

# OPEN FILE

PETRO-CANADA  
COAL DIVISION

MONKMAN COAL PROJECT  
1983

NTS 93I/15B

THE STRUCTURAL GEOLOGY  
OF  
DUKE PIT

Lat.  $54^{\circ}45'N - 54^{\circ}48'N$   
Long.  $120^{\circ}42'W - 120^{\circ}46'30''W$   
Peace River Land District

COAL LICENCES:	3225	3239	3946
	3226	3242	3947
	3227		3949

PREPARED BY: L.A. SMITH  
CONSULTING AND DEVELOPMENT LTD.  
1983-12-31

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# THE STRUCTURAL GEOLOGY OF DUKE PIT

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*Maps and  
cross-sections  
in separate  
file pocket.*

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## 1.0 SUMMARY

The Project: This report presents the findings of a detailed 1:2000 scale structural study of Duke Pit, Monkman Coal Project. The results confirm the folded thrust concept suggested by the authors in a 1982 study.

Scope: The scope was defined as a compilation of all relevant geological data within the study area onto 1:2000 base and to provide a detailed interpretation, the interpretation to include twelve cross-sections and a structure contour map on the base of B1 Seam.

Methodology: The methodology utilized the compiled computer data base for the area, augmented and corrected where necessary, and used the interactive graphics capability of the TRIPOD computer package to determine the direction and plunge needed to project the drillhole and outcrop data onto the lines of section. The TRIPOD software also carried out the raw data plotting onto the geology maps and the cross-sections.

After determination of the data projections and completion of the raw data plots, the cross-sections and maps were interpreted. The structural contour map is the result of a compilation of data points from drillhole information, cross-section information and a down-plunge grid of data points.

Stratigraphy: The Gates Formation of Lower Cretaceous Age contains the coal measures of economic interest in this area, and the bulk of the stratigraphic and structural data is derived from the Gates Formation.

Folding: The dominant fold in the study area is the Quintette Syncline, a southerly plunging structure that has coal subcropping in the hinge zone from 15800N to 17200N. To the south the coal outcrops on the west flank along the northeast slope of Duke Mountain. To the east the coal subcrops in a southeast trend that extends outside the study area. Structural thickening of coal seams does occur near the hinge zone where the structures are very flat. Flexural slip movement is the mechanism of fold deformation.

Faulting: Two major and several minor thrust faults lie in the study area. The lowermost Quintette Thrust separates Duke Pit from the Honeymoon Pits and limits Duke Pit on the east flank. The overlying Duke Thrust has a modest 100 m throw and provides repeat sections of the coal measures in the northeast portion of Duke Pit. The two thrust faults generally parallel one another. They trend southeast of the study area at about Section 15000N.

Reserve Potential in Duke Pit: Due to the nature of the thrust faulting that effectively repeats coal seams in certain areas, and because of the structural thickening of coal seams (see MDD 78-12 and MH 8060B), the reserve potential within Duke Pit will undoubtedly be greater than has been measured in the past.



## 1.0 SUMMARY (cont'd)

Duke Pit Potential Reserve Additions: This study indicates that Duke Pit may be expanded in two directions (see Map 8). These potential reserve additions are:

The East Flank - this area extends eastward from the old (1981) pit highwall and will effectively move the highwall eastward (see Map 8). Although an in-place possible reserve of 20 megatonnes is estimated for the East Flank, additional exploration is required to delineate the reserve area, size and potential.

Duke Pit South Extension - this reserve area at the south end of Duke Pit extends from 13800N in a southerly direction off the study area. It is believed that this area may be mined all the way to Fearless Creek (Section 11000N) and add at least 15 megatonnes in-place coal reserves.

Overburden: Thick amounts of till (up to +90 m) cover the coal measures in the northern part of Duke Pit. This till is so thick that the volumes of unconsolidated material will provide a serious constraint on mining in this area. Localized zones of up to 25 metre thick till occurs elsewhere in the map area. The till thickness is represented on Maps 5a, 5b and 5c.

Additional Exploration: Additional data collection is necessary to define Duke Thrust, Quintette Thrust and the small thrust west of Duke Pit on Section 16600N. Possibly thickened coal zones in the axis of Quintette Syncline require drilling and may occur on both the Duke and Quintette Thrust Sheets. Additional mesoscopic scale structures (both thrust faults and folds) will be identified as more data is collected in Duke Pit. The East Flank requires major amounts of data collection to confirm and delineate the structure. Overburden studies are required in the reserve areas on the north map sheet and the northern part of the central map sheet. Localized areas of till elsewhere in the pit require greater definition.

## 2.0 INTRODUCTION

This report provides a written account of a structural geology study of the Duke Pit, Monkman Coal Project as requested by Mr. Tom Covert on 21 September, 1983 and approved by Mr. John Steward on 29 September, 1983. The study was limited to the structural interpretation and a structure contour map of B1 Seam. The work is authorized by a consulting contract dated 30 September, 1983.

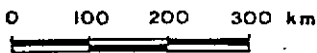
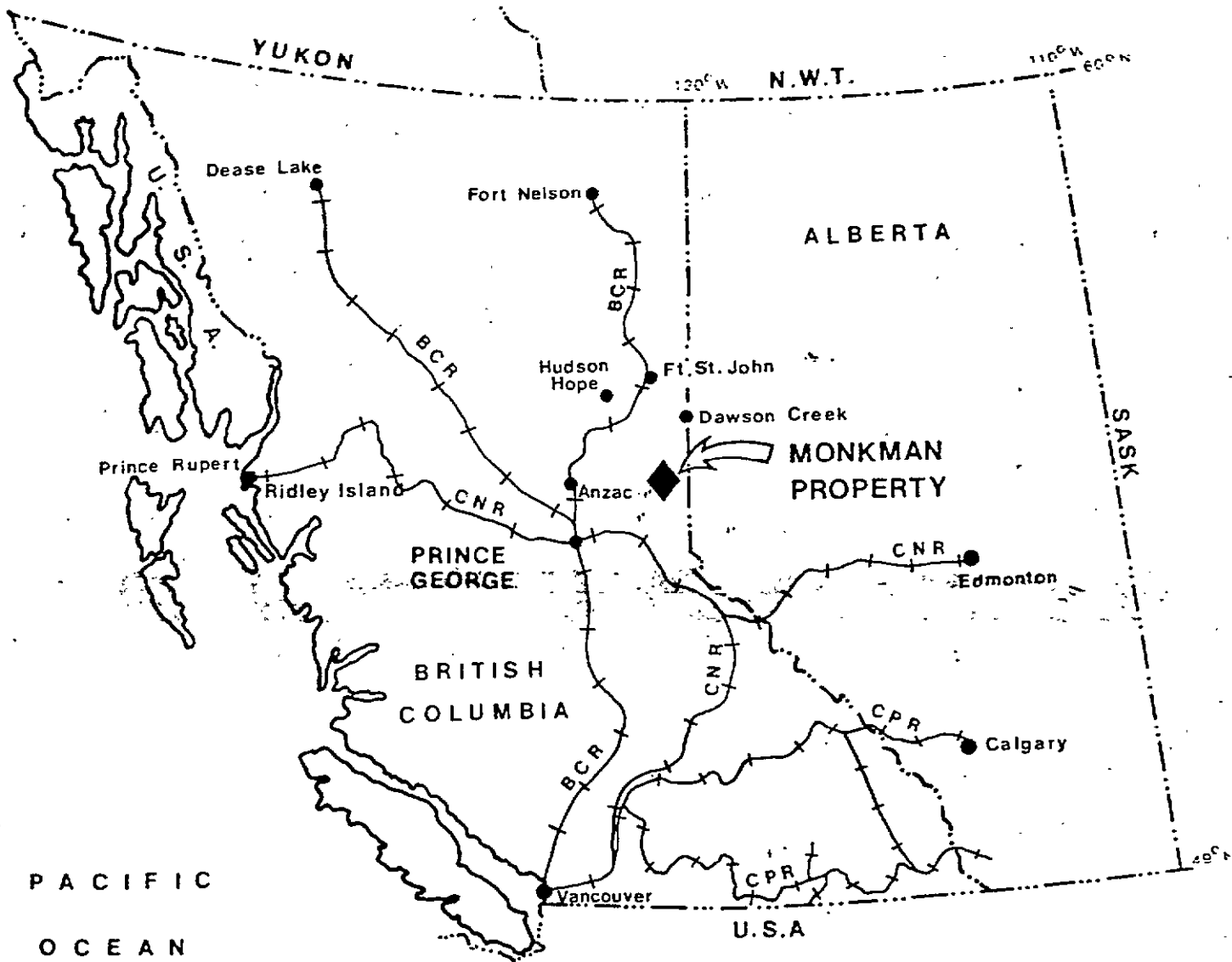
The Monkman Coal Project lies in northeast B. C. at  $54^{\circ} 47' N - 120^{\circ} 45' W$  and about 40 km immediately south of Tumbler Ridge, B. C. Duke Pit is located in the north central portion of the main Duke Block coal leases. The open pit reserves lie on the northeast side of Duke Mountain and extend northward into Honeymoon Creek Valley.

The deposit was discovered in 1977 when drillhole MDD 77-2B penetrated the major coal zones (B1 to B9) in the central portion of the dip slope. The area was assumed to be a relatively simple dip slope until drillhole MDD 78-02 indicated zones of structurally thickened coal and fault repeated coal measures. Additional structural complications were indicated by very steep ( $70^{\circ}$  dip) strata in MDD 78-12.

A study by the authors in 1982 indicated that faulting in the north end of the reserve area consists of west-dipping thrusts that were subsequently folded. This interpretation pointed out serious conflicts with the existing mine plan with regard to pit design and configuration, coal seam thickening, location of dumps and, ultimately, the coal reserves available for mining.

This study is intended to resolve as much as is practical the structural configuration on 1:2000 scale. This will provide a higher level of understanding of the geology in the pit area. The geology is presented in sufficient detail to allow the mine planners to carry out reasonably detailed design work.

The TRIPOD computer package is used in this study to enhance data handling, maximize utilization of outcrop data, and to determine the limits of data projection. The use of this software has greatly enhanced the quality and detail of the structural interpretation.



**MONKMAN COAL PROJECT  
BRITISH COLUMBIA  
GENERAL LOCATION MAP  
MAP 1**

### 3.0 SCOPE AND OBJECTIVE

#### Data Base

The data base for the structural interpretation consists of several sets of data:

- i) outcrop information - listed in Appendix 1,
- ii) drillhole stratigraphic information - listed in Appendix 2,
- iii) drillhole deviation data - listed in Appendix 2,
- iv) dipmeter data for 1982 drillholes,
- v) 1:2000 scale topographic maps, and
- vi) air photos.

#### The Coordinate System

Two grid systems are currently used on the Monkman Coal Project: the UTM and Mine Grid Systems. Mine Grid North is oriented 40° west of true north and roughly parallels the trend of the structural geology. The origin of the system is located at UTM 51721.4592E and 57557.7076N.

The outcrop data compiled during the 1:5000 scale study completed in 1981 were recorded in UTM coordinates. The Petro-Canada engineering staff supplied grid conversion equations to this study. A computer program was designed and used to convert coordinates and outcrop dip directions to the Mine Grid System.

All orientations and location coordinates used in this study are in the Mine Grid System.

#### Project Area

The study area is defined by the following coordinates on the mine grid (see Map 2):

3700E - 17500N  
 6000E - 17500N  
 3700E - 13000N  
 6000E - 13000N

Drillhole and outcrop data from an expanded area has been used to provide the additional structural data required for this study. The rough outline of the expanded area is as follows:

3200E - 12500N  
 6500E - 12500N  
 3200E - 18000N  
 6500E - 18000N

## Stratigraphy

Rocks that range from the Jurassic Minnes Group to the Ku Shaftsbury Formation subcrop and outcrop in the study area. The study is, however, primarily concerned with Gates Formation strata. Coal seam stratigraphy has been reviewed in detail and each drillhole in the study area has been correlated. During compilation of the structural geology, this correlation has been reviewed extensively because detailed knowledge of the coal seam stratigraphy is necessary to determine the structural geology. The correlation chart (Fig. 5) represents the coal seam stratigraphy used in this study.

## Structural Geology

The object of this study is to delineate the structural geology of the defined project area on 1:2000 scale. As defined in the proposal dated 1983.09, 1:2000 scale cross-sections are drawn on 400 m intervals on the following section lines:

13000N	15400N
13400N	15800N
<del>13800N</del>	16200N
14200N	16600N
14600N	17000N
<del>15000N</del>	17400N
15200N	

*All but four have been lost.  
A set of more recent  
1:5000 sections, covering  
13,000N - 17,500N is  
substituted  
JWS 3/7/86*

Each section line extends from 3700E to 6000E.

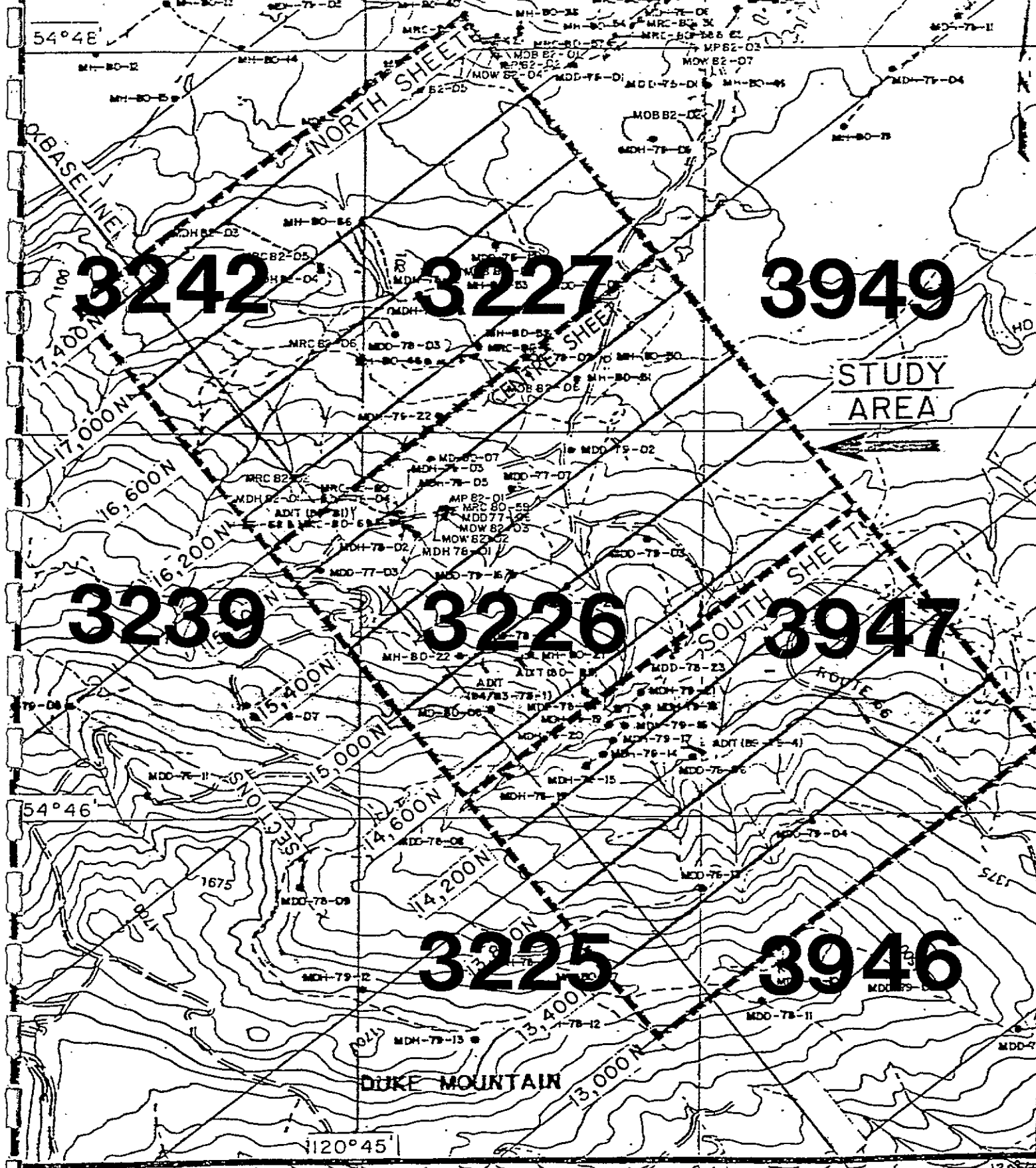
The geology map portrays the subcrop geology on three maps, the south, centre and north sheets (see Map 6a, b, c). In order to facilitate proper definition of the subcrop geology, an overburden isopach map was required (Map 5a, b, c).

## Structure Contours

The original proposal requested structure contour maps with 15 m contours drawn at the base of B9, B7, B5, B4, B3 and B1 Seams. The scope was reduced by Petro-Canada Coal Division to include a single structure contour map on the base of B1 Seam using 15 m contours. This is represented on Map 7a, b, c.

## Required Exploration

Areas with insufficient data have been examined in as much detail as is practical in this study. In certain areas the structural geology has not been



NTS : 93 I / 15 B

NEW STUDY AREA

SCALE: 1:25000

MAP 2

### Required Exploration (cont'd)

resolved adequately and additional data is required to fully understand the geology. These problem areas are identified and discussed and data collection methods are proposed.

#### 4.0 THE TRIPOD COMPUTER PACKAGE

The TRIPOD computer package was designed to assist geologists working with structurally deformed sedimentary rocks. It is used to store, edit, retrieve, process and graphically reproduce structural and stratigraphic geological data accurately and swiftly while leaving the interpretation to the geologist.

Raw data used by the package consists of both outcrop and drillhole information. Cross-sections, geological maps, structure contour maps, isopach maps, isoburden maps and orientation diagrams are generally produced after data processing and geological interpretation is complete.

The TRIPOD package allows the geologist to utilize more data, handle plunging structures more effectively and eliminate graphical errors. In addition, the numerical techniques employed to evaluate a structure are purely objective and the results are reproducible by other geologists.

#### 5.0 METHODOLOGY

##### 5.1 General

Graphical procedures normally used to evaluate orientation data have numerical bases. These numerical techniques, although more accurate than graphical methods, are tedious and time consuming.

Since the advent of computers, these calculations can be performed in an efficient, cost-effective manner. Advances in computer graphics allow the results of the numerical procedures to be displayed in a visual fashion.

The TRIPOD computer package utilizes the numerical methods and computer graphics to describe and display the geology of complex structural features.

## 5.2 Data Collection

Well collected, reliable raw data is of the utmost importance for undertaking any geological study. Both outcrop and drillhole data must be collected in a consistent fashion. This is particularly important for outcrop data because the TRIPOD package employs statistical techniques that require consistent high quality data.

### Outcrop Data

Well collected outcrop data can be used to determine the surface traces and dips of map units and the trend and plunge of structural features. Ideally, outcrop information should be collected with consideration given to the use to which it will be put. For example, outcrop data collected during 1:10,000 or 1:5000 reconnaissance mapping will be useful but certainly will not be accurate enough for detailed geological studies on a 1:2000 or 1:1000 scale. While the data may be good quality for its intended purpose, it is not accurate enough for use in a detailed evaluation.

Two data forms are used to record outcrop information. At each outcrop the outcrop number, location and stratigraphic horizon are coded on Form A (Fig. 1) along with a code to indicate whether the strata is right way up or overturned. Orientation data describing folds, faults, joint sets, slickenside striae and planar strata is entered into Form B (Fig 1). In this study, only orientations referring to planar bedded strata were collected. Normally four to ten bedding orientations are collected at each outcrop in order to utilize the statistical capabilities of TRIPOD to the fullest extent. In many map areas, as is the case for this study, only one bedding orientation was collected at each outcrop.

### Drillhole Data

Drillhole data is collected and entered into Forms C and D (Fig. 2). Form C contains the collar coordinates, the original orientation of the drillhole, the total depth, overburden thickness and deviation measurements recorded as depth, trend of the hole and the angle between the hole and vertical ( $90^\circ$  - plunge). Form D contains a drillhole intersection entered as the stratigraphic horizon and a depth.



FORM A

1	2	
Edit Code <input type="text"/>	Outcrop Number <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>	
6	9	10
Type/Number <input type="text"/> <input type="text"/> <input type="text"/>	Horizon <input type="text"/>	Way Up <input type="text"/>

Coordinates

11	17	23
<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>	<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>	<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>
(easting)	(northing)	(elevation)

FORM B

1	2	6
Edit Code <input type="text"/>	Outcrop Number <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>	Type <input type="text"/>
7	9	12
Number <input type="text"/> <input type="text"/>	Pitch <input type="text"/> <input type="text"/> <input type="text"/>	Sense <input type="text"/>

13	18	
Axial Trace <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>	Measurements <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>	
23	28	33
<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>	<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>	<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>
38	43	48
<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>	<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>	<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>
53	58	63
<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>	<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>	<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>

Fig. 1. Format of Forms A and B.

FORM C

	1		2		6
Edit Code	<input type="text"/>	Drillhole Number	<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>	Type/Number	<input type="text"/> <input type="text"/> <input type="text"/>
	9				
	<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>		( easting )		
Collar	15				
	<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>		( northing )		
Coordinates	21			25	
	<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>		( elev )	Orientation	<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>
	30			35	
Total Depth	<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>		Overburden	<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>	

Deviation Measurements

39	<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>	48	<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>
57	<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>	66	<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>

FORM D

	1		2		6
Edit Code	<input type="text"/>	Drillhole Number	<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>	Type	<input type="text"/>
	7		9	10	
Number	<input type="text"/> <input type="text"/>	Horizon	<input type="text"/>	Depth	<input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/> <input type="text"/>

Fig. 2. Format of Forms B and C. Note that up to 150 sets of deviation measurements may be recorded on Form C.

### Raw Data File

All of the raw data on Forms A through D are entered into one data file. The data types are entered sequentially with Type A data entered first followed by B through D, respectively. This file (Appendix 3) is generally listed, checked for errors and corrected.

## 5.3 Data Processing

### Master Files

The initial phase of data processing involves reading the raw data file with the TRIPOD package, performing some preliminary calculations and storing the information in four master data files written in binary code. These data are now in a format ready for data processing and suitable for use in a structural interpretation. Mean bedding orientations have been calculated for each outcrop and a path of each deviated drillhole has been determined.

The data contained in the master files can be easily retrieved and displayed (Appendix 4).

### Error Checking and Editing

~~Data entered into the computer data files needs to be carefully~~ scrutinized for errors. Numerical errors or errors in stratigraphic codes can be located by carefully examining each line of the raw data file. When the raw data is read into the TRIPOD package, errors in data spacing, outcrop or drillhole numbers, the sequence of drillhole intersections or in drillhole deviation sequences will be identified by the computer and an error message will be generated.

The first column in each line of the raw data file is used as an editing space. The number 1 is entered into this space of an erroneous line and the corrected line is added to the raw data file. When these two lines are read into the TRIPOD package, the erroneous data is eliminated from the master file and is replaced by the corrected information. This procedure eliminates the necessity of re-reading the complete data file each time an error is located.

### Data Retrieval

Once the data has been checked and edited, the preliminary processing complete and the data stored in the master data files, data processing and geological interpretation can begin. Both outcrop and drillhole information can be retrieved based upon a number of parameters:

- 1) geographical area outlined by the apices of a polygon;
- 2) drillhole or outcrop numbers;
- 3) stratigraphic horizon encountered at an outcrop or drillhole intersection;
- 4) type of structural data (i.e. bedding, joints, etc.).

### Outcrop and Drillhole Maps

Geological information retrieved from the master files can be displayed on geological maps of any size or scale. Outcrops, drillholes, joint sets, small scale folds, etc. can be represented.

#### 5.4 Cylindricity and Structural Domains

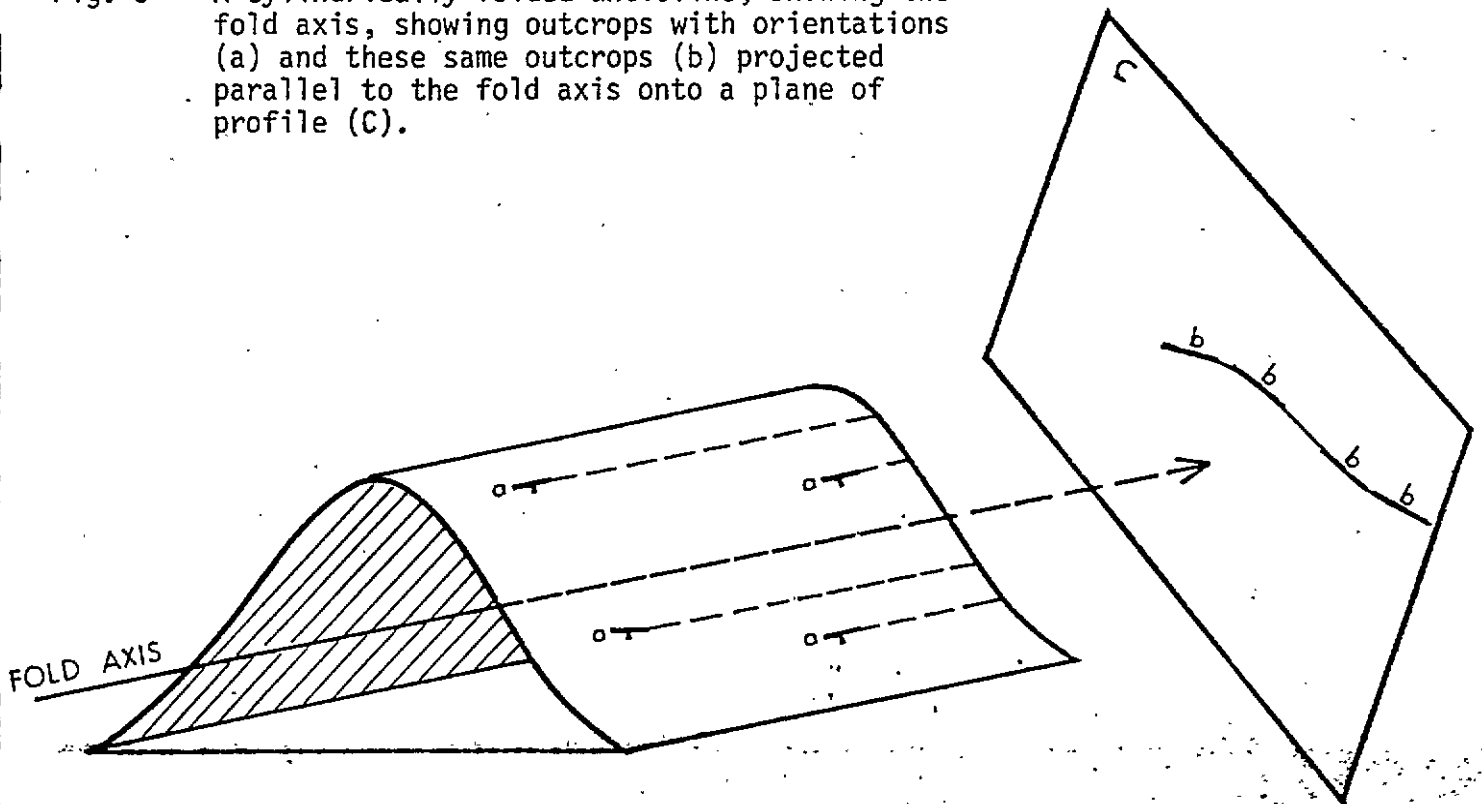
A structure is defined as being cylindrical if a line of fixed orientation (the fold axis) can be used to trace out the bedding surfaces simply by changing the position of the line (Fig. 3). It holds that if a structure displays this property, then all of the data collected on the stratigraphic surfaces may be projected parallel to the fold axis onto a vertical cross-section or an inclined plane or profile. This ideal situation seldom exists in nature so techniques have been developed to test the "goodness of fit" of real data to the cylindrical ideal.

#### Structural Domains

Outcrop data within the Duke Pit Study limits and within a 500 m perimeter of the area was plotted on a 1:5000 scale outcrop map. These data were examined qualitatively to assess the potential limits of cylindrical domains.

Outcrop information in Duke Pit is severely restricted due to extensive overburden, and generally speaking, outcrop data is only available along the southwest limb of the structure. This limits the use of the cylindrical fold model and planar segments of the structure were examined rather than cylindrical segments. The statistical tests used for defining cylindricity do not apply to this study and accordingly will not be discussed further (See Appendix 6).

Fig. 3 A cylindrically folded anticline, showing the fold axis, showing outcrops with orientations (a) and these same outcrops (b) projected parallel to the fold axis onto a plane of profile (C).



### Slice Plots

When cylindrical domains with associated fold axes cannot be proven based upon the outcrop data, the initial stage of geological interpretation is done on "slice plots". Data within narrow strips, centred on the section lines, can be projected onto each line of section. The trend and plunge of the projection axis is based upon the regional structural grain. The projection axis orientation is refined by use of interactive graphics.

This procedure is effective when a large number of drillholes are available. If data is sparse and if these data are projected for a long distance, either a) insufficient data on each section prevents one from arriving at a reasonable interpretation, or b) excessive projection distances make a hodge-podge of the data displayed on each line of section.

### Slice Plots (cont'd)

Two sets of slice plots were prepared for the Duke Pit Study. Data from 400 m and 600 m wide slices was projected onto each line of section. These plots provided some initial indications of the geology of the study area. However, the structural geology in some parts of Duke Pit is very complex and all of the data in one slice could not be projected along a single projection axis.

### Use of Interactive Graphics

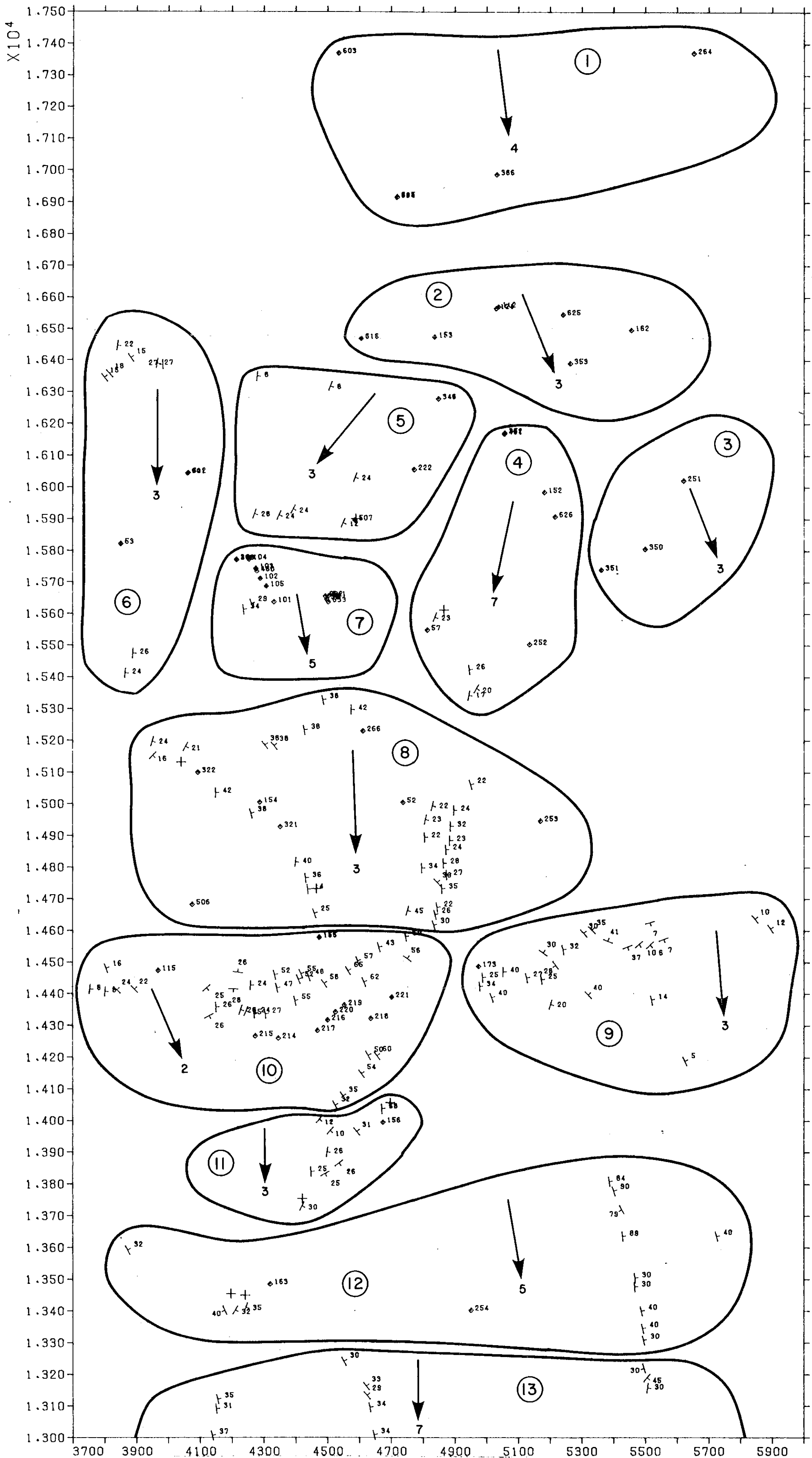
Interactive graphics can be used extensively when cylindrical domains cannot be defined statistically. Surface bedding orientations are examined and general trends of the structural grain are established. Data from specific areas are retrieved and plotted onto a profile. The size of the data set can be changed, the projection axis adjusted and the display updated immediately. This procedure is repeated until the geologist achieves a visual "best fit" of the data while using a projection axis that is compatible with the structural geology of the area.

Data from specific areas in Duke Pit was plotted onto profiles using the TRIPOD package and interactive graphics. Each data set was reviewed using several different projection axes and the data sets were enlarged or reduced until a data set size and a projection axis were combined to produce the most reasonable geological picture for a given area. This procedure was repeated for the entire Duke Pit Area. Thirteen structural domains (Map 3) were finally established. Down-plunge profiles of each structural domain were prepared and these plots were used during preparation of the structure contour grid on the base of B1 Seam.

### Composite Plots

Once the structural domains had been established, twelve composite cross-sections at 400 m spacing were prepared. Data from structural domains which straddled the cross-sections were projected parallel to their respective projection axes onto the cross-sections. The geology of Duke Pit was interpreted and drawn onto these cross-sections.

DOMAIN MAP



LEGEND

- ⑩ DOMAIN NUMBER
- PROJECTION AXIS
- 3 - TREND & PLUNGE

PEWEE CANADA RESOURCES

DUKE PIT

STRUCTURAL

DOMAIN MAP

DATE	BY	CHKD BY
1984	...	...
PROJECT NO.	...	...
SCALE	...	...

LAS

SCALE 1:10,000

### Interpretation

Structural domains defined in Duke Pit are shown on Map 3. The geology was interpreted on both the domain profiles and the twelve composite cross-sections. The subcrop geology from each of the cross-sections was plotted onto the geology maps and the three subcrop geology maps (Maps 6a, b, c) were prepared in this fashion.

### Structure Contour Maps

Structure contour maps can be generated from two data sources by using the TRIPOD package. Drillhole intersections and outcrops for a specific horizon can be retrieved and the elevations posted on a map. These values can then be machine or manually contoured.

The second method involves utilizing the down-plunge profiles prepared for each domain. The trace of the horizon of interest is drawn and digitized on each profile. This trace is then projected parallel to the projection axis to create a grid of data points representing the surface of interest. This grid of data points is then combined with the outcrops and drillhole intersections. If necessary, the grid values are adjusted to be compatible with the outcrop and drillhole values. The grid values and the intersected values can then be machine or manually contoured. The TRIPOD package also generates a dip direction and dip at each grid value, therefore it is advantageous to use a contouring package with an algorithm that utilizes orientation data as well as coordinate values.

Surface topography can also be incorporated into the grid of elevations. Overburden isopachs, seam isopachs, interburden and structure contour maps can be generated for any number of surfaces.

## 6.0 OVERBURDEN

The outcrop data locations and the drillhole information were combined to provide a depth of overburden data base. The interpreted data is represented in two methods, in planar view on Maps 5a, b and c and in section on each cross-section at 400 m spacing.



## 6.0 OVERBURDEN (cont'd)

On the south map sheet, a localized zone of till from 5 to 25 metres thick has covered a reserve area centred on 14200N, between 4500E and 5500E. A zone of till up to 15 m thick extends from this area in a northern direction onto the centre map sheet. The rest of the south sheet has nominal amounts of till according to the very sparse data base.

The centre sheet contains two areas with thick till. An area around 4500E between 14500N to 15200N contains up to 27 m of till. This irregular shaped area is defined by only two drillholes and urgently requires greater resolution. In all likelihood, it has been interpreted in a liberal method.

The main area with deep till lies in the northeast corner of the centre sheet and in a large area trending through the centre and eastern portion of north sheet. On the centre sheet the till attains a maximum thickness of 45 m along the northern boundary. Further to the northwest, on the north sheet, the area of deep till covers nearly two-thirds of the map sheet. This till attains a maximum thickness of 100 metres in a north trending linear zone immediately east of 5000E. The thick till will have a major bearing on pit design and coal extraction for the entire northern and eastern part of Duke Pit.

## 7.0 THE STRATIGRAPHY OF DUKE PIT AREA

### 7.1 Stratigraphic Nomenclature

During early exploration in the 1970's, the exploration staff used Stott's 1973 nomenclature. The stratigraphy used for this study, however, uses terminology adopted by Duff and Gilchrist (1981) for the southeast section of the Peace River Coalfield (Fig. 4). Extensive exploration throughout the coalfield in recent years has resulted in abandoning the Commotion Formation and elevation of the Gates, Hulcross and Boulder Creek to formational status. In addition, a marine sand and silt unit at the base of the Gates has been moved into the Moosebar Formation. The Torrens Member of the Moosebar Formation is an easily recognizable unit within the Moosebar Formation and is shown on the maps and cross-sections.

STRATIGRAPHIC NOMENCLATURE

HUGHES (1967)		STOTT (1973)		STOTT (1978, 1982?)		DUFF GILCHRIST (THIS REPORT)		
FT. ST. JOHN GROUP	COMMOTION FM.	MEMBER (IV)	COMMOTION FM.	BOULDER CR. MEMBER	FT. ST. JOHN GROUP	BOULDER CR. FORMATION	BOULDER CR. FORMATION	
		MEMBER (iii)		HULCROSS MEMBER		HULCROSS FM.	HULCROSS FM.	
		MEMBER (ii)	COMMOTION FM.	GATES MEMBER	FT. ST. JOHN GROUP	GATES FORMATION	GATES FM.	UPPER SILTY MBR
	MEMBER (i)	MOOSEBAR FORMATION						MOOSEBAR FORMATION
GATES MARINE TONGUE	SANDY COAL-BEARING MEMBER							
MOOSEBAR FORMATION	MOOSEBAR FORMATION	MOOSEBAR FORMATION	FT. ST. JOHN GROUP	MOOSEBAR FORMATION	MOOSEBAR FM.	TORRENS MBR.		
						SPIEKER MBR.		
						MUDSTONE MBR.		
						<table border="1" style="width: 100%; height: 100%;"> <tr> <td style="width: 50%;">LWR. SILTY MEMBER (GETHING MARINE TONGUE)</td> <td style="width: 50%;">CHAMBERLAIN MBR.</td> </tr> </table>	LWR. SILTY MEMBER (GETHING MARINE TONGUE)	CHAMBERLAIN MBR.
LWR. SILTY MEMBER (GETHING MARINE TONGUE)	CHAMBERLAIN MBR.							
CRASSIER GP.	GETHING FORMATION	BULLHEAD GP.	GETHING FORMATION	BULLHEAD GP.	GETHING FORMATION	BULLHEAD GP.	GETHING FORMATION	
	DRESSER FORMATION		CADOMIN FM.		CADOMIN FM.		CADOMIN FM.	
							N.W. ← → S.E.	

from Duff and Gilchrist, 1981

Fig. 4

## 7.2 The Minnes Group (Ju)

Although the Minnes Group (Nikinassin Formation equivalent) of Upper Jurassic Age does not outcrop within the map area, it underlies the coal measures everywhere within the project area. The Minnes Group is a thick (+1000 m) unit of generally recessive continental sediments that is mainly comprised of siltstone and sandstone but does contain conglomerate, shale, claystone and thin coal seams.

## 7.3 The Bullhead Group

The Bullhead Group of Lower Cretaceous Age was deposited following a major hiatus that occurred near the end of the Jurassic Period. The Group contains two formations, the Cadomin Formation and the overlying Gething Formation. Both units outcrop in the study area.

### Cadomin Formation

The Cadomin Conglomerate is one of the excellent marker horizons in the Inner Foothills of the Rocky Mountains between Luscar and the Pine Pass. It commonly consists of conglomerate pebbles and cobbles, sandstone matrix and silica cement. A major diagnostic feature in the Monkman area is the inclusion of extremely hard pebbles of green, grey and pink chert. The unit is harder than conglomerates in either the Gates or Gething and exhibits a flat gamma curve. Regionally, the Cadomin Formation varies from 35 m to 150 m. It is assumed to be 50 m thick in the Duke Pit Area.

### Gething Formation

In the Monkman Area, the Gething Formation consists of three units. A marine tongue representing the central unit is absent. The lower unit is comprised of mainly thin sands, silts and thin coal seams. The upper unit contains thick clean sandstones and conglomerates and thick continuous coal seams. All of the significant coal seams (A2 and A3) in the Duke Mountain Area lie within the upper unit. The Upper Gething contains, in general, cleaner sandstone units than does the Gates Formation. The clean sandstone at the top of the Gething is correlated to be the Bluesky Formation equivalent (Panchy, 1982).

### Gething Formation (cont'd)

The Gething Formation varies from 100 metres thick at Dokken Ridge to 155 metres in the Honeymoon Area and averages about 125 m thick (Panchy, 1982). Within the Duke Pit Area, Table 6.1 below indicates the Gething varies from 115 m to 150 m and averages about 130 m thick. The average thickness of 130 m is used on the cross-sections unless a local drill interval is available.

TABLE 7.1  
GETHING FORMATION THICKNESS

<u>Drillhole</u>	<u>True Thickness (m)</u>
MDD-7803	127.8
MDD-7807	126.5
MDD-7808	122.9
MDD-7703	150.1
MDH-8201	115.3
MDH-8204	144.7
	<u>131.0 (average)</u>

#### 7.4 The Fort St. John Group

The Fort St. John Group represents the major Lower Cretaceous ~~depositional sequence. It contains two marine transgressive phases and~~ two phases of predominantly continental clastic deposition. The major coal deposition in this portion of northeast B. C. occurs in the lower thick continental sequence that is sandwiched between two thick intervals of fine-grained marine sediments.

#### The Moosebar Formation (includes Torrens Member)

The Moosebar Formation was deposited during the southward transgression of the Moosebar Sea. In the Monkman Area, the Moosebar Formation consists of three units, a lower silty member that contains a diagnostic and persistent ash horizon (coded 'P' on the computer data files), a middle sandy member that grades upwards into a coarser-grained sequence and the upper Torrens Member. The Torrens Member is a clean sandstone deposited in a beach-bar environment. For the purposes of this report, the Torrens Member is shown as a separate zone of the Moosebar because it provides a resistant and easily recognizable marker horizon.

The Moosebar Formation (includes Torrens Member) (cont'd)

Duff and Gilchrist (1981) note the lower member is 15 m thick and the middle 120 metres thick at Babcock Mountain to the north. On Saxon Ridge, the lower unit is absent and the middle is only 70 metres thick. On the Duke Mountain Block of the Monkman Property, the combined lower and middle units (excluding the Torrens Member) average about 115 m thick. This is confirmed by the 119 metre thickness in MDH-7922 and the 110 metre thickness in MDD-7804. In this report, a thickness of 110 to 115 metres is commonly used.

The Torrens Member varies from 14 metres thick to over 30 metres. Numerous intersections of the Torrens Member provide adequate control, however where data is lacking a thickness of 20 m to 25 m is used.

Gates Formation

The Gates Formation is the thickest unit in the Lower Cretaceous and also the best understood because it contains the primary economic coal measures in this area. The data base for the Gates Formation on this property and adjoining properties (Quintette, Belcourt and Saxon) is very extensive.

According to Duff et al (1981), the Gates Formation consists of two members in the Monkman area. The lower Sandy Coal Bearing Member varies from 150 m to 170 m thick (thickening southwards). Local changes of 20 to 30 metres in thickness are common. Drillhole data at Duke Mountain suggest an average thickness of 190 m for this unit.

The Sandy Coal Bearing Member consists predominantly of mudstones and siltstones with numerous sandstone zones and thin claystone and shale units. Coal Seams B1 to B9 all occur within this unit. They are described in detail in Section 8. The correlation chart (Fig. 5) indicates the strata included in the Sandy Coal Bearing Member.

Conformably overlying the Sandy Coal Bearing Member is the Upper Silty Member. It is commonly about 50 m thick. The upper contact is gradational into the Hulcross (Stott, 1968) but shown to be unconformable by Carmichael (1983). The Upper Silty Member is comprised of fine-grained

Gates Formation (cont'd)

siltstone. Three coal seams (B10, B11 and B12) usually occur within this unit. B10 Seam and B12 Seam are persistent within the Pit Area, however B11 Seam does shale out occasionally.

The Gates Formation is shown by drillhole data to average 240 metres thick within Duke Pit (see Table 6.2 below). Where local drillhole definition is absent, a thickness of 240 metres is used.

TABLE 7.2  
GATES FORMATION UNIT THICKNESS

<u>Drillhole</u>	<u>Thickness (m)</u>
MDD-7822	251
MDD-7902	249
MDD-7905	241
MDD-7906	234
MDD-7914	<u>233</u>
	240 (average)

The Hulcross Formation

The Hulcross Formation represents a major marine incursion from the north and, accordingly, thins to the southeast. The lower contact is a fining upward sequence that may or may not be conformable with the underlying Gates Formation. The lower unit is a fining upward sequence that is characterized by thinly laminated siltstone that is dark in color and contains numerous very thin light colored fine-grained sand bands. This thinly laminated texture is a diagnostic feature that makes the Hulcross readily distinguishable from the Moosebar Formation. The Hulcross averages about 85 metres in thickness as evidenced by Table 6.3 below.

TABLE 7.3  
HULCROSS FORMATION THICKNESS

<u>Drillhole</u>	<u>Unit Thickness (m)</u>
MDD-7822	83.3
MDH-7912	84.6
MDD-7903	80.1
MDD-7906	86.3
MDH-7904	<u>80.5</u>
	83.0 (average)

### The Boulder Creek Formation (K1)

The Boulder Creek Formation is a remarkably consistent, clean conglomerate and sandstone unit containing rare fine-grained clastics and thin coal zones. None of the coal zones are recognized to have commercial importance. Because of the high coarse-grained silica content the unit is very resistant and commonly forms resistant ridges and provides a craggy capping to mountain tops such as Babcock Mountain and Duke Syncline area of Duke Mountain.

Duff et al (1981) notes the unit is from 107 m to 122 m in thickness with the thicker interval to the north. Plachner et al (1981) estimates the thickness to be 150 m. Where required, a general thickness of 150 m is used for the Boulder Creek Formation.

### Shaftsbury Formation (Ku)

The youngest strata in the project area is the Upper Cretaceous Shaftsbury Formation. This unit is predominantly shale that contains Belemnites. To the northwest, the unit partially grades into the Hasler Formation. No thickness is ascribed to this unit.

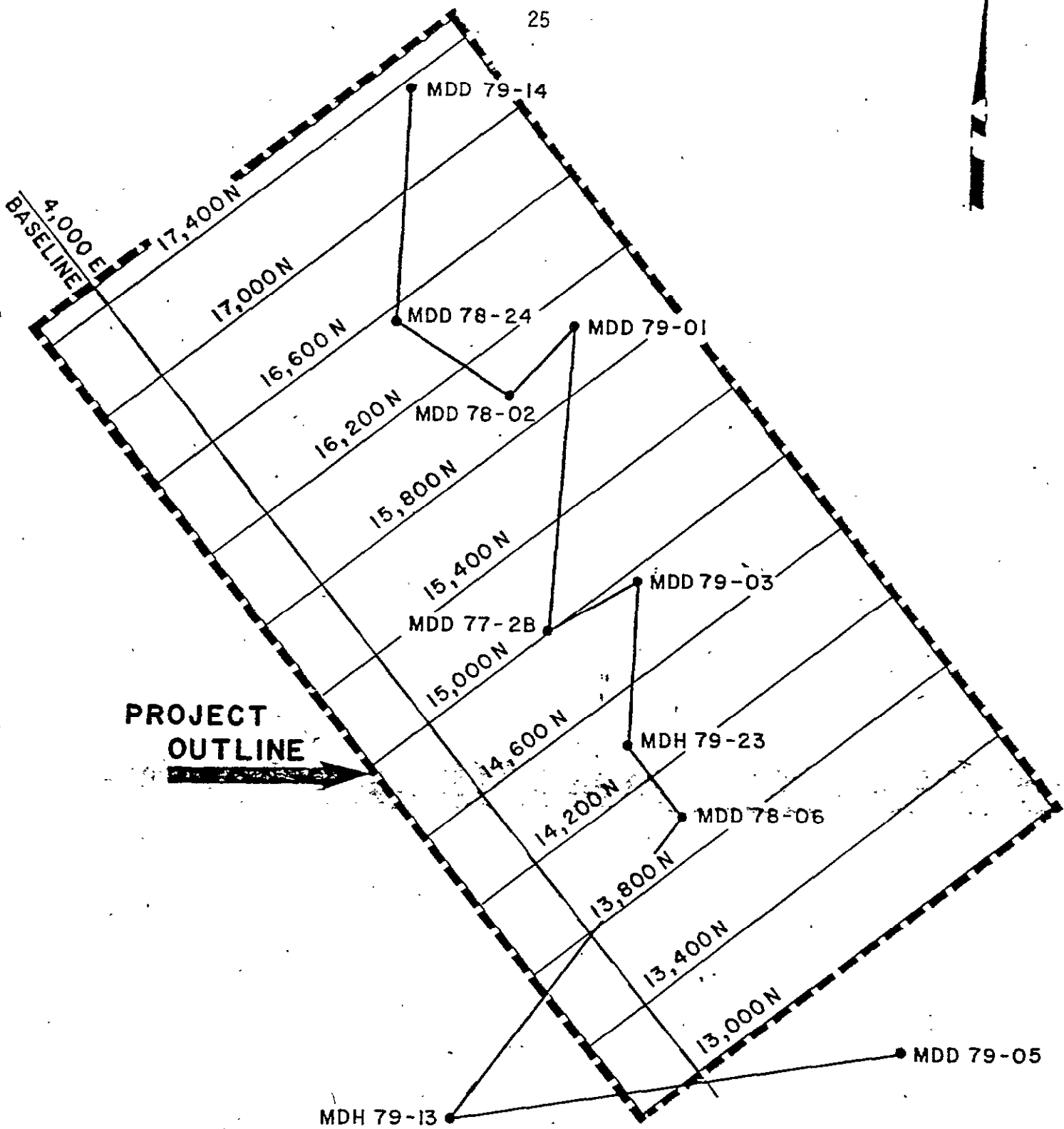
## 8.0 COAL SEAM DEVELOPMENT (see Fig. 5 and Map 4)

### 8.1 B1 Seam

B1 Seam usually lies less than 5 metres above the Torrens Sandstone and the base of the Gates Formation. The coal seam is continuous throughout the property and is a single clean coal zone at the south and north ends of Duke Pit. In the central part of the pit, up to two shale partings often occur. B1 Seam exhibits a thickening trend from southeast to northwest. South and west of Duke Pit, B1 Seam is less than 1 metre thick, and it thickens progressively north to Section 16000N where the thickness often exceeds 5 metres at the east side of the pit.

### 8.2 B2 Seam

B2 Seam is a thin reasonably continuous coal seam. It lies 15 m to 30 m above B1 Seam and contains a rock parting only in the area around



**PROJECT  
OUTLINE**

**PETRO-CANADA RESOURCES**

**DUKE PIT**

**DRILL HOLES USED IN CORRELATION CHART**

DESIGNED BY: SL	DRAWN: L.R.C.	DATE: 83/12
COMPILED BY: L.R.C.	CLIENT: APPL	DWG NO: JMAP 4
SCALE: HERE 1:25,000		FILE NO.

**LAS** & A. SMITH CONSULTING & DEVELOPMENT LTD



## 8.2 B2 Seam (cont'd)

Section 14000N. The seam is absent in the western portion of the northwest end of the pit. B2 Seam will not contribute a significant amount of coal reserves in any part of the pit due to its thin development.

## 8.3 B3 Seam

B3 Seam is a very persistent and major seam that will be mined in all areas of the pit. It lies from 15 m to 25 m above B2 Seam. Although it contains partings in all areas, it is unlikely that any of the rock partings can be wasted due to thin development. The seam varies from less than 4 metres thick to in excess of 12 metres with the thickest development occurring in areas where the coal seam appears structurally thickened. A thin coal zone sporadically occurs below the base of the main seam and will not be included in the pit reserves in any part of Duke Pit.

## 8.4 B4 Seam

B4 Seam is the thickest coal seam developed within Duke Pit. Within the pit area it varies from about 7 m to 15 m in thickness. There are three distinct parts to the coal seam. The lower zone is always the cleanest. This zone is separated from the central portion by a rock parting that starts at 15000N and thickens to about 2 m thick by Section 13000N. The central portion contains predominantly coal with a few thin partings. This zone does not achieve the low ash quality of the lower zone in any portion of the pit. It will represent pit reserves in all areas except the outcrop area (west portion) of Sections 14000N and 13000N. Here it shales to the west and is absent to the west of Duke Pit (see MDH 79-13 on Fig. 5). The upper coal zone is developed in Sections 17000N and 16000N and progressively shales to the south. At Section 15000N, the upper zone is represented by a slightly carbonaceous shale. It is absent further south. Detailed coal quality studies are required to establish where this upper zone will contribute coal.

A major period of siltstone deposition occurs above B4 Seam. The unit is 20 to 50 metres thick and is barren of coaly material.

### 8.5 B5 Seam

B5 Seam was deposited over a thick (20 m to 50 m) succession of fine-grained sediments. Although B5 Seam will, in all probability, provide plant feed in all areas of Duke Pit, two areas may provide coal with very high ash content. These areas are at both extreme ends of the pit, Section 13000N where the material is very shaly, and 17000N where, to the east of the pit, B5 Seam is extremely thin. Generally B5 Seam is 2 to 4 metres thick and commonly contains splits and partings.

### 8.6 B6 Seam

B6 Seam is a coal zone that is continuous throughout Duke Pit. It lies about 20 m above B5 Seam and is, in all localities, either two separate coal zones with a 1 m to 3 m parting, or else a single coal zone with the other undeveloped. It is unlikely that B6 Seam will contribute coal reserves to the mine.

### 8.7 B7 Seam

B7 Seam occurs in the western part of Duke Pit and overlies B6 Seam by 2 m to 15 m but usually about 8 m. B7 Seam is less than 3 m thick but is of mineable thickness in all areas except the east central portion of Duke Pit.

### 8.8 B8 Seam

B8 Seam represents a continuous but thin and dirty coal zone. At the north end of the pit, it immediately overlies B7 Seam. At the south end of Duke Pit, it is separated from B7 Seam by about 30 m of rock. B8 Seam will not likely contribute coal to run of mine coal reserves.

### 8.9 B9 Seam

B9 Seam varies from 1.5 m to 4 m thick in the Duke Pit Area. It is likely that it will contribute reserves. It is generally quite clean with only rare partings and splits. At the very south end of the pit it attains a maximum thickness of greater than 4 m. To the west of Section 13000N, it is split into two zones that together represent in excess of 5 m of coal.

### 8.10 Upper Seams (B10, B11 & B12)

In the upper 50 m to 80 m of Gates Strata (and equivalent to the Upper Silty Member of Duff et al, 1981), three coal seams occur. The lowest, B10, is thin and persistent throughout. The middle seam, B11, is thin and split in some localities. It is absent in some locations around 16000N and is split into two coal seams at Section 15000N and 15400N. B12 Seam is always present and always thin, generally less than 1 m. It is unlikely that these 3 seams will represent mineable coal reserves except in isolated localities.

### 8.11 Structurally Thickened Coal

In those areas of the pit where the structures are very tight and complex, structural thickening of the coal seams is indicated. In particular, the hinge zone of Quintette Syncline between Sections 16200N and 17000N appears to contain structurally thickened coal seams. Additional drilling will undoubtedly identify local areas with structurally thickened coal seams.

## 9.0 STRUCTURAL GEOLOGY OF DUKE PIT

### 9.1 Introduction

The structural geology of the coal-bearing strata in Duke Pit is a complex association of folding and thrust faulting. The earliest phase of structural deformation appears to be thrust faulting. This was followed by folding and continued development of the thrusts.

The study area is bounded to the east by the Quintette Thrust. Strata in this thrust sheet ranges from Minnes Formation to Hulcross Formation rocks. The Duke Thrust Fault, which is a splay from Quintette Thrust, overlies the Quintette Thrust Sheet. Minnes to Shaftsbury Strata lie within the Duke Thrust Sheet.

Folding during and after thrusting altered the geometry of the rocks within the two thrust sheets. From east to west the major folds are Quintette Syncline, Duke Anticline and Duke Syncline. Duke Anticline and Duke Syncline lie to the west of the study area. The steep orientation of

### 9.1 Introduction (cont'd)

Quintette and Duke Thrusts at the subcrop are due to the later phase of folding. The surfaces of both thrust faults have been folded below the strata of Duke Pit. Thrusting continued during this period of folding, as evidenced by the variation in the geometry of the folded strata in each of the thrust sheets.

The mechanism of folding is flexural slip movement. It has resulted in structural thickening of the coal seams with associated shortening in the more competent units by small thrusts and folds.

### 9.2 Quintette Thrust Sheet

Drillhole MDD 78-12 suggests that the Quintette Thrust Fault is a major structure separating the Duke and Honeymoon areas. Moosebar strata overlies badly fractured and sheared Boulder Creek rocks. The stratigraphic throw on the fault is estimated to be in the order of 400 to 500 m, however, there is very little information to confirm this. The Quintette Thrust overlies the entire Duke Pit and Duke Mountain Area. The fault developed early in the structural history of the area and was folded during later structural deformation. It has probably originated as a splay from a deeper seated sole thrust, that may be located in the underlying Fernie Formation.

Near the subcrop in the north end of the study area, the thrust dips to the west at about 60°. It steepens to approximately 65° near Section 16600N and then shallows to 40° to 50° in a southerly direction. This thrust gradually cuts up section in a southerly direction. At the north end of the study area, Moosebar Strata to B3 Seam subcrops in the Quintette Thrust Sheet whereas further to the south, B4 to B9 Seams subcrop. The surface trace of the thrust extends off the map sheet in a southeasterly direction near Section 15400N. It continues in this direction for an unknown distance.

### 9.3 Duke Thrust Sheet

The Duke Thrust Fault has probably developed as a splay from Quintette Thrust. The stratigraphic throw is estimated to be approximately 100 m.

### 9.3 Duke Thrust Sheet (cont'd)

In the north end of the study area, the fault dips to the west at about 60°. It steepens to about 65° near section 16600N and then becomes slightly shallower to about 55° to the south. This thrust is folded below Duke Pit and may reverse its orientation to east dipping further to the west.

Coal seams located in the footwall strata of Duke Thrust may be structurally thickened near the plane of the thrust. Along Section 17000N the footwall strata are folded into a tight syncline and Duke Thrust terminates the western limb of the syncline close to the hinge zone. Both B3 and B4 Seams appear to be structurally thickened (MH-8066).

Duke Thrust cuts up section to the southeast. Strata sub-cropping against the surface trace of the thrust range from Moosebar Strata in the north to Hullcross Strata near Section 15000N. South of Section 14600N, the thrust extends off the map sheet to the southeast.

Drillholes MDD 78-02, MH 80-51 and MH 80-66 intersect and define the thrust fault. Additional information is available in the footwall of the thrust from drillholes MDD 79-01, MH 80-50 and MH 80-53. This limited data base is inadequate to define the structure in anything but an approximate manner.

### 9.4 Quintette Syncline

Most of the Duke Pit Study Area lies in Quintette Syncline. The western limb of the structure forms a dip slope along the eastern slope of Duke Mountain and the eastern limb is truncated by Duke Thrust Fault. The geometry and structural geology of the syncline changes dramatically from north to south. In the north end, it is a tight fold closely associated with thrusting, and in the south it is an open less complex structure.

The fold axes (projection axes) and structural domains, shown on Map 3, are only approximations. They have been determined by interactive graphics and honor the data base, but they have no statistical basis. Consequently, additional data collection and geological interpretation will alter these values, and as a result refine the structural interpretation to a greater degree.

#### 9.4 Quintette Syncline (cont'd)

Generally, the syncline trends at approximately  $175^\circ$  and plunges south at  $5^\circ$ . This trend and plunge is fairly constant south of Section 15400N except for Sections 14600N and 14200N west of 4900E. Here the structure is complicated by a small thrust (drillhole MDH 79-21) which repeats Seams B6 and B7 in the subsurface. Seams B8 and B9 are probably repeated near the surface (Map 5b). The fault is interpreted to flatten into an underlying coal seam (B5). It may repeat additional strata lower down in the stratigraphic succession.

The mechanism of structural deformation appears to be flexural slip movement. This is confirmed by the large number of small scale faults and bedding plane slickenside striae noted in the core descriptions. Small thrusts can be expected to be common in the limbs and hinge zone of the syncline. Mesoscopic scale structural features and areas of coal zone thickening have not been represented on the cross-sections because the limited data base prevents adequate definition of these structures.

North of Section 15400N the structural geology of Quintette Syncline becomes more complex. The central portion of the structure ~~continues to plunge to the south but the trend has changed to about  $190^\circ$ ,~~ whereas the western limb of the structure becomes much steeper and trends at  $220^\circ$ . Near Section 16200N the syncline fold axis trends about  $160^\circ$  and plunges at about  $3^\circ$ . Here the fold becomes very tight. Between Sections 16200N and 16600N the fold axis trends at  $160^\circ$  but the plunge flattens to  $0^\circ$ . Further north, the syncline axis trends at  $170^\circ$  and plunges  $4^\circ$  to the south.

An easterly dipping thrust fault with about 70 m of stratigraphic throw is present in the Moosebar Formation in drillhole MDD 78-03. The origin of the fault is uncertain. It may have developed as a shortening mechanism in the Moosebar Formation due to the tight folding or it may be a more significant thrust related to deeper structural features. Almost certainly the abrupt change in the orientation of the syncline and the steepening of the limbs of the syncline are related to underlying structural changes. These changes may be related to a change in the geometry or the nature of the underlying thrust faults.

#### 9.4 Quintette Syncline (cont'd)

The hinge zone of Quintette Syncline has not been drilled. Coal seams may be structurally thickened in the hinge zone, particularly where the structure changes trend and in the north, where it is very tight (Map 5c). B3 Seam is structurally thickened in drillhole MDD 78-02 (Section 16200N). B4 Seam is very thick in this hole but it appears to be stratigraphic rather than structural thickening.

#### 9.5 Structure Contour Maps, Base of B1 Seam

Structure contour maps were prepared on the base of B1 Seam for both the Quintette and Duke Thrust Sheets. Elevations of B1 Seam in the Duke Thrust Sheet range from a minimum of 585 m in the centre of Quintette Syncline to 1560 m on the southern end of the eastern limb of the syncline. The base of B1 Seam has been encountered by twenty drillholes in the Duke Thrust Sheet. The data points are poorly distributed on the map sheets with four in the south, twelve in the centre and four in the north, respectively. Many of the data points are closely grouped, especially on the centre sheet. Considering the limited data base, the structure contours on the base of B1 Seam can be defined in only an approximate manner. Elevations of B1 Seam in Quintette Thrust Sheet range from 915 to 600 m.

Two data points are located on the centre map sheet and one on the north sheet. The structure contour maps on the base of B1 Seam in the Quintette Thrust Sheet are, accordingly, only an approximation.

The structure contour maps confirm the structural trends discussed in the Sections 9.2 to 9.4. In the Quintette Thrust Sheet, the structure contour maps indicate a reversal of the plunge of Quintette Syncline between Sections 16600N and 16200N. Here the syncline axis trends at  $330^{\circ}$  and plunges  $14^{\circ}$ . With the exception of this area, Quintette Syncline plunges in a southerly direction in both Duke and Quintette Thrust Sheets.

## 10.0 EXPLORATION REQUIREMENTS

### 10.1 Exploration Concepts

The role of exploration in a pit is to provide a geological interpretation in sufficient detail and at a level of confidence suitable for the required engineering studies. At present, the data base for Duke Pit is sufficient to provide an interpretation on 1:2000 scale, but lacks the level of confidence required for detailed mine planning. Prior to detailed mine planning, additional data collection and interpretation is necessary to resolve certain problems identified by this and other studies. In addition, exploration is required to confirm possible reserve extensions in at least two areas.

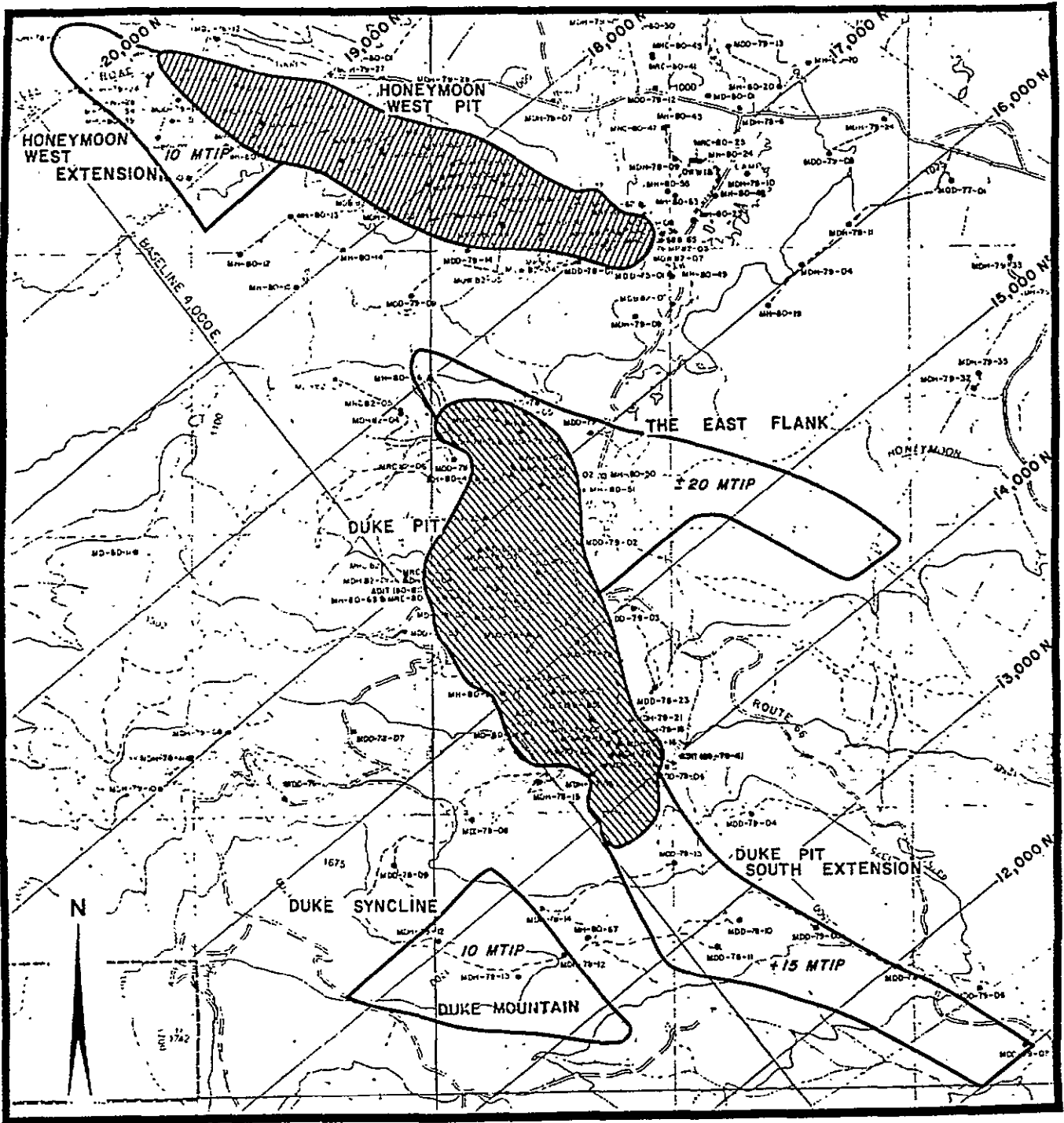
### 10.2 Geological Mapping

All of the outcrop data has been collected on 1:5000 scale without careful identification of stratigraphic horizons, collection of multiple orientations and proper plotting of the outcrop locations. This data must now be re-collected because the requirements call for detailed geology for mine planning purposes. Attention must be paid to detailed geology and additional traverses are required to collect data in many areas not already mapped. It is estimated that 20 to 30 days with a two-man crew (geologist and assistant) will be sufficient to collect all the outcrop data that is available.



### 10.3 Reserve Extensions (see Map 8)

Indicated reserve extensions in two areas, Duke Pit South Extension and The East Flank on Sections 14000N to Section 17000N, require evaluation for probable reserve additions. These areas are significant because they could provide up to a 35 megatonne in-place reserve expansion within Duke Pit. The 3000 m zone from Section 12000N to 11000N has an adequate data base for a preliminary evaluation of the Duke Pit South Extension. The East Flank portion of Duke Pit will require additional drilling information to prove and delineate the reserve area. The drill program should be designed to progressively test the structures both in an easterly direction (along section) and in a south-easterly direction (along structural trend) in order to fully delineate the potential reserve area.

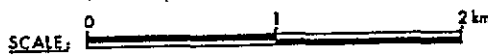








Legend

-  Recognized Reserve Area
-  Potential Reserve Addition

Note:  
RESOURCES LISTED AS MTIP  
(MEGATONNES IN PLACE)



PETRO-CANADA RESOURCES	
	DUKE PIT POTENTIAL RESERVE ADDITIONS
	
	BASE MAP
	DATE

### 10.3 Reserve Extensions (see Map 8) (cont'd)

Two smaller, but potentially significant open pit reserve areas that require evaluation are the Gates coal measures at the south end of Duke Syncline and the Gates and Gething coal measures at the north end of Quintette Syncline (Honeymoon West Extension). The Duke Syncline prospect has potential for a mining situation similar to 4 Pit at Tent Mountain. The backwall area progressively reaches higher ratios and the cutoff can be chosen at an economically attractive position. An estimate of up to 10 megatonnes in-place coal resource awaits evaluation. The Honeymoon West Extension is of interest because the very steep structure at the nose of Honeymoon Syncline will likely contain structurally thickened coal zones within the hinge zone. Possible coal resources in the order of 5 to 10 megatonnes in-place may occur and add significantly to the Honeymoon West reserve.

### 10.4 Drilling Requirements

#### Duke Pit South Sheet

In order to provide a suitable reserve definition, additional rotary drilling with spot coring is recommended as follows:

TABLE 10.1

#### SOUTH SHEET DRILLING REQUIREMENTS

<u>Section</u>	<u>No. of Drillholes</u>
1300N	3
1350N	2
1400N	1
1450N	<u>1</u>
Total:	7

The above drilling will provide sufficient detail to place all open pit coal reserves into the probable category, and a large portion will be proven. Additional definition would not be required until pre-development drilling commences.

#### 10.4 Drilling Requirements (cont'd)

##### Duke Pit Centre Sheet

There are several problems that require resolution in the centre sheet. Of paramount importance is resolution of the East Flank geology. Along the West Flank (Duke Pit as presently defined), additional work must be performed to define the fault structures. The amount of drilling required for proper definition of the East Flank will depend upon the size, complexity and reserve potential of that very interesting resource area.

##### Duke Pit North Sheet

Drilling requirements in the north sheet are necessary to solve two related problems - definition of the complicated structures and to outline the mineable reserve areas. This program will have to be well planned and coordinated with engineering input to ensure that the areas with mineable reserves are properly defined. All three fault structures require definition throughout the reserve area, the fold hinge and limbs require definition, and the coal-bearing strata must be drilled to the north beyond the pit endwall. In addition, the overburden thickness must be defined in greater detail. The drill program should be used in conjunction with a surface geophysical program.

#### 10.5 Surface Geophysics

Surface geophysical techniques can be used to provide information concerning subcrop geology, bedrock topography and till thickness and composition. Seismic, resistivity and EM surveys may be employed. A combination of several techniques is often necessary in areas with rapid variations in overburden thickness and the extremely thick zones of till encountered in some areas. These techniques should be reviewed by Petro-Canada mining staff as a possible method of rapidly and inexpensively mapping the till thickness in the northern part of Duke Pit.

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A P P E N D I X I

STRATIGRAPHIC CODE

DUKE MOUNTAIN STRATIGRAPHIC CODE

Shaftsbury Formation	S
Boulder Creek Formation	B
Hullcross Formation	H
Tonstein Bed	Q
Gates Formation	G

SEAMS

Base 12 Seam	Z
Base 11 Seam	Y
Base 10 Seam	X
Base 9 Seam	9
Base 8 Seam	8
Base 7 Seam	7
Base 6 Seam	6
Base 5 Seam	5
Base 4 Seam	4
Base 3 Seam	3
Base 2 Seam	2
Base 1 Seam	1
Unidentified	U
Torrrens Member	T
Moosebar Formation	M
k-ash bed	P
Gething Formation	E
Base of Gething Coal Seam	O
Cadomin Formation	C
Minnes Group	N
Fault	F

A P P E N D I X I I

DRILLHOLE NUMBERING CODE.



DRILLHOLE NUMBERING CODE

<u>Computer File Drillhole No.</u>	<u>Petro-Canada Drillhole No.</u>	<u>Computer File Drillhole No.</u>	<u>Petro-Canada Drillhole No.</u>
1	MQD 75-01	214	MDH 79-14
11	MDD 76-11	215	-15
52	MDD 77-02B	216	-16
53	MDD 77-03	217	-17
57	MDD 77-07		
58	MDD 77-08	218	MDH 79-18
		219	-19
101	MDH 78-01	220	-20
102	MDH 78-02	221	-21
103	MDH 78-03		
104	-04	222	MDH 79-22
105	-05	226	-26
112	-12	232	-32
114	-14	235	-35
115	-15		
121	-21	251	MDD 79-01
		252	-02
151	MDD 78-01	253	-03
152	-02	254	-04
153	-03	255	-05
154	-04		
		256	MDD 79-06
155	MDD 78-05	259	-09
156	-06	264	-14
157	-07	266	-16
158	-08		
		307	MH 80-07
159	MDD 78-09	308	-08
160	-10	310	-10
161	-11	312	-12
162	-12	313	-13
		314	-14
163	MDD 78-13	315	-15
172	-22	317	-17
173	-23		
174	-24	319	MH 80-19
		321	-21
204	MDH 79-04	322	-22
205	-05		
208	-08	334	MH 80-34
209	-09	338	-38
		339	-39
210	MDH 79-10	340	-40
211	-11		
212	-12	346	MH 80-46
213	-13	349	-49
		350	-50
		351	-51

<u>Computer File Drillhole No.</u>		<u>Petro-Canada Drillhole No.</u>
352		MH 80-52
353		-53
357		-57
366		MH 80-66
367		-67
368		-68
442		MRC 80-42
444		-44
459		-59
460		-60
461		-61
469		-69
506		MD 80-06
507		-07
511		-11
601		MDH 82-01
603		-03
604		-04
612		MRC 82-02
615		-05
616		-06
621	O.B.	MOB 82-01
622	O.B.	-02
625	O.B.	-05
626	O.B.	-06
632		MOW 82-02
633		-03
634		-04
635		-05
641		MP 82-01
642		-02

A P P E N D I X I I I

DUKE PIT RAW DATA

OUTCROP AND DRILLHOLE DATA

V	30	G1	5883	17787	945
V	450	G1	5896	17746	950
V	331	G1	6169	17589	943
V	431	G1	6170	17550	942
V	334	H1	2992	13605	1658
V	452	H1	3014	13552	1663
V	453	H1	3052	13493	1640
V	446	H1	4622	13163	1540
V	454	H1	4624	13134	1554
V	447	H1	4633	13096	1568
V	455	B1	4646	13009	1571
V	450	A1	4155	13122	1600
V	456	A1	4151	13092	1599
V	455	H1	4769	12554	1520
V	457	H1	4823	12475	1526
V	454	H1	4766	12440	1509
V	455	H1	4819	12404	1516
V	455	H1	4857	12383	1518
V	459	H1	4834	12366	1510
V	460	H1	4847	12305	1495
V	461	E1	3798	12590	1466
V	461	E1	3818	12561	1460
V	462	E1	3818	12546	1459
V	463	E1	3839	12497	1457
V	465	E1	3610	12603	1445
V	464	E1	3604	12580	1442
V	466	E1	3577	12489	1431
V	465	E1	3613	12466	1426
V	466	E1	3618	12433	1419
V	189	C1	4046	17850	1075
V	467	C1	4049	17817	1075
V	194	C1	3294	17659	1138
V	468	C1	3357	17642	1146
V	469	C1	3409	17650	1147
V	195	N1	3227	17727	1099
V	470	N1	3249	17686	1115
V	196	C1	3265	17564	1152
V	471	C1	3349	17531	1122
V	198	C1	3198	17450	1186
V	472	C1	3195	17428	1202
V	473	C1	3206	17417	1202
V	474	C1	3221	17396	1202
V	199	C1	3140	17393	1222
V	475	C1	3101	17390	1224
V	201	C1	2889	17363	1277
V	476	C1	2847	17335	1284
V	477	C1	2806	17319	1288
V	202	C1	2777	17228	1285
V	478	C1	2737	17315	1282
V	479	C1	2689	17298	1286
V	223	E1	3965	16390	1121
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V	481	E1	3882	16408	1130
V	223	E1	3815	16357	1157
V	482	E1	3799	16345	1162
V	223	E1	3579	16331	1201
V	483	E1	3601	16234	1220
V	223	E1	3378	16087	1267
V	484	E1	3350	16077	1273
V	223	E1	4510	16319	1276
V	485	E1	4288	16350	1323
V	224	G1	2907	15221	1515
V	486	G1	2937	15196	1514
V	488	G1	2779	15232	1540
V	341	G1	4349	15912	1125
V	489	G1	4393	15931	1155
V	342	G1	4233	15613	1167
V	490	G1	4262	15633	1166
V	350	G1	4304	15188	1188
V	491	G1	4333	15183	1182
V	351	M1	3889	15475	1274
V	492	M1	3865	15413	1275
V	352	M1	3950	15197	1275
V	493	M1	3952	15153	1290
V	344	G1	4946	15424	1068
V	494	G1	4969	15365	1067
V	495	G1	4945	15344	1072
V	357	G1	4431	14766	1269
V	496	G1	4438	14730	1270



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V	17	C1	3715	2066	6610	207
V	18	C1	3758	2057	1198	877
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V	20	S1	6945	1412	2510	079
V	21	S1	7106	1393	3910	944
V	22	S1	7484	1377	1910	092
V	23	S1	7424	1383	3410	086
V	24	S1	7474	1379	2210	085
V	25	S1	7420	1379	3311	101
V	26	S1	7437	1377	5511	103
V	27	S1	7520	1346	6671	105
V	28	S1	8366	1268	8611	118
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V	30	G1	6123	1747	2299	744
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V	32	G1	3227	1355	1316	333
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V	35	T1	3872	1359	2215	519
V	36	G1	4420	1373	3311	376
V	37	A1	4242	1345	0146	655
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V	39	A1	4244	1341	2214	881
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V	42	A1	4551	1324	2215	519
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V	68	N1	1382	1863	4410	188
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V	79	E1	1179	1863	3810	188
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V 4811  
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7544  
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27245  
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8962  
7762  
7440  
9157  
7949  
6618  
10220  
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26840  
23953  
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25137  
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26343  
26144  
24535  
24047  
22743  
21130  
24235  
24748  
24044  
26160  
24450  
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23818  
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29729  
23826  
24142  
24040  
24258  
23440

















>	15889	30	55
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>	15999	102	147
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>	15999	121	187
>	15999	13T	195
>	15999	14M	224
>	16009	1	11
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>	16009	9	134
>	16009	10	138
>	16009	11	141
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>	16009	13	155
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>	16009	162	187
>	16009	17	221
>	16009	181	211
>	16009	19T	215
>	1619	1	23
>	1619	2	27
>	1619	3	30
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>	1619	5	44
>	1619	63	47
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>	1619	81	102
>	1619	9T	106
>	1619	10M	138
>	1619	11P	200
>	1629	1H	200
>	1639	1	27
>	1639	2	30
>	1639	3	33
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>	1639	7	102
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>	1639	9T	107
>	1639	10M	137
>	1729	1H	19
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>	1729	3	112
>	1729	4Z	112
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>	1729	8X	151
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>	1729	16	241
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>	1729	186	245
>	1729	19	257
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V	3679	90	133	.6
V	3679	100	133	.6
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V	4429	27	322	.4
V	4429	33	488	.2
V	4429	44	499	.4
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V	4429	66	556	.3
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V	4429	85	755	.8
V	4429	99	107	.3
V	4429	104	113	.5
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V	4429	133	171	.5
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V	4449	11	220	.4
V	4449	29	222	.9
V	4449	35	266	.2
V	4449	48	311	.0
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V	4449	125	111	.9
V	4449	133	117	.3
V	4449	144	124	.3
V	4449	155	145	.1
V	4449	163	149	.0
V	4449	177	183	.6
V	4449	181	186	.6
V	4699	11	100	.5
V	4699	22	122	.0
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V	4699	42	166	.1
V	4699	55	199	.0
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V	4699	81	224	.8
V	4699	99	226	.8
V	1149	1P	122	.5
V	1149	2E	552	.0
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V	1149	55	911	.8
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2 240236 2 253231 2 256225 2 270227 2 290238 2 293239 2 310  
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1048      1018      4333 15637114732989 -49 12 15329 1 25231 1 3  
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5 98 2 48 48 1  
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1051      2168      4501 14317127322089 -110 10 20220 4 40220 5 6  
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1052      2178      4469 142841279 9999 -61 21 22 99 3 24100 3 3  
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9 130289 8 131291 8  
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 2 150 5024 160 5027 171 4427 177 4028 181 3830 190 3528 205  
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 6 150 817 165 518 180 1017  
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 0 97 9 45 9717 55 9729 60 9730 75 9743 90 9743 105 241  
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1109	<u>5118</u>	2797	172981286	090	428	3	0
1110	<u>6158</u>	4720	169171032	090	157	45	0
1111	<u>6328</u>	4494	156551120	090	148	3	0
1112	<u>1518</u>	6301	16999 992	090	267	35	
1113	<u>1608</u>	4388	129331576	090	240	5	
1114	<u>2568</u>	5422	115161353	090	435	12	
1115	<u>2648</u>	5653	17371 965	090	386	68	
1116	<u>1028</u>	4290	157121151	090	31	2	
1117	<u>1148</u>	3456	138191508	090	184	9	
1118	<u>2058</u>	5512	18053 947	090	269	18	
1119	<u>2128</u>	2739	140651629	090	232	6	
1120	<u>2138</u>	3067	135231642	090	239	0	
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1123	<u>3408</u>	6037	17484 978	090	183	6	
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1125	<u>3688</u>	4215	157721159	090	32	6	
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1127	<u>4428</u>	6186	17254 977	090	181	14	
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1129	<u>4698</u>	4216	157721158	090	31	6	
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1131	<u>6228</u>	6587	163431001	090	67	66	
1132	<u>6258</u>	5242	165461007	090	91	89	
1133	<u>6268</u>	5217	159081020	090	34	29	
1134	<u>6348</u>	6026	17293 978	090	254	15	
1135	<u>6358</u>	6017	17324 979	090	252	15	
1136	<u>6428</u>	6034	17299 979	090	252	13	
1137	<u>3678</u>	3563	134131604	090	165	1	

A P P E N D I X I V

DUKE PIT COMPILED DATA

OUTCROP AND DRILLHOLE DATA







>	OUTCROP	33								
>	B 1-	2921.	13705.	1670.	0	0	0	0.	1	
>	178	0	0	0	0	0	0			
>	265 57	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	34								
>	H 1-	2992.	13605.	1658.	0	0	0	0.	1	
>	6	0	0	0	0	0	0			
>	227 32	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	35								
>	G 1-	3227.	13513.	1633.	0	0	0	0.	1	
>	179	0	0	0	0	0	0			
>	233 52	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	36								
>	M 1-	3487.	13613.	1580.	0	0	0	0.	1	
>	180	0	0	0	0	0	0			
>	241 43	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	37								
>	M 1-	3588.	13602.	1560.	0	0	0	0.	1	
>	181	0	0	0	0	0	0			
>	86 28	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	38								
>	T 1-	3872.	13592.	1519.	0	0	0	0.	1	
>	182	0	0	0	0	0	0			
>	63 32	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	39								
>	G 1-	4420.	13731.	1376.	0	0	0	0.	1	
>	183	0	0	0	0	0	0			
>	117 30	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	40								
>	4 1-	4242.	13450.	1465.	0	0	0	0.	0	
>	184	0	0	0	0	0	0			
>	0 0	0.0	0.0	0.0	0	0	0			
>	OUTCROP	41								
>	3 1-	4197.	13455.	1465.	0	0	0	0.	0	
>	185	0	0	0	0	0	0			
>	0 0	0.0	0.0	0.0	0	0	0			
>	OUTCROP	42								
>	G 1-	4244.	13412.	1481.	0	0	0	0.	1	
>	186	0	0	0	0	0	0			
>	111 35	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	43								
>	3 1-	4211.	13403.	1490.	0	0	0	0.	1	
>	187	0	0	0	0	0	0			
>	120 32	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	44								
>	3 1-	4178.	13402.	1490.	0	0	0	0.	1	
>	188	0	0	0	0	0	0			
>	246 40	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	45								
>	G 1-	4551.	13242.	1515.	0	0	0	0.	1	
>	189	0	0	0	0	0	0			
>	62 30	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	46								
>	H 1-	4622.	13163.	1540.	0	0	0	0.	1	
>	9	0	0	0	0	0	0			
>	52 33	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	47								
>	H 1-	4633.	13096.	1568.	0	0	0	0.	1	
>	11	0	0	0	0	0	0			
>	79 34	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	48								
>	B 1-	4715.	12899.	1552.	0	0	0	0.	1	
>	190	0	0	0	0	0	0			
>	69 39	1.0000	0.0	0.0	0	0	0			

>	>OUTCROP	49							
>	H 1.	4611.	12954.	1564.	0	0	0	0.	1
>	191	0	0	0	0	0	0		
>	67 39	1.0000	0.0	0.0	0	0	0		
>	>OUTCROP	50							
>	4 1.	4155.	13122.	1600.	0	0	0	0.	1
>	13	0	0	0	0	0	0		
>	77 35	1.0000	0.0	0.0	0	0	0		
>	>OUTCROP	51							
>	4 1.	4138.	13007.	1587.	0	0	0	0.	1
>	192	0	0	0	0	0	0		
>	76 37	1.0000	0.0	0.0	0	0	0		
>	>OUTCROP	52							
>	4 1.	4221.	12841.	1560.	0	0	0	0.	1
>	193	0	0	0	0	0	0		
>	59 36	1.0000	0.0	0.0	0	0	0		
>	>OUTCROP	53							
>	H 1.	4769.	12554.	1520.	0	0	0	0.	1
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>	72 38	1.0000	0.0	0.0	0	0	0		
>	>OUTCROP	54							
>	H 1.	4766.	12440.	1509.	0	0	0	0.	1
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>	71 38	1.0000	0.0	0.0	0	0	0		
>	>OUTCROP	55							
>	H 1.	4857.	12383.	1518.	0	0	0	0.	1
>	19	0	0	0	0	0	0		
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>	194	0	0	0	0	0	0		
>	60 34	1.0000	0.0	0.0	0	0	0		
>	>OUTCROP	57							
>	E 1.	3798.	12590.	1466.	0	0	0	0.	1
>	22	0	0	0	0	0	0		
>	62 20	1.0000	0.0	0.0	0	0	0		
>	>OUTCROP	58							
>	E 1.	3628.	12647.	1453.	0	0	0	0.	1
>	195	0	0	0	0	0	0		
>	280 50	1.0000	0.0	0.0	0	0	0		
>	>OUTCROP	59							
>	E 1.	3610.	12603.	1445.	0	0	0	0.	1
>	26	0	0	0	0	0	0		
>	258 50	1.0000	0.0	0.0	0	0	0		
>	>OUTCROP	60							
>	E 1.	3662.	12529.	1442.	0	0	0	0.	1
>	196	0	0	0	0	0	0		
>	244 50	1.0000	0.0	0.0	0	0	0		
>	>OUTCROP	61							
>	E 1.	3635.	12441.	1427.	0	0	0	0.	1
>	197	0	0	0	0	0	0		
>	276 40	1.0000	0.0	0.0	0	0	0		
>	>OUTCROP	62							
>	E 1.	3577.	12489.	1431.	0	0	0	0.	1
>	28	0	0	0	0	0	0		
>	260 56	1.0000	0.0	0.0	0	0	0		
>	>OUTCROP	63							
>	E 1.	3611.	12340.	1407.	0	0	0	0.	1
>	198	0	0	0	0	0	0		
>	256 50	1.0000	0.0	0.0	0	0	0		
>	>OUTCROP	64							
>	C 1.	4637.	11518.	1313.	0	0	0	0.	1
>	199	0	0	0	0	0	0		
>	76 26	1.0000	0.0	0.0	0	0	0		

> OUTCROP	65								
> M 1-	4446.	11543.	1325.	0	0	0	0.	1	
> 200	0	0	0	0	0	0	0		
> 92 56	1.0000	0.0	0.0	0	0	0			
> OUTCROP	66								
> E 1-	4411.	11041.	1438.	0	0	0	0.	1	
> 201	0	0	0	0	0	0			
> 78 33	1.0000	0.0	0.0	0	0	0			
> OUTCROP	67								
> E 1-	4327.	11101.	1285.	0	0	0	0.	1	
> 202	0	0	0	0	0	0			
> 75 24	1.0000	0.0	0.0	0	0	0			
> OUTCROP	68								
> E 1-	4220.	11034.	1256.	0	0	0	0.	1	
> 203	0	0	0	0	0	0			
> 66 24	1.0000	0.0	0.0	0	0	0			
> OUTCROP	69								
> N 1-	1291.	19330.	994.	0	0	0	0.	1	
> 204	0	0	0	0	0	0			
> 266 24	1.0000	0.0	0.0	0	0	0			
> OUTCROP	70								
> N 1-	1353.	19233.	1110.	0	0	0	0.	1	
> 205	0	0	0	0	0	0			
> 252 23	1.0000	0.0	0.0	0	0	0			
> OUTCROP	71								
> N 1-	1381.	19178.	1025.	0	0	0	0.	1	
> 206	0	0	0	0	0	0			
> 253 61	1.0000	0.0	0.0	0	0	0			
> OUTCROP	72								
> C 1-	1353.	19128.	1040.	0	0	0	0.	1	
> 207	0	0	0	0	0	0			
> 269 47	1.0000	0.0	0.0	0	0	0			
> OUTCROP	73								
> N 1-	1386.	19109.	1044.	0	0	0	0.	1	
> 208	0	0	0	0	0	0			
> 265 32	1.0000	0.0	0.0	0	0	0			
> OUTCROP	74								
> N 1-	1404.	19018.	1041.	0	0	0	0.	1	
> 209	0	0	0	0	0	0			
> 264 61	1.0000	0.0	0.0	0	0	0			
> OUTCROP	75								
> C 1-	1356.	18975.	1035.	0	0	0	0.	1	
> 210	0	0	0	0	0	0			
> 256 58	1.0000	0.0	0.0	0	0	0			
> OUTCROP	76								
> C 1-	1380.	18912.	1028.	0	0	0	0.	1	
> 211	0	0	0	0	0	0			
> 257 66	1.0000	0.0	0.0	0	0	0			
> OUTCROP	77								
> N 1-	1365.	18793.	1110.	0	0	0	0.	1	
> 212	0	0	0	0	0	0			
> 272 59	1.0000	0.0	0.0	0	0	0			
> OUTCROP	78								
> E 1-	1207.	18893.	996.	0	0	0	0.	1	
> 213	0	0	0	0	0	0			
> 263 66	1.0000	0.0	0.0	0	0	0			
> OUTCROP	79								
> E 1-	1238.	18803.	998.	0	0	0	0.	1	
> 214	0	0	0	0	0	0			
> 272 45	1.0000	0.0	0.0	0	0	0			
> OUTCROP	80								
> N 1-	1382.	18634.	1018.	0	0	0	0.	1	
> 215	0	0	0	0	0	0			
> 272 79	1.0000	0.0	0.0	0	0	0			

> OUTCROP	81								
> N 1.	1416.	18504.	1033.	0	0	0	0.	1	
> 216	0	0	0	0	0	0			
> 264 39	1.0000	0.0	0.0	0	0	0			
> OUTCROP	82								
> N 1.	1461.	18403.	1060.	0	0	0	0.	1	
> 217	0	0	0	0	0	0			
> 282 19	1.0000	0.0	0.0	0	0	0			
> OUTCROP	83								
> N 1.	1546.	18270.	1073.	0	0	0	0.	1	
> 218	0	0	0	0	0	0			
> 254 12	1.0000	0.0	0.0	0	0	0			
> OUTCROP	84								
> C 1.	1549.	18072.	1114.	0	0	0	0.	1	
> 219	0	0	0	0	0	0			
> 281 13	1.0000	0.0	0.0	0	0	0			
> OUTCROP	85								
> E 1.	1646.	17894.	1160.	0	0	0	0.	1	
> 220	0	0	0	0	0	0			
> 171 10	1.0000	0.0	0.0	0	0	0			
> OUTCROP	86								
> E 1.	1560.	18063.	1138.	0	0	0	0.	1	
> 221	0	0	0	0	0	0			
> 237 13	1.0000	0.0	0.0	0	0	0			
> OUTCROP	87								
> E 1.	1417.	18179.	1018.	0	0	0	0.	1	
> 222	0	0	0	0	0	0			
> 201 8	1.0000	0.0	0.0	0	0	0			
> OUTCROP	88								
> E 1.	1265.	18323.	1078.	0	0	0	0.	1	
> 223	0	0	0	0	0	0			
> 260 50	1.0000	0.0	0.0	0	0	0			
> OUTCROP	89								
> E 1.	1207.	18457.	1041.	0	0	0	0.	1	
> 224	0	0	0	0	0	0			
> 249 63	1.0000	0.0	0.0	0	0	0			
> OUTCROP	90								
> E 1.	1171.	18565.	1030.	0	0	0	0.	1	
> 225	0	0	0	0	0	0			
> 248 54	1.0000	0.0	0.0	0	0	0			
> OUTCROP	91								
> E 1.	1179.	18638.	1018.	0	0	0	0.	1	
> 226	0	0	0	0	0	0			
> 296 44	1.0000	0.0	0.0	0	0	0			
> OUTCROP	92								
> E 1.	1147.	18431.	1032.	0	0	0	0.	1	
> 227	0	0	0	0	0	0			
> 75 44	1.0000	0.0	0.0	0	0	0			
> OUTCROP	93								
> E 1.	1123.	18413.	1035.	0	0	0	0.	1	
> 228	0	0	0	0	0	0			
> 127 15	1.0000	0.0	0.0	0	0	0			
> OUTCROP	94								
> E 1.	1074.	18392.	1029.	0	0	0	0.	1	
> 229	0	0	0	0	0	0			
> 86 24	1.0000	0.0	0.0	0	0	0			
> OUTCROP	95								
> E 1.	1205.	18269.	1048.	0	0	0	0.	1	
> 230	0	0	0	0	0	0			
> 272 45	1.0000	0.0	0.0	0	0	0			
> OUTCROP	96								
> E 1.	1246.	18202.	1063.	0	0	0	0.	1	
> 231	0	0	0	0	0	0			
> 278 45	1.0000	0.0	0.0	0	0	0			

>	OUTCROP	97								
>	E 1.	1225.	18136.	1070.	0	0	0	0.	1	
>	232	0	0	0	0	0	0			
>	250 42	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	98								
>	E 1.	1276.	18029.	1100.	0	0	0	0.	1	
>	233	0	0	0	0	0	0			
>	254 24	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	99								
>	E 1.	1205.	18029.	1080.	0	0	0	0.	1	
>	234	0	0	0	0	0	0			
>	270 52	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	100								
>	E 1.	1093.	18197.	1095.	0	0	0	0.	1	
>	235	0	0	0	0	0	0			
>	297 16	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	101								
>	E 1.	1048.	18274.	1055.	0	0	0	0.	1	
>	236	0	0	0	0	0	0			
>	104 24	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	102								
>	E 1.	992.	18179.	1065.	0	0	0	0.	1	
>	237	0	0	0	0	0	0			
>	86 15	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	103								
>	C 1.	926.	18216.	1060.	0	0	0	0.	1	
>	238	0	0	0	0	0	0			
>	127 23	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	104								
>	C 1.	781.	18171.	1095.	0	0	0	0.	1	
>	239	0	0	0	0	0	0			
>	110 35	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	105								
>	N 1.	736.	18108.	1074.	0	0	0	0.	1	
>	240	0	0	0	0	0	0			
>	102 36	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	106								
>	N 1.	682.	18166.	1095.	0	0	0	0.	1	
>	241	0	0	0	0	0	0			
>	89 62	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	107								
>	N 1.	671.	18254.	1130.	0	0	0	0.	1	
>	242	0	0	0	0	0	0			
>	77 62	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	108								
>	N 1.	632.	18184.	1090.	0	0	0	0.	1	
>	243	0	0	0	0	0	0			
>	74 40	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	109								
>	N 1.	593.	18574.	1105.	0	0	0	0.	1	
>	244	0	0	0	0	0	0			
>	91 57	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	110								
>	C 1.	650.	18815.	1090.	0	0	0	0.	1	
>	245	0	0	0	0	0	0			
>	79 49	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	111								
>	N 1.	666.	18964.	1058.	0	0	0	0.	1	
>	246	0	0	0	0	0	0			
>	66 18	1.0000	0.0	0.0	0	0	0			
>	OUTCROP	112								
>	C 1.	709.	18960.	1058.	0	0	0	0.	1	
>	247	0	0	0	0	0	0			
>	102 20	1.0000	0.0	0.0	0	0	0			

> OUTCROP	113								
> M 1.	3202.	14651.	1538.	0	0	0	0.	1	
> 248	0	0	0	0	0	0			
> 247 34	1.0000	0.0	0.0	0	0	0			
> OUTCROP	114								
> G 1.	3062.	14762.	1553.	0	0	0	0.	1	
> 249	0	0	0	0	0	0			
> 244 34	1.0000	0.0	0.0	0	0	0			
> OUTCROP	115								
> 3 1.	3041.	14729.	1542.	0	0	0	0.	1	
> 250	0	0	0	0	0	0			
> 252 26	1.0000	0.0	0.0	0	0	0			
> OUTCROP	116								
> S 1.	3049.	14832.	1576.	0	0	0	0.	1	
> 251	0	0	0	0	0	0			
> 247 42	1.0000	0.0	0.0	0	0	0			
> OUTCROP	117								
> G 1.	3014.	14852.	1583.	0	0	0	0.	1	
> 252	0	0	0	0	0	0			
> 252 28	1.0000	0.0	0.0	0	0	0			
> OUTCROP	118								
> S 1.	3012.	14831.	1577.	0	0	0	0.	0	
> 253	0	0	0	0	0	0			
> 0 0	0.0	0.0	0.0	0	0	0			
> OUTCROP	119								
> S 1.	2963.	14832.	1590.	0	0	0	0.	0	
> 254	0	0	0	0	0	0			
> 0 0	0.0	0.0	0.0	0	0	0			
> OUTCROP	120								
> G 1.	2970.	14850.	1594.	0	0	0	0.	1	
> 255	0	0	0	0	0	0			
> 268 22	1.0000	0.0	0.0	0	0	0			
> OUTCROP	121								
> 4 1.	2951.	14866.	1600.	0	0	0	0.	1	
> 256	0	0	0	0	0	0			
> 267 90	1.0000	0.0	0.0	0	0	0			
> OUTCROP	122								
> S 1.	2924.	14870.	1588.	0	0	0	0.	0	
> 257	0	0	0	0	0	0			
> 0 0	0.0	0.0	0.0	0	0	0			
> OUTCROP	123								
> 4 1.	2966.	14707.	1539.	0	0	0	0.	1	
> 258	0	0	0	0	0	0			
> 257 29	1.0000	0.0	0.0	0	0	0			
> OUTCROP	124								
> 4 1.	2895.	14854.	1595.	0	0	0	0.	1	
> 259	0	0	0	0	0	0			
> 263 44	1.0000	0.0	0.0	0	0	0			
> OUTCROP	125								
> S 1.	2855.	14818.	1596.	0	0	0	0.	0	
> 260	0	0	0	0	0	0			
> 0 0	0.0	0.0	0.0	0	0	0			
> OUTCROP	126								
> G 1.	2844.	14815.	1595.	0	0	0	0.	1	
> 261	0	0	0	0	0	0			
> 256 54	1.0000	0.0	0.0	0	0	0			
> OUTCROP	127								
> S 1.	2866.	14663.	1553.	0	0	0	0.	0	
> 262	0	0	0	0	0	0			
> 0 0	0.0	0.0	0.0	0	0	0			
> OUTCROP	129								
> S 1.	2777.	14743.	1604.	0	0	0	0.	0	
> 263	0	0	0	0	0	0			
> 0 0	0.0	0.0	0.0	0	0	0			

> OUTCROP	130								
> S 1-	2793.	14756.	1600.	0	0	0	0.	0	
> 264	0	0	0	0	0	0			
> 0 0	0.0	0.0	0.0	0	0	0			
> OUTCROP	131								
> S 1-	2804.	14766.	1600.	0	0	0	0.	0	
> 265	0	0	0	0	0	0			
> 0 0	0.0	0.0	0.0	0	0	0			
> OUTCROP	132								
> G 1-	2800.	14833.	1614.	0	0	0	0.	1	
> 266	0	0	0	0	0	0			
> 268 40	1.0000	0.0	0.0	0	0	0			
> OUTCROP	133								
> H 1-	2673.	14939.	1675.	0	0	0	0.	1	
> 267	0	0	0	0	0	0			
> 239 53	1.0000	0.0	0.0	0	0	0			
> OUTCROP	134								
> G 1-	2762.	14740.	1608.	0	0	0	0.	1	
> 268	0	0	0	0	0	0			
> 268 55	1.0000	0.0	0.0	0	0	0			
> OUTCROP	135								
> B 1-	2659.	14866.	1670.	0	0	0	0.	1	
> 269	0	0	0	0	0	0			
> 227 48	1.0000	0.0	0.0	0	0	0			
> OUTCROP	136								
> H 1-	2675.	14608.	1603.	0	0	0	0.	1	
> 270	0	0	0	0	0	0			
> 272 33	1.0000	0.0	0.0	0	0	0			
> OUTCROP	137								
> B 1-	2543.	14626.	1617.	0	0	0	0.	1	
> 271	0	0	0	0	0	0			
> 251 37	1.0000	0.0	0.0	0	0	0			
> OUTCROP	138								
> B 1-	2616.	14689.	1633.	0	0	0	0.	1	
> 272	0	0	0	0	0	0			
> 247 40	1.0000	0.0	0.0	0	0	0			
> OUTCROP	139								
> B 1-	2594.	14793.	1662.	0	0	0	0.	1	
> 273	0	0	0	0	0	0			
> 242 33	1.0000	0.0	0.0	0	0	0			
> OUTCROP	140								
> B 1-	2441.	14927.	1655.	0	0	0	0.	1	
> 274	0	0	0	0	0	0			
> 263 43	1.0000	0.0	0.0	0	0	0			
> OUTCROP	141								
> B 1-	2585.	14895.	1683.	0	0	0	0.	1	
> 275	0	0	0	0	0	0			
> 261 44	1.0000	0.0	0.0	0	0	0			
> OUTCROP	142								
> B 1-	2553.	15017.	1685.	0	0	0	0.	1	
> 276	0	0	0	0	0	0			
> 245 35	1.0000	0.0	0.0	0	0	0			
> OUTCROP	143								
> H 1-	2560.	15156.	1654.	0	0	0	0.	1	
> 277	0	0	0	0	0	0			
> 240 47	1.0000	0.0	0.0	0	0	0			
> OUTCROP	144								
> B 1-	2522.	15256.	1631.	0	0	0	0.	1	
> 278	0	0	0	0	0	0			
> 227 43	1.0000	0.0	0.0	0	0	0			
> OUTCROP	145								
> E 1-	4293.	20918.	1042.	0	0	0	0.	1	
> 279	0	0	0	0	0	0			
> 211 30	1.0000	0.0	0.0	0	0	0			







> E 1-	5781.	19213.	998.	0	0	0	0.	1
>> 311	0	0	0	0	0	0		
>> 256 34	1.0000	0.0	0.0	0	0	0		
> OUTCROP	179							
> E 1-	5727.	19403.	1015.	0	0	0	0.	1
>> 312	0	0	0	0	0	0		
>> 238 45	1.0000	0.0	0.0	0	0	0		
> OUTCROP	180							
> E 1-	5664.	19530.	1029.	0	0	0	0.	1
>> 313	0	0	0	0	0	0		
>> 246 52	1.0000	0.0	0.0	0	0	0		
> OUTCROP	181							
> E 1-	5626.	19650.	1035.	0	0	0	0.	1
>> 314	0	0	0	0	0	0		
>> 233 46	1.0000	0.0	0.0	0	0	0		
> OUTCROP	182							
> E 1-	5572.	19742.	1045.	0	0	0	0.	1
>> 315	0	0	0	0	0	0		
>> 243 50	1.0000	0.0	0.0	0	0	0		
> OUTCROP	183							
> C 1-	3794.	20267.	992.	0	0	0	0.	1
>> 316	0	0	0	0	0	0		
>> 276 75	1.0000	0.0	0.0	0	0	0		
> OUTCROP	184							
> E 1-	3931.	20120.	995.	0	0	0	0.	1
>> 317	0	0	0	0	0	0		
>> 92 83	1.0000	0.0	0.0	0	0	0		
> OUTCROP	185							
> C 1-	3825.	20058.	990.	0	0	0	0.	1
>> 318	0	0	0	0	0	0		
>> 84 82	1.0000	0.0	0.0	0	0	0		
> OUTCROP	186							
> C 1-	3899.	19975.	990.	0	0	0	0.	1
>> 319	0	0	0	0	0	0		
>> 91 77	1.0000	0.0	0.0	0	0	0		
> OUTCROP	187							
> C 1-	3916.	19846.	975.	0	0	0	0.	1
>> 320	0	0	0	0	0	0		
>> 92 84	1.0000	0.0	0.0	0	0	0		
> OUTCROP	188							
> C 1-	3927.	19678.	1942.	0	0	0	0.	1
>> 321	0	0	0	0	0	0		
>> 92 73	1.0000	0.0	0.0	0	0	0		
> OUTCROP	189							
> C 1-	4046.	17850.	1075.	0	0	0	0.	1
>> 31	0	0	0	0	0	0		
>> 145 22	1.0000	0.0	0.0	0	0	0		
> OUTCROP	190							
> C 1-	3914.	17770.	1060.	0	0	0	0.	1
>> 322	0	0	0	0	0	0		
>> 111 15	1.0000	0.0	0.0	0	0	0		
> OUTCROP	191							
> C 1-	3845.	17723.	1089.	0	0	0	0.	1
>> 323	0	0	0	0	0	0		
>> 220 18	1.0000	0.0	0.0	0	0	0		
> OUTCROP	192							
> C 1-	3516.	17799.	1113.	0	0	0	0.	1
>> 324	0	0	0	0	0	0		
>> 157 22	1.0000	0.0	0.0	0	0	0		
> OUTCROP	193							
> N 1-	3486.	17741.	1125.	0	0	0	0.	1
>> 325	0	0	0	0	0	0		
>> 116 11	1.0000	0.0	0.0	0	0	0		
> OUTCROP	194							

> C	1.	3294.	17659.	1138.	0	0	0.	1
>>	33	0	0	0	0	0	0	
>>	166 13	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	195						
>>	N 1.	3275.	17727.	1093.	0	0	0.	1
>>	36	0	0	0	0	0	0	
>>	123 17	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	196						
>>	C 1.	3265.	17564.	1152.	0	0	0.	1
>>	38	0	0	0	0	0	0	
>>	60 44	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	197						
>>	C 1.	3254.	17487.	1173.	0	0	0.	1
>>	326	0	0	0	0	0	0	
>>	86 16	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	198						
>>	C 1.	3198.	17450.	1186.	0	0	0.	1
>>	40	0	0	0	0	0	0	
>>	185 14	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	199						
>>	C 1.	3140.	17393.	1227.	0	0	0.	1
>>	44	0	0	0	0	0	0	
>>	215 38	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	200						
>>	C 1.	3014.	17349.	1262.	0	0	0.	1
>>	327	0	0	0	0	0	0	
>>	39 17	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	201						
>>	C 1.	2889.	17363.	1277.	0	0	0.	1
>>	46	0	0	0	0	0	0	
>>	165 20	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	202						
>>	C 1.	2773.	17289.	1285.	0	0	0.	1
>>	49	0	0	0	0	0	0	
>>	131 10	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	203						
>>	C 1.	2615.	17385.	1298.	0	0	0.	1
>>	328	0	0	0	0	0	0	
>>	323 11	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	204						
>>	C 1.	2529.	17376.	1296.	0	0	0.	1
>>	329	0	0	0	0	0	0	
>>	333 17	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	205						
>>	C 1.	2567.	17293.	1296.	0	0	0.	1
>>	330	0	0	0	0	0	0	
>>	78 11	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	206						
>>	C 1.	2402.	17470.	1277.	0	0	0.	1
>>	331	0	0	0	0	0	0	
>>	224 33	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	207						
>>	C 1.	2410.	17606.	1268.	0	0	0.	1
>>	332	0	0	0	0	0	0	
>>	223 40	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	208						
>>	C 1.	2341.	17629.	1262.	0	0	0.	1
>>	333	0	0	0	0	0	0	
>>	199 4	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	209						
>>	C 1.	2224.	17655.	1242.	0	0	0.	1
>>	334	0	0	0	0	0	0	
>>	216 35	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	210						

> N	1.	2252.	17726.	1210.	0	0	0.	1
>>	335	0	0	0	0	0	0	
>>	222 27	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	211						
>>	C	1.	2110.	17674.	1211.	0	0	0.
>>	336	0	0	0	0	0	0	1
>>	245 42	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	212						
>>	C	1.	2015.	17750.	1180.	0	0	0.
>>	337	0	0	0	0	0	0	1
>>	245 45	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	213						
>>	N	1.	2059.	17825.	1150.	0	0	0.
>>	338	0	0	0	0	0	0	1
>>	303 50	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	214						
>>	C	1.	1902.	17824.	1130.	0	0	0.
>>	339	0	0	0	0	0	0	1
>>	129 5	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	215						
>>	C	1.	1749.	17975.	1100.	0	0	0.
>>	340	0	0	0	0	0	0	1
>>	187 16	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	216						
>>	E	1.	1703.	17811.	1158.	0	0	0.
>>	341	0	0	0	0	0	0	1
>>	156 18	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	217						
>>	E	1.	1856.	17677.	1154.	0	0	0.
>>	342	0	0	0	0	0	0	1
>>	219 20	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	218						
>>	E	1.	1917.	17571.	1160.	0	0	0.
>>	343	0	0	0	0	0	0	1
>>	238 17	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	219						
>>	E	1.	2164.	17449.	1250.	0	0	0.
>>	344	0	0	0	0	0	0	1
>>	216 32	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	220						
>>	E	1.	2322.	17196.	1290.	0	0	0.
>>	345	0	0	0	0	0	0	1
>>	248 43	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	221						
>>	C	1.	2514.	17223.	1282.	0	0	0.
>>	346	0	0	0	0	0	0	1
>>	62 13	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	222						
>>	E	1.	2476.	17163.	1272.	0	0	0.
>>	347	0	0	0	0	0	0	1
>>	258 60	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	223						
>>	C	1.	2528.	17140.	1286.	0	0	0.
>>	348	0	0	0	0	0	0	1
>>	68 20	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	224						
>>	C	1.	2595.	17106.	1292.	0	0	0.
>>	349	0	0	0	0	0	0	1
>>	271 32	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	225						
>>	C	1.	2658.	16988.	1297.	0	0	0.
>>	350	0	0	0	0	0	0	1
>>	13 17	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	226						

> E 1.	2586.	16894.	1294.	0	0	0.	1
> 351	0	0	0	0	0	0	
> 122 15	1.0000	0.0	0.0	0	0		
> OUTCROP	227						
> E 1.	2696.	16619.	1286.	0	0	0.	1
> 352	0	0	0	0	0	0	
> 258 55	1.0000	0.0	0.0	0	0		
> OUTCROP	228						
> E 1.	2774.	16554.	1300.	0	0	0.	1
> 353	0	0	0	0	0	0	
> 261 40	1.0000	0.0	0.0	0	0		
> OUTCROP	229						
> E 1.	2979.	16550.	1297.	0	0	0.	1
> 354	0	0	0	0	0	0	
> 139 35	1.0000	0.0	0.0	0	0		
> OUTCROP	230						
> E 1.	3965.	16390.	1121.	0	0	0.	1
> 52	0	0	0	0	0	0	
> 101 27	1.0000	0.0	0.0	0	0		
> OUTCROP	231						
> E 1.	3840.	16447.	1145.	0	0	0.	1
> 54	0	0	0	0	0	0	
> 98 22	1.0000	0.0	0.0	0	0		
> OUTCROP	232						
> E 1.	3815.	16357.	1157.	0	0	0.	1
> 56	0	0	0	0	0	0	
> 49 18	1.0000	0.0	0.0	0	0		
> OUTCROP	233						
> E 1.	3579.	16310.	1201.	0	0	0.	1
> 58	0	0	0	0	0	0	
> 77 29	1.0000	0.0	0.0	0	0		
> OUTCROP	234						
> E 1.	3324.	16128.	1271.	0	0	0.	1
> 355	0	0	0	0	0	0	
> 4 6	1.0000	0.0	0.0	0	0		
> OUTCROP	235						
> E 1.	3378.	16087.	1267.	0	0	0.	1
> 60	0	0	0	0	0	0	
> 214 5	1.0000	0.0	0.0	0	0		
> OUTCROP	236						
> E 1.	2868.	16103.	1387.	0	0	0.	1
> 356	0	0	0	0	0	0	
> 245 7	1.0000	0.0	0.0	0	0		
> OUTCROP	237						
> E 1.	2928.	16134.	1367.	0	0	0.	1
> 357	0	0	0	0	0	0	
> 60 28	1.0000	0.0	0.0	0	0		
> OUTCROP	238						
> E 1.	2964.	15902.	1379.	0	0	0.	1
> 358	0	0	0	0	0	0	
> 228 5	1.0000	0.0	0.0	0	0		
> OUTCROP	239						
> E 1.	4510.	16319.	1276.	0	0	0.	1
> 62	0	0	0	0	0	0	
> 112 8	1.0000	0.0	0.0	0	0		
> OUTCROP	240						
> M 1.	3004.	15227.	1488.	0	0	0.	1
> 359	0	0	0	0	0	0	
> 228 35	1.0000	0.0	0.0	0	0		
> OUTCROP	241						
> G 1.	2931.	15237.	1502.	0	0	0.	1
> 360	0	0	0	0	0	0	
> 261 11	1.0000	0.0	0.0	0	0		
> OUTCROP	242						

> G 1.	2907.	15210.	1515.	0	0	0.	1
> 64	0	0	0	0	0	0	
> 260 30	1.0000	0.0	0.0	0	0	0	
> OUTCROP	244						
> 3 1.	3018.	14944.	1612.	0	0	0.	1
> 361	0	0	0	0	0	0	
> 208 17	1.0000	0.0	0.0	0	0	0	
> OUTCROP	245						
> 4 1.	2982.	14949.	1615.	0	0	0.	1
> 362	0	0	0	0	0	0	
> 211 16	1.0000	0.0	0.0	0	0	0	
> OUTCROP	246						
> 6 1.	2917.	15008.	1620.	0	0	0.	1
> 363	0	0	0	0	0	0	
> 208 12	1.0000	0.0	0.0	0	0	0	
> OUTCROP	247						
> 4 1.	2866.	15169.	1542.	0	0	0.	1
> 364	0	0	0	0	0	0	
> 272 41	1.0000	0.0	0.0	0	0	0	
> OUTCROP	248						
> S 1.	2840.	15229.	1525.	0	0	0.	0
> 365	0	0	0	0	0	0	
> 0 0	0.0	0.0	0.0	0	0	0	
> OUTCROP	249						
> G 1.	2827.	15286.	1518.	0	0	0.	1
> 366	0	0	0	0	0	0	
> 255 36	1.0000	0.0	0.0	0	0	0	
> OUTCROP	250						
> 3 1.	2843.	15295.	1513.	0	0	0.	1
> 367	0	0	0	0	0	0	
> 266 43	1.0000	0.0	0.0	0	0	0	
> OUTCROP	251						
> S 1.	2801.	15239.	1534.	0	0	0.	0
> 368	0	0	0	0	0	0	
> 0 0	0.0	0.0	0.0	0	0	0	
> OUTCROP	253						
> S 1.	2732.	15246.	1546.	0	0	0.	0
> 369	0	0	0	0	0	0	
> 0 0	0.0	0.0	0.0	0	0	0	
> OUTCROP	254						
> G 1.	2075.	14539.	1569.	0	0	0.	1
> 370	0	0	0	0	0	0	
> 266 42	1.0000	0.0	0.0	0	0	0	
> OUTCROP	255						
> S 1.	2701.	15266.	1556.	0	0	0.	0
> 371	0	0	0	0	0	0	
> 0 0	0.0	0.0	0.0	0	0	0	
> OUTCROP	256						
> G 1.	2718.	15293.	1544.	0	0	0.	1
> 372	0	0	0	0	0	0	
> 264 51	1.0000	0.0	0.0	0	0	0	
> OUTCROP	257						
> G 1.	2664.	15329.	1555.	0	0	0.	1
> 373	0	0	0	0	0	0	
> 259 22	1.0000	0.0	0.0	0	0	0	
> OUTCROP	258						
> S 1.	2624.	15323.	1568.	0	0	0.	0
> 374	0	0	0	0	0	0	
> 0 0	0.0	0.0	0.0	0	0	0	
> OUTCROP	259						
> G 1.	2603.	15368.	1562.	0	0	0.	1
> 375	0	0	0	0	0	0	
> 262 58	1.0000	0.0	0.0	0	0	0	
> OUTCROP	260						

> H 1-	2538.	15363.	1588.	0	0	0	0.	1
>> 376	0	0	0	0	0	0		
>> 262 40	1.0000	0.0	0.0	0	0	0		
> OUTCROP	261							
> H 1-	2472.	15416.	1577.	0	0	0	0.	1
>> 377	0	0	0	0	0	0		
>> 241 43	1.0000	0.0	0.0	0	0	0		
> OUTCROP	262							
> S 1-	2783.	15517.	1495.	0	0	0	0.	0
>> 378	0	0	0	0	0	0		
>> 0 0	0.0	0.0	0.0	0	0	0		
> OUTCROP	263							
> G 1-	2743.	15559.	1506.	0	0	0	0.	1
>> 379	0	0	0	0	0	0		
>> 253 36	1.0000	0.0	0.0	0	0	0		
> OUTCROP	264							
> G 1-	2678.	15643.	1514.	0	0	0	0.	1
>> 380	0	0	0	0	0	0		
>> 256 40	1.0000	0.0	0.0	0	0	0		
> OUTCROP	265							
> G 1-	2582.	15479.	1568.	0	0	0	0.	1
>> 381	0	0	0	0	0	0		
>> 247 49	1.0000	0.0	0.0	0	0	0		
> OUTCROP	266							
> S 1-	2563.	15517.	1566.	0	0	0	0.	0
>> 382	0	0	0	0	0	0		
>> 0 0	0.0	0.0	0.0	0	0	0		
> OUTCROP	267							
> S 1-	2568.	15573.	1555.	0	0	0	0.	0
>> 383	0	0	0	0	0	0		
>> 0 0	0.0	0.0	0.0	0	0	0		
> OUTCROP	268							
> G 1-	2549.	15575.	1551.	0	0	0	0.	1
>> 384	0	0	0	0	0	0		
>> 255 39	1.0000	0.0	0.0	0	0	0		
> OUTCROP	269							
> S 1-	2588.	15662.	1538.	0	0	0	0.	0
>> 385	0	0	0	0	0	0		
>> 0 0	0.0	0.0	0.0	0	0	0		
> OUTCROP	270							
> G 1-	2494.	15638.	1518.	0	0	0	0.	1
>> 386	0	0	0	0	0	0		
>> 271 51	1.0000	0.0	0.0	0	0	0		
> OUTCROP	271							
> G 1-	2537.	15671.	1527.	0	0	0	0.	1
>> 387	0	0	0	0	0	0		
>> 248 44	1.0000	0.0	0.0	0	0	0		
> OUTCROP	272							
> G 1-	2572.	15708.	1531.	0	0	0	0.	1
>> 388	0	0	0	0	0	0		
>> 258 40	1.0000	0.0	0.0	0	0	0		
> OUTCROP	273							
> S 1-	2619.	15732.	1515.	0	0	0	0.	0
>> 389	0	0	0	0	0	0		
>> 0 0	0.0	0.0	0.0	0	0	0		
> OUTCROP	274							
> 4 1-	2602.	15805.	1505.	0	0	0	0.	0
>> 390	0	0	0	0	0	0		
>> 0 0	0.0	0.0	0.0	0	0	0		
> OUTCROP	275							
> F 1-	2581.	15821.	1503.	0	0	0	0.	1
>> 391	0	0	0	0	0	0		
>> 242 40	1.0000	0.0	0.0	0	0	0		
> OUTCROP	276							

> G 1.	2541.	15808.	1506.	0	0	0.	1
> 392	0	0	0	0	0	0	
> 252 40	1.0000	0.0	0.0	0	0		
> OUTCROP	277						
> G 1.	2486.	15742.	1497.	0	0	0.	1
> 393	0	0	0	0	0		
> 233 46	1.0000	0.0	0.0	0	0		
> OUTCROP	278						
> H 1.	2306.	15572.	1536.	0	0	0.	1
> 394	0	0	0	0	0		
> 68 18	1.0000	0.0	0.0	0	0		
> OUTCROP	279						
> G 1.	2295.	15632.	1525.	0	0	0.	1
> 395	0	0	0	0	0		
> 37 20	1.0000	0.0	0.0	0	0		
> OUTCROP	280						
> G 1.	2185.	15594.	1542.	0	0	0.	1
> 396	0	0	0	0	0		
> 34 21	1.0000	0.0	0.0	0	0		
> OUTCROP	281						
> G 1.	2398.	15767.	1470.	0	0	0.	1
> 397	0	0	0	0	0		
> 239 22	1.0000	0.0	0.0	0	0		
> OUTCROP	282						
> G 1.	2388.	15819.	1460.	0	0	0.	1
> 398	0	0	0	0	0		
> 233 40	1.0000	0.0	0.0	0	0		
> OUTCROP	283						
> G 1.	2404.	15876.	1447.	0	0	0.	1
> 399	0	0	0	0	0		
> 247 44	1.0000	0.0	0.0	0	0		
> OUTCROP	284						
> G 1.	2586.	15879.	1481.	0	0	0.	1
> 400	0	0	0	0	0		
> 280 58	1.0000	0.0	0.0	0	0		
> OUTCROP	285						
> G 1.	2589.	15923.	1473.	0	0	0.	1
> 401	0	0	0	0	0		
> 264 53	1.0000	0.0	0.0	0	0		
> OUTCROP	286						
> G 1.	2624.	15949.	1464.	0	0	0.	1
> 402	0	0	0	0	0		
> 255 55	1.0000	0.0	0.0	0	0		
> OUTCROP	287						
> S 1.	2578.	15983.	1461.	0	0	0.	0
> 403	0	0	0	0	0		
> 0 0	0.0	0.0	0.0	0	0		
> OUTCROP	288						
> S 1.	2609.	15983.	1458.	0	0	0.	0
> 404	0	0	0	0	0		
> 0 0	0.0	0.0	0.0	0	0		
> OUTCROP	289						
> G 1.	2647.	16044.	1449.	0	0	0.	1
> 405	0	0	0	0	0		
> 263 40	1.0000	0.0	0.0	0	0		
> OUTCROP	290						
> C 1.	2704.	16015.	1451.	0	0	0.	1
> 406	0	0	0	0	0		
> 288 46	1.0000	0.0	0.0	0	0		
> OUTCROP	291						
> C 1.	2639.	16086.	1442.	0	0	0.	1
> 407	0	0	0	0	0		
> 256 44	1.0000	0.0	0.0	0	0		
> OUTCROP	292						



> M 1.	2645.	16195.	1422.	0	0	0.	1
> 408	0	0	0	0	0	0	
> 267 43	1.0000	0.0	0.0	0	0	0	
> OUTCROP	293						
> M 1.	2585.	16307.	1394.	0	0	0.	1
> 409	0	0	0	0	0	0	
> 249 36	1.0000	0.0	0.0	0	0	0	
> OUTCROP	294						
> C 1.	2542.	16304.	1390.	0	0	0.	1
> 410	0	0	0	0	0	0	
> 267 33	1.0000	0.0	0.0	0	0	0	
> OUTCROP	295						
> 4 1.	2352.	16267.	1372.	0	0	0.	1
> 411	0	0	0	0	0	0	
> 237 34	1.0000	0.0	0.0	0	0	0	
> OUTCROP	296						
> G 1.	2357.	16166.	1385.	0	0	0.	1
> 412	0	0	0	0	0	0	
> 256 24	1.0000	0.0	0.0	0	0	0	
> OUTCROP	297						
> S 1.	2351.	16118.	1397.	0	0	0.	0
> 413	0	0	0	0	0	0	
> 0 0	0.0	0.0	0.0	0	0	0	
> OUTCROP	298						
> G 1.	2373.	16067.	1402.	0	0	0.	1
> 414	0	0	0	0	0	0	
> 256 51	1.0000	0.0	0.0	0	0	0	
> OUTCROP	299						
> G 1.	2094.	15752.	1519.	0	0	0.	1
> 415	0	0	0	0	0	0	
> 70 27	1.0000	0.0	0.0	0	0	0	
> OUTCROP	300						
> G 1.	2038.	15704.	1539.	0	0	0.	1
> 416	0	0	0	0	0	0	
> 65 36	1.0000	0.0	0.0	0	0	0	
> OUTCROP	301						
> 4 1.	1864.	15819.	1465.	0	0	0.	1
> 417	0	0	0	0	0	0	
> 87 32	1.0000	0.0	0.0	0	0	0	
> OUTCROP	302						
> G 1.	2039.	15886.	1501.	0	0	0.	1
> 418	0	0	0	0	0	0	
> 62 26	1.0000	0.0	0.0	0	0	0	
> OUTCROP	303						
> S 1.	2071.	15878.	1500.	0	0	0.	0
> 419	0	0	0	0	0	0	
> 0 0	0.0	0.0	0.0	0	0	0	
> OUTCROP	304						
> S 1.	2082.	15932.	1489.	0	0	0.	0
> 420	0	0	0	0	0	0	
> 0 0	0.0	0.0	0.0	0	0	0	
> OUTCROP	305						
> G 1.	2042.	15976.	1478.	0	0	0.	1
> 421	0	0	0	0	0	0	
> 76 16	1.0000	0.0	0.0	0	0	0	
> OUTCROP	306						
> G 1.	2050.	16035.	1456.	0	0	0.	1
> 422	0	0	0	0	0	0	
> 93 24	1.0000	0.0	0.0	0	0	0	
> OUTCROP	307						
> G 1.	2020.	15989.	1470.	0	0	0.	0
> 423	0	0	0	0	0	0	
> 0 0	0.0	0.0	0.0	0	0	0	
> OUTCROP	308						

> G	1.	1961.	15946.	1468.	0	0	0.	1
>>	424	0	0	0	0	0		
>>	80 28	1.0000	0.0	0.0	0	0.		
>>								
> OUTCROP	309							
> S	1.	1980.	15975.	1468.	0	0	0.	0
>>	425	0	0	0	0	0		
>>	0 0	0.0	0.0	0.0	0	0		
>>								
> OUTCROP	310							
> G	1.	1843.	15968.	1430.	0	0	0.	1
>>	426	0	0	0	0	0		
>>	90 32	1.0000	0.0	0.0	0	0		
>>								
> OUTCROP	311							
> S	1.	1824.	15966.	1420.	0	0	0.	0
>>	427	0	0	0	0	0		
>>	0 0	0.0	0.0	0.0	0	0		
>>								
> OUTCROP	312							
> G	1.	1781.	16027.	1404.	0	0	0.	1
>>	428	0	0	0	0	0		
>>	88 33	1.0000	0.0	0.0	0	0		
>>								
> OUTCROP	313							
> G	1.	1708.	16101.	1395.	0	0	0.	1
>>	429	0	0	0	0	0		
>>	89 33	1.0000	0.0	0.0	0	0		
>>								
> OUTCROP	314							
> G	1.	1705.	16212.	1352.	0	0	0.	1
>>	430	0	0	0	0	0		
>>	76 36	1.0000	0.0	0.0	0	0		
>>								
> OUTCROP	315							
> M	1.	1545.	16518.	1278.	0	0	0.	1
>>	431	0	0	0	0	0		
>>	106 24	1.0000	0.0	0.0	0	0		
>>								
> OUTCROP	316							
> M	1.	1453.	16596.	1257.	0	0	0.	1
>>	432	0	0	0	0	0		
>>	73 25	1.0000	0.0	0.0	0	0		
>>								
> OUTCROP	317							
> E	1.	1377.	16662.	1243.	0	0	0.	1
>>	433	0	0	0	0	0		
>>	74 50	1.0000	0.0	0.0	0	0		
>>								
> OUTCROP	318							
> M	1.	1440.	16678.	1268.	0	0	0.	1
>>	434	0	0	0	0	0		
>>	93 40	1.0000	0.0	0.0	0	0		
>>								
> OUTCROP	319							
> M	1.	1377.	16774.	1233.	0	0	0.	1
>>	435	0	0	0	0	0		
>>	67 33	1.0000	0.0	0.0	0	0		
>>								
> OUTCROP	320							
> M	1.	1363.	16944.	1213.	0	0	0.	1
>>	436	0	0	0	0	0		
>>	69 36	1.0000	0.0	0.0	0	0		
>>								
> OUTCROP	321							
> E	1.	1318.	16976.	1206.	0	0	0.	1
>>	437	0	0	0	0	0		
>>	68 36	1.0000	0.0	0.0	0	0		
>>								
> OUTCROP	322							
> E	1.	1243.	17333.	1165.	0	0	0.	1
>>	438	0	0	0	0	0		
>>	94 20	1.0000	0.0	0.0	0	0		
>>								
> OUTCROP	323							
> G	1.	1501.	17387.	1254.	0	0	0.	1
>>	439	0	0	0	0	0		
>>	79 10	1.0000	0.0	0.0	0	0		
>>								
> OUTCROP	324							

> G 1.	1726.	17372.	1256.	0	0	0.	1
>> 440	0	0	0	0	0	0	
>> 205 10	1.0000	0.0	0.0	0	0		
> OUTCROP	325						
> G 1.	1859.	17316.	1254.	0	0	0.	1
>> 441	0	0	0	0	0	0	
>> 194 15	1.0000	0.0	0.0	0	0		
> OUTCROP	326						
> G 1.	2001.	17197.	1230.	0	0	0.	1
>> 442	0	0	0	0	0	0	
>> 120 10	1.0000	0.0	0.0	0	0		
> OUTCROP	327						
> M 1.	2076.	17248.	1240.	0	0	0.	1
>> 443	0	0	0	0	0	0	
>> 237 27	1.0000	0.0	0.0	0	0		
> OUTCROP	328						
> G 1.	2050.	17093.	1254.	0	0	0.	1
>> 444	0	0	0	0	0	0	
>> 129 20	1.0000	0.0	0.0	0	0		
> OUTCROP	329						
> C 1.	2104.	17087.	1245.	0	0	0.	1
>> 445	0	0	0	0	0	0	
>> 226 28	1.0000	0.0	0.0	0	0		
> OUTCROP	330						
> G 1.	2087.	17017.	1255.	0	0	0.	1
>> 446	0	0	0	0	0	0	
>> 257 27	1.0000	0.0	0.0	0	0		
> OUTCROP	331						
> M 1.	2317.	16895.	1310.	0	0	0.	1
>> 447	0	0	0	0	0	0	
>> 271 38	1.0000	0.0	0.0	0	0		
> OUTCROP	332						
> C 1.	2290.	16836.	1303.	0	0	0.	1
>> 448	0	0	0	0	0	0	
>> 249 35	1.0000	0.0	0.0	0	0		
> OUTCROP	333						
> G 1.	2279.	16735.	1309.	0	0	0.	1
>> 449	0	0	0	0	0	0	
>> 229 32	1.0000	0.0	0.0	0	0		
> OUTCROP	334						
> C 1.	2366.	16710.	1320.	0	0	0.	1
>> 450	0	0	0	0	0	0	
>> 252 30	1.0000	0.0	0.0	0	0		
> OUTCROP	335						
> C 1.	2390.	16637.	1329.	0	0	0.	1
>> 451	0	0	0	0	0	0	
>> 265 28	1.0000	0.0	0.0	0	0		
> OUTCROP	336						
> 4 1.	2135.	16630.	1318.	0	0	0.	1
>> 452	0	0	0	0	0	0	
>> 262 18	1.0000	0.0	0.0	0	0		
> OUTCROP	337						
> 4 1.	2224.	16462.	1340.	0	0	0.	1
>> 453	0	0	0	0	0	0	
>> 237 21	1.0000	0.0	0.0	0	0		
> OUTCROP	338						
> G 1.	4588.	16031.	1070.	0	0	0.	1
>> 454	0	0	0	0	0	0	
>> 111 24	1.0000	0.0	0.0	0	0		
> OUTCROP	339						
> 5 1.	4590.	15901.	1085.	0	0	0.	0
>> 455	0	0	0	0	0	0	
>> 0 0	0.0	0.0	0.0	0	0		
> OUTCROP	340						

> G 1.	4550.	15888.	1090.	0	0	0	0.	1
>> 456	0	0	0	0	0	0		
>>> 114 12	1.0000	0.0	0.0	0	0	0		
> OUTCROP	341							
>> 4 1.	4349.	15912.	1125.	0	0	0	0.	1
>>> 67	0	0	0	0	0	0		
>>>> 114 24	1.0000	0.0	0.0	0	0	0		
> OUTCROP	342							
>> 6 1.	4272.	15916.	1137.	0	0	0	0.	1
>>> 457	0	0	0	0	0	0		
>>>> 110 28	1.0000	0.0	0.0	0	0	0		
> OUTCROP	343							
>> 6 1.	4237.	15613.	1167.	0	0	0	0.	1
>>> 69	0	0	0	0	0	0		
>>>> 82 34	1.0000	0.0	0.0	0	0	0		
> OUTCROP	344							
>> 6 1.	4838.	15590.	1070.	0	0	0	0.	1
>>> 458	0	0	0	0	0	0		
>>>> 112 23	1.0000	0.0	0.0	0	0	0		
> OUTCROP	345							
>> 6 1.	4946.	15424.	1068.	0	0	0	0.	1
>>> 77	0	0	0	0	0	0		
>>>> 83 26	1.0000	0.0	0.0	0	0	0		
> OUTCROP	346							
>> H 1.	4950.	15062.	1117.	0	0	0	0.	1
>>> 459	0	0	0	0	0	0		
>>>> 74 22	1.0000	0.0	0.0	0	0	0		
> OUTCROP	347							
>> 6 1.	4575.	15298.	1130.	0	0	0	0.	1
>>> 460	0	0	0	0	0	0		
>>>> 92 42	1.0000	0.0	0.0	0	0	0		
> OUTCROP	348							
>> 6 1.	4486.	15328.	1150.	0	0	0	0.	1
>>> 461	0	0	0	0	0	0		
>>>> 77 38	1.0000	0.0	0.0	0	0	0		
> OUTCROP	349							
>> 5 1.	4427.	15233.	1165.	0	0	0	0.	1
>>> 462	0	0	0	0	0	0		
>>>> 81 38	1.0000	0.0	0.0	0	0	0		
> OUTCROP	350							
>> 6 1.	4304.	15185.	1188.	0	0	0	0.	1
>>> 71	0	0	0	0	0	0		
>>>> 52 38	1.0000	0.0	0.0	0	0	0		
> OUTCROP	351							
>> M 1.	3889.	15475.	1274.	0	0	0	0.	1
>>> 73	0	0	0	0	0	0		
>>>> 95 26	1.0000	0.0	0.0	0	0	0		
> OUTCROP	352							
>> M 1.	3950.	15197.	1275.	0	0	0	0.	1
>>> 75	0	0	0	0	0	0		
>>>> 107 24	1.0000	0.0	0.0	0	0	0		
> OUTCROP	353							
>> T 1.	4055.	15181.	1245.	0	0	0	0.	1
>>> 463	0	0	0	0	0	0		
>>>> 119 21	1.0000	0.0	0.0	0	0	0		
> OUTCROP	354							
>> 6 1.	4149.	15035.	1265.	0	0	0	0.	1
>>> 464	0	0	0	0	0	0		
>>>> 89 42	1.0000	0.0	0.0	0	0	0		
> OUTCROP	355							
>> 6 1.	4260.	14970.	1263.	0	0	0	0.	1
>>> 465	0	0	0	0	0	0		
>>>> 74 38	1.0000	0.0	0.0	0	0	0		
> OUTCROP	356							

> G 1.	4400.	14817.	1267.	0	0	0.	1
> 466	0	0	0	0	0	0	
> 97 40	1.0000	0.0	0.0	0	0		
> OUTCROP	357						
> G 1.	4431.	14766.	1269.	0	0	0.	1
> 80	0	0	0	0	0	0	
> 82 36	1.0000	0.0	0.0	0	0		
> OUTCROP	358						
> S 1.	4466.	14732.	1260.	0	0	0.	0
> 467	0	0	0	0	0	0	
> 0 0	0.0	0.0	0.0	0	0		
> OUTCROP	359						
> G 1.	4459.	14654.	1270.	0	0	0.	1
> 468	0	0	0	0	0	0	
> 70 25	1.0000	0.0	0.0	0	0		
> OUTCROP	360						
> G 1.	4595.	14504.	1212.	0	0	0.	1
> 82	0	0	0	0	0	0	
> 69 57	1.0000	0.0	0.0	0	0		
> OUTCROP	361						
> G 1.	4565.	14473.	1215.	0	0	0.	1
> 469	0	0	0	0	0	0	
> 60 65	1.0000	0.0	0.0	0	0		
> OUTCROP	362						
> G 1.	4490.	14432.	1238.	0	0	0.	1
> 470	0	0	0	0	0	0	
> 55 58	1.0000	0.0	0.0	0	0		
> OUTCROP	363						
> 4 1.	4409.	14445.	1255.	0	0	0.	1
> 84	0	0	0	0	0	0	
> 67 52	1.0000	0.0	0.0	0	0		
> OUTCROP	364						
> 4 1.	4334.	14460.	1276.	0	0	0.	1
> 471	0	0	0	0	0	0	
> 75 52	1.0000	0.0	0.0	0	0		
> OUTCROP	365						
> G 1.	4341.	14418.	1264.	0	0	0.	1
> 472	0	0	0	0	0	0	
> 76 47	1.0000	0.0	0.0	0	0		
> OUTCROP	366						
> 4 1.	4398.	14377.	1267.	0	0	0.	1
> 473	0	0	0	0	0	0	
> 76 55	1.0000	0.0	0.0	0	0		
> OUTCROP	367						
> G 1.	4219.	14468.	1360.	0	0	0.	1
> 474	0	0	0	0	0	0	
> 8 26	1.0000	0.0	0.0	0	0		
> OUTCROP	368						
> G 1.	4259.	14427.	1325.	0	0	0.	1
> 475	0	0	0	0	0	0	
> 93 24	1.0000	0.0	0.0	0	0		
> OUTCROP	369						
> G 1.	4228.	14349.	1311.	0	0	0.	1
> 87	0	0	0	0	0	0	
> 109 26	1.0000	0.0	0.0	0	0		
> OUTCROP	370						
> G 1.	4206.	14415.	1325.	0	0	0.	1
> 476	0	0	0	0	0	0	
> 183 28	1.0000	0.0	0.0	0	0		
> OUTCROP	371						
> T 1.	4150.	14357.	1346.	0	0	0.	1
> 477	0	0	0	0	0	0	
> 87 26	1.0000	0.0	0.0	0	0		
> OUTCROP	372						

> T 1-	4121.	14418.	1335.	0	0	0	0.	1
>> 91	0	0	0	0	0	0	0	
>> 137 25	1.0000	0.0	0.0					
> OUTCROP	373							
>> M 1-	3839.	14412.	1388.	0	0	0	0.	1
>> 93	0	0	0	0	0	0	0	
>> 45 24	1.0000	0.0	0.0					
> OUTCROP	374							
>> M 1-	3805.	14481.	1394.	0	0	0	0.	1
>> 478	0	0	0	0	0	0	0	
>> 70 16	1.0000	0.0	0.0					
> OUTCROP	375							
>> M 1-	3754.	14415.	1398.	0	0	0	0.	1
>> 95	0	0	0	0	0	0	0	
>> 97 8	1.0000	0.0	0.0					
> OUTCROP	376							
>> G 1-	4448.	13839.	1357.	0	0	0	0.	1
>> 97	0	0	0	0	0	0	0	
>> 86 25	1.0000	0.0	0.0					
> OUTCROP	377							
>> G 1-	4499.	13901.	1336.	0	0	0	0.	1
>> 99	0	0	0	0	0	0	0	
>> 100 26	1.0000	0.0	0.0					
> OUTCROP	378							
>> G 1-	4475.	14005.	1300.	0	0	0	0.	1
>> 101	0	0	0	0	0	0	0	
>> 131 12	1.0000	0.0	0.0					
> OUTCROP	379							
>> G 1-	4592.	13965.	1340.	0	0	0	0.	1
>> 479	0	0	0	0	0	0	0	
>> 52 31	1.0000	0.0	0.0					
> OUTCROP	380							
>> G 1-	4524.	14049.	1290.	0	0	0	0.	1
>> 480	0	0	0	0	0	0	0	
>> 61 32	1.0000	0.0	0.0					
> OUTCROP	381							
>> G 1-	4549.	14078.	1286.	0	0	0	0.	1
>> 481	0	0	0	0	0	0	0	
>> 57 35	1.0000	0.0	0.0					
> OUTCROP	382							
>> G 1-	4671.	14038.	1290.	0	0	0	0.	1
>> 482	0	0	0	0	0	0	0	
>> 87 68	1.0000	0.0	0.0					
> OUTCROP	383							
>> G 1-	4607.	14148.	1265.	0	0	0	0.	1
>> 483	0	0	0	0	0	0	0	
>> 54 54	1.0000	0.0	0.0					
> OUTCROP	384							
>> G 1-	4628.	14206.	1255.	0	0	0	0.	1
>> 484	0	0	0	0	0	0	0	
>> 62 50	1.0000	0.0	0.0					
> OUTCROP	385							
>> G 1-	4656.	14205.	1254.	0	0	0	0.	1
>> 485	0	0	0	0	0	0	0	
>> 54 60	1.0000	0.0	0.0					
> OUTCROP	386							
>> G 1-	4662.	14548.	1190.	0	0	0	0.	1
>> 486	0	0	0	0	0	0	0	
>> 74 43	1.0000	0.0	0.0					
> OUTCROP	387							
>> G 1-	4751.	14512.	1217.	0	0	0	0.	1
>> 487	0	0	0	0	0	0	0	
>> 38 56	1.0000	0.0	0.0					
> OUTCROP	388							

> G	1.	4746.	14581.	1180.	0	0	0.	1
>>	488	0	0	0	0	0	0	
>>	78 50	1.0000	0.0	0.0	0	0	0	
>>								
> OUTCROP	389							
> G	1.	4752.	14663.	1164.	0	0	0.	1
>>	489	0	0	0	0	0	0	
>>	106 45	1.0000	0.0	0.0	0	0	0	
>>								
> OUTCROP	390							
> G	1.	4844.	14674.	1190.	0	0	0.	1
>>	103	0	0	0	0	0	0	
>>	81 22	1.0000	0.0	0.0	0	0	0	
>>								
> OUTCROP	391							
> G	1.	4796.	14799.	1140.	0	0	0.	1
>>	490	0	0	0	0	0	0	
>>	90 34	1.0000	0.0	0.0	0	0	0	
>>								
> OUTCROP	392							
> G	1.	4845.	14753.	1169.	0	0	0.	1
>>	106	0	0	0	0	0	0	
>>	48 30	1.0000	0.0	0.0	0	0	0	
>>								
> OUTCROP	393							
> G	1.	4872.	14857.	1157.	0	0	0.	1
>>	108	0	0	0	0	0	0	
>>	85 24	1.0000	0.0	0.0	0	0	0	
>>								
> OUTCROP	394							
> G	1.	4805.	14896.	1127.	0	0	0.	1
>>	111	0	0	0	0	0	0	
>>	88 22	1.0000	0.0	0.0	0	0	0	
>>								
> OUTCROP	395							
> G	1.	4884.	14886.	1155.	0	0	0.	1
>>	114	0	0	0	0	0	0	
>>	91 23	1.0000	0.0	0.0	0	0	0	
>>								
> OUTCROP	396							
> B	1.	4987.	14452.	1186.	0	0	0.	1
>>	117	0	0	0	0	0	0	
>>	84 25	1.0000	0.0	0.0	0	0	0	
>>								
> OUTCROP	397							
> B	1.	5052.	14471.	1170.	0	0	0.	1
>>	491	0	0	0	0	0	0	
>>	91 40	1.0000	0.0	0.0	0	0	0	
>>								
> OUTCROP	398							
> B	1.	5126.	14451.	1169.	0	0	0.	1
>>	120	0	0	0	0	0	0	
>>	77 27	1.0000	0.0	0.0	0	0	0	
>>								
> OUTCROP	399							
> B	1.	5202.	14367.	1168.	0	0	0.	1
>>	492	0	0	0	0	0	0	
>>	107 20	1.0000	0.0	0.0	0	0	0	
>>								
> OUTCROP	400							
> B	1.	5320.	14397.	1145.	0	0	0.	1
>>	493	0	0	0	0	0	0	
>>	48 40	1.0000	0.0	0.0	0	0	0	
>>								
> OUTCROP	401							
> B	1.	5218.	14492.	1154.	0	0	0.	1
>>	494	0	0	0	0	0	0	
>>	234 28	1.0000	0.0	0.0	0	0	0	
>>								
> OUTCROP	402							
> B	1.	5178.	14531.	1135.	0	0	0.	1
>>	122	0	0	0	0	0	0	
>>	36 30	1.0000	0.0	0.0	0	0	0	
>>								
> OUTCROP	403							
> B	1.	5306.	14593.	1118.	0	0	0.	1
>>	124	0	0	0	0	0	0	
>>	49 30	1.0000	0.0	0.0	0	0	0	
>>								
> OUTCROP	404							

> B	1-	5444.	14550.	1120.	0	0	0.	1
>>	495	0	0	0	0	0	0	
>>	159 37	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	405						
>>	B	1-	5480.	14558.	1120.	0	0	0.
>>	127	0	0	0	0	0	0	1
>>	140 10	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	406						
>>	S	1-	5515.	14627.	1110.	0	0	0.
>>	496	0	0	0	0	0	0	1
>>	164 7	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	407						
>>	B	1-	5558.	14574.	1109.	0	0	0.
>>	497	0	0	0	0	0	0	1
>>	159 7	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	408						
>>	B	1-	5845.	14638.	1070.	0	0	0.
>>	129	0	0	0	0	0	0	1
>>	51 10	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	409						
>>	S	1-	5519.	14381.	1148.	0	0	0.
>>	498	0	0	0	0	0	0	1
>>	78 14	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	410						
>>	S	1-	5624.	14189.	1167.	0	0	0.
>>	499	0	0	0	0	0	0	1
>>	65 5	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	411						
>>	S	1-	5386.	13809.	1242.	0	0	0.
>>	500	0	0	0	0	0	0	1
>>	81 84	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	412						
>>	S	1-	5400.	13779.	1245.	0	0	0.
>>	501	0	0	0	0	0	0	1
>>	71 90	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	413						
>>	S	1-	5426.	13720.	1250.	0	0	0.
>>	502	0	0	0	0	0	0	1
>>	241 79	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	414						
>>	S	1-	5428.	13636.	1271.	0	0	0.
>>	503	0	0	0	0	0	0	1
>>	83 89	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	415						
>>	S	1-	5467.	13505.	1285.	0	0	0.
>>	131	0	0	0	0	0	0	1
>>	82 30	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	416						
>>	S	1-	5487.	13400.	1295.	0	0	0.
>>	133	0	0	0	0	0	0	1
>>	76 40	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	417						
>>	S	1-	5496.	13220.	1317.	0	0	0.
>>	136	0	0	0	0	0	0	1
>>	252 30	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	418						
>>	S	1-	5537.	12996.	1333.	0	0	0.
>>	139	0	0	0	0	0	0	1
>>	82 35	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	419						
>>	S	1-	5724.	13636.	1229.	0	0	0.
>>	504	0	0	0	0	0	0	1
>>	75 40	1.0000	0.0	0.0	0	0	0	
>>	OUTCROP	420						



> S	1.	6424.	13878.	1135.	0	0	0.	1
>	505	0	0	0	0	0	0	
>	133 15	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	421						
> S	1.	6472.	13961.	1128.	0	0	0.	1
>	141	0	0	0	0	0	0	
>	89 16	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	422						
> S	1.	6562.	14082.	1095.	0	0	0.	1
>	506	0	0	0	0	0	0	
>	173 5	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	423						
> S	1.	6542.	14137.	1089.	0	0	0.	1
>	507	0	0	0	0	0	0	
>	351 11	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	450						
> G	1.	5896.	17746.	950.	0	0	0.	1
>	3	0	0	0	0	0	0	
>	271 32	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	451						
> G	1.	6170.	17550.	942.	0	0	0.	1
>	5	0	0	0	0	0	0	
>	258 42	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	452						
> H	1.	3014.	13552.	1663.	0	0	0.	1
>	7	0	0	0	0	0	0	
>	276 37	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	453						
> H	1.	3052.	13493.	1640.	0	0	0.	1
>	8	0	0	0	0	0	0	
>	234 38	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	454						
> H	1.	4624.	13134.	1554.	0	0	0.	1
>	10	0	0	0	0	0	0	
>	50 29	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	455						
> B	1.	4646.	13009.	1571.	0	0	0.	1
>	12	0	0	0	0	0	0	
>	77 34	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	456						
> 4	1.	4151.	13092.	1599.	0	0	0.	1
>	14	0	0	0	0	0	0	
>	83 31	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	457						
> H	1.	4823.	12475.	1526.	0	0	0.	1
>	16	0	0	0	0	0	0	
>	72 33	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	458						
> H	1.	4819.	12404.	1516.	0	0	0.	1
>	18	0	0	0	0	0	0	
>	69 43	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	459						
> H	1.	4834.	12364.	1510.	0	0	0.	1
>	20	0	0	0	0	0	0	
>	71 37	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	460						
> H	1.	4847.	12305.	1495.	0	0	0.	1
>	21	0	0	0	0	0	0	
>	70 34	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	461						
> E	1.	3818.	12561.	1460.	0	0	0.	1
>	23	0	0	0	0	0	0	
>	67 22	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	462						

> E	1.	3818.	12546.	1459.	0	0	0.	1
>	24	0	0	0	0	0	0	
>	71 28	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	463						
> E	1.	3839.	12497.	1457.	0	0	0.	1
>	25	0	0	0	0	0	0	
>	66 17	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	464						
> E	1.	3604.	12580.	1442.	0	0	0.	1
>	27	0	0	0	0	0	0	
>	259 49	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	465						
> E	1.	3613.	12469.	1426.	0	0	0.	1
>	29	0	0	0	0	0	0	
>	264 55	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	466						
> E	1.	3618.	12433.	1419.	0	0	0.	1
>	30	0	0	0	0	0	0	
>	262 60	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	467						
> C	1.	4049.	17817.	1075.	0	0	0.	1
>	32	0	0	0	0	0	0	
>	172 20	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	468						
> C	1.	3357.	17642.	1146.	0	0	0.	1
>	34	0	0	0	0	0	0	
>	94 14	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	469						
> C	1.	3409.	17650.	1147.	0	0	0.	1
>	35	0	0	0	0	0	0	
>	137 20	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	470						
> N	1.	3249.	17686.	1115.	0	0	0.	1
>	37	0	0	0	0	0	0	
>	184 12	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	471						
> C	1.	3349.	17531.	1122.	0	0	0.	1
>	39	0	0	0	0	0	0	
>	98 38	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	472						
> C	1.	3195.	17428.	1202.	0	0	0.	1
>	41	0	0	0	0	0	0	
>	136 19	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	473						
> C	1.	3206.	17417.	1202.	0	0	0.	1
>	42	0	0	0	0	0	0	
>	193 9	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	474						
> C	1.	3221.	17396.	1202.	0	0	0.	1
>	43	0	0	0	0	0	0	
>	154 16	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	475						
> C	1.	3101.	17390.	1240.	0	0	0.	1
>	45	0	0	0	0	0	0	
>	165 38	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	476						
> C	1.	2847.	17350.	1284.	0	0	0.	1
>	47	0	0	0	0	0	0	
>	171 8	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	477						
> C	1.	2806.	17319.	1287.	0	0	0.	1
>	48	0	0	0	0	0	0	
>	171 9	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	478						

> C	1.	2737.	17315.	1282.	0	0	0	0.	1
>	50	0	0	0	0	0	0		
>	217	5	1.0000	0.0	0.0	0	0		
>	OUTCROP	479							
>	C	1.	2689.	17298.	1286.	0	0	0.	1
>	51	0	0	0	0	0	0		
>	101	4	1.0000	0.0	0.0	0	0		
>	OUTCROP	480							
>	E	1.	3983.	16386.	1180.	0	0	0.	1
>	53	0	0	0	0	0	0		
>	267	27	1.0000	0.0	0.0	0	0		
>	OUTCROP	481							
>	E	1.	3882.	16408.	1130.	0	0	0.	1
>	55	0	0	0	0	0	0		
>	57	15	1.0000	0.0	0.0	0	0		
>	OUTCROP	482							
>	E	1.	3799.	16345.	1162.	0	0	0.	1
>	57	0	0	0	0	0	0		
>	52	15	1.0000	0.0	0.0	0	0		
>	OUTCROP	483							
>	E	1.	3601.	16234.	1220.	0	0	0.	1
>	59	0	0	0	0	0	0		
>	46	27	1.0000	0.0	0.0	0	0		
>	OUTCROP	484							
>	E	1.	3350.	16077.	1273.	0	0	0.	1
>	61	0	0	0	0	0	0		
>	210	6	1.0000	0.0	0.0	0	0		
>	OUTCROP	485							
>	E	1.	4280.	16350.	1323.	0	0	0.	1
>	63	0	0	0	0	0	0		
>	97	8	1.0000	0.0	0.0	0	0		
>	OUTCROP	486							
>	G	1.	2937.	15196.	1514.	0	0	0.	1
>	65	0	0	0	0	0	0		
>	255	21	1.0000	0.0	0.0	0	0		
>	OUTCROP	487							
>	G	1.	2779.	15232.	1540.	0	0	0.	1
>	66	0	0	0	0	0	0		
>	265	43	1.0000	0.0	0.0	0	0		
>	OUTCROP	489							
>	G	1.	4393.	15931.	1115.	0	0	0.	1
>	68	0	0	0	0	0	0		
>	117	24	1.0000	0.0	0.0	0	0		
>	OUTCROP	490							
>	G	1.	4262.	15632.	1166.	0	0	0.	1
>	70	0	0	0	0	0	0		
>	72	29	1.0000	0.0	0.0	0	0		
>	OUTCROP	491							
>	G	1.	4333.	15183.	1182.	0	0	0.	1
>	72	0	0	0	0	0	0		
>	51	38	1.0000	0.0	0.0	0	0		
>	OUTCROP	492							
>	M	1.	3865.	15413.	1275.	0	0	0.	1
>	74	0	0	0	0	0	0		
>	96	24	1.0000	0.0	0.0	0	0		
>	OUTCROP	493							
>	M	1.	3952.	15153.	1290.	0	0	0.	1
>	76	0	0	0	0	0	0		
>	134	16	1.0000	0.0	0.0	0	0		
>	OUTCROP	494							
>	G	1.	4969.	15365.	1067.	0	0	0.	1
>	78	0	0	0	0	0	0		
>	121	20	1.0000	0.0	0.0	0	0		
>	OUTCROP	495							

> G 1-	4945.	15343.	1672.	0	0	0.	1
>> 79	0	0	0	0	0	0	
>> 101 17	1.0000	0.0	0.0	0	0	0	
> OUTCROP	496			0	0	0.	1
>> G 1-	4438.	14730.	1270.	0	0	0	
>>> 81	0	0	0	0	0	0	
>>> 83 14	1.0000	0.0	0.0	0	0	0	
> OUTCROP	497			0	0	0.	1
>> G 1-	4615.	14437.	1217.	0	0	0	
>>> 83	0	0	0	0	0	0	
>>> 67 62	1.0000	0.0	0.0	0	0	0	
> OUTCROP	498			0	0	0.	1
>> 5 1-	4417.	14463.	1261.	0	0	0	
>>> 85	0	0	0	0	0	0	
>>> 67 55	1.0000	0.0	0.0	0	0	0	
> OUTCROP	499			0	0	0.	1
>> 5 1-	4441.	14454.	1255.	0	0	0	
>>> 86	0	0	0	0	0	0	
>>> 69 48	1.0000	0.0	0.0	0	0	0	
> OUTCROP	500			0	0	0.	1
>> G 1-	4245.	14345.	1305.	0	0	0	
>>> 88	0	0	0	0	0	0	
>>> 113 25	1.0000	0.0	0.0	0	0	0	
> OUTCROP	501			0	0	0.	1
>> G 1-	4270.	14338.	1300.	0	0	0	
>>> 89	0	0	0	0	0	0	
>>> 83 24	1.0000	0.0	0.0	0	0	0	
> OUTCROP	502			0	0	0.	1
>> G 1-	4305.	14336.	1300.	0	0	0	
>>> 90	0	0	0	0	0	0	
>>> 82 27	1.0000	0.0	0.0	0	0	0	
> OUTCROP	503			0	0	0.	1
>> T 1-	4129.	14330.	1345.	0	0	0	
>>> 92	0	0	0	0	0	0	
>>> 151 26	1.0000	0.0	0.0	0	0	0	
> OUTCROP	504			0	0	0.	1
>> M 1-	3894.	14414.	1376.	0	0	0	
>>> 94	0	0	0	0	0	0	
>>> 46 22	1.0000	0.0	0.0	0	0	0	
> OUTCROP	505			0	0	0.	1
>> M 1-	3802.	14407.	1394.	0	0	0	
>>> 96	0	0	0	0	0	0	
>>> 96 8	1.0000	0.0	0.0	0	0	0	
> OUTCROP	506			0	0	0.	1
>> G 1-	4493.	13833.	1348.	0	0	0	
>>> 98	0	0	0	0	0	0	
>>> 151 25	1.0000	0.0	0.0	0	0	0	
> OUTCROP	507			0	0	0.	1
>> G 1-	4537.	13866.	1358.	0	0	0	
>>> 100	0	0	0	0	0	0	
>>> 143 26	1.0000	0.0	0.0	0	0	0	
> OUTCROP	508			0	0	0.	1
>> G 1-	4509.	13968.	1314.	0	0	0	
>>> 102	0	0	0	0	0	0	
>>> 132 10	1.0000	0.0	0.0	0	0	0	
> OUTCROP	509			0	0	0.	1
>> G 1-	4838.	14651.	1194.	0	0	0	
>>> 104	0	0	0	0	0	0	
>>> 74 26	1.0000	0.0	0.0	0	0	0	
> OUTCROP	510			0	0	0.	1
>> G 1-	4834.	14618.	1202.	0	0	0	
>>> 105	0	0	0	0	0	0	
>>> 72 30	1.0000	0.0	0.0	0	0	0	
> OUTCROP	511						

> G 1.	4859.	14733.	1179.	0	0	0	0.	1
>> 107	0	0	0	0	0	0		
>> 86 35	1.0000	0.0	0.0	0	0	0		
>>> OUTCROP	512							
> G 1.	4864.	14814.	1166.	0	0	0	0.	1
>> 109	0	0	0	0	0	0		
>> 88 28	1.0000	0.0	0.0	0	0	0		
>>> OUTCROP	513							
> G 1.	4874.	14777.	1173.	0	0	0	0.	1
>> 110	0	0	0	0	0	0		
>> 87 27	1.0000	0.0	0.0	0	0	0		
>>> OUTCROP	514							
> G 1.	4808.	14952.	1122.	0	0	0	0.	1
>> 112	0	0	0	0	0	0		
>> 103 23	1.0000	0.0	0.0	0	0	0		
>>> OUTCROP	515							
> G 1.	4830.	14995.	1109.	0	0	0	0.	1
>> 113	0	0	0	0	0	0		
>> 105 22	1.0000	0.0	0.0	0	0	0		
>>> OUTCROP	516							
> G 1.	4886.	14931.	1146.	0	0	0	0.	1
>> 115	0	0	0	0	0	0		
>> 90 32	1.0000	0.0	0.0	0	0	0		
>>> OUTCROP	517							
> G 1.	4897.	14981.	1135.	0	0	0	0.	1
>> 116	0	0	0	0	0	0		
>> 91 24	1.0000	0.0	0.0	0	0	0		
>>> OUTCROP	518							
> B 1.	4978.	14424.	1174.	0	0	0	0.	1
>> 118	0	0	0	0	0	0		
>> 85 34	1.0000	0.0	0.0	0	0	0		
>>> OUTCROP	519							
> B 1.	5016.	14388.	1193.	0	0	0	0.	1
>> 119	0	0	0	0	0	0		
>> 69 40	1.0000	0.0	0.0	0	0	0		
>>> OUTCROP	520							
> B 1.	5173.	14446.	1163.	0	0	0	0.	1
>> 121	0	0	0	0	0	0		
>> 82 25	1.0000	0.0	0.0	0	0	0		
>>> OUTCROP	521							
> B 1.	5241.	14541.	1126.	0	0	0	0.	1
>> 123	0	0	0	0	0	0		
>> 78 32	1.0000	0.0	0.0	0	0	0		
>>> OUTCROP	522							
> B 1.	5332.	14603.	1114.	0	0	0	0.	1
>> 125	0	0	0	0	0	0		
>> 46 35	1.0000	0.0	0.0	0	0	0		
>>> OUTCROP	523							
> B 1.	5382.	14568.	1110.	0	0	0	0.	1
>> 126	0	0	0	0	0	0		
>> 23 41	1.0000	0.0	0.0	0	0	0		
>>> OUTCROP	524							
> B 1.	5515.	14556.	1118.	0	0	0	0.	1
>> 128	0	0	0	0	0	0		
>> 136 6	1.0000	0.0	0.0	0	0	0		
>>> OUTCROP	525							
> B 1.	5894.	14607.	1073.	0	0	0	0.	1
>> 130	0	0	0	0	0	0		
>> 56 12	1.0000	0.0	0.0	0	0	0		
>>> OUTCROP	526							
> S 1.	5466.	13477.	1289.	0	0	0	0.	1
>> 132	0	0	0	0	0	0		
>> 84 30	1.0000	0.0	0.0	0	0	0		
>>> OUTCROP	527							

>	S	1.	5491.	13345.	1305.	0	0	0.	1
>		134	0	0	0	0	0	0	
>		76 40	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	528							
>	S	1.	5494.	13308.	1310.	0	0	0.	1
>		135	0	0	0	0	0	0	
>		75 30	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	529							
>	S	1.	5505.	13190.	1315.	0	0	0.	1
>		137	0	0	0	0	0	0	
>		128 45	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	530							
>	S	1.	5507.	13158.	1317.	0	0	0.	1
>		138	0	0	0	0	0	0	
>		98 30	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	531							
>	S	1.	5548.	12938.	1340.	0	0	0.	1
>		140	0	0	0	0	0	0	
>		74 35	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	532							
>	S	1.	6491.	14011.	1115.	0	0	0.	1
>		142	0	0	0	0	0	0	
>		107 10	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	533							
>	S	1.	6533.	14049.	1107.	0	0	0.	1
>		143	0	0	0	0	0	0	
>		97 5	1.0000	0.0	0.0	0	0	0	
>	OUTCROP	534							
>	U	1.	4866.	15613.	1062.	0	0	0.	0
>		144	0	0	0	0	0	0	
>		0 0	0.0	0.0	0.0	0	0	0	
>	OUTCROP	535							
>	U	1.	4041.	15132.	1265.	0	0	0.	0
>		145	0	0	0	0	0	0	
>		0 0	0.0	0.0	0.0	0	0	0	
>	OUTCROP	536							
>	U	1.	4698.	14057.	1270.	0	0	0.	0
>		146	0	0	0	0	0	0	
>		0 0	0.0	0.0	0.0	0	0	0	
>	OUTCROP	537							
>	U	1.	4421.	13754.	1365.	0	0	0.	0
>		147	0	0	0	0	0	0	
>		0 0	0.0	0.0	0.0	0	0	0	

BOREHOLE		1	997.	6838.	16629.	966.	6838.	16629.
>	6838.	16629.	997.	6838.	16629.	966.	6838.	16629.
>	7	6838.	16629.	958.				744.
>		6838.	16629.	957.				
>		6838.	16629.	947.				
>		6838.	16629.	946.				
>	6	6838.	16629.	942.				
>		6838.	16629.	941.				
>		6838.	16629.	933.				
>	5	6838.	16629.	931.				
>		6838.	16629.	877.				
>	4	6838.	16629.	871.				
>		6838.	16629.	851.				
>	3	6838.	16629.	847.				
>		6838.	16629.	828.				
>	2	6838.	16629.	827.				
>		6838.	16629.	813.				
>	1	6838.	16629.	810.				
>	T	6838.	16629.	801.				
>	M	6838.	16629.	786.				

BOREHOLE		11	1566.	2554.	15480.	1556.	2640.	15612.
>	2551.	15475.	1566.	2554.	15480.	1556.	2640.	15612.
>	6	2556.	15482.	1550.				
>		2559.	15487.	1539.				
>	9	2560.	15488.	1537.				1271.

>		2563.	15494.	1525.
>	8	2564.	15494.	1524.
>		2569.	15502.	1507.
>	7	2573.	15509.	1494.
>		2578.	15517.	1475.
>	6	2580.	15520.	1470.
>		2585.	15527.	1454.
>		2597.	15546.	1412.
>	4	2600.	15551.	1403.
>		2603.	15556.	1393.
>	3	2604.	15557.	1389.
>		2608.	15563.	1376.
>	2	2609.	15564.	1375.
>		2613.	15571.	1360.
>	1	2614.	15572.	1357.
>	T	2614.	15573.	1356.
>	M	2621.	15583.	1334.

>	BOREHOLE	52						
>	4738.	15005.	1139.	4737.	15005.	1117.	4727.	15004.
>	Y	4737.	15006.	1099.				863.
>		4737.	15006.	1098.				
>	X	4736.	15006.	1082.				
>		4736.	15006.	1078.				
>	9	4735.	15006.	1061.				
>		4735.	15006.	1058.				
>	8	4735.	15006.	1044.				
>		4734.	15006.	1043.				
>	7	4734.	15007.	1028.				
>		4734.	15007.	1026.				
>	6	4734.	15007.	1011.				
>		4733.	15007.	995.				
>	5	4733.	15007.	993.				
>		4732.	15007.	947.				
>	4	4732.	15007.	936.				
>		4731.	15006.	930.				
>	3	4731.	15006.	925.				
>		4731.	15006.	909.				
>	2	4731.	15006.	908.				
>		4730.	15006.	889.				
>	T	4730.	15006.	886.				
>	M	4730.	15006.	882.				
>		4729.	15005.	858.				

>	BOREHOLE	53						
>	3851.	15822.	1216.	3851.	15822.	1211.	3850.	15810.
>	E	3851.	15821.	1199.				1036.
>		3851.	15820.	1178.				
>	O	3851.	15820.	1177.				
>		3852.	15819.	1150.				
>	O	3852.	15819.	1146.				
>		3851.	15813.	1066.				
>	O	3851.	15813.	1065.				
>		3851.	15813.	1061.				
>	O	3851.	15813.	1060.				
>	C	3850.	15811.	1041.				

>	BOREHOLE	57						
>	4814.	15549.	1074.	4814.	15549.	1070.	4811.	15548.
>	X	4814.	15549.	1066.				865.
>		4814.	15549.	1062.				
>	9	4814.	15549.	1044.				
>		4814.	15549.	1041.				
>	8	4814.	15549.	1026.				
>		4814.	15549.	1025.				
>	7	4814.	15549.	1018.				
>		4814.	15549.	1015.				
>	6	4814.	15549.	1003.				
>		4814.	15549.	1001.				
>	5	4814.	15549.	987.				
>		4813.	15548.	985.				
>	4	4813.	15548.	942.				
>		4813.	15548.	933.				
>	3	4813.	15548.	921.				
>		4812.	15548.	916.				
>	2	4812.	15548.	899.				
>		4811.	15548.	899.				
>	1	4811.	15548.	886.				
>		4811.	15548.	883.				

> T	4811.	15548.	881.					
> BOREHOLE	58							
> 4498.	15646.	1120.	4498.	15646.	1116.	4498.	15646.	
> 5	4498.	15646.	1099.					1020.
> 4	4498.	15646.	1097.					
> 4	4498.	15646.	1061.					
> 4	4498.	15646.	1051.					
> 4	4498.	15646.	1032.					
> 3	4498.	15646.	1027.					
> T	4498.	15646.	1023.					
> BOREHOLE	101							
> 4333.	15637.	1147.	4333.	15637.	1135.	4332.	15637.	
> 4	4333.	15637.	1135.					109E.
> 4	4333.	15637.	1133.					
> 3	4333.	15637.	1112.					
> 3	4332.	15637.	1104.					
> BOREHOLE	102							
> 4290.	15712.	1151.	4290.	15712.	1149.	4290.	15712.	
> 3	4290.	15712.	1137.					1120.
> 3	4290.	15712.	1129.					
> BOREHOLE	103							
> 4276.	15744.	1151.	4276.	15744.	1146.	4276.	15744.	
> 3	4276.	15744.	1142.					1126.
> 3	4276.	15744.	1134.					
> BOREHOLE	104							
> 4255.	15773.	1150.	4255.	15773.	1138.	4255.	15773.	
> BOREHOLE	105							
> 4309.	15687.	1149.	4309.	15687.	1146.	4309.	15687.	
> 3	4309.	15687.	1125.					1112.
> 3	4309.	15687.	1117.					
> BOREHOLE	112							
> 5038.	16571.	1010.	5038.	16571.	1009.	5038.	16571.	
> BOREHOLE	114							
> 3456.	13819.	1508.	3456.	13819.	1499.	3456.	13819.	
> P	3456.	13819.	1496.					
> E	3456.	13819.	1456.					1324.
> 0	3456.	13819.	1444.					
> 0	3456.	13819.	1444.					
> 0	3456.	13819.	1416.					
> 0	3456.	13819.	1414.					
> 0	3456.	13819.	1349.					
> 0	3456.	13819.	1348.					
> 0	3456.	13819.	1338.					
> 0	3456.	13819.	1337.					
> BOREHOLE	115							
> 3969.	14474.	1373.	3969.	14474.	1371.	3969.	14474.	
> P	3969.	14474.	1315.					
> E	3969.	14474.	1284.					1190.
> 0	3969.	14474.	1264.					
> 0	3969.	14474.	1261.					
> 0	3969.	14474.	1233.					
> 0	3969.	14474.	1230.					
> 0	3969.	14474.	1210.					
> 0	3969.	14474.	1208.					
> BOREHOLE	121							
> 5031.	16566.	1012.	5031.	16566.	950.	5031.	16566.	
> BOREHOLE	151							
> 6301.	16999.	992.	6301.	16999.	957.	6301.	16999.	
> 8	6301.	16999.	957.					
> 7	6301.	16999.	940.					725.
> 7	6301.	16999.	939.					
> 6	6301.	16999.	922.					
> 6	6301.	16999.	920.					
> 6	6301.	16999.	915.					
> 6	6301.	16999.	914.					
> 5	6301.	16999.	902.					
> 5	6301.	16999.	898.					
> 4	6301.	16999.	856.					
> 4	6301.	16999.	850.					



>	6301.	16999.	831.
>>	3 6301.	16999.	827.
>>>	6301.	16999.	790.
>>>	1 6301.	16999.	786.
>>>	T 6301.	16999.	778.
>>>	M 6301.	16999.	754.

>	BOREHOLE	152					
>>	5183.	15985	1021.	5184.	15985.	989.	5183. 15988.
>>>	F 5184.	15985.	989.				664.
>>>	5184.	15985.	982.				
>>>	6 5184.	15985.	976.				
>>>	F 5184.	15985.	972.				
>>>	5 5184.	15985.	948.				
>>>	5 5184.	15985.	946.				
>>>	5 5185.	15985.	879.				
>>>	F 5186.	15985.	871.				
>>>	4 5186.	15985.	862.				
>>>	5 5186.	15985.	852.				
>>>	F 5186.	15985.	848.				
>>>	F 5186.	15985.	843.				
>>>	3 5186.	15985.	838.				
>>>	5 5186.	15985.	818.				
>>>	2 5186.	15985.	817.				
>>>	5 5186.	15985.	815.				
>>>	1 5186.	15985.	810.				
>>>	T 5186.	15985.	804.				
>>>	M 5186.	15985.	790.				
>>>	F 5186.	15986.	753.				
>>>	3 5186.	15986.	751.				
>>>	5 5186.	15986.	730.				
>>>	2 5186.	15986.	729.				
>>>	5 5186.	15986.	726.				
>>>	1 5185.	15986.	722.				
>>>	T 5185.	15987.	718.				
>>>	M 5185.	15987.	705.				

>	BOREHOLE	153					
>>	4837.	16475	1022.	4837.	16475.	1001.	4832. 16492.
>>>	P 4838.	16475.	954.				691.
>>>	F 4838.	16475.	936.				
>>>	P 4836.	16473.	866.				
>>>	E 4836.	16475.	831.				
>>>	4836.	16476.	823.				
>>>	0 4836.	16477.	820.				
>>>	4835.	16480.	789.				
>>>	0 4835.	16481.	786.				
>>>	4835.	16484.	760.				
>>>	0 4835.	16484.	760.				
>>>	C 4832.	16492.	695.				

>	BOREHOLE	154					
>>	4288.	15005	1239.	4288.	15005.	1236.	4273. 14997.
>>>	4287.	15005.	1205.				538.
>>>	4 4286.	15005.	1194.				
>>>	4286.	15005.	1181.				
>>>	3 4286.	15006.	1174.				
>>>	4285.	15006.	1156.				
>>>	2 4285.	15006.	1156.				
>>>	4284.	15006.	1136.				
>>>	1 4284.	15006.	1134.				
>>>	T 4284.	15006.	1132.				
>>>	M 4283.	15005.	1100.				
>>>	P 4281.	15004.	1022.				
>>>	E 4279.	15004.	985.				
>>>	4279.	15003.	974.				
>>>	0 4278.	15003.	971.				
>>>	4277.	15002.	936.				
>>>	0 4277.	15002.	933.				
>>>	4276.	15001.	910.				
>>>	0 4276.	15001.	909.				
>>>	C 4273.	14998.	842.				

>	BOREHOLE	155					
>>	4475.	14579	1246.	4475.	14579.	1219.	4478. 14584.
>>>	4475.	14579.	1207.				978.
>>>	7 4475.	14579.	1204.				
>>>	4475.	14580.	1189.				
>>>	6 4475.	14580.	1185.				
>>>	4476.	14581.	1167.				

>	5	4476.	14581.	1164.
>		4476.	14582.	1116.
>	4	4476.	14582.	1105.
>		4476.	14582.	1098.
>	3	4476.	14582.	1092.
>		4477.	14582.	1042.
>	2	4477.	14582.	1041.
>		4477.	14583.	1040.
>	1	4477.	14583.	1038.
>	T	4477.	14583.	1034.
>	M	4478.	14584.	1002.

>	BOREHOLE	156						
>	4675.	13995.	1302.	4675.	13995.	1298.	4673.	13975.
>		4675.	13995.					
>	8	4675.	13995.					936.
>		4674.	13995.					
>	7	4674.	13995.					
>		4674.	13994.					
>		4674.	13994.					
>	6	4674.	13994.					
>		4673.	13994.					
>	5	4673.	13994.					
>		4673.	13994.					
>	5	4673.	13994.					
>		4673.	13991.					
>	4	4674.	13991.					
>		4674.	13990.					
>	3	4674.	13989.					
>		4674.	13988.					
>	2	4674.	13988.					
>		4674.	13985.					
>	1	4674.	13985.					
>	T	4674.	13984.					
>	M	4674.	13981.					

>	BOREHOLE	157						
>	3182.	15511.	1404.	3182.	15511.	1395.	3180.	15512.
>	P	3181.	15512.					
>	E	3181.	15512.					1196.
>		3180.	15512.					
>	O	3180.	15512.					
>		3180.	15513.					
>	O	3180.	15513.					
>	C	3180.	15512.					

>	BOREHOLE	158						
>	3425.	14579.	1466.	3425.	14579.	1461.	3425.	14579.
>	E	3425.	14579.					1290.
>		3425.	14579.					
>	O	3425.	14579.					
>		3425.	14579.					
>	O	3425.	14579.					
>	C	3425.	14579.					

>	BOREHOLE	159						
>	2847.	15644.	1553.	2847.	15644.	1549.	2865.	15659.
>		2847.	15644.					
>	5	2847.	15644.					1316.
>		2846.	15644.					
>	4	2846.	15646.					
>	F	2847.	15646.					
>	4	2847.	15650.					
>		2848.	15652.					
>	3	2848.	15652.					
>		2849.	15655.					
>	2	2849.	15655.					
>		2854.	15657.					
>	1	2855.	15657.					
>	T	2857.	15658.					
>	M	2862.	15658.					

>	BOREHOLE	160						
>	4388.	12933.	1576.	4388.	12933.	1571.	4388.	12933.
>		4388.	12933.					
>	9	4388.	12933.					
>		4388.	12933.					1336.
>	7	4388.	12933.					
>		4388.	12933.					

>	6	43888	12933	1494
>		43888	12933	1482
>	5	43888	12933	1479
>		43888	12933	1442
>		43888	12933	1438
>	4	43888	12933	1435
>		43888	12933	1420
>	3	43888	12933	1417
>		43888	12933	1389
>	2	43888	12933	1389
>		43888	12933	1366
>	1	43888	12933	1365
>	T	43888	12933	1360

>	BOREHOLE	161					
>		4199	12856	1559	4199	12856	1553
>		4199	12857	1535			4194
>		4199	12857	1532			12861
>		4199	12857	1529			1371
>	4	4199	12857	1527			
>		4199	12858	1515			
>	3	4199	12858	1511			
>		4198	12859	1457			
>	1	4198	12859	1456			
>	T	4198	12860	1452			
>	M	4197	12860	1421			
>	P	4195	12861	1359			

>	BOREHOLE	162					
>		5457	16497	1004	5454	16498	920
>	H	5450	16500	803			5448
>							16503
>							746

>	BOREHOLE	163					
>		4320	13485	1440	4320	13485	1434
>		4320	13484	1413			4318
>		4320	13484	1409			13475
>		4320	13484	1407			1231
>	4	4320	13484	1403			
>		4320	13483	1393			
>	3	4321	13483	1389			
>		4320	13482	1338			
>	1	4320	13481	1336			
>	T	4320	13481	1333			
>	M	4320	13480	1303			

>	BOREHOLE	172					
>		5062	11980	1437	5062	11980	1434
>	H	5061	11980	1418			5020
>	G	5055	11979	1330			11947
>		5054	11979	1325			1111
>	Z	5054	11979	1324			
>		5053	11978	1312			
>	Y	5053	11978	1312			
>		5051	11977	1287			
>	X	5051	11977	1286			
>		5050	11977	1269			
>	9	5049	11976	1264			
>		5048	11975	1249			
>	8	5048	11975	1248			
>		5044	11973	1209			
>	7	5044	11973	1209			
>		5043	11972	1198			
>		5043	11972	1196			
>		5042	11971	1193			
>	6	5042	11971	1193			
>		5041	11970	1181			
>	5	5041	11970	1175			
>		5038	11968	1152			
>		5038	11967	1149			
>		5037	11967	1146			
>	4	5037	11967	1144			
>		5035	11965	1128			
>	3	5035	11964	1123			
>		5030	11960	1087			
>	2	5030	11960	1087			
>		5028	11958	1072			
>	1	5028	11958	1071			
>	T	5028	11957	1067			
>	M	5025	11954	1046			

BOREHOLE	173	1194.	4975.	14488.	1186.	4951.	14477.
H	4974.	14488.					803.
G	4969.	14488.					
Z	4969.	14488.					
X	4967.	14488.					
9	4966.	14487.					
8	4965.	14487.					
7	4964.	14486.					
6	4963.	14486.					
5	4961.	14485.					
4	4957.	14482.					
3	4956.	14481.					
2	4955.	14480.					
1	4952.	14478.					
T	4952.	14478.					

BOREHOLE	174	1012.	5031.	16566.	931.	5023.	16577.
F	5029.	16571.					751.
4	5028.	16571.					
3	5027.	16572.					
2	5027.	16573.					
1	5026.	16574.					
T	5026.	16575.					
M	5025.	16576.					
P	5024.	16577.					

BOREHOLE	204	1008.	7453.	16033.	994.	7432.	16075.
H	7454.	16033.					788.
G	7447.	16046.					
Z	7446.	16046.					
Y	7446.	16047.					
9	7440.	16057.					
8	7438.	16062.					
	7437.	16063.					

BOREHOLE	205	947.	5512.	18053.	929.	5512.	18053.
X	5512.	18053.					678.
9	5512.	18053.					
8	5512.	18053.					
7	5512.	18053.					
6	5512.	18053.					
5	5512.	18053.					
4	5512.	18053.					
3	5512.	18053.					
F	5512.	18053.					
3	5512.	18053.					

>		5512.	18053.	719.				
>	1	5512.	18053.	716.				
>	T	5512.	18053.	711.				
>	M	5512.	18053.	684.				

>	BOREHOLE	208						
>		2561.	15994.	1458.	2561.	15994.	1453.	2590. 16040.
>		2561.	15994.	1456.				1254.
>		2561.	15994.	1453.				
>		2561.	15994.	1444.				
>	4	2561.	15995.	1440.				
>	F	2561.	15995.	1439.				
>		2561.	15995.	1438.				
>	4	2561.	15995.	1432.				
>		2561.	15997.	1418.				
>	3	2561.	15998.	1412.				
>		2561.	16001.	1393.				
>	2	2561.	16001.	1391.				
>		2562.	16004.	1376.				
>	1	2563.	16005.	1372.				
>	T	2563.	16006.	1368.				
>	M	2567.	16012.	1337.				
>	Q	2585.	16034.	1267.				

>	BOREHOLE	209						
>		6360.	16456.	1000.	6358.	16456.	961.	6435. 16494.
>		6357.	16456.	950.				761.
>	Z	6357.	16456.	948.				
>		6356.	16458.	918.				
>	Y	6356.	16458.	918.				
>		6357.	16461.	901.				
>	X	6357.	16461.	900.				
>		6358.	16463.	891.				
>	9	6358.	16463.	889.				
>		6362.	16471.	858.				
>	7	6363.	16471.	857.				
>		6371.	16474.	840.				
>	6	6371.	16475.	840.				
>		6375.	16476.	833.				
>	5	6376.	16477.	830.				
>		6404.	16494.	789.				
>	4	6407.	16496.	785.				
>		6421.	16499.	772.				
>	3	6424.	16497.	770.				

>	BOREHOLE	210						
>		1970.	15994.	1463.	1970.	15994.	1458.	1932. 15964.
>		1969.	15994.	1435.				1274.
>		1969.	15994.	1434.				
>		1968.	15993.	1424.				
>	6	1968.	15993.	1423.				
>		1966.	15992.	1407.				
>	5	1965.	15992.	1404.				
>		1961.	15988.	1381.				
>		1960.	15988.	1377.				
>		1954.	15983.	1354.				
>	4	1954.	15982.	1352.				
>		1952.	15981.	1345.				
>	3	1951.	15980.	1340.				
>		1946.	15975.	1323.				
>	2	1945.	15974.	1321.				
>		1941.	15970.	1306.				
>	1	1941.	15970.	1305.				
>	T	1939.	15968.	1296.				

>	BOREHOLE	211						
>		2226.	16007.	1433.	2226.	16007.	1427.	2209. 15996.
>		2226.	16007.	1410.				1198.
>	Y	2226.	16007.	1410.				
>		2226.	16007.	1389.				
>	X	2226.	16007.	1387.				
>		2226.	16007.	1374.				
>	9	2226.	16007.	1371.				
>		2225.	16006.	1343.				
>	8	2225.	16006.	1342.				
>		2224.	16006.	1332.				
>	7	2224.	16006.	1331.				
>		2224.	16005.	1315.				
>	6	2223.	16005.	1312.				
>		2220.	16003.	1280.				



>	BOREHOLE	217						
>		4469.	14284.	1279.	4470.	14284.	1258.	4471. 14282.
>		4470.	14284.	1257.				
>		4470.	14284.	1254.				1276.
>		4470.	14284.	1252.				
>	4	4470.	14284.	1249.				
>		4470.	14284.	1241.				
>	3	4471.	14283.	1235.				
>	BOREHOLE	218						
>		4637.	14322.	1243.	4637.	14322.	1231.	4637. 14322.
>	BOREHOLE	219						1231.
>		4554.	14364.	1257.	4554.	14364.	1252.	4553. 14358.
>		4554.	14364.	1247.				
>	7	4554.	14363.	1244.				1171.
>		4554.	14362.	1229.				
>		4554.	14362.	1229.				
>		4554.	14362.	1227.				
>	6	4554.	14362.	1225.				
>		4553.	14359.	1186.				
>	5	4553.	14359.	1182.				
>	BOREHOLE	220						
>		4526.	14342.	1266.	4526.	14342.	1260.	4518. 14349.
>		4525.	14343.	1232.				
>	5	4525.	14343.	1228.				1132.
>		4521.	14348.	1154.				
>		4521.	14348.	1153.				
>		4521.	14348.	1152.				
>		4520.	14348.	1144.				
>		4519.	14348.	1143.				
>	4	4518.	14349.	1137.				
>	BOREHOLE	221						
>		4703.	14389.	1224.	4703.	14389.	1210.	4686. 14358.
>		4703.	14388.	1208.				
>	9	4703.	14388.	1204.				961.
>		4703.	14387.	1188.				
>	8	4703.	14387.	1187.				
>		4703.	14383.	1146.				
>	7	4704.	14383.	1143.				
>		4704.	14381.	1134.				
>		4704.	14381.	1133.				
>		4704.	14381.	1131.				
>	6	4704.	14380.	1129.				
>		4703.	14376.	1104.				
>		4702.	14371.	1075.				
>	7	4702.	14371.	1074.				
>		4702.	14369.	1066.				
>		4702.	14369.	1065.				
>		4702.	14369.	1064.				
>	6	4702.	14368.	1062.				
>		4699.	14365.	1040.				
>	5	4699.	14364.	1038.				
>		4691.	14360.	990.				
>		4690.	14359.	982.				
>		4689.	14359.	977.				
>	4	4688.	14359.	971.				
>	BOREHOLE	222						
>		4773.	16056.	1038.	4773.	16056.	1032.	4750. 16070.
>		4773.	16056.	1026.				
>	3	4773.	16055.	1021.				
>		4772.	16055.	1002.				828.
>	2	4772.	16055.	1001.				
>	F	4772.	16055.	1000.				
>		4771.	16054.	985.				
>	2	4771.	16054.	985.				
>		4770.	16054.	971.				
>	1	4769.	16055.	968.				
>	T	4769.	16055.	965.				
>	M	4765.	16056.	932.				
>	P	4755.	16064.	861.				
>	E	4750.	16070.	830.				
>	BOREHOLE	226						
>		4366.	19956.	959.	4366.	19956.	929.	4359. 19950.
>		4364.	19954.	891.				
>	1	4364.	19954.	888.				824.

>	M	4363.	19952.	866.					
>	BOREHOLE	232							
>		7921.	14674.	1056.	7921.	14674.	1051.	7892.	14681.
>	B	7910.	14680.	883.					752.
>	H	7895.	14681.	771.					
>	BOREHOLE	235							
>		8048.	14707.	1045.	8048.	14707.	1041.	8048.	14707.
>	S	8048.	14707.	1044.					1040.
>	BOREHOLE	251							
>		5621.	16022.	1010.	5620.	16022.	968.	5619.	16022.
>		5620.	16022.	927.					729.
>	4	5620.	16022.	914.					
>		5619.	16022.	896.					
>	3	5619.	16022.	890.					
>		5619.	16022.	869.					
>	2	5619.	16022.	869.					
>	F	5619.	16022.	867.					
>		5619.	16022.	857.					
>	2	5619.	16022.	855.					
>		5619.	16022.	844.					
>	1	5619.	16022.	839.					
>	T	5619.	16022.	834.					
>	M	5619.	16022.	801.					
>	BOREHOLE	252							
>		5136.	15504.	1043.	5136.	15504.	1029.	5134.	15507.
>		5136.	15504.	1022.					741.
>	Z	5136.	15504.	1021.					
>		5136.	15504.	1012.					
>		5136.	15504.	1011.					
>		5136.	15504.	1008.					
>	Y	5136.	15504.	1007.					
>		5136.	15504.	979.					
>		5136.	15504.	978.					
>		5136.	15504.	962.					
>	X	5136.	15504.	962.					
>		5136.	15504.	937.					
>	9	5136.	15504.	934.					
>		5136.	15504.	924.					
>	8	5136.	15504.	923.					
>		5136.	15504.	909.					
>	7	5136.	15504.	907.					
>		5136.	15504.	889.					
>	6	5136.	15504.	888.					
>		5136.	15504.	871.					
>	5	5136.	15504.	870.					
>		5135.	15505.	821.					
>	4	5135.	15505.	812.					
>		5135.	15505.	810.					
>	3	5135.	15505.	803.					
>		5135.	15506.	786.					
>	2	5135.	15506.	785.					
>		5135.	15506.	768.					
>	1	5135.	15506.	765.					
>	F	5134.	15507.	758.					
>		5134.	15507.	750.					
>	1	5134.	15507.	745.					
>	BOREHOLE	253							
>		5170.	14948.	1121.	5170.	14948.	1118.	5161.	14941.
>	H	5170.	14948.	1085.					702.
>	G	5169.	14946.	951.					
>		5169.	14946.	946.					
>	Z	5169.	14946.	946.					
>		5169.	14946.	939.					
>	Y	5169.	14946.	938.					
>		5169.	14946.	910.					
>	X	5169.	14946.	909.					
>		5168.	14945.	868.					
>	9	5167.	14945.	865.					
>		5167.	14945.	862.					
>	8	5167.	14945.	861.					
>		5167.	14944.	830.					
>	7	5166.	14944.	828.					
>		5166.	14944.	819.					
>	6	5166.	14944.	814.					
>		5165.	14943.	793.					



>	5	5165.	14943.	791.
>>		5163.	14942.	740.
>>	4	5163.	14942.	731.
>>		5162.	14942.	725.
>>	3	5162.	14941.	720.

>	BOREHOLE	254					
>	4951.	13403.	1417.	4951.	13403.	1415.	4951. 13406.
>>	Q	4951.	13403.				
>>	F	4951.	13403.				1160.
>>	Q	4951.	13403.				
>>	F	4951.	13403.				
>>	Q	4951.	13403.				
>>	G	4951.	13404.				
>>		4951.	13404.				
>>	Z	4951.	13404.				
>>		4951.	13405.				
>>	Y	4951.	13405.				
>>		4951.	13406.				
>>	X	4951.	13406.				
>>		4951.	13406.				
>>	9	4951.	13406.				

>	BOREHOLE	255					
>	4797.	12527.	1518.	4797.	12527.	1509.	4786. 12524.
>>	G	4797.	12527.				1156.
>>		4797.	12527.				
>>	Z	4797.	12527.				
>>		4797.	12527.				
>>	Y	4797.	12527.				
>>		4796.	12527.				
>>	X	4796.	12527.				
>>		4796.	12527.				
>>	9	4796.	12527.				
>>		4796.	12527.				
>>	8	4796.	12527.				
>>		4795.	12526.				
>>	7	4795.	12526.				
>>		4794.	12526.				
>>		4794.	12526.				
>>		4794.	12526.				
>>	6	4794.	12526.				
>>		4793.	12526.				
>>	5	4793.	12526.				
>>		4792.	12526.				
>>		4791.	12526.				
>>	4	4791.	12526.				
>>		4790.	12525.				
>>	3	4790.	12525.				
>>		4788.	12525.				
>>	2	4788.	12525.				
>>		4786.	12524.				
>>	1	4786.	12524.				
>>	T	4786.	12524.				

>	BOREHOLE	256					
>	5422.	11516.	1353.	5422.	11516.	1341.	5422. 11516.
>>	H	5422.	11516.				918.
>>	G	5422.	11516.				
>>		5422.	11516.				
>>	Z	5422.	11516.				
>>		5422.	11516.				
>>	Y	5422.	11516.				
>>		5422.	11516.				
>>	X	5422.	11516.				
>>		5422.	11516.				
>>	9	5422.	11516.				
>>		5422.	11516.				
>>	8	5422.	11516.				
>>		5422.	11516.				
>>	7	5422.	11516.				
>>		5422.	11516.				
>>		5422.	11516.				
>>		5422.	11516.				
>>	6	5422.	11516.				
>>		5422.	11516.				
>>	5	5422.	11516.				
>>		5422.	11516.				
>>		5422.	11516.				

V	5422.	11516.	1010.
V	5422.	11516.	1007.
V	5422.	11516.	987.
V	5422.	11516.	983.
V	5422.	11516.	981.
V	5422.	11516.	981.
V	5422.	11516.	966.
V	5422.	11516.	963.
V	5422.	11516.	943.
V	5422.	11516.	942.
V	5422.	11516.	937.

>BOREHOLE	259						
V	5260.	17506.	958.	5260.	17506.	857.	5260. 17506. 857.

>BOREHOLE	264						
V	5653.	17371.	965.	5653.	17371.	897.	5653. 17371. 579.

V	G	5653.	17371.	841.
V	Z	5653.	17371.	831.
V		5653.	17371.	830.
V	Y	5653.	17371.	803.
V		5653.	17371.	802.
V	X	5653.	17371.	782.
V		5653.	17371.	781.
V	9	5653.	17371.	763.
V		5653.	17371.	760.
V		5653.	17371.	755.
V		5653.	17371.	754.
V		5653.	17371.	750.
V	8	5653.	17371.	749.
V		5653.	17371.	741.
V	7	5653.	17371.	740.
V		5653.	17371.	723.
V		5653.	17371.	722.
V	6	5653.	17371.	715.
V		5653.	17371.	714.
V		5653.	17371.	680.
V	5	5653.	17371.	677.
V		5653.	17371.	674.
V	4	5653.	17371.	667.
V		5653.	17371.	639.
V	3	5653.	17371.	635.
V		5653.	17371.	604.
V	1	5653.	17371.	600.
V	T	5653.	17371.	591.

>BOREHOLE	266						
V	4612.	15230.	1136.	4612.	15230.	1133.	4610. 15229. 433.

V	9	4612.	15230.	1115.
V		4612.	15230.	1111.
V		4612.	15230.	1099.
V	8	4612.	15230.	1097.
V		4612.	15230.	1086.
V	7	4612.	15230.	1085.
V		4612.	15230.	1072.
V	6	4612.	15230.	1068.
V		4612.	15230.	1052.
V	5	4612.	15230.	1050.
V		4611.	15229.	1004.
V	4	4611.	15229.	994.
V		4611.	15229.	984.
V	3	4611.	15229.	977.
V		4611.	15229.	960.
V	2	4611.	15229.	959.
V		4611.	15229.	943.
V	1	4610.	15229.	939.
V	T	4610.	15229.	934.

>BOREHOLE	307						
V	4584.	19373.	934.	4584.	19373.	864.	4584. 19373. 830.

V	3	4584.	19373.	844.
V		4584.	19373.	839.

>BOREHOLE	308						
V	4916.	19031.	933.	4916.	19031.	842.	4916. 19031. 842.

>BOREHOLE	310						
V	4590.	19037.	932.	4590.	19037.	836.	4590. 19037. 812.

>BOREHOLE	312						
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>	4554.	18424.	936.	4554.	18424.	863.	4554.	18424.
>	BOREHOLE	313						
>	4981.	18422.	937.	4981.	18422.	876.	4981.	18422.
>	BOREHOLE	314						872.
>	5114.	18013.	939.	5114.	18013.	860.	5114.	18013.
>	BOREHOLE	315						860.
>	4692.	17992.	940.	4692.	17992.	880.	4692.	17992.
>	BOREHOLE	317						880.
>	4905.	19031.	933.	4902.	19029.	835.	4879.	19026.
>	H	4905.	19031.					729.
>	Q	4901.	19029.					
>	G	4895.	19026.					
>		4895.	19026.					
>	Z	4894.	19026.					
>		4894.	19026.					
>		4894.	19026.					
>		4893.	19026.					
>	Y	4893.	19026.					
>		4888.	19026.					
>		4888.	19026.					
>		4887.	19026.					
>	X	4887.	19026.					
>		4886.	19025.					
>	9	4885.	19025.					
>	BOREHOLE	319						
>	7102.	15932.	1002.	7102.	15931.	984.	7083.	15925.
>		7102.	15932.					314.
>	S	7102.	15931.					
>	H	7101.	15930.					
>	G	7091.	15926.					
>		7091.	15926.					
>	S	7091.	15926.					
>		7090.	15926.					
>	S	7090.	15926.					
>		7086.	15925.					
>	X	7086.	15925.					
>		7085.	15925.					
>	9	7085.	15925.					
>	BOREHOLE	321						
>	4352.	14928.	1243.	4352.	14928.	1237.	4351.	14933.
>		4352.	14928.					1151.
>	5	4352.	14928.					
>		4352.	14931.					
>		4352.	14932.					
>		4351.	14932.					
>	4	4351.	14932.					
>	BOREHOLE	322						
>	4094.	15100.	1259.	4094.	15100.	1253.	4095.	15101.
>		4094.	15100.					1228.
>	1	4094.	15100.					
>	BOREHOLE	334						
>	4796.	19745.	953.	4796.	19745.	876.	4796.	19745.
>	BOREHOLE	338						566.
>	6197.	17261.	977.	6197.	17261.	968.	6197.	17261.
>		6197.	17261.					797.
>	8	6197.	17261.					
>		6197.	17261.					
>	7	6197.	17261.					
>		6197.	17261.					
>		6197.	17261.					
>		6197.	17261.					
>	6	6197.	17261.					
>		6197.	17261.					
>	5	6197.	17261.					
>		6197.	17261.					
>	4	6197.	17261.					
>		6197.	17261.					
>	3	6197.	17261.					
>		6197.	17261.					
>	1	6197.	17261.					
>	T	6197.	17261.					

>	BOREHOLE	339						
>	4788	19745	953	4789	19747	867	4792	19754
>		4789	19747					777
>	3	4790	19748					
>		4792	19752					
>	1	4792	19753					

>	BOREHOLE	340						
>	6037	17484	978	6037	17484	972	6037	17484
>		6037	17484					745
>	9	6037	17484					
>		6037	17484					
>		6037	17484					
>		6037	17484					
>	8	6037	17484					
>		6037	17484					
>		6037	17484					
>	7	6037	17484					
>		6037	17484					
>		6037	17484					
>	6	6037	17484					
>		6037	17484					
>		6037	17484					
>	5	6037	17484					
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>		6037	17484					
>	4	6037	17484					
>		6037	17484					
>		6037	17484					
>	3	6037	17484					

>	BOREHOLE	346						
>	4849	16279	1030	4849	16279	1019	4831	16281
>	M	4849	16279					902
>	P	4836	16280					

>	BOREHOLE	349						
>	6750	16485	1001	6750	16485	974	6742	16493
>		6750	16485					895
>	7	6750	16485					
>		6749	16487					
>	6	6749	16487					
>		6748	16488					
>	5	6748	16488					

>	BOREHOLE	350						
>	5500	15807	1016	5500	15805	989	5546	15847
>		5503	15803					777
>		5503	15803					
>		5504	15804					
>	6	5504	15804					
>		5508	15806					
>	5	5508	15806					
>		5523	15818					
>		5525	15820					
>		5525	15820					
>	4	5527	15821					
>		5529	15824					
>	3	5530	15825					
>		5539	15837					
>	2	5539	15837					
>		5542	15841					
>	1	5544	15843					
>	T	5546	15846					

>	BOREHOLE	351						
>	5362	15741	1022	5362	15741	998	5373	15798
>		5362	15741					756
>	8	5362	15741					
>		5363	15744					
>		5363	15744					
>		5363	15744					
>	6	5363	15744					
>		5364	15747					
>	5	5364	15748					
>		5367	15761					
>	U	5367	15761					
>	F	5367	15762					
>	4	5367	15764					
>		5369	15773					
>	U	5369	15778					
>		5372	15792					

> 4 5372. 15795. 768.  
 > 5372. 15796. 765.  
 > 3 5373. 15796. 762.  
 >  
 > BOREHOLE 352  
 > 5058. 16172. 1024. 5058. 16172. 1008. 5063. 16172.  
 > 5058. 16173. 973.  
 > 4 5059. 16173. 961. 879.  
 > 5059. 16174. 957.  
 > 3 5059. 16174. 951.  
 > 5060. 16174. 936.  
 > 2 5060. 16174. 935.  
 > 5061. 16173. 923.  
 > 1 5061. 16173. 919.  
 > T 5061. 16172. 916.  
 > M 5062. 16171. 893.

> BOREHOLE 353  
 > 5264. 16391. 1007. 5282. 16389. 935. 5354. 16422.  
 > 5299. 16393. 901.  
 > 5300. 16393. 901. 779.  
 > 5300. 16394. 898.  
 > 6 5301. 16394. 897.  
 > 5305. 16395. 886.  
 > 5 5306. 16396. 883.  
 > 5327. 16401. 842.  
 > 4 5332. 16403. 833.  
 > 5341. 16410. 812.  
 > 3 5343. 16412. 806.  
 > 5348. 16416. 793.  
 > 5348. 16416. 792.  
 > 5349. 16418. 789.  
 > 2 5349. 16418. 789.

> BOREHOLE 357  
 > 6499. 16962. 1001. 6499. 16962. 965. 6499. 16962.  
 > 6499. 16962. 944. 934.  
 > 3 6499. 16962. 940.

> BOREHOLE 366  
 > 5033. 16987. 1002. 5026. 16987. 904. 5014. 17006.  
 > 5025. 16987. 878. 724.  
 > 5025. 16987. 877.  
 > 1/2 5024. 16988. 872.  
 > M 5021. 16988. 824.  
 > F 5020. 16988. 809.  
 > 5020. 16988. 805.  
 > 4 5018. 16989. 791.  
 > 5016. 16993. 771.  
 > 5016. 16993. 770.  
 > 5016. 16994. 769.  
 > 5016. 16995. 765.  
 > 5016. 16995. 764.

> BOREHOLE 367  
 > 3563. 13413. 1604. 3563. 13413. 1603. 3563. 13413.  
 > P 3563. 13413. 1528. 1434.  
 > E 3563. 13413. 1492.  
 > 3563. 13413. 1481.  
 > O 3563. 13413. 1480.  
 > 3563. 13413. 1477.  
 > 3563. 13413. 1477.  
 > 3563. 13413. 1470.  
 > O 3563. 13413. 1469.  
 > 3563. 13413. 1468.  
 > O 3563. 13413. 1468.

> BOREHOLE 368  
 > 4215. 15772. 1159. 4215. 15772. 1153. 4215. 15772.  
 > F 4215. 15772. 1144. 1127.  
 > 4215. 15772. 1139.  
 > 1 4215. 15772. 1135.

> BOREHOLE 442  
 > 6186. 17254. 977. 6186. 17254. 963. 6186. 17254.  
 > 6186. 17254. 947. 796.  
 > 7 6186. 17254. 945.  
 > 6186. 17254. 929.  
 > 6186. 17254. 928.  
 > 6186. 17254. 921.

>	6	6186.	17254.	921.
>		6186.	17254.	907.
>	5	6186.	17254.	901.
>		6186.	17254.	870.
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>		6186.	17254.	844.
>	3	6186.	17254.	840.
>		6186.	17254.	806.
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>	BOREHOLE	444						
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>								727.
>	9	6040.	17472.	959.				
>		6040.	17472.	956.				
>		6040.	17472.	953.				
>	8	6040.	17472.	948.				
>		6040.	17472.	932.				
>	7	6040.	17472.	929.				
>		6040.	17472.	914.				
>		6040.	17472.	913.				
>		6040.	17472.	905.				
>	6	6040.	17472.	904.				
>		6040.	17472.	871.				
>	5	6040.	17472.	867.				
>		6040.	17472.	862.				
>	4	6040.	17472.	855.				
>		6040.	17472.	834.				
>	3	6040.	17472.	830.				
>		6040.	17472.	795.				
>	1	6040.	17472.	792.				

>	BOREHOLE	460						
>		4279.	15735.	1152.	4279.	15735.	1148.	4276. 15732.
>								1072.
>	3	4279.	15735.	1141.				
>		4279.	15735.	1134.				
>		4278.	15735.	1114.				
>		4278.	15735.	1113.				
>		4278.	15735.	1111.				
>		4278.	15735.	1111.				
>		4278.	15735.	1109.				
>		4278.	15735.	1108.				
>		4278.	15735.	1108.				
>		4278.	15735.	1106.				
>		4277.	15735.	1105.				
>	1	4277.	15734.	1102.				
>	T	4277.	15733.	1090.				

>	BOREHOLE	461						
>		5057.	16169.	1024.	5057.	16169.	1000.	5055. 16170.
>								924.
>	4	5057.	16170.	972.				
>		5057.	16170.	960.				
>		5056.	16170.	956.				
>	3	5056.	16170.	949.				
>		5055.	16170.	934.				
>	2	5055.	16170.	933.				
>		5055.	16170.	929.				

>	BOREHOLE	469						
>		4216.	15772.	1158.	4216.	15772.	1152.	4216. 15772.
>								1127.
>		4216.	15772.	1148.				
>		4216.	15772.	1146.				
>		4216.	15772.	1143.				
>	2	4216.	15772.	1142.				
>		4216.	15772.	1139.				
>		4216.	15772.	1138.				
>		4216.	15772.	1137.				
>	1	4216.	15772.	1133.				
>	T	4216.	15772.	1131.				

>	BOREHOLE	506						
>		4076.	14682.	1399.	4076.	14682.	1393.	4076. 14682.
>								1345.
>	2	4076.	14682.	1358.				
>		4076.	14682.	1357.				
>		4076.	14682.	1356.				
>	1	4076.	14682.	1354.				
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>	BOREHOLE	507						
>		4587.	15896.	1078.	4587.	15896.	1075.	4587. 15896.
>								967.
>		4587.	15896.	1073.				

>	5	4587.	15896.	1071.
>		4587.	15896.	1040.
>	4	4587.	15896.	1031.
>		4587.	15896.	1012.
>	3	4587.	15896.	1008.
>		4587.	15896.	985.
>	2	4587.	15896.	985.
>		4587.	15896.	980.
>	1	4587.	15896.	977.
>	T	4587.	15896.	974.

>	BOREHOLE	511						
>		2797.	17298.	1286.	2797.	17298.	1283.	2797.
>	N	2797.	17298.	1240.				17298.
								85E.

>	BOREHOLE	601						
>		4062.	16044.	1160.	4062.	16044.	1157.	4039.
>	E	4057.	16041.	1070.				16034.
>		4056.	16041.	1064.				93E.
>	O	4056.	16040.	1061.				
>		4053.	16039.	1035.				
>	O	4052.	16039.	1030.				
>		4042.	16035.	957.				
>	O	4042.	16035.	956.				
>	C	4040.	16034.	944.				

>	BOREHOLE	603						
>		4535.	17370.	1020.	4533.	17373.	968.	4528.
>	C	4529.	17379.	883.				17380.
								872.

>	BOREHOLE	604						
>		4719.	16915.	1032.	4718.	16914.	989.	4701.
>	E	4715.	16915.	945.				16928.
>		4716.	16916.	931.				7E4.
>	O	4716.	16916.	927.				
>		4714.	16919.	896.				
>	O	4714.	16920.	890.				
>	C	4703.	16928.	792.				

>	BOREHOLE	612						
>		4064.	16045.	1160.	4064.	16045.	1157.	4054.
>	P	4062.	16046.	1102.				16047.
>	E	4059.	16047.	1068.				1227.
>		4058.	16047.	1061.				
>	O	4058.	16047.	1059.				
>		4054.	16047.	1030.				
>	D	4054.	16047.	1029.				

>	BOREHOLE	615						
>		4720.	16917.	1032.	4720.	16917.	987.	4720.
>	P	4720.	16917.	960.				16917.
>	E	4720.	16917.	945.				875.
>		4720.	16917.	925.				
>	O	4720.	16917.	923.				
>		4720.	16917.	887.				
>	O	4720.	16917.	884.				
>		4720.	16917.	883.				
>	O	4720.	16917.	882.				

>	BOREHOLE	616						
>		4607.	16469.	1037.	4607.	16469.	1020.	4604.
>	E	4607.	16480.	939.				16489.
>		4606.	16481.	934.				897.
>	O	4606.	16481.	931.				
>		4605.	16488.	903.				
>	O	4604.	16489.	899.				

>	BOREHOLE	621						
>		6056.	17313.	978.	6056.	17313.	966.	6056.
								17313.
								423.

>	BOREHOLE	622						
>		6587.	16343.	1001.	6587.	16343.	935.	6587.
								16343.
								434.

>	BOREHOLE	625						
>		5242.	16546.	1007.	5242.	16546.	918.	5242.
								16546.
								911.

>	BOREHOLE	626						
>		5217.	15908.	1020.	5217.	15908.	991.	5217.
								15908.
								9E6.

>BOREHOLE 632





>	4	4502.	15655.	1051.
>		4499.	15653.	1033.
>	3	4498.	15653.	1027.
>		4496.	15652.	1012.
>	2	4496.	15652.	1011.
>		4495.	15651.	1003.
>	1	4495.	15651.	1000.
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>	BOREHOLE	642						
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>		6034.	17299.					727.
>	X	6034.	17299.					
>		6034.	17299.					
>	9	6034.	17299.					
>		6034.	17299.					
>		6034.	17299.					
>	8	6034.	17299.					
>		6034.	17299.					
>	7	6034.	17299.					
>		6034.	17299.					
>		6034.	17299.					
>	6	6034.	17299.					
>		6034.	17299.					
>	5	6034.	17299.					
>		6034.	17299.					
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>		6034.	17299.					
>	3	6034.	17299.					
>		6034.	17299.					
>	1	6034.	17299.					
#	T=2.479	DR=0	\$4.22,				\$4.24T	

A P P E N D I X V

DUKE PIT CONDENSED COORDINATE

LISTING

OUTCROP AND DRILLHOLE DATA

#Invalid MTS command  
#T=0, DR=0 S.05, S.11T  
>#>DRAW LISTING

>>PETRO-CAN DUKE PIT, DEC. 9, 1983

>>DOMAIN MAP

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444	442	110	11
445	442	110	11
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451	442	110	11
452	442	110	11
453	442	110	11
454	442	110	11
455	442	110	11
456	442	110	11
457	442	110	11
458	442	110	11
459	442	110	11
460	442	110	11
461	442	110	11
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463	442	110	11
464	442	110	11
465	442	110	11
466	442	110	11
467	442	110	11
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469	442	110	11
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471	442	110	11
472	442	110	11
473	442	110	11
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475	442	110	11
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477	442	110	11
478	442	110	11
479	442	110	11
480	442	110	11
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482	442	110	11
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492	442	110	11
493	442	110	11
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495	442	110	11
496	442	110	11
497	442	110	11
498	442	110	11
499	442	110	11
500	442	110	11



>DRAW LISTING

>PETRO-CAN DUKE PIT, DEC. 9, 1983

>DOMAIN MAP

ID	COORDINATES			ORIENTATION	HRZN
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53	3851.	15822.	1216.	BORE	
57	4814.	15549.	1074.	BORE	
58	4498.	15646.	1120.	BORE	
101	4333.	15637.	1147.	BORE	
102	4290.	15712.	1151.	BORE	
103	4276.	15744.	1151.	BORE	
104	4255.	15773.	1150.	BORE	
105	4309.	15687.	1149.	BORE	
112	5038.	16571.	1010.	BORE	
115	3969.	14474.	1373.	BORE	
121	5031.	16566.	1012.	BORE	
152	5183.	15985.	1021.	BORE	
153	4837.	16475.	1022.	BORE	
154	4288.	15005.	1239.	BORE	
155	4475.	14579.	1246.	BORE	
156	4675.	13995.	1302.	BORE	
162	5457.	16497.	1004.	BORE	
163	4320.	13485.	1440.	BORE	
173	4975.	14488.	1194.	BORE	
174	5031.	16566.	1012.	BORE	
214	4346.	14260.	1310.	BORE	
215	4274.	14267.	1321.	BORE	
216	4501.	14317.	1273.	BORE	
217	4469.	14284.	1279.	BORE	
218	4637.	14322.	1243.	BORE	
219	4554.	14364.	1257.	BORE	
220	4526.	14342.	1266.	BORE	
221	4703.	14389.	1224.	BORE	
222	4773.	16056.	1038.	BORE	
225	5621.	16022.	1010.	BORE	
225	5136.	15504.	1043.	BORE	
225	5170.	14948.	1121.	BORE	
225	4951.	13403.	1417.	BORE	
226	5653.	17371.	965.	BORE	
226	4612.	15230.	1136.	BORE	
227	4352.	14928.	1243.	BORE	
227	4094.	15100.	1259.	BORE	
227	4849.	16279.	1030.	BORE	
228	5300.	15807.	1016.	BORE	
233	5362.	15741.	1022.	BORE	
233	5058.	16172.	1024.	BORE	
233	5264.	16391.	1007.	BORE	
236	5033.	16987.	1002.	BORE	
236	4215.	15772.	1159.	BORE	
246	4279.	15735.	1152.	BORE	
246	5057.	16169.	1024.	BORE	
246	4216.	15772.	1158.	BORE	
250	4076.	14682.	1399.	BORE	
250	4587.	15896.	1078.	BORE	
260	4062.	16044.	1160.	BORE	
260	4535.	17370.	1020.	BORE	
260	4719.	16915.	1032.	BORE	
261	4064.	16045.	1160.	BORE	
261	4720.	16917.	1032.	BORE	
261	4607.	16469.	1037.	BORE	
262	5242.	16546.	1007.	BORE	
266	5217.	15908.	1020.	BORE	
266	4494.	15655.	1120.	BORE	
266	4504.	15637.	1120.	BORE	
266	4504.	15656.	1120.	BORE	
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A P P E N D I X V I

STATISTICAL PROCEDURES

#### 4.0 THE TRIPOD SOFTWARE PACKAGE

The TRIPOD computer package consists of a main program and a series of sub-routines which are designed to assist the geologist with data handling and processing for interpreting complex, structurally deformed geological terrain.

It is based upon the principle of cylindricity, a basic assumption being that most structures display the property of cylindricity, or that they can be divided into segments that are cylindrical. A cylindrical structure is one that maintains constant geometry along the length of its fold axis.

The package provides the facility to quickly, easily and efficiently retrieve data, process it and then display the results in a fashion that is readily usable by the structural geologist. The data may be displayed in the form of maps, cross-sections, tables or orientation diagrams. A wide variety of outcrop data and drill hole information can be stored, processed and displayed using this package.

#### 5.0 METHODOLOGY

##### 5.1 GENERAL

Structural interpretation studies using the TRIPOD software package require the use of good data, a common sense approach to data handling, knowledge of the statistical techniques used for analyses of data orientation, the ability to use the software and the ability to understand and interpret structural Geology. This system can be effectively utilized in any type of structural terrain because the computer only handles the data in the manner that it is instructed to, the structures interpreted are necessarily a product of the Geologist. The resultant interpretation is effected using greater amounts of data and thus should be more reliable and in greater detail than a comparable study completed without use of this software.

##### 5.2 DATA COLLECTION

###### 5.2.1 Outcrop Data

Field outcrop, trench and adit data should be collected in such a fashion that information is presented on all of the following:

Map Grid - each data point should be located on a chosen map grid such that the location is recorded as a northing, easting and elevation.

Lithologic description - this should contain the map symbol of the rock unit at the point of measurement and may be at a contact or within a unit.

Bedding Orientations - orientations should be recorded as dip direction/dip or right hand strike/dip and measured as degrees, grads, or radians. Normally, degrees are used with dip directions varying from 0° to 359° and dips from 0° to 90° with a special notation for overturned beds. Multiple bedding plane orientations should be collected within a more or less standard outcrop size; the size being dependent upon the detail of the mapping and the scale of structures to be represented. Additional data may be collected if mesoscopic scale structural features are in evidence.

Other Planar Features - if other planar features such as joints and faults are present, they should be measured and recorded in a similar fashion to bedding measurements.

Linear Features - all linear features such as slickenside striae require multiple measurements of their pitch on the surface on which they occur. In addition, notes and a diagram of the structure are very useful.

## 5.2.2 Drill Hole Data

Several types of drill hole information are required:

Collar Location - once again described by grid location and elevation

Drill Hole Deviation - any <sup>number</sup> of deviation measurements can be recorded and entered into the computer file for each drill hole.



Overburden Depth - the overburden depth is recorded to identify bedrock location.

Drill Hole Intersections - any number of intersections can be identified. Many of these units will, however, represent a stratigraphic zone rather than a contact.

Bedding Angles - these are commonly measured as "bedding to core normal" angles and are, at present, hand plotted on the sections. It is planned that this feature will be incorporated into future revisions of the program.

### 5.3 DATA HANDLING

#### 5.3.1 Raw Data Files

The outcrop and the drill hole data are entered into 4 files, of which 2 each are used for outcrop and drill hole data. Generally, mine adit and trench data are considered to be outcrop data and are included in those files.

#### OUTCROP DATA

Outcrop Location File - This file contains the northing, easting and elevation data for each outcrop number.

Outcrop Data File - This file contains the required structural and stratigraphic data for each numbered outcrop.

#### DRILL HOLE DATA

Drill Hole Location File - This file contains the northing, easting, elevation, depth, and deviation data for each drill hole.

Drill Hole Data File - This file contains the drill hole stratigraphic and structural information.

#### 5.3.2 Master Files

The raw data files are read in to the TRIPOD package and the data are then stored in 4 master data files, in an easily retrievable and processable format.

### 5.3.3 Errors

Upon compilation and entry of the basic data, the data base must be checked for errors. This is carried out in several ways:

- (i) Data Listing - A listing of the data files will provide error messages for those types of errors of incorrect data entry; for example, if two outcrops have the same number, if drill hole depth measurements do not continually progress, if drill hole intersection numbers are not sequentially numbered, if an orientation direction of 360° is used, and if a dip measurement is >90°. If the data format is violated, an error message also occurs.
- (ii) Map Review - Outcrop and drill hole maps are printed and generally checked for obvious errors.
- (iii) Drill Holes - Drill holes are called up on the graphics terminal for each domain and viewed for completeness and correctness of data.

### 5.3.4 Data Handling on Computer

After the data files are created, the data can be recalled based upon:

- outcrop number
- drill hole number
- stratigraphic code
- type of orientation data
- an area outlined by a polygon

Commonly all of the outcrop data and/or drill hole data will be retrieved for a specified area (polygon), for example, a possible domain area. In addition, outcrop data can be restricted by type of orientation data, and/or by outcrop numbers. Recalled data within a domain may be projected parallel to the fold axis onto selected planes of profile which are used as the basis for cross-sections. Typically, all of the data within the domain are utilized. Composite sections may be prepared by projecting all of the data from several domains onto a composite line of section.

Some project areas have insufficient outcrop data to permit determination of domain boundaries and fold axis orientations, and some project areas consist of a large planar feature with an undeterminable fold axis orientation. On projects with these problems, the data from slices of selected widths can be projected onto lines of section. In such cases, the direction and angle of projection must be estimated and then checked against other projection directions with the use of interactive graphics. This technique is utilized on outcrop and drillhole data when difficulties are encountered during initial domain definition. These difficulties arise from 2 sources:

- (a) poor identification of the stratigraphic horizons at each outcrop resulting in spurious stratigraphic codes being plotted on the profiles, and
- (b) poor quality outcrop data

#### 5.4 DOMAINS

Structural analysis and data handling must first be carried out on a domain by domain basis. The first step after data entry and proofing is to prepare a surface geological map with outcrops and all the structural and stratigraphic information, and then divide the map area into potential domains within which, by inspection, folding appears to be cylindrical. If folds cannot be identified the area should be divided into planar segments within which bedding appears to be of fairly constant orientation.

Upon selection of the domain boundaries, the outcrop data in each domain must be analyzed to determine whether or not the structure is cylindrical, and the fold axis orientation is calculated. Both of these functions are carried out by computer. The fold axis orientation provides:

- (i) a quantitative description of folding, and
- (ii) the trend and plunge to be used in preparing down-plunge projections

The Domain analysis involves determining whether a structure is cylindrical or not. A series of statistical tests and the geologist's judgement are the determining factors employed in order to test and accept or reject the hypothesis of cylindricity.

## 5.5 CYLINDRICITY

5.5.1 Defined: A cylindrical fold is a fold that maintains similar shape along the trend of the fold axis. In such a case, all of the bedding poles lie in a plane normal to the fold axis. All data within this cylindrically folded area may be projected parallel to the fold axis onto a plane placed at any location and orientation within the "cylindrical" domain.

### 5.5.2 Testing Cylindricity

Several tests are used to determine whether or not a structure is cylindrical. In order to perform these tests however, the fold axis orientation must be calculated numerically and a number of associated statistics must be determined. The minimum eigen vector associated with a symmetric  $3 \times 3$  matrix of summations of direction cosine products gives the fold axis orientation only if the folding is cylindrical. Therefore, the structural data must be viewed with the intent of delineating areas where the deformation can be considered cylindrical.

#### 5.5.2.1 Eigen Values

In an ideal cylindrical fold, there is no scatter of bedding poles about the plane normal to the fold axis and the minimum eigen value ( $\lambda_3$ ) is 0. When using real data some departure from this ideal situation can be expected and would be due to:

- (a) measurement errors
- (b) incongruent small-scale folds
- (c) bedding plane roughness.

In addition, a cylindrical fold should also display a wide spread of bedding poles within the plane normal to the fold axis orientation. A uniform distribution would result in the maximum eigen value ( $\lambda_1$ ) and the intermediate eigen value ( $\lambda_2$ ) being equal.

In marked contrast to this, the orientations associated with homoclinal strata would result in  $\lambda_1$  being very large and both  $\lambda_2$  and  $\lambda_3$  being very small and approaching 0 (Cruden, 1968, Charlesworth et al, 1976).

The minimum eigen value ( $\lambda_3$ ) is equal to  $\frac{1}{n} \sum \cos^2 \phi_i$  where  $\phi_i$  is the angle between the fold axis and the  $i$ th of  $n$  poles to bedding. Therefore the variance and standard deviation of  $\cos \phi_i$  are given by  $\lambda_3/n$  and  $\sqrt{\lambda_3/n}$ , respectively.

#### 5.5.2.2 Standard Scattering Angle

The standard scattering angle is another measure of scatter about the plane normal to the fold axis and is given by the arcsine of the standard deviation mentioned above.

#### 5.5.2.3 Chi-Square Test

One method used to determine how much deviation from the ideal situation may be allowed in a "cylindrical" fold uses a chi-square test to compare the variance at the outcrop scale, measured by the pooled estimate  $K$  of the concentration parameters of the repeated measurements at the outcrops with the variance in the whole area ( $\lambda_3$ ). The hypothesis of cylindricity is rejected if  $K \times \lambda_3$  is greater than the appropriate chi-square value (Charlesworth et al, 1976).

#### 5.5.2.4 F-Test

The F-test compares the variance in the area as a whole with that in two halves of the area. Firstly the variance in the 2 halves of the domain must be roughly equal, and secondly the minimum eigenvalue ( $\lambda_3$ ) in the whole area cannot be significantly greater than the sum of  $\lambda_3$  for the two halves (Charlesworth et al, 1976).

#### 5.5.2.5. Cylindricity

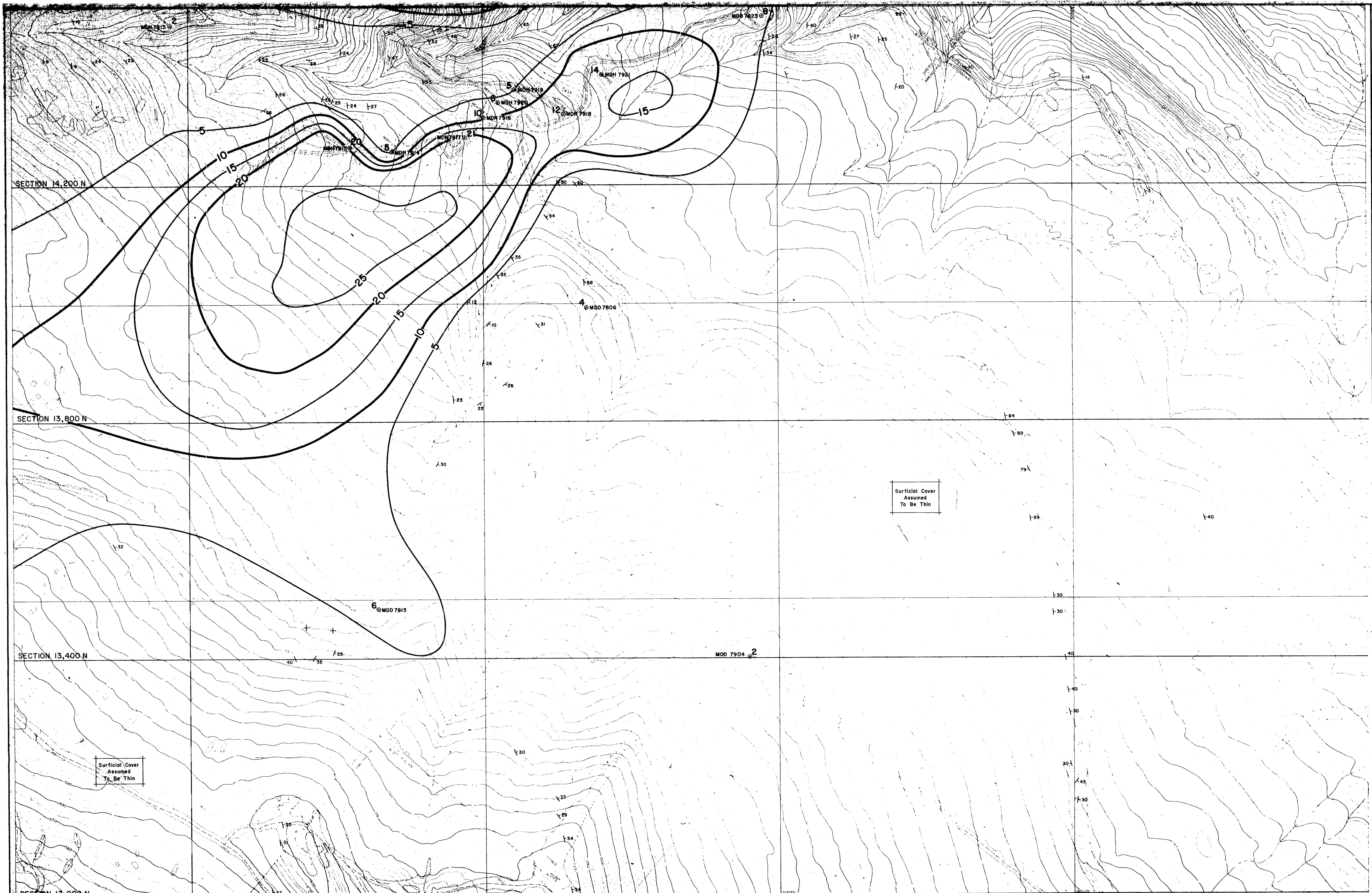
In general, cylindricity can be assumed when:

- (i)  $\lambda_2$  is less than an order of magnitude smaller than  $\lambda_1$  and more than an order of magnitude larger than  $\lambda_3$ .
- (ii) the standard scattering angle is small.
- (iii)  $k$  (precision parameter) times  $\lambda_3$  (minimum eigenvalue) is less than the appropriate chi-square value from the critical values of the chi-square distribution table, and
- (iv) the F-Test, which compares the variance from the 2 halves of the domain is satisfied.
- (v)  $\lambda_3$  of a domain is not significantly greater than sum of  $\lambda_3$  for each half of the domain.

#### 5.6 DOMAIN PROFILE PLOTS

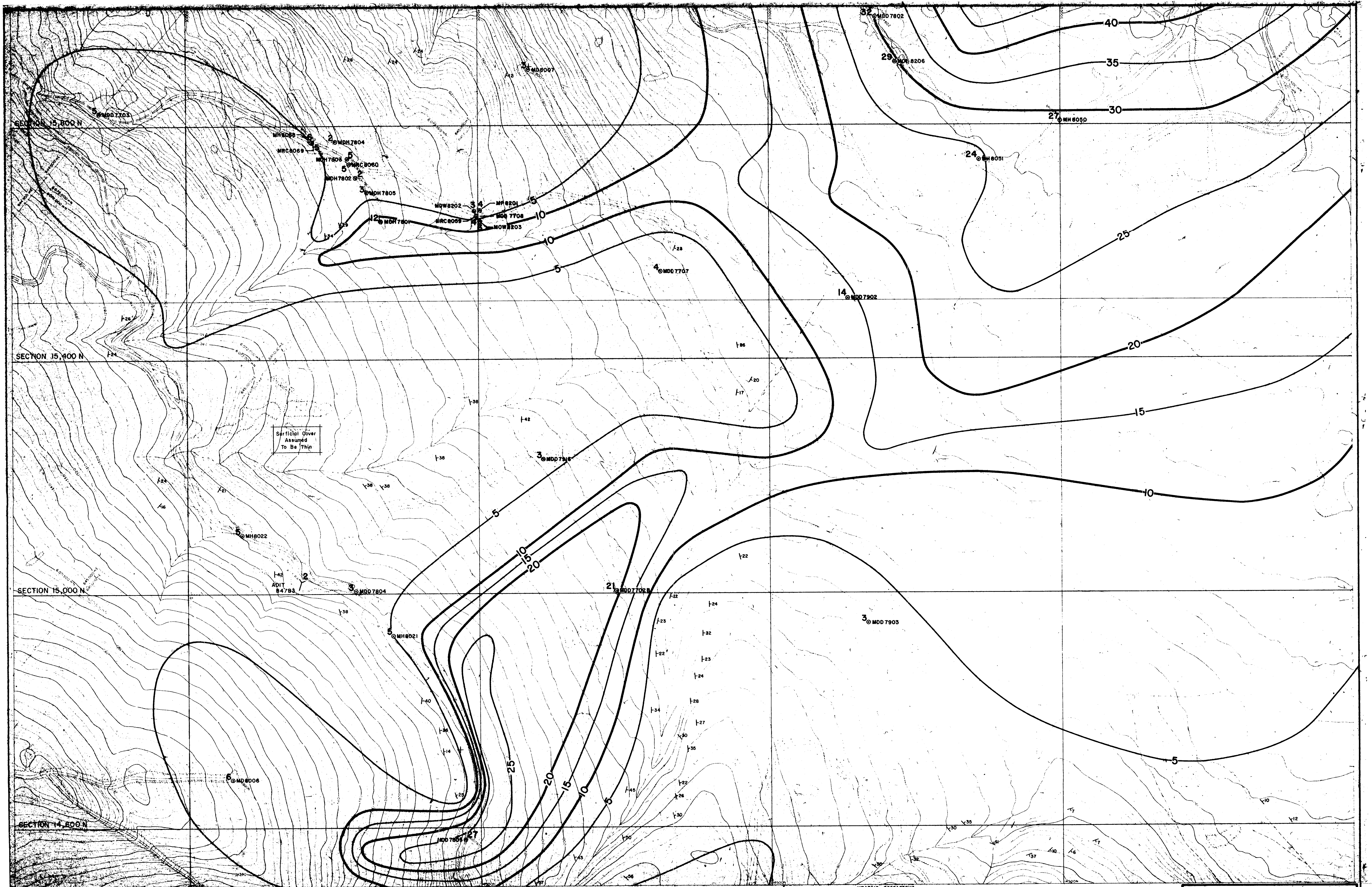
Upon completion of domain selection and receipt of positive proof that the domain is cylindrical, a line of section is chosen. This section can be oriented in any direction except parallel to the fold axis but is usually at 90° to the fold axis. In many cases, however, vertical profiles that are perpendicular to the regional strike are drawn. These section plots will contain all outcrop and drill hole data within the specified domain.





<b>LEGEND</b> Road: --- Track or trail: - - - Dike line: - - - Building: [ ] Pond: [ ] Irrigated channel: [ ] Contour: [ ] Depression contour: [ ] Spot elevation: [ ]		<b>SCALE 1:2000</b> 0 100 200 300 metres <b>CONTOUR INTERVAL 2m (5m under heavy tree cover)</b> <b>DATE OF PHOTOGRAPHY 1980</b> <b>SURVEY NOTE</b> The horizontal and vertical coordinates were established by Donald E. ... The contours and elevations were derived from the ... All spot elevations were taken on ground points and all coordinates refer to ...		<b>ALLOGEOLOGICAL LEGEND</b> COAL SEAM SUBCROP GEOLOGICAL BOUNDARY THRUST FAULT - UPPER TRACE THRUST FAULT - LOWER TRACE SYNCLINAL, ANTICLINAL AXIS DIP & STRIKE (Dipping, Vert., Horiz.)		<b>MEIOGEOLOGICAL LEGEND</b> DRILL HOLE LOCATION TRENCH LOCATION ADIT LOCATION CONGLOMERATE SANDSTONE SILTSTONE MUDSTONE COAL		<b>LOWER CRETACEOUS</b> K1a SHAYESBURT FM. K1b ROULDER CREEK FM. K1c HULCROSS FM. K1d GATES FM. K1e MOOSEBAR FM. († Torrens Member) K1f OETHING FM. K1g CADOMN FM.		<b>JURASSIC - CRETACEOUS</b> J1a MINNES GROUP (undivided) <b>PALEOZOIC</b> P1 DEVONIAN, MISSISSIPPIAN		<b>MINNES GROUP</b> FORT ST. JOHN GROUP BULLHEAD GROUP		<b>ISOPACH CONTOURS</b> 20 15 10 NOTE: ISOPACHS AND THICKNESSES ARE IN METRES		<b>PETRO-CANADA RESOURCES</b> <b>DUKE PIT ISOPACH OF SURFICIAL COVER</b> <b>SOUTH SHEET</b> DRAWN BY: BS CHECKED: L.A.S. DATE: 83/12 COMPILED BY: L.A.S./C.B.N. CLIENT APPL.: SCALE: HORIZ. 1:2 000 VERT.: PROJ. NO.: MAP 3a FILE NO.: L.A.S. CONSULTING & DEVELOPMENT LTD.	
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**LEGEND**

Scale: 1:2000  
 Contour Interval: 2m (5m under heavy tree cover)  
 Date of Photography: 1980

**SURVEY NOTE**  
 The topographic and geological information was obtained by DuPont & ...  
 ...  
 ...

**LYONBROOK LEGEND**

- COAL SEAM SUBCROP
- GEOLOGICAL BOUNDARY
- THRUST FAULT - UPPER TRACE
- THRUST FAULT - LOWER TRACE
- SYNCLINAL ANTICLINAL AXIS
- DIP & STRIKE (Dipping, Vert., Horiz.)
- DRILL HOLE LOCATION
- TRENCH LOCATION
- ADIT LOCATION
- CONGLOMERATE
- SANDSTONE
- SILTSTONE
- MUDSTONE
- COAL

**LOWER CRETACEOUS**

- SHA/RESOURCY FM.
- BOULDER CREEK FM.
- HARROSS FM.
- GATES FM.
- MOOSEBAR FM. (1 - Terrain Marker)
- GETHENS FM.
- CAPORN FM.

**JURASSIC - CRETACEOUS**

- MINNES GROUP (undivided)

**PALEOZOIC**

- DEVONIAN, MISSISSIPPIAN

**PORT ST. JOHN GROUP**

**ISOPACH CONTOURS**

NOTE: ISOPACHS AND THICKNESSES ARE IN METRES

**PETRO-CANADA RESOURCES**

**DUKE PIT ISOPACH OF SURFICIAL COVER**

CENTRE SHEET

DATE: 83/12

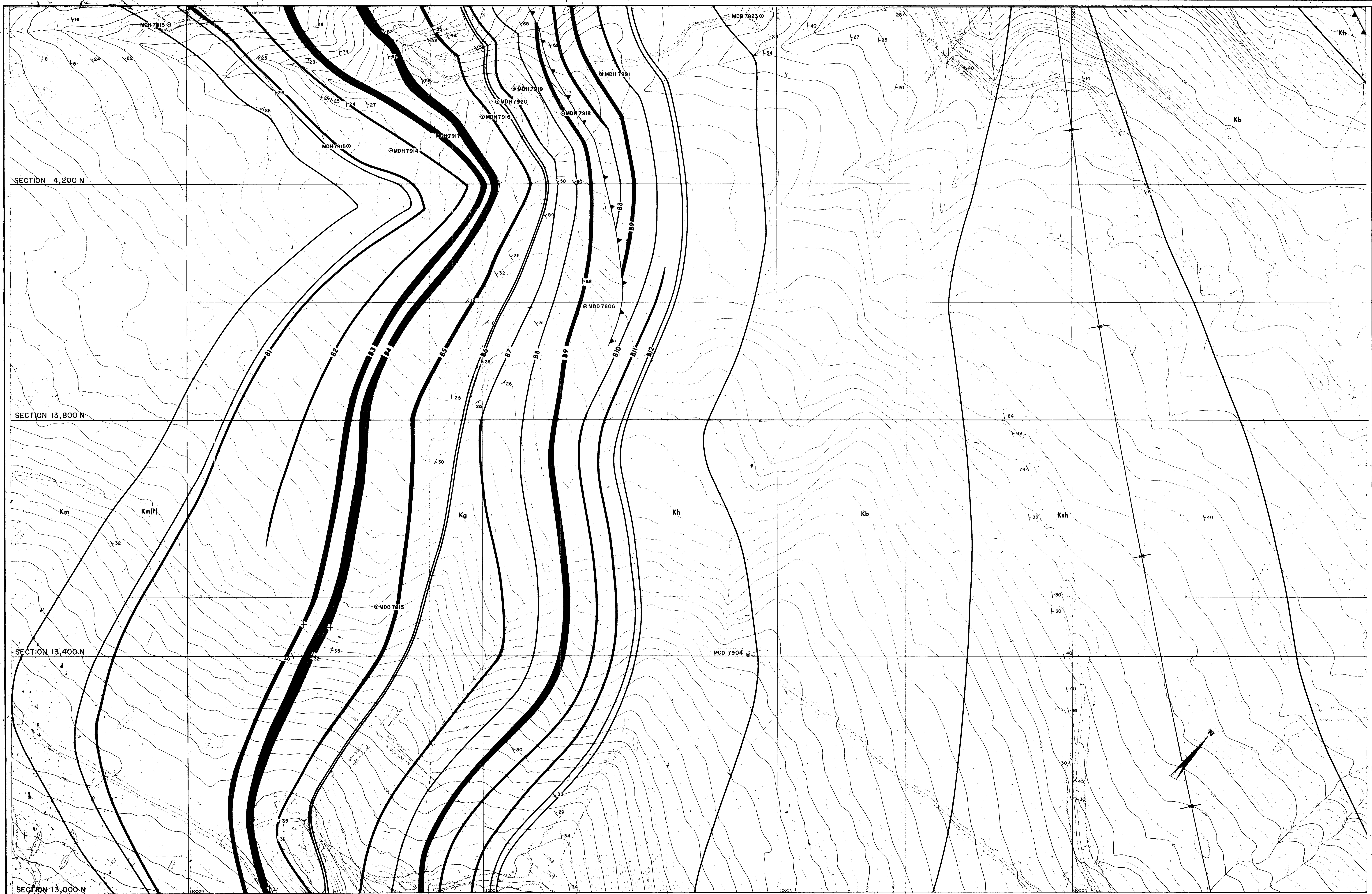
SCALE: 1:2000

FILE NO.









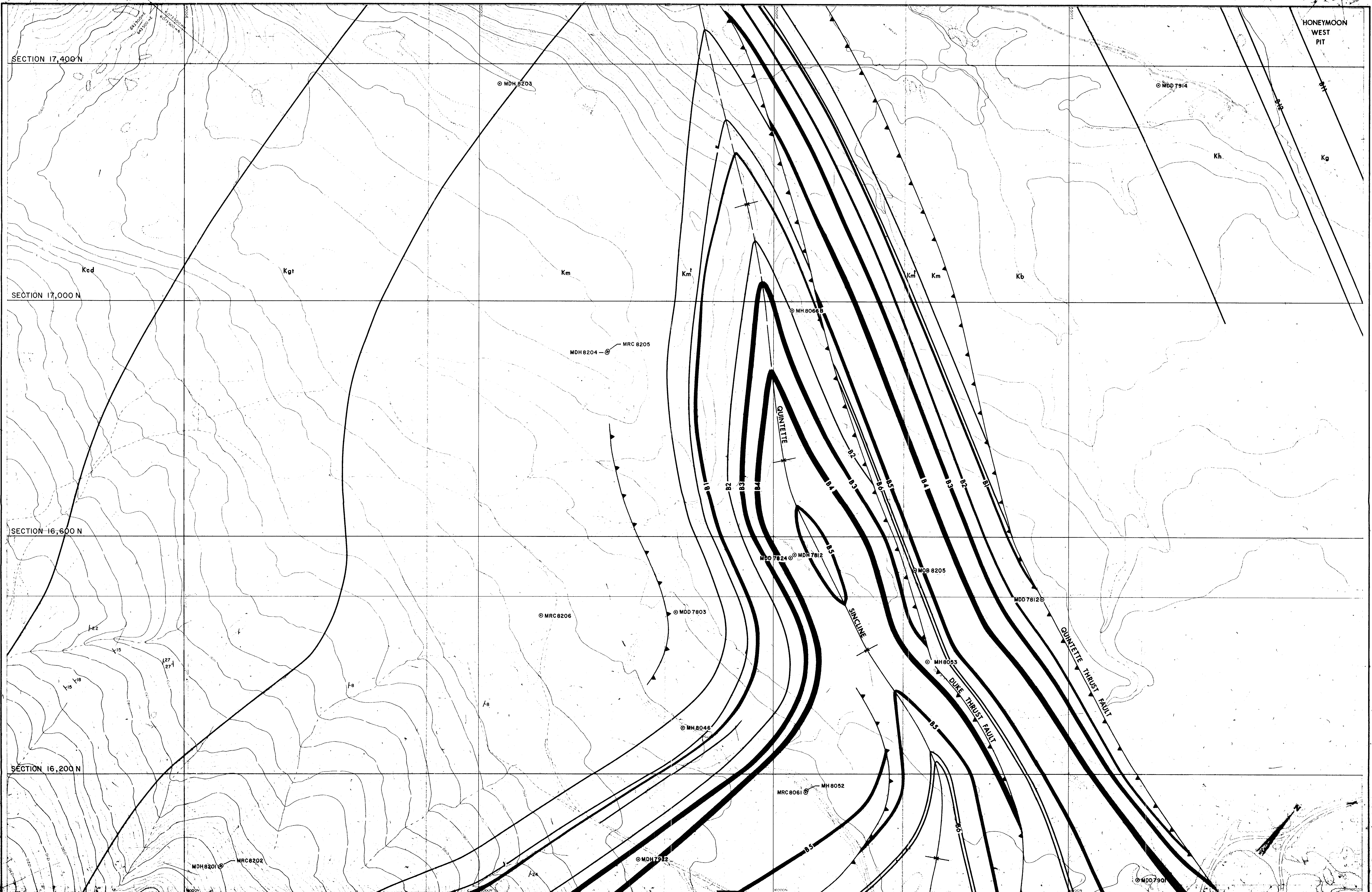
<b>LEGEND</b> River Stream Lake Swamp Building Fence Vertical control Horizontal control Drill hole		<b>SCALE 1:2000</b> 0 100 200 300 metres <b>CONTOUR INTERVAL 2m (5m under heavy tree cover)</b> DATE OF PHOTOGRAPHY 1980 <b>SURVEY NOTE</b> The horizontal and vertical coordinates were established by Donald E. Wilson Survey Ltd., Horizon Energy, Marine and Associates Ltd., and Petro-Canada. The coordinates and elevations were obtained from the long traverse E. Cluette St. Marie, Hwy. 401, and Kincardine. All vertical values were based on geoid datum and all coordinates refer to the Universal Transverse Mercator Grid Zone 18.		<b>LITHOLOGICAL LEGEND</b> B1 COAL SEAM SUBCROP B2 GEOLOGICAL BOUNDARY B3 THRUST FAULT - UPPER TRACE THRUST FAULT - LOWER TRACE SYNCLINAL, ANTICLINAL AXIS DIP & STRIKE (Dipping, Vert., Horiz.)		<b>DRILL HOLE LOCATION</b> TRENCH LOCATION ADIT LOCATION CONGLOMERATE SANDSTONE SILTSTONE MUDSTONE COAL		<b>GEOLOGICAL LEGEND</b> LOWER CRETACEOUS Ksh SHAFRESBURY FM. Kb BOULDER CREEK FM. Kh HULCROSS FM. Kg GATES FM. Km MOOSEBAR FM. (Torrus Member) Kst OETHING FM. Kcd CADDON FM.		JURASSIC - CRETACEOUS Kmi MINNES GROUP (undivided) PALEOZOIC F DEVONIAN, MISSISSIPPIAN PORT ST. JOHN GROUP BULLHEAD GROUP		<b>MINNES GROUP</b> MINNES GROUP		<b>PETRO-CANADA RESOURCES</b> <b>DUKE PIT</b> SUBCROP GEOLOGY MAP SOUTH SHEET DRAWN BY: B.B. CHECKED: C.A.S. DATE: 05/12 COMPILED BY: L.A.S./C.S.W. CLIENT APPL: DWG. NO. MAP 6a SCALE: HORIZ. 1:2000 VERT. 1:2000 FILE NO. I.A. SMITH CONSULTING & DEVELOPMENT LTD.	
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<p><b>Legend</b></p> <p>Scale 1:2000</p> <p>CONTOUR INTERVAL 2m (5m under heavy tree cover) DATE OF PHOTOGRAPHY 1980</p> <p><b>SURVEY NOTE</b> The horizontal and vertical coordinates were established by Dennis E. Heston, Survey, Ltd., located, 1979. The map was compiled by the same firm. The horizontal coordinates were based on specific data and all coordinates refer to the Universal Transverse Mercator Grid Zone 18.</p>		<p><b>LOWER CRETACEOUS</b></p> <ul style="list-style-type: none"> <li>Sh Shafsbury fm.</li> <li>Bs Boulder Creek fm.</li> <li>Mc McCross fm.</li> <li>Gg Gates sq.</li> <li>Mo Moosbar fm. (+ Torrens Member)</li> <li>Ge Gething fm.</li> <li>Cd Cadomin fm.</li> </ul>	<p><b>JURASSIC-CRETACEOUS</b></p> <ul style="list-style-type: none"> <li>Mn Minnes Group (undivided)</li> <li>Dev Devonian, Mississippian</li> </ul>	<p><b>PALEOZOIC</b></p> <ul style="list-style-type: none"> <li>Fort St. John Group</li> <li>Bullhead Group</li> </ul>	<p><b>SYMBOLS</b></p> <ul style="list-style-type: none"> <li>○ DRILL HOLE LOCATION</li> <li>— TRENCH LOCATION</li> <li>— ADIT LOCATION</li> <li>— CONGLOMERATE</li> <li>— SANDSTONE</li> <li>— SILTSTONE</li> <li>— MUDSTONE</li> <li>— COAL</li> </ul>	<p><b>SYMBOLS</b></p> <ul style="list-style-type: none"> <li>— COAL SEAM SUBCROP</li> <li>— GEOLOGICAL BOUNDARY</li> <li>— THRUST FAULT - UPPER TRACE</li> <li>— THRUST FAULT - LOWER TRACE</li> <li>— SYNCLINAL ANTICLINAL AXIS</li> <li>— DIP &amp; STRIKE (Dipping Vert., Horiz.)</li> </ul>
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**PETRO-CANADA RESOURCES**

**DUKE PIT**  
SUBCROP GEOLOGY MAP

NORTH SHEET: [ ]

DATE: 8/15

FILE NO. [ ]





**LEGEND**

--- COAL SEAM SUBCROP  
 --- GEOLOGICAL BOUNDARY  
 --- THRUST FAULT - UPPER TRACE  
 --- THRUST FAULT - LOWER TRACE  
 --- SYNCLINAL, ANTICLINAL AXIS  
 --- DIP & STRIKE (Dipping, Vert., Horiz.)

**SCALE METRES**

0 100 200 300 400

**CONTOUR INTERVAL 2m (5m under heavy tree cover)**  
DATE OF PHOTOGRAPHY 1992

**SURVEY NOTE**  
This document and the data herein are the property of Petro-Canada Resources Ltd. and are not to be used for any other purpose without the written consent of Petro-Canada Resources Ltd. and the author. The author is not responsible for any errors or omissions in this document.

**LITHOLOGICAL LEGEND**

● DRILL HOLE LOCATION  
 ○ TRENCH LOCATION  
 ○ ADIT LOCATION  
 ■ CONGLOMERATE  
 ■ SANDSTONE  
 ■ SILTSTONE  
 ■ MUDSTONE  
 ■ COAL

**GEOLOGICAL LEGEND**

**LOWER CRETACEOUS**  
 Shattesbury FM.  
 Commonion FM. (Builder Creek Member)  
 Commonion FM. (Hudson Member)  
 Commonion FM. (Gates Member)  
 Moorebar FM. (Lower)  
 Gething FM.  
 Cadomin FM.

**JURASSIC - CRETACEOUS**  
 Fort St. John Group  
**PALEOZOIC**  
 Devonian, Mississippian  
 Minnes Group

NOTE: CONTOUR INTERVAL 15 METRES

**PETRO-CANADA RESOURCES**

**DUKE PIT**

STRUCTURE CONTOUR MAP  
BASE OF B1 SEAM

CENTER SHEET

DRAWN BY: L.A.S./C.S.M. DATE: 05/12  
 CHECKED BY: L.A.S./C.S.M. DATE: 05/12  
 COMPILED BY: L.A.S./C.S.M. DATE: 05/12  
 SCALE: 1:1000 MAP 78  
 FILE NO.

L.A.S. CONSULTING & DEVELOPMENT LTD.



SECTION 17,000 N

SECTION 16,000 N

SECTION 15,000 N

SECTION 14,000 N

SECTION 13,000 N

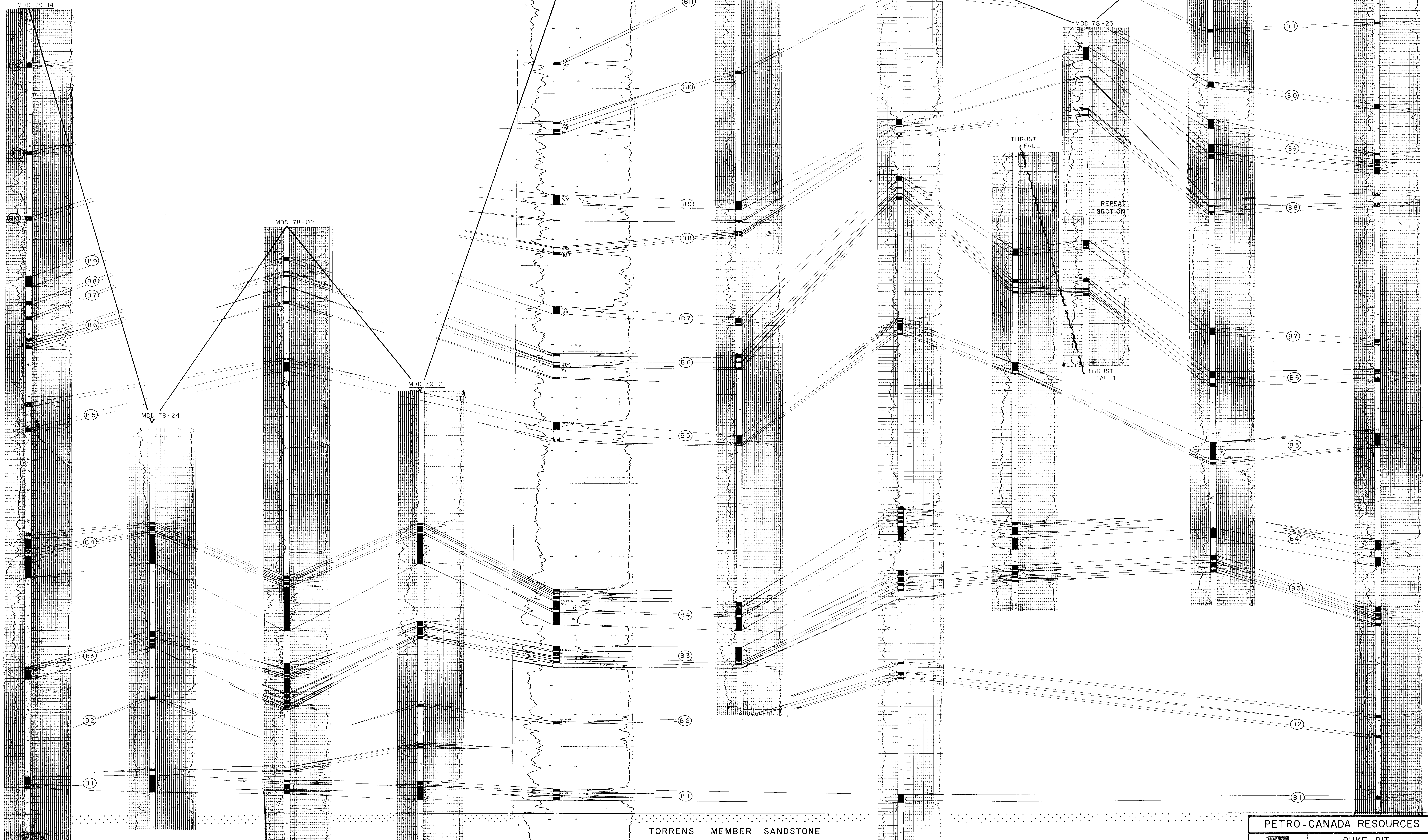
East West

West East

West East

West East

West East



TORRENS MEMBER SANDSTONE

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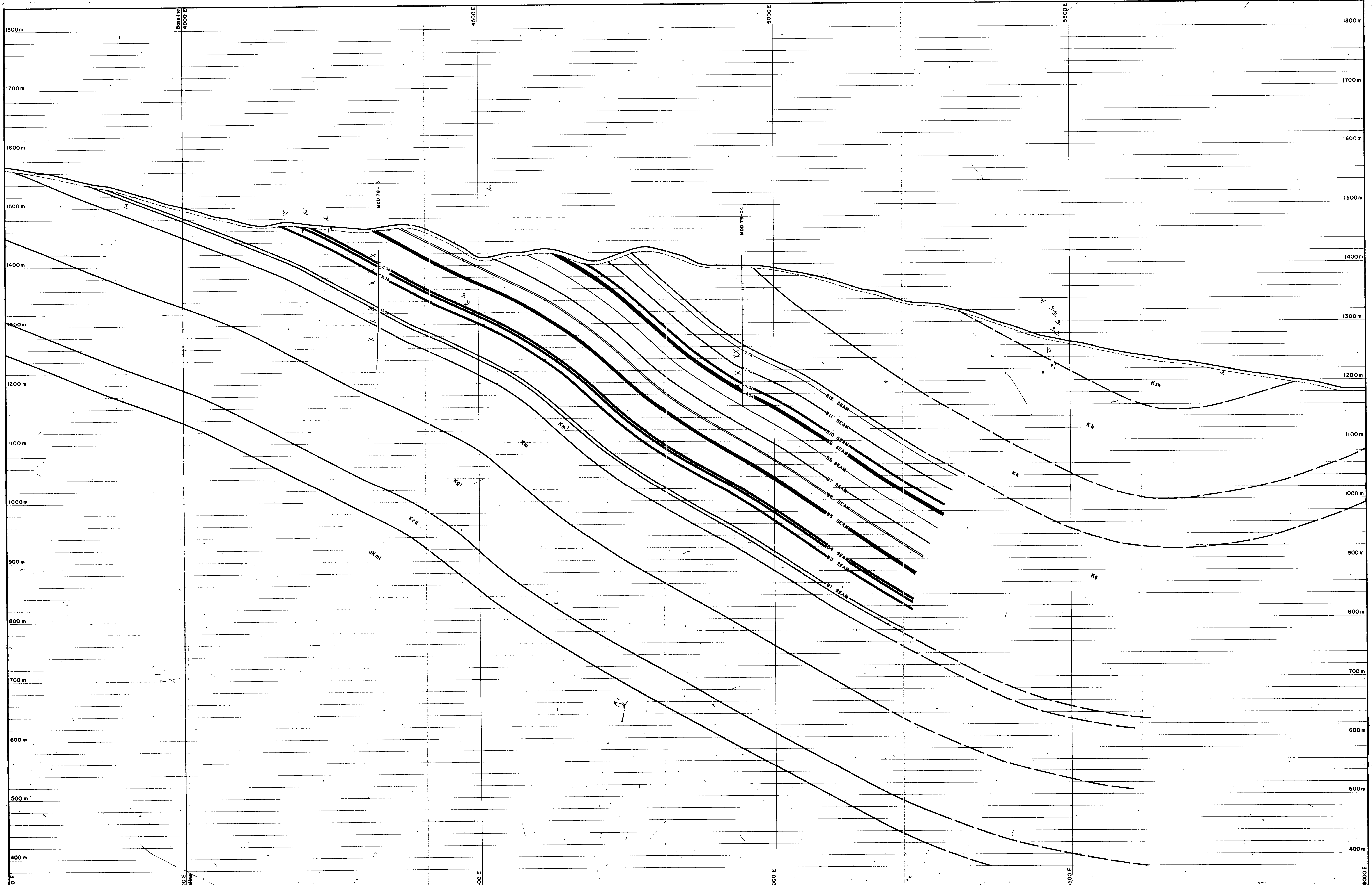
PETRO-CANADA RESOURCES

DUKE PIT  
GATES COAL SEAMS  
CORRELATION CHART

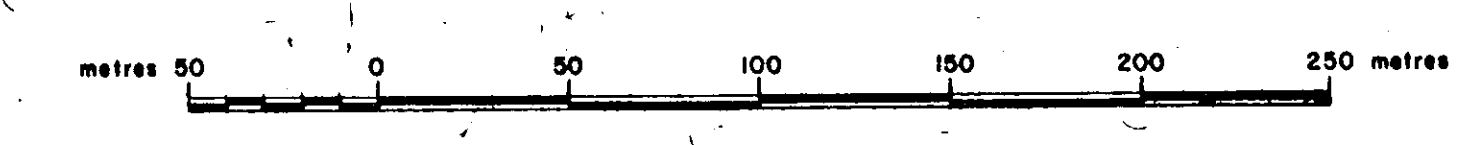
DRAWN BY: B.S.	CHECKED: A.S.	DATE: 8/7/11
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SCALE: HORIZ. 1" = 100'	VERT. 1" = 100'	FILE NO.

LAS L.A. SMITH CONSULTING & DEVELOPMENT LTD.





LOWER CRETACEOUS		JURASSIC - CRETACEOUS	
K1h	SHAFERSBURG FM.	K1m	MINNES GROUP (undivided)
K1b	BOULDER CREEK FM.	PALEOZOIC	
K1a	HULCROSS FM.	K1d	DEVONIAN, MISSISSIPPIAN
K0g	DATES FM.	FORT ST. JOHN GROUP	
K0m	MOOSEBAR F.M. (1st Torrens Member)	BULLHEAD GROUP	
K0t	GETHING FM.		
K0d	CADOMH FM.		

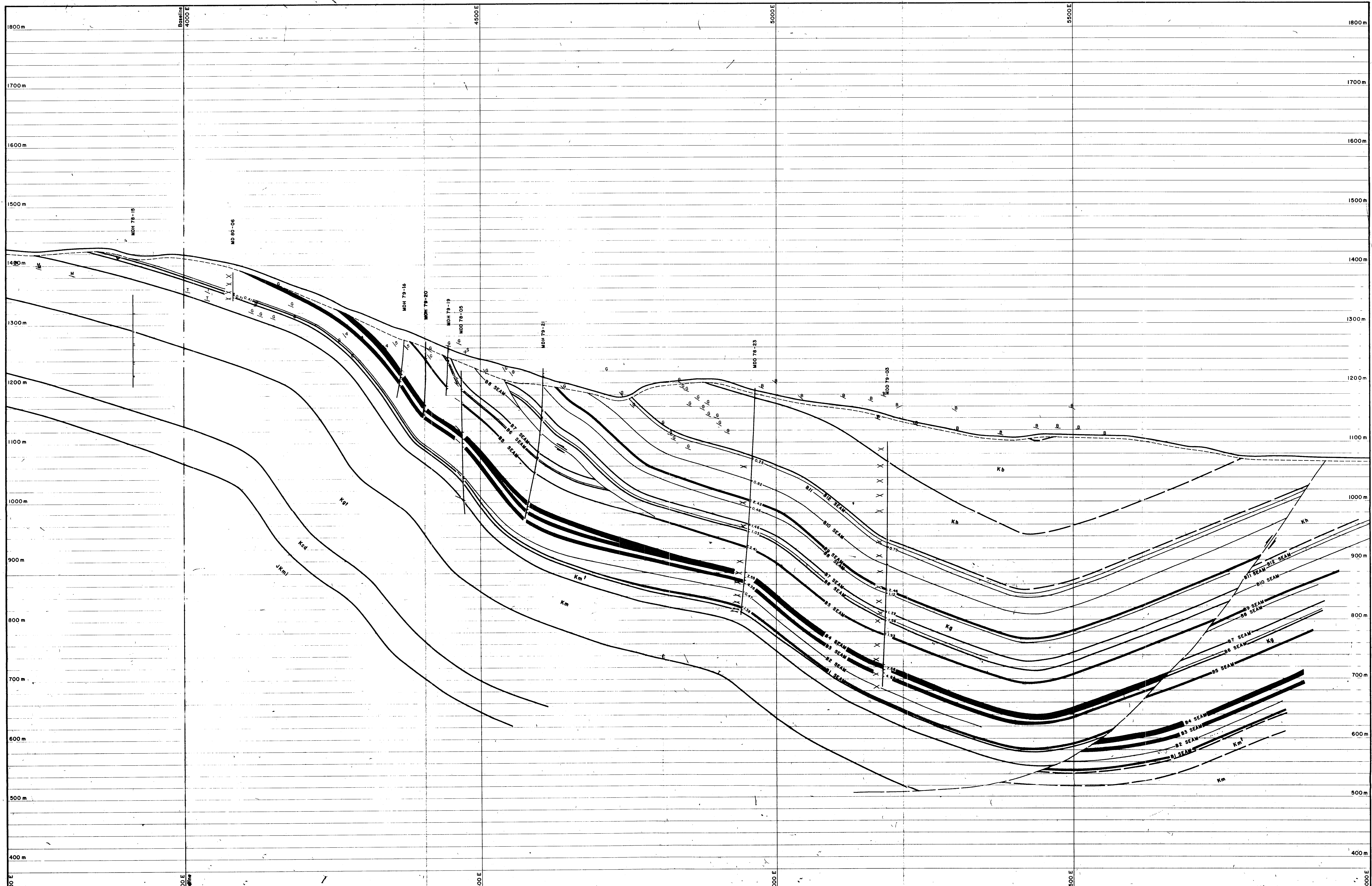


**PETRO-CANADA RESOURCES**  
**DUKE PIT**  
**SECTION 13,400N**

Drawn by: C.A.V./L.A.S.	Checked: J.A.S.	DATE: 02/11
Scale: 1:10,000	Scale: 1:10,000	Scale: 1:10,000
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L.S. L.A. SMITH CONSULTING & DEVELOPMENT INC.

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**GEOLOGICAL LEGEND**

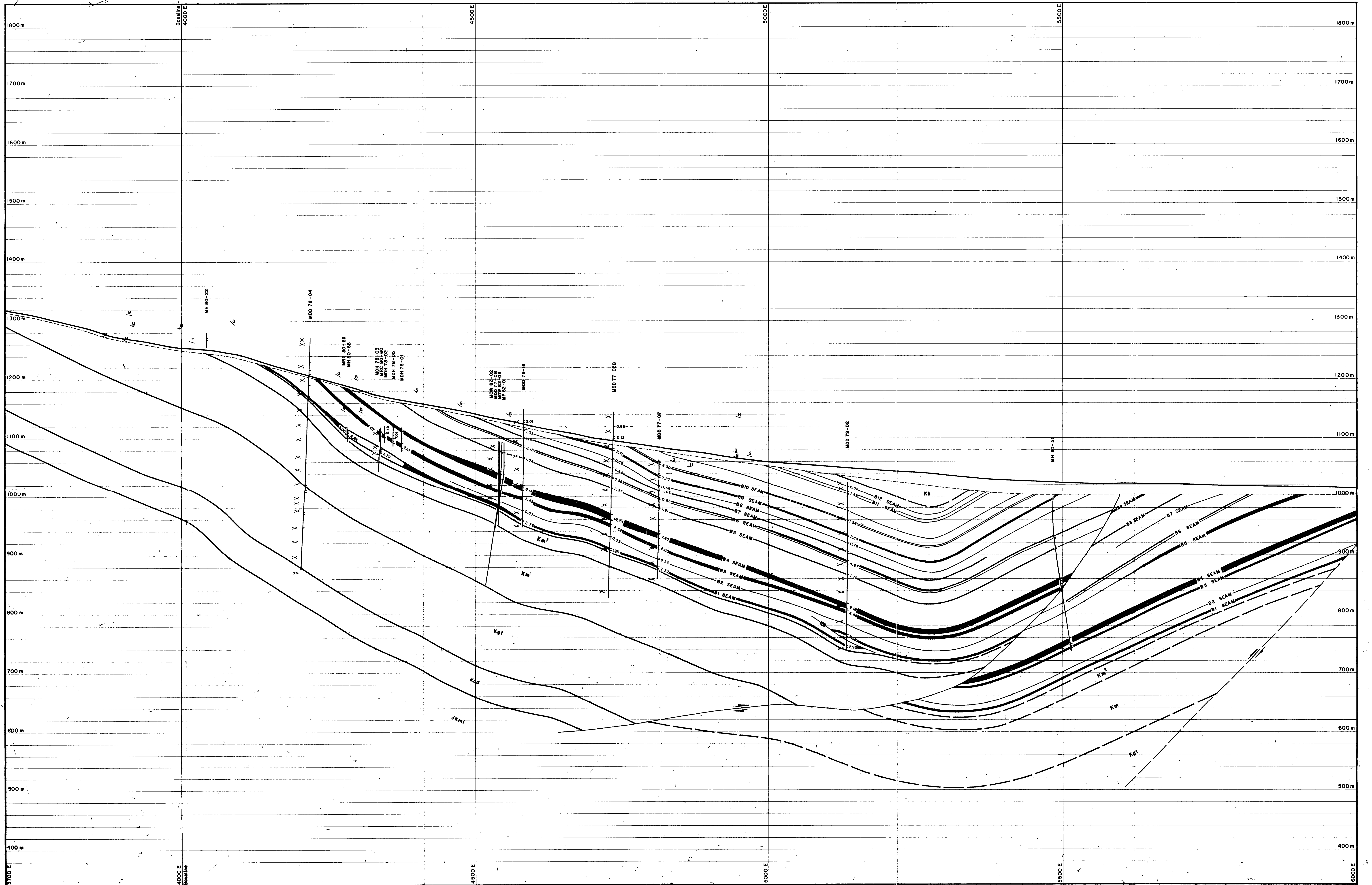
<b>LOWER CRETACEOUS</b>	<b>JURASSIC - CRETACEOUS</b>	<b>MINNESOTA GROUP</b>
Kb SHAFERBURT FM.	Jkm1 MINNESOTA GROUP (undivided)	Km MINNESOTA GROUP
Kd BOUNDER CREEK FM.	<b>PALEOZOIC</b>	
Kp HULCROSS FM.	Fort St. John Group	
Kq GATES FM.	Devonian, Mississippian	
Km1 MOOSEBAR FM. (1 + Torran Member)		
Kf GETTING FM.		
Kg CADOMIN FM.		
	<b>BULLHEAD GROUP</b>	

**PETRO-CANADA RESOURCES**  
**DUKE PIT**  
**SECTION 14,600 N**

Drawn by: [ ] Checked: L.A.S. Date: 02/11  
 Compiled by: C.W./L.A.S. Drawn by: [ ]  
 Scale: HORIZ. 1:12,000 VERT. 1:12,000  
 L.A.S. CONSULTING & DEVELOPMENT LTD. FILE NO. [ ]

503





**LOWER CRETACEOUS**

Kah	SHAFTESBURY FM.
Kb	BOULDER CREEK FM.
Kh	HULCROSS FM.
Kg	GATES FM.
Km	MOOSEBAR FM. (± Torrens Member)
Kgl	GETHING FM.
Kcd	CADOMIN FM.

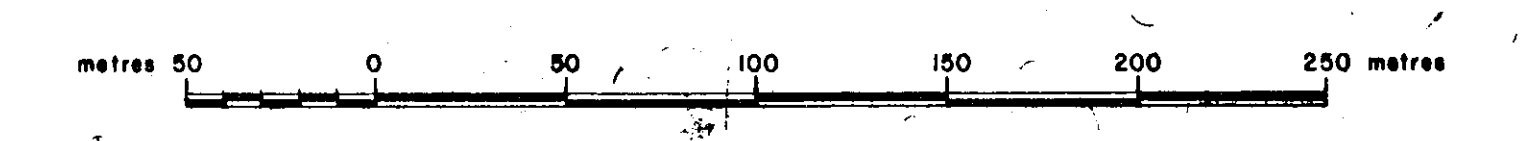
**JURASSIC - CRETACEOUS**

JKml	MINNIS GROUP (undivided)
Kf	DEVONIAN, MISSISSIPPIAN

**FORT ST. JOHN GROUP**

**BULLHEAD GROUP**

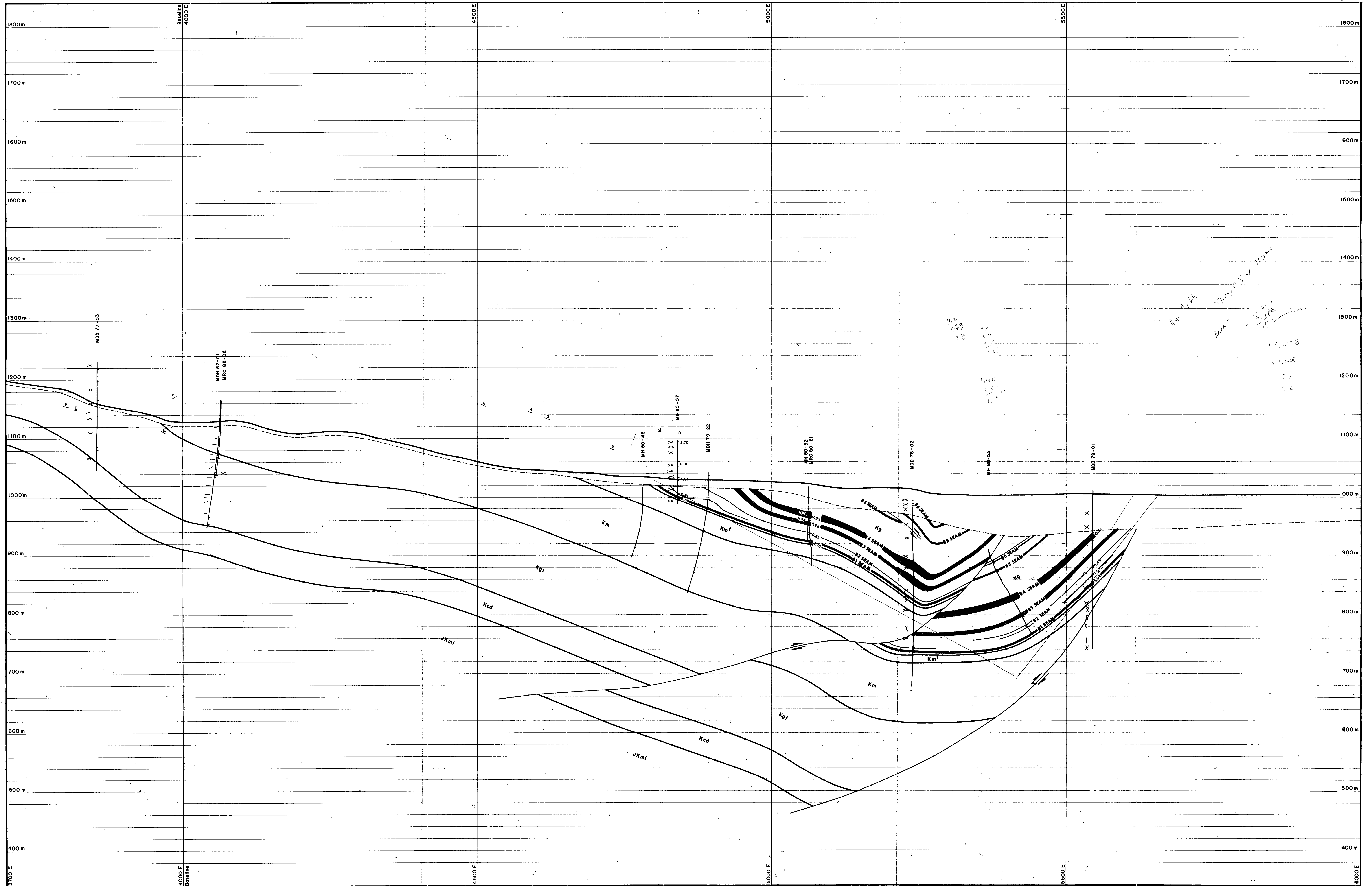
**MINNIS GROUP**



**PETRO-CANADA RESOURCES**  
**DUKE PIT**  
**SECTION 15,400 N**

DESIGNED BY: C. W. / L.A.S.	CHECKED: L.A.S.	DATE: 02/11
COMPILED BY: C. W. / L.A.S.	GEOPLOTTER: C.W.	DWG. NO.
SCALE: HORIZ. 1:12,000	VERT. 1:2,000	FILE NO.

L.A.S. CONSULTING & DEVELOPMENT LTD.



Handwritten notes and calculations:

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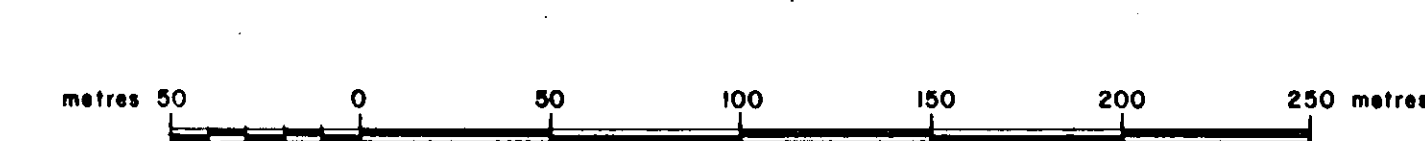
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**GEOLOGICAL LEGEND**

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Km	BOULDER CREEK FM.	Km	MINNES GROUP
Kgt	HILLCROSS FM.	7	PALEOZOIC
Km	GATES FM.	7	DEVONIAN, MISSISSIPPIAN
Kgt	MOOSEBAR FM. (1 + Torrey Member)		
Km	GETHING FM.		
Kcd	CADOMIN FM.		

Fort St. John Group  
Bulnheo Group

JKmi	JURASSIC CRETACEOUS
Kcd	SHAFTSBURY FM.
Km	BOULDER CREEK FM.
Kgt	HILLCROSS FM.
Km	GATES FM.
Kgt	MOOSEBAR FM. (1 + Torrey Member)
Km	GETHING FM.
Kcd	CADOMIN FM.



**PETRO-CANADA RESOURCES**

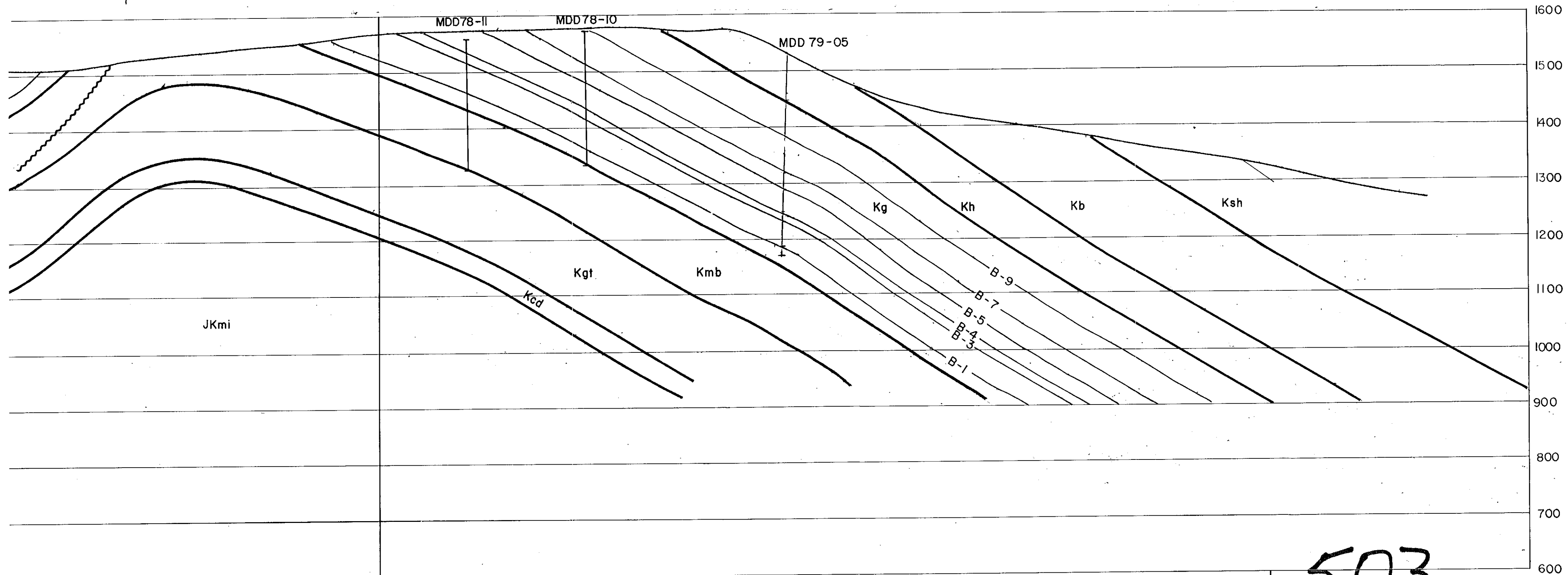
**DUKE PIT**

**SECTION 16, 200N**

CDAL DIVISION

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L.A. SMITH CONSULTING & DEVELOPMENT LTD.



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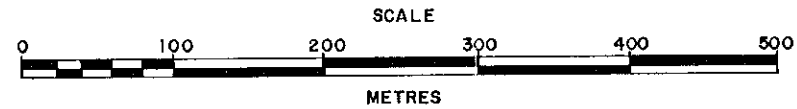


PETRO CANADA  
COAL DIVISION

DATE DECEMBER 1981.  
REVISED JAN '86  
AUTHOR J.M. T.C.  
DRAFTED S.R.T.  
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MONKMAN COAL PROJECT

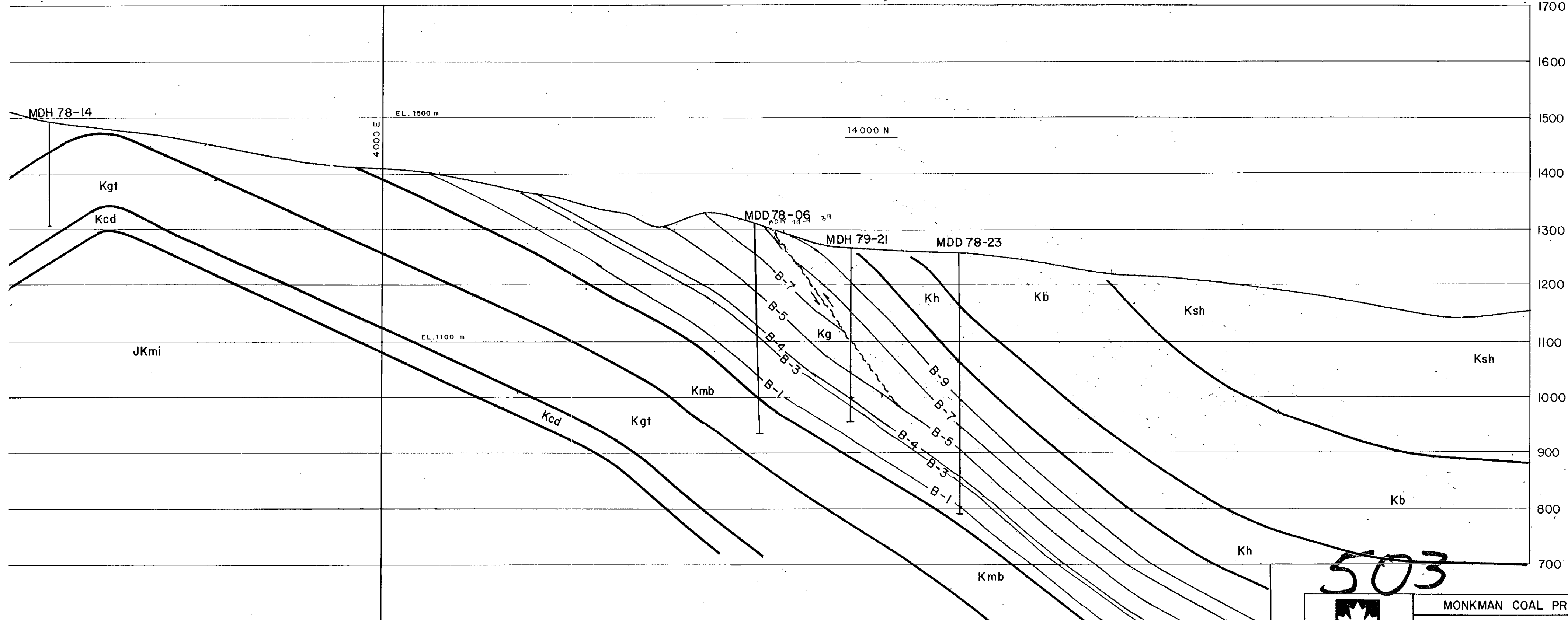
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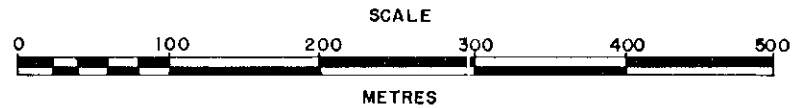
Attached to 1983 Report







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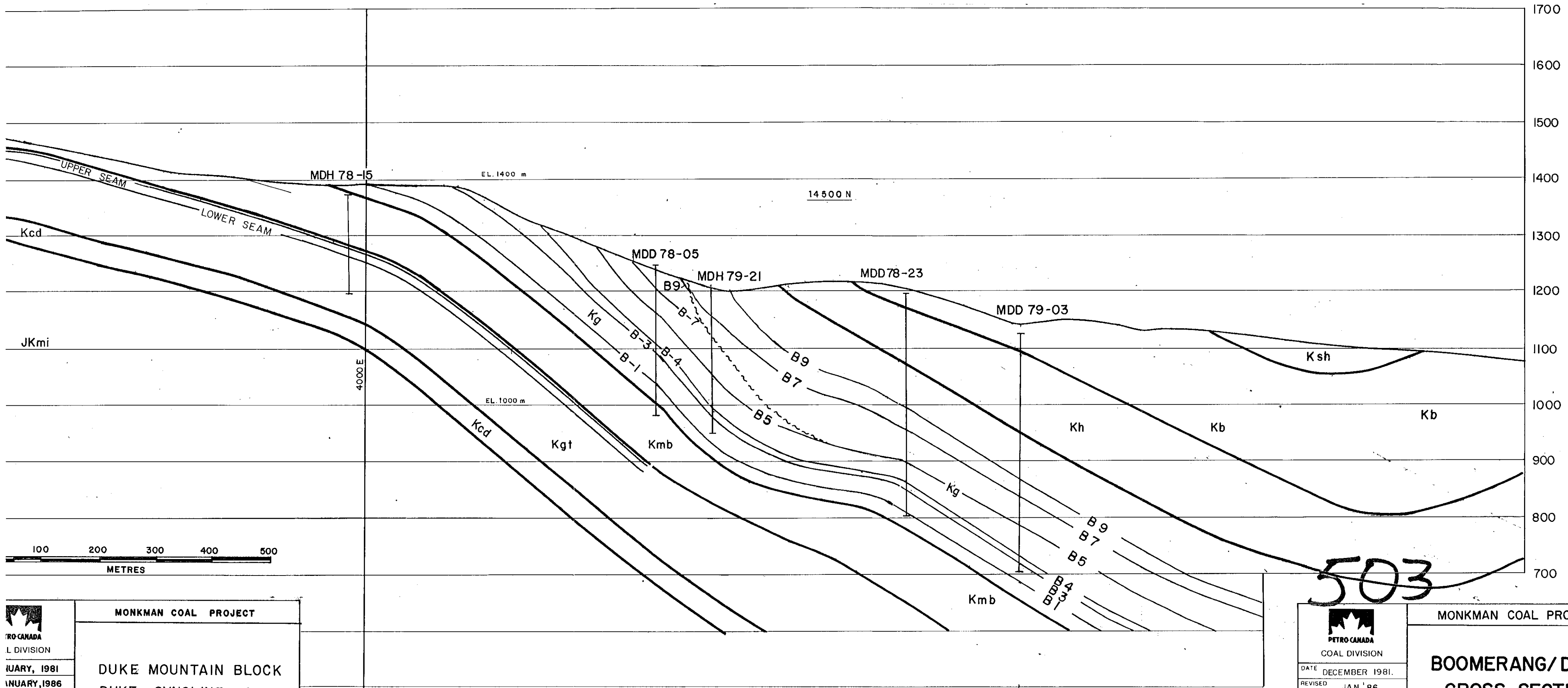


 <b>PETRO CANADA</b> COAL DIVISION	
DATE	DECEMBER 1981.
REVISED	JAN '86
AUTHOR	J.M. T.C.
DRAFTED	S.R.T.
SCALE	1 : 5000


MONKMAN COAL PROJECT


**BOOMERANG/DUKE  
CROSS SECTION  
14,000 N**

Attached to 1983 Report

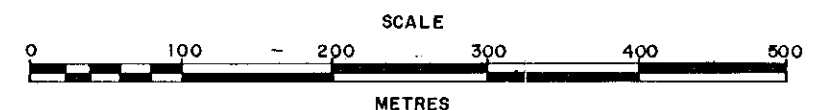


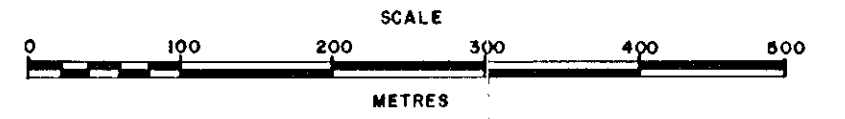
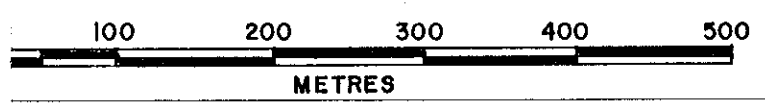
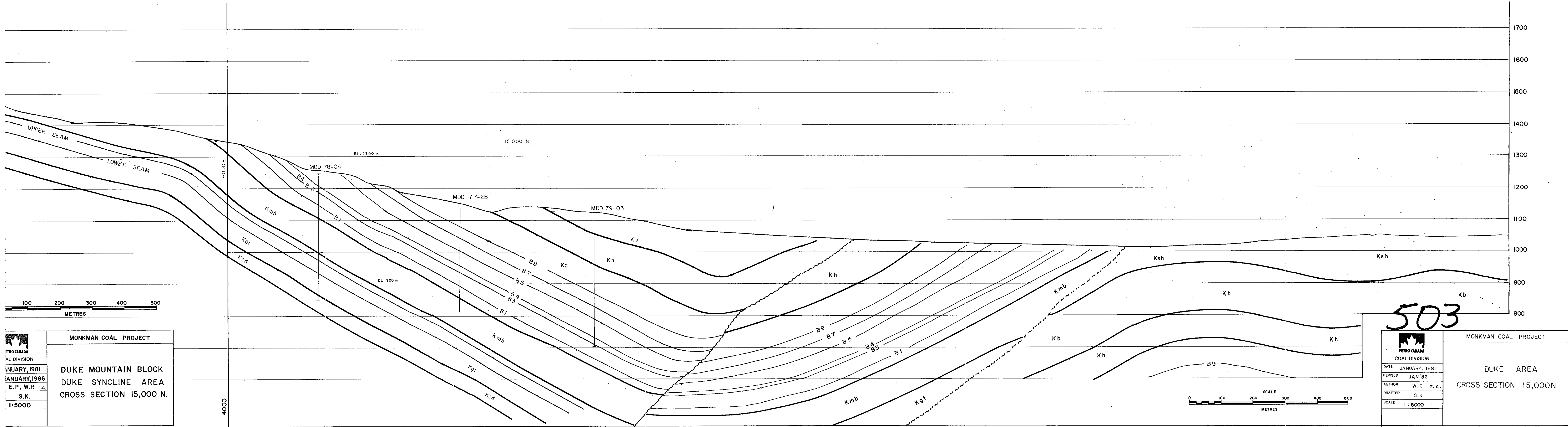
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 PETRO-CANADA COAL DIVISION	MONKMAN COAL PROJECT
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 PETRO-CANADA COAL DIVISION	MONKMAN COAL PROJECT
	BOOMERANG/ DUKE CROSS SECTION 14,500 N
	DATE DECEMBER 1981. REVISED JAN '86 AUTHOR J.M. T.C. DRAFTED S.R.T. SCALE 1: 5000
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MONKMAN COAL PROJECT BOOMERANG/ DUKE CROSS SECTION 14,500 N Attached to 1983 Report
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**MONKMAN COAL PROJECT**  
 PETRO-CANADA  
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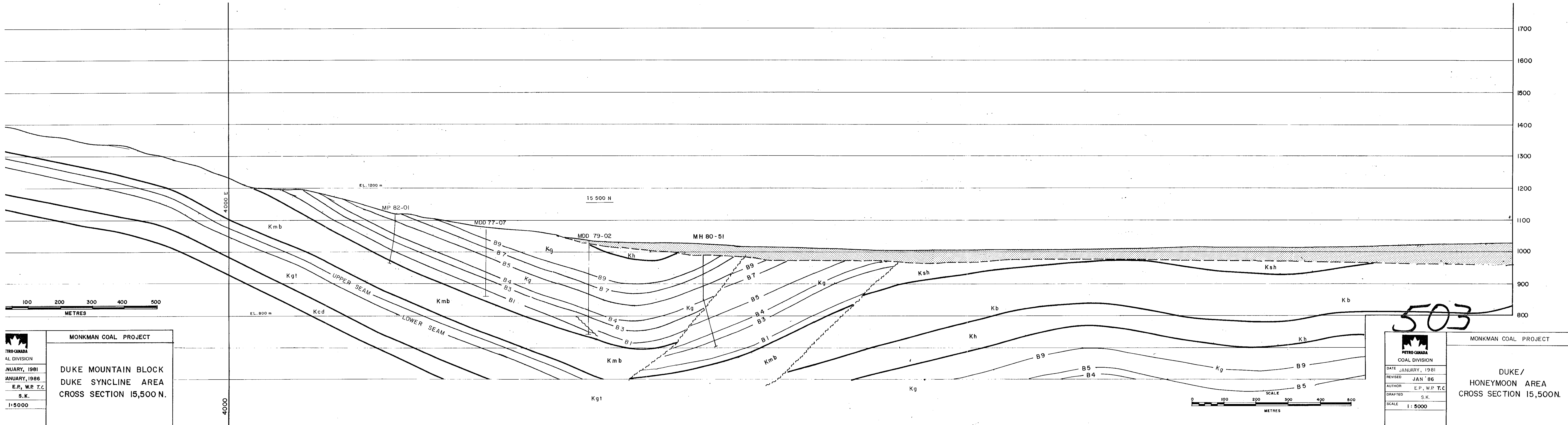
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**DUKE SYNCLINE AREA**  
**CROSS SECTION 15,000 N.**


**MONKMAN COAL PROJECT**  
 PETRO-CANADA  
 COAL DIVISION  
 DATE JANUARY, 1981  
 REVISED JAN '86  
 AUTHOR W. P. T.C.  
 DRAFTED S. K.  
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**DUKE AREA**  
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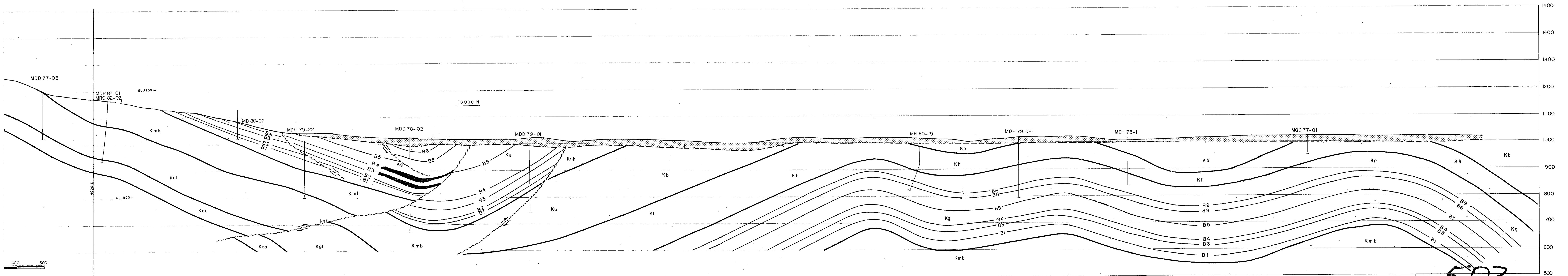


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	DUKE MOUNTAIN BLOCK DUKE SYNCLINE AREA CROSS SECTION 15,500 N.
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	REVISIONS REVISED JAN '86
	AUTHOR E.P., W.P. T.C. DRAFTED S.K. SCALE 1:5000

 PETRO-CANADA COAL DIVISION	MONKMAN COAL PROJECT
	DUKE/ HONEYMOON AREA CROSS SECTION 15,500N.
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	AUTHOR E.P., W.P. T.C. DRAFTED S.K. SCALE 1:5000

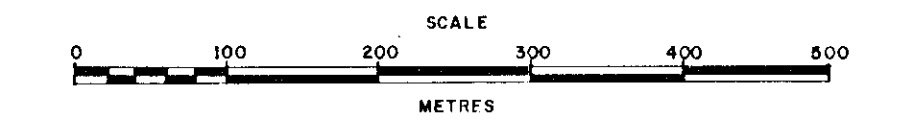
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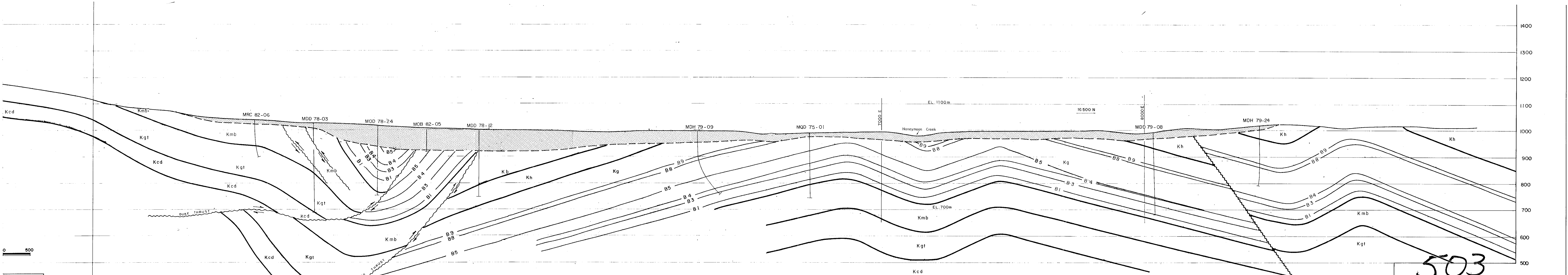


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COAL DIVISION
DATE JANUARY, 1981
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AUTHOR E.P., W.F. T.C.
DRAFTED S.K.
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MONKMAN COAL PROJECT  
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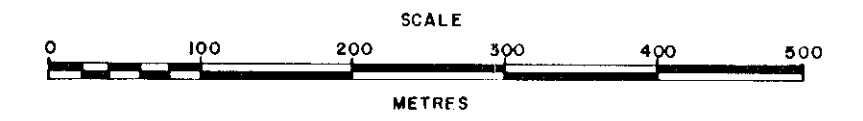
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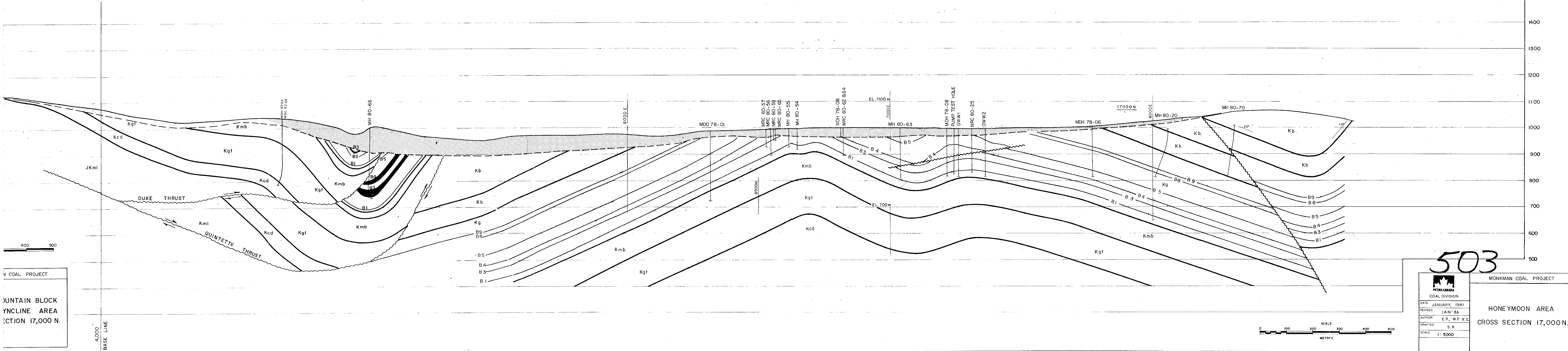


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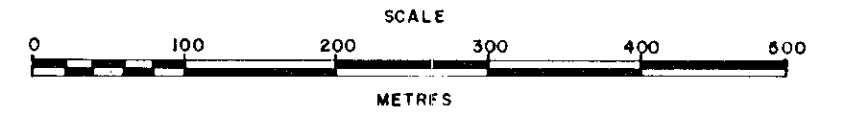
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MONKMAN COAL PROJECT  
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<b>PETRO CANADA</b>	
COAL DIVISION	
DATE	JANUARY, 1981
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AUTHOR	E.P., W.P.T.C.
DRAFTED	S.K.
SCALE	1:5000

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MONKMAN COAL PROJECT  
 HONEYMOON AREA  
 CROSS SECTION 17,000 N.

Attached to 1983 Report



PETRO-CANADA

COAL DIVISION

MONKMAN COAL PROJECT

ANNUAL RECLAMATION REPORT - 1983

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Denis E. Kerfoot

Mine Manager

Monkman Coal Project

FEBRUARY 1984

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MINISTRY OF ENERGY, MINES AND PETROLEUM RESOURCES		
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1. INTRODUCTION
2. PROPERTY LOCATION
3. PROPOSED 1983 DRILLING PROGRAMME
4. CONSTRUCTION
5. RECLAMATION
6. SEED TYPE & FERTILIZERS
7. RECLAMATION COSTS
8. SUMMARY

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APPENDIX II: 1983 RECLAMATION SUMMARY

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PLAN 2: 1983 PROPOSED DRILL PROGRAM - DUKE PIT AREA

PLAN 3: 1983 RECLAMATION SUMMARY

MONKMAN COAL PROJECT  
ANNUAL RECLAMATION REPORT - 1983

1. INTRODUCTION

The Monkman Coal Project is a joint venture of Canadian Superior Oil Limited, McIntyre Mines Limited and Petro-Canada Inc. Annual exploration programmes have been undertaken on the property since 1975, with emphasis on the Duke Mountain Block where medium volatile bituminous coal has been demonstrated to exist in substantial quantity.

The 1983 exploration work was carried out during the first quarter of the year when access roads were prepared for a proposed drilling programme in the northern portion of the Duke Mountain area. The drilling programme was subsequently postponed due to unseasonably warm weather, and in June, 1983 a decision was made to suspend operations at the Monkman Camp in response to changes in the anticipated development schedule for the mine. Reclamation requirements for the property were determined as a result of field inspections and consultations in late May and early June with Mr. E. J. Hall, Reclamation Inspector-Technician, Ministry of Energy, Mines and Petroleum Resources. The camp facilities were removed from the site in July, 1983 and the reclamation work was completed in August, 1983.

2. PROPERTY LOCATION (PLAN NO. 1)

The Monkman Property is located in the southern part of the North East Coal Block approximately 630 km northwest of Vancouver, British Columbia.

Access to the property is provided by all-weather, gravel-surface roads from Tupper, B.C. and Beaverlodge, Alberta on Highway 2 which connects Dawson Creek, B.C. and Grande Prairie, Alberta. A third all-weather route, the Fellers Heights Road/Heritage Highway, starts approximately 16 km west of Dawson Creek and passes through the new town of Tumbler Ridge.

The Quasar airstrip is located 15 km by road to the north of the Monkman Camp site and provides year-round access for medium and light aircraft.

3. PROPOSED 1983 DRILLING PROGRAMME (PLAN NO. 2)

The proposed drilling programme covered an area of relatively flat ground on the northeastern side of Duke Mountain at elevations ranging from 925-1125 metres.

The lower slopes of Duke Mountain support a mixed forest cover of lodgepole pine (Pinus contorta), trembling aspen (Populus tremuloides), black cottonwood (Populus trichocarpa) and some immature white spruce (Picea glauca). The forested areas to the



northwest contain a mixed timber growth of white spruce, lodgepole pine and alpine fir (Abies lasiocarpa). The lower, wet areas in the valley floors support a more-diverse vegetation cover consisting primarily of black spruce (Picea mariana) tamarack (Larix laricina), willow (Salix spp.) and alder (Alnus spp.).

The proposed drilling operations consisted of:

- (a) a maximum of 13 open holes to be drilled to depths of up to 400 m for further assessment of coal reserves;
- (b) flushing and re-logging of 3 previously - drilled holes (MDD 78-12, MH 80-53 and MH 80-66); and
- (c) a total of 6-7 holes to be drilled to depths of 30 m for the installation of piezometers.

The precise number and sequence of drill holes for the further assessment of coal reserves was to be determined on the basis of geological information obtained during the field programme. In order to provide a measure of flexibility to this component of the work programme, a total of 19 drill sites (16 new, 3 existing) were prepared. No clearing was undertaken for the proposed installation of the piezometers.

#### 4. CONSTRUCTION

Access to the locations of the drilling sites was designed to optimize the use of existing trails and roads, thereby minimizing the amount of surface disturbance. A D-6 caterpillar was used to remove the snow from approximately 12.93 km of existing roads and 3 drill sites.

A total of 1.71 km of new access roads was required in support of the proposed 1983 drilling programme. These new routes were traversed in the field to determine that the terrain conditions were suitable. Road development was commenced by slashing to a width of approximately 8 metres, followed by construction of the road surface with a bulldozer. During the latter procedure road grades were maintained at 10% or less to simplify erosion control procedures. In general, all slashed material was cut to a maximum length of 2 metres and wind-rowed with the stumps on the downhill side of the roadway.

The total new construction consisted of 1.71 km (1.36 ha) of roads and 16 drill sites (0.64 ha).

#### 5. RECLAMATION (PLAN NO. 2)

All of the 1983 new construction sites were reclaimed during the months of May and June. A total of 2.00 ha (1.36 ha of roads and

0.64 ha at drillsites) was seeded and fertilized. In addition, 5.04 ha of existing roads (26N, 27D, 27E, 28A, 28S, 28N) and 0.12 ha at three existing drill sites prepared for use in the proposed 1983 exploration programme were reclaimed. Erosion bars were established on the access roads, stream courses were cleared of debris, and a total of 5.16 ha was seeded and fertilized.

The reclamation identified above was directly related to the clearing of new and existing sites in preparation for the proposed 1983 programme. Immediately following the decision to suspend operations at the Monkman Property, aerial and ground inspections of the entire property were made with Mr. E. J. Hall, Reclamation Inspector, Fort St. John on May 25, June 1 and June 3, 1983. As a result of these inspections, additional reclamation work was identified to enhance environmental stability on the property for the term of the project suspension. This work was completed prior to, or immediately following, the removal of the camp as follows:

- o "Route 66" - culverts were removed and trenches or cross-ditches were cut at appropriate intervals along a 4 km section of the road to prevent erosion of the road bed. Dead trees in a 0.2 ha area subjected to earlier mudslides were felled. A deep trench was cut near the junction of "Route 66" and the McIntyre Road to divert

surface water across the road and into its original channel.

- o Adits - Partial subsidence was observed at the entrances to Adits B4-79-1, B1-79-2 and B5-79-3. The areas of subsidence were caved in and excavated with a backhoe and any accessible timbering was removed. The adit entrances were then sealed and backfilled and all disturbed surfaces were graded and seeded.
  
- o Flowing Holes - Attempts were made to plug four holes (MH-80-72; MRC-80-73; MH-81-01 and MH-81-02) from which groundwater was observed to be flowing. Two holes (MH-81-01 and MH-81-02) were plugged but attempts to seal the remaining two holes were unsuccessful.
  
- o Duchess Area - A "Bombi" all-terrain unit was used to provide access to trails 10, 10A and 10B which were seeded by hand.

A backhoe was used to dig two large trenches across the first 1.5 km of the

main access road to the Duchess Area to restrict public use of the road.

- o Fuel Drums - All fuel drums on the property were transported by helicopter to the camp for disposal.
- o Storage Area - All materials stored at the MH-80-23 drill site were removed.
- o Incinerator Site - Refuse pits were backfilled with a backhoe and the incinerator site (2.0 ha) was seeded.
- o Camp Site - all buildings, equipment and perishable materials were removed from the site in July, 1983. The camp foundations and miscellaneous stored materials were enclosed by a barbed-wire fence.

The additional work requirements were completed by August and a final inspection was conducted by Mr. Hall on September 13, 1983.

## 6. SEED TYPES AND FERTILIZERS

The seed mixtures used in the reclamation procedures were:

(a) Standard Forestry Mix:

Climax Timothy	-	20%
Creeping Red Fescue	-	40%
Red Top Fescue	-	15%
Alsike Clover	-	25%

(b) Alpine Mix:

Alsike Clover	-	15%
Boreal Creeping Red Fescue	-	25%
Meadow Foxtail	-	25%
Climax Timothy	-	20%
Kentucky Blue Grass	-	5%
Carlton Bromegrass	-	10%

Fertilizer Mix used consisted of:

Nitrogen	-	10 parts
Phosphates	-	30 parts
Sulphur	-	10 parts

In the 1983 reclamation programme, the Alpine Mix was used at the higher elevations in the Duchess area and the Standard Forestry Mix was used at all other sites.

7. RECLAMATION COSTS

The costs involved in the 1983 reclamation programme were as follows:

Equipment and Fuel	6,360.00
Helicopter and Fuel	4,406.14
Seed and Fertilizer	1,425.80
Contractor Labour	8,270.00
Labour Accommodation	3,575.00

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TOTAL: \$24,036.94

8. SUMMARY

Reclamation work at the Monkman Property in 1983 included the restoration of areas disturbed in preparation for a proposed exploration programme and measures designed to achieve environmental stability on the property for the term of the project suspension.

Reclamation on the Monkman Property is now considered to be current. Periodic inspections will be made in consultation with the local office of the Ministry of Energy, Mines and Petroleum Resources, to ensure that environmental stability has been achieved.

PETRO-CANADA MONKMAN COAL PROJECT  
ROADS AND DRILL SITES - 1983 RECLAMATION REPORT

NAME	ROADS				DRILL SITES			RECLAMATION		
	EXISTING		NEW		DRILL HOLE	EXISTING	NEW	AREA RECONTOURED (ha)	AREA SEEDED AND FERTILIZED (ha)	TOTAL AREA WORKED (ha)
	LENGTH (km)	AREA (ha)	LENGTH (km)	AREA (ha)		AREA (ha)	AREA (ha)			
<u>1983 PROGRAMME</u>										
25A	0.08	0.06	0.25	0.20	II-19		0.04		0.24	0.24
26 SOUTH	2.68	2.14			II-14		0.04		0.04	0.04
26 NORTH	0.91	0.73			I-3		0.04		0.77	0.77
27	1.43	1.14							-	-
27A	0.75	0.60			I-9		0.04		0.04	0.04
27B			0.13	0.10	II-20		0.04		0.14	0.14
27C	0.40	0.32			I-8	0.04			0.04	0.04
27D	0.58	0.46			I-6	0.04			0.50	0.50
27E	0.21	0.17			I-7	0.04			0.21	0.21
27F			0.74	0.59	I-4		0.04		0.63	0.63
					II-5		0.04		0.04	0.04
28 SOUTH	2.71	2.17			II-16		0.04		2.21	2.21
					II-18		0.04		0.04	0.04
28 SOUTH	1.64	1.31			I-10		0.04		1.35	1.35
					II-11		0.04		0.04	0.04
28A	0.25	0.20			II-17		0.04		0.24	0.24
28B			0.48	0.38	I-1		0.04		0.42	0.42
					II-12		0.04		0.04	0.04
28C			0.11	0.09	II-13		0.04		0.13	0.13
ROUTE 66	1.29	1.03			I-2		0.04		0.04	0.04

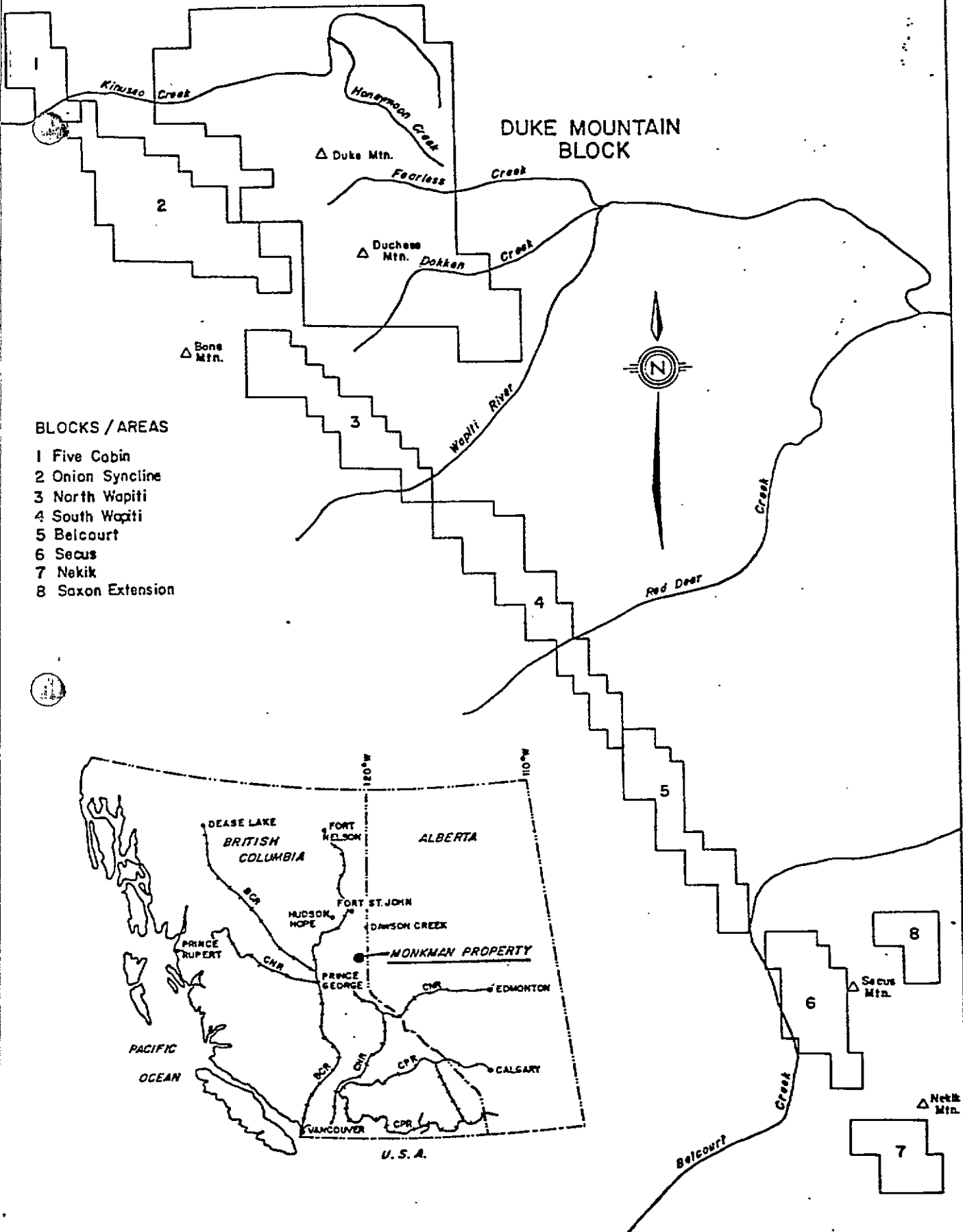


PETRO-CANADA MONKMAN COAL PROJECT  
ROADS AND DRILL SITES - 1983 RECLAMATION REPORT

NAME	ROADS				DRILL SITES			RECLAMATION		
	EXISTING		NEW		DRILL HOLE	EXISTING	NEW	AREA RECONTOURED (ha)	AREA SEEDED AND FERTILIZED (ha)	TOTAL AREA WORKED (ha)
	LENGTH (km)	AREA (ha)	LENGTH (km)	AREA (ha)		AREA (ha)	AREA (ha)			
<u>OTHER</u>										
2A	0.40	0.32							0.32	0.32
10A	2.06	1.65							1.65	1.65
10A	0.80	0.64							0.64	0.64
10B	0.60	0.48							0.48	0.48
ADITS								1.00	1.00	1.00
INCINE- RATOR SITE								2.00	2.00	2.00
TOTALS	16.79	13.42	1.71	1.36		0.12	0.64	3.00	13.25	13.25

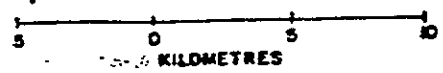
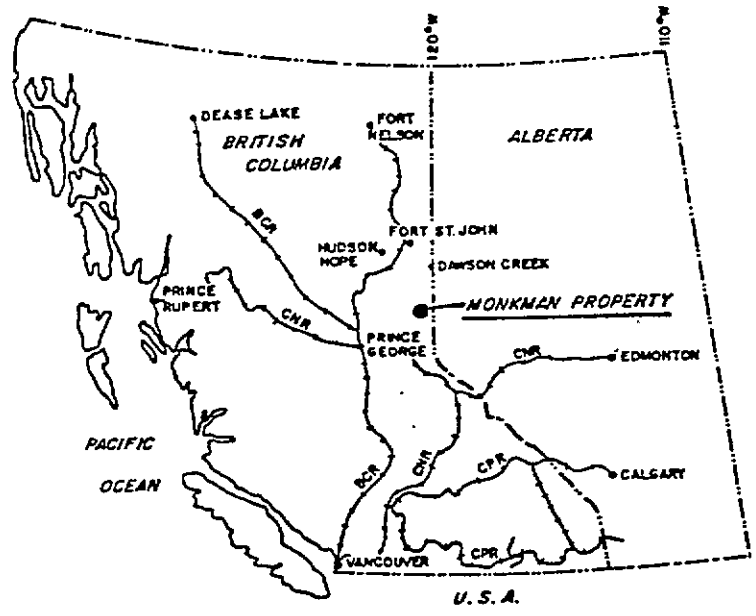
PETRO-CANADA MONKMAN COAL PROJECT  
1983 RECLAMATION SUMMARY

TYPE OF DISTURBANCE	LENGTH (km)	AREA (ha)	RECLAMATION				BALANCE
			RECONTOURED	SEEDED & FERTILIZED	NATURAL	TOTAL	
NEW ROADS	1.71	1.36	0	1.36		1.36	0
EXISTING ROADS	16.79	13.42	0	8.13	5.29	13.42	0
ADITS	-	1.00	1.00	1.00		1.00	0
NEW DRILL SITES	16 <sup>(1)</sup>	0.64	0	0.64		0.64	0
EXISTING DRILL SITES	3 <sup>(1)</sup>	0.12	0	0.12		0.12	0
OTHER <sup>(2)</sup>	-	2.00	2.00	2.00		2.00	0
TOTAL	18.50	18.54	3.00	13.25	5.29	18.54	0



**BLOCKS / AREAS**

- 1 Five Cabin
- 2 Onion Syncline
- 3 North Wapiti
- 4 South Wapiti
- 5 Belcourt
- 6 Secus
- 7 Nekik
- 8 Saxon Extension



**MONKMAN COAL PROJECT  
LOCATION MAP  
PLAN 1**





**LEGEND**

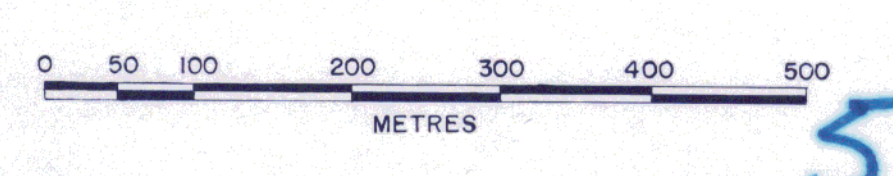
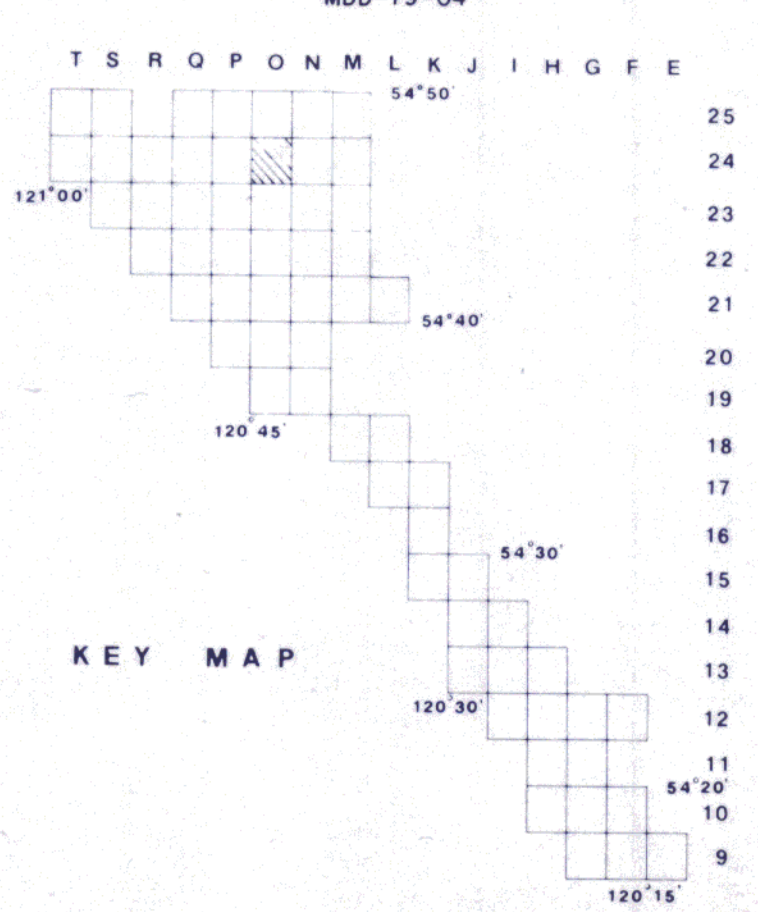
Improved road  
 Secondary road  
 Track or trail  
 Cut line  
 Tree area  
 River  
 Stream  
 Intermittent stream  
 Swamp  
 Contours  
 Horizontal control  
 Vertical control  
 Spot elevation  
 Iron Pin

CONTOUR INTERVAL: 5 METRES  
 DATE OF SURVEY: 1977-1978  
 DATE OF PHOTOGRAPHY: SEPTEMBER 1975  
 DATE OF MAPPING: 1977-1978

**SURVEY NOTE**  
 The Horizontal and Vertical Coordinates were established by D. W. Watson, B.C.S., using conventional and I.T.M. survey equipment. Horizontal and vertical coordinates and elevations are derived from Trig Stations Dunsmuir, E. Dunsmuir, S.W. Maria, Hawk, Marco, Kinross. All coordinates referred to Universal Transverse Mercator Grid Zone 18. Elevations are above Mean Sea Level were established by first leveling vertical angles being read at both ends of each course simultaneously.

**LEGEND**

○ Existing Drill Holes  
 ● Proposed Rotary Hole Location  
 ○ Location of Existing Hole To Be Flushed And Relogged Geophysically  
 I I Priority Of Hole And Sequence In Program  
 - - - - - New Access To Be Built



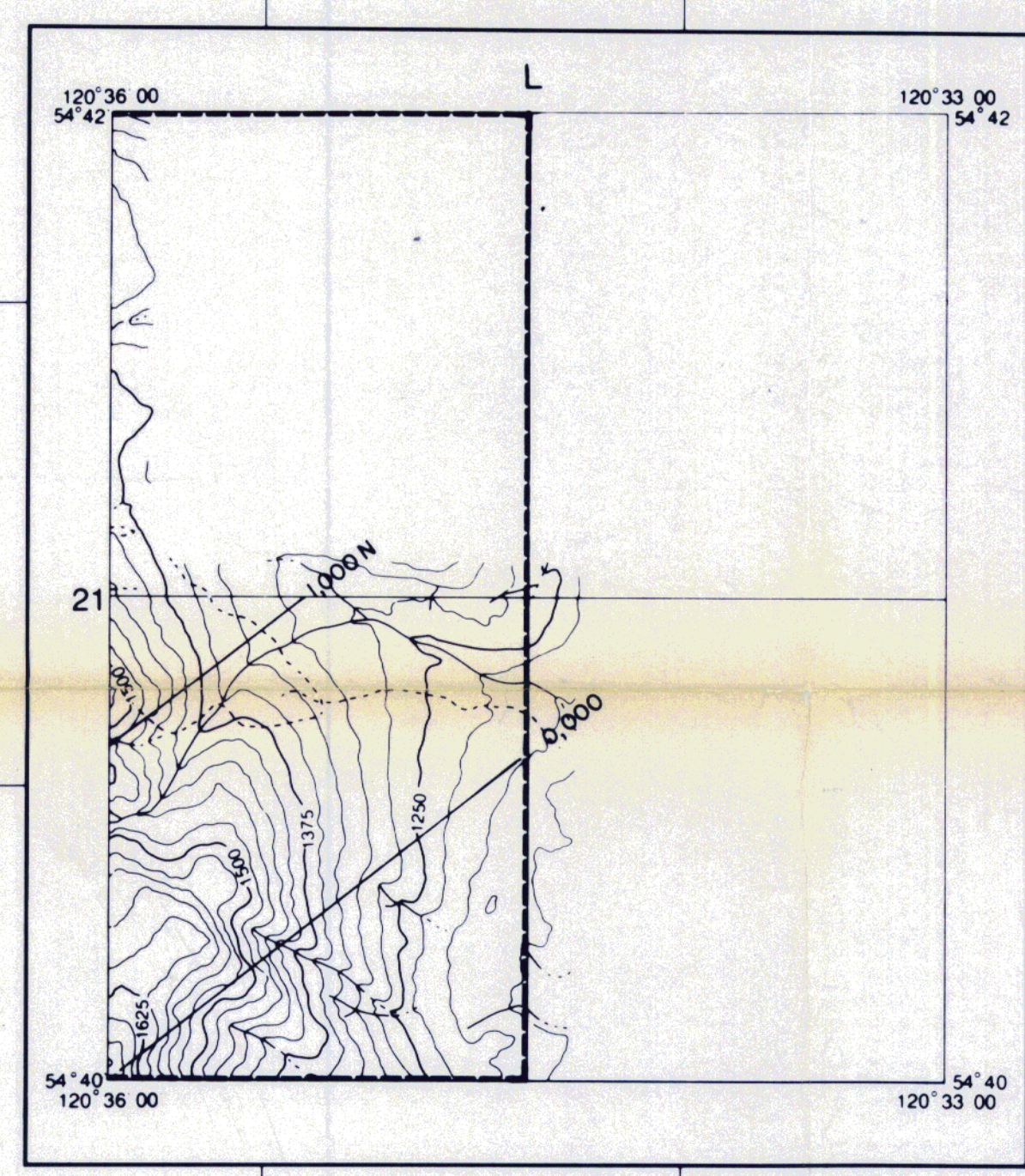
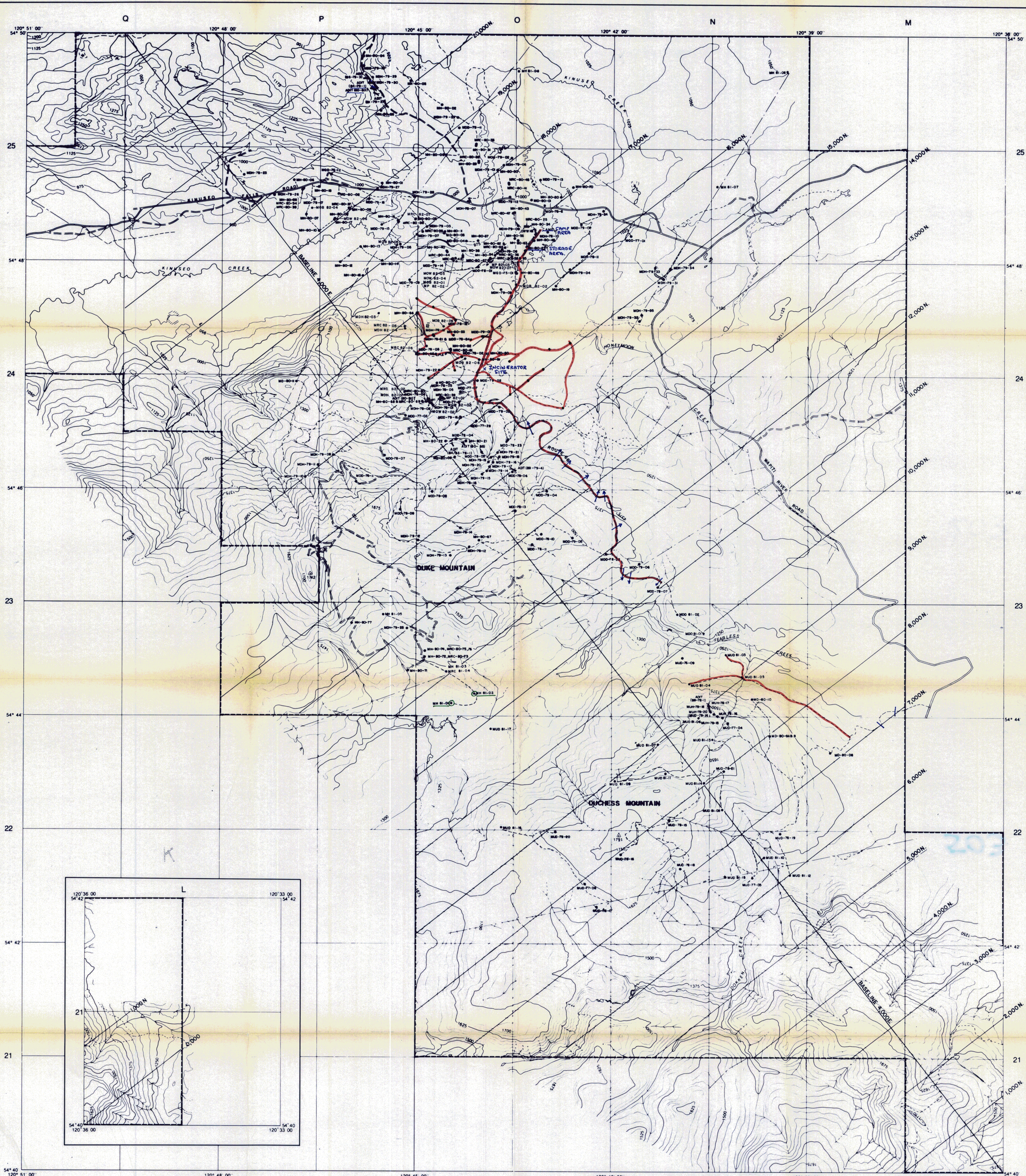
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<b>PETRO-CANADA EXPLORATION, INC.</b>	
COAL DIVISION	
MONKMAN COAL PROJECT	
Date	JANUARY 12, 1983
Revised	
Author	
Drafted	S. K.
Scale	1:5,000

**1983 PROPOSED  
 DRILL PROGRAM  
 DUKE PIT AREA**

O 24





**TOPOGRAPHIC LEGEND**

- MAIN ACCESS ROAD — DRY WEATHER
- EXPLORATION ROAD
- EXPLORATION TRAIL
- AIR STRIP
- SEISMIC LINE, CUT LINE
- POWER TRANSMISSION LINE
- RIVER
- STREAM
- LAKE
- SWAMP
- CONTOURS
- DEPRESSION CONTOUR

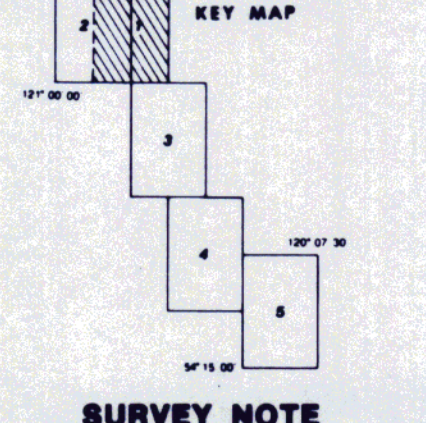
**GEOLOGICAL LEGEND**

- LOWER CRETACEOUS**
- Ksh SHAFTESBURY FORMATION
  - Kb BOULDER CREEK FORMATION
  - Kh HULCROSS FORMATION
  - Kg GATES FORMATION
  - Kmb MOOSEBAR FORMATION
  - Kgl GETHING FORMATION
  - Kcd CADOMIN FORMATION
- JURASSIC — CRETACEOUS**
- Jkm MINNES GROUP

**SYMBOLS**

- PROPERTY BOUNDARY
- GEOLOGICAL CONTACT
- DIP AND STRIKE: REGULAR
- VERTICAL
- HORIZONTAL
- OVERTURNED
- THRUST: FLAGS SHOW DIP DIRECTION
- AREA OF 20m+ OVERBURDEN
- ANTICLINE, SYNCLINE
- DRILL HOLE COLLAR
- ADIT
- PIT AREAS

**KEY MAP**



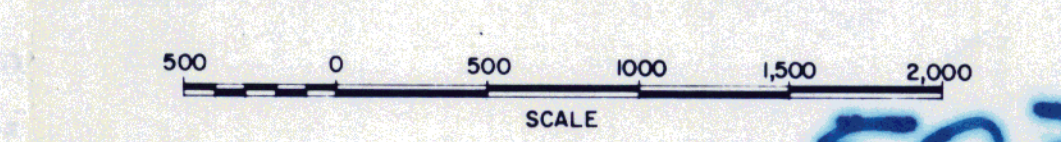
**SURVEY NOTE**

Control Survey was carried out for Photogrammetric Mapping to cover MONKMAN COAL PROJECT COAL LEASES. Mapping outside of the Coal Lease was taken from existing 1:25,000 maps, and 25 metre contour intervals were interpolated.

CONTOUR INTERVAL 25m

R.L. HAREY & ASSOCIATES LTD.

1978



**PETRO CANADA**  
COAL DIVISION

DATE: DECEMBER, 1981  
REVISED: DECEMBER 1983  
AUTHOR:  
DRAFTED: S.R.T., S.K.  
SCALE: 1:25,000

**MONKMAN COAL PROJECT**

**1983 RECLAMATION SUMMARY**

- ACCESS ROUTES
- CROSS-DITCHES
- DRILL SITES
- FLOWING HOLES
- ADITS

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