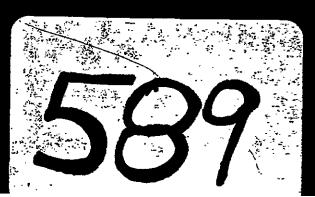
08589 93019 Report on Pine Pass Repair on ..... Project Shell Canada Kepources Inc. G.S. Singhau CL.# 6743-6276 July 1981

1

- 2

PR-Pine Pass ED() # B



Crews	Nest Recou	Inces Limited
	PINE PA	
PINE	PASS	L PROPERTY
IN SINGHA	T INCALS	(Incloturi n. /

VANCOUVER; B.C., V6B IN2

DATE : JULY 31, 1981

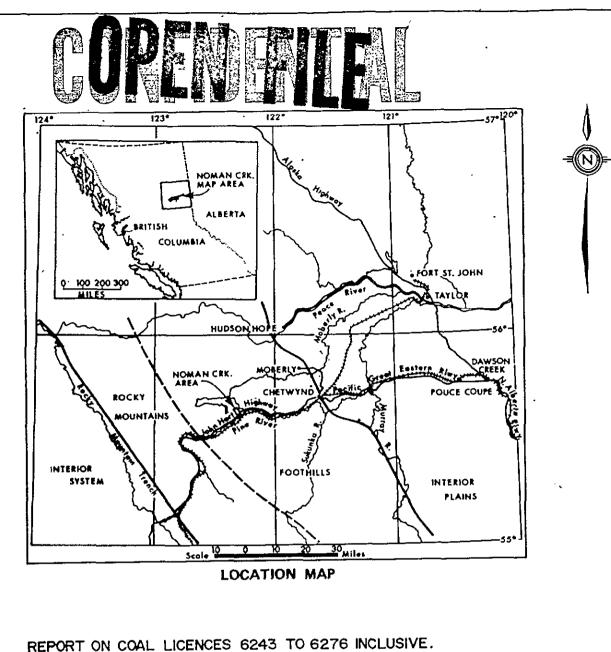
AUTHOR ' G.S. SINGHAI, P. ENGINEER

SINGHAI, ENGINEERING INTERNATIONAL 901, 675 WEST HASTINGS STREET

HELD BY : SHELL CANADA RESOURCES LIMITED OPERATED BY : CROWS NEST RESOURCES LIMITED LAT. 55° 32' TO 55°40' LONG. 122° 07' TO 122° 22' NTS, B.C. GOV'T. COAL DISPOSITION MAP : 93-0/9 CNRL COAL LAND DISPOSITION MAP : HF-188

PEACE RIVER, LAND DISTRICT, BRITISH COLUMBIA JULY 31, 1981 ON FIELD WORK DONE IN PERIOD OF JUNE 9, 1980 TO AUGUST 29, 1980

V



# PINE PASS

# COAL EXPLORATION

# - 1980 -

Coal Licences 6243-6276 Inclusive

Peace River Land District, Northeast British Columbia

National Topographic Sheet #930/9

Latitude: 55° 37' 00" North

Longitude: 120° 20' 00" West

Owner: Shell Canada Resources Limited

Operator: Crows Nest Resources Limited

Consultant and Author: G.C. Singhai, M.Tech., P.Eng. Singhai Engineering International Ltd. #901, 675 West Hastings Street Vancouver, B.C., V6B 1N2

Field Work: June 9th through August 29, 1980

Submission Date: June 2, 1981

CNRL Coal Land Disposition Map HF-73B



# TABLE OF CONTENTS

.

			PAGE
1.0	SUMMA	RY ,	1 - 1
2.0	INTRO	DUCTION	2 - 1
	2.1 2.2 2.3	Coal Land Tenure Location, Geography and Physiography Access	2 - 1 2 - 2 2 - 3
3.0	WORK	DONE	3 - 1
	3.1 3.2 3.3 3.4	Scope and Objective of 1980 Exploration Work Done in 1980	3 - 1 3 - 4 3 - 5 3 - 9
4.0	GEOLO	GY	4 - 1
	4.1 4.1A 4.2	Geology of Area	4 - 1 4 - 2 4 - 4
5.0	NOMAN	CREEK AREA	5 - 1
	5.1 5.2 5.3 5.4 5.5	Geological Structure Coal Geology Coal Reserves Mineability Coal Quality	5 - 1 5 - 5 5 - 9 5 - 10 5 - 11
6.0	WILLO	DW CREEK AREA	6 - 1
	6.2 6.3 6.4	Location Previous Work Work Done in 1980 Stratigraphy and Structure Coal Geology Conclusion and Recommendations	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$
7.0	FALL	ING-BEAUDETTE CREEKS AREA	7 - 1
	7.1 7.2 7.3 7.4 7.5 7.6 7.7	Structure	7 - 1 7 - 1 7 - 2 7 - 2 7 - 2 7 - 2 7 - 4

1

# LIST OF ENCLOSURES

.

ł

~

----

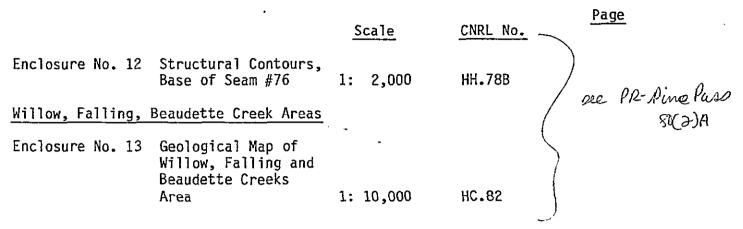
....

~

Following Page No.

							Page No.
	Noman Creek A	rea			Scale	CNRL No.	
	Enclosure No.	1	Location Map	as	shown	HE.41E	1
	Enclosure No.	2	Access Map	1:0	600,000	HE.41D	2-4
	Enclosure No.	3	Coal Land Disposition Map	1:	50,000	HF.18B	
	Enclosure No.	4	Stratigraphic Section				
	Enclosure No.	5	Regional Geological Map with Coal Land Overlays	1:	50,000	HF.19C	ree PR-Pine Pass 80(2)B
	Enclosure No.	6	Regional Structural Cross Section			HE.41B	
	Enclosure No.	7	Geological Maps (2) 7-1 South 7-2 North	1: 1:	2,000 2,000	HD.79 HD.79A	
-	Enclosure No.	8	Cross Section from Cadomin/Gething to Gething/Moosebar Contact	1:	1,000	HK.77	
	Enclosure No.	9	Geological Sections Section 9-1 to 9-12	1:	2,000	HB.79 to	НВ.79К
	Enclosure No.	10	Measured Trench Sections (2D) 10-1 to 10-21 (W1-W21)	1:	200	HF.79 to	HF.79S
	Enclosure No.	11	Measured Trench Sections (10) 11-1 to 11-10 (E1-E10)	1:	200	HJ.81 to	HJ.811

•- •



# TABLES

		Following Page No
TABLE I	B.C. Coal Licences Tenure Standing	2-1
TABLE II	Table of Formations	4-2
TABLE III	Table of Formation, Pine Pass Region	4-3
TABLE IV	Analysis of Drill Core Coal Samples	5-6
TABLE V	Pine Pass Coal Co. Bulk Sample - Seam 76	5-6
TABLE VI	Reserve Calculations Pine Pass Project	5-9
TABLE VII	Coal Quality	5-10

# APPENDICES

Appendix A	Application to Extend Term of Licenc	e	3-9
Appendix B	Survey 1980 Records Survey 1980 (2) Scale as show and List of Coordinates	HH78 HH78A	

A3/AQb.54

- ----

#### 1.0 SUMMARY

The Pine Pass Coal Property consists of 34 coal licences covering 9962 hectares of land held by Shell Canada Resources Limited. The licences are located about 45 air kilometers west of Chetwynd, north and south of the Pine River, in the Peace River Land District, Liard Mining Division of Northeast British Columbia. The history of the property dates back to 1948-51 when N.D. McKechnie, Geologist with the Coal Division of the British Columbia Department of Lands and Forest initiated an exploration program of geological mapping and diamond drilling 24 holes totalling 15,835 feet. Later in 1969, Brameda Resources Ltd. completed 23 diamond drill holes totalling 4,787 meters, and estimated about 11,618,600 short tons of coal.

The property is underlain by the Cadomin and Gething formations of the Bullhead Group and Moosebar Formation of the Fort St. John Group, both of the Lower Cretaceous age. The Gething formation coal measures are the prime prospect for coal. The geology of the Noman Creek area is complicated by tight folding and faulting.

The Noman Creek syncline is a tight southerly plunging fold preserving 300 - 400 meters of Gething formation. This syncline strikes at N 40° W. The south end of the fold is cut off by alluvial deposits in the Pine River Valley, while the northern end extends for about 7 kilometers. The middle zone of Gething covers two main coal seams which occur about 250 meters below the contacts of Gething and Moosebar. The coal seams are about 30 meters apart with an aggregate thickness of about 10 meters. The preliminary coal reserves estimates indicate about 24.6 metric million tonnes in place with the overburden ratio of 4.6 bank cubic meters per tonne. This coal can be mined by open pit.

The total cost of the 1980 exploration program was \$301,806.69. Further exploration work of 3751 meters of rotary drilling, 3,800 meters of backhoe trenching, and 4.5 kilometers of road building is recommended for 1981.

A3/AQb.2

- ---- -

#### 2.0 INTRODUCTION

-----

This report describes the work carried out by Mr. G.C. Singhai, P. Eng., Consulting Geologist of Singhai Engineering International Ltd., #901, 675 West Hastings Street, Vancouver, B.C. on behalf of Crows Nest Resources Limited of Calgary, Alberta, the operator of the property, during the period of June 9, 1980 to August 30, 1980, in an attempt to evaluate an economically viable coal deposit of metallurgical grade coking or Steam Coal on coal licences held by Shell Canada Resources Limited in the Pine Pass area of Northeast British Columbia. This exploration program was initiated as an encouraging result of the work carried out by Mr. Eric Pancy, Geologist of Crows Nest Resources Limited during the summer of 1979.

# 2.1 Coal Land Tenure

Shell Canada Resources Limited holds 34 coal licences (No's 6243 to 6276 Inclusive) covering 9962 hectares of land in the Land District of Peace River, Northeast British Columbia. The property is operated by Crows Nest Resources Limited, a wholly owned subsidiary of Shell Canada Resources Limited.

The following table, entitled "B.C. Coal Licences Tenure Standing" gives details of tenure.

# CROWS NEST RESOURCES LIMITED EXPLORATION

• / •

B.C. COAL LICENCES TENURE STANDING

BLOCK: PINE PASS GROUP: UNGROUPED

- ·

. · ·

- -

PROJECT:

YEAR:

Pi	ROJE	<u></u>		BLOC	K.	1	GROU	10			LICENCE		Loco	NOA/		TALS	r	0	OUTREMENT			1 011	DGET			AND DISTRICT	<u> </u>
		AREA TOTAL AC/HA	NAME	LIC	AREA TOTAL AC/HA	NO.	LICS.	AREA TOTAL AC/HA		NO.	LEGAL DESCRIPTION	AREA TOTAL AC/HA	F	EES			EXPIRED,		ENT YEAR ME-				ENT YEAR	101%	DELL	DINER THAN B.C. DOV'T DESCRIPTION	RE
PINE PASS	1	9962	PIKE PASS	34	9962	-		ACZHA	<u>  YEPR</u>	<u> </u>		1	YEAR		<u> </u>		1		i i	1	,	AFE	*10 <sup>3</sup>	=1C <sup>3</sup>	1		┢
	<u> ~</u>	3302	FINE FROD		9902			• ·			NTS 93-0-9	9962	80	240	49,810	99.6	74.7	2	124,525 1-3/	4 227.5	MAY 21			402.2	<u> </u>	<b></b>	╞
											BLOCK B UNITS										<u> .</u>		, , ,,				
		•									43, 44, 53, 59 45, 46, 55, 56						•								Ţ_		
<u>.,,</u>				Ī						6245	47, 48, 57, 58 49, 50, 59, 60	293									# # 1		i				ŀ
										5247	65, 66, 75, 76	293					1			<u> </u>			 1				+
···· · · ·					<u>  `</u>	<u>.</u>				6 <u>248</u> 6249	67, 68, 77, 78 69, 70, 79, 80	293	┝╺╼╬				· · · · !			<u> </u>					<u> </u>		
-				ļ	<u> </u>					6250	81, 82, 91, 92	293					i		Ì	:	1		ļ		L.		
				[						6251 6252	87, 88, 97, 98	293															
									1		BLOCK C UNITS	İ					1			!					<b></b>		-
				┼──							41, 42, 51, 52 61, 62, 71, 72							_		!	. <u> </u>				—		┡
					<u>.</u>					6255	63, 64, 73, 74	293													<b>_</b>		
				;	:					6256 6257	83, 84, 93, 94 85, 86, 95, 96	- 293 - 293					1	ļ		!	;						
				;							BLOCK F UNITS		1						,,		,			***			Γ
				<del>                                      </del>	s 5	<u></u>	1 1				<u>3, 4, 13, 14</u> 5, 6, 15, 16		i						;						┼──		┢
			<del></del>	· · · · ·						6260	· 7, 8, 17, 18	293					<u>'</u>			<u> </u>	;		<u> </u>				Ļ
				1							25, 26, 35, 36																
								1			29, 30, 39, 40 45, 46, 55, 56																Γ
					:					6265	47, 48, 57, 58	293	i				; ,		 	 							F
			·		·					6266	49, 50, 59, 60 67, 68, 77, 78	293															⊢
										6268	89, 90, 99,100	293			, ,				; 1	· · ·							
											BLOCK 6 UNITS						1	,	, I								F
						•					BLOCK B UNITS				i				1		· · · ·						F
			• • •								61, 62, 71, 72 63, 64, 73, 74						<u> </u>	;					<u> </u>		<u> </u>		┢
										6272	83, 84, 93, 94	293	•				+		ii							•	L
											85, 86, 95, 96 BLOCK 6 UNITS		1		, ,			ĺ	i								1
										6274	7, 8, 17, 18	293						;								·	Γ
			<u> </u>		-	· · · · -	╬┈┿			6275	BLOCK F UNITS 23, 24, 33, 34	293					<u> </u>		<del>¦</del> ;								1
				L			<u> </u>			6276	<u>69, 70, 79, 80</u>	293		1004			; ;		· · · · · · · · · · · · · · · · · · ·								1
														NORK DONE	1980							i 					
	ļ											•	1	\$	302,290		!	ļ	' !								1
ENERAL I S THE O	REMA PERA	RKS: F	ILL NECES	SPRI	I LINES	S AND COLU	MIIS D	1.LYJ (	CAL	DEVE:	LOPMENT POT	ENTIAL	15	"Y" (	PRIME	UN⊾E	SS 01-8	ERK	188 STATE: -	D, L:C	ENCES H	£10	₽¥ 5,4	ELL C4	ANAD	A ABSOURCES LT	)

. .

Table I

06.4

#### 2.2 Location, Geography and Physiography

The Pine Pass property is located contiguously north and south of the Pine River, about 45 air kilometers west of Chetwynd and 55 air kilometers southwest of Hudson Hope in the Peace River Land District and Liard Mining Division of Northeast British Columbia (see Encl. #3). The property is centered approximately 55° 37' North Latitude and 122° 20' West Longitude on Topo Sheet N.T.S. 93-0-9.

These coal licenses are situated on the eastern slope of Mount Bickford and Pyramis Peak on the north and south of Pine River respectively, in the foothills of the Rocky Mountains. Elevations throughout the licences range from 655 meters in the Pine River Valley to 1220 meters in the northwest part of the Noman Creek area and to 1372 meters on the peak east of Willow Creek in the southern part of the area. The area is characterized by relatively low, rounded, northwest-southeast trending ridges and valleys dissected by the northeast-southwest trending 1.5 kilometer wide Pine River Valley. Physiographically, this valley divides the licence area into two main blocks: north (Noman Creek area) and south (Falling Creek and Willow Creek areas). The ridges are separated by valleys of creeks (Cleveland Creek, Fisher Creek, Noman Creek - in the north; and Willow Creek, Falling Creek, and

Beaudette Creek - in the south of Pine River) which are tributaries of the Pine River.

The area is well forested by poplar and some birch in low elevations as in the Pine River Valley, and fir or spruce at higher elevations. In wet areas willows and devils club are common. The timberline is at an elevation of about 1300 meters above sea level.

## 2.3 Access

~»- ····· ·

The property is accessible by highway #97 (John Hart Highway) which runs through the middle of the property north of the Pine River. It is an all-weather road connecting Prince George to Dawson Creek via Chetwynd. The town of Chetwynd is about 70 kilometers east of the property by this highway and the deep sea ports of Vancouver and Prince Rupert are about 1200 kilometers west of the area.

The British Columbia Railway line runs south of the Pine River which connects the area with the Vancouver and Prince Rupert sea ports. This is the only property in the northwestern coal field which has road and railway access to the deep sea ports at present.

Dawson Creek and Fort St. John, about 100 km and 160 km north of Chetwynd respectively, are serviced by daily flights of commercial airlines. Numerous helicopters are available at Chetwynd.

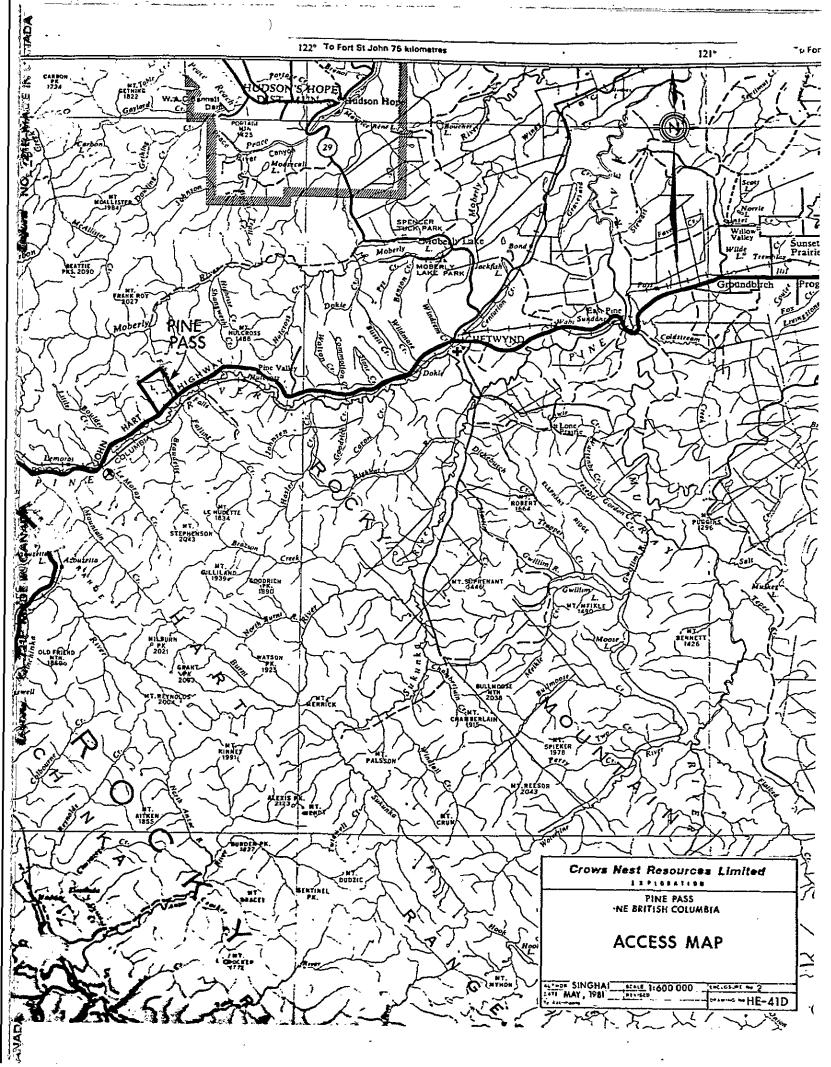
The Noman area is immediately north of the main highway and railway and is accessible on good dirt roads as a result of previous exploration and high voltage power line construction by B.C. Hydro.

There is a reasonably good dirt road on the east edge of the licences along Willow Creek, but most of the property on the south side of the Pine River is accessible by helicopter only. Landing sites are very few due to relatively thick forest cover. These dirt roads are accessible by four-wheel drive vehicles.

Two high voltage power lines run through the Noman Creek area which could supply all power requirements. Water is available from the Pine River and its tributaries. Mining and exploration can be carried out throughout the year (see Encl. #2).

A3/AQb.6

۰.



# 3.0 WORK DONE

# 3.1 Summary of Previous Work

The history of the area goes back to as late as 1946 and 1951 when the British Columbia Department of Mines carried out an exploration program of geological mapping, trenching and diamond drilling of coal deposits in the Peace River District, about 100 kilometers west of Dawson Creek. The coal field extended from about 1.6 kilometers north of the Pine River to some 29 kilometers southeast. The objective of the work was to estimate the tonnage of mineable coal that might be available contiguous to a proposed route of the Pacific Great Eastern Railroad into the Peace River District. Since then the area has been fairly active. The principle sources of data are the following published reports (see Bibliography):

#### a) McKechnie, N.D., 1955

The Coal Division of the Department of Lands and Forests of British Columbia carried out geological mapping and diamond drilling, 1948 to 1951, under the supervision of Mr. N.D. McKechnie, Geologist with the B.C. Government. During this period he drilled 24 holes to a total of 15,835 feet in and 39 holes to a total of 25,447 feet in Noman Creek and Willow Creek areas respectively. The proximate analysis of coal intersections were performed by the department laboratory (B.C. Dept. of Mines, Bulletin No. 36).

# b) Muller, J.E., 1961

The geological map 11-1961 published by the Geological Survey of Canada at a scale of 1:250,000, completed by Mr. J.E. Muller, is of little significance as mapping is too generalized and of doubtful quality.

# c) Hughes, J.E., 1964

Reconnaissance geological mapping at a scale of 2 inches to 1 mile, of the Pine Pass area, carried out by Mr. J. Hughes during 1954-1958 in order to describe the succession of Jurassic and Cretaceous strata in detail (B.C. Dept. of Mines and Petroleum Resources Bulletin #51).

# d) Hughes, J.E., 1967

Regional geological mapping at a scale of 1 inch to 1 mile was carried out during 1954-1960. The geological map accompanies B.C. Mines Bulletin #52 which describes the geology along the John Hart Highway in the area under study. This is probably the most detailed geological map published at this scale.

# e) Pine Pass Coal Company, 1968

đ

As a result of the N.D. McKechnie report of 1955, Pine Pass Coal Company drove an adit into a thick coal seam along strike for a distance of 120 feet, and at this point a crosscut of uniform length. A bulk sample was collected from the adit and submitted for proximate and ultimate analysis to Warnock Hersey (see Table V).

# f) Brameda Resources Ltd.

Brameda Resources Ltd. conducted a coal exploration program in the Noman Creek area during 1968-69 under the supervision of Mr. Harold M. Jones, P. Eng., of Vancouver, B.C. This program consisted of geological mapping at a scale of 1:4800, bulldozer trenching, diamond drilling and sampling. They drilling 23 diamond drill holes totalling 4,787 meters. Trenching was carried out in association with road construction. Trench descriptions are missing but core

A3/AQb.9

descriptions are available. They estimated about 11,618,600 short tonnes in place. Most of the reserves are estimated from coal seams #76 and 78 with average thickness of 5 feet to 18.5 feet over a strike length of 9,600 feet and dip length of 1380 feet.

# g) Crows Nest Resources Limited, 1979

Crows Nest Resources Limited carried out a program of geological mapping at a scale of 1:5000, limited hand trenching and sampling of exposed coal in these trenches. The samples were shipped for analysis to Crows Nest Resources' Laboratory in Fernie, B.C.

Preliminary coal reserves were estimated at 5 to 10 million tonnes open pit mineable at 5:1 to 10:1 overburden ratio. The two main seams 78 and 76 were taken into consideration mainly due to their thickness and continuity in the area.

## 3.2 Scope and Objective of 1980 Exploration

The previous extensive exploration drilling and geological mapping program by the B.C. Government and Brameda Resources Limited during the periods 1948-1951 and 1968-1969 respectively, did not resolve the problems of structure or seam correlation. Thus reserve estimations could not be made properly. Early reserve estimates of about 10 million tonnes with a stripping ratio of 10:1 was not economically feasible.

The exploration program of 1980 was oriented towards structural setting, correlation of coal seams, and to increase coal reserves if possible. The most economical way of achieving this objective was by detailed geological mapping on a scale of 1:2000, backhoe trenching and sampling exposed coal seams. This would allow the preparation of detailed structural cross-sections on a scale of 1:1000. The cross-sections could then be used for estimation of coal reserves, geological interpretation of the area, and for planning of 1981 exploration program if warranted.

## 3.3 Work Done in 1980

The majority of the exploration work was carried out on Noman Creek area, north of the Pine River, east of Cleveland Creek and west of Fisher Creek, for a length of about 7 km. This area was given importance because of the availability of detailed information of previous extensive exploration work, potential for increasing reserves, and easy access to the area. During the period of June 9th to August 30, 1980, the following program was carried out.

- a) Detailed geological mapping of the Noman Creek area on a scale of 1:2000 using topographic sheets as the base, prepared by Crows Nest Resources Limited. Details are shown on the geological maps contained in the enclosures (see Encl. 7-1, 7-2).
- Trenching was carried out by a John Deere 450C crawler type b) combination front end loader-backhoe. These trenches were laid out in the areas of interest by running a flagged compass line down the proposed centerline of the trench along existing roads, bulldoze trails and old trenched areas. Depth of overburden was variable from 0.2 meters to greater than 3.5 meters. Most trenches averaged 0.5 meters in width and 1.0 - 1.2 meters in depth, except in significant coal seams which were deepened to at least 2.5 meters in search of fresher coal. When bedrock was lost due to deep burial several pits were dug to approximately 4 meters, the limit of the equipment. When no bedrock was encountered trenching was terminated. The geology and intersections of coal seams were mapped in detail, on a scale of 1:200 and measured (see Encl. 10 and 11). A total of 30 trenches with a total length of 3434 meters were completed and surveyed (Appendix B).

3 - 6

In addition to the above backhoe trenches, one hand trench was dug near the intersection of the southernmost powerline right-of-way and Noman Creek to protect environmental conditions.

- c) About 2.30 km of 5-meter wide roads were built by bulldozer as an access to the proposed drill holes as a result of 1979 field work. Drill sites were prepared, however, the holes were not started. These roads were laid out in such a way that the road cut perpendicular to the strike of the beds so that trenches and exposed bedrock information could be gathered.
- d) All exposed intersections of coal were systematically sampled, marked by paint and photographed. Samples were sent to Crows Nest Resources Lab, Fernie, B.C., for proximate analysis.
- e) A section from Cadomin Conglomerate, which is exposed at about 500 meters west of Cleveland Creek to the base of Moosebar Formation, was measured and a section was prepared.

- f) All these trenches, diamond drill hole locations, and roads were surveyed and survey stations marked by iron pins were established. The survey work was started from the known bench marks and traverses were closed. Surveying was carried out by Tronnes Surveys Limited of Calgary, Alberta (Appendix B).
- g) All these trenches were filled after collecting available information. Road and recovered trenched areas were seeded and fertilized as per Ministry of Environment of British Columbia requirements.
- h) In addition to the above work in Noman Creek area some geological mapping was initiated in Willow Creek and Falling Creek areas. Due to heavy overburden and thick undergrowth, most of the area was not accessible. Apart from this, few exposures of bedding or coal were found except along some creeks or roads.

A successful and on-schedule completion of the 1980 program is due to average weather conditions and a good effort from the support staff.

A3/AQb.14

\_\_\_\_\_

-----

# 3.4 Cost of Work Done in 1980

The detailed costs of the 1980 exploration program are contained in the Application to Extend Term of Licence on the following pages. The figures have been apportioned to all the licences, reflecting those parts of the total area in which Crows Nest Resources Limited has interests.

The 1980 exploration program was completed at a cost of \$301,806.89.



Province of British Columbia Ministry of Energy, Mines and Petroleum Resources

# APPLICATION TO EXTEND TERM OF LICENCE

I. Bolton Agnew (Name)	agent for Shell Canada Resources Limited . (Name)
P.O. Box 100	400 - 4 Avenue, S.W.
(Address)	(Address)
Calgary, Alberta	Calgary, Alberta, T2P 2H5
•	Valid FMC No. 207568
hereby apply to the Minister to extend the term of Co Thirty-four B.C. Crown Coal Licence:	ai Licance(s) No(s)
for a further period of one year.	
2. Property name Pine Pass Coal Project,	Peace River Land District
	orfeit
•••••••••	
4. I have performed, or caused to be performed, during the	he period May 21, 1980 to
<u>May</u> .20 1981	, work to the value of at least \$ 302, 290, 54

. . . . . .

on the location of coal licence(s) as follows:

CATEGORY OF WORK

. .

<u> </u>	Licence(s) No(s).	Apportioned Cost
Geological mapping	6243-6276 Incl.	
Surveys: Geophysical		
Geochemical	<b>-</b>	
Other	6259-6276 Incl.	42,613.79
Road construction	6260,6262,6263,626	
Surface work	.6260_6262_6263_626	6 50,411.92
Underground work		-
Drilling		
Logging, sampling, and testing	.6260,6262,6263,626	
Reclamation	6260,6262,6263,626	6
Other work (specify)		
Off-property costs		
5. I wish to apply \$. 302,290.54	. of this value of work on Co	al Licence(s) No(s). 6243 - 6276 Incl.
•••••••••••••••••••••••••••••••••••••••		
6. I wish to pay cash in lieu of work in the	amount of \$	on Coal Licence(s) No(s).
•••••••••••••••••••••••••••••••••••••••		
7. The work performed on the location(s)	is detailed in the attached rep	port entitled
Pine Pass Geological I	Report 1980, will be	submitted in ninety days
••••••••		
		OBIOTRIAL DIONED EX
N 00 1001		ORIGINAL SIGNED SY
May 20, 1981 (Date)	••••••	BOLTON AGNEW (Signature)
		Land Supervisor
	•••	(Position)

(FORMS AND REPORT TO BE SUBMITTED IN DUPLICATE)

Appendia A

40

#### CATEGORY OF WORK

\_\_\_\_

GEOLOGICAL	MAPPING		Yes 🖾	No		
		1000 Area (	Hectares)	1:2,000	Scale Q	Duration
Reconnaissan						
Detail:	Surface					
	Underground					
Other (specify						
	• • • • • • • • • • • • •			• • • • • • • • • • •	Total Cost	s100.750.83.
		CAL SURVEYS		No		
Tenerraphie	Photogr	ammetric ma	apping and 1	ocation s	urveys	
Other (specify						
		••••••			Total Cost	s .42,613.79
ROAD CONS	TRUCTION		Yes 🖾	No	0	
Length	2.3 km			/idth	m	
On Licencels	No(s) 6260,	6262, 626	6266			
Access to	/ 140(3)					
					Total Cost	\$ 53,678.99
Upgrading	g old roads	s: 2.5 km			total Cost	9.558555555
	<b>~</b> ~//		Yes 🖾	No	m	
URFACE W	URK	1 .4	Width		—	Cost
		Length .3434 .m			Depth 	.:50,411,92
Trenching						•••••
Seam Tracing	•••		• • • • • • • • • •			• • • • • • • • • • • •
Crosscutting						• • • • • • • • • • • •
					Total Cost	\$ .50.411.92
	-				-	
UNDERGROL	JND WORK .		Yes 🛛	No	N N	
		F A .P.	Maximum Length	No. of	Total Manage	Cost
		o, of Adits			Total Metres	
Test Adits						• • • • • • • • • • •
Other working	ngs					
• • • • • • • • •					Total Cost	s –
•••••	• • • • • • • • • • • •		• • • • • • • • • • • • •		Total Cost	\$ <del>.</del>
					Total Cost	\$ <del>.</del>
			Yes 🖸	No	Total Cost	\$ <del>.</del>
			Yes 🖸		Total Cost	S
	Diamond	. Ha	Yes 🗖	No No, of Holes	Total Cost	Cost
DRILLING	Diamond	. Ho	Yes 🗖	No. of Holes	Total Cost 친 Total Metres	Cost
DRILLING Core:	Diamond Wireline	. Ha	Yes 🗖	No No, of Holes	Total Cost 친 Total Metres	Cost
DRILLING	Diamond Wireline Conventional	. Ho 	Yes 🗖	No No, of Holes	Total Cost 전 Total Metres	Cost
DRILLING Core: Rotary:	Diamond Wireline Conventional Reverse circula	. Ho 	Yes 🗖	No. of Holes	Total Cost 전 Total Metres	Cost
DRILLING Core: Rotary: *Other (specif	Diamond Wireline Conventional Reverse circula	. Ha  	Yes 🗖	No. of Holes	Total Cost 전 Total Metres	Cost
DRILLING Core: Rotary: *Other (specif	Diamond Wireline Conventional Reverse circula	. Ha  	Yes 🗖	No. of Holes	Total Cost 전 Total Metres	Cost
DRILLING Core: Rotary: *Other (specid Contractor.	Diamond Wireline Conventional Reverse circula	. Ho 	Yes 🗖	No. of Holes	Total Cost 전 Total Metres	Cost
DRILLING Core: Rotary: *Other (specif	Diamond Wireline Conventional Reverse circula	. Ho 	Yes 🗖	No. of Holes	Total Cost 전 Total Metres	Cost
DRILLING Core: Rotary: *Other (specif	Diamond Wireline Conventional Reverse circula	. Ho 	Yes 🗖	No. of Holes	Total Cost 전 Total Metres	Cost
DRILLING Core: Rotary: *Other (specif	Diamond Wireline Conventional Reverse circula	. Ho 	Yes 🗖	No. of Holes	Total Cost	Cost
Core: Rotary: Other (specif Contractor . Where is the	Diamond Wireline Conventional Reverse circula (y) 	. Ho	Yes 🗖	No. of Holes	Total Cost	Cost
Core: Rotary: Other (specif Contractor. Where is the LOGGING, S	Diamond Wireline Conventional Reverse circula (y) 	. Ho	Yes D	No. of Holes	Total Cost	Cost
DRILLING Core: Rotary: *Other (specif Contractor. Where is the LOGGING, S Lithology:	Diamond Wireline Conventional Reverse circula (y) core stored?	Ha  ntion D TESTING	Yes D ble Size	No. of Holes	Total Cost	Cost
DRILLING Core: Rotary: *Other (specif Contractor . Where is the LOGGING, S Lithology: Logs: .	Diamond Wireline Conventional Reverse circula (y) core stored?	D TESTING	Yes D ble Size Yes D Core samples Density	No. of Holes	Total Cost	Cost
DRILLING Core: Rotary: *Other (specif Contractor . Where is the LOGGING, S Lithology: Logs: . *Other (specif	Diamond Wireline Conventional Reverse circula fy) core stored? AMPLING AN Drill samples Gamma-neutro fy). 47. Backl	Ho  ation D TESTING D TESTING D TESTING D TESTING	Yes Density Samples, .ani	No No. of Holes No I I I I I I Slysed .bot	Total Cost Total Metres Total Metres Total Cost Bulk samples	Cost 
DRILLING Core: Rotary: *Other (specif Contractor . Where is the LOGGING, S Lithology: Logs: . *Other (specif	Diamond Wireline Conventional Reverse circula (y) core stored? AMPLING AN Drill samples Gamma-neutro (y) .47. Backl Proximate anal	D TESTING	Yes Density Samples, .and FSI	No. of Holes No. of No alysed.bot	Total Cost	Cost 
DRILLING Core: Rotary: *Other (specif Contractor . Where is the LOGGING, S Lithology: Logs: . *Other (specif Testing:	Diamond Wireline Conventional Reverse circula (y)	Ho intion D TESTING D TESTING I D too trenct. Iysis II	Yes D ble Size Yes D Core samples Density samples, .and FSI Petrographic	No. of Holes No. of No alysed .bot	Total Cost Total Metres Total Metres Total Cost Total Cost Bulk samples ch.raw.and.washe Washability Plasticity	Cost 
DRILLING Core: Rotary: *Other (specid Contractor . Where is the LOGGING, S Lithology: Logs: . *Other (specid Testing:	Diamond Wireline Conventional Reverse circula (y)	Ho intion D TESTING D TESTING I D too trenct. Iysis II	Yes D ble Size Yes D Core samples Density samples, .and FSI Petrographic	No. of Holes No. of No alysed .bot	Total Cost Total Metres Total Metres Total Cost Total Cost Bulk samples ch.raw.and.washe Washability Plasticity	Cost 
DRILLING Core: Rotary: *Other (specif Contractor . Where is the LOGGING, S Lithology: Logs: . *Other (specif Testing: *Other (specif OTHER WOR	Diamond Wireline Conventional Reverse circula fy) core stored?	Ha htion D TESTING D TESTING D TESTING L hoe trench. lysis lysis	Yes Dele Size	No. of Holes No. of Holes	Total Cost Total Metres Total Metres Total Cost Bulk samples ch.raw.and.washe Washability Plasticity Total Cos	Cost 
DRILLING Core: Rotary: *Other (specif Contractor . Where is the LOGGING, S Lithology: Logs: . *Other (specif Testing: *Other (specif OTHER WOR	Diamond Wireline Conventional Reverse circula fy) core stored? core st	Ha  htion D TESTING D TESTING D TESTING I boe, trench. I lysis I sils)	Yes Density Samples, and FSI Petrographic	No No. of Holes No alysed.bot	Total Cost Total Metres Total Metres Total Cost Bulk samples ch.raw.and.washe Washability Plasticity Total Cost	Cost 
DRILLING Core: Rotary: *Other (specif Contractor . Where is the LOGGING, S Lithology: Logs: . *Other (specif Testing: *Other (specif Other (specif	Diamond Wireline Conventional Reverse circula fy) core stored? core st	Ha  htion D TESTING D TESTING D TESTING I boe, trench. I lysis I sils)	Yes Density Samples, and FSI Petrographic	No No. of Holes No alysed.bot	Total Cost Total Metres Total Metres Total Cost Bulk samples ch.raw.and.washe Washability Plasticity Total Cost	Cost 
DRILLING Core: Rotary: *Other (specif Contractor . Where is the LOGGING, S Lithology: Logs: . *Other (specif Testing: *Other (specif Other (specif	Diamond Wireline Conventional Reverse circula fy) core stored? core st	Ha  htion D TESTING D TESTING D TESTING I boe, trench. I lysis I sils)	Yes Density Samples, and FSI Petrographic	No No. of Holes No alysed.bot	Total Cost Total Metres Total Metres Total Cost Bulk samples ch.raw.and.washe Washability Plasticity Total Cost	Cost 
DRILLING Core: Rotary: *Other (specif Contractor. Where is the LOGGING, S Lithology: Logs: *Other (specif Testing: *Other (specif Other (specif	Diamond Wireline Conventional Reverse circula fy) core stored? core st	Ha  htion D TESTING D TESTING D TESTING I boe, trench. I lysis I sils)	Yes Density Samples, and FSI Petrographic	No No. of Holes No alysed.bot	Total Cost Total Metres Total Metres Total Cost Bulk samples ch.raw.and.washe Washability Plasticity Total Cost	Cost 
DRILLING Core: Rotary: *Other (specif Contractor . Where is the LOGGING, S Lithology: Logs: . *Other (specif Testing: *Other (specif OTHER WOR	Diamond Wireline Conventional Reverse circula fy) core stored? core st	Ha  htion D TESTING D TESTING D TESTING I boe, trench. I lysis I sils)	Yes Density Samples, and FSI Petrographic	No No. of Holes No alysed.bot	Total Cost Total Metres Total Metres Total Cost Total Cost Bulk samples th.raw.and.washe Washability Plasticity Total Cost Total Cost On-property cost	Cost 
DRILLING Core: Rotary: *Other (specif Contractor . Where is the LOGGING, S Lithology: Logs: . *Other (specif Testing: *Other (specif Other (specif	Diamond Wireline Conventional Reverse circula fy) core stored? core st	Ha  htion D TESTING D TESTING D TESTING I boe, trench. I lysis I sils)	Yes Density Samples, and FSI Petrographic	No No. of Holes No alysed.bot	Total Cost Total Metres Total Metres Total Cost Total Cost Bulk samples th.raw.and.washe Washability Plasticity Total Cost Total Cost On-property cost Off-property cost	Cost 
DRILLING Core: Rotary: *Other (specif Contractor . Where is the LOGGING, S Lithology: Logs: . *Other (specif Testing: *Other (specif Other (specif	Diamond Wireline Conventional Reverse circula fy) core stored? core st	Ha  htion D TESTING D TESTING D TESTING I boe, trench. I lysis I sils)	Yes Density Samples, and FSI Petrographic	No No. of Holes No alysed.bot	Total Cost Total Metres Total Metres Total Cost Total Cost Bulk samples th.raw.and.washe Washability Plasticity Total Cost Total Cost On-property cost	Cost 
DRILLING Core: Rotary: *Other (specif Contractor . Where is the LOGGING, S Lithology: Logs: . *Other (specif Testing: *Other (specif OTHER WOR	Diamond Wireline Conventional Reverse circula (y)	Ha  ation D TESTING D TESTING	Yes Density Samples, and FSI Petrographic	No No. of Holes No alysed.bot	Total Cost Total Metres Total Metres Total Cost Total Cost Bulk samples th.raw.and.washe Washability Plasticity Total Cost Total Cost On-property cost Off-property cost	Cost 
DRILLING Core: Rotary: *Other (specif Contractor . Where is the LOGGING, S Lithology: Logs: . *Other (specif Testing: *Other (specif Other (specif	Diamond Wireline Conventional Reverse circula fy) core stored? core st	Ha  ation D TESTING D TESTING	Yes Density Samples, and FSI Petrographic	No No. of Holes No alysed.bot	Total Cost Total Metres Total Metres Total Cost Total Cost Bulk samples th.raw.and.washe Washability Plasticity Total Cost Total Cost On-property cost Off-property cost	Cost 
DRILLING Core: Rotary: *Other (specif Contractor. Where is the LOGGING, S Lithology: Logs: *Other (specif Testing: *Other (specif Other (specif	Diamond Wireline Conventional Reverse circula (y)	Ha  ation D TESTING D TESTING	Yes Density Samples, and FSI Petrographic	No No. of Holes No alysed.bot	Total Cost Total Metres Total Metres Total Cost Total Cost Bulk samples th.raw.and.washe Washability Plasticity Total Cost On-property cost Off-property cost Off-property cost Total Expenditures	Cost 
DRILLING Core: Rotary: *Other (specif Contractor. Where is the LOGGING, S Lithology: Logs: *Other (specif Testing: *Other (specif Other (specif	Diamond Wireline Conventional Reverse circula (y)	Ha  ation D TESTING D TESTING	Yes Density Samples, and FSI Petrographic	No No. of Holes No alysed.bot	Total Cost Total Metres Total Metres Total Cost Total Cost Bulk samples th.raw.and.washe Washability Plasticity Total Cost Total Cost On-property cost Off-property cost	Cost 
DRILLING Core: Rotary: *Other (specif Contractor . Where is the LOGGING, S Lithology: Logs: . *Other (specif Testing: *Other (specif Other (specif	Diamond Wireline Conventional Reverse circula (y)	Ha  ation D TESTING D TESTING	Yes Density Samples, and FSI Petrographic	No No, of Holes No i slysed .bot	Total Cost Total Metres Total Metres Total Cost Total Cost Bulk samples ch.raw.and.washe Washability Plasticity Total Cost On-property cost Off-property cost Total Expenditures (Signature)	Cost 
DRILLING Core: Rotary: *Other (specif Contractor . Where is the LOGGING, S Lithology: Logs: . *Other (specif Testing: *Other (specif Other (specif	Diamond Wireline Conventional Reverse circula (y)	Ha  ation D TESTING D TESTING	Yes Density Samples, and FSI Petrographic	No No, of Holes No i slysed .bot	Total Cost Total Metres Total Metres Total Cost Total Cost Bulk samples th.raw.and.washe Washability Plasticity Total Cost On-property cost Off-property cost Off-property cost Total Expenditures	Cost 

10

\*A full explanation of other work is to be included.

#### 4.0 GEOLOGY

#### 4.1 Regional Geology

The area under consideration lies within the Rocky Mountain Foothills and trends northwesterly along the front of the Rocky Mountains between the Sukunka and north of the Pine Rivers in northeastern British Columbia. The strata outcropping in the Pine River Valley are of Mesozoic age, from middle Triassic to upper Cretaceous, which were deposited on the shelf of a miogeosyncline. These formations thin eastwards across the Foothills and onto the plains. The sedimentary environment in the Foothills and Plains were continuous and similar.

Triassic strata is marine in origin, consisting of limestone, calcareous shales, siltstone and sandstone. Jurassic sediments are also mainly marine shales. The lower Cretaceous sediments of sandstone, shales and coal measures of deltaic deposition marked the end of marine sedimentation. The coal bearing beds of lower Cretaceous age outcrop extensively along the Foothills of Alberta and Northeast British Columbia. These sediments have been assigned to the Blairmore, Bullhead and Fort St. John groups (see Encl. 5).

These sediments were folded, thrust faulted and uplifted during the Columbian orogeny and being deformed into elongate plunging anticlines and synclines with associated faulting. These rocks are exposed in a series of en echelon folds and thrust belts trending northwest-southeast (see Encl. 6).

Regional Stratigraphic studies have been made by the Geological Survey of Canada and published as Stott (1968a) and Stott (1971) (see Table of Formation #11).

Several local stratigraphic and mapping projects have been completed within the area - both by Geological Survey of Canada and by the British Columbia Department of Mines. These are documented by Hughes (1964), Hughes (1967), McLean and Kindle (1950), McKechnie (1955) and Spivate (1944).

## A. Geology of Area

The geology of the area has been mapped at a scale of  $1^{"} = 4$  miles by Muller (1961) and Stott (1961), of Geological Survey of Canada. These two maps are of a reconnaissance nature only.

# TABLE 11

. . .

# TAPLE OF FORMATIONS

.

1				
		ormation r Group	Thickness (feet)	Lithology
	G	ort St. John roup (includes oosebar fm.)	3,000 - 5,000	Dark grey, marine shale with fine grained sandstone.
Lower Cretaceous	Bullhead Group 0-2	Gething Formation	1,000 - 3,000 (?)	Fine-grained, cherty to quartzose sandstone; rusty weathering shales; carbonaceous mudstone and coal seams; minor conglomerate.
	2,500	Cadomin Formation	100 - 500	Massive chert conglomerate and coarse-grained sand- stone; carbonaceous shale, minor coal.
				y; bevels rocks of rd and eastward.
	 M	linnes Group	0 - 6,000	Massive quartzose sand- stone; alternating units of fine-grained sand- stone and mudstone; minor carbonaceous sediments.
Jurassic		ernie ormation	500 - 1,000	Calcareous and phosphatic shales; rusty weathering shales; glauconitic silt- stone; sideritic shales; thinly interbedded sand- stone, shale, and silt- stone.

Mapping was also done by McKechnie, N.D. (1955) and Hughes, J.E. (1967), Department of Mines and Petroleum Resources, British Columbia. Mr. Hughes published a map at a scale of 1" = 1 mile to accompany Bulletin No. 52. Detailed mapping was completed for the Noman Creek area by Brameda Resources on a scale of 1:4800 during the period 1968-1969.

The Noman Creek area, on which most of the exploration and geological mapping at a scale of 1:2000 was carried out during 1980, is underlain by the Cadomin and Gething formations of Bullhead Group and Moosebar formations of Fort St. John Group of Lower Cretaceous age (see Table III).

A3/AQ5.18

		HUGHES	SCOTT		_
		1964	1968		
GROUP		MOOSEBAR FM	MOOSEBAR FM	-	FORT ST.JOHN GROUP
	d D	GETHING FM	GETHING FM		
	IER GROUP	URESSER FM	CADOMIN FM	BULLH	
	CRASSIER		UNCONFORMITY		
	С В	BRENOT FM	UNNAMED		
	DI	SCONFORMITY		-	•
		MONACH FM	MONACH FM		
• •	GROUP	BEATTIE PEAKS FM	BEATTIE PEAKS FM	NES GROUP	- -
	BEAUDETTE	MONTEITH FM	MONTEITH FM	MINNES	

ς,

Crows Hest	Resources Limited
	PLORATION
	PINE PASS TISH COLUMBIA
TABLE OF	FORMATIONS
PINE P	ASS REGION
MIT DEC 1979 ANTIN	TABLE -
To Attimutery	• HE-41C

入

# 4.2 Stratigraphy

The rocks exposed in the area of the Crows Nest Coal Licences and in particular in the Noman Creek area are the main coal bearing horizon, the Gething formation. The Minnes group of Jurassic age is exposed about 600 meters west of Cleveland Creek out of the licence area. It is not discussed in this report other than to record its presence underlying the Cadomin formation which marks the base of the Bullhead group of Lower Cretaceous age.

#### A. Bullhead Group

The Bullhead group contains two formations: the coal bearing Gething formation and its basal conglomerate unit - the Cadomin formation.

### i) Cadomin Formation

The coarser sediments consist of conglomerates and gritty sands which grade laterally into siltstones and mudstones and seem to be flood plain sediments. Outcrops of Cadomin formation stand in relief against those of the Gething, though they are not distinctive everywhere. On hilly ground or above treeline, the

steeply dipping beds of coarse clastics form ridges, such as those above 500 m west of Cleveland Creek. The conglomerates form thick beds and lenses but at places it is missing or replaced by grit and/or very coarse-grained sandstone. The thickness of Cadomin formation about 600 meters west of Cleveland Creek is approximately 10 meters.

# ii) Gething Formation

The term Gething was given first by McLean when he was working in the Peace River Foothills (1918, 1923). It indicates a productive coal measures in the upper part of the Bullhead succession, and separates them from underlying non-marine sandstones, lean coal measures and its basal conglomeratic unit - the Cadomin formation.

The Gething formation is predominantly a sequence of shales, siltstones, sandstone and coal seams. In the Noman Creek area approximately 300 meters of Gething strata could be measured. Both the lower and upper contacts exist. However, wide covered intervals, complicated structural setting, difficulties in

correlating strata above and below coal seams 78 and 76, made it impossible at this time to establish a type section.

# 4.2 B. Moosebar Formation

The Gething Formation is overlain by Moosebar formation. A thin chert pebble bed of 0.25-1.00 meters thickness marks the contact usually in this area. This conglomeratic bed is known as the Blue Sky conglomerate.

The Moosebar formation is lithologically distinct from the Gething formation and consists mostly of dark gray, rubbly and partly calcareous mudstones and shales with minor beds of argillaceous sandstones and ironstone bands. Thin layers of bentonite are also noticed occasionally. Clasts in the basal Moosebar conglomerate are well rounded and 0.2 to 2.5 cm in diameter, mostly vari-colored chert pebbles with a matrix of sandstone and mudstone. The contact is regarded as disconformable, and indicating an overall marine transgression. The Moosebar formation is probably about 360 meters thick. It is soft and easily weathered. Their outcrops are generally in the valleys of Fisher, Falling and Beaudette Creeks and cliff faces.

#### 5.0 NOMAN CREEK AREA

## 5.1 Geological Structure

The available geological and structural data suggests that the structure of the Noman Creek area is complex consisting of

small scale folds and faults. The problem is compounded by poor outcrop. An attempt was made to interpret the structure of the area by twelve structural cross-sections (Encl. 9, Section 1-12) and a structural contour map at the base of coal seam #76 (Encl. 12).

The Noman Creek syncline, Noman Creek anticline, and Fisher Creek syncline are three main folds in the area. The folding of Lower Cretaceous strata is complicated by several shear zones and three reverse faults in this area.

The Noman Creek syncline is assymetrical in shape with variable dips of 42°-80° on the west limb and 35°-70° on the east limb. The axis of the syncline strikes about North 30° West (330°) and plunges approximately 12° to the southeast in the southern part of the area or close to the John Hart Highway. But the plunge of the syncline decreases towards the northwest and at about 900 meters (between Section 6 and 7; Encl.9) north of the highway, the plunge almost disappears. The east limb of the syncline or west limb of the Noman Creek anticline is cut by the Noman Creek reserve fault. This fault strikes North 33° West and dips 60° southwest. About 700 meters north of the highway the strike of fault changes to 320°, possibly deflected by a thick sandstone bed on the crest of the Noman Creek anticline. This fault can be traced up to about 1.5 km north of the highway and most probably terminated by a 246° striking fault which runs along the termination point of Noman Creek towards the west.

The Noman Creek fault is also displaced about 80 meters to the west by a normal fault which strikes about northeast-southwest and occurs about 300 meters north of the highway. About 170 meters of displacement on the Noman Creek fault is indicated by McKechnie (1955).

About 400 meters east of Noman Creek fault, the Eastern Reverse fault occurs which strikes N 50° W, and dips 60° N.E. and displaces the northeast limb of the Noman Creek anticline up dip by 135 meters. As a result of the fault, the contact of Moosebar and Gething is repeated. As a result of the Noman Creek and Eastern Reverse faults of opposite dips, a down-dropped block was formed causing a rift valley at the central part of the anticline. It indicates that in between these two faults seams #76

and 78 are preserved which are intersected by diamond drill holes nos. PR-12 and PR-16 (see Section 8-7 Encl. 9). From the present interpretation these seams should be intersected in proposed rotary drill hole #29 at a depth of 75 and 95 meters.

There is another reverse fault called the Far Eastern Fault, which strikes N 55° W and dips 75° NE at 280 meters east of Eastern Fault or about 600 meters west of Fisher Creek. This fault gives the effect of a step fault and Gething-Moosebar contact repeats again.

East of the Noman Creek anticline is the Fisher Creek syncline. Its axis runs east of Fisher Creek and strikes N 35° W. Its west limb dips 30° while the east limb dips 50°. This syncline is entirely of Moosebar formation. About 7 kilometers north of the John Hart highway, the Gething formation outcrops on the west limb.

East of the Fisher Creek syncline and Fisher Creek, the Cadomin formation including some coal up to one meter thick, is exposed with steep dip towards the west.

A3/AQb.24

5 - 3

In the area of trench #W.17 the strike and dip of the formation suddenly changes to N 59° E and dipping 50° to 58° N.W. (see Encl. #7-2 and 10 - Trench #W-17). The abrupt change in the attitudes of the strikes may be due to faulting or some structural change which is not known at the present time.

### 5.2 Coal Geology

In the area under consideration only the Gething formation is prospective for coal. Coal seams have been reported in the Cadomin formation but these are not thought to be economically feasible.

The coal bearing Gething formation can be divided into three zones. The upper, middle, and lower Gething. A small marine fauna collected in-situ, about 46 meters below the top of the Gething formation at Fisher Creek area indicates marine conditions of its deposition. However, in the north (Peace River) and south (Sukunka River) areas, and Pine River, prime coal zones - Superior-Trojan Zone and Chamberlain-Skeeter Zone - lie within the upper 60 meters of the Gething formation.

There are four coal seams exposed in trench #E-7 (Encl. 7-1 and 11-7) just east of the Gething and Moosebar contact varying in nhickness from 2.8 - 5.2 meters. These seams could be equivalent

to the Chamberlain or Trojan seams but neither the continuity nor the stratigraphic position has been established at the present time.

The second and main coal bearing horizon is approximately 150 meters below the first zone and finally, the third zone is about 100 meters below the second zone.

In Noman Creek area two major coal seams #76 and 78 were recognized by previous drilling and exploration (McKechnie 1948-51 and Brameda 1964). Their stratigraphic depth below the top of the Gething averages about 168 meters for seam #78 and 200 meters for seam #76. Stratigraphic separation betwen 78 and 76 is maintained at approximately 30 meters. There are some other minor seams which have a tendency to thicken towards the northwest. The main seams in the area are:

	Depth Below Moosebar-	Interval	Thickness
Seam	Gething Contact	(Meters)	(Meters)
60	50 - 75 m		0-1.6
78	165 – 175 m	115-125	1-4
76	200 m	25-35	4-6
40	246 m	40	0-1
39	275 m	35	0-1.5

The intervals and thicknesses of seams depend on the correlation. At present the correlation of these seams is a problem due to complicated structure, thick overburden, lack of outcrops and no down hole electric logs from previous diamond drill holes.

Seam 60 varied considerably in its thickness and continuity in the area. The seam is mostly dirty and dull coal.

Seams 78 and 76 are estimated to be within the second zone (Encl. 5). Seam 78 has a tendency to vary in thickness from 1-4.2 meters and has breaks in continuity. This could be due to miscorrelation. This is a fairly clean coal with an average ash content of 7% and volatiles of 25.8% (McKechnie, 1951) and on an air-dried basis (Table IV).

Seam 76, the most important seam, has a maximum known thickness of 7 meters and an average thickness in its main bench of 4.7 meters. It has the greatest continuity in the area (Encl. #4, and Encl. 9-1 to 9-12). The Pine Pass Coal Company drove an adit into this seam and the results on an air-dried basis are, on a 76% yield: an average ash of 5%; volatile of 23% and an F.S.I. of 8 (Table V). The quality results look very encouraging.

A3/AQb.27

5 - 6

TABLE	I۷
-------	----

·· ··

--- --- -

HOLE NO.	THICKNES			V.11.		<u> </u>	HEAT VALUE
"Seam 78	" Feet	¢; /6	%	6, /6	%	%	BTUAD.
P.R. 7	1	58	3.8	26.5	69.7	0.9	15,030
P.R. 8	2	37	15.5	22.3	62.2	1.0	13,110
P.R. 14	2	55	1.5	22.2	76.0	0.7	15,200
P.R. 19	3	33	7.2	29.9	62.9	0.8	14,270
P.R. 21	4	32	6.8	27.5	65.7	0.7	14,230
P.R. 22	10	43	7.6	26.9	65.5	0.5	14,010
"Seam 76	<b>5</b> 5						
P.R. 14	5	26	6.3	20.9	72.8	0.7	14,420
P.R. 16	10	44	2.5	23.1	74.4	0.4	15,070
P.R. 17	15	41	2.4	25.2	75.1	0.4	15,080
P.R. 18	22	22	5.0	20.5	74.5	0.7	14,810
P.R. 19	6	100	9.8	26.9	63.5	0.4	13,590
P.R. 20	21	31	11.9	20.8	60.1	0.5	13,070
P.R. 22	10	35	3.3	22.4	74.3	0.4	14,930
P.R. 23	2	33	13.3	28.0	58.7	0.6	12,720

ANALYSES OF DRILL CORE COAL SAMPLES BY MCKECHNIE (1955) OF NOMAN CREEK AREA

- -- -- ...

\* taken from B.C. Dept. of Mines, Bulletin No. 36 - p. 28

2

	TOP 8 As Rec'd %	FEET Air Dried %	BOTTOM As Rec'd %	8 FEET Air Dried %	COMPOSIT AIR DRIED %
lioisture					
Total	5.4		4.7		
Inherent	0.71	0.74	0.64	0.67	0.70
Surface	4.70		4.10		
Ash	15.34	16,10	19.27	20.09	18.07
Volatile	19.73	20.70	17.37	18.11	19.30
Fixed Carbon	59.52	62.46	58.62	61.13	61.93
Sulpher	0.63	0.66	0.57	0.59	0.63
BTU/LB	12,721	13,348	12,202	12,724	13,024
F.S.I.	-	6 1/2	-	7	7

1	'ABL	E	V
1	ADL		v

--- ---

PINE PASS COAL CO. - BULK SAMPLE - SEAM 76

SINK FLOAT TEST AT 1.50 S.G.

.

	TOP 8 FEET	BOTTOM 8 FEET
Yield	72.28	79.75
Ash	5.30	4.60
Volatile	22.01	24.18
F.S.I.	8.00	8.00

Seams 39 and 40 are discontinuous and too deep to be of any significance and contribute very little to the coal reserves at the present time. Seams 39 and 40 vary in thickness from 0.5 to 2.5 meters and 0.3 - 2.0 meters respectively, but these thickenings could be due to structure.

Structural thickening of some of the coal seams was also noticed (see about 150 meters west of trench #W2, and Encl. 9-4). A coal seam occurs in the core of an anticline which is thickened by structure. It is also noticed in trench #W15 and W16.

A3/AQb.28

#### 5.3 Coal Reserves

The in-situ coal reserves were estimated by using geological and structural cross-sections (Encl. 9-1 to 9.12). These cross-sections are prepared perpendicular to the average strike of formation using all the information collected from diamond drill holes, trenches and outcrop. The locations of these cross-sections are marked on the geological maps (Encl. 7-1 and 7-2).

To make the reserve calculations, the following factors are taken into consideration:

- a) A specific gravity of 1.60 for the coal was used.
- b) It is calculated for the total strike length of 3360 meters and the total depth of 50 meters to about 200 meters. At places the bottom of Seam 76 is taken into consideration. The pit area is marked on the sections as Limit of Pit.
- c) The middle point of the strike length of two sections is taken as length of influence for each section.
- d) Areas occupied by coal seams 76 and 78, and waste material between seams have been scaled by using planimeter. This area is multiplied by the strike length influenced by each section.

The preliminary estimates indicate some 25 million metric tonnes open pit mineable geological in place reserves at 4.6 bank cubic meters per tonne overburden ratio (see Table #VI).

#### 5.4 Mineability

These coal seams are exposed in a quasi-dip slope situation amenable to open pit mining with about 4.6:1 overburden ratio.

One of the main advantages of the area is the proximity of the railway, the paved highway and the town of Chetwynd. The railway and highway run through the middle of the Crows Nest licences as does the power line. This is a distinct advantage for any coal property as one of the major problems common to many is the need of many miles of railway.

Another advantage is the town of Chetwynd, connected to the area by all-weather paved highway. Chetwynd could be used as a townsite for persons working at the mine. These factors make a considerable difference to the economics of operating a coal mine.

### TABLE VI

ŧ

----

- ----- -

.

-----

#### RESERVE CALCULATIONS

WEIGHTED RATIOS

AND

TOTAL RESERVES (ESTIMATED)

SECTIONS 1 TO 12

.

PINE PASS PROJECT

CROWS NEST RESOURCES LIMITED

1

#### Combined East & West Pit Ratios

Combined Weighted =  $\frac{(5.29 \times 3722416) + (2.45 \times 1247840)}{3,722,416 + 1,247,840}$ 

Combined Weighted Ratio = 4.58:1

ŕ

SECTIONS	6	 12	

SECTION	TONNAGE (METRIC)	O/B VOLUME (M <sup>3</sup> )	STRIPPING RATIO	TONNAGE X RATIO
6	1,856256	11,849,520	6.38:1	11,842,913.0
7 Pit 1	1,354,680	8,671,940	6.40:1	8,669,952.0
Pit 2	2,016,400	11,296,100	5.60:1	11,291,840.0
8	410,400	1,795,500	4.38:1	1,797,552.0
9	2,115,480	9,435,000	4.46:1	9,435,040.8
10 Pit 1	4,008,960	19,336,800	4.82:1	19,323,187.0
Pit 2	635,520	1,440,000	2.27:1	1,442,630.4
11	6,596,000	24,079,765	3.65:1	24,075,400.0
12	694,896	2,271,857	3.27:1	2,272,309.9
=	19,688,592			= 90,150,823.0

Weighted Ratio =  $\frac{90,150,823.0}{19,688,592.0}$ 

Weighted Ratio = 4.58:1

TOTAL RESERVES WEIGHTED RATIO: SECTION 1 - 12
$= \frac{(4.58 \times 19,688,592 + 4,48 \times 4,970,256)}{19,688,592 + 4,970,256}$
$= \frac{90173751 + 22763772}{24658848} = \frac{112,937,523}{24658848}$
Total combined weighted average ratio = $4.58.1$
TOTAL COAL RESERVES = $24,658,848$ metric tonnes @ SPG = 1.60 (ESTIMATED) Sections 1- 12
TOTAL WASTE VOLUME = $113,178,990 \text{ m}^3$ (ESTIMATED)
AVERAGE STRIPPING RATIO = $4.58:1$

SECTION	TONNAGE (METRIC)	O/B VOLUME (M <sup>3</sup> )	STRIPPING RATIO	TONNAGE X RATIO
1	585,600	2,385,927	4.07:1	2,383,392
2	465,840	2,262,150	4.85:1	2,259,324
3	557,632	3,360,000	6.02:1	3,356,944
4	870,144	4,125,825	4.74:1	4,124,482
5	1,243,200	7,597,765	6.11:1	7,595,952
X	= 3,722,416			≈ = 19,720,094

WEST OF NOMAX CREEK FAULT: SECTIONS 1 - 5

- ----

Weighted Ratio = ≍(Tonnage x Ratio) ≍ Tonnage

Weighted Ratio =  $\frac{19,720,094}{3,722,416}$  m<sup>3</sup> =  $\frac{5.29:1}{5.29:1}$ 

۱

EAST	OF	NOMAN	CREEK	FAULT:	SECTIONS	2	 5

SECTION	TONNAGE (METRIC)	O/B VOLUME (M <sup>3'</sup> )	STRIPPING RATIO	TONNAGE X RATIO
2	120,960	512,000	3.02:1	365,299
3	169,600	742,500	6.14:1	1,041,344
4	258,720	922,350	3.57:1	923,630
• 5	592,000 <sup>pi</sup>	t <sup>1</sup> 779,641	1.32:1	769,600
	106,560 <sup>pi</sup>	<sup>t 2</sup> 316,350	2.97:1	316,483
Σ =	= 1,247,840			¤ = 3,051,057

Weighted Ratio =  $\frac{3,051,057}{1,247,840}$  m<sup>3</sup> =  $\frac{2.45:1}{2.45:1}$ 

						· . :			
}ECT10N	N SEAN NO.	STRIKE LENCTH (M)	COAL AREA . (M <sup>2</sup> )	COAL VOLUME (M <sup>3</sup> )	E COAL TONNAGE (METRIC)	O/B AREA (M <sup>2</sup> )	O/B VOLUME (M <sup>3</sup> )	STRIPPING RATIO	REMARKS *SPG = 1.60*
, <u></u>	Upper Coals	425	945	401,625	642,600	3700 <sup>1</sup>	1,572,500		1. OB Surface to Bottom of Upper Coals
	Hiddle Coals	425	845	359,125	574,600	2600 <sup>2</sup>	1,105,000		2. OB Between 76 and Bottom of Middle Coals
x	78	425	300	127,500	204,000	10400 <sup>3</sup>	4,420,000		3. OB Surface to top of 78
	76	425	821	348,925	558,280	4050 <sup>4</sup>	1,721,250		4. OB Between 78 & 76
	Lower Coals	425	200	85,000	$\frac{136,000}{2,115,480}$	1450 <sup>5</sup>	<u>616,250</u> 9,435,000		5. OB Surrounding Lower Coals See Section 9 For Seam Location
10	Upper Coals	600	1820	1,092,000	1,747,200	22500 <sup>1</sup>	13,500,000		1. OB Surface to Top 78
Pit 1	78	600	785	471,000	753,600	6800 <sup>2</sup>	4,080,000		2. OB Between 78 & 76
	76	600	1571		$\frac{1,508,160}{4,008,960}$	2928 <sup>3</sup>	$\frac{1,756,800}{19,336,800}$	4.82:1	3. OB Beneath 76 (to maintain pitwall angle)
10 Pit 2	?	600	662	397,200	635,520	2400	1,440,000	2.27:1	Unidentified Coal Seams East of 76 Outcrop
,11	?	485	8500	4,122,500	6,596,000	49649	24,079,765	3.65:1	Unidentified Coal Seams (Combine Areas)
12	?	310	1401	434,310	694,896	7328	2,271,857	3.27:1	Unidentified Coal Seams (Combin Areas)

.

șect lon	SEAM NO.	STRIKE LENGTH (M)	COAL AREA (M <sup>2</sup> )	COAL VOLUME (M <sup>3</sup> )	COAL TONNAGE (METRIC)	O/B AREA (M <sup>2</sup> )	O/B VOLUME (M <sup>3</sup> )	STRIPPING RATIO	REMARKS *SPG = 1.60*
5 (west)	78 76	185 185	1500 2700	277,500 499,500	444,000 799,200 1,243,200	27141 13928*	5,021,085 <u>2,576,680</u> 7,597,765	6.11:1	West of Noman Creek Fault only does not include coal above 78 or below 76 *Area O/B between 78 & 76
5 (east)	76 Pit 2 Coal	185 185	2000 360	370,000 66,600	592,000 106,560	4214 1710	779,641 316,350	1.32:1 2.97:1	East of Noman Creek Fault only see section 5 for Pit 2 location Seams numbers are unidentified
6	78 76	240 240	1906 2928	457,440 702,720	731,904 1,124,352 1,856,256	30535 18838*	7,328,400 4,521,120 11,849,520	6.38:1	Includes coal west and east of Noman Creek Fault Area of O/B between 78 & 76
7 Pit 1	78 76	355 355	1071 1314	380,205 466,470	608,328 <u>746,352</u> 1,354,680	14571 9857*	5,172,705 3,499,235 8,671,940	6.40:1	West Limb of Syncline does not include coal other than 78 & 76 *Area of O/B between 78 & 76
7 Pit 2	78 76	355 355	750 2800	266,250 994,000	426,000 <u>1,590,400</u> 2,016,400	26000 5820*	9,230,000 2,066,100 11,296,100	5.60:1	East Limb of Syncline (both side of NC Fault) Includes split of seam 76 *Area of O/B between 78 & 76
8	78 76 40	285 285 285	150 600 150	42,750 171,000 42,750	68,400 273,600 <u>68,400</u> 410,400	2000 1420* 2880**	570,000 404,700 <u>820,800</u> 1,795,500	4.38:1	West Limb of Syncline *Area of O/B between 78 & 76 **Area of O/B between 40 & 76

ì

RESERVE CA LATIONS

.

- - - - -

( ) }

SECTION	SEAM NO.	STRIKE LENGTH (M)	COAL AREA (M <sup>2</sup> )	COAL VOLUME (M <sup>3</sup> )	COAL TONNAGE (METRIC)	O/B AREA (M <sup>2</sup> )	O/B VOLUME (M <sup>3</sup> )	STRIPPING RATIO	REMARKS *SPG = 1.60*
1	78 76	120 120	1400 1650	168,000 198,000	268,800 <u>316,800</u> 585,600	12850 7015*	1,542,091 <u>841,836</u> 2,383,927	4.07:1	West of Noman Creek Fault only does not include coal above 78 or below 76 *Area of O/B between 78 and 76
2 (west)	78 76	90 90	1520 1715	136,800 154,350	218,880 246,960 465,840	17170 7965*	1,545,300 716,850 2,262,150	4.85:1	West of Noman Creek Fault only does not include coal above 78 or below 76 *Area of O/B between 78 and 76
2 (cast)	78 76	90 90	200 640	18,000 57,600	28,800 92,160 120,960	6500 1750*	585,000 <u>157,500</u> 742,500	6.14:1	East of Noman Creek Fault only does not include coal above 78 or below 76 <u>*Area of O/B between 78 and 76</u>
3 (west)	78 76	100 100	1150 2350	115,000 235,000	181,632 <u>376,000</u> 557,632	20500 13100*	2,050,000 1,310,000 3,360,000	6.02:1	West of Noman Creek Fault only does not include coal above 78 or below 76 *Area of O/B between 78 & 76
3 (east)	78 76	100 100	210 850	21,000 \$ 85,000	336,000 <u>136,000</u> 169,600	4050 1070*	405,000 <u>107,000</u> 512,000	3.02:1	East of Noman Creek Fault only does not include coal above 78 or below 76 *Area of O/B between 78 & 76
4 (west)	78 76	165 165	1000 2296	165,000 378,840	264,000 <u>606,144</u> 870,144	15025 9980*	2,479,125 <u>1,646,700</u> 4,125,825	4.74:1	West of Noman Creek Fault only does not include coal above 78 or below 76 *Area of O/B between 78 & 76
4 (east)	78 76	165 165	100 880	16,500 145,200	26,400 232, <u>320</u> 258,620	290 5300*	47,850 <u>874,500</u> 922,350	3.57:1	East of Noman Creek Fault only does not include coal above 78 or below 76 *Area of O/B bewteen 78 & 76

McKechnie sampled intersections of drill core from seams 76 and 78 for proximate analysis. The results of these analyses are given in Table #IV.

Based largely on the results of this McKechnie work, Pine Pass Coal Company Ltd. acquired coal licences in the area 1968 and drove an adit into seam 76, adjacent to the highway, for a length of 36.5 meters and then cross-cut to obtain bulk samples. At the sampling point the seam had a true thickness of 4.8 meters. This sample was analyzed by Warnock-Hersey. For results see Table V.

The result of this was most encouraging and suggested that seam 76 may, in fact, be an excellent coking coal.

During the summer of 1980, 30 backhoe trenches were cut and 46 channel samples were collected from exposed seams including 76 and 78 seams. These samples were sent to Crows Nest Laboratory, Fernie, B.C. (for results see Table VII).

This analysis indicated that the percentage of ash and volatile matter is almost constant ranging from ash 6% - 11% and volatile 28% - 32% on an air-dried basis. This percentage of volatiles is

-

						TABLE VII								
	SAMPLE NO.	TRENCH NO.	THICKNESS METERS	RAW AS RECEIVEI MOISTURE %	BIAS ASH %	CLEAN FLOAT AT YIELD %	SG 1.6 I.M. %	ASH %	v.m. %	F.Ç. %	AIR DR ASH %	IED BIAS V.M. %	F.C. %	VM DMM
C -704 :713 .722 .723 .724	2 1 1	BELOW SEAM W1 W10 W15 W15 W15 W15	76 4.2 0.3 1.7 2.5	2.68 1.97 0.93 2.13 2.99	35.91 37.64 87.05 54.17 15.71	50/ 37 0 20 66	2.89 2.83 2.91 2.33	7.47 12.07 12.02 6.23		59.58 57.70 54.76	7.69 12.36 12.38 6.38	30.95 28.57 31.22	61.36 59.07 56.40	33.5 32.6 35.6

• - ,,	· · · · · · · · · · · · · · · · · · ·			-		TABLE VII	•			•				
	•				<u>-</u>	COAL QUALLTY	~							
								<u>.</u>			1	<u> </u>	<u> </u>	
r r	SAMPLE RO.	TRENCH NO.	THICKNESS METERS	RAW AS RECEIVE MOISTURE . %	D BIAS ASH %	CLEA FLOAT AT YIELD %	N SG 1.6 I.M. %	ASH %	V.M. %	F.C. %	AIR DF ASH %	RIED BIAS V.M. %	F.C. %	VM DMMI
SEA	SEAN 78 con't													
730	4D	W15	0.6	1.11	89.07	0								
.731	4E	W15	1.1	4.21	34.19	51	3.32	· 8.62	30.64	57.42	8.92	31.69	59.39	34.8
•738	2	TW18	3.2	2.98	48.03	32	3.56	10.78			11.18	1		
						1								
	AM 76	<b></b>					0.05	1. 5. 60	20.15		F 70	20.07	60.05	
:698	1	E1	8.4	4.05	26.98	56	2.65	5.62	30.15	61.58	5.78	30.97	63.25	32.9
3699	1	E2	4.6	3.30	43.52	41	4.03	10.92	1	l	11.38	3		
700	I	E3	3.1	4.98	16.01 38.77	72	3.85 4.02	6.85	30.50	54.17	11.78	31.78	56.44	36.0
+701 +702	,	E6 TE5	8.5 3.5	4.21 4.39	32.39	49	4.02	8.77	30.50		9.15	51.70	50.44	50.0
702 1703	2	TE5	3.3 4.7	4.59	22.00	59	4.10	9.40			9.80			
705		W2	4.7	1.09	88.28	0 0	4.00	9.40		t t	89.26			
710	2	N7	4.4	3.19	15.94	69	3.44	6.97	30.42	59.17	7.22	31.50	61.28	34.0
-711		W8		2.07	35.92	47	2.91	6.80	50112		7.01	}		
-714	1A	W11	2.3	3.17	31.76	46	2.17	9.36		]	9.57	1	ł	
r715	1 B	W11	1.9	1.51	76.17	9	3.23	10.75			11.11			
-716	10	W11	3.0	3.51	21.28	59	2.80	7.08	29.82	60.30	7.28	1	62.04	33.1
-725	3A	₩15	.7	3.30	41.33	26	4.49	11.45	29.22	54.85	11.99	1	57.41	
726	3C	W15	J	4.57	24.65	52	4.34	9.14		ļ	9.56			
737	L	TW18	3,0	4.02	20.53	59	3.61	9.51	29.87	57.01	9.89		59.14	34.4
- <del>-</del> 741	1	TW20	6.7	3.46	47.95	27	2.30	10.31	l		10.55			
-742	2	TW20	2.8	.42	28.80	51	2.52	9.80	į	1	10.05			
- 7.13		W2	3.5	3.76	12.41	81	3.07	7.35	31.82	57.76	. 7.58	32.83	59.59	35.5

· · ····							TABLE VII. COAL QUALITY								
	SAMPLE NO.	TRENCH NO.	THICKNESS METERS	RAW AS RECEIVEI MOISTURE · %	) BIAS ASH %	CLEAI FLOAT AT YIELD %	N SG 1.6 I.M. %	ASH %	v.M. %	F.C. %	AIR DR ASH %	IED BIAS V.M. %	F.C. %	VM DMMF	
1 1	AL SEAMS A	BOVE SEAM	78										}		
718		W12	2.0	2.52	22.09	64	3.33	7.74			8,01				
719	1A	W14	2.7	1.56	60.85	17	3.15	9.99	28.27	58.59	10.31	29.19	60.50	32.5	
720	18	W14	0.7	4.67	27.53	58	3.95	9.12			9.49				
721	IC	W14	2.3	2.66	32.99	50 (1)	2.52	8.85	•		9.08	[	[	· ·	
732	5	W15	1.0	4.69	16.07	68 59	2.46	8.96		)	9.19				
733	6	W15	4.0	5.17	22.64		2.15	. 7.06	20.1/	50.00	7.22	30.83	60.36	33.8	
·734	1	W16	6.7	3.13	22.12	60	2.23	8.61	30.14	59.02	8.81	30.03	00.30	33.0	
·735		W17	3.1	3.79	14.86	72 26	3.57	7.97		11.26	0.27	ļ			
·736 ·739	2	W17 TW18	1.5 3.2	2.28	50.98 29.66		3.48	10:87 8.81		11,20	9.07			[	
•740	4	TW18	3.1	4.69	29.00	67	2.80	9.21	28.88	59.02	9.48	29.74	60.78	32.9	
744	ч   1	S29	1	1.75	7.68	88	1.84	4.84	20.00	39.02	4.93	25.14	00.70	52.5	
744	1	329	L L	1./5	7.00	.00	1.04	4.04			4.95	ļ	Į		
A SE	лм 78												1	ļ	
· 705		W2	3.0	2.80	36.32	46	2.59	9.19			9.44				
+707	-	W6	3.7	3.98	36.88	1	3.84	10.25	32.25	53.66	10.66	33.54	55.80	37.5	
-708	2	W6	1.3	2.55	44.41	33	4.04	11.01		-	11.48			ļ	
<b>₹</b> 709		W7		1.99	44.62		3.25	8.03		} ·	8.58	ł			
712		W9	2.3	2.03	24.24	59	1.69	5.81			5.91				
; -/17	2	WLI	2.5	2.91	22.38	69	1.96	5.50		ĺ	5.62				
£727		W15	1	3.46	20.01	65	3.85	9.35	28.98	57.82	9.73	30.14	60.13	33.4	
- 728		W15	0.8	0.73	85.03	1 .									
=729	i	WI 5	3.0	2.34	41.06		· 2.02	8.54			8.72				
	F E			κ.					,					ļ	

expected as these samples are from shallow depths and thus have been oxidized. Therefore, it really does not give a true idea of the quality at the present.

Analysis of the 1980 backhoe trench samples (Table VII) did not significantly change the quality picture put forward by previous operators (Tables IV and V).

## 6.0 WILLOW CREEK AREA

#### 6.1 Location

The Willow Creek area is located immediately northeast of Falls Mountain and bounded to the northwest by the Pine River. Willow Creek flows through the middle of the property along a northwest course.

#### 6.2 Previous Work

The area was mapped in detail at a scale of 1:9600 during the period of 1948 to 1951 by N.D. McKechnie. In addition, he drilled 39 diamond drill holes totalling 25,447 feet in which coal intersections were sampled and analyzed. McKechnie calculated geologic in place coal reserves of 23.8 million short tonnes. However, if all seams averaging thinner than 1.5 meters are excluded from this calculation reserves decline to 21.5 million short tonnes. McKechnie's calculations for coal reserves are affected greatly by problems in resolving seam correlation and continuity of seams. McKechnie (1955) reported nine coal seams of commercial thickness but stated that these seams were lenticular and discontinuous.

#### 6.3 Work Done in 1980

During the summer of 1980 only a reconnaissance geological mapping program at a scale of 1:10000 could be carried out due to lack of time and shortage of crew.

### 6.4 Stratigraphy and Structure

The Willow Creek area is underlain by the coal bearing Gething Formation of the Bullhead Group. This formation is overlain by the Moosebar and Commotion Formations of the Fort St. John Group. Both of these groups are of Lower Cretaceous age.

The structure of the area is complicated by the southeast shallow plunging 10°, Pine River anticline. Willow Creek more or less follows the axis of this anticline. Numerous faults, both reverse and normal, are known also to cut the anticline at the crest and the limbs. The Willow Fault is a normal fault that apparently cuts the thrust faults, thus it is believed to be of younger age. Displacement on the Willow Fault is thought to be approximately 180 meters of dip slope movement. Strike slip movement has not yet been proven.

A3/AQ5.34

Coal bearing Gething strata outcrop on both limbs of this anticline with dips of 25° - 35°. These strata are overlain by Moosebar shales and on the west limb by younger sequences. On the southwest limb (Falls Mountain), there is an outlier of Commotion Formation which is the dominant feature approximately 150 meters thick with less than 10° southwesterly dip. Falls Mountain is a large, almost flat-topped mountain which stands about 460 meters above the surrounding area. Its gently dipping top is about 5 kilometers long and 1.5 kilometers wide. No rocks older than the Gething Formation have been noticed in the axis of the Willow Creek anticlinorium.

The change of dips between the underlying Gething and overlying Moosebar and Commotion may be possibly due to the change of relative competencies of the rocks. The Gething is a more competent sequence overall than the incompetent shales of the Moosebar. Thus, tectonism which folded and faulted the Gething Formation was absorbed by the Moosebar shales. This absorption of tectonic activity left the overlying Commotion relatively flat lying and homogenous.

A3/AQb.35

6 - 3

### 6.5 Coal Geology

The Gething Formation is the only coal bearing strata which contains economically mineable coal in the area. The Commotion group does contain coal, except in the marine Moosebar member, but no thick seams have been reported north of the Sukunka region.

In the Peace River region, the Trojan zone appears within the upper 60 meters of the Gething. This upper sequence is prospective elsewhere and may hold the same potential in the Willow Creek area. However, the Gething represented in Willow Creek is not yet defined as upper, middle or lower Gething. No comprehensive study into which stratigraphic horizon is represented has been done as of yet.

The nine seams reported by McKechnie are of variable thickness from 1.2 to 3.5 meters. He reports also that these seams may be discontinuous and lenticular. Seams stratigraphically lower than those reported by McKechnie have never been investigated. Thus, the potential of finding more coal reserves lower than those known may exist.

The coal is probably best mined by open pit techniques due to the structural complexity of the ground. Underground mining potential does still exist if a relatively thick continuous seam could be found. However, present seams are thin and show local complexity in structure. The relationship of topography and stratigraphy in the identification of open pit targets has also never been performed in the Willow Creek area. Dip slope or quasi-dip slope mining situation may exist if the structure could be proved.

### 6.6 Conclusions and Recommendations

To define further coal reserves and the structure of the property further work must be performed.

This can be done by relatively inexpensive exploration methods of mapping, trenching, compilation and evaluation of all available information, old and new. Mechanical exploration such as diamond drilling would follow if and when warranted from future work.

### 7.0 FALLING CREEK - BEAUDETTE CREEK AREA

### 7.1 Location

The Falling-Beaudette Creeks area is located to the immediate west of Falls Mountain, on the south side of the Pine River Valley. Falling Creek traverses through the middle of the area and Beaudette Creek runs through the southwest licences.

## 7.2 Previous Work

Very little in the way of serious exploration has been performed on the Falling Creek-Beaudette Creek area. Pan Ocean did drill three diamond holes south of the Shell licences. Two holes were located immediately south of the licences and one some 1-1/2 miles upstream towards the south. The purpose of these holes was to intersect possible coal sections within the Gething by drilling through the upper Moosebar. One hole failed to intersect the Gething.

#### 7.3 Work Done in 1980

Reconnaissance geological mapping was carried out in the Falling Creek valley and along the west ridge. More detailed work could not be completed due to shortage of time and crew.

7 - 1

### 7.4 Geology

The area is mainly underlain by the Moosebar formation of the Fort St. John Group along the Falling Creek valley. Towards the west of the valley, a high ridge is underlain princi by steeply dipping Gething formations and possibly older formations of the Bullhead succession of Lower Cretaceous age.

#### 7.5 Structure

The structure of the area is complex as indicated by the highly variable dips in the Moosebar formation along Falling Creek. A traverse of Beaudette Creek reveals many folds and faults in Gething and older Bullhead Group rocks. In many places, beds of these formations are vertical or overturned.

#### 7.6 Coal

The occurrence of economically viable coal seams have not been noticed in the Falling Creek valley due to the extensive outcropping of Moosebar shales. In view of the reported thickness of Moosebar formation and the relative elevation of the Commotion formation on Falls Mountain, it is possible that the Gething formation is covered by a thin layer of Moosebar in Falling Creek. However, the holes drilled in 1975 by Pan Ocean, to a depth of more than 900 feet failed to intersect the Gething Moosebar contact. The hole was located 1-1/2 miles upstream from the Shell licences bottomed out in Moosebar.

Pan Ocean drilled two other diamond holes on the west side of Falling Creek immediately southwest of the southeast end of Falls Mountain which intersected the Moosebar-Gething contact dipping to the southwest. About 1000 feet of Gething section was tested. These holes intersected two coal seams at 150 feet and 750 feet below the Moosebar-Gething contact with true thicknesses of about 12 and 27 feet respectively. The lower seam has a three-foot mudstone parting.

The analysis on 1/4" x 28 m fraction floated at 1.45 S.G. was as follows:

Seam No.	Yield	<u>Ash</u>	F.S.I.
1	91.3%	3.6%	1-1/2
2	81.4%	2.9%	1-1/2
Lower Part Seam 2	79.9%	2.3%	8-1/2

The F.S.I. of the lower portion of the seam is interesting. The excellent yield-ash characteristics of all coal intersections are noteworthy.

7 - 3

Although the structure of the Gething formation along the west side of Falling Creek is complex, a potential of finding more coal exists. Especially 'in Beaudette Creek an excellent possibility of discovering workable seams exists in the immediate vicinity.

## 7.7 Conclusions and Recommendations

Refer to Willow Creek area Conclusions and Recommendations (Section 6.6).

A3/AQb.41

ı

### 8.0 RECOMMENDATIONS FOR FURTHER WORK

The result of the exploration work carried out during 1980 is very encouraging. This work includes about 25 million metric tonnes of geological in place coal with a ratio of overburden to coal 4.5:1. It is economically feasible to mine open pit.

The structural and correlation problems are still unresolved. There are still unexplored areas left to find more reserves of coal and previous evaluations of coal reserves and coal quality to be confirmed. Therefore, further exploration work is recommended.

- Additional trenching of 3800 meters to test continuity of coal seams and expose the structure.
- 38 rotary drill holes by drilling 3750 meters and down hole logging to prove reserves and correlation of seams.
- Build new roads of 4800 meters as an access to drill sites and also expose the geology if possible.
- 4. Additional mapping to resolve the structural problems and to find new horizons of coal in the Gething formation.
- 5. There is a dire need for core samples. Continuous core (diamond) drilling is, however, recommended to be postponed to 1982 when most of the structural problems are resolved. This more expensive drilling would be better utilized then.

# **BIBLIOGRAPHY**

-

1

Alberta Stud		Lower Cretaceous of the Peace River Region; Western Canada Sedimentary Basin, Rutherford Mem. Vol; Am. Assoc. Petrol. Geol., Tulsa, Okla.
Dickson, J.	1948:	Analyses of British Columbia Coals; B.C. Department of Mines, Bull. 14.
Dowling, D.H	3. 1915a:	Coal Fields of British Columbia; Geol. Surv. Can., Mem. 69-
	1915b:	The Cretaceous Sea in Alberta; Trans. Roy Soc. Can., 3rd ser., Vol. 9, Sec. 4, pp. 27-42
Dyson, P.	1979:	Pine Pass Area, B.C. For Shell Canada Resources Ltd. Calgary, Alberta March 1979
Eric, P.	1979:	Report on Coal Licences Peace River Land District, British Columbia December 29, 1979
Fitzgerald,	H.L. 1968:	Structure of British Columbia Foothills, Canada, Bull. Amer. Assoc. Petrol. Geol., Vol. 52, No. 4, pp. 641-664.
Hage, C.O.	1944:	Geology adjacent to the Alaska Highway between Fort St. John and Fort Nelson, British Columbia; Geol. Surv. Can., Paper 44-30.
Hughes, J.E	1964:	Jurassic and Cretaceous strata of the Bullhead succession in the Peace and Pine River Foothills; B.C. Dept. Mines and Petrol. Res., Bull. No. 51.
	1967:	Geology of the Pine Valley, Mount Wabi to Solitude Mountain, northeastern British Columbia; B.C. Dept. Mines and Petrol. Res., Bull. No. 52.
McLean, F.H	. & Irish, E.J.W. 1944:	Some coal deposits of the Peace River Foothills, British Columbia; Geol. Surv. Can., Paper 44-15
McLearn, F.	H. & Kindle, E.D. 1950:	Geology of Northeastern British Columbia; Geol. Surv. Can., Mem. 259.

-

•

McKechnie,	N.D. 1955:	Coal Reserves of the Hasler Creek-Pine River Area; B.C. Dept. of Mines, Bull. 36.
Muller, J.E	1961:	Pine Pass, British Columbia; Geol. Surv. Can., 'Map 11-1961.
Nicolls, H.	H.H. 1952:	Analyses of Canadian Coals and Peat Fuels; Mines Branch, Pub. #831.
Spivak, J.	1944:	Geology and Coal Deposits of Hasler Creek Area, British Columbia, Geol. Surv. Can., Paper 44-7.
Stott, D.A.	1960a:	Cretaceous rocks between Smoky and Pine Rivers, Rocky Mountain Foothills, Alberta and British Columbia; Geol. Surv. Can., Paper 60-16.
	1961a:	Dawson Creek map-area, British Columbia; Geol. Surv. Can., Paper 61-10.
	1963:	Stratigraphy of the Lower Cretaceous Fort St. John Group, Gething and Cadomin Formations, Foothills of Northern Alberta and British Columbia; Geol. Surv. Can., Paper 62-39.
	1968a: ·	Lower Cretaceous Bullhead and Fort St. John Groups, between Smoky and Peace Rivers, Rocky Mountain Foothills, Alberta and British Columbia; Geol. Surv. Can., Bull. 152, 279 pp.
	1971:	Lower Cretaceous Bullhead Group between Bullmoose Mountain and Tetsa River, Rocky Mountain Foothills, Northeastern British Columbia; Geol. Surv. Can. Open File Report.
Ziegler, W.	H. & Pocock, S.A.J. 1960:	The Minnes Formation: Edmonton Geol. Soc., Second Ann. Field Conf., Guidebook, pp. 43-71.

\*\* \* \*

### CERTIFICATION

I, Gyan Chand Singhai of 5620 Clearwater Drive, Richmond, B.C., do hereby certify that:

- (1) I am a member of the Association of Professional Engineers of British Columbia since 1969, and member of the Canadian Institute of Mining and Metallurgy.
- (2) I am a post-graduate in Applied Geology (1959) from the University of Saugor, Sagar, Madhya Pradesh, India, and have been practising my profession since that time.
- (3) I was teaching in the University of Saugor, Sagar, and Ravishankar University, Raiput in India, and practised my profession in India, Canada, West Indies, Mexico, Peru, U.S.A., Chile, Australia, Indonesia, and Venezuela.
- (4) This report is based on report of working on the property during the period June - August, 1980.

Dated at 901 - 675 West Hastings Street Vancouver, B.C. May 20, 1981

G.C. Singhai, M. Tech. P. Eng.