1.60 64.00 16.57 1.50 22.48 59.45 6696.00 .41 1.50 5 211.69 212.08 201 RAW .00 .00 34.14 1.07 20.46 44.33 5113.00 .40 2.00															
6 202.58 203.92 198 WASH 1.60 53.00 10.95 1.79 23.36 63.90 7165.00 .59 2.00 70 206.68 207.00 199 RAW .00 .00 30.59 1.07 21.31 47.03 5452.00 .52 1.50 70 206.68 207.00 199 WASH 1.60 68.00 17.95 1.43 23.58 57.04 6577.00 .42 1.50 70 7210.76 211.29 200 RAW .00 .00 32.87 1.13 19.94 46.16 5274.00 .34 1.50 70 210.76 211.29 200 WASH 1.60 64.00 16.57 1.50 22.48 59.45 6696.00 .41 1.50 70 211.69 212.08 201 RAW .00 .00 34.14 1.07 20.46 44.33 5113.00 .40 2.00															
7Q 206.68 207.00 199 RAW .00 .00 30.59 1.07 21.31 47.03 5452.00 .52 1.50 7Q 206.68 207.00 199 WASH 1.60 68.00 17.95 1.43 23.58 57.04 6577.00 .42 1.50 7Q -210.76 211.29 200 RAW .00 .00 32.87 1.13 19.94 46.16 5274.00 .34 1.50 Q 210.76 211.29 200 WASH 1.60 64.00 16.57 1.50 22.48 59.45 6696.00 .41 1.50 -5 211.69 212.08 201 RAW .00 .00 34.14 1.07 20.46 44.33 5113.00 .40 2.00															-
**O 206.68 207.00 199 WASH 1.60 68.00 17.95 1.43 23.58 57.04 6577.00 .42 1.50 **O **210.76 211.29 200 RAW .00 .00 32.87 1.13 19.94 46.16 5274.00 .34 1.50 **O 210.76 211.29 200 WASH 1.60 64.00 16.57 1.50 22.48 59.45 6696.00 .41 1.50 **5 211.69 212.08 201 RAW .00 .00 34.14 1.07 20.46 44.33 5113.00 .40 2.00								_							. ^
7Q 7210.76 211.29 200 RAW .00 .00 32.87 1.13 19.94 46.16 5274.00 .34 1.50 210.76 211.29 200 WASH 1.60 64.00 16.57 1.50 22.48 59.45 6696.00 .41 1.50 5 211.69 212.08 201 RAW .00 .00 34.14 1.07 20.46 44.33 5113.00 .40 2.00	50 [* *]	1.50	. 52	5452.00	47.03	21.31	1.07		.00						Ų
Q 210.76 211.29 200 WASH 1.60 64.00 16.57 1.50 22.48 59.45 6696.00 .41 1.50 211.69 212.08 201 RAW .00 .00 34.14 1.07 20.46 44.33 5113.00 .40 2.00	50 ' /	1.50	.42	6577.00	57.04	23.58	1.43	17.95	68.00	1.60	WASH	199	207.00	206.68	~ 0
Q 210.76 211.29 200 WASH 1.60 64.00 16.57 1.50 22.48 59.45 6696.00 .41 1.50 211.69 212.08 201 RAW .00 .00 34.14 1.07 20.46 44.33 5113.00 .40 2.00	The state of the s	1.50	. 34	5274.00	46.16	19.94	1.13	32.87	.00	.00	RAW	200	211.29	-210.76	•Q
►5 211.69 212.08 201 RAW .00 .00 34.14 1.07 20.46 44.33 5113.00 .40 2.00		1.50	. 4 1	6696.00	59.45	22.48	1.50	16.57	64.00	1.60	WASH	200	211.29	210.76	Q
		2.00			44.33		1.07	34.14	.00	.00	RAW	201	212.08	211.69	- 5
5 211.69 212.08 201 WASH 1.60 62.00 14.16 1.40 23.98 60.64 6914.00 .53 2.00		2.00					1.40	14.16	62.00	1.60	WASH	201	212.08	211.69	5
No. 10 01 01 00 00 00 00 00 00 00 00 00 00		2.00						24.70	.00	.00	RAW	202	217.57	217,21	~ 5
	· · · · · · · · · · · · · · · · · · ·	2.00				 .					WASH	202	217.57	217.21	-5
D		2.00									_	-			~2
000 000		2.50										_		257.74	2
2.50	30	2.50	0.10	1000.00	01.01	£1.55									

SEAM	TOP	вот	SAMPLE	ATYP	5G	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
		,					~							
8	44.80	47.44	` 337	RAW	- 00	.00	10.32	1.19	28.74	59.75	7356.00	. 91	-1.00	
8	44.80	47.44		WASH	1.60	95.00	8.63	1.28	29.36	60.73	7479.00	. 83	1.50	
8	49.48	52.00		RAW	.00	.00	18.71	1.15	25.30	54.84	6580.00	1.67	-1.00	
8	49.48	52.00		WASH	1.60	85.00	11.73	1.31	27.28	59.68	7188.00	.97	1.00	
7	57.51	58.99		RAW	.00	.00	34.04	1.08	24.77	40.11	5069.00	4.00	-1.00	
7	57.51	58.99		WASH	1.60	61.00	12.12	. 94	30.71	56.23	7187.00	1.29	f . QO	
7	59.66	60.19		RAW	.00	.00	30.30	. 98	21,48	47.24	5574.00	.72	-1.00	
7	59.66	60.19		WASH	1.60	62.00	13.53	1.20	25.48	59.79	7020.00	.63	1.00	
Q	61.23	61.53		RAW	.00	.00	27.19	1.00	21.70	50.11	5770.00	. 37	-1.00	
Q	61.23	61.53	341	WASH	1.60	72.00	22.34	1.61	22.54	53.51	6184.00	. 40	1.00	
Q	62.43	63.07	342	RAW	.00	.00	47.19	. 75	23.21	28.85	.00	. 37	-1.00	
6	65.16	67.37 67.37	_ 343	RAW	.00	.00	36.05	. 85	24.79	38.31	5009.00	1.44	-1.00	-
6	65.1 6	67.37	343	WASH	1.60	60.00	11.53	1.71	30.22	56.54	7228.00	1,88	2.50	
6	68.41	68.75		RAW	.00	.00	34.91	. 79	22.09	42,21	5036.00	.51	-1.00	
6	68,41	68.75	_344	WASH	1.60	53.00	13.97	1.38	25.01	59.64	6970.00	.72	1.00	
4	70.49	71.25 71.25 81.48	_ 345	RAW	.00	.00	32.12	. 90	23.53	43.45	5414.00	1.06	-1.00	
4	70.49	71.25	_ 345	WASH	1.60	61.00	14.27	1.11	28.18	56.44	7016.00	. 9Q	1.00	
3	81.05	81.48	~ 346	RAW	.00	.00	19.70	1.10	26.43	52.77	6564.00	1.35	-1.00	
3	81.05	81.48	346	WASH	1.60	73.00	10.35	1.26	28.83	59.5 6	7349,00	1.12	1.00	
3	83.17	83.81	347	RAW	. 00	.00	18.18	1.11	23.76	56.95	6538.00	. 46	-1.00	
3	83.17	83.81 96.13	<u>.</u> 347	WASH	1.60	78.00	11.93	1.53	25.18	61.36	7062.00	. 39	1.00	
2	95.32	96.13	ຼ 348	RAW	.00	.00	19.65	. 98	32.92	46.45	5920.00	. 39	-1.00	
2	95.32	96.13		WASH	1.60	61.00	8.28	1.31	29.35	61.06	7439.00	. 46	1.50	
2	96.98	98.06		RAW	. 00	00	23.41	. 88	25.01	50.70	6069.00	. 44	-1.00	
2	96.98	98.06		WASH	1.60	75.00	8.29	1.29	26.92	63.50	7028.00	. 44	2.00	
2	98.70	99.15		RAW	.00	.00	18.46	. 73	28.13	52.65	6443.00	.82	-1.00	
2	98.70	99.15	350	WASH	1.60	80.00	8.54	1.26	27.40	62.80	7129.00	. 86	1.00	

EAM	TOP	BOT	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FS1
	21.04	21.36	327	RAW	.00	. 00	23.86	. 92	31.32	43.90	5547.00	. 48	-1.00
	21.04	21.36	`327	WASH	1.60	62.00	11.85	1.22	30.21	56.72	7112.00	. 56	4.50
	22.65	24.66		RAW	.00	, 00	13.89	1.23	26.63	58.25	6899.00	. 37	-1.00
	22.65	24.66		WASH	1.60	85.00	9.06	1.48	26.83	62.63	7374.00	.37	1.50
	116.46	116.80	` 329	RAW	.00	.00	29.78	. 57	32.57	37.08	5269.00	3.77	-1.00
	116.46	116.80	`329	WASH	1.60	46.00	12.07	1.01	31.85	55.07	7330.00	1,11	7.00
	117.02	119.46	, 330	RAW	. 00	.00	23.71	. 72	27.39	48.18	6170.00	2.30	-1.00
	117.02	119.46	-330	WASH	1.60	70.00	11.25	. 98	30.46	57.31	7437.00	. 83	3.50
	119.90	121.01		RAW	.00	.00	23.76	. 82	27.06	48.36	6159.00	.32	-1.00
	119.90	121.01	` 331	WASH	1.60	66.00	11.70	. 93	30.40	56.97	7376.00	. 33	6.00
	125.95	126.68	<u>~</u> 332	RAW	.00	.00	30.94	.74	25.12	43.17	5387.00	. 27	-1.00
	125.95	126.68	332	WASH	1.60	57.00	17.60	. 95	27.38	54.07	6792.00	.32	3.50

PAGE 56 TW82D-261 FSI ASH RESMOIST VOL CARB KÇAL **ŞULF** SEAM TOP BOT SAMPLE ATYP YIELD .00 22.97 . 44 1.00 134.01 134.37 446 RAW .00 35.92 . 94 40.17 4782.00 1.50 134.01 134.37 446 WASH 1.60 50.00 12.51 1.32 26.43 59.74 7017.00 . 58 . 49 Q RAW .00 .00 37.90 1.02 21.34 39.74 4684.00 2.00 134.64 134.96 447

PAGE	57													
TW82D	-262			_										
SEAM	TOP	BOT SAMPLE		<u> </u>	YIELD	ASH 	RESMOIST	VOL	CARB	KCAL	SULF	FSI		
f: "	D _{67.60}	72.80 333 72.80 333 75.85 334 75.85 334 80.46 335 80.46 335	RAW Wash	.00 1.70	.00 93 23	13.89 9.99	1.07 3.84	.00 29.37	.00 56.80	.00 7161.00	1.48 1.04	.00 .00		
1	74.0 9	75.85 334	RAW	. 00	.00	35.90	.82	24.55	38.73	4938.00	. 54	-1.00		
0	74.09 79.80	80.46 335	WASH RAW	.00	50,00 .00	11.44 37.71	.98 .53	29.64 24.29	57.94 34.47	7300.00 4616.00	. 54 . 26	5.50 -1.00		
Q	79.80	80.46 335	WASH	1.60	49.00	20.75	. 95	26.53		6425.00	. 34	1.50	•	
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TV SE	MGE 58 M82D-264 AM TOP 34.51 36.24 36.24 185.12 187.25 187.54 192.46	80T 35.34 37.16 37.16 187.25 187.25 187.54 187.82 193.38 193.38	SAMPLE 450 451 451 452 452 453 454 454 455 455	ATYP RAW WASH RAW WASH RAW WASH RAW WASH RAW WASH	SG .00 1.60 .00 1.60 .00 1.60 .00 1.60 .00	YIELD 	ASH 21.24 11.98 19.53 8.83 35.01 12.55 72.80 33.78 14.40 42.71 20.54	RESMOIST	VOL 27.40 28.14 26.06 -28.56 24.13 28.79 15.09 29.84 30.70 19.80 23.83	6200.00 7104.00 6457.00 7419.00 4985.00 7220.00 1458.00 6749.00 4314.00 6420.00	SULF .44 .46 1.19 .79 2.84 .84 1.64 1.25 1.09 .30	FSI 1.00 1.00 1.00 2.50 3.50 .00 3.50 5.50 1.00 1.00	
9700 g.P.S										 			

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EAM_	TOP	BOT	SAMPLE		SG	YIELD	ASH		VOL	CARB	KCAL	SULF	FSI		
- - -	60.93	61,60	437	RAW	.00	.00	48.71	.93	21.24	29.12	3727.00	5.12	1.00		
	60.93	61.60	437	WASH	1.60	12.00	20.10	.1.06	29.10	49.73	6437.00	4.43	5.50		
	63.09	63.35	438	RAW	.00	.00	19.56	1.00	28.26	51.18	51.00	1.67	2.50		
	63.09	63.35	438	WASH	1.60	76.00	8.66	1.13	30.38	59.83	751.00	1.39	3.00		
	94.57	95.04	439	RAW	.00	.00	17.66	1.01	26.01	55.32	6553.QO	. 76	1.00		
	94.57	95.04	439	WASH	1.60	77.00	11.20	1.28	26.15	61.37	7269.00	. 53	1.00		
	<u> </u>	97.37	440	RAW	,00	.00	26.10	. 99	25.25	47.66	5898.00	3.16	1.00		
	96.85 98.88	97.37 100.26	440 441	WASH	1.60	71.00	11.20	1.19	28.26	59.35	7266.00	1.51	1.00		
	98.88	100.26	441	RAW Wash	-00 1.60	.00 66.00	26.67 10.85	1.07 1.19	22.83 25.70	49.43 62.26	5815.00 7294.00	5.25 2.87	1.00		
	263.12	263.94	442	RAW	.00	.00	16.84	.97	23.46	58.73	6848.00	1.12	1.00		
	~263.12	263.94	442	WASH	1.60	66.00	9.91	1.07	24.33		7467.00	1.09	1.50	-	
	> 264.30	266.56	443	RAW	.00	.00	25.99	.97	23.64	49.40	5921.00	3.29	2.00		
,	264.30	266.56	443	WASH	1.60	58.00	12.22	1.15	25.61	61.02	7231.00	1.60	3.QO		
	267.10	270.72	444	RAW	- 00	- 00	31.56	. 96	22.73	44.75	5387.00	1.55	1.00		
	~267.10	270.72	444	WASH	1.60	52.00	20.75	1.26	24.75	53.24	6345.00	1.01	3.00		
	~ 275.33	275.80	445	RAW	.00	.00	35.92	. 93	21.50			. 48	. 50		
`	275.33	275.80	445	WASH	1.60	59.00	21.73	1.38	22,95	53.94	6219.00	. 57	1.50		
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TW82D- Seam	· 26 / TOP	вот	SAMPLE	ATYP	SG	YIEŁD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
SEAM 	10P	BO !	SAMPLE	ALTE		LIELD	A 3 FT	KESMUIS!	VOL	CAKO	NCAL .	20 L		
)	40.31	41.44	361	RAW	.00	.00	29.35	1.15	21.46	48.04	5491.00	. 48	-1.00	
j	40.31		`361	WASH	1.60	62.00	8.97	1.51	24.97	64.55	7425.00	.66	1.50	
Ó	59.62	60.35	362	RAW	.00	.00	21.63	.92	'24.62	52.83	6322.00	4.10	-1.00	
7	59.62	60.35		WASH	1.60	72.00	10.98	1.03	25.80	62.19	7327.00	3.20	2.00	
)	66.20	67.26	^ 363	RAW	.00	.00	15.34	. 76	26.54	57.36	6973.00	2.30	-1.00	
o)	66.20	67.26		WASH	1.60	45.00	9.14	1.09	27.75	62.02	7524.00	2.00	4.50	
Ò	78.14	79.04	364	RAW	.00	.00	21.26	. 8 1	24.34	53.59	6332.00	5.79	-1.00	
o -	78.14	79.04	364	WĂSH	1.6Ö	75.00	9.61	1.15	24.77	64,47	7397.00	2.90	1.50	
10	81.46	82.65	` 365	RAW	.00	.00	27.24	. 83	23.44	48.49	5724.00	3.78	-1.00	
10	81.46	82.65	> 365	WASH	1.60	62.00	10.25	1.30	25.32	63.13	7285.00	2.69	2.50	
9	88.37	89.01	366	RAW	.00	.00	25.74	.80	23.57	49.89	5925.00	7.31	-1.00	
9	88.37	89.01	366	WASH	1.60	59.00	10.69	1,10	25.71	62.50	7276.00	3.07	2.50	
8	94.68	98.30	367	RAW	.00	.00	17.22	. 93	22.52	59.33	6651.00	1.41	-1.00	
8	94.68	98.30	` 367	WASH	1.60	81.00	10.12	1.93	23.22	64.73	7216.00	1.21	1.00	
7	120.40	120.92	7368	RAW	.00	.00	20.26	. 86	23.58	55.30	6406.00	3.62	-1.00	
7	120.40	120.92	- 368	WASH	1.60	75.00	9.08	1.34	24.28	65.30	7378.00	2.69	1.50	
6U	126.54	128.60	~369 .	RAW	.00	.00	18.84	.96	24.02	56.18	6486.00	. 92	-1.00	
6U	126.54	128.60	-369	WASH	1.60	80.00	7.25	1.45	25,24	66.06	7509.00	. 98	2.00	
6L	130.80	136.57	~370	RAW	. 00	.00	13.40	1.36	23.80	61.44	6920.00	. 46	-1.00	
6L	130.80	136.57	-370	WASH	1.60	87.00	6.84	1.82	24.46	66.88	7528.00	. 4 1	1.00	
3	141.38	142.32	¬ 371	RAW	.00	.00	9.35	.87	23.80	65.98	7478.00	1.05	-1.00	
3	141.38	142.32	~ 371	WASH	1.60	93.00	7.25	1.67	24.02	77.06	7579.00	.80	1.50	
3	143.04	143.74		RAW	. 00	.00	32.12	. 73	20.79	46.36	5327.00	1.41	-1.00	
3	143.04	143.74	-	WASH	1.60	53.00	13.21	1.34	22.24	63.21	7008.00	1.31	1.00	
3	144.32	144.68		RAW	.00	.00	27.43	.61	25.19	46.77	5598.00	1.57	-1.00	
3	144.32	144.68		WASH	1.60	63.00	15.92	. 95	24.00	59.13	6825.00	1.06	2.50	
3	145.19	145.49		RAW	.00	.00	24.47	.73	23.25	51.55	5902.00	1.87	-1.00	
3	145.19	145.49		WASH	1.60	66.00	14.16	1.13	21.39	63.32	6998.00	1.26	1.00	
3	146,37	146.68		RAW	- 00	00	44.08	. 54	24.57	30.81	3815.00	1.43	-1.00	
3	146.37	146.68		WASH	1.60	29.00	14.38	1.41	26.08	58.13	6956.00	2.04	4.50	
2	150,67	152.77		RAW	- 00	- 00	24.60		23.00	51.61	5965.00	3.22	~1,00	
2	150.67	152.77		WASH	1.60	70.00	11.77	1.56	23.58	63.09	7196.00	1.48	1.50	
2	154.56	155.81	` 977	RAW	.00	.00	11.26	1.35	23.53	63.85	7199.00	. 48	-1.00	
2	154.5 6	155.81	377	WASH	1.60	93.00	9.07	1.76	23.96	65.21	7370.00	.39	1.50	

0.000

PAGE 62

TW82D-	-268												
SEAM	TOP	BOT SAMPLE	ATYP	5G	YIELD	ASH	RESMOIST	VOL	CARB	KÇAL	SULF	FSI	
	400.05	400 FE \$440				45.54							
10	102.95	103.55 412	RAW	.00	.00	18.61	.81	27.25	53.33	6683.00	. 4 1	-1.00	
10 9	102.95	103.55 \ 412 106.10 \ 413	WASH	1.60	87.00	14.16	1.05	27.81	56.98	7057.00	.41	2.00	
9	105.00	106.10 413	RAW WASH	1.60	47.00	38.46	. 67 . 99	23.24	37.63	4798.00	1.82	-1.00	•
9		106.10 ~413		.00		14.29		28.53	56.19	7092.00	.50	3.00	
9	106.44 106.44	106.75 -414	RAW Wash	1.60	.00 67.00	22.79 10.21	. 58 1 . 07	29.24 32.02	46.81 56.70	6229.00 7475.00	1.26	-1.00 8.50	
8	107.58	110.48 7415	RAW	.00	.00	33.07	.77	23.58	42.58	5328.00	.61 .36	-1.00	
8	107.58	110.48 • 415	WASH	1.60	61.00	15.14	1.29	27.61	55.96	6955.00	. 43	3.50	
8	110.72	112.04 416	RAW	.00	.00	42.62	.59	22.20	34.59	4499.00	1.39	-1.00	
8	110.72	112.04 416	WASH	1.60	54.00	18.54	1.06	28.77	51,63	6686.00	.58	5.50	
Q	115.53	115.75 417	RAW	.00	.00	56.01	.38	22.94	20.67	2699.00	.60	-1.00	
Q	115.53	115.75 417	WASH	1.60	19.00	14.80	1, 11	28.64	55.45	6910.00	.44	3.50	
6	117.96	119.16 118	RAW	.00	.00	49.19	58	19.24	30.99	3788.00	5.28	-1.00	
6	117.96	119.16 *418	WASH	1.60	40.00	14.75	.79	26.73	57.73	7012.00	4.90	1.00	
6	120.68	121.05 • 419	RAW	.00	.00	17.80	.96	25.14	56.10	6758.00	1.83	-1.00	
6	120.68	121.05 - 419	WASH	1.60	88.00	13.10	. 94	25.90	60.06	7192.00	1.22	1.00	
3	137.90	138.38 *420	RAW	.00	.00	29.47	.82	24.43	45.28	5662.00	3.50	-1.00	
3	137.90	138.38 *420	WASH	1.60	64.00	15.78	. 75	27.19	56.28	6980.00	2.67	1.00	
3	139.43	140.78. 421	RAW	.00	.00	13.38	.91	25.94	59.77	7081.00	1.79	-1.00	
3	139.43	140.78 421	WASH	1.60	86.00	9.08	1.15	26.95	62.82	7465.00	1,12	1.00	
3	141.73	142.09 422	RAW	.00	,00	16.56	.87	25.36	57.21	6758.00	1.71	-1.00	
3	141.73	142.09 *422	WASH	1.60	87.00	10.86	1.11	24.80	63.23	7342.00	1.16	1,00	
3	142.77	143.13 1423	RAW	.00	.00	30.28	.74	24.67	44.31	5321.00	1.22	-1.00	
3	142.77	143.13 423	WASH	1,60	60.00	13.03	1.06	25.44	60.47	7078.00	1.10	1.00	
2	148.40	148.98 424	RAW	.00	.00	37.63	.77	22.40	39.20	4882.00	3.08	-1.00	
2	148.40	148.98 424	WASH	1.60	48,00	19.50	1.04	25.50	53.96	6589.00	1.64	1.00	
2	151.20	151.62 \425	RAW	.00	.00	17.02	.64	29.42	52.92	6737.00	2.55	-1.00	
2	151.20	151.62 425	WASH	1.60	80.00	9.46	. 86	29.80	59.88	7472.00	1.74	5.50	
2	151.84	153.22 \426	RAW	.00	.00	20.03	.86	25.51	53.60	6401.00	. 48	-1.00	
2	151.84	153.22 \426	WASH	1.60	79.00	9.95	1.43	26.30	62.32	7486.00	. 52	1.00	
2	156.12	156.70 ~427	RAW	.00	.00	20.91	. 94	23.33	54.82	6426.00	3.42	-1.00	
2	156.12	156.70 427	WASH	1.60	72.00	10.80	1.20	25.76	62.24	7275.00	1.20	1.00	
1	266.40	266.60 7428	RAW	.00	.00	46.44	. 58	21.19	31.79	4167.00	1.72	-1.00	
1	266.40	266.60 > 428	WASH	1.60	29.00	24.72	, 69	26.96	47.63	5247.00	.81	7.00	
1	266.82	267.31 ~429	RAW	.00	.00	16.94	. 52	27.23	55.31	6833.00	. 69	-1.00	
1	266.82	267.31 429	WASH	1.60	82.00	11.11	. 95	27.64	60.30	7389.00	. 63	3.50	
1	267.64	268.67 ~ 430	RAW	.00	.00	19.49	.67	27.48	52.36	6657,00	1,44	-1.00	
1	267.64	268.67 ~430	WASH	1.60	77.00	11.34	. 90	29.05	58.71	7410.00	. 99	5.50	
1	275.97	277.88 -431	RAW	.00	.00	18.73	. 44	26.43	54.40	6698.00	2.33	-1.00	
1	275.97	277.88 `431	WASH	1.60	74.00	9.09	. 88	28.40	61.63	7592.00	1.19	5.00	
1	278.10	279.02 ~ 432	RAW	.00	.00	34,60	.45	24.77	40.18	5211.00	1.06	-1.00	
1	278.10	279.02 - 432	WASH	1.60	53. Q O	15.39	.76	30.39	53.46	7038.00	1.25	6.00	
1	279.88	281.60 ~433	RAW	.00	.00	27.45	. 39	27.09	45.07	5683.00	1.88	-1.00	
1	279.88	281.60 `433	WASH	1.60	62.00	12.11	.71	28.93	58,25	7352.00	1.09	6.00	
1	281.98	282.20 ~ 434	RAW	.00	.00	13.30	. 33	28.69	57.68	7078.00	. 90	-1.00	
1	281.98	282.20 > 434	WASH	1.60	83.00	6.87	.99	28.06	64.08	7784.00	.90	5.00	
1	283.04	284.11 ~ 435	RAW	.00	.00	27.37	1.00	24.90	46.73	5715.00	.39	-1.00	
1	283.04	284.11 - 435	WASH	1.60	63.00	10.40	. 98	27.73	60.89	7424.00	. 48	5.50	
Q	288.36	289.46 - 436	RAW	.00	.00	44.56	. 92	19.84	34.68	4176.00	. 26	-1.00	· ·
0	288.36	289.46 436	WASH	1.60	30.00	18.37	1.02	24.86	55.75	6664.00	. 37	4.50	
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PAGE	63													
TW82D		DOT CAMPLE	. TVD	20	VIELD	4.011	25040107							
SEAM 	TOP	BOT SAMPLE		SG	YIELD		RESMOIST	VOL	CARB	KCAL	SULF	FSI		
8	4.78 4.78	6.40 406 6.40 406 21.20 407	RAW Wash	.00 .00	.00	14.05 6.64	1.42	25.66 27.01	58.87 64.24	7478.00	. 52 . 50	-1.00 2.00		
7	20.68 20.68	21,20 407	WASH	1.60	.00 33.00	40.35 19.55	1.19 .82	21.24 27.34,	52.29	4521.00 6485.00	1.30	-1.00 4.00		 -
5 5	39.86 39.86	40.95 408 40.95 408	RAW Wash	.00 1.60	.00 81.00	13.72 9.41	1.03 1.22	26.55 27.62		7027.00 7408.00	. 48 . 37	-1.00 1.00		
4	46.12 46.12	49.45 409 49.45 409	RAW WASH	.00 1.60	.00	12.27 7.30	.97 1.04	27.83 29.79	58.93	7198.00 7640.00	. 49 . 50	-1.00 3.50		
2	53.21 53.21	54.74 \ 410 54.74 \ 410	RAW WASH	.00	.00	42.05 16.88	.79	21.41	35.75	4325.00 6734.00	. 38	-1.00		
1	217.52	218.35 `411	RAW	1.60	47.00	22.22	. 95 . 78	26.42 24.99	52.01	6427.00	.48 1.73	1.00 -1.00		
1	217.52	218.35 411	WASH	1 - 60	76.00	16.48	. 89	26.86	55.77	6956.00	.74	2.50		
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EAM	TOP	BOT SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI
7	42.94	44 . 10 ~400	RAW	.00	.00	16.32	.78	27.26	55.64	6771.00	3.15	-1.00
7	42.94	44.10 \400	WASH	1.60	81.00	8.18	. 79	29.96	61.07	7544.00	1.47	2.50
5	53.95	55.80 `401	RAW	,00	.00	14.69	. 87	27.17	57.27	6889.00	. 90	-1.00
5	53.95	55.80 \401	WASH	1.60	80.00	7.89	1.04	28.39	62.68	7498.00	.76	1.00
6	59.12	59.6 4 ~ 402	RAW	.00	.00	32.32	.90	23.67	43.11	5300.00	. 44	-1.00
5	59.12	59.64 > 402	WASH	1.60	56.00	3.90	. 78	31.20	64.12	7897.00	. 56	2.00
2	83.88	84.18 ~403	RAW	.00	.00	32.77	. 68	20.66	45.89	5273.00	. 38	-1.00
2	83.88	84.18 403	WASH	1.60	43.00	14.98	.89	24.83	59.30	6886.00	. 46	1.50
2	87.43	87.90 >404	RAW	.00	.00	44.57	. 85	5.88	48.70	3982.00	. 42	-1.00
2	87.43	87.90 ~404	WASH	1.60	28.00	14.19	.64	6,40	78.77	6998.00	. 69	- 00
2	88.08	88.84 ~405	RAW	.00	.00	13.35	.77	25.93	59.95	7066.00	1.05	-1.00
2	88.08	88.84 🛰405	WASH	1.60	86,00	8.52	1.17	27.48	62.83	7463.00	.79	1.50

183 D-	301													
AM_	TOP	BOT	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	F5I	
	≥ 13.10 -	14.08	468	RAW	- 00	.00	22.96	. 98	.00	.00	6030.00	. 44	-1.00	
	13.10 15.53		468	WASH	1.80	85.15	13.97	1.66	26.77	57.60	6785.00	. 45	1.50	
	15.53	17.32 17.32		WASH	1.80	94.90	9.32 7.81	2.08	29.95	60 16	7340.00 7299.00	1.71 1.14	-1.00 1.00	
	~ 32.70	33.22	470	RAW	.00	.00	21.14	.74	.00	.00	6337.00	3.43	-1.00	
	32.70	33.22	470	WASH	1.80	94.08	14.58	1.21	27.63		6902.00	2.16	1.00	
	33.97 33.97	35.20 35.20		WASH	1.80	95.68	16.03	. 94 2 . 44	.00 26.47		6757.00 6808.00	1.85	-1.00 1.00	
	36.06	26 40	`	RAW	.00	.00	13.63	.79	-00		7081.00	2.34	~1.00	
	36.06	36.40	472	WASH	1.80	96.96	12.11	1.40	26.60	59.89	7096.00	1.54	. 50	
	36.77 36.77	36.40 36.40 37.12 37.12 46.50	473	RAW	.00	.00	32.52	. 73	.00		4924.00	2.16	-1.00	
	44.7 6	46.50	474	WASH RAW	1.80 .00	68.70 .00	21.26 13.04	1.45 .88	26.82		6101.00 6929.00	1.86 .41	1.00 -1.00	
	44.76	46.50	474	WASH	1.80	96.85	11.33	1.18	27.06		7116.00	. 4 1	1.00	
												· · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·
														
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 11.41 11.41 12.96 14.47 14.47 14.69 26.08 26.08	11.97 11.97 14.11 14.11 14.54 14.54 14.84 14.84 30.36 30.36	480 481 481 482 482 483 483 484	ATYP RAW WASH RAW WASH RAW WASH RAW WASH RAW WASH RAW	5G .00 1.80 .00 1.80 .00 1.80 .00 1.80	90.54 .00 83.17 .00 9.75 .00 69.40 .00 90.28	A5H 19.14 14.86 27.43 17.07 76.39 34.73 32.93 22.69 16.94 9.44	. 70 1.57 1.14 2.10 1.16 1.04 .72 1.48 .88 2.02	26.97 .00	56,30 .00 55,92 .00 37,63 00 48,86 .00	KCAL 6566.00 6848.00 5761.00 6565.00 1308.00 4821.00 4920.00 6021.00 6758.00 7350.00		FSI -1.00 .50 -1.00 1.00 -1.00 1.00 -1.00 1.00 -1.00
 												
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SEAM	TOP	BOT	SAMPLE	ATYP	\$G	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
、														
6	5.00	6.00	485	RAW	.00	- 00	10.14	. 83	.00	.00	7295.00	, 50	-1.00	
6	5.00	6.00	485	WASH	1.80	98.81	8.27	2.98	27.79	60.96	7273.00	. 49	1.00	
6	7.28	9.21	486	RAW	.00	.00	6.91	1.30	.00	- 00	7440.00	2.67	-1.00	
6	7.28	9.21	486	WASH	1.80	97.80	5.59	2.06	29.20	63.15	7649.00	.89	1.50	
3	25.62	26.08	487	RAW	.00	.00	18.96	. 65	.00	.00	6623.00	2.45	-1.00	
3 ~~	25.62	26.08	487	WASH	1.80	94.18	17,12	2.35	24.65	55.88	6630.00	2.09	1.00	
3	26.91	28.00	488	RAW	.00	.00	21.44	.70	- 00	.00	6312.00	2.62	-1.00	
3	26.91	28.00	488	WASH	1.80	88.89	15.25	2.06	24.84	57.85	6771.00	2.00	1.00	
3	~ 28.98	29.30	489	RAW	.00	.00	19.56	. 64	- 00	.00	6585.00	1.28	-1.00	
3	28.98	29.30	489	WASH	1.80	90.60	15.02	2.43	25.28	57.27	6852.00	1.22	1.00	
Q	- 29.30	29.66	490	RAW	. 00	.00	84.65	1.32	.00	- 00	596.00	2.69	-1.00	
) -	7 29.30	29.66	490	WASH	1.80	1.61	31.39	1.78	25.61	41.22	5355.00	3.29	3.00	
3 _	29.62	29.94	491	RAW	.00	.00	35.18	. 79	.00	.00	4853.00	2.25	-1-00	
3	29.62	29.94	491	WASH	1.80	70.53	21.29	2.19	26.01	50.51	6138.00	2.03	1.00	
Q .	33.81	34.48	492	RAW	.00	. 00	66.42	1 . 15	.00	.00	2077.00	2.73	-1.00	
0 (33.81	34.48	492	WASH	1.80	20.58	28.73	1.80	25.99	43.48	5571.00	2.98	1.00	
2 _	37.70	39.74	493	RAW	.00	.00	14.78	. 92	.00	.00	6849.00	1.88	-1.00	
2	37.70	39.74	493	WASH	1.80	92.49	9.31	2.10	28.71	59 .88	7384.00	. 49	. 50	
2	40.08	40.74	494	RAW	.00	.00	12.21	. 89	.00	.00	7109.00	.68	-1.00	
2	~4 0.08	40.74	494	WASH	1.80	96.20	10.07	2.73	26.57	60.63	7229.00	.61	1.00	

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6 3 3 Q	TOP 13.76 13.76 29.16 29.16 34.85 34.85 46.98	18.70 18.70 30.07	496 496 497 497 498	ATYP RAW WASH RAW WASH RAW WASH RAW WASH RAW	SG .00 1.80 .00 1.80 .00 1.80	YIELD .00 58.88 .00 73.38 .00 73.41 .00 91.19	ASH 38.96 10.95 32.06 17.58 37.68 30.59 16.01 9.83	RESMOIST 1.14 2.54 -79 2.78 -85 1.63 1.22 3.57	VOL .00 26.45 .00 23.11 .00 20.74 .00 26.93	60.06 .00 56.53 .00 47.04	KCAL 4675.00 7030.00 5288.00 6587.00 4972.00 5576.00 6789.00 7158.00	SULF .45 .53 3.16 1.45 2.83 2.10 .66	FSI -1.00 1.50 -1.00 1.00 -1.00 -1.00 -1.00 -1.50	
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TWB3D	-306													
SEAM	TOP	BOT	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
8	9.6 0	10.56	499	RAW	.00	.00	12.16	1.24	.00	.00	7159.00	1.13	-1.00	
8	9.60	10.56	499	WASH	1.80	98.31	9.50	1.88	29.32	59.30	7288.00	1.18	1.00	
7	26.46	27.02	500	RAW	.00	.00	11.67	1.18	.00	.00	7206.00	1.32	-1.00	
7	26.46	27.02	500	WASH	1.80	97.31	11.02	2.47	28.84	57.67	7079.00	1.28	1.00	
6	31.40	32.21	501	RAW	- 00	.00	14.92	1.20	.00	.00	6859.00	2.40	-1,00	
6	>31.40	32.21	501	WASH	1.80	95.73	11.73	2.69	27.58	58.00	6987.00	1.66	1.00	
6	33.28	34.44	502	RAW	- 00	.00	13.34	1.20	.00	.00	7050.00	1.93	-1.00	
6 .	33.28	34.44	502	WASH	î.BŌ	92.69	9.68	2.75	28,81	58.76	7178.00	1.44	1.00	
6	39.85	41.15	503	RAW	.00	. 00	13.40	1.26	.00	.00	6893.00	1.15	-1.00	
6	39.85	41.15	503	WASH	1.80	86.96	6.06	2.33	30.71	60.09	7513.00	.71	. 50	
3	58.00	58.46	504	RAW	.00	.00	15.97	1.14	.00	.00	6872.00	1.83	-1,00	
3	58.00	58.46	504	WASH	1.80	95.49	14.73	2.41	27.76	55.10	6829.00	1.52	1.00	
Э.	58.84	60.05	505	RAW	.00	.00	18.02	. 1.19	.00	.00	6608.00	2.79	-1.00	
3	58.84	60.Q5	505	WASH	1.80	91.23	11.81	3.34	26.06	58.25	6966.00	1.22	. 50	
3	61.12	61.40	506	RAW	.00	.00	19.24	1.01	.00	.00	6554.00	3.92	-1.00	
3	61.12	61.40	506	WASH	1.80	90.18	13.89	2.24	26.39	57.48	6954.00	2.32	.50	
Q	66.86	67.46	507	RAW	.00	.00	46.72	1.06	.00	.00	3829.00	4.60	-1.00	
Q	66.86	67.46	507	WASH	1.80	51.26	27.7 9	1.68	27.02	43.51	5720.00	2.64	1.00	
2	~ 69.65	72.59	508	RAW	.00	.00	11.65	1,34	.00	.00	7164.00	.61	-1.00	
2	69.65	72.59	508	WASH	1.80	96.57	10.92	3.11	26.75	59.22	7018.00	.47	1.00	

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TW83D	-307													
SEAM.	TOP	BOT	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
	<u> </u>										7400 00		4.00	
10	22.17	23.09	509	RAW	.00	-00	8.83	1.06	.00	.00	7480.00	3.15	-1.00	
10 _	22.17	23.09	509	WASH	1.80	98.89	8.80	1.97	31.41	57.82	7399.00	2.96	2.00	
9	34.09	35.18	510	RAW	,00	.00	10.90	1.04	.00	.00	7338.00	2.64	-1.00	
9	34.09	35.18	510	WASH	. 00	.00	10.25	1.91	32.87	54.97	7317.00	2.19	4.50	
3	37.02	39.46	511	RAW	.00	.00	15.87	1.37	- 00	. 00	6746.00	1.07	-1.00	
3 -	37.02	39.46	511	WASH	1.80	94.06	9.45	2.13	29.63	58.79	7260.00	. 93	1.00	
7	54.54	55.66	512	RAW	.00	.00	10.40	1.08	- 00	.00	7354.00	1.81	-1.00	
7	54.54	55.66	512	WASH	1.80	96.84	9.05	2.23	30.32	58.40	7336.00	1.66	1.00	
5	58.47	58.77	513	RAW	.00	.00	9.21	1.02	.00	.00	7517.00	2.08	-1.00	
5	58.47	58.77	513	WASH	1.80	97.36	7.26	1.83	30.42	60.49	7588.00	1.26	1.00	
6	59.11	59.41	514	RAW	.00	.00	14.82	1.07	.00	.00	6999.00	2.73	-1.00	
3	59.11	59.41	514	WASH	1.80	89.93	9.97	1.63	28.83	59.57	7339.00	1.48	1.00	
5	59.76	60.52	5 1 5	RAW	.00	. 00	30.51	1.03	.00	,00*	5352.00	10.73	-1.00	
5	59.76	60.52	515	WASH	1.80	77.34	14.87	2.13	26.83	56.17	6799.00	1.54	1.00	
6	61.01	62.52	516	RAW	. 00	.00	14.84	1,28	.00	. 00	6808.00	. 86	-1.00	
6	61.01	62.52	516	WASH	1.80	86.30	8.12	2.34	29.73	59.81	7299.00	.61	1.00	
5	73.31	76.13	517	RAW	.00	.00	14.38	1.33	.00	.00	6920.00	. 78	-1.00	
5	73.31	76.13	517	WASH	1.80	93.19	8.50	2.85	28.46	60.19	7283.00	. 52	1.00	
4	78.73	80.36	518	RAW	.00	.00	10.58	1.30	.00	.00	7248.00	1.78	-1.00	
4	78.73	80.36	518	WASH	1.80	96.22	8.97	2.97	28.84	59.22	7174.00	. 70	1.00	
3	86.07	86.82	519	RAW	.00	.00	22.97	1.05	.00	- 00	5675.00	. 38	-1.00	
3	86.07	86.82	519	WASH	1.80	86.91	7.21	1.63	34.87	56.29	7648.00	1.49	4.50	
3	87.36	90.14	520	RAW	.00	.00	21.69	1.21	.00	.00	6124.00	. 53	-1.00	
3	87.36	90.14	520	WASH	. 00	.00	7.21	1.82	32.62	58.35	7614.00	2.45	2.00	
Q.	90.67	91.31	521	RAW	.00	.00	38.95	. 89	.00	.00	4742.00	2.85	-1.00	
Õ.	90.67	91.31	521	WASH	1.80	65.06	14.94	1.61	30.34	53,11	6837.00	. 67	4.50	
·	92.61	94.35	522	RAW	.00	.00	22.26	.89	-00	.00	6101.00	. 66	-1.00	
2	92.61	94.35	522	WASH	1.80	84.17	24.74	1.26	27.48	46.52	6099.00	2.28	1.00	

SEAM	TOP	BOT	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL.	CARB	KCAL	SULF	<u>FŠI</u>	
10	14.37	15.24	523	RAW	.00	.00	7.49	.77	.00	.00	7617.00	2.42	-1.00	
10	14.37	15.24	523	WASH	1.80	98.60	7.26	1.62	32.71	58.41	7663.00	2.35	3.50	•
9	21.43	22.71	524	RAW	.00	.00	9.95	. 82	.00	.00	7459.00	2.18	-1.00	
)	21.43	22.71	524	WASH	1.80	95.25	8.46	1.61	33.45	56.49	7531.00	1.89	5.00	
}	24.67	27.24	525	RAW	.00	.00	14.08	1.11	.00	.00	6945.00	3.28	-1.00	
ţ	24.67	27.24	525	WASH	1.80	92.59	9.16	3.14	28.65	59.05	7195.00	1.38	- 50	
7	46.92	48.42	526	RAW	-00	.00	14.38	1.10	.00	.00	6938.00	1.57	-1.00	
7	46.92	48.42	526	WASH	1.80	91.50	11.13	2.67	29.04	57.16	7054.00	1.39	2.50	
7	50.91	52.32	527	RAW	. 00	.00	19.62	. 95	.00	.00	6445.00	2.23	-1.00	
7	50.91	52.32	527	WASH	1.80	88.55	11.22	2.80	28.25	57.73	7038.00	2.03	.50	
5	59.02	59.37	528	RAW	.00	.00	13.73	.78	.00	.00	7160.00	1.27	-1.00	
;	59.02	59.37	528	WASH	1.80	-81.73	8.19	2.11	30.02	59.68	7484.00	1.17	1.00	
i	~ 59.92	62.84	529	RAW	, 00	.00	14.24	1.03	.00	.00	6953.00	1.31	-1.00	
3	59.92	62.84	529	WASH	1.80	86.25	9.18	3.09	28.00	59.73	7225.00	1.31	. 50	
5	72.87	76.12	530	RAW	. 00	-00	13.27	1.91	.00	.00	6887.00	. 50	-1.00	
,	72.87	76.12	530	WASH	1.80	82.85	6.83	3.36	* 29.6 5	- 60.16	7391.00	. 54	.50	
ļ	79.51	81.12	53†	RAW	.00	.00	23.09	.82	.00	.00	5268.00	. 39	-1.00	
Į.	_~79.51	81,12	531	WASH	- 1.80	64.70	13.73	1.41	32.13	52.73	6571.00	.48	1.00	
3	83.34	84.42	532	RAW	.00	.00	19.75	1.11	. 00	- 00	6428,00	.43	-1.00	
3	83.34	84.42	532	WASH	1.80	95.91	16.02	1.69	27.32	54.97	6667.00	.42	- 50	
2	86.00	86,22	533	RAW	.00	.00	33.35	.95	.00	.00	.00	. 75	-1.00	
2	86.00	86.22	533	WASH	1.80	81.56	25.38	1.40	26.98	46.24	5786.00	.75	1.00	
2	36.64	87.20	534	RAW	.00	.00	14.65	1.04	.00	.00	6879.00	1.31	-1-00	
2	~ 86.64	87.20	534	WASH	1.80	91.62	11.69	1.73	29.99	56.59	7092.00	1.20	1.00	

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ΔM	TOP		SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
	8.90	9.74	535	RAW	.00	.00	13.51	2.05	.00	.00	6961.00	2.46	4.00	
	્રે 8.90	9.74	535	WASH	1.80	97.00	11.65	1.42	28.71	58.22	6961.00 7096.00	2.46	-1.00 .50	
	11.88	12.90	536	RAW	.00	00	14.94	1.88	00	.00	6778.00	1.10	-1.00	
	11.88 24.14	12.90 26.32	536 537	WASH RAW	1.80	88,78 .00	9.50 15.87	1.40	31.65	57.45	7264.00	1.11	.50	
	24.14	26.32	537	WASH	1.80	88.63	10.38	1.24 1.60	.00 29.62	.00 58.40	6704.00 7139.00	. 49 . 50	-1.00 1.00	
	27.36	29.02	538	_RAW	.00	.00	8.84	1.23	.00	.00	7370.00	1.78	-1.00	
	27.36 45.32	29.02	538	WASH	1.80	95.76	6.45	2.10	30.24	61.21	.00	1.11	. 50	
	45.32	45.74 45.74	539 539	RAW Wash	.00 1.80	.00 96.93	19.39 15.65	.99 1.35	.00 28.33	.00 54.67	6522.00 6786.00	2.46 2.16	-1.00 1.00	
	46 87	47.98	540	RAW	.00	.00	18.81	1.07	-00	.00	6280.00	.91	-1.00	
_	46.87	47.98	540	WASH	1.80	85.98	12.98	2.02	28.32	56.68	6868.00	.78	.50	
~	.49.44 49.44	49.77 49.77	541 541	WASH RAW	1.80	58.28 .00	27.73 38.13	1.36 .94	28.25	42.66	5491.00	2.81	1.00	
	≺ 56.18	60.60	542	RAW	.00	.00	17.09	1.12	.00	.00	4337.00 6617.00	2.77 .47	-1.00 -1.00	
	56.18	60.60	542	WASH	1.80	91.47	12.42	1.58	29.08	56.92	7026.00	.49	.50	
	60.78 60.78	61.44 61.44	543 543	RAW Wash	.00 1.80	-00 96.75	9,93 9,64	1.22	.00 29.27	.00	7258.00	. 56	-1.00	
	00.70	01.77	545	MH JII	1.00	30.75	9.04	1.37 .	29.21	59.72	7290.00	. 5 5	1.00	
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PAGE	80													
W83D	-310													
EAM	TOP	вот	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
														
0	9.06	10.09	544	RAW	.00	. 00	12.72	1.43	.00	.00	7117.00	3.02	-1.00	
0	9.06	10.09	544	WASH	1.80	94.05	10.62	1.23	34.22	53.93	7315.00	2.55	-1.00	
	77.28	18.32	545	RAW	.00	.00	12.89	1.10	.00	.00	.00	1.95	-1.00	
	17.28	18.32	545	WASH	1.70	93.34	8.71	1.53	34.08	55.68	7420.00	1.57	-1.00	
	20.20	22.56	546	RAW	.00	.00	12.98	1.53	.00	.00	.00	1.40	-1.00	
	20.20	22.56	546	WASH	1.70	92.66	8.26	2.55	30.03	59.16	7284.00	. 90	-1.00	
	41.24	42.48	547	RAW	00	.00	20.32	1.45	.00	.00	.00	1.74	-1.00	
	41.24	42.48	547	WASH	1.70	82.81	9.88	2.21	30.19	57.72	7190.00	1.33	-1.00	
	48.61	49.32	548	RAW	.00	.00	36.59	1.38	.00	.00	.00	2.63	-1.00	
	48.61	49.32	548	WASH	1.70	66.57	14.60	1.39	28.32	55.69	6817.00	2.95	-1.00	
	50.38	52.16	549	RAW	.00	.00	35.80	1.39	.00	.00	.00	1.35	-1.00	
	50.38	52.16	549	WASH	1.70	59.90	13.52	2.23	26.77	57.48	6832.00	1.12	-1.00	
	252.60	54.16	550	RAW	- 00	.00	21.23	1.25	- 00	.00	.00	.83	-1.00	
•	52.60	54.16	550	WASH	1.70	83.04	9.77	2.36	30.07	57.80	7165.00	. 58	-1.00	
	71.46	71.93	551	RAW	.00	. 00	30.60	.92	.00	.00	.00	2.83	-1.00	
	71.46	71.93	551	WASH	1.70	64.63	25.34	1.49	27.09	46.08	5948.00	1.06	-1.00	
	74.49	74.86	552	RAW	.00	.00	49.27	1.28	.00	.00	.00	. 27	-1.00	
	74.49	74.86	552	WASH	1.70	41.96	17.4 6	1.90	28.03	52.61	6545.00	. 25	-1.00	•
	77.16	79.49	553	RAW	- 00	.00	23.43	1.32	.00	.00	.00	. 43	-1.00	
	77.16	79.49	553	WASH	1.70	81.32	- 13.13	2.39	29.58	54.90	6899.00	. 4 1	-1.00	
	79.83	80.90	554	RAW	.00	. 00	23.93	1.31	.00	.00	.00	. 43	~1.00	
	79.83	80.90	554	WASH	1.70	81.56	11.74	3.88	26.19	58.19	6955.00	. 26	-1.00	
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SEAM		BQT	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
7	~ 6.55	7.83	561	RAW	.00	.00	12.34	1.61	.00	.00	.00	. 48	-1.00	
7	≈ 6.55	7.83	561	WASH	1.70	92.15	8.25	1.95	29.58	60.22	7234.00	. 47	-1.00	
7	9.40	11.38	562	RAW	.00	.00	6.25	1.60	.00	.00	,00	.99	-1.00	
7	9.40	11.38	562	WASH	> 1.70	96.43	4,71	2.67	30.63	61,99	7398.00	.83	-1.00	
6	~ 17.62	19.12	563	RAW	.00	.00	15.16	1.21	.00	.00	.00	.59	-1.00	•
6	17.62	19.12	563	WASH	1.70	93.92	11.56	2.59	27.79	58.06	7034.00	. 30	-1.00	
6	№ 19.29	21.28	564	RAW	.00	.00	13.20	1.22	.00	.00	.00	1.86	-1.00	
6	19.29	21.28	564	WASH	1.70	88.90	7.68	3.44	29.11	59.77	7267.00	.44	-1.00	
3	~ 35.20	35.52	565	RAW	.00	.00	25.54	1.09	.00	.00	.00	3.33	-1.00	
3	85.20	35.52	565	WASH	1.70	81.50	14.19	1.71	26.06	58.04	6938.00	1.30	-1.00	
0	41.42	41.78	566	RAW	.00	.00	33.63	. 95	.00	.00	.00	1.51	-1.00	
Q	41.42	41.78	566	WASH	1.70	78.04	28.59	1.33	27.97	42.10	5714.00	. 75	-1.00	
3	44.60	46.56	567	RAW	.00	.00	15.19	1.19	.00	.00	.00	1.77	-1.00	
3	44.60	46.56	567	WASH	1.70	84.11	10.86	1.47	35.27	52.40	7289,00	.77	-1.00	
3	47.03	47.26	568	RAW	.00	.00	36.04	1,19	.00	.00	.00	1.83		
3	47.03	47.26	568	WASH	1.70	57.63	17.62	1.80	31.97	- 48.61	6631.00		-1.00	
2	> 51.96	53.00	569	RAW	.00	.00	26.85	1.23	.00	.00	.00	1.14		
2	51,96	53.00	569	WASH	1.70	79.58	16.64	2.28	26.95	54.13	6670.00	.46	-1.00	
2	53.94	57.80	570	RAW	.00	.00	18.89	1.39	.00	.00			-1.00	
2	53.94	57.80	570	WASH	1.70	85.41	9.85	3.07	27.47	59.61	.00	. 56	-1-00	
-	, ·	20	2,0	.,,,,	0	JJ.71	5.65	4.07	21.41	J9.61	7141.00	. 24	-1.00	

Things on the Xerex 9730 E.P.

AM		TOP	BOT	SAMPLE	ATYP	SG 	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
	32 32 38	. 32 . 32	33.22 33.22 39.32	571	RAW Wash Raw	.00 1.70 .00	.00 80.01	20.83 12.64	.91 1.26	.00 29.95	.00 56.15	.00 7084.00	6.23 3.75	-1.00 -1.00	
	38	.80 47	39.32 39.32 41.08	572	WASH RAW	1.70	.00 69.46 .00	22.60 12.79 48.61	.82 1.42 1.12	.00 27.21 .00	,00 58.58 .00	,00 7031.00 .00	1.96 1.04 1.95	-1.00 -1.00 -1.00	
	40 47	. 47 . 68	41.08 51.76	574	WASH RAW	1.70	35.71 .00	13.71 25.54	1.37 1.2 6	30.51 .00	54.41 00	6984.00	1.81 .56	-1.00 -1.00	
	47	. 68	51.76	574	WASH	1.70	74.05	11.46	2.32	29.83	56.39	7023.00	. 61	-1.00	-
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83D-0	TQP	ВОТ	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
	44.30 44.30 55.62 55.62	44.60 44.60 56.40	575 575 576 576	RAW WASH RAW WASH	.00 1.70 .00 1.70	.00 82.92 .00 80.80	20.33 12.56 20.76	1.06 1.32 1.17 2.67	.00 30.82 .00 28.67	.00 55.30 .00 58.61	.00 7106.00 .00 7226.00	3.26 2.80 1.46	-1.00 -1.00 -1.00 -1.00	
_	63.84 63.84	66.42 66.42	577 577	RAW WASH	.00 1.70	.00 74.54	24.09 11.03	.97 3.17	.00 28.98	.00 56.82	.00 7083.00 	, 93 . 58	-1.00 -1.00	
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EAM	-318 TOP	ВОТ	SAMPLE	ATYP	\$ G	YIELD	ASH 	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
	89.73	91.97	600	RAW	.00	.00	10.28	1.27	. 00	.00	.00	1.38	-1.00	
	89.73 92.28	91.97 95.06		WASH RAW	1.70	93.54 .00	7.20 14.53	1.34 1.18	29. 61 .00	61.85 .00	7647.00 .00	.49 1.38	-1.00 -1.00	
	92.28	95.06 98.32		WASH RAW	1.70	90.12	10.78	1.31	29.13	58.78	7238.00	.51	-1.00	
	> 97.18	98.32	602	WASH	.00 1.70	,00 82.48	21.52 15.34	1.36 1.62	.00 28.60	.00 54.44	.00 6763.00	. 35 . 19	-1.00 -1.00	
	103.22	103.94		RAW WASH	1.70	,00 69.68	34.57 23.36	. 93 1.42	.00 25.35	- <u>- 00</u> 49.87	.00	. 32	-1.00 -1.00	
,	108.68	109.54	604	RAW	.00	.00	55.81	1.16	.00	.00	.00	. 19 . 18	-1.00	
	108.68	109.54	604	WASH	1.70	27.33	32.29	1.31	23.52	42.88	5208.00	. 16	-1.00	
														
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W83D- Eam	TOP	вот	SAMPLE	ATYP	SG	YIELD	4517	RESMOIST	VOL	CARB	KON	CIII E		
	105		SAMPLE	ALTE		TIELD	ASH	KESMOISI	VUL	CARB	KCAL	SULF	FSI	
>	5.20	6.24	586	RAW	.00	.00	13.51	1.03	.00	.00	.00	3.06	-1.00	
)	5.20	6.24	586	WASH	1.70	92.95	9.63	1.13	32.87	56.37	7428.00	1.47	-1.00	
	12.83	14.40	587	RAW	.00	.00	10.18	. 96	.00	.00	.00	2.87	-1.00	
	12.83	14.40	587	WASH	1.70	92.65	6.81	1.03	34.86	57.30	7663.00	. 86	-1.00	
	15.36	17,74	588	RAW	. 00	.00	13.51	1.17	.00	.00	.00	1.68	-1.00	
	15.36	17.74	588	WASH	1.70	90.20	8.18	1.77	31.41	58.64	7425.00	. 64	-1.00	
	37.56	38.84	589	RAW	.00	.00	16.94	1.20	.00	.00	.00	1.30	-1.00	
	37.56	38.84	589	WASH	1,70	88.01	9.81	1.61	30.51	58.07	7285.00	. 57	-1.00	
	42.79	43.09	590	RAW	.00	.00	24.53	1.01	.00	.00	.00	4 01	-1.00	
	42.79	43.09	590	WASH	1.70	79.23	13,07	. 95	29.54	56.44	7112.00	1.59	-1.00	
	43.76	44,16	591	RAW	.00	.00	60.94	1.13	.00	.00	.00	2.44	-1.00	
	43.76	44.16	591	WASH	1.70	18.45	17.34	1,19	25.30	56.17	6554.00	1.03	-1.00	
	52.60	55.21	592	RAW	.00	.00	11.33	1.03	.00	.00	.00	.46	-1.00	
	52.60	55.21	592	WASH	1.70	88.30	4.34	1.57	31.83	62.26	7790.00	. 25	-1.00	
	55.39	55.68	593	RAW	.00	.00	26.63	1.06	.00	.00	.00	2.58	-1.00	
	55.39	55.68	593	WASH	1.70	76.44	20.01	. 98	25.52	53.49	6447.00	1.24	-1.00	
	57.43	61.26	594	RAW	.00	.00	16.01	1.63	.00	.00	.00	.51	-1.00	
	57.43	61,26	594	WASH	1.70	87.40	10.02	2.61	29.09	8.28	7146.00	. 24	-1.00	
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EAM	-320 TOP	вот	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
	85.28	85.72	610	RAW	.00	.00	36.58	. 1.06	.00	.00	.00	1.68	-1.00	
	85.28	85.72	610	WASH	1.70	63.39	25.42	1.55	26.01	47.02	6028.00	.97	-1.00	
	86.75	87.84	611	RAW	.00	-00	11,94	1.19	.00	.00	.00	.76	-1.00	
	86.75	87.84	611	WASH	1.70	98.03	10.17	4.19	27.19	58.45	7139.00	.32	-1.00	
	*87.84	88.13	612	RAW	.00	.00	83.02	1.89	.00	.00	.00	3.90	-1.00	
	~ 87,84	88.13	612	WASH	1.70	1.81	14.00	2.24	26.56	57.20	6732.00	1.70	-1.00	
	88.13	88.36	613	RAW	.00	.00	22.36	.89	-00	.00	.00	.89	-1.00	
	88.13	88.36	613	WASH	1.70	71.88	12.65	2.44	26.01	58.90	7032.00	. 44	-1.00	
	89.19	89.58	614	RAW	.00	.00	32,87	1.06	.00	.00	.00	1.56	-1.00	
	▶89.19	89.58	614	WASH	1,70	62.54	20.35	2.32	25.71	51,62	6241.00	.86	-1.00	
	93.90	94.50	615	RAW	.00	.00	40.69	.88	.00	.00	.00	3.64	-1.00	
	>93.90	94.50	615	WASH	1.70	52.80	17.70	2.06	26.81	53.43	6606.00	1.57	-1.00	
	> 96.27	98.16	616	RAW	.00	.00	9.85	1.19	.00	.00	.00	.50	-1.00	
	96 27	98.16	616	WASH	.00	.00	7.72	2.39	29.95	59.94	7490.00	. 25	-1.00	
	98.74	99.31	617	RAW	.00	. ŏŏ	20.08	.88	.00	.00	.00	3.14	-1.00	
	98.74	99.31	617	WASH	1.70	91.50	16.51	2.56	28,02	52.91	6594.00	1.46	-1.00	
	99.31	99.64	618	RAW	.00	.00	82.65	1.01	.00	.00	.00	1.66	-1.00	
	> 99.31	99.64	618	WASH	1.70	3.93	19.88	1.64	27.46	51.02	6259.00	3.76	-1.00	
	99.64	100.50	619	RAW	.00	-00	25,33	.98	.00	.00	.00	4.56	-1.00	
	99.64	100.50	619	WASH	1.70	77.94	13.21	3.11	27.88	55.80	6909.00	.54	-1.00	
	≥ 100.50	100.73	620	RAW	.00	.00	76.58	.93	.00	.00	.00			
	100.50	100.73	620	WASH	1.70	5.97	8.23	2.09	30.65	59.03	7350.00	2.79	-1.00	
	100.73	101.27	621	RAW	.00	.00	9.14	.96	.00	.00		1.41 3.20	-1.00	
	100.73	101,27	621	WASH	1.70	93.51	5.11	1.98	30.36	62.55	7801.00		-1.00	
	101.27	101.45	622	RAW	-00	.00	73.25	.83	.00	.00		.62	-1.00	
	101 27	101.45	622	WASH	1.70	15.16	19.18	1.93	30.52	48.37	.00	2.93	-1.00	
	101.45	102.14	623	RAW	.00	.00	20.06	.96	.00	.00	6363.00	1.75	-1.00	
	101.45	102.14	623	WASH	1.70	95.13	17.41	1.29		53.89	.00	2.51	-1.00	
	117.08	117.52	624	RAW	.00	.00	26.63	, 92	27,41	.00	6670.00	.73	-1.00	
	117.08	117.52	624	WASH	1.70	78.12	14.04	1.02	.00		.00	3.34	-1.00	
	118.28	119.06	625	RAW	.00	-00			29.05	55.89	7070.00	1.26	-1.00	
	118.28	119.06	625	WASH	1.70		19.88	.96	.00	<u></u>	.00	1.85	-1.00	
	119.83	120.14	626	RAW		88.82	15.12	1.62	26.87	56,39	6928.00	.89	-1.00	
	119.83	120.14	626	WASH	.00 1.70	.00	25.37	1.12	.00	.00	.00	2.24	-1.00	
	~ 120.14	120.14	627			82.67	10.51	1.32	27.01	61.16	7405.00	.50	-1.00	
	∼ 120 14	120.28		RAW	.00		64.69	1.66	.00	.00	.00	3.06	-1.00	
	120.28	120.28	627 628	WASH Raw	1.70	21.04	20.32	1.09	30.07	48.52	6591.00	1.34	-1.00	
	120.28	120.44	628	WASH	.00	00	29.59	1.08	.00	.00	.00	1.61	-1.00	
	124.41	124.99	629		1.70	66.70	16.47	1.91	27.72	53.90	6713.00	. 84	-1.00	
	124.41	124.99		RAW		-00	28.02	. 99	.00	00	.00	2.55	-1.00	
	128.02	124.99	629 630	WASH	1.70	72.52	20.50	1.16	28.09	50.25	6437.00	1.13	-1.00	
	128.02	128.73	630	RAW	.00	.00	20.11	1.05	.00	.00	.00	. 58	-1.00	
	128.02	128.73	631	WASH	1.70	88.56	13.63	1.46	26.96	57.95	6986.00	. 30	-1.00	
	128.84	129.76		RAW	.00	.00	9.34	.97	.00	.00	- 00	. 49	-1.00	
			631	WASH	1.70	95.84	6.60	1.30	28.92	63.18	7638.00	. 24	-1.00	
	129.76	129.90	632	RAW	.00	.00	57.05	1.27	.00	.00	.00	62	-1.00	
	129.76	129.90	632	WASH	1.70	31.02	22.00	1.17	24.21	52.62	6264.00	.51	-1.00	
	129.90	130.64	633	RAW	. 00	. 00	29.82	1.07	.00	.00	.00	. 54	-1.00	
	129.90	130.64	633	WASH	1.70	68.05	14.17	1.52	27 33	56.98	6697.00	. 31	-1-00	
	131.08	131.34	634	RAW	.00	.00	29.99	. 95	. 00	.00	.00	1.08	-1.00	
	131.08	131.34	634	WASH	1.70	76.94	21.74	1.07	18.72	58.47	6257.00	. 50	-1.00	

MA.	-321 TOP	вот	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	F\$I	
	\$81.06	82.03	595	RAW	.00	.00	18.44	1.08	.00	.00	.00	3.07	-1.00	
	81.06	82.03	595	WASH	1.70	86.58	11.06	1.21	31.92		7275,00	1.24	-1.00	
	× 87.58	89.60	596	RAW	.00	.00	20.30	1.12	.00	.00	.00	3.43	-1.00	
	87.58	89,60	5 96	WASH	1.70	83.25	9.26	2.45	29.74		7380.00	- 80	-1.00	•
	90.71 90.71 93.00	91.07	597	RAW	. 00	.00	71.60	1.21	.00	.00	.00	. 19	-1.00	
	90.71	91.07	597	WASH	1.70	20.61	9.63	1.46	27.92		7264.00	. 23	-1.00	
	93.00	93.26 93.26	598 598	RAW WASH	.00 1.70	.00 57.39	42.41	1.21	.00	. 00	.00	1.28	-1.00	
	93.00	94.00	598 599	RAW	.00	.00	19.05 13.55	1.34 1.20	26.22 .00	.00	6479.00	. 52 . 87	-1.00 -1.00	
	93.44	94.00		WASH	1.70	91.83	7.31	2.39	29.14		7485.00	.30	-1.00	
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WB3D. Eam	-322 TOP	вот	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
														•
	^ 108.36	110.14	742	RAW	.00	.00	26.45	. 86	. 00	.00	.00	11.52	-1.00	
	108.36	110.14	742	WASH	1.70	60.75	14.58	1.54	34.10		6954.00	4.96	-1.00	
	<u>~110.30</u>	111.23	743	RAW	- 00	.00	17.94	1.10	.00	.00	.00	2.96	- 1 - 00	
	110.30	111.23	743	WASH	1.70	83.98	11.81	2.12	31.98	54.72		2.06	-1.00	
	134.37	135.99 135.99	744 744	RAW	.00	.00	12.42	1.16	.00	.00	.00	. 53	-1.00	
	134.37	135.99	745	WASH RAW	1.70 .00	90.19 .00	7.23 34.72	2.86	30.85		7447.00	.55	-1.00	
	►136.18	136.48	745	WASH	1.70	74.58	24.10	1,63	.00	.00 50.26	6103.00	1.85	-1.00 -1.00	
	151.11	151.50	746	RAW	.00	,00	26.33	.91	.00	.00	.00	1.89	-1.00	
	151.11	151.50	746	WASH	1.70	74.92	20.56	1.59	26.64		6383.00	1.71	-1.00	
	152.15	153.36	747	RAW	.00	.00	17.57	1.07	.00	.00	.00	1.46	-1.00	
· · ·	152.15	153.36	747	WASH	1.70	89.95	13.46	2.44	24.98	59.12		1.23	-1.00	
	154.89	156.12	748	RAW	.00	.00	50.87	1.59	.00	.00	.00	3.02	-1.00	
	154.89	156.12	748	WASH	1.70	45.00	18.89	1.46	26.04	53.61	6548.00	3.16	-1.00	
1	159.44	160.18	749	RAW	.00	.00	33.52	1.18	.00	.00	.00	1.56	-1.00	
1	159.44	16Q.18	749	WASH	1.70	63.65	18.55	1.52	27.55	52.38	6513.00	1.43	-1.00	
	162.68	164.51	750	RAW	.00	.00	14.39	1.09	- 00	.00	.00	. 67	~1.00	
	162.68	164.51	750	WASH	1.70	88.86	9.67	2.25	27.80		7339.00	. 63	-1.00	
<u>. </u>	164.82	165.85	751	RAW	.00	.00	22.23	1.14	.00	. 00	,00	. 65	-1.00	
	164.82 166.62	165.85	751 750	WASH	1.70	86.77	17.64	2.81	25.51		6559.00	.64	-1.00	
	166.62	167.13 167.13	752 752	RAW Wash	.00 1.70	.00 88.31	17.60 12.04	1.13 2.23	.00	.00	.00	1.26	-1.00	
	100.02	107.13	752	WASH	1.70	00.31	12.04	2.20	27.69	58.04	7149.00	.91	-1.00	
								<u>.</u> <u>.</u>						
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EAM	TOP	BOT	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL .	CARB	KCAL	SULF	FSI	
													*	
6	4.12	7.15	659	RAW	- 00	.00	14,48	1.22	.00	.00	.00	. 70	-1.00	
6	4.12	7.15	659	WASH	1.70	88.82	9.27	3.60	27.33	59.80	7106.00	.61	-1.00	
6	8.73	9.43	660	RAW	.00	. 00	14.86	. 99	.00	.00	.00	4.17	-1.00	
6	8.73	9.43	660	WASH	1.70	82.60	7.27	2.04	31.67	59.02	7477.00	2.54	-1.00	
3	\ 25.50	25.96	661	RAW	. 00	.00	15.92	1.14	.00	.00	.00	6.09	-1.00	
3	25.50	25.96	6 6 1	WASH	1.70	92.84	13.55	1.82	27.81	56.82	6983.00	1.71	-1.00	
3	27.30	27.92	662	RAW	.00	.00	31.55	1.27	.00	.00	.00	1.62	-1.00	
3	27.30	27.92	662	WASH	1.70	72.33	20.09	2.20	23.78	53.93	6295.00	. 82	-1.00	
3	28.31	28.59	663	RAW	.00	.00	20.52	1.20	.00	.00	.00	2.27	-1.00	
3	` 28.31	28.59	663	WASH	1.70	81.56	12.74	1.86	25.29	60.11	7055.00	. 98	-1.00	
2	32.62	32.97	664	RAW	.00	.00	30.09	1.02	.00	.00	. 00	3.50	-1.00	
2	32.62	32.97	664	WASH	1.70	70.01	21.97	1.92	24.59	51.52	6224.00	2,12	-1.00	
2	34.65	37.04	665	RAW	.00	.00	24.57	1.38	.00	.00	.00	1.29	-1.00	
2	34.65	37.04	665	WASH	1.70	76.89	13.53	3.52	27.18	55.77	6796.00	. 80	-1.00	

EAM	TOP	801	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	F51	
														· · · · · ·
8	12.20	14.00	653	RAW	.00	.00	18.59	. 95	. 00	.00	.00	1.25	-1.00	
8	12.20	14.00	653	WASH	1.70	75.51	10.11	3.70	29.34	57.48	7131.00	. 60	-1.00	
Q	14.60	15.15	654	RAW	.00	.00	30.45	1.02	.00	.00	.00	. 63	-1.00	
Q	14.60	15.15	654	WASH	1.70	69.06	17.02	1.79	25.96	55.23	6639.00	. 32	-1.00	
0	₹19.17	19.46	655	RAW	.00	.00	11.42	1.02	.00	.00	.00	3.22	~ f . 00	
Q	19.17	19.46	655	WASH	1.70	93.71	8.88	1.75	30.28	59.09	7389.00	1.42	-1.00	
7	33.00	33.68	656	RAW	.00	.00	21.19	1.19	.00	.00	.00	2.48	-1.00	
7	33.00	33.68	656	WASH	1.70	83.07	15.78	1.89	23.94	58.39	6675.00	. 69	-1.00	
Q	1 43.95	44.36	657	RAW	.00	.00	37.19	1.40	.00	.00	.00	2.10	-1.00	
Q	43.95	44.36	657	WASH	1.70	65.02	21.53	2.47	25.49	50.51	6158.00	1.02	-1.00	
6	49.78	51.72	658	RAW	. 00	.00	18.64	1.28	.00	.00	.00	1.88	-1.00	
6	49.78	51.72	658	WASH	1.70	81.52	9.72	2.22	30.76	57.30	7335.00	. 80	-1.00	

-	PAGE	96													
	TW83D SEAM	TOP		SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	AOT.	CARB	KCAL	SULF	FSI	
	3 3 3 3 2 2 2 2 2	36.86 36.86 40.24 40.24 46.92 46.92 47.92 47.92 49.00	37.87 37.87 41.57 41.57 47.61 47.61	541 541 642 642 643 643 643 644 644	RAW WASH RAW WASH RAW WASH RAW WASH RAW WASH	.00 1.70 .00 1.70 .00 1.70 .00 1.70 .00	00 92.28 .00 92.56 .00 68.62 .00 70.40 .00 73.88	10.08 7.07 10.71 7.37 31.86 10.55 35.91 18.78 20.11 12.96	1 . 12 1 . 85 1 . 20 2 . 30 1 . 62 1 . 91 1 . 26 1 . 57 1 . 12 1 . 70	.00 28.39 .00 29.02 .00 28.24 .00 25.49 .00 26.18	.00 62.69 .00 61.31 .00 59.30 .00 54.16	.00 7528.00 .00 7449.00 .00 7185.00 .00 6435.00 .00 6926.00	1.00 .44 1.38 .56 2.84 .23 .32 .24 .52	-1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00	
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SEAM	TOP	BOT	SAMPLE	ATYP	* SG	YIELD	A5H	RESMOIST	VOL	CARB	KCAL	SULF	F5I	
6	4.87	7.59	736	RAW	.00	.00	15.15	1.43	.00	.00	.00	. 92	-1.00	
6	4.87	7.59	736	WASH	1.70	89.28	10.48	3.08	28.49	57.95	7071.00	.73	-1.00	
6	8.33	8.97	737	RAW	.00	.00	19.45	1.10	.00	.00	.00	1,14	-1.00	
6	8.33	8.97	737	WASH	1.70	95.41	16.89	1.59	26.08	55.44	6722.00	1.03	-1.00	
6	_ ▶10.56	11.01	738	RAW	.00	.00	6.71	1.23	.00	.00	.00	2.29	-1.00	
6	10.56	11.01	738	WASH	1.70	98.60	6.45	1.85	30.57	61.13	7533.00	2.23	-1.00	
3	32.71	33.93	739	RAW	.00	.00	12.84	1.13	.00	-00	.00	.91	-1.00	
3	32.71	33.93	739	WASH	1.70	95.93	10.74	2.97	27.88	58.41	7036.00	.83	-1.00	
2	39.17	39.90	741	RAW	.00	.00	23.39	1.20	.00	.00	.00	2.64	-1.00	
2	_ 39.17	39.90	741	WASH	1.70	78.54	13.26	2.45	29.07	55.22	6981.00	1.92	-1,00	
2	42.05	43.18	740	RAW	.00	.00	31.32	1.33	- 00	.00	.00	.49	-1.00	
2	42.05	43.18	740	WASH	1.70	69.28	13.13	3.62	26.89	56.36	.00	. 58	-1.00	
i														

SEAM)-329 TOP	ВОТ	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI
0	49.20	49.85	753	WASH	1.70	86.38	16.21	1.78	28.86	53.15	6697.00	2.38	-1.00
0	49.20	49.85	753	RAW	.00	.00	21.71	1.18	.00	.00	- 00	3.08	~1.00
9	53.60	54.46	754	RAW	.00	.00	14.05	1.17	.00	- 00	.00	1.83	-1.00
€	53.60	54.46	754	WASH	1.70	93.84	11.34	1.73	33.50	53.43	7132.00	1.75	-1.00
3	54.84	56.80	755	RAW	.00	.00	14.67	1.37	.00	. 00	.00	1.49	~1.00
3	5 4.84	56.80	755	WASH	1.70	89.70	9.58	2.83	30.67	56.92	7125.00	1.01	-1.00
7	76.07	77.26	756	RAW	.00	.00	20.71	1.40	.00	.00	.00	2.45	-1.00
7	76.07	77.26	756	WASH	1.70	79.31	10.42	2.84	29.09	57.65	7089.00	1.83	-1.00
5	83.10	85.64	757	RAW	. 00	.00	15.25	1.52	.00	.00	.00	1.72	-1.00
5	83.10	85.64	757	WASH	1.70	86.02	6.77	3.65	27.99	61.59	7271.00	. 84	~1.00
5	92.52	94.74	758	RAW	.00	.00	12.68	1.54	.00	.00	- 00	.50	-1.00
3	92.52	94.74	758	WASH	1.70	90.09	7.35	3.86	28.21	60.58	7322.00	. 52	-1.00
7	97.26	97.75	759	RAW	.00	.00	7.46	1.32	.00	.00	.00	. 65	-1.00
>	97.26	97.75	759	WASH	1.70	93,98	4.62	3.02	28.52	63.84	7609.00	. 64	-1.00
5	101.59	104.00	760	RAW	.00	. 00	13.94	1.50	.00	.00	.00	44	-1.00
5	101.59	104.00	760	WASH	1.70	88.04	7.73	4.32	26.73	61.22	7166.00	. 43	-1.00
)	~ 106.66	107.61	761	RAW	.00	.00	8.65	1.43	.00	.00	.00	. 43	-1.00
,	~106.66	107.61	761	WASH	1.70	94.59	5.78	4.66	27.21	62.35	7287.00	. 44	-1.00
1	114.30	116.24	762	RAW	.00	.00	16.93	1.28	.00	.00	.00	. 46	-1.00
1	114.30	116.24	762	WASH	1.70	_ 86.62	10.02	3 .20	26.98	59.80	7079.00	.48	-1.00
)	118.18	118.72	763	RAW	.00 4	<u> 00</u>	9.92	4 1.17	.00	.00	.00	2.81	-1.00
>	118.18	118.72	763	WASH	1.70	¥ 1.70	7.05	₹ 93.51	28.29	62.46	7520.00	1.34	-1.00
) .	120.32	120.94	764	RAW	.00	.00	14.76	1.25	.00	.00	.00	1.36	-1.00
2	120.32	120.94	764	WASH	1.70	65.12	8.72	1.93	29.63	59.72	7369.00	1.64	-1.00
3	140.78	141.85	765	RAW	.00	.00	29.92	1.07	.00	.00	.00	2.08	-1.00
3	140.78	141.85	765	WASH	1.70	89.74	10.41	2.89	25.89	60.81	7142.00	1.08	-1.00
3	143.00	143.74	766	RAW	.00	.00	27.20	1.27	.00	.00	.00	2.42	-1.00
3	<u>- 143.00</u>	143.74	766	WASH	1.70	70.44	13.00	1.90	26.64	58.46	6996.00	1.61	-1.00
2	149.02	151.12	767	RAW	.00	.00	32.78	1.07	.00	.00	.00	1.96	-1.00
2 '	149.02	151.12	767	WASH	1.70	60.40	11.95	1.90	30.48	55,67	7160.00	1.54	~1.00
2	-152.08	152.24	768	RAW	.00	.00	48.07	1.00	.00	.00	.00	. 49	-1.00
2	→ 152.08	152.24	768	WASH	1.70	30.60	22.59	1.72	27.76	47.93	6104.00		-1.00
2	152.80	153.18	769	RAW	.00	.00	27.95	1.13	.00	.00	.00	. 7 1	-1.00
2	-152.80	153.18	769	WASH	1.70	84.74	18.87	2.47	22.75	55.91	6381.00	.48	-1.00

PAGE 100 TW83D-330 BOT SAMPLE ATYP SEAM TOP SG YIELD ASH RESMOIST VOL CARB KCAŁ SULF FSI Q 90.58 91.44 770 RAW .00 .00 46.51 1.25 .00 .00 .00 -1.00 1.89 90.58 91.44 770 WASH 1.70 53.95 13.14 2.12 27.27 57.47 7031.00 2.08 -1.00

TOP 52.10 52.10 53.76 53.76 72.70 72.70 80.26	52.64 52.64 55.22 55.22 73.62 73.62	720 720 721 721	RAW WASH RAW	.00 1.70	.00 86.58	ASH 17.38	RESMOIST 1.25		CARB	KCAL	SULF	FSI	
52.10 52.10 53.76 53.76 72.70 72.70	52.64 52.64 55.22 55.22 73.62	720 721 721	WASH RAW	.00 1.70		17.38	1.25						
52.10 53.76 53.76 72.70 72.70	52.64 55.22 55.22 73.62	720 721 721	WASH RAW	1.70			1.25						
53.76 53.76 72.70 72.70	55.22 55.22 73.62	721 721	RAW	•	86.58			.00	.00	.00	2.26	-1.00	
53.76 72.70 72.70	55.22 73.62	721			~~	7.81	1.47	31.28	59.44	7431.00	2.11	-1.00	
72.70 72.70	73.62				.00	8.57	1.38	.00	. 00	-00	2.01	-1.00	
72.70			WASH	1.70	91.65	5.83	2.32	28.80	63.05	7492.00	1.56	-1.00	
	73.62	722	RAW	.00	.00	12.92	. 44	.00	.00	.00	1.47	-1.00	
80.26		722	WASH	1.70	92.11	8.25	4.88	27.60	59.27	7024.00	1.38	-1.00	
	82.52	723	RAW		.00	20.41	1.19	.00	.00	.00	.92	-1.00	
80.26	82.52	723	WASH	1.70	80.22	6.85	3.32	27.81	62.02	7314.00	. 69	-1.00	
		. — .											
95.84		44 /											<u></u>
100.62	101.69				88.12		_						
107.24	110.08				.00								
107.24	110.08	727	WASH	1.70	90.40	6.66	5.13	26.10	62.11		.61		
120.50	122.52	728	RAW	.00	.00	15.90	1,41						
120.50	122.52	728	WASH	1.70	86.92	8.65	3.39	27.15	60.81	7082.00	. 55	~1.00	
135.94	137.14	729	RAW	.00	.00	15.19	1.27	.00	.00	.00	. 87	-1.00	
135.94	137.14	729	WASH	1.70	90.18	11.03	2.52	27.07	59.38	7200.00	.83	-1.00	
137.90	138.68	730	RAW	.00	.00	15.44	1.25	.00	.00	.00	1.15	-1.00	
137.90	138.68	730	WASH	1.70	86.82	9.73	3.07	26.26	61.04	7249.00	1.03	-1.00	
145.94	147.12	731	RAW	.00	.00	13.39	1.25	.00	.00	.00	1.09	-1.00	
145.94	147.12	731	WASH	1.70	93.13	10.51	3.76	26.69	59.04	7224.00	.86	-1.00	
		732	RAW	.00	.00	22.96	1.15	.00	.00	.00	. 96	-1.00	
147.80	148.60	732	WASH	1.70	76.74	10.71	2.72	26.10	60.47	7238.00	. 77	-1.00	
-	-										1.91	-1.00	
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	89.10 89.10 95.84 95.84 100.62 107.24 120.50 120.50 135.94 135.94 137.90 145.94 145.94 147.80	89.10 91.14 89.10 91.14 95.84 96.38 95.84 96.38 95.84 96.38 100.62 101.69 100.62 101.69 107.24 110.08 120.50 122.52 120.50 122.52 120.50 122.52 135.94 137.14 137.90 138.68 145.94 147.12 145.94 147.12 147.80 148.60 147.80 148.60 154.27 156.88 165.30 165.60 165.30 165.60 166.54 167.18	89.10 91.14 724 89.10 91.14 724 95.84 96.38 725 95.84 96.38 725 100.62 101.69 726 100.62 101.69 726 107.24 110.08 727 107.24 110.08 727 120.50 122.52 728 135.94 137.14 729 135.94 137.14 729 137.90 138.68 730 145.94 147.12 731 145.94 147.12 731 147.80 148.60 732 147.80 148.60 732 154.27 156.88 733 165.30 165.60 734 165.30 165.60 734 166.54 167.18 735	89.10 91.14 724 RAW 89.10 91.14 724 WASH 95.84 96.38 725 RAW 95.84 96.38 725 WASH 100.62 101.69 726 RAW 100.62 101.69 726 WASH 107.24 110.08 727 RAW 107.24 110.08 727 WASH 120.50 122.52 728 RAW 120.50 122.52 728 WASH 135.94 137.14 729 RAW 135.94 137.14 729 WASH 137.90 138.68 730 RAW 137.90 138.68 730 WASH 145.94 147.12 731 RAW 145.94 147.12 731 RAW 145.94 147.12 731 RAW 145.94 147.12 731 RAW 145.94 147.12 731 RAW 145.94 147.12 731 RAW 145.94 147.12 731 RAW 145.94 147.12 731 RAW 145.94 147.12 731 RAW 145.94 147.12 731 RAW 145.95 148.60 732 RAW 147.80 148.60 732 WASH 154.27 156.88 733 RAW 165.30 165.60 734 WASH 165.30 165.60 734 WASH 166.54 167.18 735 RAW	89.10 91.14 724 RAW .00 89.10 91.14 724 WASH 1.70 95.84 96.38 725 RAW .00 95.84 96.38 725 WASH 1.70 100.62 101.69 726 RAW .00 100.62 101.69 726 WASH 1.70 107.24 110.08 727 RAW .00 107.24 110.08 727 WASH 1.70 120.50 122.52 728 RAW .00 120.50 122.52 728 WASH 1.70 135.94 137.14 729 RAW .00 135.94 137.14 729 WASH 1.70 137.90 138.68 730 RAW .00 145.94 147.12 731 RAW .00 145.94 147.12 731 WASH 1.70 147.80 148.60 732 <t< td=""><td>89.10 91.14 724 RAW .00 .00 89.10 91.14 724 WASH 1.70 88.44 95.84 96.38 725 RAW .00 .00 95.84 96.38 725 WASH 1.70 86.73 100.62 101.69 726 RAW .00 .00 100.62 101.69 726 WASH 1.70 88.12 107.24 110.08 727 RAW .00 .00 107.24 110.08 727 WASH 1.70 90.40 120.50 122.52 728 RAW .00 .00 120.50 122.52 728 WASH 1.70 86.92 135.94 137.14 729 RAW .00 .00 137.90 138.68 730 RAW .00 .00 137.90 138.68 730 WASH 1.70 93.13 147.80 148.60</td><td>89,10 91,14 724 RAW .00 .00 15,17 89,10 91,14 724 WASH 1,70 88,44 9,95 95,84 96,38 725 RAW .00 .00 13,57 95,84 96,38 725 WASH 1,70 86,73 7,67 100,62 101,69 726 RAW .00 .00 8,31 100,62 101,69 726 WASH 1,70 88,12 7,74 107,24 110,08 727 RAW .00 .00 11,88 107,24 110,08 727 WASH 1,70 90,40 6,66 120,50 122,52 728 RAW .00 .00 15,90 120,50 122,52 728 WASH 1,70 86,92 8,65 135,94 137,14 729 WASH 1,70 90,18 11,03 137,90 138,68 730 RAW .00</td><td>89,10 91,14 724 RAW .00 .00 15,17 1,48 89,10 91,14 724 WASH 1,70 88,44 9,95 2,83 95,84 96,38 725 WASH 1,70 86,73 7,67 2,18 100,62 101,69 726 RAW .00 .00 8,31 1,53 100,62 101,69 726 WASH 1,70 88,12 7,74 1,02 107,24 110,08 727 RAW .00 .00 11,88 1,52 107,24 110,08 727 WASH 1,70 90,40 6,66 5,13 120,50 122,52 728 RAW .00 .00 15,90 1,41 120,50 122,52 728 WASH 1,70 86,92 8,65 3,39 135,94 137,14 729 WASH 1,70 90,18 11,03 2,52 137,90 138,68 730</td><td>89.10 91.14 724 RAW .00 .00 15.17 1.48 .00 89.10 91.14 724 WASH 1.70 88.44 9.95 2.83 28.00 95.84 96.38 725 WASH 1.70 86.73 7.67 2.18 28.80 100.62 101.69 726 RAW .00 .00 8.31 1.53 .00 100.62 101.69 726 WASH 1.70 88.12 7.74 1.02 28.59 107.24 110.08 727 RAW .00 .00 11.88 1.52 .00 120.50 122.52 728 RAW .00 .00 15.90 1.41 .00 120.50 122.52 728 WASH 1.70 86.92 8.65 3.39 27.15 135.94 137.14 729 WASH 1.70 86.92 8.65 3.39 27.15 135.94 137.14 729<</td><td> 89.10</td><td>89,10 91,14 724 RAW .00 .00 15.17 1.48 .00 .00 .00 89.10 91.14 724 WASH 1.70 88.44 9.95 2.83 28.00 59.22 6983.00 95.84 96.38 725 WASH 1.70 86.73 7.67 2.18 28.80 61.35 7346.00 100.62 101.69 726 RAW .00 .00 8.31 1.53 .00 .00 .00 107.24 110.08 727 RAW .00 .00 8.31 1.53 .00 .00 .00 107.24 110.08 727 RAW .00 .00 .18 1.52 .00 .00 .00 120.50 122.52 728 RAW .00 .00 15.90 1.41 .00 .00 .00 135.94 137.14 729 RAW .00 .00 15.19 1.27 .00</td><td>89.10 91.14 724 RAW .00 .00 15.17 1.48 .00 .00 .00 .46 89.10 91.14 724 WASH 1.70 88.44 9.95 2.83 28.00 59.22 6983.00 .48 95.84 96.38 725 WASH 1.70 86.73 7.67 2.18 28.80 61.35 7346.00 1.24 100.62 101.69 726 RAW .00 .00 8.31 1.53 .00 .00 .00 .00 1.24 100.62 101.69 726 WASH 1.70 88.12 7.74 1.02 28.59 62.65 7423.00 1.49 107.24 110.08 727 WASH 1.70 90.40 6.66 5.13 26.10 62.11 7236.00 .61 120.50 122.52 728 RAW .00 .00 15.90 1.41 .00 .00 .00 .53 135.94 137.14 729 RAW .00 .00 15.19 1.27 .00</td><td> 89.10</td></t<>	89.10 91.14 724 RAW .00 .00 89.10 91.14 724 WASH 1.70 88.44 95.84 96.38 725 RAW .00 .00 95.84 96.38 725 WASH 1.70 86.73 100.62 101.69 726 RAW .00 .00 100.62 101.69 726 WASH 1.70 88.12 107.24 110.08 727 RAW .00 .00 107.24 110.08 727 WASH 1.70 90.40 120.50 122.52 728 RAW .00 .00 120.50 122.52 728 WASH 1.70 86.92 135.94 137.14 729 RAW .00 .00 137.90 138.68 730 RAW .00 .00 137.90 138.68 730 WASH 1.70 93.13 147.80 148.60	89,10 91,14 724 RAW .00 .00 15,17 89,10 91,14 724 WASH 1,70 88,44 9,95 95,84 96,38 725 RAW .00 .00 13,57 95,84 96,38 725 WASH 1,70 86,73 7,67 100,62 101,69 726 RAW .00 .00 8,31 100,62 101,69 726 WASH 1,70 88,12 7,74 107,24 110,08 727 RAW .00 .00 11,88 107,24 110,08 727 WASH 1,70 90,40 6,66 120,50 122,52 728 RAW .00 .00 15,90 120,50 122,52 728 WASH 1,70 86,92 8,65 135,94 137,14 729 WASH 1,70 90,18 11,03 137,90 138,68 730 RAW .00	89,10 91,14 724 RAW .00 .00 15,17 1,48 89,10 91,14 724 WASH 1,70 88,44 9,95 2,83 95,84 96,38 725 WASH 1,70 86,73 7,67 2,18 100,62 101,69 726 RAW .00 .00 8,31 1,53 100,62 101,69 726 WASH 1,70 88,12 7,74 1,02 107,24 110,08 727 RAW .00 .00 11,88 1,52 107,24 110,08 727 WASH 1,70 90,40 6,66 5,13 120,50 122,52 728 RAW .00 .00 15,90 1,41 120,50 122,52 728 WASH 1,70 86,92 8,65 3,39 135,94 137,14 729 WASH 1,70 90,18 11,03 2,52 137,90 138,68 730	89.10 91.14 724 RAW .00 .00 15.17 1.48 .00 89.10 91.14 724 WASH 1.70 88.44 9.95 2.83 28.00 95.84 96.38 725 WASH 1.70 86.73 7.67 2.18 28.80 100.62 101.69 726 RAW .00 .00 8.31 1.53 .00 100.62 101.69 726 WASH 1.70 88.12 7.74 1.02 28.59 107.24 110.08 727 RAW .00 .00 11.88 1.52 .00 120.50 122.52 728 RAW .00 .00 15.90 1.41 .00 120.50 122.52 728 WASH 1.70 86.92 8.65 3.39 27.15 135.94 137.14 729 WASH 1.70 86.92 8.65 3.39 27.15 135.94 137.14 729<	89.10	89,10 91,14 724 RAW .00 .00 15.17 1.48 .00 .00 .00 89.10 91.14 724 WASH 1.70 88.44 9.95 2.83 28.00 59.22 6983.00 95.84 96.38 725 WASH 1.70 86.73 7.67 2.18 28.80 61.35 7346.00 100.62 101.69 726 RAW .00 .00 8.31 1.53 .00 .00 .00 107.24 110.08 727 RAW .00 .00 8.31 1.53 .00 .00 .00 107.24 110.08 727 RAW .00 .00 .18 1.52 .00 .00 .00 120.50 122.52 728 RAW .00 .00 15.90 1.41 .00 .00 .00 135.94 137.14 729 RAW .00 .00 15.19 1.27 .00	89.10 91.14 724 RAW .00 .00 15.17 1.48 .00 .00 .00 .46 89.10 91.14 724 WASH 1.70 88.44 9.95 2.83 28.00 59.22 6983.00 .48 95.84 96.38 725 WASH 1.70 86.73 7.67 2.18 28.80 61.35 7346.00 1.24 100.62 101.69 726 RAW .00 .00 8.31 1.53 .00 .00 .00 .00 1.24 100.62 101.69 726 WASH 1.70 88.12 7.74 1.02 28.59 62.65 7423.00 1.49 107.24 110.08 727 WASH 1.70 90.40 6.66 5.13 26.10 62.11 7236.00 .61 120.50 122.52 728 RAW .00 .00 15.90 1.41 .00 .00 .00 .53 135.94 137.14 729 RAW .00 .00 15.19 1.27 .00	89.10

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AM	332 TOP		SAMPLE		\$G	YIELD	A \$H	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
· ·	83.98	84.42	785	RAW	.00	.00	33.19	1.27	.00	.00	.00	3.30	-1.00	
	83.98	84.42		WASH	1,70	62.72	9.77	2.47	28.17		7198.00	3.45	-1.00	
	20 0 71	91.40		RAW	.00	.00	14.80	1.06	.00	.00	.00	3.47	-1.00	
	90.72	91.40	786	WASH	1.70	93.46	11.19	2.80	28.41	57.60	7061.00	2.76	-1.00	
	97.63	98.88	787	RAW	.00	.00	11.32	1.17	.00	.00	.00	2.19	-1.00	
	97.63	98.88		WASH	1.70	96.36	9.55	3.61	27.00		7141.00	.71	-1.00	
	108.55	109.74		RAW	.00	.00	15.82	1-01	. 00	.00	.00	3.58	-1.00	
•	108.55 110.20	109.74	788 780	WASH	1.70	85.34	8.27	3.25	29.37		7323.00	1.71	-1.00	
	110.20	110.64 110.64	789 789	RAW Wash	.00 1.70	.00 47.07	37.38 16.45	.71 3.37	.00 30.10	.00 50.08	.00 6410.00	3.10 2.11	-1.00 -1.00	
	111.20	110.64		RAW	.00	.00	11.51	1.13	.00	00.0	.00	1,63	-1.00	
	111.20	112.63		WASH	1.70	92.55	7.13	3.56	29.47	59.84	7355.00	1.41	-1.00	
	118.08	118.62		RAW	. 00	.00	36.04	1.00	.00	.00	.00	4.92	-1.00	
	118.08	118.62	791	WASH	1.70	62.88	21.04	2.70	23.31		6284.00	2.55	-1.00	
	119.12	121.20		RAW	.00	.00	20.64	1.10	.00	.00	.00	3.58	-1.00	
	119.12	121.20	792	WASH	1.70	83.41	12.10	4.02	24.66	59.22	6900.00	. 93	-1.00	
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TW830	0-333													
SEAM	TOP	BOT	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
10	36.56	37.08	771	RAW	.00	.00	11.86	1.06	.00	.00	.00	2.53	-1.QO	
10	36.56	37.08	77 1	WASH	1.70	96.77	10.67	. 95	30.41	57.97	7294.00	2.27	-1.00	
9	42.92	43.88	772	RAW	.00	.00	15.84	1.18	.00	.00	.00	4.31	-1.00	
9	42.92	43.88	772	WASH	1.70	88.71	10.35	1.40	33.46	54.79	7272.00	2.87	-1.00	
8	46.97	49.54	773	RAW	- 00	. 00	31.10	1.43	. 00	. 00	.00	3.65	-1.00	
8	46.97	49.54	773	WASH	1.70	64.15	10.23	1.62	29.89	58.26	7249.00	1.45	-1.00	
7	66.52	67.57	774	RAW	.00	.00	13.55	1.33	.00	. 00	00	1.78	-1.00	
7	66.52	67.57	774	WASH	1.70	92.40	9.53	. 1.50	30.40	58.57	7247.00	1.63	-1.00	
6	74.42	78.30	775	RAW	.00	.00	12.65	1.40	.00	.00	.00	. 86	-1.00	
6	74.42	78.30	775	WASH	1.70	89.33	7.28	2.19	30.40	60.13	7421.00	.77	-1-00	
6	80.18	82.76	776	RAW	.00	.00	14.02	1.42	.00	.00	.00	. 47	-1.00	
6	80.18	82.76	776	WASH	1.70	88.88	8.82	1.65	29.44	60.09	7272.00	. 49	-1.00	
6	84.32	85.52	777	RAW	.00	.00	15.33	1.32	, 00	.00	.00	3.19	-1.00	
6	84.32	85.52	777	WASH	1.70	81.48	4.81	2.27	29.17	63.75	7681.00	. 99	-1.00	
7	97.52	98.67	778	RAW	- 00	.00	15.62	1.12	. 00	.00	.00	2.54	-1.00	
7	97.52	98.67	778	WASH	1.70	87.05	9.28	1.98	30.48	58.26	7407.00	1.80	-1.00	
6	106.16	109.11	779	RAW	.00	.00	12.41	1.33	.00	.00	.00	. 92	-1.00	
6	106.16	109,11	779	WASH	1.70	89.07	6.75	2.93	28.48	61.84	7483.00	. 76	-1.00	
6	<u>_</u> 115.35	117.10	780	RAW	. 00	. 00	15.22	1.33	.00	.00	.00	. 42	-1.00	
6	115.35	117.10	780	WASH	1.70	90.05	10.28	2.86	28.58	58.28	7143.00	. 48	-1.00	
6	121.70	123.46	781	RAW	.00	.00	10.72	1.10	.00	.00	.00	1.25	-1.00	
6	121.70	123.46	781	WASH	1.70	90.15	6.72	2.42	29.58	61.28	7344.00	1.12	-1.00	
2	149.93	150.79	782	RAW	.00	.00	15.08	1.06	.00	.00	.00	. 89	-1.00	
2	149.93	150.79	782	WASH	1.70	91.66	10.56	3.69	26,59	59.16	7123.00	. 73	-1.00	
2	151.44	152.2 6	783	RAW	.00	.00	53.53	1.58	.00	.00	.00	2.63	-1.00	
2 ,	151.44	152.26	783	WASH	1.70	39.75	11.11	2.05	27.43	59.41	7184.00	1.04	-1.00	
2 \	154.49	154.80	784	RAW	.00	.00	37.25	1.12	.00	.00	.00	2.86	-1.00	<u>-</u>
2	154 49	154.80	784	WASH	1.70	65.69	21.24	2.02	28.28	48.46	6349.00	1.70	-1.00	

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TW83D-334

SEAM	TOP	BOT	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	ŞULF	F5I	
7	12.83	13.92	821	RAW	.00	.00	14.04	1.12	.00	.00	.00	4,14	-1.00	
7	12.83	13.92	821	WASH	1.70	86.03	7.84	1.81	35.02	55.33	7414.00	2.11	-1.00	
6	₹27.98	32.08	822	RAW	.00	.00	15.71	1.34	.00	.00	.00	1.98	-1.00	
6	27.98	32.08	822	WASH	1.70	87.49	9.17	2.20	29.30	59.33	7186.00	. 90	-1.00	
2	57.50	59.60	823	RAW	.00	.00	14.10	1.24	.00	.00	.00	2.03	~1.00	
2	> 57.50	59.60	823	WASH	1.70	86.89	7.75	3.47	29.18	59.60	7417.00	1.37	-1.00	
Q	77.94	78.12	824	RAW	.00	.00	25.34	1.29	.00	.00	.00	1.49	-1.00	
Q	77.94	78.12	824	WASH	1.70	73.13	11.00	1.68	29.43	57.89	7212.00	1.57	-1.00	
Q	78.38	78.96	825	RAW	.00	.00	16.92	1.56	.00	.00	.00	1.71	-1.00	
0	78.38	78.96	825	WASH	1.70	85.14	10.70	2.28	29.92	57.10	7236.00	1.58	-1.00	
6	82.18	82.81	826	RAW	.00	.00	18.37	1.30	.00	.00	.00	2.62	-1.00	
6	82.18	82.81	826	WASH	1.70	79.02	9.61	1.79	29.83	58.77	7281.00	2.08	-1.00	

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W83D	-335													
EAM	TOP	BOT	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
	11.10		604	DAW				0.00				4 77	-1.00	
		11.40	681	RAW	.00	.00	90.08	2.00	.00	.00	.00	1,77	• •	
_	11.10	11.40	681	WASH	1.70	.41	50.62	2.30	17.30	29.78	3451.00	1.39	-1.00	
<u>0</u>	11.40	11.90	682 682	WASH	1.70	.00 88.73	14.18 8.80	1.40	.00 31.54	.00 57.84	.00 7440.00	3.13 2.43	-1.00 -1.00	
U			683					1.82						
	11.90	12.20		RAW	.00	.00	85.86	1.71	.00	.00	.00	1.71	-1.00	
	11.90	12.20	683 684	WASH	1.70 .00	1.81	20.66	1.82	30.43	47.09	6393.00	3.14	-1.00	
	16.00	16.30 16.30	684	WASH	1.70	.00	, 78.66	1.76	24.63	44.84	.00 5613.00	4.58 2.71	-1.00 -1.00	
	16.02						_ 28.76	. 1.77						
	16.02	17.19 17.19	685 685	RAW	.00	.00 96.99	8.67 7.21	1.34	.00	.00	.00	1.87	-1.00	
	17.16	17.19	686	WASH RAW	1.70 .00	.00	83.98	1.68 2.09	34.68	56.43	7614.00	1.69	-1.00	
	17.16	·							.00	.00	.00	4.47	-1.00	
	18.00	17.46 18.30	686	WASH	1.70	1.80	30.58	2.08	29.58	37.76	5451.00	3.05	-1.00	
	18.00	18.30	687 687	RAW Wash	.00 1.70	.00 5.30	80.87 33.72	2.11 1.71	.00 20.77	.00	.00 5148.00	4.48	-1.00	
	18.32	-	688			_			-	43.80		4.31	-1.00	
	18.32	20.12	688	RAW WASH	1.70	.00 89.93	13.55 7.52	1.46 3.19	28.64	.00	7301.00	2.31	-1.00	
	~ 20.64	20.12	689	RAW	.00					60.65		1.25	-1.00	
					1.70	.00	91.41	1.30	.00	.00	.00	. 10	-1.00	
	20.64 240.99	20.94 41.29	689 690	WASH RAW	.00	1,96	14.48 89.23	1.72	31.58	52.22 .00	6917.00	1.00	-1.00	
	40.99	41.29	690	WASH	1.70	. 18	58.48	1.61	15.02	24.70	.00 2876.00	1.62	-1.00	
-	41.27		691	RAW	.00	.00	18.70	_	,00	.00		1.78	-1.00	
,	41.27	42.44 42.44	691	WASH		82.54	9.09	1.38			.00	4.18	-1.00	
		42.44	692	RAW	1.70 .00	.00	82.07	1.68 1.72	30.23 .00	59.00	7358.00	1.52	-1.00	
	42.40	42.70		WASH	1.70					.00	.00	. 69	-1.00	
	48.06		692	–		4.61	27.18	1.55	26.06	45.21	5823.00	1.56	-1.00	
	48.06	48.18 48.18	693 693	RAW Wash	.00 1.70	.00 1.83	84.90 10.20	1.69 1.58	.00	.00 57.49	.00	2.22	-1.00	
	48.35	50.56	694	RAW	,00	.00	22.61	1.49	30.73 .00	.00	7308.00 .00	1.52	-1.00	
	48.35	50.56	694	WASH	1.70	80.05	8.17	2.74	28.50	60.59		1.00	-1.00	
	50.56	50.86	695	RAW	.00	.00	87.26	1.62	.00	.00	7413.00 .00	. 67 . 05	-1.00 -1.00	
	50.56	50.86	695	WASH	1.70	.61	31.00	1.52	22.31	45.17	5466.00	.41	-1.00	
	58.24	58.57	696	RAW	.00	.00	78.79	.98	.00	.00	.00	.54	-1.00	
	58.24	58.57	696	WASH	1.70	.68	51.70	1.20	20.62	26.48	3260,00	. 73	-1.00	
	58.56	60.96	698	RAW	- 1.00	.00	87.70	1,54	.00	.00	.00	.60	-1.00	
•		60.96	698	WASH	1.70	.86	40.70	1.50	22.44	35.36	4606.00	1.08	-1.00	
	58.57	60.80	697	RAW	.00	.00	15.48	1.47	.00	.00	.00		-1.00	
	58.57	60.80	697	WASH	1.70	87.35	9.01	1.91	29.52	59.56	7266.00	. 56	-1.00	
	61.90	62.20	699	RAW	.00	-00	-86.92	1.68	,00	.00	.00	1.89	-1.00	
	61.90	62.20	699	WASH	1.70	, 14	19.95	1.52	28.14	50.39	6465.00	1.51	-1.00	
	62.31	62.98	700	RAW	.00	.00	32.86	1.39	.00	.00	.00	2.49	-1.00	
	62.31	62.98	700	WASH	1.70	62.23	10.77	2.48	28.25	58.50	7141.00	1.26	-1.00	
-	62.75	63.05	701	RAW	.00	.00	88.13	1.49	00	.00	.00	1.27	-1.00	
`	62.75	63.05	701	WASH	1.70	.99	32.94	1.77	25.24	40.05	5266.00	1.74	-1.00	
	 64.10	64.40	702	RAW	.00	.00	85.13	1.33	.00	.00	.00	3.95	-1.00	
	64.10	64.40	702	WASH	1.70	1.22	14.46	1.88	33.08	50.58	6835.00	4.04	-1.00	
	64.46	65.20	702	RAW	.00	.00	12.81	1.18	.00	.00	.00	3.02	-1.00	
	64.46	65.20	703	WASH	1.70	91.67	8.26	2.30	31.10	58.34	7736.00	2.55	-1.00	
	-65.00	65.30	719	RAW	.00	.00	89.17	1.72	-00	.00	.00	, 13	-1.00	
 I	65.00	65.30	719	WASH	1.70	1.93	39.46	1.66	23.21	35.67	4415.00	.82	-1.00	
	86.30	86.60	704	RAW	.00	.00	82.21	1.87	.00	.00	.00	4.29	-1.00	
,	86.30	86.60	704	WASH	1.70	1.13	14.74	2.16	28.26	54.84		1.55		
	86.71	90.46	704 705	RAW	-00	.00	19.48	1.29	.00	.00	6902.00 .00		-1.00	
 :	86.71	90.46	705	WASH	1.70	84,49	10.41					1.15	<u>-1.00</u>	
	→ 50./1	90.46	100	WASH	1.70	54,49	10.41	2.86	26.18	60.55	7289.00	. 92	-1.00	

			706	 Daul				0.45					4 00	
Ö.	90.25	90.55	706	RAW	.00 1.70	.00	85.51	2.15	.00	.00	.00	. 27	-1.00	
0	~ 90.25	90.55	70 6 71 6	WASH RAW		1.89	32.92	2.02	22.19	42.87	5214.00	. 59	-1.00	
0	95.90 95.90	96.20	716		1.70		80.62	2.30 1.52	.00	. 00	-00 5414.00	5.29	-1.00	
2	95.90 ~96.24	96.20 96.84	716 717	WASH RAW	.00	1.26	32.47 28.91	1.32	30.93 .00	35.08 .00	.00	1.09 1.96	-1.00 -1.00	
2	96.24	96.84	717	WASH	1.70	73,24	16.82	1.56	27.87	53.75	6825.00	1.71	-1.00	
	96.70		7 1 8	RAW	.00	.00	75.47	2.27	.00	.00	.00	1./I .86	-1.00	
Q	96.70	97.00 97.00	718	WASH	1.70	13.41	26.46	1.71	24.52	47.31	5897.00	1.34	-1.00	-
ů,	 98.50	98.80	707	RAW	.00	.00	84.28	2.38	.00	.00	.00	2.47	-1.00	
Ò	98.50	98.80	707	WASH	1.70	1,19	29.78	1.88	24.64	43.70	5504.00	2.45	~1.00	
2	98.75	99.60	708	RAW	.00	.00	20.41	1.31	.00	.00	.00	1.32	-1.00	
2	98.75	99,60	708	WASH	1.70	82.75	10.20	1.90	30.72	57.18	7098.00	1.03	-1.00	
Q	> 99.38	99.68	709	RAW	.00	.00	82.17	1.71	.00	.00	.00	2.09	-1.00	
Ö	99.38	99.68	709	WASH	1.70	2.69	22.28	1.88	28.43	47.41	6163.00	1.77	-1.00	
Õ	100.00	100.30	710	RAW	.00	.00	78.58	1.69	.00	-00	.00	2.48	-1.00	
Ö	100.00	100.30	710	WASH	1.70	4.45	22.48	2.11	25.28	50.13	6196,00	1.08	-1.00	
2	100.27	101.35	711	RAW	.00	.00	16.08	1.41	.00	.00	.00	1.29	-1.00	
2	₹00.27	101.35	711	WASH	1.70	85.36	8.37	2.21	30.18	59.24	7455.00	.84	-1.00	
0 /	101.10	101.40	712	RAW	-00	.00	79.65	1.92	.00	.00	.00	2.34	-1.00	
رُ	101.10	101.40	712	WASH	.00	.00	22.65	1.59	-22.31/	53.45	.00	2.60	-1.00	
ر o	7 101.10	101.40	712 &	RAW	.00	.00	_ 79.65	- 1.92	.00	.00	.00	2.34	-1.00	
Q (/ 101.10	101.40	712/71	RAW	.00	.00	79.65	- 1 .92	.00_	.00	.00	2.34	-1.00	
਼	ጟ 101.10	101.40	712/71	WA5H	1.70	4.47	7 22.65	~ 1.59	22.31	53.45	-6183.00	2.60	-1.00	
Ź	<u>- 101.66</u>	102.13	714	RAW	.00	.00	17.28	1.61	.00	.00	.00	1.11	-1.00	
2	101.66	102.13	714	WASH	1.70	88.77	11.10	2.61	25.60	60.69	7123.00	. 86	-1.00	
Q	102.10	102.40	715	RAW	.00	.00	83.49	1.45	.00	.00	.00	. 46	-1.00	
Q	~ 102.10	102.40	715	WASH	1.70	4.81	22.18	1.88	27.60	48.34	6235.00	1.04	-1.00	
•						•	· · · · · · · · · · · · · · · · · · ·							

TW83D Seam	TOP	BOT	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FŞI	
Q	~ 57.48	57.62	666	RAW	. 00	.00	87.82	1.00	.00	.00	.00	. 20	-1.00	
Q	57.48	57. 6 2	666	WASH	1.70	1.08	30.28	2.24	24.19	43.29	5480.00	. 60	-1.00	
3	58.72	59.05	667	RAW	.00	.00	26.80	. 95	.00	.00	.00	1.00	-1.00	
3	58.72	59.Q5	667	WASH	1.70	64.64	11.71	2.30	30.30	55.69	7100.00	1.00	-1.00	
`	59.05	59.35	668	WASH	1.70	3.92	13.62	2.06	29.33	54.99	6946.00	1.53	-1.00	
Q	59.05	59.35	668	RAW	.00	. 00	86.21	- 1.07	.00	.00	. 00	. 96	-1.00	
Q	60.24	60.54	669 🛥	RAW	.00	.00	60.85	1.06	.00	.00	.00	7.71	-1-00	
Q	60.24	60.54	669	WASH	1.70	16.12	33.08	2.07	24.54	40.31	5222.00	1.93	-1.00	
3	60.54	61.95	670	RAW	.00	.00	67.93	1.28	.00	.00	.00	3.13	-1.00	
3	60.54	61.95	670	WASH	1.70	12.61	27.47	1.88	25.40	45.25	5638.00	1.75	-1.00	
Q	~ 61.95	62.25	671	RAW	00	.00	89.77	1 <u>17</u>	.00	.00	.00	. 5 1	-1.00	
Q	61.95	62.25	671	WASH	1.70	. 68	5.56	1.38	18.30	74.75	7904.00	1.20	-1.00	
)	े 67.09	67.39	672	RAW	.00	.00	87.12	1.36	.00	.00	.00	. 33	-1.00	
Q	67.09	67.39	672	WASH	1.70	. 68	29.60	2,16	25.27	42.97	5390.00	1.10	-1.00	
2	 67.39	68.04	673	RAW	.00	.00	47.08	1.24	- 00	.00	.00	. 55	-1.00	
2	67.39	68.04	673	WASH	1.70	49.68	16.36	3.18	25.23	55.23	6681.00	. 65	-1.00	
٥	68.04	68.34	674	RAW	.00	.00	83.06	1.75	.00	. 00	.00	- 07	~1.00	
Q	68.04	68.34	674	WASH	1.70	2.61	26.31	1.95	23.74	47.99	5836.00	. 45	-1.00	
<u> </u>	68.34	68.65	675	RAW	.00	.00	86.32	1.72	.00	.00		. 12	-1.00	
Q	68.34	68.65	675	WASH	1.70	.91	6.88	2.38	29.38	61.36	7594.00	. 66	-1.00	
2	68.65	69.14	676	RAW	.00	.00	31.89	1.40	.00	.00	.00	. 35	-1.00	
2	68.65	69.14	676	WASH	1.70	71.13	17.14	3.92	24.39	54.55	6419.00	. 36	-1.00	
	69.14	69.44	677	RAW	- 00	.00	89.43	1.85	.00	.00	. 00	. 26	-1.00	
ο,	69.14	69.44	677	WASH	1.70	. 67	36.84	2.00	21.05	40.11	4903.00	1.14	-1.00	
Q	69.69	70.09	678	RAW	.00	.00	86.24	1.79	.00	.00	.00	2.19	-1.00	
Q.	69.69	70.09	678	WASH	1.70	. 69	35.26	2.18	23.70	38.86	5058.00	2.62	-1.00	
<u> </u>	70.09	70.57	679	RAW	- 00	.00	21.65	1.52	.00	.00	. 00	1.41	-1.00	
2	70.09	70.57	679	WASH	1.70	87.97	16.37	2.57	26.22	54.84	6620.00	1.23	-1.00	
Q	70.57	70.87	680	RAW	.00	.00	89.69	2.07	.00	.00	.00	.08	-1.00	
Q	70.57	70.87	680	WASH	1.70	. 64	55.18	2.18	15.91	26.73	2986.00	. 32	-1.00	

Figure 4 at the Nation 9700 F

SEAM	TOP	BOT	SAMPLE	ATYP	5G	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
7	11.57	11.84	871	RAW	.00	.00	41.88	1.68	.00	.00	.00	1.69	-1.00	
Q	11.57	11.84	871	WASH	1.70	58.82	25.86	1.38	26.47	46.29	5876.00	2.31	-1.00	
Q.	12.68	13.55	872	RAW	.00	.00	52.03	1.64	.00	.00	.00	5.92	-1.00	
Q	12.68	13.55	872	WASH	1.70	31.69	26.77	2.49	24.97	45.77	5611.00	1.72	-1.00	
0	17.76	18.36	873	RAW	.00	.00	25.87	1.32	.00	.00	.00	1.98	-1.00	
Q	17.76	18.36	873	WASH	1.70	79.30	16.85	2.12	24.27	56.76	6600.00	1.29	-1.00	
Q	25.64	26.75	874	RAW	.00	.00	39.80	1.43	. 00	.00	.00	2.17	-1.00	
Ċ.	25.64	26.75	874	WASH	1.70	50.75	27.70	1.95	26.84	43.51	5693.00	1.62	-1.00	
2	38.44	88.88	875	RAW	.00	.00	68.50	1.29	.00	.00	.00	. 26	-1.00	
2	ે 88.44	88.88	875	WASH	1.70	19.70	28.57	2.11	22.97	46.35	5571.00	.61	-1.00	
2	> 89.07	89.40	876	RAW	.00	.00	41.12	1.25	.00	.00	.00	. 33	-1.00	
2	89.07	89.40	87 6	WASH	1.70	63.18	21.20	1.66	22.23	54.91	6268.00	. 43	-1.00	
2	90.62	91.11	877	RAW	.00	.00	33.25	1.45	.00	.00	.00	. 49	-1.00	
2	290.62	91.11	877	WASH	1.70	62.08	13.64	2.11	27.92	56.33	6906.00	. 46	-1.00	
2	91.63	92.24	878	RAW	.00	.00	26.26	1.44	.00	.00	.00	. 38	-1.00	
2	91.63	92.24	878	WASH	1.70	77.49	17.65	2.77	26.28	53.30	6484.00	. 41	-1.00	
2	9 3.44	93.96	879	RAW	.00	.00	19.28	1.33	.00	. 00	.00	1.40	-1.00	
2	~ 93.44	93.96	879	WASH	1.70	88.41	15.35	2.19	25.73	56.73	6795.00	1.29	-1.00	

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33D-338													
M TOP	BOT	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
69.48	70.54	807	RAW	.00	.00	12.46	1.49	.00	.00	.00	1.51	-1.00	
- 69.48	70.54	807	WASH	1.70	86.16	7.78	2.39	30.70	59.13	7425.00	.82	-1.00	
131.95	134.68	808	RAW	.00	.00	18,42	1.50	.00	.00	.00	. 76	-1.00	
∑131.95	134.68	808	WASH	1.70	85.45	9.31	5.13	26.57	58.99	6970.00	.82	-1.00	
<u>~</u> 146.95	247.88	809	RAW	.00	.00	24.80	1.01	.00	.00	.00	1.64	-1.00	
_ 146.95	247.88	809	WASH	1.70	71.42	12.77	2.84	27.46	56.93	6994.00	1.31	-1.00	
152.90	154.92	810	RAW	.00	. 00	17.67	1.20	. 00	.00	.00	1.75	-1.00	
~152.90	154.92	810	WASH	1.70	82.13	9.40	4.32	27.71	58.57	7142.00	. 65	-1.00	
7171.60	172.04	811	RAW	.00	. 00	32.58	. 85	.00	.00	.00	4.33	-1.00	
171.60	172.04	811	WA2H	1.70	61.98	19.49	1.97	27.80	50.74	6603.00	2.69	-1.00	
173.52	174.95	812	RAW	_,00	,00	12,42	. 93	.00	.00	.00	1.08	- 1 - 00	
173.52	174.95	812	WASH	1.70	94.38	10.35	3.45	26.69	59.51	7259.00	1.06	-1.00	
7 175.33	175.88	813	RAW	.00	.00	15.92	. 98	.00	.00	.00	1.17	-1.00	
175.33	175.88	813	WASH	1.70	84.93	10.70	2.94	24.95	61.41	7244.00	. 49	-1.00	
176.34	176.81	814	RAW	.00	.00	24.95	1.10	.00	.00	.00	1.47	-1.00	
176.34	176.81	814	WASH	1.70	73.49	14.43	2.89	25.48	57.20	6904.00	. 75	-1.00	
185.92	186.45	815	RAW	.00	.00	38.56	1.14	. QO	.00	.00	3.67	-1.00	
185.92	186.45	815	WASH	1.70	54.43	23.14	2.14	25.01	49.71	6199.00	1.24	-1.00	
<u>>187.70</u>	190.04	816	RAW	.00	.00	23.01	1.13	.00	.00	.00	1.10	-1.00	
<u>~</u> 187.70	190.04	816	WASH	1.70	75.43	13.16	4.06	26.08	56.70	6961.00	. 80	-1.00	
190.91	191.24	817	RAW	.00	.00	32.08	1.15	. 00	.00	.00	1.80	-1.00	
190.91	191.24	817	WASH	1.70	70.74	18.99	1.24	25.17	54.60	6481,00	1.69	-1.00	
191.79	192.14	818	RAW	.00	.00	36.37	. 94	.00	.00	.00	. 38	-1.00	
191.79	192.14	8 18	WASH	1.70	50.36	17.31	2.96	23.58	56.15	6747.00	. 44	-1.00	
194.29	194.61	819	RAW	.00	.00	26.83	1.13	.00	.00	.00	.97	-1.00	
194.29	194.61	819	WASH	1.70	78.10	18.23	2.75	23.24	55.78	6330.00	. 54	-1.00	
195.38	196.01	820	RAW	.00	.00	19.10	1.12	00	- 00	.00	.69	-1.00	
195.38	196.01	820	WASH	1.70	83.26	11.76	1.92	25.81	60.51	7201.00	. 78	-1.00	

rinted on the Xerox 970G E

EAM 	-339 TOP	BOT	SAMPLE	ATYP	SG 	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
,	14.43	15.74 15.74	793 793	RAW Wash	.00 1.70	.00. 81.38	23.16 14.32	1.02 2.86	.00 28.68	.00	.00	2.30	-1.00 -1.00	
	~ 29.70 ~ 29.70	30.40	794 794	RAW WASH	1.70	.00 94.08	8.9i 6.87	1.01	.00	.00 58.40	.00	3.21	-1.00	
	~40.55	41.64	795	RAW	.00	.00	20,33	1,14	31.59 .00	. 00	7353.00 .00	2.17 2.64	-1.00 -1.00	
	40.55 43.98	41.64 44.34	795 796	WASH RAW	1.70	85.56 .00	12.45 37.33	3.90 1.17	28.43	55.22 .00	6828.00 .00	1.60 7.63	-1.00 -1.00	
-	43.98	44.34 46.08	796 797	WASH RAW	1.70	55.41	17.25	2.44	25.69	54.62	6434.00	4.33	-1.00	
-	44.34	46.08	797	WASH	1.70	.00 77.65	24.94 11.89	1.19 2.67	.00 28.82	.00 56.62	.00 6923.00	2.12 1.47	-1.00 -1.00	
	63.56	66.23 66.23	798 798	RAW WASH	1.70	93.05	13.62	1.42 6.31	. <u>00</u> 25.38	.00 58.18	.00 6781.00		- <u>1.00</u> -1.00	
								7.0.	20.00	00.10	0701.00		1.00	
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	D-340	. 28 . 80 . 80 . 57 . 57 . 12 . 12	104.28	914 913 913 912 912 911	ATYP RAW WASH RAW WASH RAW WASH RAW WASH RAW WASH RAW	\$G 1.70 .00 1.70 .00 1.70 .00 1.70 .00	YIELD .00 83.42 .00 85.39 .00 56.66 .00 58.34 .00 85.61	ASH 20.49 14.44 21.53 16.35 41.50 21.00 40.92 18.60 14.59 8.36	RESMOIST 1.07 1.28 .94 1.71 1.00 1.38 .93 .93 .92 .70	VOL .00 26.70 .00 26.08 .00 27.18 .00 25.12 .00 28.05	.00 55.86 .00 50.44 .00 55.35	KCAL	SULF 3.57 .48 .45 .33 .42 .57 .41 .55 3.91	FSI -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00	

TW83E	0-342													
SEAM	TOP	BOT	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
10	<u></u> 43.08	44.16	799	RAW	.00	.00	17.45	1.03	.00	.00	.00	3.30	-1.00	
10	43.08	44.16	799	WASH	1.70	82.49	8.43	2.11	31.96	57.50	7473.00	2.45	-1.00	
9	57.30	58.70	800	RAW	.00	.00	26.40	1.13	.00	.00	.00	4.72	-1.00	
9	57.30	58.70	800	WASH	1.70	67.93	8.36	1.60	32.86	57.18	7528.QO	1.62	-1.00	
8	- 61.33	64.28	801	RAW	.00	.00	14.20	1.45	.00	.00	.00	2.56	-1.00	
8	61.33	64.28	801	WASH	1.70	86.03	8.68	1.97	27.74	61.61	7362.00	1.28	-1.00	
7	172.49	74.07	802	RAW	.00	.00	14.27	1.28	.00	.00	.00	45	-1.00	
7	72.49	74.07	802	WASH	1.70	87.81	9.06	1.93	29.33	59.68	7345.00	43	-1.00	
5	81.66	84.91	803	RAW	.00	.00	14.49	1.35	.00	.00	.00	. 52	-1.00	
5	81.66	84.91	803	WASH	1.70	86.32	7.49	2.28	28.59	61.64	7471.00	.38	-1.00	
4	88.79	~90.50	804	RAW	.00	.00	8.27	1.40	.00	.00	.00	. 58	-1.00	
4	88.79	90.50	804	WASH	1.70	89.94	3.97	2.16	28.80	65.07	7794.00	. 56	-1.00	
3	~ 97 . 40	99.10	805	RAW	.00	.00	19.35	1.24	.00	.00	.00	. 45	-1.00	
3	97.40	99.10	805	WASH	1.70	81.59	11.18	1.73	28.09	59,00	7159.00	.46	-1.00	
2	~√ 101.32	101.90	806	RAW	.00	.00	21.74	1.40	.00	.00	.00	1.38	-1.00	
2	101.32	101.90	806	WASH	1.70	77,14	8.06	2.76	26.91	62.27	7395.00	. 76	-1.00	

Printed on the Xarox 9730 F.P.

SEAM	D-343 TOP	вот	SAMPLE	ATYP	SG	YIELD	ASH	DECMOTET	V01	0400	160.41			
						71660	ASIT	RESMOIST	VOL	CARB	KCAL	SULF	FSI 	
10	73.46	73.80	885	RAW	.00	.00	21,71	1.02	.00	.00	.00	9.34	~1.00	
10	73.46	73.80	885	WASH	1.70	74.16	11,47	1.71	31.64	55.18	7208.00	2.10	-1.00	
9	~75.27	75.60	886	RAW	.00	.00	27.11	1.24	.00	.00	.00	7.03	-1.00	
9	_ 75.27	75.60	886	WASH	1.70	66.38	10.61	1.54	30.22	57.53	7274.00	2.60	-1.00	
8	76.24	78.48	887	RAW	.00	.00	12.18	1.37	.00	.00	.00	1.55	-1.00	
8	76.24	78.48	887	WASH	1.70	90.28	8.56	1.91	28.70	60.83	7350.00	1.10	-1.00	
7	39.86	91.18	888	RAW	.00	.00	16.84	1.16	.00	.00	.00	2.17	-1.00	
7	89.86	91.18	888	WASH	1.70	80.00	9.55	1,40	30.03	59.02	7310.00	i 36	-1.00	—
7	~94.60	94.65	889	RAW	.00	.00	21.09	1.42	.00	.00	.00	1.15	-1.00	
7	94.60	94.65	889	WASH	1.70	82.40	12.83	2.22	27.94	57.01	6986.00	1,10	-1.00	
7	96.24	97.32	890	RAW	-00	.00	9.68	1.30	.00	.00	.00	.61	-1.00	
7	96.24	97.32	890	WASH	1.70	94.27	8.15	1.09	29.34	61.42	7462.00	.59	- 1 , 00	
6	102.30	105.12	891	RAW	.00	. 00	13.24	1.31	.00	.00	.00	. 46	-1.00	
6	102.30	105.12	891	WASH	1.70	87.33	7.91	1.30	29.17	61.62	7489.00	. 48	-1.00	
6	106.67	108.09	892	RAW	.00	.00	10.96	1.23	.00	.00	.00	. 85	-1,00	
6	106.67	108.09	892	WASH	1.70	92.85	8.09	2.70	29.77	59.44	7389.00	.71	-1.00	
3	124.90	125.28	893	RAW	.00	. 00	24.68	1.26	.00	.00	.00	4.23	-1.00	
3	124.90	125.28	893	WASH	1.70	78.07	17.28	1.34	27.28	54.10	6735.00	2.42	-1.00	
3	126.14	127.16	894	RAW	.00	. 00	19.21	.91	.00	.00	,00	. 76	-1.00	
3	126.14	127.16	894	WASH	1.70	89.25	13.97	3.71	25.49	56.83	6848.00	.65	-1.00	
3	127.69	128.04	895	RAW	.00	. 00	15.03	. 95	.00	.00	.00	1.16	-1.00	
3	127.69	128.04	895	WASH	1.70	92.47	11.02	2.35	25.82	60.81	7246.00	.86	-1.00	
2	139.05	140.05	896	RAW	.00	. 00	8.15	1.00	.00	.00	.00	.45	-1.00	
2	39.Q5	140.05	896	WASH	1.70	96.65	6.92	3.55	26.62	62.91	7466.00	. 45	-1.00	
2	140.86	141.20	900	RAW	- 00	, 00	22.21	1.00	.00	.00	.00	.42	-1.00	
2	140.85	141.20	900	WASH	1.70	87.48	18.43	1.91	23,00	56.66	6594.00	. 43	-1.00	
Q	142.62	142.92	897	RAW	.00	.00	30.82	1.01	- 00	.00	.00	. 34	-1.00	
Q	142.62	142.92	897	WASH	1.70	73.55	20.09	1.97	22.33	55.61	6325.00	. 39	-1,00	
2	्रे 144.01	144.58	898	RAW	.00	.00	19.34	1.02	.00	.00	.00	2.06	-1.00	
2	144.01	144.58	898	WASH	1.70	88.55	13.97	2.36	26.70	56.97	7062.00	1.50	-1.00	

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SEAN	# TOP	BOT	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL_	CARB	KCAL	SULF	FSI	
9	62.00	63.12	901	RAW	.00	.00	9.45	1.12	.00	.00	.00	2.78	-1.00	
9	€ 62.00	63.12	901	WASH	1.70	92.83	7.18	, 1.04	32.93	58.85	7692.00	1.68	-1.00	
8	64.58	65.70	902	RAW	.00	.00	13.14	1.36	.00	.00	.00	1.87	- 1 . 00	1
8	64.58	65.70	902	WASH	1.70	92.64	8.12	. 65	_30.96	60.27	7536.00	1.24	-1.00	
7	≥85.21	87.29	903	RAW	.00	.00	14.30	1.39	.00	.00	.00	.61	-1.00	
7	_ 85.21	87.29	903	WASH	1.70	91.23	8.64	. 7 1	29.33	61.32	7469.00	.42	-1.00	
6	94.74	95.Q5	904	RAW	. 00	.00	11.73	1.36	.00	.00	.00	. 60	-1.00	
6	94.74	95.05	904	WASH	1.70	91.51	8.10	1,17	28.18	62.55	7462.00	. 56	-1.00	
6	95.15	96.94	905	RAW	.00	.00	29.91	1.11	.00	.00	.00	2.47	-1.00	i
6	2 95.15	96.94	905	WASH	1.70	67.66	11.93	1.09	28.18	58.80	7209.00	1.18	-1.00	
3	~, 111.96	112.60	906	RAW	.00	.00	22.76	1.16	.00	.00	.00	.51	-1.00	
3	111.96	112.60	906	WASH	1.70	81.54	16.84	1.07	25.82	56.27	6745.00	.57	-1.00	
3	112.88	113.50	9Q8	RAW	.00	.00	27.57	1.21	. 00	.00	.00	1.88	-1.00	
3	112.88	113.50	908	WASH	1.70	69.65	12.61	. 56	27.70	59.13	7213.00	1.31	-1.00	
2	№ 119.12	119.72	907	RAW	.00	.00	12.88	1.42	.00	.00	.00	. 52	-1.00	1
2	119.12	119.72	907	WASH	1.70	87.38	8.77	.66	29.15	61.42	7441.00	.57	-1.00	
2	_ 121.42	121.64	909	RAW	.00	. 00	37.77	1.37	.00	.00	.00	. 58	-1.00	j
2	121.42	121.64	909	WASH	1.70	59.97	21.48	. 88	23.87	53.77	6299.00	. 52	-1.00	
2	122.43	123.52	910	RAW	.00	.00	19.50	. 90	.00	.00	.00	. 79	-1.00	ļ
2	122.43	123.52	910	WASH	1.70	82.23	14.27	. 94	27.97	56.82	6968.00	. 77	-1.00	
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TOP	вот	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	<u>-</u>
							4 07						
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									•				
43.60													
43.60		843	WASH										
50.12	51.25	844	RAW	.00		·							
5 0.12	51.25	844	WASH	1.70									
→ 51.60	52.38	845	RAW	.00	.00	_ 35.42	1.25						
~ 51.60	52.38	845	WASH	1.70	57.77	9.73							
> 58.20	58.76	846	RAW	. 00	.00	13.53	1.06	.00		.00			
58.20	58.76	846	WASH	1.70	89.96	6.32	2.06	21.75	69.87	7419.00			
59.31	59.84	847	RAW	.00	.00	12.48	1.27	.00	.00	.00			
 59.31	59.84	847	WASH	_ 1.70	86.39	5.78	1.55	26.71	65.96	7511.00	.64	-1.00	
50.01	61.93	848	RAW	.00	. 00	12.99	1,28	- 00	.00	.00	3.21		
~60.01	61.93	848	WASH	1.70	85.97	4.66	2.08	28.16	65.10	7577.00	. 90	-1.00	
	76.19	849	RAW	.00	.00	8.43	1.40	.00	.00	.00	. 65	-1.00	
	76.19	849	WASH	1.70	89.58	5.55	3.20	25.98	65.27	7371.00	. 63	-1.00	
		850	RAW	.00	.00	23.77	1.34	. 00	.00	.00	.73	-1.00	
				1.70	78.04	8.77	2.75	24.27	64.21	7096.00	.78	-1.00	
				.00	.00	17.88	1.31	.00	.00	.00	.43	-1.00	
			WASH	1.70	81.85	9.59	2.53	_ 25.10	62.78	7025.00	. 5 1	-1.00	
			RAW	.00	.00	- 25.29	. 98	.00	.00	.00	.36	-1.00	
				1.70	55.23	17.06	, 73	29.54	52.67	5857.00	. 44	-1.00	
				_	.00	27.05	1.37	.00	.00	. 00	2.32	-1.00	
				1.70	69.53	15.07	1.11	22.59	61.23	6790.00	1.69	-1.00	
						_	1.39	.00	.00	.00	1.64	-1.00	
							.91	25,21	60.77	6817.00	1.30	-1.00	
									_		. 95	-1.00	
-	-												
	38.56 38.56 38.56 42.58 42.58 43.60 43.60 50.12 50.12 51.60 51.60 58.20 59.31 59.31 59.31 59.31 50.01 75.26 76.85 76.85 82.83 82.83 83.76 96.00	38.56 39.64 38.56 39.64 42.58 43.38 42.58 43.38 42.58 43.38 43.60 45.20 43.60 45.20 50.12 51.25 50.12 51.25 51.60 52.38 51.60 52.38 58.20 58.76 58.20 58.76 59.31 59.84 59.31 59.84 60.01 61.93 75.26 76.19 75.26 76.19 75.26 76.19 76.85 78.20 76.85 78.20 76.85 78.20 82.83 83.33 83.76 83.92 96.00 96.35 96.00 96.35 96.00 96.35 100.54 102.62 100.54 102.62	38.56 39.64 841 38.56 39.64 841 42.58 43.38 842 42.58 43.38 842 43.60 45.20 843 43.60 45.20 843 50.12 51.25 844 51.60 52.38 845 51.60 52.38 845 58.20 58.76 846 59.31 59.84 847 59.31 59.84 847 59.31 59.84 847 60.01 61.93 848 60.01 61.93 848 75.26 76.19 849 75.26 76.85 78.20 850 850 82.83 83.33 851 83.76 83.92 852 852 83.76 83.92 852 852 853 96.00 96.35 853 96.00 96	38.56 39.64 841 RAW 38.56 39.64 841 WASH 42.58 43.38 842 WASH 43.60 45.20 843 WASH 50.12 51.25 844 RAW 50.12 51.25 844 WASH 51.60 52.38 845 WASH 51.60 52.38 845 WASH 58.20 58.76 846 WASH 59.31 59.84 847 RAW 59.31 59.84 847 RAW 59.31 59.84 847 RAW 59.31 59.84 847 WASH 60.01 61.93 848 RAW 60.01 61.93 848 RAW 75.26 76.19 849 WASH 75.26 76.19 849 WASH 75.26 76.19 849 WASH 75.26 76.19 849 WASH 75.26 76.19 849 WASH 75.26 76.19 849 WASH 75.26 76.19 849 WASH 75.26 76.19 849 WASH 83.76 83.92 852 RAW 82.83 83.33 851 RAW 82.83 83.33 851 RAW 82.83 83.33 851 RAW 83.76 83.92 852 RAW 96.00 96.35 853 RAW 96.00 96.35 853 RAW 96.00 96.35 853 RAW	38.56 39.64 841 RAW .00 38.56 39.64 841 WASH 1.70 42.58 43.38 842 RAW .00 42.58 43.38 842 WASH 1.70 43.60 45.20 843 WASH 1.70 50.12 51.25 844 RAW .00 50.12 51.25 844 RAW .00 50.12 51.25 844 WASH 1.70 51.60 52.38 845 RAW .00 51.60 52.38 845 RAW .00 51.60 52.38 845 RAW .00 51.60 52.38 845 RAW .00 59.31 59.84 847 RAW .00 59.31 59.84 847 RAW .00 59.31 59.84 847 WASH 1.70 60.01 61.93 848 RAW .00 60.01 61.93 848 RAW .00 60.01 61.93 848 RAW .00 75.26 76.19 849 RAW .00 75.26 76.19 849 WASH 1.70 76.85 78.20 850 WASH 1.70 76.85 78.20 850 RAW .00 76.85 78.20 850 RAW .00 82.83 83.33 851 RAW .00 82.83 83.33 851 RAW .00 82.83 83.33 851 RAW .00 82.83 83.33 851 RAW .00 83.76 83.92 852 RAW .00 83.76 83.92 852 RAW .00 96.00 96.35 853 RAW .00 96.00 96.35 853 RAW .00	38.56	38.56	38.56	38.56 39.64 841 RAW .00 .00 14.29 1.27 .00 38.56 39.64 841 WASH 1.70 87.44 8.57 .59 26.88 42.58 43.38 842 WASH 1.70 69.55 12.82 1.30 25.06 43.60 45.20 843 WASH 1.70 89.36 6.76 89 26.83 50.12 51.25 844 WASH 1.70 89.36 6.76 89 26.83 50.12 51.25 844 WASH 1.70 89.36 6.76 89 26.83 50.12 51.25 844 WASH 1.70 87.71 8.42 1.33 28.26 51.60 52.38 845 WASH 1.70 87.71 8.42 1.33 28.26 51.60 52.38 845 WASH 1.70 87.71 8.42 1.33 28.26 51.60 52.38 845 WASH 1.70 87.71 8.42 1.33 28.26 51.60 52.38 845 WASH 1.70 57.77 9.73 1.67 27.05 58.20 58.76 846 WASH 1.70 87.71 8.42 1.25 .00 59.31 59.84 847 WASH 1.70 89.96 6.32 2.06 21.75 59.31 59.84 847 WASH 1.70 89.96 6.32 2.06 21.75 59.31 59.84 847 WASH 1.70 89.96 6.32 2.06 21.75 60.01 61.93 848 WASH 1.70 86.39 5.78 1.55 26.71 60.01 61.93 848 WASH 1.70 86.39 5.78 1.55 26.71 60.01 61.93 848 WASH 1.70 89.96 6.32 2.06 20.82 8.16 60.01 61.93 848 WASH 1.70 89.58 5.55 3.20 25.98 76.85 78.20 850 WASH 1.70 89.58 5.55 3.20 25.98 76.85 78.20 850 WASH 1.70 89.58 5.55 3.20 25.98 76.85 78.20 850 WASH 1.70 89.58 5.55 3.20 25.98 76.85 78.20 850 WASH 1.70 89.58 5.55 3.20 25.98 76.85 78.20 850 WASH 1.70 89.58 5.55 3.20 25.98 76.85 78.20 850 WASH 1.70 89.58 5.55 3.20 25.98 76.85 78.20 850 WASH 1.70 89.58 5.55 3.20 25.98 76.85 78.20 850 WASH 1.70 89.58 5.55 3.20 25.98 76.85 78.20 850 WASH 1.70 89.58 5.55 3.20 25.98 76.85 78.20 850 WASH 1.70 89.58 5.55 3.20 25.98 76.85 78.20 850 WASH 1.70 89.58 5.55 3.20 25.98 76.85 78.20 850 WASH 1.70 89.58 5.55 3.20 25.98 76.85 78.20 850 WASH 1.70 89.58 5.55 3.20 25.98 76.85 78.20 850 WASH 1.70 89.58 5.55 3.20 25.98 76.85 78.20 850 WASH 1.70 89.58 5.55 3.20 25.98 76.85 78.20 850 WASH 1.70 89.58 5.55 3.20 25.99 76.85 78.20 850 WASH 1.70 89.58 5.55 3.20 25.95 7	38.56 39.64 841 RAW	38.56 39.64 841 RAW	38.56 39.64 841 RAW	38.56 39.64 841 RAW

PAGE 117							•							
TW83D-347 SEAM TOP	BOT S	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI		
5L 25.30 6L 25.30 6L 30.63	30.48 8 30.48 8 30.82 8	327 327 328	RAW WASH RAW	. 00 1 . 70 . 00	.00 95.92 .00	11.99 7.58 12.87	1.76 2.39 1.61	.00 26.92 .00	.00 63.11 .00	.00 7127,00 .00	1.41 1.00 .62	-1.00 -1.00 -1.00		
30.63 5L 31.01 6L 31.01 5L 31.36	30.82 8 31.15 8 31.15 8 32.52 8	329 330	WASH RAW WASH RAW WASH	1.70 .00 1.70 .00	91.09 .00 90.42 .00 92.29	7.23 -12.26 6.72 10.14 6.20	1.59 -1.59 1.29 1.90	26.85 .00 26.30 .00	.00 65.69 .00	7392.00 .00 7522.00 .00 7413.00	.63 -68 .70 .78	-1.00 -1.00 -1.00 -1.00		
3 34.16 3 34.16 2 40.62 2 40.62	34.87 8 34.87 8 45.80 8	331 331 332	RAW WASH RAW WASH	.00 1.70 .00 1.70	.00 91.49 .00 90.11	7,12 3,11 7,38 6,67	1.59 1.31 <u>1.64</u> 2.39	.00 29.21 .00 26.09	.00 66.37 .00 64.85	.00 7825.00 .00 7479.00	.73 .74 .45	-1.00 -1.00 -1.00 -1.00		
Q 52.06 Q 52.06	52.54 8 52.54 8		RAW WASH		.00 87.35	13.06 7.72	1.49 1.66	.00		.00 7352.00	2.45 1.22	-1.00 -1.00		
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W83D-34 E <u>am</u>	TOP		SAMPLE		SG	AIEFD		RESMOI		CARB	KCAL	SULF	FSI	
·	20.48	124.15	867	RAW	.00	.00	33.91	1.		.00	.00	2.93	-1.00	
~ i		124.15		WASH	1.70	59.79	12.06	1.0		59.62		.35	-1.00	
	25.28	126.07	868	RAW	.00	.00	18.33	_ (00	.00	1.78	-1.00	
_ 1		126.07		WASH	1.70	84.36	10.08	. 9		61.88		1.46	-1.00	
	26.48	127.04		RAW	.00	.00	_26.91	1.0		.00	.00	1.35	-1.00	
	26.48 28.13	127.04 129.45		WASH Raw	1.70 .00	77.61 .00	18.07 20.23	1.0			6588.00	1.03	-1.00	
	28 13	129.45		WASH	1.70	89.85	16.85	1 1.:		.00	.00	.45	-1.00	
	20.10	123.43	0,0	WAS!!	1.70	65.65	10.03	- '	23.73	50.50	0383.00	. 40	7.00	
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TW831	D-351												
SEAM	TOP	BOT	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	F\$I
3	17.21	17.81	835	RAW	.00	.00	29.43	1.06	.00	.00	.00	1.61	-1.00
3	17.21	17.81	835	WASH	1.70	69.26	20.51	1.79	24.49	53.21	6488.00	1.56	-1.00
3 .	18.46	19.76	836	RAW	.00	.00	16.89	1.02	.00	.00	.00	. 78	-1.00
3	18.46	19.76	836	WASH	1.70	85.52	9.30	2.71	27.47	60.52	7283.00	.72	-1.00
2		24.12	837	RAW	.00	.00	27.71	1.09	.00	.00	.00	2.45	-1.00
2	23.08	24.12	837	WASH	1.70	62.07	11.03	1.41	28.46	59.10	7283.00	1.50	-1.00
2	~25.20	26.48	838	RAW	.00	.00	10.57	1.21	.00	.00	.00	. 59	-1.00
2	25.20	26.48	838	WASH	1.70	88.01	6.50	2,75	29.40	61.35	7538.00	. 47	-1.00
2	- 26.98	28.14	839	RAW	.00	.00	15.71	1.23	. 00	.00	. 00	. 55	-1.00
2	~26.98	28.14	839 .	WASH	1.70	91.35	11.85	1.52	28.00	58.63	6875.00	. 50	-1.00
2	28.36	28.97	840	RAW	.00	.00	16.72	1.21	.00	.00	.00	. 97	-1.00
2	28.36	28.97	840	WASH	1.70	84.38	10.66	2.39	28.01	58.94	7221.00	. 84	-1.00

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	TOP	вот	SAMPLE	ATYP	5G	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
		47.00	050	DAN				1 10				4 04		
. ~	16.44 16.44	17.29 17.29	85 6 856	RAW Wash	.00 1.70	.00 87.78	14.85 10.88	1.10 .90	.00 30.32	.00 57.90	.00 7019.00	4.91 2.39	-1,00 -1,00	
_	35.71	36.86	857	RAW	.00	.00	11.89	1,09	.00	.00	.00	2.25	-1.00	
	35.71	36.86	857	WASH	1.70	90.69	8.22	1,09	29.34	61.35	7301.00	1.28	-1.00	
	64 25	64.62	859	RAW	.00	.00	23.43	. 92	.00	.00	.00	2.20	-1.00	
	64.25	64.62		WASH	1.70	79.30	13.72	1.64	31.11	53.53	7049.00	1.98	-1.00	
-	~ 66.39	66.98	860	RAW	,00	.00	16.14	1.07	,00	.00	.00	2.08	-1.00	
	66.39	66.98		WASH	1.70	90.17	12.08	1.14	26.89	59.89	7072.00	1.63	-1.00	
	~ 71.49	72.56	861	RAW	.00	.00	11.46	1.06	.00	.00	.00	2.10	-1.00	
	- 71.49	72.56		WASH	1.70	92.59	8.15	1.31	29.40	61.14	7520.00	1.55	-1.00	
	~ 79.09	81.91	862	RAW	-00	- 00	14.62	1.14	.00	.00	.00	.44	-1.00	
	79.09	81.91	862	WASH	1.70	86.14	7.97	.99	28.42	62.62	7432.00	48	-1.00	•
	82.88	84.65	863	RAW	.00	.00	10.88	1.04	.00	. 00	.00	1.04	-1.00	
-	82.88	84.65	863	WASH	1.70	91.07	7.37	1.37	29.38°	61.88	7442.00	. 53	-1.00	
	<u> </u>	102.32	864	RAW	.00	.00	29,96	1.01	.00	.00	.00	2.47	-1.00	
	101.32	102.32	864	WASH	1.70	67.68	16.07	-1.00	24.69	58.24	6827.00	1.51	-1.00	
	103.32	103.81	865	RAW	.00	.00	21.72	1.10	.00	.00	.00	. 99	-1.00	
	103.32	103.81	865	WASH	1.70	BO.70	16.33	. 99	25.25	57.43	6699.00	1.01	-1.00	
	→ 105.72	110.07	866	RAW	.00	.00	13,11	1.36	,00	.00	,00	.43	-1.00	
-	105.72	110.07	866	WASH	1.70	89.20	11.45	. 98	27.21	60.36	7043.00	. 43	-1.00	
_														

AGE 12	4						•								
W83D-357	TOP	ват	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	ŞULF	FSI		
6	9.04 9.04 11.76	70.28 70.28 82.82	916 916	RAW WASH RAW	-00 -1.70	.00	59.17 20.14 30.48	.94 1.58	.00 25.36	.00	.00 6512.00	1.03	-1.00 -1.00 -1.00		
8	11.76 13.92 13.92	82.82 84.44 84.44	917 918 918	WASH RAW Wash	-1.70 .00 -1.70	65.51 -00 94.49	15.32 14.93 11.77	1.10 ,76 1.00	.00 25.35 .00 28.09	58.23 .00 59.14	.00 6966.00 .00 7307.00	2.05 .77 .88 .86	-1.00 -1.00 -1.00	····	
~ 8	35.58 35.58 91.57	89.64 89.64 92.10 92.10	919 920	RAW WASH RAW Wash	-00 -1,70 -00 -1-70	.00 61.87 .00 60.08	36.38 19.10 47.32 31.02	.77 1.81 .69	.77 ² · 24 . 11 . 00	54.98 00	.00 6554.00 .00	.24	-1.00 -1.00 -1.00 -1.00		
		92.10		WASH	-1.70	60.08	31.02	1.26	21.40	46.32	5598.00	. 60	-1.00		
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AM	TOP	BOT	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
1,	13.50	14.42	926	RAW	.00	.00	42.08	. 72	.00	.00	.00	2.75	-1.00	
-	13.50	14.42	926	WASH	-1.70	62.91	12.77	1.52	26.99	58.72	7060.00	1.97	~1.00	
· >_	19.96	21.06	927	RAW	. 00	00	45.50		.00	.00	.00	4.98	-1.00	
_	19.96	21.06	927	WASH	-1.70	48.37	26.40	1.38	24.83	47.39	5808.00	2.78	-1.00	•
~ ~	50, 74	52.70	928	RAW	.00	.00	13.06	1.06	.00	.00	.00	1.35	-1.00	
	50.74	52.70	928	WASH	-1.70	95.07	10.27	2.56	26.55	60.62	7118.00	. 77	-1.00	
	76.29	77.89	929	RAW	.00	.00	20.90	1.21	.00	.00	.00	4.29	-1.00	
	76.29	77.89	929	WASH	-1.70	79.73	8.04	2.62	30.00	59.34	7372.00	1.44	-1.00	
_	90.07	90.62	930	RAW	.00	.00	26.52	.97	.00	.00	.00	1.93	-1.00	
	90.07	90.62	930	WASH	-1.70	76.21	11.65	1.77	27.82	58.76	7107.00	1.56	-1.00	
	93.77	93.92	931	RAW	.00	.00	40.85	. 88	.00	.00	.00	.86	-1.00	
_	93.77	93.92	931	WASH	-1.70	51.72	26.32	1.62	23.74	48.32	5846.00	1.14	-1.00	
	94.29	95.33	932	RAW	.00	. 00	16.66	.61	.00	.00	.00	. 96	-1.00	
_	94.29	95.33	932	WASH	-1.70	91.34	#11.93	1.01	28.84	58.22	7098.00	. 88	-1.00	
	<u>.95.67</u>	95.82	933	RAW	.00	.00	45.30	.57	.00	.00	.00	2.47	-1.00	
	95.67	95.82	933	WASH	-1.70	54.12	- 35.94	1.11	21.00	41.95	5058.00	2.44	-1.00	
~	125.10	125.57	934	RAW	.00	.00	22.35	. 65	.00	.00	.00	2.46	-1.00	
~	125.10	125.57	934	WASH	-1.70	88.09	14.88	1.25	28.47	55.40	6959.00	1.25	-1.00	
	125.83	126.76	935	RAW	.00	.00	15.24	. 67	.00	.00	.00	3.39	-1.00	
_	125.83	126.76	935	WASH	-1.70	87.68	8.78	. 83	31.08	59.31	7519.00	1.17	-1.00	
-	126.98	127.55	936	RAW	.00	. 00	30.88	.74	.00	-00	.00	. 87	-1.00	
	126.98	127.55	936	WASH	-1.70	64.99	16.58	1.11	27.58	54.73	6713.00	.85	-1.00	
-	136.05	136.40	937	RAW	.00	.00	18.06	. 66	.00	.00	.00	2.77	-1.00	
	136.Q5	136.40	937	WASH	- i . 7ō	89.79	15.58	1.07	28.98	54.37	6962,00	2 25	-1.00	
	137.97	139.35	938	RAW	.00	.00	20.50	. 75	.00	.00	.00		-1.00	
_	137.97	139.35	938	WASH	-1.70	81.67	13.31	1,19						
	137.97	139.35		938	938 RAW	938 RAW .00	938 RAW .00 .00	938 RAW .00 .00 20.50	938 RAW .00 .00 20.50 .75	938 RAW .00 .00 20.50 .75 .00	938 RAW .00 .00 20.50 .75 .00 .00	938 RAW .00 .00 20.50 .75 .00 .00 .00	938 RAW .00 .00 20.50 .75 .00 .00 .00 2.94	938 RAW .00 .00 20.50 .75 .00 .00 .00 2.94 -1.00

The Chick and the beautiful

PAGE 127 TW83D-361 SEAM TOP 1 56.43 1 57.10 1 67.10 1 69.05 1 71.17 1 71.17 1 72.40 1 90.55 1 90.55	BOT SAMPLE	ATYP RAW WASH RAW WASH RAW WASH RAW WASH RAW WASH RAW WASH	SG -1.70 .00 -1.70 .00 -1.70 .00 -1.70 .00 -1.70	YIELD 	ASH 14.95 12.08 41.01 19.98 21.34 13.47 14.95 11.69 32.52 21.55 37.12 26.55	RESMOIST .51 .87 .72 1.26 .57 .81 .56 .94 .70 1.27 .64	VOL 00 27.39 .00 24.53 .00 31.14 .00 27.49 .00 24.84 .00 22.64	.00 54.23 .00 54.58 .00 59.88 .00 52.34	KCAL .00 7301.00 .00 6443.00 .00 7186.00 .00 7311.00 .00 6332.00 .00 5824.00	SULF 1.01 .79 .33 .30 2.65 1.27 1.49 .59 .26 .30 .27	FSI -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00	•
						,						

	362 TOP		SAMPLE		ŞG	YIELD		RESMOIST	VOL	CARB	KCAL	SULF	FSI	
_	106.94	108.42	957	RAW	.00	.00	32.73	.81	-00	.00	.00	1.86	-1.00	
~~	106.94	108.42		WASH	-1.70	66.03	14.31	1,80	29.31		6916.00	1.54	-1.00	
	126.06 126.06	128.71	958	RAW WASH	.00 -1.70	93.23	12.75 9.32	. 86 1.69	.00 29.46	.00 59,53	7343.00	2,62 1,87	-1,00 -1,00	
_	149 29	150.49	959	RAW	.00	.00	21.04	.78	.00	.00	.00	2.49	-1.00	
_	149.29	150.49		WASH	-1.70	79.65	6.96	1.25	32.27		7617.00	1.69	-1.00	
	158.28 158.28	158.66 158.66	960	RAW WASH	.00 -1.70	.00 97.35	8.38 7.09	. 80 2.06	.00 29.96	.00 60.89	.00 7582.00	1.60	-1.00 -1.00	
-	158.88	159.28	961	RAW	.00	.00	27.39	90	.00	.00	.00	1.57	-1.00	
	158.88	159.28 160.67		WASH	-1.70	68.41	8.83	1.86	28.94		7419.00	1.00	-1.00	
	159.38 159.38	160.67		WASH	.00 -1.70	92.05	16.34	. <u>92</u> 2.87	.00 25.70	.00 58.96	.00 6972.00	1.72	-1.00 -1.00	
						02.00	(2),,	2.07	20.70	00.00	03.2.00		1.00	
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EAM	-363 T <u>OP</u>		SAMPLE		SG	YIELD		RESMOIST	VOL	CARB	KCAL	SULF	FSI	
 D	16.20	16.97	945	RAW	.00	.00	10.80	.66	.00	.00	.00	2.19	-1.00	
)	~ 16.20	16.97		WASH	-1.70	92.80	6.52	1.53	33.75	58.20	7661.00	1.83	-1.00	
-	24.80	25.32		RAW		.00	64.13	. 61	.00	00	.00	2.68	~1.00	
	24.80 56.50	25.32 59.24	946 947	WASH RAW	-1.70 .00	22.34 .00	23,54 45.54	1.54 .60	25.70 .00	49.22	6074.00 .00	3.24 .97	-1.00 -1.00	
	> 56.50	59.24	947	WASH	-1.70	46.97	21.61	1.69	24.14	52.56	6298.00	1.26	-1.00	
	67.47	69.58	948	RAW	- 00	.00	20.60	. 74	.00	.00	-00	1.77	-1.00	
	67.47	69.58	948	WASH	-1.70	93.72	17.40	1.65	25,28	55.67	6675.00	1.60	-1.00	
	80.84	82.68 82.68	949 949	RAW Wash	.00 -1.70	.00 92.84	20.91 16.47	1.17	.00	.00	.00	1.47	-1.00	
	90.40	96.20	950	RAW	.00	.00	18.12	2.67 1.76	27.76 .00	53.10 .00	6750.00 .00	1.26 .79	-1.00 -1.00	
	90.40	96.20	950	WASH	-1.70	81.62	7.16	2.26	28.07	62.51	7532.00	.58	-1.00	
	99.85	101.66		RAW	.00	.00	10.53	1.01	.00	.00	.00	.43	-1.00	
	99.85 118.90	101.66 120.20		WASH RAW	-1.70 .00	93.48 .00	7.67 56.27	1.61 1.17	27.81	62.91	7469.00	- 44	-1.00	
	- 118 .90	120.20		WASH	-1.70	39.96	15.69	2.97	.00 25.12	.00 56.22	-00 6804.00	. <u>4 1</u> . 52	-1.00 -1.00	
	121.78	123.77		RAW	. 00	.00	73.84	1.97	.00	.00	.00	. 27	-1.00	
	121.78	123.77	953	WASH	-1.70	7.86	32.20	1.67	22.48	43.65	5371.00	. 64	-1.00	
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<u> </u>	TOP	BOT			SG	YIELD	ASH		VOL	CARB	KCAL	SULF	FSI	
	74.03	75.13	968	RAW										
	74.03	75.13 75.13		WASH	.00 -1.70	.00 81.80	25.15 15.94	. 82 . 78	.00	.00	.00	2.23	-1.00	
	№ 81.17	81.51		RAW	- 1.70	.00	47.91	. 78	28.49	54.79		1.35	-1.00	
	~ 81.17	81.51		WASH	-1.70	44.43	28.87	.80	- <u>00</u> 22 - 67	.00 47.66	.00 5791.00	25 .31	-1.00 -1.00	
	91,19	91.70		RAW	.00	.00	53.73	.85	.00	.00	.00	.81	-1.00	
	- 91.19	91.70		WASH	-1.70	31,89	27.22	.83	25.25	46.70		.50	-1.00	
	94.30	97.75		RAW	.00	.00	40.87	.93	.00	.00	-00	.50	-1.00	
— `	94.30	97.75		WASH	-1.70	59.29	22.44	.92	25.47		6311.00	.71	-1.00	
	112.38		972	RAW	.00	.00	53.33	.87	.00	.00	.00	. 13	-1.00	
•	112.38	113.04		WASH	-1.70	35.19	30.51	1.49	20.90		5509.00	. 19	-1.00	
							-						7.00	
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<u>М</u> ЗD −:	369 TOP	вот	SAMPLE	ATYP	SG	YIELD	ASH	RESMOIST	VOL	CARB	KCAL	SULF	FSI	
~	38.42	39.54	963	RAW	.00	.00	19.65	. 95	.00	. 00	.00	1.23	~1.00	
~	38.42	39.54	963	WASH	-1.70	92.77	17.57	1.00	27.93	53.50	6982.00	1.13	-1.00	
_	44.85	45.26	964	RAW	.00	.00	31.46	- 90	.00	.00	.00	.39	-1.00	
	44.85	45.26	964	WASH	-1.70	76.25	19.40	1.24	25.86	53.50	6567.00	.40	-1.00	
_	~ 46.38	49.05	965	RAW	- 00	.00	27.51	.86	.00	.00	.00	. 59	-1.00	
_	46.38	49.05	965	WASH	-1.70	84.75	21.44	1.57	25.06	50.93	6325.00	. 58	-1-00	
	51.10	51.60	966	RAW	.00	.00	33.57	. 92	- 00	.00	.00	3.07	-1.00	
	51.10	51.60	966	WASH	-1.70	63.25	20.03	.80	28.28	50.89	6648.00	1.29	-1.00	
	60.84	61.35	967	RAW	.00	.00	45.66	1.08	.00	.00	.00	. 17	-1.00	
	60.84	61.35	967	WASH	-1.70	51,12	26.57	1.37	23.43	49.63	5880.00	.22	-1.00	
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TW-81D-112 GOBTHORN EAST

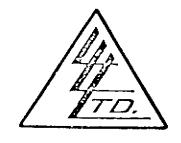
- RHEOLOGICAL
- ULTIMATE
- ASH ANALYSIS
- ASH FUSION

SAMPLE IDENTIFICATION

HOLE NO. TW81D-112

SAMPLE NUMBER	SEAM NAME
1001 1002 1003 1004 1005 1006 1007 1008 1009 1010 1011	10 1+2 9 3+7 8 5+6 7 7+8 6 7+10 5 11+12 4 13+14 3 2 5 4 3 3
1013 1014	2 .
81-1164+1165 81-1182 to 1185 81-1168+1169	8 3 6

To: CROWSNEST. RESOURCES LTD
525=3rd.AvenueS.W
Calgary, Alberta T2P 2M7
ATTN: T. Cole



File No. 23248-1

Date March 23, 1982

Samples Coal

P.O. # CN 20928

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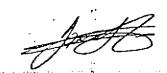
LORING LABORATORIES LTD.

Page # 1

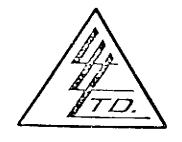
SAMPLE No.	GEISELER PLASTICITY TESTS							
				·				
				•				
				•				
	,				_			
"Clean Coal"	DDPM	START TEMP (°C)	M/ DDPM	AXIMUM TEMP (°C)	DDPM	RANGE TEMP (°C)	RANGI	
81-1164+1165	1	437	2	448	0	479	42	
81-1182-1185	1	430	. 8	448	0	478	48	
81-1168+1169	1	441	1	450	0	478	3 7	
		•						
				•				
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-						•		

Rejects Retained one month.

Pulps Retained one month
unless specific arrangements
made in advance.



Tor CROWSNEST, RESOURCES, LTD.,,
.5253rd.Avenue.S.W.
Calgary, Alberta T2P 2M7
ATTN: I. Cole



File No. 23248-1

Date March 23, 1982

Samples Coal

P.O. # CN 20928

Schifficator of

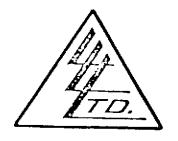
LORING LABORATORIES LTD.

Page # 2

SAMPLE No.		DTI	LATATION TEST		
				: - <u></u> -	·- <u>-</u> -
] ; [٠,		
		. 0			
"Clean Coal"	S.T. (°C)	M.D.T. (°C)	M.C. %	M.D. %	G. No.
81-1164+1165	368	-	23% @ 476°	-	-
81-1182-1185	374	_	20% @ 437°	-	-
81-1168+1169	386	-	15% @ 485°	-	-
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		eby Certify тнат	THE ABOVE RESULTS A	ARE THOSE	
		DE BY ME UPON THE HE			

Rejects Retained one month, Pulps Retained one month unless specific arrangements made in advance. JAK.

To:ckowsnesi	RESOURCES, LTD.
5253rd .Aver	ue S.W.
Calgary, Alber	ta T2P 2M7
	·
ATTN: T. Cole	<u>.</u>



File No. 23118-2

Date March 23, 1982

Samples Coal

P.O. # CN 20928

Sexificator ASSAY

LORING LABORATORIES LTD.

					Washes	J	
SAMPLE No.	% H2O	% C	% H	% N	% Ash	% S	% 0 (diff)
Comp -1.60 Flt							9.999
"Ultimate Analysis	<u>, '</u>		•				.777
"Air Dried"			•		•		,
TW-81D-112	· .				· •	•	
1001	₹ .90	70.85	4.08	.51	~12.14	1.78	9.74
1002	.77	. ~ 70.04	4.45	. 72	>9.05	2.44	12.53
1003	.98	72.37	4.40	.72	`8.29	1.35	11.89
1004	1.04	72.84	\4.55	.72	~8.02	1.36	11.47
1005	-2.09	√ 73.00	4.36	1.11	`6.19	.75	12.50
1006	1.57	73.50	\4.31	√ . 70	> 6.09-	.56	13.27
1007	1.72	₹74.50	√4.34	1.09	>5.33	.98	12.04
1008	1.45	\74.54	4.63	380	>5.24	.70	12.64
1009	1.40	74.66	>4.41	.79	- 5.62	.53	12.59
1010	1.19	72.71	~4.23 ~	➤.58	> 9.73	1.16	10.40
1011	1.21	72.36	~ 4.24	~.76	~ 10.31	×1.07	~10.05
1012	.86	65.29	4.25	.55	~ 16.49	. 1.67	10.89
1013	1.01	~71.96	~ 4.57	➤ .77	`9.29	.83	11.57
1014	1.17	74.50	4.58	69	~ 6.19	.64	12.23
	* Hyd	lrogen & Ox	ygen do	not includ	le H & O in	sample moist	ure.
		. () ~	2	-	ABOVE RESUL		
,	,	ASSAYS MADE	BY ME UPO	N THE HEREI	N DESCRIBED S	AMPLES	

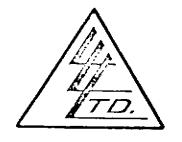
Rejects Retained one month, Pulps Retained one month unless specific arrangements made in advance, AR

To: CROWSNEST RESOURCES LTD.,

525 - 3rd Avenue S.W.,

Calgary, Alberta T2P 2M7

ATTN: T. Cole



File No. 23118-1

Date March 5, 1982

Samples Coal Ash

P.O. # CN 20928

Sextificato

LORING LABORATORIES LTD.

Page # 3

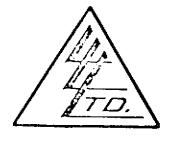
SAMPLE No.		TELKWA	1.60 FLT	
SAIVIFLE IVU.	1011	1013	1013	1014
	1 /4	,		. . •
nalysis of Ash"				
%				
Si 02	67.54	69.12	61.80	62.44
A1203	19.85	17.20	25.52	24.19
Ti 02	1.21	.93	2.08	1.80
Fe203	6.29	7.29	2.15	2.57
CaO	.98	.92	3.53	3.22
MgO	.28	.50	.53	.53
Na2O	.65	.59	.92	.84
к20	.18	.30	.30	.24
P205	∼ .49	∖ .02	\ 2.04	2.28
S03	.51	1.03	.84	.95
Undetermined	-2.02	-2.10	29	94
	II	jerchy Certify that	THE ABOVE RESULTS ARE THE	ROSE

Rejects Retained one month.

Pulps Retained one month unless specific arrangements made in advance.



Tof. CROWSNEST RESOURCES LTD.,
.525 - 3rd Avenue S.W.,
Calgary, Alberta T2P 2M7



File No. 23118-1

Date March 5, 1982

Samples Coal Ash

P.O. # CN 20928

ATTN: T. Cole

Servificate of

LORING LABORATORIES LTD.

Page # 2

SAMPLE No.			TELKWA 1.60 F		
SAMI LE 110.	1006	1007	1008	1009	1010
"Analysis of Ash"	5	4	2	9 2.*	5
%					
SiO2	61.28	58.82	56.76	57.34	64.32
A1203	31.57	18.52	28.54	29.30	20.41
Ti 02	2.06	.96	1.58	1.79	1.54
Fe203	.93	7.72	2.93	2.29	7.01
Ca0	.95	6.02	4.51	3.64	1.76
MgO	. 45	.99	.99	.90	-75
Na20	1.05	.92	.92	.92	.84
к20	. 36	.12	-24	.24	.18
P205	↓ .04	₺ 3.31	1.37	1.19	.31
S03	.65	2.55	2.33	2.26	1.62
Undetermined	66	07	+ .17	13	-1.26
			THAT THE ABOVE I		

Rejects Retained one month.

Pulps Retained one month
unless specific arrangements
made in advance.

Rub S. C.

Tot: CROWSNEST RESOURCES LTD.,.
525. = 3rd Avenue S.W.,.....
Calgary, Alberta T2P 2M7....

ATTN: T. Cole

ITD.

File No. 23118-1

Date March 5, 1982

Samples Coal Ash

P.O. # CN 20928

Sextificate ox

LORING LABORATORIES LTD.

Page # 1

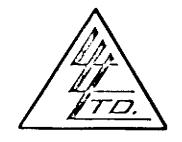
CALADI E M.			TELKWA 1.60 FI	T	
SAMPLE No.	1001	1002	1003	1004	1005
	1	T.	Ş	7	4
"Analysis of Ash"	ļ				
%					
Si02	67.46	51.32	50.72	59.72	60.96
A1203	12.49	16.64	26.46	22.68	27.60
Ti02	1.44	1.57	2.42	2.36	1.58
Fe203	9.72	21.16	9.72	8.15	2.36
CaO ,	2.94	2.52	2.94	1.74	1.99
MgO	.82	.86	1.33	.75	. •55
Na20	.57	.65	.92	.81	.97
к20	.24	.24	.30	.24	.42
P205	⋋ .02	.72	V.69	53. ا	1.17
S03	2.15	2.15	2.48	1.42	.82
Undetermined	-2.15	-2.17	-2.02	-1.60	-1.58
			THAT THE ABOVE F		
			THE HEREIN DESCRI		

Rejects Retained one month.
Pulps Retained one month
unless specific arrangements
made in advance.

relas of

Assayer

To: CROWSNEST RESOL	RCES LTD.,
525 - 3rd Avenue \$	S.W.,
Calgary, Alberta	T2P 2M7



File No. 23118

Date February 24, 1982

Samples Coal Ash

P.O. # CN 20928

ATIN: I. Cole

Sextificate ox

LORING LABORATORIES LTD.

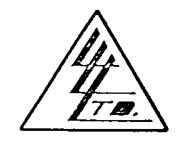
Page # 7

SAMPLE No.	I.D. (F ⁰)	OXIDIZING A H=W (F°)	TMOSPHERE H=½W (F ^O)	Fluid (F°)
h Fusion Analysis"	<u> </u>			
Clean Coal				
T'I-81D-112				
1001	2628	+2650	+2650	+2650
1002	2408	2533	+2650	+2650
1003	+2650	+2650	+2650	+2650
1004	+2650	+2650	+2650	+2650
1005	+2650	+2650	+2650	+2650
1006	+2650	+2650	+2650	+2650
1007	2368	2388	2418	2453
1008	2413	2448	2493	2573
1009	+2650	+2650	+2650	+2650
1010	+2650	+2650	+2650	+2650
1011	+2650	+2650	+2650	+2650
1012	+2650	+2650	+2650	+2650
1013	+2650	+2650	+2650	+2650
1014	+2650	+2650	+2650	+2650

Rejects Retained one month.

Pulps Retained one month unless specific arrangements made in advance.

TO B



File No. 23118

Date February 24, 1982

Samples Coal Ash

P.O. # CN 20928

Scrafficare ox

LORING LABORATORIES LTD.

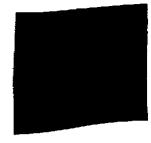
Page # 6

SAMPLE No.	I.D. (F°)	REDUC H=W (F°)	ING ATMOSPI	HERE	') 	Fluid (F	°)
sh Fusion Analysis"		•			,		
Clean Coal	lh,	14			.	4	
TW-81D-112	h,	Soft		i si		V .	
1001	2543 14956	2573	1411 c'	2603	1428 c°	+2650	1454
1002	2274 1945 -	2294	16560	2333	1278 c°	2388	1308
1003 T	2598 14252	+2650	1451/ 2"	+2650	1454 c	+2650	1454
1004	+2650 1454c	+2650	1454c°	+2650	14540	+2650	1454
1005	+2650 /036	+2650	raignes y	+2650	15500	+2650	1454
1006	+2650 14542	+2650	1426	+2650	1454 0	+2650	1454
1007	2294 18566	2308	126420	2413	132200	2443	1339
1008	2363 129500	2388	1808 0	2408	1320 c	2483	1361
1009	+2650 /035	+2650	4445°	+2650	1227 1 5	+2650	1454
1010	2643 1450 1	+2650	1 Wille	+2650	1000	+2650	1454
1011	+2650 // 4 /	+2650	1454 6	+2650		+2650	1054
1012	+2650 /### · ·	+2650	12 80 6	+2650	13000	+2650	
1013	+2650 /45 6	+2650	14301	+2650		+2650	17.
1014	+2650 1454	+2650	19.00 pt	+2650	West of	+2650	4, 12
	GL GC 4 1E	e c		DP#/// TO	ADE THOSE		
	I Hereby C assays made by m	CCIIID THE	AT THE ABOVE HEREIN DESCI	RESULTS RIBED SAN	IPLES	•	

Rejects Retained one month.

Pulps Retained one month
unless specific arrangements
made in advance.

ALL.



NQ CORE WASHABILITY

CONFIDENTIAL

CONTROL OF CHIS REST RESEARCES LIMITED FRO ECT TELYAR OCHE SARPLE NOS. 77 + 59.

HOLE NO. 237, SEAM &

LAS NO: 5340

DATE: 50% 28, 1983

AS RECEIVED SAMPLE ATTRITED FOR 2 MINUTES (DRY ATTRITION)
(MINUS 9.5MY AFTER 2 MINUTES ATTRITION = 34.7%)
PEAD RAW | B.G.I. = 57

SIZE & RAW AMALYSES

	GCTION	нтх	RHX	ASHZ	57 .	HTZ	ASH7.
19 X	im) + 19 + : 1.7+ : 0.3* : 0 +	50.30 35.80 9.80 4.10	1.90 1.70 2.30 2.40	16.90 19.60 17.70 22.60	 91 42 26 42 	50.30 86.10 95.90 100.00	16,90 18,02 17,99 18,18

LARGEST PARTICLE SIZE (+1955) = 70 KM LONG

FLOAT - SINY ARREYSIS, six dried basis: +1700			CUHULATI		
S.G. FRACTION	MTZ	ASHX	SI	HTX	ASHZ
FLCAT - 1.60 1.60 - 1.70 1.70 - 1.80 1.80 - SINK	64.80 3.90 NIL 11.30	9.30 37.10 — 67.10	0,93 0,53 0,90	84.80 89.70 88.70 100.00	9.30 10.52 10.52 16.92

FLOAT - SDBK AMALYSI	S, air dried	វ basis: 19ះមា	X 1.764	CUMUL	ATIVE
S.C. FRACTION	HTX	ASH7.	SI	жтх	ASHI
FLCAT - 1.60 1.60 - 1.70 1.70 - 1.60 1.80 - SINK	79.20 3.60 1.20 16.00	7.60 37.20 45.70 72.90	0.85 1.31 1.20 4.29	79.20 82.80 84.00 100.00	7,60 8,89 9,41 19,57

Birtley Coal & Minerals Testing

CODERT: CHO-S NUST RESOURCES LIBITED PROJECT: TELKMA DORE SATTLE NOS. 77 + 99.

HOLE NO. 237, SEAN &

LAS NO: 5340

DATE: 2008 28, 1983

FLOAT - SIPRI ARALY	SIS. air crie	o basis¦ 1.70°	1 X 0.5391		
(20.1)	,	CUAL.	ATIVE		
S.G. FRACTION	HTZ	ASHX	SX	HTX.	XH2A
FLGAT - 1.60	81.30	5,80	0.85	91.30	5.80
1.60 - 1.70	1,60	32,70	1.96	82.50	6.32
1.70 - 1.80	1.20	33,70	2.11	B4.10	6.78
1.90 - STW	15.90	74.50	3.02	100.00	17.55

FROTH-FLOTATIO	N IEST, as red	CUMLLATIVE			
FROODET	KTX	ASHIZ	S%	KTZ	AS+TA
STAGE I STAGE II TATLINGS	23.10 8.00 <i>6</i> 9.90	9 .10 20.60 26.80	0.81 1.64 1.63	23.10 31.10 100.00	9.10 12.06 22.22

PULP DE#SITY = 10% REAGENT/DDBASE = 4:1 = KERCSENE: HISC/0.50 LEVIDENE
COMPITIONING = 60 SECONDS
STACE I = FIRST MIMBLE FROTH
STAGE II = SECOND HINDTE FROTH

- + ANALYSIS ON AIR DRIED BASIS (ON COMPOSITE OF 5.6, FRACTIONS)
- * AMALYSIS ON AS RECEIVED PASIS

COLEMI: CHOWS MUST RESPONSES LIMINED PROJECT: TECHNA COME SAWALE NO. 200

HOLE NO. 231, SEAM 5

LAS: NOT 5341

DATE: JUNE 28, 1983

AS RECEIVED SAMPLE ATTRITED FOR 2-1/2 MIRUTES (DRY ATTRITION)

(MIRUS 9.5MM AFTER 2 MIRUTES ATTRITION = 32.0%; AFTER 2-1/2 MIRUTES = 36.1%)

HEAD RAW H.G.I. = 59

SIZE & RAW AWALYSES

					CUHULATIVE		
SIZE FRACTION	HT%	RH7	ASHV.	S%	MTZ	ASH Z	
(NH) + 19 ← 19 X 1,7 ← 1,7 X 0,3 ←	53.10 39.10 12.20	2.10 1.70 3.00	11.10 10.20 6.70	0.38 0.43 0.45	53.10 83.20 95.40	11.10 10.77 10.25	
0.3 X C 🖛	4.60	2.60	۶,50	0.45	100 .00	10.22	

LARGEST PARTICLE SIZE (+198M) = 70 KM LONG

FLOAT - SINK AMALYS	IS, air dried	i basis: +197	H	CUSIL	ATIVE
S.G. FRACTION	HTZ	ASHV.	SX .	MTZ	ASHX
FLOAT - 1.60 1.60 - 1.70 1.70 - 1.80 1.80 - SINK	93.60 NTL 2.20 4.20	8.10 49.70 60.70	0.39 — 0.22 0.17	93.60 93.60 95.80 100.00	8.10 8.10 8.74 11.11
FLOAT - STAN AMALYS	IS, air dried	lbasis: 19MM	X 1.7MH	Clear	ATIVE
S.G. FRACTION	KII	ASHX.	S%	жтж	asht.
FLOAT - 1.60 1.60 - 1.70 1.70 - 1.80 1.80 - SD#K	94.10 1.40 0.70 3.80	7.10 36.70 42.60 70.30	0.44 0.26 0.23 0.17	94.10 95.50 96.20 100.00	7.10 7.53 7.79 10.16

CRIERT: CHEMS MEST RESCURCES LIMITED FROCECT: TELKMA CORE SAMPLE NO. 300 HOLE NO. 231, SEAM 5

L//5 NO: 5341

DATE: JUNE 28, 1983

FLOAT - SINK ANALYS	IS, air dried	lbesis: 1.787	X 0.344		
	.			CUMALA	TIVE
S.G. FFACTION	HTZ	ASHX	SI	MTZ	XH2A
FLOAT - 1.60	95.50	4.50	0.47	95,50	4.50
1.60 - 1.70	0.90	28.50	0.28	96.40	4.72
1.70 - 1.80	0.80	36.B0	0.24	97.20	4,99
1.80 - SD&	7.80	54.60	0.19	100.00	6.43

FFOTH-FLCTATION	l IEST, as res	telved basis:	. 03min X 1		
				DUMU	LATIVE
PRODUCT	HTZ	XHEA	5%	HTX	ASH V
STAGE I	31,20	4.70	0.48	31.20	4,70
STARE II	7.40	6.70	0.45	33.60	5,12
TAILINGS	61.40	12.00	C. 44	100.00	9.35

FULF DESETTY = 10%

REAGENT/DESAGE = 4:1 = KERDSENE:MIFC/0.50 LB/TORNE

COMMITTIONING = 60 SECONOS

STAGE I = FIRST MINUTE FROTH

STAGE II = SECONO MIRUTE FROTH

gray so we greatly wististic is no base to

⁺ ANALYSIS ON AIR DRIED BASIS (ON COMPOSITE OF S.G. FRACTIONS)

^{*} ANALYSIS ON AS RECEIVED BASIS

CONTINENTIAL

TELKWA SURVEY REPORT

DECEMBER 1983

00239 part 5

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3)	COORDINATES OF DECEMBER 1983 SURVEY	
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	TRAVERSE NUMBER 22 SURVEY PLAN TRAVERSE NUMBER 22 TRAVERSE NUMBER 22 (REFERENCE STATIONS)	6 7 8
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CROW'S HEST RESOURCES LIMITED TELKWA PROJECT.

COORDINATES OF 1983 DRILL HOLES
SURVEYED: 16 - 20 DECEMBER 1983

NOTE:

FLEVATIONS are on Geodetic Datum and are derived by reciprocal trigonometric levelling from bench marks 1523, 3324, 1629, 2565, 2968 & 2574

COORDINATES are on UTM (Zone 9) grid and are derived from Government stations: CREEK, MUCHO, PABLO, P.CON. 18, POWER, & TACK.

JANUARY 10, 1984

D.E. WATSON B.C.L.S.

FILE 4275

TELKWA PROJECT

DRILL HOLES

DRILL HOLE	TAG #	NORTHING	EASTING	TAG ELEVATION	GROUND ELEVATION
DH354	3293	6,055,912.47	622,890.32	660.86	660.9
DH355	3296	6,055,411.37	622,898.28	685.73	685.7
DH356	3299	6,055,886.27	622,453.74	670.44	670.4
DH357	3309	6,055,645.92	621,641.44	686.92	686.B
DH358	3316	6,055.461.26	622,403.53	684.79	684.8
	3311	6,055,393.88	621,855.85	694.42	694.4
DH359	3302	6,054,759.74	622,190.14	722.33	722.3
DH360	3300	6,055,642.72	621,882.97	684.48	684.5
DH361	3319	6.054,457.38	622,094.53	740.93	740.9
DH362	3315	6,055,137.13	621,886.45	703.99	704.0
DH363	3317	6,055,145.15	622,617.83	692.60	692.5
DH364	3303	6,054,359.06	622,395.49	749.44	749. 4
DH365		6,055,639.21	622,135.11	685.96	686.0
DH366	3313	6,054,422.69	622,863.66	752.81	752.B
DH367	3306	• •	622,088.73	690.00	690.0
DH368	3308	6,055,398.25	621,902.38	675.23	675.2
DH369	3297	6,055,901.67	021,302-30	2/3.43	

STATION	DESCRIPTION	BEARING	GRID DISTANCE	STATION ELEVATION	GROUND ELEVATION	NORTHING	EASTING	HAP SHEET
1523 2565 3309 3324 3310 3300 3312 3307 3314 1629 1523	75cm Iron Pin 75cm Iron Pin D.H. 357 D.H. 344 - Nail & Tag 75cm Iron Pin D.H. 361 20cm Spike 20cm Spike 75cm Iron Pin 75cm Iron Pin 75cm Iron Pin	331-01-58 101-05-43 184-28-16 93-29-10 2-54-25 94-17-13 194-05-05 221-05-20 80-05-25 159-10-47	4338.60 315.03 215.94 247.29 227.42 282.90 229.47 332.31 296.36 3518.54	1216.59 676.72 686.92 694.27 693.22 684.48 687.41 691.28 704.89 698.26	1216.2 676.7 - 686.8 694.3 693.2 684.5 687.4 691.3 704.9 698.3	6,051,910.71 6,055,706.54 6,055,645.92 6,055,415.60 6,055,642.72 6,055,621.58 6,055,399.00 6,055,148.55 6,055,199.49 6,051,910.71	623,433.52 621,332.30 621,641.44 621,624.49 621,871.44 621,882.97 622,165.08 622,109.24 621,890.84 622,182.90 623,433.52	835E

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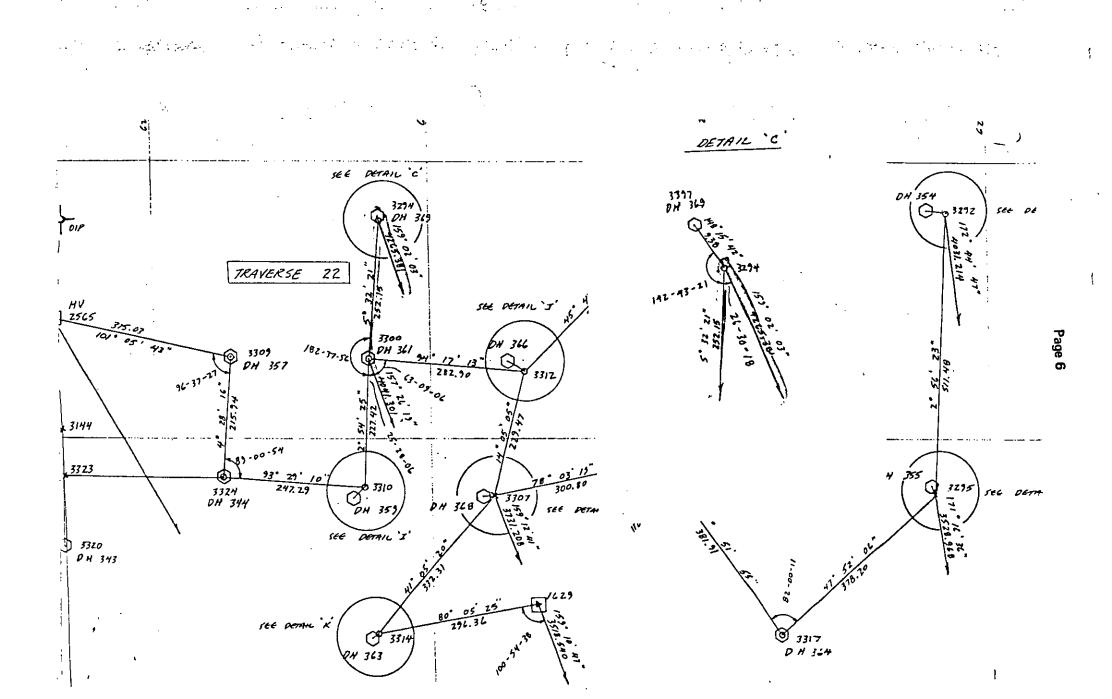
TRAVERSE 21 - TAG NUMBERS

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STATION	DESCRIPTION	BEARING	GRID . DISTANCE	STATION ELEVATION	GROUND ELEVATION	NORTHING	EASTING	HAP SHEET
3309	Drill Hole 357			686.92	686.8	6,055,645.92	621,641.44	B3NW
3310	75cm Iron Pin	215-40-25	26.72	693.22	693.2	6,055,415.60	621,871.44	BBNW
·	Drill Hole 359-Yag 3311	215-40-25	26.73	694.42	694.4	6,055,393.88	621,855.85	
3300	Drill Hole 361			684.48	684.5	6,055,642.72	621,882.97	83 NW
3312	20 cm Spike		÷	687.41	687.4	6,055,621.58	622,165.08	BSNu
	Drill Hole 366-Tag 3313	300-28-08	34.77	685.96	686.0	6,055,639.21	622,135.11	b b b b b b b b b b b b b b b b b b b
3307	20cm Spike			691.28	691.3	6,055,399.00	622,109.24	
	Orill Hole 368-Tag 3308	267-53-01	20.52	690.00	690.0	6,055,398.25	622,088.73	. B3N4
3314	75cm Iron Pin		.,	704.89	704.9	6,055,148.55	621,890.84	
	Drill Hole 363-Tag 3315	201-00-10	12.23	703.99	704.0	6,055,137.13	621,886.45	B3Nin

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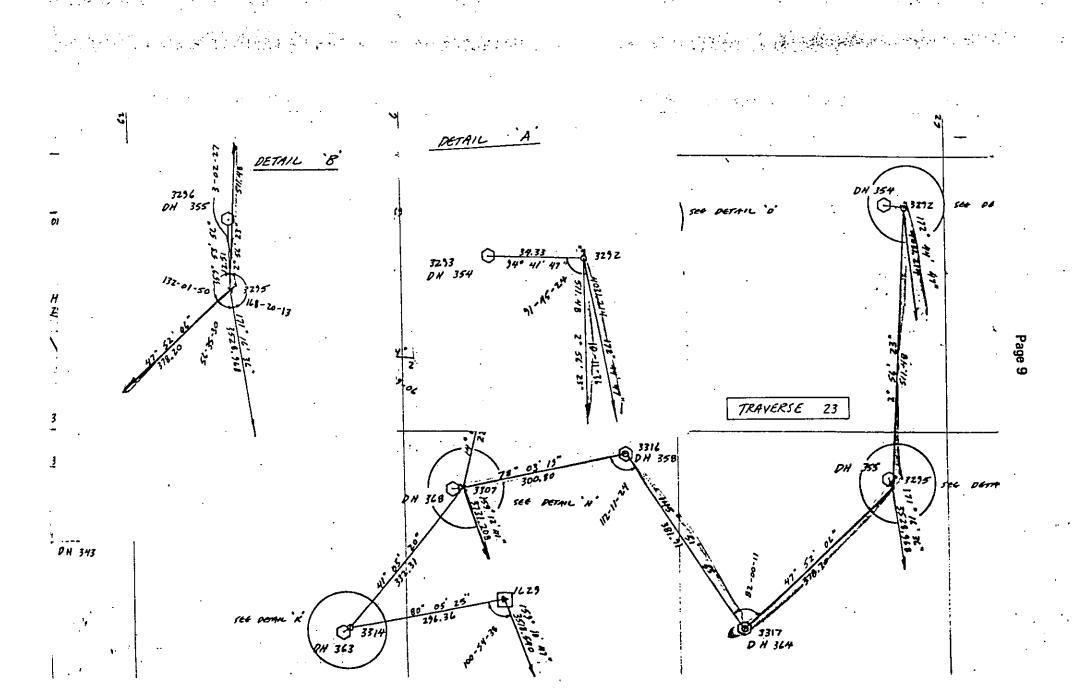
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	TRAVERSE 22 - SURVEY S						· · · · · · · · · · · · · · · · · · ·	
STATION	DESCRIPTION	BEARING	GRID DISTANCE	STATION ELEVATION	GROUND ELEVATION	NORTHING	' EASTING	HAP SHEET
1523 3300 3294 1523	75cm Iron Pin D.H. 361 75cm Iron Pin 75cm Iron Pin	337-26-19 5-32-21 159-02-03	4041.30 252.15 4265.38	1216.59 684.48 675.25 1216.59	684.5 675.2 1216.2	6,051,910.71 6,055,642.72 6,055,893.70 6,051,910.71	623,433.52 621,882.97 621,907.31 623,433.52	835E 83Nu 83Nu 83SE
•								

TRAVERSE 22 - TAG NUMBERS

STATION	DESCRIPTION	BEARING	GRID DISTANCE	STATION ELEVATION	GROUND ELEVATION	NORTHING	EASTING	SHEE
3294	75cm Iron Pin	328-15-42		675.25	675.2	6,055,893.70	621,907.31	83 NV
	Drill Hole 369-Tag 3297	328-15-42	9.38	675.23	675.2	6,055,901.67	621,902.38	BING

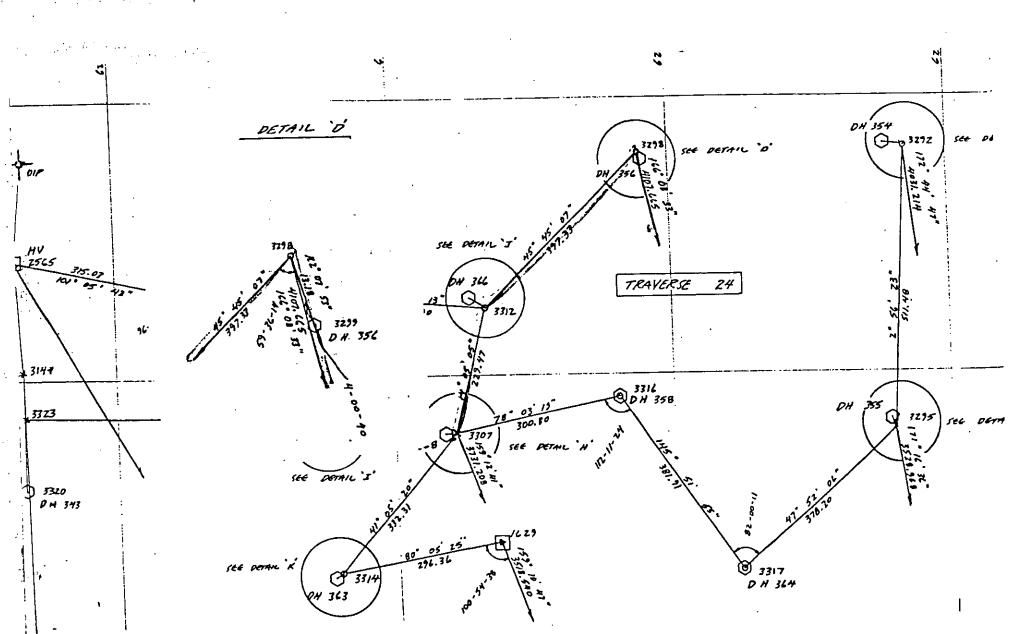
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	TRAVERSE 23 - SURVEY STATIONS						•	,	
STATION	DESCRIPTION	BEARING	GRID DISTANCE	STATION ELEVATION	GROUND ELEVATION	NORTH1 NG	EASTING	MAP SHEET	•
1523 3307 3316 3317 3295 3292 1523	75cm Iron Pin 20cm Spike D.H. 358 D.H. 364 20cm Spike 75cm Iron Pin 75cm Iron Pin	339-12-41 78-03-19 145-51-55 47-52-06 2-56-23 172-44-47	3731.21 300.80 381.91 379.20 511.48 4031.21	1216.59 691.28 684.79 692.60 686.64 661.34	1216.2 691.3 684.8 692.5 686.6 661.3	6,051,910.71 6,055,399.00 6,055,461.26 6,055,145.15 6,055,398.86 6,055,909.66 6,051,910.71	623,433.52 622,109.24 622,403.53 622,617.83 622,898.31 622,924.54 623,433.52	B3SE B3NW B3SE	

. . .

3316 Drill Hole 358 684.79 684.8 6.055,461.26 622,403.53 23NW 3317 Drill Hole 364 3295 20 cm Spike Drill Hole 355-Tag 3296 359-53-56 12.51 685.73 685.7 685.73 685.7 6055,411.37 622,898.28 375 cm Iron Pin 274-41-47 34.33 660.86 660.9 660.9 6,055,912.47 622,890.32	TATION'	TRAVERSE 23 - TAG NUMBERS , DESCRIPTION	BEARING	GRID	STATION ELEVATION	GROUND ELEVATION	NORTHING	EASTING	HAP SHEET	
3316 Drill Hole 358 3317 Drill Hole 364 3295 20 cm Spike Drill Hole 355-Tag 3296 359-53-56 3292 75 cm Iron Pin 274-41-47 34-33 660.86 692.60 692.5 6,055,145.15 622,617.83 83NN 686.64 686.6 6,055,398.86 622,898.31 83NN 661,34 661,34 661,34 660.9 6,055,909.66 622,924.54 33NN 660.86 600.9 6,055,912.47 622,890.32	1211011			DISTANCE	FLEANILON	CEETATION	 	<u> </u>		
3317 Drill Hole 364 3295 20 cm Spike Drill Hole 355-Tag 3296 359-53-56 12.51 686.64 686.6 6.055,398.86 622,898.31 83NW 685.73 685.7 6.055,411.37 622,898.28 83NW 3292 75 cm Iron Pin 274-41-47 34.33 660.86 660.9 6.055,912.47 622,890.32	3316	Drill Hole 358			684.79	684.8	6,055,461.26	622,403.53	B3NW	-
3295 20 cm Spike 359-53-56 12.51 686.64 686.6 6,055,398.86 622,898.31 83NW Drill Hole 355-Tag 3296 685.7 6,055,411.37 622,898.28 75 cm Iron Pin 274-41-47 34.33 660.86 660.9 6,055,912.47 622,890.32		2-:11 Hole 364			692.60	692.5	6,055,145.15	622,617.83	BSNIJ	
3295 20 cm Spike Drill Hole 355-Tag 3296 359-53-56 12.51 685.73 685.7 6,055,411.37 622,898.28 2340 3292 75 cm Iron Pin 274-41-47 34.33 660.86 660.9 6,055,912.47 622,890.32	3317	Britt hole 501		<u> </u>	686.64	686.6	6,055,398.86	622,898.31		
Drill Hole 355-Tag 3296 3292 75 cm Iron Pin 274-41-47 34.33 660.86 660.9 6,055,912.47 622,890.32	3295	20 cm Spike	359-53-56	12.51			·	1	ا ما المادم	
3292 75 cm 1 ron Pln 274-41-47 34.33 661.3 6.055,909.66 622,924.54 83NW		Drill Hole 355-Tag 3296	`		685.73	685.7	6,055,411.37	l e	-	
274-41-47 34.33 660.9 6,055,912.47 622,890.32	· · · · · · · · · · · · · · · · · · ·	Tr Iron Pin	·		661,34	661.3	6,055,909.66	622,924.54	BRUW	
Drill Hole 354-Tag 3293	*		274-41-47	34.33	_660.86	660.9	6,055,912.47	622,890.32		
	•	Drill Hole 354-Tag 3293	1	*	1	١	ı			
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	TRAVERSE 24 - SURVEY STATIONS			· · · · · · · · · · · · · · · · · · ·	000000	NORTHING	EASTING	MAP	-
STATION	DESCRIPTION	BEARING	GRID DISTANCE	STATION ELEVATION	GROUND ELEVATION	NORTHING	- CASTING	SHEET	
3307 3312 3298 1523	20cm Spike 20cm Spike 75cm Iron Pin 75cm Iron Pin	14-05-05 45-45-07 166-08-33	229.47 397.33 4107.67	691.28 687.41 670.72 1216.59	691.3 687.4 670.7 1216.2	6,055,399.00 6,055,621.58 6,055,898.82 6,051,910.71	622,109.24 622,165.08 622,449.70 623,433.52	B3NW B3NW B3NW B3SG	
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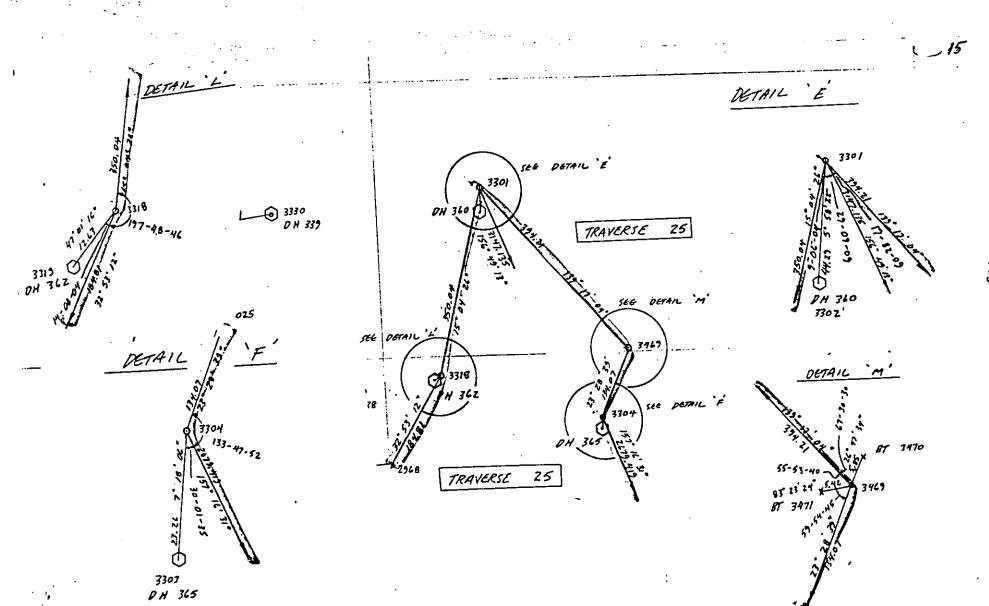
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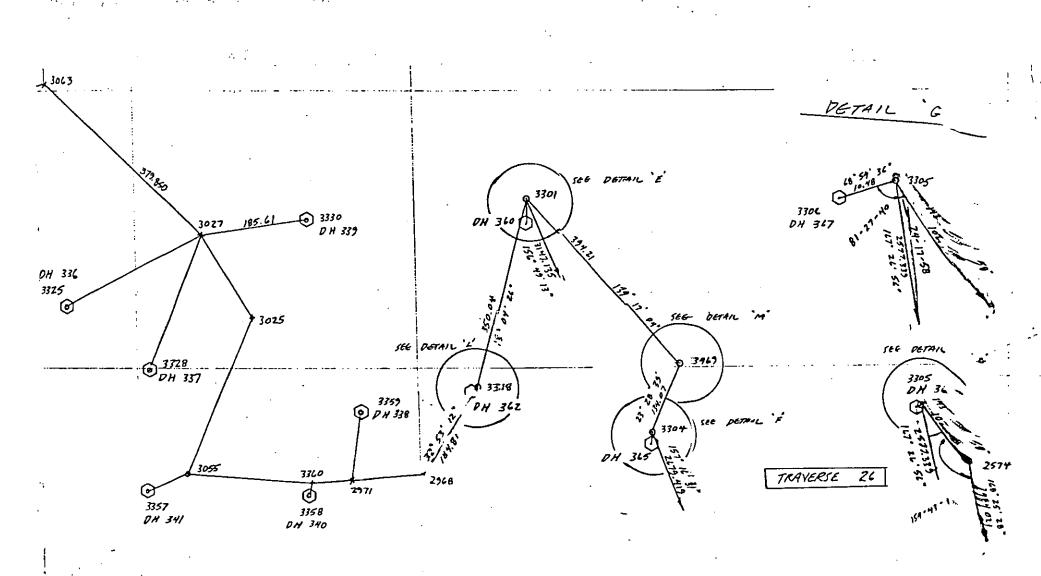
TRAVERSE 24 - TAG NUMBERS

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STATION	DESCRIPTION	BEARING	GRID DISTANCE	STATION ELEVATION	GROUND ELEVATION	NORTH I NG	EASTING	HAP SHEET
3298	75cm Iron Pin		:	670.72	670.7	6,055,898.82	622,449.70	BBNW
	Drill Hole 356-Tag 3299	162-07-53	13.18	670.44	670.4	6,055,886.27	622,453.74	B3NW



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STATION	DESCRIPTION	BEARING	GRID DISTANCE	STATION ELEVATION	GROUND ELEVATION	NORTHING	EASTING	MAP SHEET
								.
3318	75cm Iron Pin			740.49	740.4	6,054,465.99	622,103.77	B3NW
	Drill Hole 362-Tag 3319	227-01-16	12.63	740.93	740.9	6,054,457.38	622,094.53	
3301	75cm Iron Pin			722.62	722.6	6,054,803.79	622,194.75	
	Drill Hole 360-Tag 3302	185-58-22	44.29	722.33	722.3	6,054,759.74	622.190.14	83NW
3469	75cm Iron Pin	,		743.43	743.3	6,054,505.06	622,451.84	
	Tag 3470 -BT 30cm Poplar	26-47-34	5.85	743.20	741.7	6,054,510.28	622,454.48	ВЗИИ
	Tag 3471 -BT 10cm Spruce	263-23-24	5.42	744.84	743.4	6,054,504.43	622,446.46	
3304	75cm Iron Pin		1	747.33	747.3	6,054,382.13	622,398.45	33NW
	Drill Hole 365-Tag 3303	187-18-06	23.26	749.44	749.4	6,054,359.06	622,395.49	25.7.2
		1'	}	•	•	•	•	

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	HEREE AC CHRIST STATIONS								. 1
STATION	VERSE 25 - SURVEY STATIONS DESCRIPTION	BEARING	GRID DISTANCE	STATION ELEVATION	GROUND ELEVATION	NORTHING	EASTING	MAP SHEET	, ,
2968 3318 3301 3469 3304 1523	20cm Spike 75cm Iron Pin 75cm Iron Pin 75cm Iron Pin 75cm Iron Pin 75cm Iron Pin	32-53-12 15-04-26 139-17-04 203-28-39 157-16-31	184.81 350.04 394.21 134.07 2679.42	751.85 740.40 722.62 743.43 747.33	752.0 740.4 722.6 743.3 747.3	6,054,310.91 6,054,465.99 6,054,803.79 6,054,505.06 6,054,382.13 6,051,910.71	622,003.50 622,103.77 622,194.75 622,451.84 622,398.45 623,433.52	B3VW B3S€	Page 16

Little Company of the

STATION	DESCRIPTION	BEARING	GRID DISTANCE	STATION ELEVATION	GROUND ELEVATION	MORTHING	EASTING	MAP SHEET
1523 3305 2574 1523	75cm Iron Pin 75cm Iron Pin (HV-36) Nail & Tag 75cm Iron Pin	347-26-56 143-08-58 168-25-28	2577.34 102.78 2484.02	1216.59 752.40 756.43 1216.59	1216.2 752.4 756.4 1216.2	6,051,910.71 6,054,426.46 6,054,344.21 6,051,910.71	623,433.52 622,873.44 622,935.08 623,433.52	835E 83NW 83NW 83SE
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等的,就可以被各种的特殊。但如此一个人,不是是一个

TRAVERSE 26 - TAG NUMBERS

STATION	DESCRIPTION	BEARING	GRID DISTANCE	STATION ELEVATION	GROUND ELEVATION	NORTHING .	EÁSTING	HAP SHEET
3305	75cm Iron Pîn	248-54-36		752.40	752.4	6,054,426.46	622,873.44	B3NW
	Drill Hole 367-Tag 3306		10.48	752.81	752.8	6,054,422.69	622,863.66	

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3294	3, 6, 7, 8
3295	9, 10, 11
3296	2, 11
3297	2, 6, 8
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3309	2, 3, 4, 5
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3314	3, 4, 5
3315	2, 3, 5
3316	2, 9 10, 11
3317	2, 9, 10, 11
3318	15, 16, 17
3319	2, 17
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3324	3,4
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