

PR-RockyCreek 81(1)A

93P14,5

B.P. Canada

Report on the Rocky  
Creek 1981 Exploration  
Program W.E.B.C.

C.L.# 3617, 4029-4032, 4034,

4036-4049, 5244-5278

A. Bowler

Dec 31 1981

620

PR-Rocky Creek  
81(1)A

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**OPEN FILE**

BP EXPLORATION CANADA LIMITED

COAL DIVISION

B. C. Government Report on the  
Rocky Creek 1981 Exploration Program, N.E. B.C.

93 P14.5  
121'45" 55'15"  
Work for 1981 Field Season  
May-August  
Coal Licence Numbers:

(TO BE RETAINED)

|         |                 |                 |                 |                 |                 |                 |                 |      |                  |
|---------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|------|------------------|
| Group A | <del>3617</del> | <del>4034</del> | <del>4036</del> | <del>4040</del> | <del>4041</del> | <del>4045</del> | <del>4046</del> |      |                  |
| Group B | 4037            | 4038            | 4039            | 4042            | 4043            | 4044            | 4047            | 4048 | 4049, 5270, 5272 |
| Group C |                 | 4029            | 4030            | 4031            | 4032            | 5262            | 5263            |      |                  |
| Group D |                 | 5249            | 5250            | 5252            | 5253            | 5254            | 5255            | 5256 | 5257, 5258       |

(TO BE DROPPED)

5268, 5278, 5277, 5276, 5275, 5274, 5273, 5271  
 5267, 5269, 5244, 5245, 5259, 5260, 5261  
 5264, 5265, 5266, 5251, 5248, 5247, 5246

Submitted:

December 31, 1981

A. Bowler

**GEOLOGICAL BRANCH  
ASSESSMENT REPORT**

00 620

BP EXPLORATION CANADA LIMITED

COAL DIVISION

ROCKY CREEK 1981 REPORT

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1. INTRODUCTION

This report has been prepared for presentation to the Coal Administrator of the British Columbia Ministry of Energy, Mines & Petroleum Resources, Victoria, British Columbia and in compliance with the Regulations under the Coal Act of 1974. It describes the exploration program carried out from May to August, 1981, on BP's Rocky Creek property.

The Rocky Creek Coal Project consists of 55 coal licences. All licences have a renewal date of December 31.

The 1981 Rocky Creek Exploration Program, south of Chetwynd, B.C., was conducted as a helicopter supported mapping and core drilling program. This project employed eight BP personnel and contracts were tendered for helicopter services, drilling, geophysical logging, coal analysis, drill site preparation, reclamation, and staff accommodation.

This report should be read in conjunction with BP's application for work credit on the "Application to Extend the term of Licence" forms for the Rocky Creek property, submitted with this report.

LOCATION OF MAJOR COAL PROPERTIES IN ROCKY MOUNTAIN AREA

- CITY / TOWN
- +— EXISTING RAILWAY
- ..... PROPOSED RAILWAY
- - - - PROVINCIAL BOUNDARY
- COAL PROPERTY
- ROCKY CREEK PROPERTY

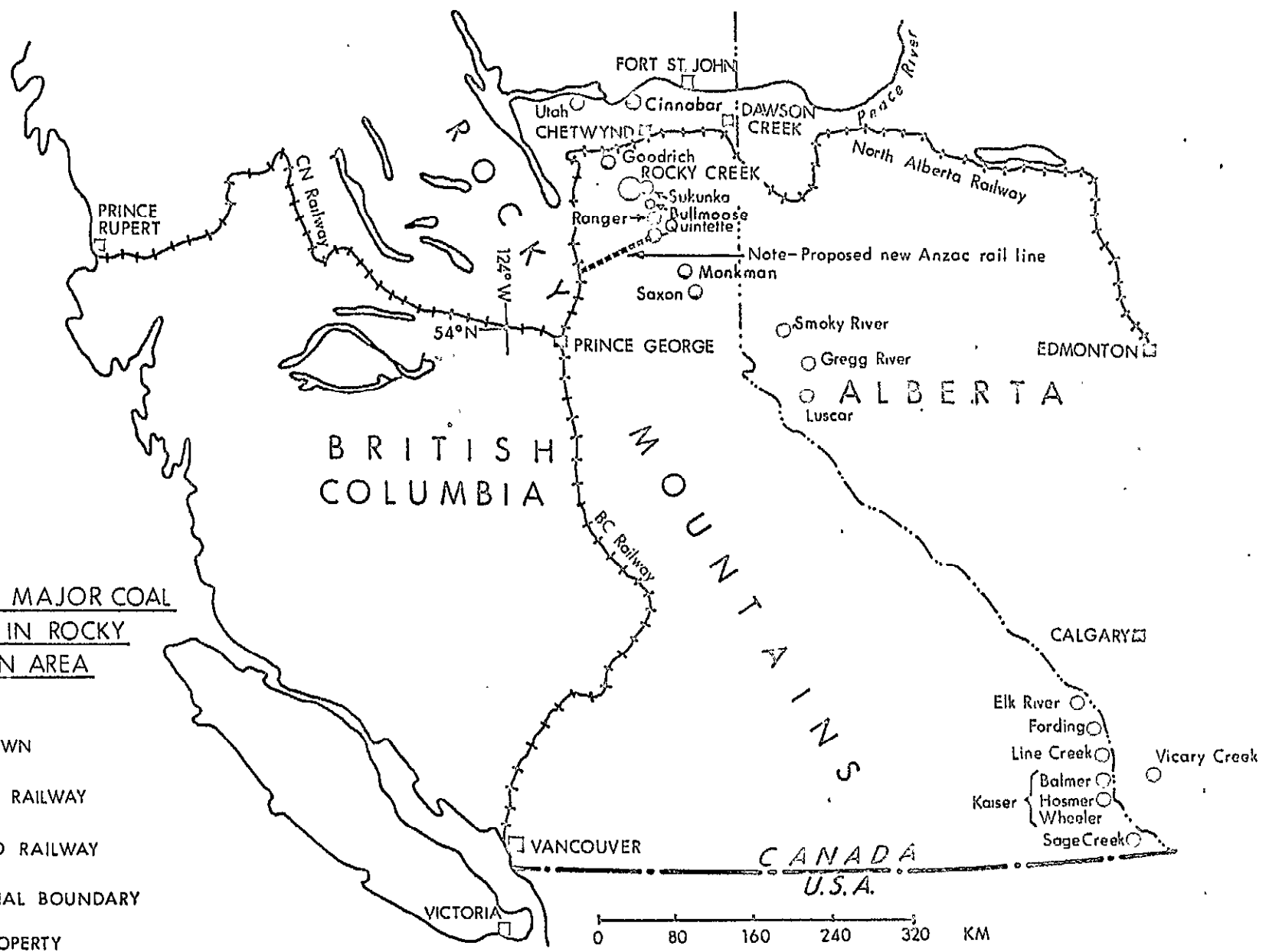


Figure 1

2. LOCATION - ACCESS - TOPOGRAPHY

The Rocky Creek property occupies an area of approximately 16,225 ha located 50 km south of the town of Chetwynd in northeastern British Columbia. Figure 1, illustrates the location of the property, its relationship to other proposed coal developments and to existing and proposed infrastructure in the region.

Access at present is via helicopter from Chetwynd as there is no bridge crossing the Sukunka River south of the Burnt River into the project area. The nearest road access to the property is the Sukunka Valley Rd. located on the east side of the valley, whereas the nearest existing rail line is the British Columbia Railway line which passes through Chetwynd. (Chetwynd is approximately 1,100 km from the ports of Vancouver and Prince Rupert).

The proposed Anzac rail link from near Prince George to the new Tumbler Ridge Townsite will cross the upper Sukunka Valley approximately 60 km south of the Rocky Creek property.



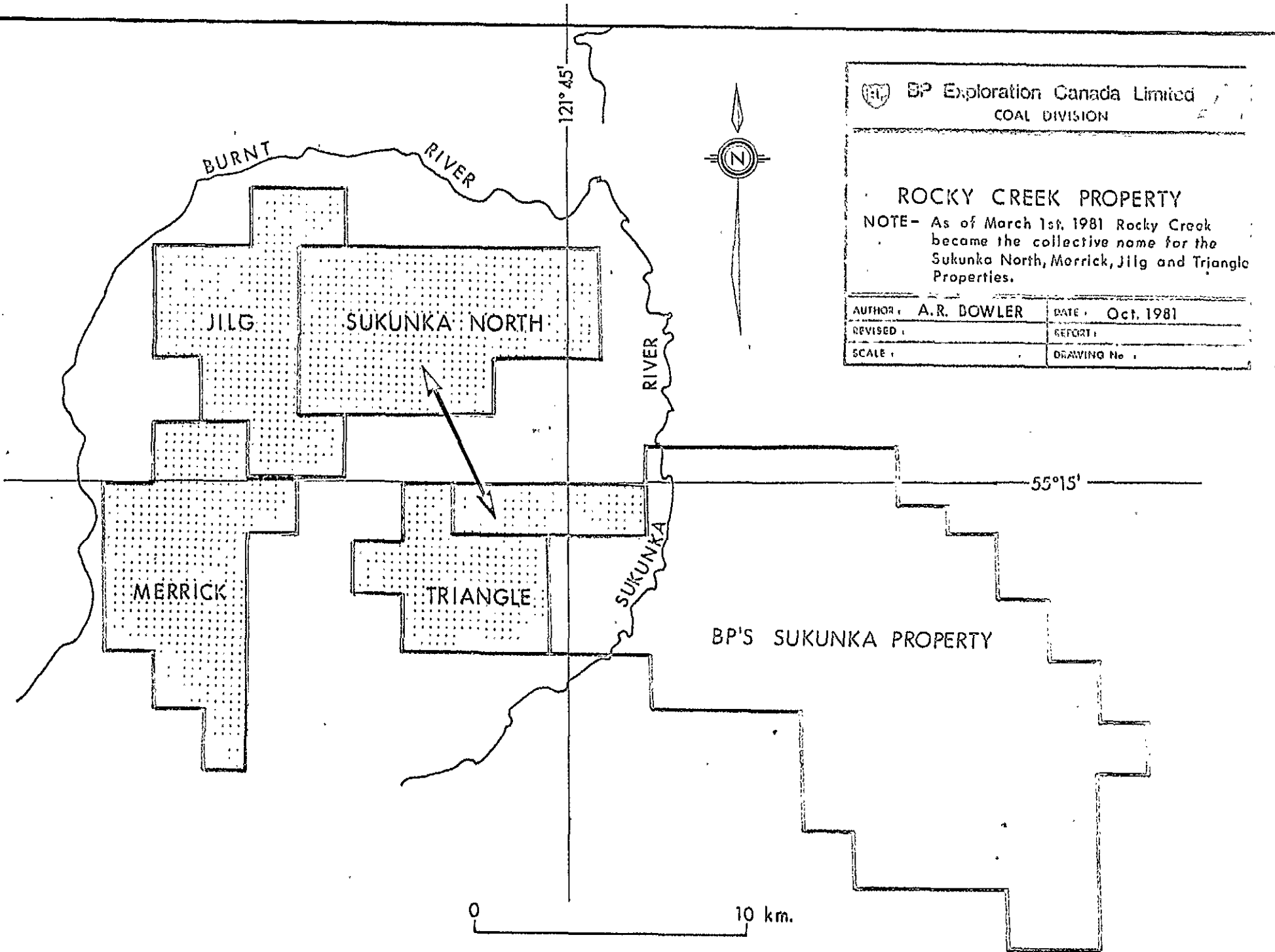
2. LOCATION - ACCESS - TOPOGRAPHY (CONTINUED)


The terrain encompassed by the study area varies from rolling mountains, to the less-rugged valleys of the Burnt and Sukunka Rivers. The surface elevation varies from 650 to 1,500 metres above sea level.

Three vegetation zones are present in the area: the Subboreal White Spruce - Alpine Fir Zone; the Sub-alpine Engelmann Spruce - Alpine Fir Zone: and the Alpine Tundra Zone. A diversity of wildlife is expected on the property, including up to 46 species of mammals and 160 species of birds. The climate of the region is Humid Continental, short summer with a mean annual temperature of 0° C and a total annual precipitation ranging from 42 - 69 cm.

3. LICENCES AND HISTORY OF OWNERSHIP

The Rocky Creek property encompasses 55 British Columbia Department of Energy Mines and Petroleum Resources coal licences for a total hectorage of approximately 16,225 ha. Prior to March 1st, 1981 the Rocky Creek property was made up of four properties as follows:-



 BP Exploration Canada Limited  
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**ROCKY CREEK PROPERTY**  
 NOTE- As of March 1st, 1981 Rocky Creek became the collective name for the Sukunka North, Merrick, Jilg and Triangle Properties.

|                      |                  |
|----------------------|------------------|
| AUTHOR : A.R. DOWLER | DATE : Oct. 1981 |
| REVISED :            | REPORT :         |
| SCALE :              | DRAWING No :     |

Figure 2

3. LICENCES AND HISTORY OF OWNERSHIP (CONTINUED)

(See Map 1 for location of specific licences)

| <u>Property</u> | <u>Licences</u>                          | <u>Area</u> |
|-----------------|--|-------------|
| Sukunka North   | 3617, 4029-4032, (20)<br>4034, 4036-4049 | 5,896 ha    |
| Jilg            | 5267 - 5278 (12)                         | 3,537 ha    |
| Merrick         | 5244 - 5258 (15)                         | 4,428 ha    |
| Triangle        | 5259 - 5266 ( 8)                         | 2,362 ha    |

Figure 2 illustrates the locations of the four properties which make up the Rocky Creek Property, and their relationship to the BP Sukunka Property.

The licence renewal date for all of these above licences is December 31st, 1981.

The Jilg Merrick and Triangle properties were filed by BP on March 27, 1979, and are held 100% by BP to this day.

The Sukunka North\* property was originally filed and held by Masters Exploration (Manalta Coal) in February, 1978. On August 1st, 1979 BP entered an option agreement with Manalta, and as a result of work performed during the 1979 and 1980 field season, BP obtained out right the Sukunka North licences on December 1st, 1980.

\* The original Sukunka North property included 35 coal licences, situated on the east bank of the Sukunka River: these licences were surrendered in March, 1980.

3. LICENCES AND HISTORY OF OWNERSHIP (CONTINUED)

Manalta Coal, as a result of this agreement, can claim a royalty on all coal produced and sold from the Sukunka North licences, calculated at the rate of 1% of the gross revenue received by BP for the coal f.o.b. the railcar at the preparation plant.

4. HISTORY OF EXPLORATION AND EXPENDITURE

Prior to the 1979 field season, only regional field mapping had taken place over the four properties. The work was either carried out by consultants, often working for oil companies, or by government geologists.

In 1979 BP initiated a detailed field mapping program of the former Sukunka North property, which at that time was optioned from Manalta Coal. During this helicopter supported program over 500 outcrop stations were plotted described, and a 1:10,000 scale surface geology map produced.

4. HISTORY OF EXPLORATION AND EXPENDITURE (CONTINUED)

Known coal occurrences on the former Triangle, Merrick and Jilg properties were substantiated during this program, however, no detailed mapping was carried out. It was during the 1979 that 2 boreholes were drilled and extensive field mapping carried out on the east bank licences of Rocky Creek. These licences were subsequently relinquished due to poor reserve potential.

The 1980 exploration program concentrated on the area now known as Rocky Creek. The main objectives of this program were to define the formations exposed on the property, obtain structural and stratigraphic data on the coals of the Lower Gething Formation as well as the Minnes Group, and to establish the rank and quality of the various coals encountered.

These objectives were accomplished by field mapping and trenching, with over 1,000 outcrop stations being visited and described; and by drilling five diamond drill holes for a total of 1,400 m of core. All field work and drilling was helicopter supported, with a base situated in the town of Chetwynd.

4. HISTORY OF EXPLORATION (CONTINUED)

As a result of the 1980 exploration program two main coal zones, the Pump and Grizzly Zones, (each 3 to 4 m thick) both of thermal coal quality were recognised. Both zones had areas which appeared to have good potential for surface mining, however, each zone exhibited considerable variations in thickness and quality over short distances.

Further drilling, mapping, trenching and sampling was proposed for the 1981 field seasons, so that the objectives outlined in the next chapter (Chapter 5) might be accomplished.

5. 1981 EXPLORATION PROGRAM OBJECTIVES

The main objectives of the 1981 Rocky Creek exploration program were:-

- (1) To delineate reserve blocks within the Lower Gething coals, in particular from the Cadomin, Grizzly, Pump, and 'B' Zones..
- (2) To obtain more detailed structural, and stratigraphic data on the above coal zones particularly within the mineable reserve blocks.
- (3) To establish the rank and quality of the coal zones encountered within each reserve block.
- (4) To determine if any coals of mineable thickness exist in the Minnes Formation.

To accomplish the above objectives 7 BP personnel were assigned to the project to supervise and to carry out geological mapping, sampling, and core logging. Originally 20 wireline N.Q. sized boreholes were planned, totalling approximately 3,800 m of drilling, however due to geological factors 6 of the holes were dropped from the program.

6. SERVICING OF PROGRAM

Major considerations in servicing the drilling and mapping programs were accommodations, transportation and field equipment. Several companies were required to service the drilling and mapping including:

| <u>Company</u>                  | <u>Personnel/Service</u>                               |
|---------------------------------|--|
| BP                              | 2 geologists, 2 technologists & 3 summer students      |
| Maple Leaf Helicopters          | 1 to 2 pilots, 206 & 204 helicopters                   |
| Northern Mountain Helicopters   | 1 pilot, 2 engineers, 205 helicopter                   |
| Highland Helicopters            | 1 pilot, 2 engineers, 212 helicopter                   |
| D.W. Coates Enterprises         | 2 - 4 man drill crews, 1 supervisor 2 - diamond drills |
| Century Geophysical Corporation | 1 borehole logging engineer                            |
| Peace Dozing & Contracting      | 2 to 3 slashers  |
| Northland Storage               | core shed facilities                                   |
| Pine Cone Motor Inn             | accommodation BP and Century Engineer                  |
| Canuck Truck Rentals            | 2 - 3/4 ton trucks                                     |
| Canadian Marconi                | Radio communications                                   |
| Canadian Freightways            | Freight transport                                      |
| Wayne Asleson Trucking          | Freight transport                                      |
| Beaver Lumber                   | Field equipment  |
| Northern Metallic               | Field equipment  |
| Ribtor Sales                    | Field equipment  |



6. SERVICING OF PROGRAM (CONTINUED)

6.1 Accommodation

Operations were conducted from field headquarters set up in the Pine Cone Motor Inn in Chetwynd, B.C. Accommodations consisted of 5 to 6 suites being rented for approximately 3 months with one of the larger suites serving as a field office.

The D. W. Coates drill crews stayed at the Pine Cone Motor Inn, as well as the Century Geophysical logger.

All other contractors used in the program operations were local and were able to travel to and from their own homes.

A core shed, serviced with electricity and water, was rented in Chetwynd from Northland Storage.

6. SERVICING OF PROGRAM (CONTINUED)

6.2 Transportation

Transportation in and around Chetwynd and to the BP mine camp, adjacent to the study area, was facilitated by two three-quarter ton trucks. They were especially useful in transporting extra helicopter fuel and supplies to the mine camp, and hauling the core to Chetwynd from the mine area. Because of its proximity to the Rocky Creek property, the BP mine camp became a depot for transporting equipment, drilling supplies and in some cases, crews to and from the field. The trucks were supplied by Canuck Truck Rentals in Chetwynd.

The helicopter transport of field mapping crews to and from the field from Chetwynd and/or the BP mine camp was by a Bell '206' helicopter from Maple Leaf Helicopter Ltd., of Chetwynd.

The Bell '206' was also used to transport drill crews from Chetwynd to the rigs, and back. For drill rig moves, a Bell '204' from Maple Leaf was employed. On several occasions, substitute helicopters were used for rig moves, specifically, a Bell '205' from Northern Mountain Helicopters, and a Bell '212' from Highland Helicopters, both from Chetwynd.

6. SERVICING OF PROGRAM (CONTINUED)

6.3 Field Equipment

Communications for the program was handled very well by tying the BP Coal Division radio systems, into the BP Oil and Gas short-wave system which utilized a repeater at the summit of Bull-moose Mountain. With this system, communication over 60 km was possible with very few problems. The suite of radios used consisted of two 40 watt units mounted in the drill rigs, and seven handheld portable radios for the helicopter dispatched mapping crews, pilots, helicopter base, and BP personnel in Chetwynd.

Field equipment not already on hand was purchased from Ribtor Sales of Calgary or Beaver Lumber and Northern Metallic Sales both of Chetwynd.

6.4 Drilling

Drill site construction was contracted to Peace Dozing and Contracting of Chetwynd. Fourteen drill sites were constructed and used during 1981. The drill pads, approximately 2,500 square metres in size, were, where geologically favourable, built on, or near, natural clearings so that timber damage was kept to a minimum.

6. SERVICING OF PROGRAM (CONTINUED)

6.4 Drilling (Continued)

As the drilling program was helicopter supported no heavy equipment work, road construction or sump preparation was undertaken, therefore reclamation was minimal.

D. W. Coates Enterprises of Vancouver, B.C. was contracted to drill the twenty proposed N.Q. diamond core holes on the Rocky Creek Property. Upon the completion of the first five holes, it was decided because of geological factors, that only fourteen of the proposed core holes should be drilled.

Maps in the rear pocket illustrates the borehole locations at scales of 1:10,000 and 1:50,000, whereas Table I lists the eastings, northings and surface elevations of the 1980 and 1981 drill holes.

D. W. Coates supplied all of the drilling equipment, and the necessary supplies and additives.

TABLE I

BOREHOLE LOCATIONS AND SURFACE ELEVATIONS

| <u>1980 PROGRAM</u> | <u>EASTING</u> | <u>NORTHING</u> | <u>SURFACE ELEVATION</u> | <u>Licence #</u> |
|---------------------|----------------|-----------------|--------------------------|------------------|
| BP-1                | 572,000 m E    | 6,127,650 m N   | 1,525 m                  |                  |
| BP-2                | 574,400 m E    | 6,128,250 m N   | 1,445 m                  |                  |
| BP-3                | 579,120 m E    | 6,127,740 m N   | 1,400 m                  |                  |
| BP-4                | 570,760 m E    | 6,129,030 m N   | 1,395 m                  |                  |
| BP-5                | 569,450 m E    | 6,122,100 m N   | 1,520 m                  |                  |
| <u>1981 Program</u> |                |                 |                          |                  |
| 1 BP-6              | 572,250 m E    | 6,126,075 m N   | 1,605 m                  | 4039             |
| 2 BP-7              | 573,590 m E    | 6,127,245 m N   | 1,420 m                  | 4043             |
| 3 BP-8              | 572,890 m E    | 6,127,880 m N   | 1,390 m                  | 4044             |
| 4 BP-9              | 573,170 m E    | 6,129,890 m N   | 1,185 m                  | 4048             |
| 5 BP-10             | 575,110 m E    | 6,129,540 m N   | 1,245 m                  | 4047             |
| 6 BP-11             | 577,970 m E    | 6,128,025 m N   | 1,300 m                  | 4041             |
| 7 BP-12             | 575,725 m E    | 6,128,520 m N   | 1,320 m                  | 4042             |
| 8 BP-13             | 580,250 m E    | 6,122,460 m N   | 1,425 m                  | 4030             |
| 9 BP-14             | 570,750 m E    | 6,130,415 m N   | 1,430 m                  | 5275             |
| 10 BP-15            | 574,730 m E    | 6,126,915 m N   | 1,315 m                  | 4038             |
| 11 BP-16            | 567,450 m E    | 6,119,075 m N   | 1,525 m                  | 5253             |
| 12 BP-17            | 569,070 m E    | 6,120,730 m N   | 1,515 m                  | 5252             |
| 13 BP-18            | 574,820 m E    | 6,127,890 m N   | 1,310 m                  | 4042             |
| 14 BP-19            | 575,275 m E    | 6,127,310 m N   | 1,260 m                  | 4042             |

6. SERVICING OF PROGRAM (CONTINUED)

6.4 Drilling (Continued)

The equipment and supplies consisted of:

- 2 Longyear 38 drills, helicopter transportable
- Auxiliary water pumps and hose
- Mud tanks
- Drill Stem and core barrels.
- Drill bits, core boxes, casing and drilling mud.
- Cement mixer/pump.

BP was responsible for all site preparation and transportation of equipment and drill crews to and from drill sites.

The drilling program commenced with the D. W. Coates rigs arriving on June 1, 1981. Aided by good weather conditions, a plentiful water supply, and good drilling practices and conditions, the program was completed on the 16th of July, 1981.

Tables 2 and 3 give details of the drilling carried out during the 1981 program.

The Geologist core log descriptions can be found in Volume 2.

BOREHOLE COMPLETION DETAILS

| Borehole     | Type                    | Prognosis<br>Depth | Actual<br>Depth | Date<br>Spudded | Date<br>Completed | Type of<br>Drill |
|--------------|-------------------------|--------------------|-----------------|-----------------|-------------------|------------------|
| BP81-06      | Vertical NQ<br>Wireline | 250 m              | 228.6 m         | June 2/81       | June 7/81         | Longyear 38      |
| BP81-07      | Vertical NQ<br>Wireline | 150 m              | 224.6 m         | June 2/81       | June 7/81         | Longyear 38      |
| BP81-08      | Vertical NQ<br>Wireline | 100 m              | 132.9 m         | June 8/81       | June 10/81        | Longyear 38      |
| BP81-09      | Vertical NQ<br>Wireline | 350 m              | 200.3 m         | June 9/81       | June 13/81        | Longyear 38      |
| BP81-10      | Vertical NQ<br>Wireline | 150 m              | 227.7 m         | June 11/81      | June 14/81        | Longyear 38      |
| BP81-11      | Vertical NQ<br>Wireline | 200 m              | 141.1 m         | June 14/81      | June 16/81        | Longyear 38      |
| BP81-12      | Vertical NQ<br>Wireline | 250 m              | 263.9 m         | June 15/81      | June 20/81        | Longyear 38      |
| BP81-13      | Vertical NQ<br>Wireline | 250 m              | 401.4 m         | June 17/81      | June 26/81        | Longyear 38      |
| BP81-14      | Vertical NQ<br>Wireline | 200 m              | 121.0 m         | June 21/81      | June 23/81        | Longyear 38      |
| BP81-15      | Vertical NQ<br>Wireline | 120 m              | 162.5 m         | June 24/81      | June 27/81        | Longyear 38      |
| BP81-16      | Vertical NQ<br>Wireline | 300 m              | 306.9 m         | June 28/81      | July 4/81         | Longyear 38      |
| BP81-17      | Vertical NQ<br>Wireline | 300 m              | 273.4 m         | July 5/81       | July 10/81        | Longyear 38      |
| BP81-18      | Vertical NQ<br>Wireline | 100 m              | 107.3 m         | July 11/81      | July 14/81        | Longyear 38      |
| BP81-19      | Vertical NQ<br>Wireline | 100 m              | 98.1 m          | July 15/81      | July 16/81        | Longyear 38      |
| 14 - TOTALS- |                         | 2,820 m            | 2,889.7 m       |                 |                   |                  |

DRILLING TIME DATATABLE 3

| BOREHOLE | CASING DEPTH<br>m | TRICONING<br>m | DHr    | DRILLING<br>m | DHr     | DRILLING RATE<br>m/hr | TRAVEL TIME<br>Mhr. |
|----------|-------------------|----------------|--------|---------------|---------|-----------------------|---------------------|
| BP81-6   | 5.5 m             | 5.5 m          | 2 hr   | 223.1 m       | 59 hr   | 3.8 m/hr              | 26 hr               |
| BP81-7   | 3.7 m             | 3.7 m          | 2 hr   | 220.9 m       | 64 hr   | 3.5 m/hr              | 29 hr               |
| BP81-8   | 15.2 m            | 15.2 m         | 6 hr   | 117.7 m       | 30.5 hr | 3.9 m/hr              | 12 hr               |
| BP81-9   | 4.3 m             | 4.3 m          | 2 hr   | 196 m         | 50 hr   | 3.9 m/hr              | 24 hr               |
| BP81-10  | 5.2 m             | 5.2 m          | 1 hr   | 222.5 m       | 58 hr   | 3.8 m/hr              | 24 hr               |
| BP81-11  | 3.0 m             | 3.0 m          | 3 hr   | 138.1 m       | 37 hr   | 3.7 m/hr              | 10 hr               |
| BP81-12  | 4.9 m             | 4.9 m          | 1 hr   | 259 m         | 82 hr   | 3.2 m/hr              | 29 hr               |
| BP81-13  | 13.4 m            | 13.4 m         | 6.5 hr | 388 m         | 154 hr  | 2.5 m/hr              | 50 hr               |
| BP81-14  | 13.1 m            | 13.1 m         | 5 hr   | 107.9 m       | 29 hr   | 3.7 m/hr              | 16 hr               |
| BP81-15  | 9.5 m             | 9.5 m          | 5 hr   | 153 m         | 40 hr   | 3.8 m/hr              | 15 hr               |
| BP81-16  | 3.4 m             | 3.4 m          | 2 hr   | 303.5 m       | 81.5 hr | 3.7 m/hr              | 28 hr               |
| BP81-17  | 3.9 m             | 3.9 m          | 2 hr   | 269.5 m       | 69 hr   | 3.9 m/hr              | 24.5 hr             |
| BP81-18  | 3.0 m             | 3.0 m          | 1 hr   | 104.3 m       | 19 hr   | 5.5 m/hr              | 16 hr               |
| BP81-19  | 3.0 m             | 3.0 m          | 2 hr   | 95.1 m        | 18 hr   | 5.3 m/hr              | 10 hr               |

m - meters

DHr - Drill Hours

m/hr - metres per hour

Mhr - Man Hours



6. SERVICING OF PROGRAM (CONTINUED)

6.5 Geophysical Logging (See Volume 3 and 4)

Century Geophysical Corporation of Calgary was contracted to run the geophysical logging program on the Rocky Creek Exploration Program. Century supplied a logging engineer, helicopter transportable logging unit, and the necessary logging sondes. Arrangements were made by BP for the logger to stay in Chetwynd and fly out to the property, where the logging unit was stationed on the next hole to be logged.

Four geophysical sondes were made available to BP by Century throughout the drilling program. These consisted of:-

- (1) the 9055 multifunction tool capable of giving gamma, resistance, spontaneous of self potential, neutron, temperature and deviation.
- (2) the 9067 slimline, which is a gamma, neutron-neutron tool.
- (3) the 9030 coal tool, recording density, gamma, resistivity and hole diameter (caliper) and,
- (4) the 9068 slimline, responses for gamma, and uncalibrated density.

Table 4 lists the geophysical logs run in each of the boreholes drilled during the 1981 programs as well as other pertinent data.

## GEOPHYSICAL LOGGING DATA

TABLE 4

| BOREHOLE | CALIPER | GAMMA | S.P. | RESISTIVITY | NEUTRON | DEVIATION | DENSITY | OPEN HOLE | THRU RODS | DEPTH<br>m | HOUR'S ON SITE | BREAKDOWN HOURS ON SITE | DATE    |
|----------|---------|-------|------|-------------|---------|-----------|---------|-----------|-----------|------------|----------------|-------------------------|---------|
| BP81-06  | X       | X     | X    | X           | X       | X         | X       | X         |           | 229.8      | 3              | 12                      | 6/8/81  |
| BP81-07  | X       | X     | X    | X           | X       | X         | X       | X         |           | 224.5      | 8              | 13                      | 6/8/81  |
| BP81-08  | X       | X     | X    | X           | X       | X         | X       | X         |           | 132.5      | 4.5            |                         | 6/10/81 |
| BP81-09  | X       | X     | X    | X           | X       | X         | X       | X         |           | 199.7      | 3              |                         | 6/12/81 |
| BP81-10  |         | X     |      |             | X       |           | X       |           | X         | 222.5      | 2.5            |                         | 6/14/81 |
| BP81-11  | X       | X     | X    | X           | X       | X         | X       | X         | X         | 140.6      | 4              |                         | 6/16/81 |
| BP81-12  |         | X     |      |             | X       |           | X       |           | X         | 255.5      | 2              |                         | 6/20/81 |
| BP81-13  | X       | X     | X    | X           | X       | X         | X       | X         | X         | 398.0      | 7              |                         | 6/25/81 |
| BP81-14  |         | X     |      |             | X       |           | X       |           | X         | 115.0      | 2              | 2                       | 6/23/81 |
| BP81-15  | X       | X     | X    | X           | X       | X         | X       | X         | X         | 158.6      | 4              |                         | 6/27/81 |
| BP81-16  |         | X     |      |             | X       |           | X       |           | X         | 298.5      | 8.5            |                         | 7/4/81  |
| BP81-17  |         | X     |      |             | X       |           | X       |           | X         | 268.7      | 4              |                         | 7/10/81 |
| BP81-18  | X       | X     | X    | X           | X       | X         | X       | X         | X         | 99.9       | 6              |                         | 7/13/81 |
| BP81-19  |         | X     |      |             | X       |           | X       |           | X         | 93.6       | 3              |                         | 7/16/81 |

All holes had casing in whilst logging took place.

6. SERVICING OF PROGRAM (CONTINUED)

6.6 Reclamation

Due to the minimal amount of surface disturbance, very little reclamation work was required. In drill site preparation, damaged and cut timber was 'bucked up' and limbed. Since road construction, levelling of drill sites, and sump preparation was not required, no erosion control or backfilling work was necessary. All drilling additives were biodegradable, and therefore no extra site clean-up was necessary, other than the removal of mud and cement bags, etc. All garbage and refuse was flown from the property area and properly disposed of.

No bulldozer or backhoe trenching work was done on the property in 1981. All trenches were hand dug, however, not all having been backfilled, as work is to be continued on the property in 1982.

The only costs incurred for reclamation was in the form of man hours and helicopter time.

7. FIELD MAPPING

The Rocky Creek coal licences were mapped in detail by one or two field parties supported by helicopter. Each party was made up of an experienced geologist or technologist and a summer student. During the three month program, over 150 outcrop stations were plotted and described, these supplement the over 1,000 stations from 1980. In addition 10 hand trenches were dug, measured, described, and sampled.

Outcrop stations and other general geologic observations were plotted on 1:10,000 base maps, prepared by Hardy and Associates. Thommen altimeters, Brunton compasses, and topofilms were used for accurate ( $\pm$  5 to 10 metres) locations of outcrops and geologic features.

Traverses generally were done along streams; major ridges, some cutlines, and occasionally through the forests as well. Helicopter access to these areas was made possible by the eighteen helicopter pads constructed in 1979, the five abandoned drillsites from 1980, and by the fourteen drillsites prepared in 1981. Enough of the remainder of the Rocky Creek Property is above tree line or has natural clearings, to allow access for helicopter landings.

7. FIELD MAPPING

The 1:50,000 scale map (Map 1) and the 1:10,000 scale maps (Maps 1A and 1B) in the pockets at the rear of the report show the location of outcrop stations and trenches. Map station and trench descriptions are found in Volume II.

8. SAMPLING AND ANALYSIS

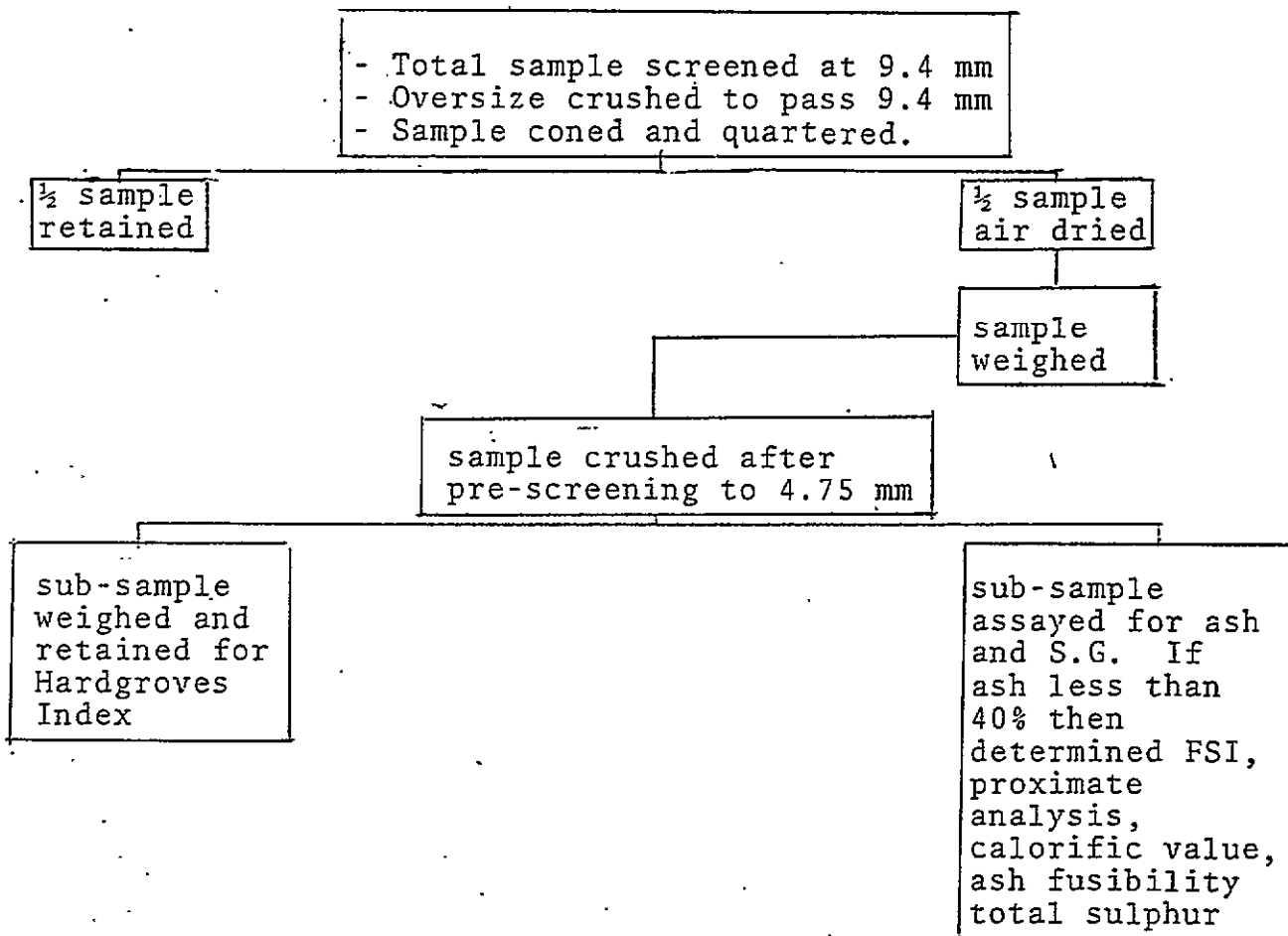
During the 1981 programme, trenching was largely confined to known major coal seams, in order to augment the analytical data. Hand trenches were driven across seam outcrops and logged in detail. Sample plys were taken with regard to visible lithological changes within the seams, and partings greater than 3 cm. were taken as individual plys. Each ply was sampled separately, in order to ensure sufficient sample volumes from the thinner plys. Upon completion of the exploration programme, the major seams were selected for analysis, while the remaining samples were retained for future use.

Core drilling was the major component of the 1981 programme, but the bulk of the holes did not encounter significant thickness of coal. Therefore, the number of coal core samples was small in comparison with last year. Cores from potentially-mineable seams were first described, and the geophysical logs were then consulted by the geologist in order to plan the sampling of each seam. Partings thicker than 3 cm were taken as separate plys, while coal sections were divided into plys on the basis of visible lithological changes and differing geophysical signatures. As with the trench samples, core samples of the major seams were subsequently sent for analysis, while other samples were retained for later use.

8. SAMPLING AND ANALYSIS (Continued)

As a result, core samples from six intersection and three sets of trench samples were sent in for proximate analyses and determinations of sulphur, FSI, Hardgroves grindability, calorific value and specific gravity.

The following analytical procedure was carried out:



Birtley Engineering (Canada) Ltd. were responsible for the analysis of the 1981 samples.

8. SAMPLING AND ANALYSIS (Continued)

Accompanying this report (Chapter 11) are some of the preliminary analytical results from this year's intersections as well as some of last year's results from borehole and trench samples from within the Rocky Creek reserve blocks. In addition to this programme of analysis, petrographic analyses of the major seams encountered were undertaken, as well as wash tests on selected seam sections from boreholes with +90% core recovery.



## 9. GEOLOGY

The Rocky Creek property is situated on the west side of the Sukunka River, within the Rocky Mountain Foothills, and trending northwesterly along the front ranges of the Rocky Mountains in northeastern British Columbia. The Lower Cretaceous coal-bearing rock successions are sporadically exposed over large areas and special attention was paid to locating economically viable coal seams within these measures.

Regional stratigraphic studies have been carried out by the Geological Survey of Canada (eg. Stott 1968, 1971). In addition, localized stratigraphic mapping projects are currently being undertaken by the British Columbia Department of Energy Mines and Petroleum Resources.

It is generally known that the Cretaceous sediments were deformed during the Laramide Orogeny. The strata have been folded into a series of en echelon anticlines and synclines and locally broken by west-dipping thrust faulting. The major fold structures constitute a regional northwesterly trend. The formations present on the Rocky Creek Property, as well as their thicknesses and lithology are listed in Table 5.

TABLE OF FORMATIONS

|                | UNIT                                    | LITHOLOGY   | THICKNESS (m)            |
|----------------|---|---|--------------------------|
| Bullhead Group | Gething Fm.    Upper<br>Middle<br>Lower | sandstone<br>siltstone, mudstone, sst.<br>sst. siltstone, mudstone,<br>coal; minor conglomerate | 10+<br>104<br>320 to 354 |
|                | Cadomin Fm.                             | Conglomerate,<br>sandstone; minor<br>fine sediments   | 25 to 35                 |
| Minnes Group   | Bickford Fm.                            | sandstone, mudstone<br>coal, conglomerate   | 285+                     |
|                | Monach Fm.                              | quartzite; finer<br>sediments as above/below  | 50+<br>—                 |
|                | Beattie Peaks Fm.                       | sandstone, mudstone<br>thin coals, conglomerate   | 300+                     |
|                | Monteith Fm.                            | quartzite, sandstone  | 600+<br>—                |

## 9. GEOLOGY (CONTINUED)

### 9.1 Stratigraphy

#### Minnes Group

These beds range in age from Jurassic to Lower Cretaceous. Four formations are encompassed; from bottom up these are the Monteith, Beattie Peaks, Monach (Mathews, 1947) and Bickford (Stott, 1981) Formations.

The Monteith Formation in the Rocky Creek area consists of quartzites and coarse sandstones. Previous BP mapping (Jones, 1959, 1960) suggests a thickness of 600 m for this unit, which is not known to be coal-bearing. The Monteith was not investigated during 1981.

Overlying the Monteith is the Beattie Peaks Formation, composed of fine sandstones, shales and generally thin coals. At least 300 m of Beattie Peaks beds are exposed in the high ground northeast of Mount Merrick; several hand trenches, along with holes BP-5, BP-16 and BP-17 are currently thought to be in Beattie Peaks beds, and show a number of coal seams, locally as thick as 2.5 m.

Insufficient work has been done to date, to determine the resource potential of these seams, although it should be noted that areas of moderate dip are of limited extent in the area in question.

9. GEOLOGY (CONTINUED)

9.1 Stratigraphy (Continued)

The Monach Formation follows the Beattie Peaks; it is not well-developed in the Rocky Creek area, being near its southward limit.

It consists of two separate bands of orthoquartzite, each about 5 to 6 m thick, separated by beds similar to those above and below it. The total thickness of the Monach is very approximately set at 50 m. No significant coals are known in this unit.

The youngest unit of the Minnes Group is the Bickford Formation; it consists of medium to coarse sandstones, shales, coals and minor conglomerate. Several thin seams, up to 1 m thick, are known from outcrops and boreholes BP-4 and BP-13. Near Mount Merrick, two seams, each about 2 m thick, occur 30 to 35 m below the top of the Bickford. They are, however dipping at 40 to 60 degrees SW and cannot be traced into less-disturbed areas.

The contact of the Bickford with the overlying Cadomin Formation is abrupt, with channel structures being exposed in several localities; notably east of hole BP-13. According to Stott, the contact is a regional unconformity; however in the Rocky Creek Area, changed dips or lateral bevelling of Minnes beds cannot be demonstrated.

9. GEOLOGY (CONTINUED)

9.1 Stratigraphy (Continued)

Bullhead Group

Cadomin Formation

This unit consists principally of thick-bedded to massive, pebble to boulder - conglomerates, and associated medium to coarse sandstones. Within the Rocky Creek area, the Cadomin commonly consists of two distinct, resistant conglomerate/sandstone zones, separated by an interval of finer, more-argillaceous beds. The Cadomin forms an excellent mapping-unit, as it commonly crops out as two lines of bluffs, separated by a recessive interval. The total thickness of the Cadomin ranges from 25 to 35 m. The contact of the Cadomin with the overlying Gething Formation is interfingering on a regional basis; in the Rocky Creek area it appears to be abrupt although some lateral transgression may have occurred.

9. GEOLOGY (CONTINUED)

9.1 Stratigraphy (Continued)

Bullhead Group (Continued)

Gething Formation

The stratigraphy of the Gething Formation has been dealt with at length in various BP internal reports; a summary will be here presented. Three informal subdivisions (each of member rank) have been established: the Lower, Middle and Upper Gething. These units have been recognised on the surface and in boreholes, on both sides of the Sukunka River:

The Lower Gething consists of sandstones, siltstones, mudstones, coals and minor conglomerate. Sandstones predominate near the top and base of this unit; the basal part locally contains abundant conglomerate and siliceous, coarse sandstone. Coals are present throughout the Lower Gething, but are most abundant in its middle third. The accompanying (Table 6) summarises coal development in the Rocky Creek area. The Chart in the rear pocket presents a correlation of the various coals and formational contacts as seen in selected boreholes.

COAL DEVELOPMENT IN THE

TABLE 6

LOWER GETHING, OF THE ROCKY CREEK PROPERTY

| <u>COAL ZONE OR HORIZON NAME</u> | <u>INTERVAL ABOVE BASE OF GETHING (m)</u> | <u>RESOURCE POTENTIAL NORTH OF ROCKY CR.</u> | <u>SOUTH OF ROCKY CREEK</u>                                  |
|----------------------------------|---|--|--|
| 'B' Upper                        | 260 m to 285 m                            | North of Rocky Creek                         | Four coal zones in BP-13; designated B through C Lower; good |
| 'B' Lower                        | 245 m to 270 m                            | None   |  |
| Pump                             | 150 m to 175 m                            | Good, near BP-1                              | None   |
| Grizzly                          | 135 m to 165 m                            | Good, near BP-1,2,6,7                        | None   |
| Unnamed Zone                     | 105 m to 145 m                            | None   | None   |
| Meadow                           | 75 m to 115 m                             | None   | None   |
| Bumpy                            | 60 m to 95 m                              | None   | None   |
| Cadomin                          | 15 m                                      | Minimal, near Mt. Jilg                       | None   |
| Lake                             | 5 m                                       | None   | None   |

9. GEOLOGY (CONTINUED)

9.1 Stratigraphy (Continued)

Bullhead Group (Continued)

Gething Formation (Continued)

The 'B/C' zones are regionally extensive, having been traced from Bullmoose Creek North to Burnt River, on both sides of the Sukunka River. The four major coals in BP-13, south of Rocky Creek, are thought to be correlative to the 'B' and 'C' zones of the Sukunka property. It is probable that the Pump and Grizzly zones of the Rocky Creek property are lateral equivalents to the 'D' and 'E' coal zones at Sukunka.

All three of the major coal zones north of Rocky Creek (Pump, Grizzly and Cadomin zones) show deterioration in an eastward direction. The Grizzly is the most extensively-developed, while the Pump is of interest only near hole BP-1, and the Cadomin coal zone is of significance only in a restricted area near its outcrop on Mount Jilg. South of Rocky Creek, none of these zones are well-developed; the four higher zones ('B' and 'C' group) are of encouraging thickness.

The total thickness of the Lower Gething at Rocky Creek is 320 to 345 m. Its contact with the overlying Middle Gething is marked by an erosional, gritty band, which may represent a local hiatus in sedimentation.



## 9. GEOLOGY (CONTINUED)

### 9.1 Stratigraphy (Continued)

#### Bullhead Group (Continued)

#### Gething Formation (Continued)

The Middle Gething is a predominantly marine sequence of dark, shelly, calcareous mudstones, siltstones and fine, locally-glaucopititic sandstones. Coals are lacking in this unit, which contains abundant Entolium fossils along with fish scales. In the Rocky Creek area it is only present in the high ground near holes BP -3 and BP-2, where it attains a thickness a 104 m.

The Upper Gething is the youngest of the three subdivisions of the Gething Formation. While in the Sukunka area it contains the Sukunka coal deposit, in the Rocky Creek area it is of extremely-limited extent, being confined to an erosional remnant of 10 m of sandstone, at hole BP-2.

### 9.2 Structure

The Rocky Creek property lies within the Inner Foothills structural province, and as such exhibits complex structural geology. Reference to Map 3 (Structural Summary Map) will be of assistance in the following discussion.

9. GEOLOGY (CONTINUED)

9.2 Structure (Continued)

The southwestern licences near Mount Merrick, are severely deformed, with Palaeozoic carbonates being thrust over Minnes and Bullhead strata. Immediately northeast of Mount Merrick, under the major thrust, the Gething and Cadomin have been folded into the tight, near-isoclinal Merrick Syncline, overturned to the northeast. To the northeast of this structure, steep southwest dips prevail in the Minnes Group exposures until a second major thrust is encountered, southwest of BP-16. From here northeast to BP-5 over a distance of 4 km gently-dipping beds of the Minnes are exposed in the broad Grizzly Ridge Syncline. Further to the northeast, Minnes beds again dip steeply to the southwest, up to the notch in the ridge southwest of Mount Jilg where a major thrust is thought to be present.

Mount Jilg is marked by the chevron-form, Jilg Anticline involving Minnes and some Bullhead strata. To the northwest, on Hill 1507, the Jilg Anticline passes to a flat-topped box-form. On both peaks, the west limb is marked by a tight, subsidiary syncline, and the east limb passes into the Rocky Creek Synclinorium.

9. GEOLOGY (CONTINUED)

9.2 Structure (Continued)

The Rocky Creek Synclinorium is characterised by gentle to moderate limb dips, common subsidiary open folds and one major internal thrust, the Rocky Creek thrust. The synclinorium covers the greater part of the northern and eastern Rocky Creek licences, and it is here that the bulk of the exploration has been done, in appreciation of its less intense deformation.

Holes BP-13, BP-3 and BP-11 are situated east of the Rocky Creek Thrust, while holes BP-1, BP-2, BP-4, BP-6 through 10, BP-12, BP-14, BP-15, BP-18 and BP-19, are situated west of the thrust. BP-10 and BP-12 have proven the thrust, which is west-dipping with a vertical throw of 90 to 100 m. Associated with the thrust are steep dips at surface, and minor tight folds.

South of Rocky Creek, the thrust may pass into a monocline in a region of steep to near-vertical eastward dips, along the deep valley immediately west of BP-13. This structure effectively cuts off the westward extension of the thick coals seen in BP-13.

## 10. COAL RESOURCES

### 10.1 Methodology

Resource figures quoted in this report are based solely upon data acquired in the 1980 and 1981 Rocky Creek programmes. Both trench and borehole data were available for this study; borehole sections have been adjusted to geophysical log control, since the Lower Gething coals commonly occur as coal zones laterally and vertically gradational boundaries. The following constraints were applied in determining seam sections for resource purposes:-

- 1) Minimum thickness of 1 m for potential surface- mineable seams; 1.5 m for underground.
- 2) Minimum coal content, in section to be 60% by thickness.

It was found that in general, the seams thus-defined show consistent sections among measurement points within a given resource block. A plan (Map 4) is enclosed, showing columnar sections of the Grizzly, Seam in its area of development north of Rocky Creek.

10. COAL RESOURCES (CONTINUED)

10.1 Methodology (Continued)

Tables of seam thicknesses and coal contents have been prepared for the following seams:

'B' through 'C' Lower Seams: Table 7

Pump Seam: Table 8

Grizzly Seam: Table 9

The data from these tables was used to construct outcrop and floor elevation maps for the various seams of interest. Where possible, surface geological data was used in the construction of these maps. Maps 2 and 5 present results from north of Rocky Creek, as well as the Terrance Hill area, south of Rocky Creek.

In-situ resources were calculated by planimetry of the outcrop lines for each seam, and multiplication by the average seam section in the given block. This was done in order to take account of the limited data and local variability of seam-sections. A specific gravity of 1.55 was used for calculation of in-situ tonnages. This value was calculated from 1980 results as the 1981 results were still pending.

TABLE 7'B' AND 'B' LOWER SEAM DATA:

| <u>HOLE</u> | <u>SEAM</u> | <u>THICKNESS</u>                      | <u>FLOOR DEPTH</u> |
|-------------|-------------|---------------------------------------|--------------------|
| BP-2        | 'B'         | 0.88 m @ 100% coal<br>(Not mineable). | 171.48 m           |
|             | 'B' lower   | 1.81 m @ 50% coal<br>(not mineable)   | 185.49 m           |
| BP-3        | 'B'         | 1.78 m @ 60% coal<br>(not mineable)   | 43.42 m            |
|             | 'B' lower   | 1.80 m @ 46% coal<br>(not mineable)   | 58.43 m            |
| BP-13       | 'B'         | 2.54 m @ 82% coal                     | 51.40 m            |
|             | 'B' lower   | 1.69 m @ 80% coal                     | 62.19 m            |

'C' AND 'C' LOWER SEAM DATA:

|       |           |                   |         |
|-------|-----------|-------------------|---------|
| BP-2  |           | (Not recognised)  |         |
| BP-3  |           | (Not recognised)  |         |
| BP-13 | 'C'       | 2.65 m @ 89% coal | 74.59 m |
|       | 'C' lower | 3.13 m @ 85% coal | 80.94 m |

PUMP SEAM (BOREHOLE & TRENCH INFORMATION)

| <u>Location</u> | <u>Thickness (m)</u> | <u>@ % Coal</u> | <u>Floor Depth</u> | <u>Elevation</u> |
|-----------------|----------------------|-----------------|--------------------|------------------|
| SNTR 19         | 3.12                 | 86              | -                  | 1,498 m          |
| BP 1            | 2.65                 | 87              | 49.41 m            | 1,476 m          |

average (2 points) 2.89 m @ 87% Coal.

Deteriorated sections in these holes:

|       |                    |            |         |
|-------|--------------------|------------|---------|
| BP 2  | Floor @ 244.48 m;  | Elev.      | 1,201 m |
| BP 3  | Floor @ 129.60 m   | Elev.      | 1,270 m |
| BP 7  | Floor @ 21.33 m    | Elev.      | 1,399 m |
| BP 18 | Floor @ 46.8 m     | Elev.      | 1,263 m |
| BP 19 | Floor near surface | Elev. near | 1,260 m |

GRIZZLY SEAM: BOREHOLE AND TRENCH DATA

| LOCATION   | THICKNESS (m)          | % COAL               | DEPTH (m) | ELEV. (m) |
|--|------------------------|----------------------|-----------|-----------|
| <u>BLOCK A</u>   |                        |                      |           |           |
| BP6  | 2.11                   | 65                   | 23.50     | 1,582     |
| SNTR 12  | 2.68                   | 65                   | N/A       | 1,570     |
| SNTR 14  | 1.64                   | 69                   | N/A       | 1,581     |
| SNTR 16  | 1.33                   | 75                   | N/A       | 1,580     |
| SNTR 17  | 1.18                   | 67                   | N/A       | 1,588     |
| Average: 5 points:   | 1.79 m @               | 68% coal             |           |           |
| SNTR 23  | 1.60 m @               | 87% coal             |           | 1,518     |
| <u>BLOCK B</u>   |                        |                      |           |           |
| BP7  | 1.85                   | 76                   | 45.55     | 1,374     |
| SNTR 25  | 1.53                   | 77                   | N/A       | 1,420     |
| Average: 2 points:   | 1.69 m @               | 77% coal             |           |           |
| <u>BLOCK C</u>   |                        |                      |           |           |
| BP2  | 2.23                   | 86                   | 285.29    | 1,160     |
| SNTR 20  | 4.41                   | 93                   | N/A       | 1,400     |
| SNTR 30  | 4.09+                  | (95)                 | N/A       | 1,405     |
| Average: 3 points:   | 3.58 m @               | 91% coal             |           |           |
| <u>BLOCK D</u>   |                        |                      |           |           |
| BP1  | 2.42                   | 77                   | 81.85     | 1,443     |
| SNTR 18  | 5.20                   | 66                   | N/A       | 1,470     |
| SNTR 31  |                        | Trench Not Completed |           | 1,460     |
| SNTR 28  | 6.93                   | 65                   | N/A       | 1,439     |
| Average: 3 points:   | 4.85 @                 | 69% coal             |           |           |
| DETERIORATED AREA:   |                        |                      |           |           |
| BP 10 Upper Plate: 14.8 m, el. 1,230; Lower Plate: 108.4 El. 1,137 Horizons only |                        |                      |           |           |
| BP3  | - Horizon at           |                      | 161.00    | 1,239     |
| BP18   | - Horizon at           |                      | 96.50     | 1,214     |
| BP19   | - Horizon at           |                      | 58.30     | 1,202     |
| BP13   | Horizon not recognised |                      |           |           |
| N/A: Not applicable  |                        |                      |           |           |



10. COAL RESOURCES (CONTINUED)

10.1 Methodology (Continued)

The total volume of rock to be excavated was obtained by the following process:

- Construction of floor elevation structure contour plan for the lowest mineable coal seam in each reserve block.
- Construction of cover contours over the seam floor by subtraction from the present ground surface.
- Planimetry of cover contours and calculation of total volume over seam floor.
- Subtraction of the volume of each mineable coal seam within the reserve block, as obtained in the course of the in-situ resource calculations.
- The remaining volume represents the total rock volume required to be excavated.

Strip ratios were calculated by dividing the total rock volume by the total in-situ tonnage of coal in a given block. The resultant ratios have dimensions of cubic metres per tonne.

10. COAL RESOURCES (Continued)

10.2 Results

The total in-situ tonnage for all five resource blocks is 24.67 MTe. Discounting Block C on grounds of excessive cover, the surface-mineable resource is 19.40 MTe, at strip ratios ranging from 2.9:1 to 5.0 cubic metres per tonne. (If Block C was mined by surface methods it would have a strip ratio of 18.7:1). Table 10 presents in-situ resource data, while Table 11 presents strip and excavation data.

IN-SITU RESOURCES

| <u>BLOCK</u>               | <u>SEAM</u> | <u>AREA</u> | <u>THICKNESS</u> | <u>WEIGHT</u>    |
|----------------------------|-------------|-------------|------------------|------------------|
| A                          | Grizzly     | 13.58 ha    | 1.79 m           | 0.38 MTe         |
| B                          | Grizzly     | 93.18 ha    | 1.69 m           | 2.44 MTe         |
| C                          | Grizzly     | 94.98 ha    | 3.58 m           | 5.27 MTe         |
| D                          | Grizzly     | 81.28 ha    | 4.85 m           | 6.11 MTe         |
| D                          | Pump        | 34.08 ha    | 2.89 m           | 1.53 MTe         |
| TOTAL NORTH OF ROCKY CREEK |             |             |                  | <u>15.73 MTe</u> |
| E                          | B           | 46.88 ha    | 2.54 m           | 1.85 MTe         |
| E                          | B Lower     | 51.54 ha    | 1.69 m           | 1.35 MTe         |
| E                          | C           | 60.18 ha    | 2.65 m           | 2.47 MTe         |
| E                          | C Lower     | 67.36 ha    | 3.13 m           | 3.27 MTe         |
| TOTAL SOUTH OF ROCKY CREEK |             |             |                  | <u>8.94 MTe</u>  |
| GRAND TOTAL                |             |             |                  | <u>24.67 MTe</u> |

STRIP RATIO AND EXCAVATION DATA

| <u>BLOCK</u> | <u>WEIGHT</u> | <u>EXCAVATION VOLUME</u>       | <u>STRIP RATIO</u> |
|--------------|---------------|--------------------------------|--------------------|
| A            | 0.38 MTe      | $1.49 \times 10^6 \text{ m}^3$ | 3.9:1              |
| B            | 2.44 MTe      | $12.3 \times 10^6 \text{ m}^3$ | 5:0:1              |
| C            | 5.27 MTe      | $97.9 \times 10^6 \text{ m}^3$ | 18.7:1             |
| D            | 7.64 MTe      | $22.2 \times 10^6 \text{ m}^3$ | 2.9:1              |
| E            | 8.94 MTe      | $25.8 \times 10^6 \text{ m}^3$ | 2.9:1              |

RATIO'S Represented are for cubic metres per tonne.

11. COAL QUALITY

Due to the late arrival of the various coal quality results very little manipulation of these results has taken place; however the following table (Table 12) provides the raw ash value of the mining sections of each seam within the five reserve blocks, as well as the proximate, CV, and sulphur, SG, FSI and Hardgrove Index of the coal product.

Table 13 provides sink float information from the three borehole sections which obtained 90%+ core recovery.

The "Birtley Coal and Mineral Testing" results and the D.E. Pearson petrographic results can be found in Volume 2.

TABLE 12: COAL QUALITY DATA

| DATA POINT           | RAW ASH | CLEAN COAL |       |       |       |            |      |      |        |        |
|----------------------|---------|------------|-------|-------|-------|------------|------|------|--------|--------|
|                      |         | M          | ASH   | VM    | FC    | Cv/<br>BTU | S    | S.G. | F.S.I. | H.G.I. |
| GRIZZLY SEAM<br>BP-6 | 49.9    | 1.29       | 40.9  | 20.1  | 52.4  | 5,973      | 0.27 | 1.65 | 1.0    | N.S.S  |
| SNT 12               | 42.4    | 6.10       | 26.45 | 23.12 | 44.34 | 8,804      | 0.35 | 1.59 | N.A.   | N.S.S  |
| SNT 17               | 33.3    | 6.0        | 16.6  | 27.7  | 49.7  | -          | 0.36 | 1.58 | 0      | 105    |
| Average (Blk. A)     | 41.9    | 4.5        | 28.0  | 23.6  | 48.8  | 7,389      | 0.33 | 1.61 | -      | -      |
| BP-7                 | 26.3    | 0.67       | 13.04 | 21.15 | 65.14 | 13,077     | 0.35 | 1.38 | 1.5    | 103    |
| SNT 25               | 30.9    | 1.06       | 21.60 | 20.70 | 56.64 | 11,534     | 0.33 | 1.46 | 1.0    | 60     |
| Average (Blk. B)     | 28.6    | 0.9        | 17.3  | 20.9  | 60.9  | 12,306     | 0.34 | 1.42 | 1.25   | 82     |
| BP2                  | 29.3    | 1.1        | 22.96 | 18.78 | 57.16 | 11,318     | 0.49 | 1.50 | 3.8    | 63     |
| SNT 20               | 16.9    | 4.36       | 12.04 | 27.67 | 55.94 | 10,336     | 0.33 | 1.52 | N.A.   | 94     |
| Average (Blk. C)     | 23.1    | 2.7        | 17.5  | 23.2  | 56.6  | 10,827     | 0.41 | 1.51 | 3.8    | 78.5   |
| BP1                  | 21.5    | 1.24       | 13.25 | 20.67 | 64.84 | 13,137     | 0.36 | 1.39 | 1.8    | 53     |
| SNT 18               | 42.6    | 3.96       | 18.29 | 23.62 | 54.13 | 10,473     | 0.33 | 1.51 | N.A.   | 83     |
| SNT 28               | 35.0    | 8.23       | 27.64 | 21.60 | 42.53 | 8,445      | 0.36 | 1.60 | 0      | 100    |
| Average (Blk. D)     | 33.0    | 4.5        | 19.7  | 22.0  | 53.8  | 10,685     | 0.35 | 1.50 | 1.8    | 79     |
| PUMP SEAM<br>BP1     | 22.4    | 1.17       | 12.54 | 23.14 | 63.15 | 13,115     | 0.40 | 1.39 | 2.7    | 55     |
| SNT 19               | 20.6    | 5.58       | 13.48 | 27.08 | 53.87 | 10,378     | 0.39 | 1.49 | N.A.   | 83     |
| Average (Blk. D)     | 21.5    | 3.4        | 13.0  | 25.1  | 58.5  | 11,747     | 0.40 | 1.44 | 2.7    | 69     |
| B SEAM<br>BP13       | 21.6    | 0.72       | 8.16  | 25.60 | 65.52 | 13,998     | 0.35 | 1.31 | 2.3    | 105    |
| B LOWER SEAM<br>BP13 | 25.8    | 0.84       | 15.11 | 22.30 | 61.75 | 12,797     | 0.38 | 1.40 | 1.49   | N.S.S  |
| C SEAM<br>BP13       | 11.4    | 0.68       | 5.52  | 24.62 | 69.15 | 14,376     | 0.34 | 1.32 | 2.3    | 120    |
| C LOWER SEAM<br>BP13 | 21.2    | 0.67       | 10.80 | 22.54 | 65.99 | 13,452     | 0.29 | 1.37 | 2.19   | 91     |
| ALL SEAMS            |         |            |       |       |       |            |      |      |        |        |
| Average (Blk. E)     | 20.0    | 0.70       | 9.9   | 23.8  | 65.6  | 13,656     | 0.34 | 1.35 | 2.07   | 105    |

Note: All Results on Air-Dried Basis

N.S.S. - Not Sufficient Sample  
N.A. - Non Agglomerating

TABLE 13

SINK FLOAT ANALYSIS adb + 28 M

| <u>Composite*</u><br><u>Sample No.</u> | <u>S.G.</u><br><u>Fraction</u> | <u>CUMULATIVE</u> |             |
|--|--------------------------------|-------------------|-------------|
|  |                                | <u>WT%</u>        | <u>ASH%</u> |
| Grizzly 703                            | 1.80                           | 72.1              | 14.2        |
| B Lower 705                            | 1.80                           | 69.8              | 13.5        |
| C Lower 707                            | 1.80                           | 75.8              | 11.2        |

\*Composite Sample No. 703 - 81/7/1/1, 81/7/1/2,  
81/7/1/3

705 - 81/13/3/1 thru to  
81/13/3/6

707 - 81/13/5/1 thru to  
81/13/5/9

12. 1981 FINANCIAL STATEMENTS

The following list illustrates expense category, principal contractors and amounts expended. Note: actual cost figures are subject to minor changes due to updates.

|                             |   |            |
|-----------------------------|---|------------|
| Core Drilling               | D. W. Coates Enterprises                                      | 307,607.08 |
| Helicopter Services         | Maple Leaf Helicopter   | 148,905.31 |
|                             | Northern Mountain   | 11,736.90  |
|                             | Highland Helicopters  | 5,843.25   |
|                             | Fuel  | 7,567.57   |
| Accommodation & Catering    | Pine Cone Motor Inn   | 30,415.00  |
| Transportation              | Canuck Truck Rentals  | 7,665.00   |
| Communications              | Canadian Marconi  | 2,574.00   |
| Field Equipment             | Ribtor's, Caldraft, Barotto Sports, Beaver, Northern Metallic | 3,685.00   |
| Geophysical Logging         | Century Geophysical Corp.                                     | 32,217.69  |
| Drill Site Preparation      | Peace Dozing & Contracting                                    | 16,107.00  |
| Laboratory                  | Wayne Asleson   | 703.50     |
|                             | Birtley Testing   | 13,000.00  |
| Petrophysical Analysis      | D. Marchioni  | 1,500.00   |
|                             | D. Pearson  | 2,500.00   |
| Travel                      | Pacific Western Airlines                                      | 9,091.50   |
| Reproduction & Photocopying | Alberta Reprographics, Rileys, & West Canadian Color          | 1,320.00   |
| Contract Personnel          | Summer Students   | 15,950.00  |



12. 1981 FINANCIAL STATEMENT (Continued)

|  |              |                  |
|--|--------------|------------------|
| BP Salaries<br>'Field'                   | BP Employees | 45,100.00        |
| BP Salaries<br>'Backup'<br>(to year end) | BP Employees | <u>21,450.00</u> |
|  |              | \$684,938.80     |

All direct charges relating to the exploration program have a 10% overhead charge extrinsic to them, whereas all indirect costs have a 5% overhead charge applied to them.

13. CONCLUSIONS

The 1981 Rocky Creek coal exploration program has substantiated many of the conclusion put forward after the 1980 program, and has brought the project to a stage where initial mine feasibility studies can be carried out. (See the Preliminary Mining Feasibility Study prepared by Marston & Marston).

The major conclusion drawn from the 1981 program is that there are five blocks where mineable resources of Lower Gething coals are present within the area formerly known as Sukunka North. Blocks A, B, C and D contain resources within the highly variable Grizzly Zone, whilst block E resources are from the 'B' seam, 'B Lower', 'C' seam and 'C Lower'. Block D also contains resources from the Pump Zone.

The in situ resources from Blocks A, B, D and E amount to 19.4 MTe, with all four blocks having the potential of being mined by surface methods. Ratios would be in the 3.0:1 to 5.0:1 range. An additional 5.27 MTe at a ratio of 18.7:1 are available from Block D.

13. CONCLUSIONS (Continued)

Generally the strata within the reserve blocks are gently undulating with dips ranging from 0 to 16°. The structural model put forward after the 1980 program which evoked a N.W. - S.E trending syncline in the Sukunka North area containing possible B seam, Pump and Grizzly Zones has been revised. The syncline is still present but is contained within sub-Grizzly seam strata and as a result eliminates any reserve potential in the northern portion of the Jilg and Sukunka North areas.

The 1981 drilling proved the Cadomin Seam to be a generally thin seam subjected to washout conditions with no reserve potential.

The two holes drilled within the Merrick area into the Minnes Group contained the Hill Seam which might have some underground potential, with thicknesses ranging from 1.5 to 2.5 m. Several thinner seams were also found with thicknesses in the 1.0 to 1.5 range.

14. RECOMMENDATIONS

From the conclusions arrived at as a result of the exploration programs carried out on the Rocky Creek property over the last three years the following recommendations can be made.

14.1 Surrendering of Licences

With reference to the licence map (Map 1) the following licences are recommended for surrender due to the lack of potential mineable coal seams:

|               |                 |                                |                   |
|---------------|-----------------|--------------------------------|-------------------|
| Triangle Area | Licence Numbers | 5259-5261<br>5264-5266         | ( 6)              |
| Merrick Area  | Licence Numbers | 5244-5248<br>5251              | ( 6)              |
| Jilg Area     | Licence Numbers | 5267-5269<br>5271<br>5273-5278 | <u>(10)</u><br>22 |

Upon surrender of the above mentioned 22 coal Licences, the Rocky Creek Property will consist of a total of 33 licences. From these 33 licences, 4 new groupings will be established, with all to be renewed December 31, 1981. The property will now consist of approximately 9,740 hectares.

14. RECOMMENDATION (Continued)

14.2 1982 Rocky Creek Exploration Program

A further exploration program is proposed for the summer of 1982 so as to:

- (a) better define the outcrops of the various mineable coal zones by having data points at 100 m spacing.
- (b) obtain additional information on the in-seam stratigraphy of the mineable coal zones.
- (c) better define the raw coal quality of the six mineable coal zones.
- (d) establish the washability characteristics of the six mineable coal zones.
- (e) provide more information on the roof and floor material of each mineable coal zone, as well as the overburden found in each site area.
- (f) provide additional information on the Minnes coals in the central portion of the Merrick block and the eastern portion of the Sukunka North block.

One way of obtaining the above objectives would be to have a land accessed program comprised of:-

- (a) Approx. 7 boreholes totalling 400 m.
- (b) Approx. 140 mechanically dug trenches.
- (c) 9 Test pits.

14. RECOMMENDATION (Continued)

14.2 1982 Rocky Creek Exploration Program (Continued)

This program would require one, or possibly two, bridges to be built across the Sukunka River and the construction of approx. 20 km of new road. Some of the newly constructed road would be used as a haul road during the mining phase. There are distinct advantages in commencing some of the bridge building and road construction this fall although the exploration work would take place in July, August and September, 1982.

The program would be based out of the Sukunka Gas Plant camp at mile 32 on the Sukunka Rd. with BP staff in charge of the geology and field logistics and contractors handling the bridge and road construction, drilling and analytical aspects.

An air photo survey would also be run at the end of the program so as to locate drillholes, test pits and access roads.

14. RECOMMENDATION (Continued)

14.2 1982 Rocky Creek Exploration Program (Continued)

Various environmental, geotechnical and hydrological studies would also take place during the field program so as to enable the commencement of final mining feasibility studies during the winter of 1982/3.

ROCKY CREEK SAMPLE IDENTIFICATION

| <u>BOREHOLE</u> | <u>BP SAMPLE NUMBER</u>  | <u>LAB SAMPLE NUMBER</u> | <u>THICKNESS M</u> | <u>DEPTH M</u> | <u>SEAM IDENTIFICATION</u> |
|-----------------|--|--------------------------|--------------------|----------------|----------------------------|
| BP 81-6         | 81/6/1/1   | 635                      | 0.10               | 21.49          | Grizzly                    |
| BP 81-6         | 81/6/1/2   | 636                      | 0.12               | 21.70          | Grizzly                    |
| BP 81-6         | 81/6/1/3   | 637                      | 0.17               | 21.87          | Grizzly                    |
| BP 81-6         | 81/6/1/4   | 638                      | 0.05               | 22.07          | Grizzly                    |
| BP 81-6         | 81/6/1/5   | 639                      | 0.06               | 22.13          | Grizzly                    |
| BP 81-6         | 81/6/1/6   | 640                      | 0.23               | 22.36          | Grizzly                    |
| BP 81-6         | 81/6/1/7   | 641                      | 0.09               | 22.45          | Grizzly                    |
| BP 81-6         | 81/6/1/8   | 642                      | 0.31               | 22.76          | Grizzly                    |
| BP 81-6         | 81/6/1/9   | 643                      | 0.18               | 23.14          | Grizzly                    |
| BP 81-6         | 81/6/1/10  | 644                      | 0.12               | 23.26          | Grizzly                    |
| BP 81-6         | 81/6/1/11  | 645                      | 0.20               | 23.70          | Grizzly                    |
| BP 81-6         | 81/6/1/12  | 646                      | 0.04               | 23.74          | Grizzly                    |
| BP 81-6         | 81/6/1/13  | 647                      | 0.27               | 24.01          | Grizzly                    |
| BP 81-6         | 81/6/1/1 thru to 81/6/1/10; Composite Sample Number 702 -<br>for petrographic analysis.  |                          |                    |                |                            |
| BP 81-7         | 81/1/7/1   | 622                      | 0.43               | 44.13          | Grizzly                    |
| BP 81-7         | 81/1/7/2   | 623                      | 0.79               | 44.95          | Grizzly                    |
| BP 81-7         | 81/1/7/3   | 624                      | 0.53               | 45.55          | Grizzly                    |
| BP 81-7         | 81/1/7/1 thru to 81/7/1/3; Composite Sample Number 703 -<br>for petrographic analysis    |                          |                    |                |                            |
| BP 81-13        | 81/13/1/R  | 596                      | 0.08               | 46.82          | Above B Seam               |
| BP 81-13        | 81/13/1/1  | 597                      | 0.27               | 47.19          | Above B Seam               |
| BP 81-13        | 81/13/1/2  | 598                      | 0.15               | 47.34          | Above B Seam               |
| BP 81-13        | 81/13/2/1  | 599                      | 0.69               | 49.55          | B Seam                     |
| BP 81-13        | 81/13/2/2  | 600                      | 0.77               | 50.32          | B Seam                     |
| BP 81-13        | 81/13/2/3  | 601                      | 0.12               | 50.55          | B Seam                     |
| BP 81-13        | 81/13/2/4  | 602                      | 0.46               | 51.06          | B Seam                     |
| BP 81-13        | 81/13/2/5  | 603                      | 0.02               | 51.40          | B Seam                     |
| BP 81-13        | 81/13/2/6  | 604                      | 0.16               | 51.56          | B Seam                     |
| BP 81-13        | 81/13/2/7  | 605                      | 0.13               | 51.89          | B Seam                     |
| BP 81-13        | 81/13/2/1 thru to 81/13/2/5: Composite Sample Number 704 -<br>for petrographic analysis. |                          |                    |                |                            |



| <u>BOREHOLES</u> | <u>BP SAMPLE NUMBER</u>      | <u>LAB SAMPLE NUMBER</u> | <u>THICKNESS M</u> | <u>DEPTH M</u> | <u>SEAM IDENTIFICATION</u>                                 |
|------------------|------------------------------|--------------------------|--------------------|----------------|--|
| BP 81-13         | 81/13/3/1                    | 574                      | 0.26               | 61.48          | B Lower Seam   |
| BP 81-13         | 81/13/3/2                    | 575                      | 0.47               | 61.95          | B Lower Seam   |
| BP 81-13         | 81/13/3/3                    | 576                      | 0.34               | 62.45          | B Lower Seam   |
| BP 81-13         | 81/13/3/4                    | 577                      | 0.08               | 62.53          | B Lower Seam   |
| BP 81-13         | 81/13/3/5                    | 578                      | 0.18               | 62.71          | B Lower Seam   |
| BP 81-13         | 81/13/3/6                    | 579                      | 0.03               | 62.91          | B Lower Seam   |
| BP 81-13         | 81/13/3/7                    | 580                      | 0.05               | 62.96          | B Lower Seam   |
| BP 81-13         | 81/13/3/1 thru to 81/13/3/6: |                          |                    |                | Composite Sample Number 705 -<br>for petrographic analysis |
| BP 81-13         | 81/13/4/1                    | 581                      | 0.47               | 72.53          | C Seam   |
| BP 81-13         | 81/13/4/2                    | 582                      | 0.04               | 72.57          | C Seam   |
| BP 81-13         | 81/13/4/3                    | 583                      | 0.10               | 72.67          | C Seam   |
| BP 81-13         | 81/13/4/4                    | 584                      | 0.25               | 72.92          | C Seam   |
| BP 81-13         | 81/13/4/5                    | 585                      | 0.77               | 73.69          | C Seam   |
| BP 81-13         | 81/13/4/6                    | 586                      | 0.51               | 74.59          | C Seam   |
| BP 81-13         | 81/13/4/1 thru to 81/13/4/6: |                          |                    |                | Composite Sample Number 706 -<br>for petrographic analysis |
| BP 81-13         | 81/13/5/1                    | 587                      | 0.69               | 78.57          | C Lower Seam   |
| BP 81-13         | 81/13/5/2                    | 588                      | 0.67               | 79.24          | C Lower Seam   |
| BP 81-13         | 81/13/5/3                    | 589                      | 0.44               | 79.68          | C Lower Seam   |
| BP 81-13         | 81/13/5/4                    | 590                      | 0.19               | 79.87          | C Lower Seam   |
| BP 81-13         | 81/13/5/5                    | 591                      | 0.18               | 80.05          | C Lower Seam   |
| BP 81-13         | 81/13/5/6                    | 592                      | 0.28               | 80.35          | C Lower Seam   |
| BP 81-13         | 81/13/5/7                    | 593                      | 0.13               | 80.48          | C Lower Seam   |
| BP 81-13         | 81/13/5/8                    | 594                      | 0.29               | 80.81          | C Lower Seam   |
| BP 81-13         | 81/13/5/9                    | 595                      | 0.16               | 80.97          | C Lower Seam   |
| BP 81-13         | 81/13/5/1 thru to 81/13/5/9: |                          |                    |                | Composite Sample Number 707 -<br>for petrographic analysis |

ROCKY CREEK SAMPLE IDENTIFICATION

| <u>TRENCH</u> | <u>BP SAMPLE NUMBER</u>       | <u>LAB SAMPLE NUMBER</u> | <u>THICKNESS M</u> | <u>DEPTH M</u>   | <u>SEAM IDENTIFICATION</u> |
|---------------|-------------------------------|--------------------------|--------------------|--|----------------------------|
| SNTR 17       | SNTR 17/1                     | 710                      | 0.55               | 0.54   | Grizzly                    |
| SNTR 17       | SNTR 17/2                     | 711                      | 0.64               | 1.18   | Grizzly                    |
| SNTR 18       | SNTR 18/8                     | 712                      | 0.21               | 4.20   | Grizzly                    |
| SNTR 18       | SNTR 18/9                     | 713                      | 0.07               | 3.99   | Grizzly                    |
| SNTR 18       | SNTR 18/10                    | 714                      | 0.45               | 3.92   | Grizzly                    |
| SNTR 18       | SNTR 18/11                    | 715                      | 0.08               | 3.47   | Grizzly                    |
| SNTR 18       | SNTR 18/12                    | 716                      | 0.30               | 3.39   | Grizzly                    |
| SNTR 25       | SNTR 25/1                     | 610                      | 0.08               | 0.08   | Grizzly                    |
| SNTR 25       | SNTR 25/2                     | 611                      | 0.31               | 0.39   | Grizzly                    |
| SNTR 25       | SNTR 25/3                     | 612                      | 0.50               | 0.89   | Grizzly                    |
| SNTR 25       | SNTR 25/4                     | 613                      | 0.32               | 1.21   | Grizzly                    |
| SNTR 25       | SNTR 25/5                     | 614                      | 0.06               | 1.27   | Grizzly                    |
| SNTR 25       | SNTR 25/6                     | 615                      | 0.14               | 1.41   | Grizzly                    |
| SNTR 25       | SNTR 25/7                     | 616                      | 0.10               | 1.51   | Grizzly                    |
| SNTR 25       | SNTR 25/8                     | 617                      | 0.13               | 1.64   | Grizzly                    |
| SNTR 25       | SNTR 25/9                     | 618                      | 0.53               | 2.16   | Grizzly                    |
| SNTR 25       | SNTR 25/10                    | 619                      | 0.05               | 2.21   | Grizzly                    |
| SNTR 25       | SNTR 25/10A                   | 620                      | 0.05               | 2.21   | Grizzly                    |
| SNTR 25       | SNTR 25/11                    | 621                      | 0.53               | 2.74   | Grizzly                    |
| SNTR 25       | SNTR 25/5 thru to SNTR 25/11: |                          |                    | Composite Sample Number 708 - for petrographic analysis. |                            |
| SNTR 28       | SNTR 28/1                     | 625                      | 0.42               | 6.93   | Grizzly                    |
| SNTR 28       | SNTR 28/2                     | 626                      | 0.14               | 6.51   | Grizzly                    |
| SNTR 28       | SNTR 28/3                     | 627                      | 1.16               | 6.37   | Grizzly                    |
| SNTR 28       | SNTR 28/4                     | 628                      | 0.87               | 5.21   | Grizzly                    |
| SNTR 28       | SNTR 28/5                     | 629                      | 0.19               | 4.34   | Grizzly                    |
| SNTR 28       | SNTR 28/6                     | 630                      | 0.08               | 4.15   | Grizzly                    |
| SNTR 28       | SNTR 28/7                     | 631                      | 0.51               | 4.07   | Grizzly                    |
| SNTR 28       | SNTR 28/8                     | 632                      | 1.12               | 3.56   | Grizzly                    |
| SNTR 28       | SNTR 28/9                     | 633                      | 0.13               | 2.44   | Grizzly                    |
| SNTR 28       | SNTR 28/10                    | 634                      | 0.33               | 2.31   | Grizzly                    |
| SNTR 28       | SNTR 28/11                    | 648                      | 1.22               | 1.98   | Grizzly                    |

| <u>TRENCH</u> | <u>BP SAMPLE NUMBER</u>  | <u>LAB SAMPLE NUMBER</u> | <u>THICKNESS M</u> | <u>DEPTH M</u> | <u>SEAM IDENTIFICATION</u> |
|---------------|--|--------------------------|--------------------|----------------|----------------------------|
| SNTR 28       | SNTR 28/12   | 649                      | 0.76               | 0.76           | Grizzly                    |
| SNTR 28       | SNTR 28/13   | 650                      | 0.12+              | 0.00           | Grizzly                    |
| SNTR 28       | SNTR 28/1 thru to SNTR 28/12: Composite Sample Number 709 for petrographic analysis. |                          |                    |                |                            |
| SNTR 29       | SNTR 29/1  | 651                      | 0.51               | 1.14           | Grizzly                    |
| SNTR 29       | SNTR 29/2  | 652                      | 0.33               | 1.47           | Grizzly                    |
| SNTR 29       | SNTR 29/3  | 653                      | 0.25               | 1.72           | Grizzly                    |
| SNTR 29       | SNTR 29/4  | 654                      | 0.33               | 2.05           | Grizzly                    |
| SNTR 29       | SNTR 29/5  | 655                      | 0.63               | 3.14           | Grizzly                    |
| SNTR 29       | SNTR 29/6  | 656                      | 0.64               | 4.17           | Grizzly                    |
| SNTR 29       | SNTR 29/7  | 657                      | 0.64               | 4.81           | Grizzly                    |
| SNTR 29       | SNTR 29/8  | 658                      | 0.49               | 5.30           | Grizzly                    |
| SNTR 29       | SNTR 29/9  | 659                      | 0.51               | 5.81           | Grizzly                    |
| SNTR 29       | SNTR 29/10   | 660                      | 0.24               | 6.05           | Grizzly                    |
| SNTR 29       | SNTR 29/11   | 661                      | 0.18+              | 6.23+          | Grizzly                    |

WM.P.L./djm

November 26, 1981

CLIENT : BP EXPLORATION CANADA

PROJECT: 81/7/1 thru 3 Composite

LAB NO.: 703

SIZE AND RAW ANALYSIS,adb

| SIZE Fraction | WT%  | RM% | ASH% | VOL% | F.C.% | S%   | CV Cal/gm |
|---------------|------|-----|------|------|-------|------|-----------|
| +28M          | 92.7 | -   | -    | -    | -     | -    | -         |
| -28M          | 7.3  | 0.9 | 22.8 | 20.8 | 55.5  | 0.37 | 6390      |

SINK-FLOAT ANALYSIS,adb + 28M

| S.G. FRACTION | WT%  | RM% | ASH% | VOL% | FC%  | S%   | CV Cal/gm | CUMULATIVE WT% | ASH% |
|---------------|------|-----|------|------|------|------|-----------|----------------|------|
| - 1.50        | 56.3 | 0.5 | 7.6  | 22.4 | 69.5 | 0.38 | 7815      | 56.3           | 7.6  |
| 1.50- 1.60    | 6.9  | 0.7 | 30.9 | 20.3 | 48.1 | 0.33 | 5592      | 63.2           | 10.1 |
| 1.60- 1.80    | 8.9  | 0.9 | 43.3 | 18.1 | 37.7 | 0.27 | 4518      | 72.1           | 14.2 |
| + 1.80        | 27.9 | 0.9 | 75.3 | -    | -    | 0.16 | -         | 100.0          | 31.3 |

#703,705,707 were part of a series prepared for petrographic analysis.

CLIENT : BP EXPLORATION CANADA  
 PROJECT: 81/13/3/1 thru 6 Composite  
 LAB NO.: 705

SIZE AND RAW ANALYSIS,adb

| SIZE Fraction | WT%  | RM% | ASH% | VOL% | F.C.% | S%   | CV Cal/gm |
|---------------|------|-----|------|------|-------|------|-----------|
| +28M          | 94.3 | -   | -    | -    | -     | -    | -         |
| -28M          | 5.7  | 1.0 | 22.5 | 1.0  | 75.5  | 0.38 | 6388      |

SINK-FLOAT ANALYSIS,adb + 28M

| S:G: FRACTION | WT%  | RM% | ASH% | VOL% | FC%  | S%   | CV Cal/gm | CUMULATIVE WT% | ASH% |
|---------------|------|-----|------|------|------|------|-----------|----------------|------|
| - 1.50        | 58.2 | 0.5 | 8.5  | 22.9 | 68.1 | 0.42 | 7734      | 58.2           | 8.5  |
| 1.50- 1.60    | 5.3  | 0.5 | 29.7 | 18.5 | 51.3 | 0.32 | 5785      | 63.5           | 10.3 |
| 1.60- 1.80    | 6.3  | 0.4 | 45.7 | 16.5 | 37.4 | 0.28 | 4328      | 69.8           | 13.5 |
| + 1.80        | 30.2 | 0.5 | 71.7 | -    | -    | 0.12 | -         | 100.0          | 31.1 |

#703,705,707 were part of a series prepared for petrographic analysis.

CLIENT : BP EXPLORATION CANADA

PROJECT: 81/13/5/1 thru 9 Composite

LAB NO.: 707

SIZE AND RAW ANALYSIS,adb

| SIZE Fraction | WT%  | RM% | ASH% | VOL% | F.C.% | S%   | CV Cal/gm |
|---------------|------|-----|------|------|-------|------|-----------|
| +28M          | 94.7 | -   | -    | -    | -     | -    | -         |
| -28M          | 5.3  | 0.9 | 31.7 | 19.4 | 48.0  | 0.23 | 5433      |

SINK-FLOAT ANALYSIS,adb + 28M

| S.G. FRACTION | WT%  | RM% | ASH% | VOL% | FC%  | S%   | CV Cal/gm | CUMULATIVE WT% | ASH% |
|---------------|------|-----|------|------|------|------|-----------|----------------|------|
| - 1.50        | 65.3 | 0.5 | 7.2  | 22.6 | 69.7 | 0.29 | 7855      | 65.3           | 7.2  |
| 1.50- 1.60    | 4.7  | 0.7 | 30.0 | 20.5 | 48.8 | 0.27 | 5652      | 70.0           | 8.7  |
| 1.60- 1.80    | 5.8  | 0.7 | 41.5 | 18.9 | 38.9 | 0.20 | 4504      | 75.8           | 11.2 |
| + 1.80        | 24.2 | 0.5 | 75.8 | -    | -    | 0.06 | -         | 100.0          | 26.9 |

#703,705,707 were part of a series prepared for petrographic analysis.

CLIENT : BP CANADA LIMITED

PROJECT: 81/ 6/1 Samples

RAW COAL ANALYSIS, air dried basis

ASH FUSION TEMPERATURES (°F)

SAMPLE # 1 LAB NO. 635

SAMPLE # 4 LAB NO.638

| ATMOSPHERE | IDT  | ST    | HT | FT | ATMOSPHERE | IDT   | ST | HT | FT |
|------------|------|-------|----|----|------------|-------|----|----|----|
| OXIDIZING  | 2730 | 2800+ |    |    | OXIDIZING  | 2800+ |    |    |    |
| REDUCING   | 2690 | 2800+ |    |    | REDUCING   | 2800+ |    |    |    |

SAMPLE # 2 LAB NO. 636

SAMPLE # 5 LAB NO.639

| ATMOSPHERE | IDT  | ST    | HT | FT | ATMOSPHERE | IDT   | ST | HT | FT |
|------------|------|-------|----|----|------------|-------|----|----|----|
| OXIDIZING  | 2780 | 2800+ |    |    | OXIDIZING  | 2800+ |    |    |    |
| REDUCING   | 2740 | 2800+ |    |    | REDUCING   | 2800  |    |    |    |

SAMPLE # 3 LAB NO. 637

SAMPLE # 6 LAB NO.640

| ATMOSPHERE | IDT   | ST | HT | FT | ATMOSPHERE | IDT   | ST | HT | FT |
|------------|-------|----|----|----|------------|-------|----|----|----|
| OXIDIZING  | 2800+ |    |    |    | OXIDIZING  | 2800+ |    |    |    |
| REDUCING   | 2800+ |    |    |    | REDUCING   | 2800+ |    |    |    |

Birtley Coal  
& Minerals Testing

A DIVISION OF GREAT WEST STEEL INDUSTRIES LTD.

CLIENT : BP CANADA LIMITED

PROJECT: 81/6 /1 Samples

RAW COAL ANALYSIS, air dried basis

ASH FUSION TEMPERATURES (°F)

SAMPLE # 7 LAB NO. 641

SAMPLE # 11 LAB NO. 645

| ATMOSPHERE | IDT   | ST | HT | FT | ATMOSPHERE | IDT  | ST    | HT   | FT    |
|------------|-------|----|----|----|------------|------|-------|------|-------|
| OXIDIZING  | 2800+ |    |    |    | OXIDIZING  | 2770 | 2800+ |      |       |
| REDUCING   | 2800+ |    |    |    | REDUCING   | 2680 | 2760  | 2780 | 2800+ |

SAMPLE # 8 LAB NO. 642

SAMPLE # 12 LAB NO. 646

| ATMOSPHERE | IDT   | ST    | HT | FT | ATMOSPHERE | IDT  | ST    | HT   | FT    |
|------------|-------|-------|----|----|------------|------|-------|------|-------|
| OXIDIZING  | 2800+ |       |    |    | OXIDIZING  | 2460 | 2800+ |      |       |
| REDUCING   | 2780  | 2800+ |    |    | REDUCING   | 2290 | 2720  | 2780 | 2800+ |

SAMPLE # 9 LAB NO. 643

SAMPLE # 13 LAB NO. 647

| ATMOSPHERE | IDT    | ST    | HT | FT | ATMOSPHERE | IDT  | ST    | HT   | FT    |
|------------|--------|-------|----|----|------------|------|-------|------|-------|
| OXIDIZING  | 2880 + |       |    |    | OXIDIZING  | 2660 | 2800+ |      |       |
| REDUCING   | 2720   | 2800+ |    |    | REDUCING   | 2600 | 2720  | 2790 | 2800+ |

SAMPLE #10 LAB NO. 644

| ATMOSPHERE | IDT  | ST    | HT | FT | ATMOSPHERE | IDT | ST | HT | FT |
|------------|------|-------|----|----|------------|-----|----|----|----|
| OXIDIZING  | 2710 | 2800+ |    |    | OXIDIZING  |     |    |    |    |
| REDUCING   | 2700 | 2800+ |    |    | REDUCING   |     |    |    |    |

Birtley Coal  
& Minerals Testing

A DIVISION OF GREAT WEST STEEL INDUSTRIES LTD.



CLIENT : BP CANADA LTD.

PROJECT: 81/7/1

RAW COAL ANALYSIS, adb

ASH FUSION TEMPERATURES (°F)

LAB NO. 622

SAMPLE NO. 1

| ATMOSPHERE | IDT  | ST   | HT   | FT   |
|------------|------|------|------|------|
| OXIDIZING  | 2400 | 2620 | 2720 | 2760 |
| REDUCING   | 2380 | 2640 | 2690 | 2760 |

LAB NO: 623

SAMPLE NO. 2

| ATMOSPHERE | IDT  | ST   | HT   | FT    |
|------------|------|------|------|-------|
| OXIDIZING  | 2560 | 2700 | 2720 | 2750  |
| REDUCING   | 2510 | 2660 | 2690 | 2800+ |

LAB NO. 624

SAMPLE NO. 3

| ATMOSPHERE | IDT  | ST   | HT   | FT    |
|------------|------|------|------|-------|
| OXIDIZING  | 2580 | 2750 | 2760 | 2800+ |
| REDUCING   | 2490 | 2720 | 2740 | 2780  |

Birtley Coal  
& Minerals Testing

A DIVISION OF GREAT WEST STEEL INDUSTRIES LTD.

CLIENT : BP CANADA LTD.

PROJECT: 81/13/1

RAW COAL ANALYSIS, adb

ASH FUSION TEMPERATURES (°F)

LAB NO. 597

SAMPLE NO. 1

| ATMOSPHERE | IDT  | ST    | HT | FT |
|------------|------|-------|----|----|
| OXIDIZING  | 2720 | 2800+ |    |    |
| REDUCING   | 2630 | 2800+ |    |    |

LAB NO. 598

SAMPLE NO. 2

| ATMOSPHERE | IDT  | ST    | HT | FT |
|------------|------|-------|----|----|
| OXIDIZING  | 2740 | 2800+ |    |    |
| REDUCING   | 2620 | 2800+ |    |    |

**Birtley Coal  
& Minerals Testing**

A DIVISION OF GREAT WEST STEEL INDUSTRIES LTD.

CLIENT : BP CANADA LIMITED

PROJECT: 81/13/2 Samples

RAW COAL ANALYSIS, air dried basis

ASH FUSION TEMPERATURES (°F)

SAMPLE # 1

LAB NO.599

SAMPLE # 6

LAB NO. 604

| ATMOSPHERE | IDT  | ST   | HT   | FT   | ATMOSPHERE | IDT  | ST   | HT   | FT    |
|------------|------|------|------|------|------------|------|------|------|-------|
| OXIDIZING  | 2210 | 2330 | 2400 | 2470 | OXIDIZING  | 2630 | 2750 | 2770 | 2800+ |
| REDUCING   | 2210 | 2290 | 2310 | 2420 | REDUCING   | 2510 | 2700 | 2750 | 2800  |

SAMPLE # 2

LAB NO.600

SAMPLE # 7

LAB NO. 605

| ATMOSPHERE | IDT  | ST   | HT   | FT   | ATMOSPHERE | IDT  | ST   | HT   | FT    |
|------------|------|------|------|------|------------|------|------|------|-------|
| OXIDIZING  | 2250 | 2330 | 2400 | 2490 | OXIDIZING  | 2650 | 2760 | 2780 | 2800+ |
| REDUCING   | 2220 | 2280 | 2290 | 2420 | REDUCING   | 2360 | 2680 | 2750 | 2800  |

SAMPLE # 4 LAB NO. 602

SAMPLE #

| ATMOSPHERE | IDT   | ST | HT | FT | ATMOSPHERE | IDT | ST | HT | FT |
|------------|-------|----|----|----|------------|-----|----|----|----|
| OXIDIZING  | 2800+ |    |    |    | OXIDIZING  |     |    |    |    |
| REDUCING   | 2800+ |    |    |    | REDUCING   |     |    |    |    |

Birtley Coal  
& Minerals Testing

A DIVISION OF GREAT WEST STEEL INDUSTRIES LTD.

CLIENT : BP CANADA LIMITED

PROJECT: 81/13/ 3 Samples

RAW COAL ANALYSIS, air dried basis

ASH FUSION TEMPERATURES (°F)

SAMPLE # 1 LAB NO.574

SAMPLE # 5 LAB NO.578

| ATMOSPHERE | IDT  | ST    | HT | FT | ATMOSPHERE | IDT  | ST    | HT   | FT    |
|------------|------|-------|----|----|------------|------|-------|------|-------|
| OXIDIZING  | 2760 | 2800+ |    |    | OXIDIZING  | 2620 | 2800+ |      |       |
| REDUCING   | 2750 | 2800+ |    |    | REDUCING   | 2600 | 2780  | 2790 | 2800+ |

SAMPLE # 2 LAB NO.575

SAMPLE # 6 LAB NO.579

| ATMOSPHERE | IDT  | ST   | HT   | FT    | ATMOSPHERE | IDT   | ST | HT | FT |
|------------|------|------|------|-------|------------|-------|----|----|----|
| OXIDIZING  | 2500 | 2760 | 2790 | 2800+ | OXIDIZING  | 2800+ |    |    |    |
| REDUCING   | 2230 | 2760 | 2780 | 2800+ | REDUCING   | 2800+ |    |    |    |

SAMPLE # 3 LAB NO.576

SAMPLE # 7 LAB NO.580

| ATMOSPHERE | IDT  | ST   | HT   | FT   | ATMOSPHERE | IDT  | ST   | HT    | FT   |
|------------|------|------|------|------|------------|------|------|-------|------|
| OXIDIZING  | 2280 | 2480 | 2600 | 2670 | OXIDIZING  | 2590 | 2780 | 2800+ |      |
| REDUCING   | 2210 | 2630 | 2700 | 2730 | REDUCING   | 2220 | 2330 | 2360  | 2650 |

SAMPLE # 4 LAB NO.577

| ATMOSPHERE | IDT  | ST    | HT    | FT | ATMOSPHERE | IDT | ST | HT | FT |
|------------|------|-------|-------|----|------------|-----|----|----|----|
| OXIDIZING  | 2680 | 2800+ |       |    | OXIDIZING  |     |    |    |    |
| REDUCING   | 2670 | 2790  | 2800+ |    | REDUCING   |     |    |    |    |

Birtley Coal  
& Minerals Testing

A DIVISION OF GREAT WEST STEEL INDUSTRIES LTD.

CLIENT : BP CANADA LIMITED

PROJECT: 81/13/4 Samples

RAW COAL ANALYSIS, air dried basis

ASH FUSION TEMPERATURES (°F)

SAMPLE # 1

LAB NO. 581

SAMPLE # 5

LAB NO. 585

| ATMOSPHERE | IDT  | ST   | HT   | FT   | ATMOSPHERE | IDT  | ST   | HT   | FT   |
|------------|------|------|------|------|------------|------|------|------|------|
| OXIDIZING  | 2240 | 2340 | 2380 | 2660 | OXIDIZING  | 2200 | 2280 | 2440 | 2650 |
| REDUCING   | 2220 | 2330 | 2360 | 2650 | REDUCING   | 2140 | 2200 | 2250 | 2640 |

SAMPLE # 2 LAB NO. 582

SAMPLE # 6 LAB NO. 586

| ATMOSPHERE | IDT  | ST   | HT   | FT   | ATMOSPHERE | IDT  | ST   | HT   | FT   |
|------------|------|------|------|------|------------|------|------|------|------|
| OXIDIZING  | 2600 | 2680 | 2720 | 2740 | OXIDIZING  | 2250 | 2280 | 2320 | 2480 |
| REDUCING   | 2180 | 2380 | 2440 | 2500 | REDUCING   | 2180 | 2250 | 2270 | 2470 |

SAMPLE # 4 LAB NO. 4

SAMPLE #

| ATMOSPHERE | IDT  | ST   | HT   | FT   | ATMOSPHERE | IDT | ST | HT | FT |
|------------|------|------|------|------|------------|-----|----|----|----|
| OXIDIZING  | 2180 | 2320 | 2680 | 2720 | OXIDIZING  |     |    |    |    |
| REDUCING   | 2100 | 2200 | 2240 | 2260 | REDUCING   |     |    |    |    |

Birtley Coal  
& Minerals Testing

A DIVISION OF GREAT WEST STEEL INDUSTRIES LTD.

CLIENT : BP CANADA LIMITED

PROJECT: 81/13/5 Samples

RAW COAL ANALYSIS, air dried basis

ASH FUSION TEMPERATURES (°F)

SAMPLE # 1 LAB NO. 587

SAMPLE # 6 LAB NO. 592

| ATMOSPHERE | IDT  | ST   | HT   | FT   | ATMOSPHERE | IDT   | ST | HT | FT |
|------------|------|------|------|------|------------|-------|----|----|----|
| OXIDIZING  | 2190 | 2300 | 2390 | 2630 | OXIDIZING  | 2800+ |    |    |    |
| REDUCING   | 2140 | 2300 | 2380 | 2530 | REDUCING   | 2800+ |    |    |    |

SAMPLE # 2 LAB NO. 588

SAMPLE # 7 LAB NO. 593

| ATMOSPHERE | IDT  | ST   | HT   | FT   | ATMOSPHERE | IDT   | ST | HT | FT |
|------------|------|------|------|------|------------|-------|----|----|----|
| OXIDIZING  | 2360 | 2630 | 2660 | 2700 | OXIDIZING  | 2800+ |    |    |    |
| REDUCING   | 2200 | 2580 | 2610 | 2690 | REDUCING   | 2800+ |    |    |    |

SAMPLE # 3 LAB NO. 589

SAMPLE # 8 LAB NO. 594

| ATMOSPHERE | IDT   | ST | HT | FT | ATMOSPHERE | IDT  | ST   | HT   | FT   |
|------------|-------|----|----|----|------------|------|------|------|------|
| OXIDIZING  | 2800+ |    |    |    | OXIDIZING  | 2310 | 2530 | 2600 | 2680 |
| REDUCING   | 2800+ |    |    |    | REDUCING   | 2150 | 2300 | 2340 | 2360 |

SAMPLE # 4 LAB NO. 590

| ATMOSPHERE | IDT   | ST | HT | FT | ATMOSPHERE | IDT | ST | HT | FT |
|------------|-------|----|----|----|------------|-----|----|----|----|
| OXIDIZING  | 2800+ |    |    |    | OXIDIZING  |     |    |    |    |
| REDUCING   | 2800+ |    |    |    | REDUCING   |     |    |    |    |

Birtley Coal  
& Minerals Testing

A DIVISION OF GREAT WEST STEEL INDUSTRIES LTD.

CLIENT : BP CANADA LIMITED

PROJECT: SNTR-25 Samples

RAW COAL ANALYSIS, air dried basis

ASH FUSION TEMPERATURES (°F)

SAMPLE # 1 LAB NO. 610

SAMPLE #8 LAB NO.617

| ATMOSPHERE | IDT   | ST | HT | FT | ATMOSPHERE | IDT   | ST | HT | FT |
|------------|-------|----|----|----|------------|-------|----|----|----|
| OXIDIZING  | 2800+ |    |    |    | OXIDIZING  | 2800+ |    |    |    |
| REDUCING   | 2800+ |    |    |    | REDUCING   | 2800+ |    |    |    |

SAMPLE # 2 LAB NO. 611

SAMPLE #9 LAB NO.618

| ATMOSPHERE | IDT   | ST | HT | FT | ATMOSPHERE | IDT  | ST   | HT   | FT    |
|------------|-------|----|----|----|------------|------|------|------|-------|
| OXIDIZING  | 2800+ |    |    |    | OXIDIZING  | 2520 | 2740 | 2760 | 2800+ |
| REDUCING   | 2800+ |    |    |    | REDUCING   | 2520 | 2710 | 2760 | 2790  |

SAMPLE # 3 LAB NO.612

SAMPLE #10A LAB NO.620

| ATMOSPHERE | IDT  | ST    | HT | FT | ATMOSPHERE | IDT  | ST   | HT   | FT   |
|------------|------|-------|----|----|------------|------|------|------|------|
| OXIDIZING  | 2740 | 2800+ |    |    | OXIDIZING  | 2360 | 2700 | 2740 | 2770 |
| REDUCING   | 2730 | 2800+ |    |    | REDUCING   | 2350 | 2400 | 2420 | 2440 |

SAMPLE #7 LAB NO. 616

SAMPLE #11 LAB NO.621

| ATMOSPHERE | IDT   | ST | HT | FT | ATMOSPHERE | IDT  | ST   | HT   | FT   |
|------------|-------|----|----|----|------------|------|------|------|------|
| OXIDIZING  | 2800+ |    |    |    | OXIDIZING  | 2160 | 2200 | 2380 | 2490 |
| REDUCING   | 2800+ |    |    |    | REDUCING   | 2140 | 2230 | 2350 | 2490 |

Birtley Coal  
& Minerals Testing

A DIVISION OF GREAT WEST STEEL INDUSTRIES LTD.

CLIENT : BP CANADA LIMITED

PROJECT: SNTR-28 Samples

RAW COAL ANALYSIS, air dried basis

ASH FUSION TEMPERATURES (°F)

SAMPLE # 1 LAB NO. 625

SAMPLE # 5 LAB NO. 629

| ATMOSPHERE | IDT  | ST   | HT   | FT   | ATMOSPHERE | IDT  | ST   | HT   | FT   |
|------------|------|------|------|------|------------|------|------|------|------|
| OXIDIZING  | 2350 | 2540 | 2610 | 2660 | OXIDIZING  | 2410 | 2520 | 2560 | 2690 |
| REDUCING   | 2380 | 2490 | 2520 | 2670 | REDUCING   | 2380 | 2460 | 2490 | 2630 |

SAMPLE # 2 LAB NO. 626

SAMPLE # 6 LAB NO. 630

| ATMOSPHERE | IDT  | ST   | HT   | FT   | ATMOSPHERE | IDT   | ST | HT | FT |
|------------|------|------|------|------|------------|-------|----|----|----|
| OXIDIZING  | 2420 | 2630 | 2680 | 2720 | OXIDIZING  | 2800+ |    |    |    |
| REDUCING   | 2420 | 2550 | 2640 | 2720 | REDUCING   | 2800+ |    |    |    |

SAMPLE # 3 LAB NO. 627

SAMPLE # 7 LAB NO. 631

| ATMOSPHERE | IDT  | ST   | HT   | FT   | ATMOSPHERE | IDT  | ST   | HT   | FT   |
|------------|------|------|------|------|------------|------|------|------|------|
| OXIDIZING  | 2290 | 2400 | 2470 | 2660 | OXIDIZING  | 2470 | 2690 | 2730 | 2760 |
| REDUCING   | 2280 | 2380 | 2420 | 2640 | REDUCING   | 2430 | 2480 | 2600 | 2750 |

SAMPLE #4 LAB NO. 628

SAMPLE #8 LAB NO. 632

| ATMOSPHERE | IDT  | ST   | HT   | FT   | ATMOSPHERE | IDT  | ST   | HT   | FT    |
|------------|------|------|------|------|------------|------|------|------|-------|
| OXIDIZING  | 2430 | 2650 | 2680 | 2740 | OXIDIZING  | 2590 | 2680 | 2740 | 2800+ |
| REDUCING   | 2430 | 2550 | 2590 | 2740 | REDUCING   | 2430 | 2660 | 2740 | 2800+ |

Birtley Coal  
& Minerals Testing

A DIVISION OF GREAT WEST STEEL INDUSTRIES LTD.



CLIENT : BP CANADA LIMITED

PROJECT: SNTR-28 Samples

RAW COAL ANALYSIS, air dried basis

ASH FUSION TEMPERATURES (°F)

SAMPLE # 9 LAB NO.633

SAMPLE # 12 LAB NO. 649

| ATMOSPHERE | IDT  | ST   | HT   | FT   | ATMOSPHERE | IDT  | ST   | HT   | FT   |
|------------|------|------|------|------|------------|------|------|------|------|
| OXIDIZING  | 2260 | 2320 | 2340 | 2500 | OXIDIZING  | 2650 | 2660 | 2670 | 2690 |
| REDUCING   | 2200 | 2300 | 2310 | 2380 | REDUCING   | 2640 | 2660 | 2670 | 2680 |

SAMPLE # 10 LAB NO. 634

SAMPLE # 13 LAB NO.650

| ATMOSPHERE | IDT  | ST   | HT   | FT   | ATMOSPHERE | IDT  | ST   | HT   | FT   |
|------------|------|------|------|------|------------|------|------|------|------|
| OXIDIZING  | 2400 | 2520 | 2600 | 2670 | OXIDIZING  | 2540 | 2710 | 2720 | 2780 |
| REDUCING   | 2380 | 2500 | 2540 | 2740 | REDUCING   | 2520 | 2640 | 2700 | 2780 |

SAMPLE # 11 LAB NO. 648

SAMPLE #

| ATMOSPHERE | IDT  | ST   | HT   | FT   | ATMOSPHERE | IDT | ST | HT | FT |
|------------|------|------|------|------|------------|-----|----|----|----|
| OXIDIZING  | 2380 | 2420 | 2520 | 2620 | OXIDIZING  |     |    |    |    |
| REDUCING   | 2280 | 2360 | 2440 | 2540 | REDUCING   |     |    |    |    |

Birtley Coal  
& Minerals Testing

A DIVISION OF GREAT WEST STEEL INDUSTRIES LTD.

CLIENT : BP CANADA LIMITED

PROJECT: SNTR-29 Samples

RAW COAL ANALYSIS, air dried basis

ASH FUSION TEMPERATURES (°F)

SAMPLE # 1

LAB NO. 651

SAMPLE # 5 LAB NO.

| ATMOSPHERE | IDT  | ST    | HT   | FT    | ATMOSPHERE | IDT  | ST    | HT    | FT |
|------------|------|-------|------|-------|------------|------|-------|-------|----|
| OXIDIZING  | 2620 | 2800+ |      | -     | OXIDIZING  | 2680 | 2800+ |       |    |
| REDUCING   | 2600 | 2760  | 2780 | 2800+ | REDUCING   | 2560 | 2720  | 2800+ |    |

SAMPLE # 2 LAB NO. 652

SAMPLE #6 LAB NO. 656

| ATMOSPHERE | IDT  | ST   | HT   | FT   | ATMOSPHERE | IDT  | ST   | HT   | FT   |
|------------|------|------|------|------|------------|------|------|------|------|
| OXIDIZING  | 2540 | 2560 | 2590 | 2620 | OXIDIZING  | 2500 | 2540 | 2580 | 2610 |
| REDUCING   | 2530 | 2540 | 2550 | 2620 | REDUCING   | 2480 | 2500 | 2520 | 2570 |

SAMPLE # 3 LAB NO.

SAMPLE # 7 LAB NO. 657

| ATMOSPHERE | IDT  | ST   | HT   | FT   | ATMOSPHERE | IDT  | ST   | HT   | FT   |
|------------|------|------|------|------|------------|------|------|------|------|
| OXIDIZING  | 2420 | 2460 | 2470 | 2520 | OXIDIZING  | 2200 | 2270 | 2380 | 2480 |
| REDUCING   | 2440 | 2460 | 2480 | 2520 | REDUCING   | 2100 | 2250 | 2290 | 2410 |

SAMPLE # 4 LAB NO. 654

SAMPLE #8 LAB NO. 658

| ATMOSPHERE | IDT   | ST | HT | FT | ATMOSPHERE | IDT  | ST   | HT   | FT    |
|------------|-------|----|----|----|------------|------|------|------|-------|
| OXIDIZING  | 2800+ |    |    |    | OXIDIZING  | 2600 | 2770 | 2790 | 2800+ |
| REDUCING   | 2800+ |    |    |    | REDUCING   | 2590 | 2740 | 2760 | 2800  |

Birtley Coal  
& Minerals Testing

A DIVISION OF GREAT WESTERN STEEL INDUSTRIES LTD

CLIENT : BP CANADA LIMITED

PROJECT: SNTR-29 Samples

RAW COAL ANALYSIS, air dried basis

ASH FUSION TEMPERATURES (°F)

SAMPLE # 9 LAB NO. 659

SAMPLE # 11 LAB NO. 661

| ATMOSPHERE | IDT  | ST   | HT   | FT   | ATMOSPHERE | IDT  | ST   | HT   | FT    |
|------------|------|------|------|------|------------|------|------|------|-------|
| OXIDIZING  | 2140 | 2160 | 2200 | 2260 | OXIDIZING  | 2540 | 2740 | 2760 | 2800+ |
| REDUCING   | 2100 | 2150 | 2200 | 2260 | REDUCING   | 2480 | 2680 | 2720 | 2800  |

SAMPLE # 10 LAB NO. 660

SAMPLE #

| ATMOSPHERE | IDT  | ST   | HT   | FT   | ATMOSPHERE | IDT | ST | HT | FT |
|------------|------|------|------|------|------------|-----|----|----|----|
| OXIDIZING  | 2330 | 2620 | 2720 | 2740 | OXIDIZING  |     |    |    |    |
| REDUCING   | 2310 | 2480 | 2520 | 2550 | REDUCING   |     |    |    |    |

Birtley Coal  
& Minerals Testing

A DIVISION OF GREAT WEST STEEL INDUSTRIES LTD

CLIENT : BP EXPLORATIONS CANADA

PROJECT: 81/6/1 Samples.

SAMPLES RECEIVED Oct. 16, 1981

RAW COAL ANALYSIS, a.d.b.

| Lab No | Sample No | ADM% | MOIST% | ASH% | VOL% | F.C.% | S%   | CV Cal/gm | SG   | F.S.I | HGI    |
|--------|-----------|------|--------|------|------|-------|------|-----------|------|-------|--------|
| 635    | 1         | 0.6  | 1.4    | 56.3 | -    | -     | 0.25 | -         | 1.82 | 1     | N.S.S. |
| 636    | 2         | 1.4  | 2.7    | 73.5 | -    | -     | 0.14 | -         | 2.14 | 0     | N.S.S. |
| 637    | 3         | 0.9  | 1.7    | 57.8 | -    | -     | 0.19 | -         | 1.87 | 1     | N.S.S. |
| 638    | 4         | 1.4  | 1.3    | 48.2 | -    | -     | 0.27 | -         | 1.73 | 1     | N.S.S. |
| 639    | 5         | 2.1  | 1.3    | 62.7 | -    | -     | 0.14 | -         | 1.94 | 0     | N.S.S. |
| 640    | 6         | 0.9  | 1.0    | 22.8 | 22.4 | 55.8  | 0.34 | 6403      | 1.46 | 2     | N.S.S. |
| 641    | 7         | 0.9  | 1.1    | 49.0 | -    | -     | 0.24 | -         | 1.74 | 1     | N.S.S. |
| 642    | 8         | 0.5  | 1.1    | 29.4 | 18.9 | 50.6  | 0.28 | 5754      | 1.50 | 1 1/2 | N.S.S. |
| 643    | 9         | 0.5  | 1.5    | 77.5 | -    | -     | 0.10 | -         | 2.13 | 0     | N.S.S. |
| 644    | 10        | 1.2  | 1.3    | 47.1 | -    | -     | 0.29 | -         | 1.67 | 3     | N.S.S. |
| 645    | 11        | 0.3  | 1.6    | 78.9 | -    | -     | 0.10 | -         | 2.21 | 0     | N.S.S. |
| 646    | 12        | 1.4  | 1.4    | 34.8 | 20.5 | 43.3  | 0.65 | 5242      | 1.53 | 5     | N.S.S. |
| 647    | 13        | 0.2  | 1.4    | 65.5 | -    | -     | 0.22 | -         | 1.91 | 1     | 56     |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |

N.S.S. - Not Sufficient Sample



CLIENT : BP EXPLORATIONS CANADA

PROJECT: 81/13/1 Samples

SAMPLES RECEIVED Oct. 16/81

RAW COAL ANALYSIS, a.d.b.

| Lab No | Sample No | ADM% | MOIST% | ASH% | VOL% | F.C.% | S%   | CV Cal/gm | S.G. | F.S.I. | HGI    |
|--------|-----------|------|--------|------|------|-------|------|-----------|------|--------|--------|
| 596    | R         | 0.6  | 1.1    | 72.2 | -    | -     | 0.17 | -         | 2.05 | 1      | N.S.S. |
| 597    | 1         | 1.0  | 0.7    | 30.0 | 23.3 | 46.0  | 0.40 | 5801      | 1.49 | 5 1/2  | 100    |
| 598    | 2         | 0.8  | 0.9    | 25.0 | 24.1 | 50.0  | 0.38 | 6302      | 1.46 | 7 1/2  | N.S.S. |
|        |           |      |        |      |      |       |      |           |      |        |        |
|        |           |      |        |      |      |       |      |           |      |        |        |
|        |           |      |        |      |      |       |      |           |      |        |        |
|        |           |      |        |      |      |       |      |           |      |        |        |
|        |           |      |        |      |      |       |      |           |      |        |        |
|        |           |      |        |      |      |       |      |           |      |        |        |
|        |           |      |        |      |      |       |      |           |      |        |        |
|        |           |      |        |      |      |       |      |           |      |        |        |
|        |           |      |        |      |      |       |      |           |      |        |        |
|        |           |      |        |      |      |       |      |           |      |        |        |
|        |           |      |        |      |      |       |      |           |      |        |        |
|        |           |      |        |      |      |       |      |           |      |        |        |
|        |           |      |        |      |      |       |      |           |      |        |        |
|        |           |      |        |      |      |       |      |           |      |        |        |
|        |           |      |        |      |      |       |      |           |      |        |        |
|        |           |      |        |      |      |       |      |           |      |        |        |
|        |           |      |        |      |      |       |      |           |      |        |        |
|        |           |      |        |      |      |       |      |           |      |        |        |
|        |           |      |        |      |      |       |      |           |      |        |        |

N.S.S. = Not sufficient sample

CLIENT : BP EXPLORATIONS CANADA

PROJECT: 81/13/2 Samples

SAMPLES RECEIVED Oct. 16, 1981

RAW COAL ANALYSIS, a.d.b.

| Lab No | Sample No | ADM% | MOIST% | ASH% | VOL% | F.C.% | S%   | CV Cal/gm | S.G. | FSI   | HGI    |
|--------|-----------|------|--------|------|------|-------|------|-----------|------|-------|--------|
| 599    | 1         | 0.3  | 0.8    | 5.0  | 22.6 | 71.6  | 0.35 | 8001      | 1.32 | 1 1/2 | 106    |
| 600    | 2         | 0.2  | 0.6    | 5.3  | 26.2 | 67.9  | 0.34 | 8053      | 1.28 | 4     | 113    |
| 601    | 3         | 1.4  | 0.5    | 11.8 | 32.7 | 55.0  | 0.33 | 7582      | 1.31 | 8     | N.S.S. |
| 602    | 4         | 0.5  | 0.9    | 76.1 | -    | -     | 0.12 | -         | 2.16 | 0     | 91     |
| 603    | 5         | 1.1  | 1.0    | 18.6 | 25.5 | 54.9  | 0.39 | 6826      | 1.38 | 8     | N.S.S. |
| 604    | 6         | 0.4  | 0.8    | 82.4 | -    | -     | 0.10 | -         | 2.29 | 0     | N.S.S. |
| 605    | 7         | 0.9  | 0.8    | 64.2 | -    | -     | 0.26 | -         | 1.88 | 1 1/2 | N.S.S. |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |
|        |           |      |        |      |      |       |      |           |      |       |        |

N.S.S. -Not Sufficient Sample

Birtley Coal  
& Minerals Testing  
A DIVISION OF GREAT WEST STEEL INDUSTRIES LTD.

CLIENT : BP EXPLORATIONS CANADA

PROJECT: 81/13/3 Samples

SAMPLES RECEIVED Oct. 16/81

RAW COAL ANALYSIS, a.d.b.

| Lab No. | Sample No. | ADM% | MOIST% | ASH% | VOL% | F.C.% | S%   | C.V. Cal/gm | S.G. | FSI   | HGI    |
|---------|------------|------|--------|------|------|-------|------|-------------|------|-------|--------|
| 574     | 1          | 0.7  | 0.9    | 55.2 | -    | -     | 0.22 | -           | 1.81 | 1     | N.S.S. |
| 575     | 2          | 0.6  | 0.8    | 11.7 | 21.6 | 65.9  | 0.38 | 7410        | 1.37 | 1     | N.S.S. |
| 576     | 3          | 0.6  | 0.9    | 10.0 | 23.0 | 66.1  | 0.38 | 7563        | 1.37 | 2     | N.S.S. |
| 577     | 4          | 0.8  | 0.8    | 22.9 | 21.3 | 55.0  | 0.36 | 6532        | 1.44 | 3 1/2 | N.S.S. |
| 578     | 5          | 0.8  | 1.1    | 59.2 | -    | -     | 0.21 | -           | 1.85 | 1 1/2 | N.S.S. |
| 579     | 6          | 1.1  | 0.8    | 32.8 | 22.6 | 43.8  | 0.37 | 5502        | 1.53 | 5     | N.S.S. |
| 580     | 7          | 1.9  | 1.1    | 69.7 | -    | -     | 0.13 | -           | 2.02 | 1     | N.S.S. |
|         |            |      |        |      |      |       |      |             |      |       |        |
|         |            |      |        |      |      |       |      |             |      |       |        |
|         |            |      |        |      |      |       |      |             |      |       |        |
|         |            |      |        |      |      |       |      |             |      |       |        |
|         |            |      |        |      |      |       |      |             |      |       |        |
|         |            |      |        |      |      |       |      |             |      |       |        |
|         |            |      |        |      |      |       |      |             |      |       |        |
|         |            |      |        |      |      |       |      |             |      |       |        |
|         |            |      |        |      |      |       |      |             |      |       |        |
|         |            |      |        |      |      |       |      |             |      |       |        |
|         |            |      |        |      |      |       |      |             |      |       |        |
|         |            |      |        |      |      |       |      |             |      |       |        |

N.S.S. - Not Sufficient Sample

Birtley Coal & Minerals Testing

A DIVISION OF GREAT WEST STEEL INDUSTRIES LTD.



CLIENT : BP EXPLORATIONS CANADA

PROJECT: 81/13/4 Samples

SAMPLES RECEIVED Oct. 16/81

RAW COAL ANALYSIS, a.d.b.

| Lab No | Sample No. | ADM% | MOIST% | ASH% | VOL% | F.C.% | S%   | C.V. Cal/gm | SG   | FSI   | HGI    |
|--------|------------|------|--------|------|------|-------|------|-------------|------|-------|--------|
| 581    | 1          | 0.7  | 0.9    | 7.5  | 24.9 | 66.7  | 0.44 | 7831        | 1.34 | 4     | 139    |
| 582    | 2          | 1.3  | 0.6    | 40.6 | -    | -     | 0.17 | -           | 2.09 | 0     | N.S.S. |
| 583    | 3          | 0.9  | 0.8    | 4.8  | 27.0 | 67.0  | 0.37 | 8035        | 1.32 | 4     | N.S.S. |
| 584    | 4          | 0.6  | 0.3    | 45.9 | -    | -     | 0.10 | -           | 2.28 | 0     | N.S.S. |
| 585    | 5          | 0.7  | 0.6    | 7.4  | 23.9 | 68.1  | 0.30 | 7782        | 1.71 | 1 1/2 | 111    |
| 586    | 6          | 0.8  | 0.6    | 2.7  | 24.8 | 71.9  | 0.31 | 8259        | 1.32 | 3     | 117    |
|        |            |      |        |      |      |       |      |             |      |       |        |
|        |            |      |        |      |      |       |      |             |      |       |        |
|        |            |      |        |      |      |       |      |             |      |       |        |
|        |            |      |        |      |      |       |      |             |      |       |        |
|        |            |      |        |      |      |       |      |             |      |       |        |
|        |            |      |        |      |      |       |      |             |      |       |        |
|        |            |      |        |      |      |       |      |             |      |       |        |
|        |            |      |        |      |      |       |      |             |      |       |        |
|        |            |      |        |      |      |       |      |             |      |       |        |
|        |            |      |        |      |      |       |      |             |      |       |        |
|        |            |      |        |      |      |       |      |             |      |       |        |
|        |            |      |        |      |      |       |      |             |      |       |        |
|        |            |      |        |      |      |       |      |             |      |       |        |
|        |            |      |        |      |      |       |      |             |      |       |        |
|        |            |      |        |      |      |       |      |             |      |       |        |
|        |            |      |        |      |      |       |      |             |      |       |        |

N.S.S. -Not Sufficient Sample

Birtley Coal & Minerals Testing

A DIVISION OF GREAT WEST STEEL INDUSTRIES LTD.

CLIENT : BP EXPLORATIONS CANADA

PROJECT: 81/13/5 Samples

SAMPLES RECEIVED Oct. 16, 1981

RAW COAL ANALYSIS, a.d.b.

| Lab No | Sample No | ADM% | MOIST% | ASH% | VOL% | F.C.% | S%   | C.V. Cal/gm | S.G. | FSI   | HGI    |
|--------|-----------|------|--------|------|------|-------|------|-------------|------|-------|--------|
| 587    | 1         | 0.7  | 0.6    | 6.5  | 21.5 | 71.4  | 0.26 | 7874        | 1.34 | 1     | 99     |
| 588    | 2         | 0.6  | 0.7    | 6.3  | 20.7 | 72.3  | 0.21 | 7864        | 1.35 | 1     | 103    |
| 589    | 3         | 0.5  | 0.6    | 18.7 | 21.6 | 59.1  | 0.23 | 6700        | 1.45 | 1 1/2 | 59     |
| 590    | 4         | 0.3  | 0.4    | 51.7 | -    | -     | 0.14 | -           | 1.84 | 1     | N.S.S. |
| 591    | 5         | 0.3  | 0.6    | 15.1 | 23.6 | 60.7  | 0.34 | 7048        | 1.40 | 4 1/2 | N.S.S. |
| 592    | 6         | 0.6  | 0.4    | 78.9 | -    | -     | 0.35 | -           | 2.36 | 0     | N.S.S. |
| 593    | 7         | 0.4  | 0.4    | 41.6 | -    | -     | 0.24 | -           | 1.69 | 1     | N.S.S. |
| 594    | 8         | 0.6  | 0.8    | 7.7  | 29.4 | 62.1  | 0.49 | 7832        | 1.31 | 9     | N.S.S. |
| 595    | 9         | 0.3  | 0.9    | 32.2 | 21.3 | 45.6  | 0.40 | 5521        | 1.52 | 5 1/2 | N.S.S. |
|        |           |      |        |      |      |       |      |             |      |       |        |
|        |           |      |        |      |      |       |      |             |      |       |        |
|        |           |      |        |      |      |       |      |             |      |       |        |
|        |           |      |        |      |      |       |      |             |      |       |        |
|        |           |      |        |      |      |       |      |             |      |       |        |

N.S.S. -Not Sufficient Sample

**Birtley Coal  
& Minerals Testing**

A DIVISION OF GREAT WEST STEEL INDUSTRIES LTD.



CLIENT : BP EXPLORATIONS CANADA

PROJECT: SNTR 18 Samples

SAMPLES RECEIVED Oct. 26, 1981

RAW COAL ANALYSIS, a.d.b.

| Lab No | Sample No | ADM% | MOIST% | ASH% | VOL% | F.C.% | S%   | CV Cal/gm | SG   | FSI | HGI |
|--------|-----------|------|--------|------|------|-------|------|-----------|------|-----|-----|
| 712    | 8         | 0.5  | 3.4    | 47.6 | -    | -     | 0.25 | -         | 1.78 | 0   | 47  |
| 713    | 9         | 0.3  | 1.7    | 34.3 | 19.4 | 44.6  | 0.32 | 5118      | 1.58 | 1/2 | 64  |
| 714    | 10        | 0.7  | 1.6    | 75.4 | -    | -     | 0.09 | -         | 2.11 | 0   | 47  |
| 715    | 11        | 0.2  | 1.4    | 37.1 | 19.7 | 41.8  | 0.27 | 4986      | 1.57 | 1   | 59  |
| 716    | 12        | nil  | 1.5    | 80.4 | -    | -     | 0.06 | -         | 2.22 | 0   | 59  |
|        |           |      |        |      |      |       |      |           |      |     |     |
|        |           |      |        |      |      |       |      |           |      |     |     |
|        |           |      |        |      |      |       |      |           |      |     |     |
|        |           |      |        |      |      |       |      |           |      |     |     |
|        |           |      |        |      |      |       |      |           |      |     |     |
|        |           |      |        |      |      |       |      |           |      |     |     |
|        |           |      |        |      |      |       |      |           |      |     |     |
|        |           |      |        |      |      |       |      |           |      |     |     |
|        |           |      |        |      |      |       |      |           |      |     |     |
|        |           |      |        |      |      |       |      |           |      |     |     |
|        |           |      |        |      |      |       |      |           |      |     |     |
|        |           |      |        |      |      |       |      |           |      |     |     |
|        |           |      |        |      |      |       |      |           |      |     |     |
|        |           |      |        |      |      |       |      |           |      |     |     |
|        |           |      |        |      |      |       |      |           |      |     |     |
|        |           |      |        |      |      |       |      |           |      |     |     |

CLIENT : BP EXPLORATIONS CANADA

PROJECT: SNTR -25 Samples

SAMPLES RECEIVED Oct. 16, 1981

RAW COAL ANALYSIS, a.d.b.

| Lab No. | Sample No. | ADM% | MOIST% | ASH% | VOL% | F.C.% | S%   | CV Cal/gr | SG   | FSI   | HGI    |
|---------|------------|------|--------|------|------|-------|------|-----------|------|-------|--------|
| 610     | 1          | 0.2  | 1.2    | 41.9 | -    | -     | 0.52 | -         | 1.67 | 1     | 82     |
| 611     | 2          | 1.2  | 1.3    | 67.1 | -    | -     | 0.23 | -         | 1.99 | 0     | 47     |
| 612     | 3          | 0.1  | 0.6    | 67.0 | -    | -     | 0.24 | -         | 2.00 | 1     | N.S.S. |
| 613     | 4          | 1.6  | 1.6    | 70.5 | -    | -     | 0.16 | -         | 2.10 | 0     | 48     |
| 614     | 5          | 1.1  | 1.4    | 36.6 | 19.6 | 42.4  | 0.39 | 4938      | 1.60 | 1     | 59     |
| 615     | 6          | 2.5  | 1.5    | 73.8 | -    | -     | 0.12 | -         | 2.14 | 0     | 79     |
| 616     | 7          | 0.3  | 1.0    | 37.5 | 20.3 | 41.2  | 0.33 | 4983      | 1.60 | 2 1/2 | 110    |
| 617     | 8          | 0.8  | 1.6    | 73.6 | -    | -     | 0.08 | -         | 2.19 | 0     | 83     |
| 618     | 9          | 0.4  | 1.1    | 18.5 | 19.7 | 60.7  | 0.33 | 6682      | 1.43 | 1 1/2 | 54     |
| 619     | 10         | 2.6  | 1.0    | 32.3 | 37.2 | 29.5  | 0.29 | 4824      | -    | -     | N.S.S. |
| 620     | 10A        | 0.4  | 0.4    | 61.8 | -    | -     | 0.10 | -         | 2.93 | 0     | 47     |
| 621     | 11         | 0.4  | 1.0    | 20.0 | 21.9 | 57.1  | 0.33 | 6571      | 1.44 | 1     | 59     |
|         |            |      |        |      |      |       |      |           |      |       |        |
|         |            |      |        |      |      |       |      |           |      |       |        |
|         |            |      |        |      |      |       |      |           |      |       |        |
|         |            |      |        |      |      |       |      |           |      |       |        |
|         |            |      |        |      |      |       |      |           |      |       |        |
|         |            |      |        |      |      |       |      |           |      |       |        |
|         |            |      |        |      |      |       |      |           |      |       |        |
|         |            |      |        |      |      |       |      |           |      |       |        |
|         |            |      |        |      |      |       |      |           |      |       |        |
|         |            |      |        |      |      |       |      |           |      |       |        |
|         |            |      |        |      |      |       |      |           |      |       |        |
|         |            |      |        |      |      |       |      |           |      |       |        |
|         |            |      |        |      |      |       |      |           |      |       |        |
|         |            |      |        |      |      |       |      |           |      |       |        |

N.S.S. -Not Sufficient Sample

Birtley Coal & Minerals Testing

A DIVISION OF GREAT WEST STEEL INDUSTRIES LTD.

CLIENT : BP EXPLORATIONS CANADA

PROJECT: SNTR-28 Samples

SAMPLES RECEIVED Oct. 16, 1981

RAW COAL ANALYSIS, a.d.b.

| Lab No | Sample No | ADM% | MOIST% | ASH% | VOL% | F.C.% | S%   | CV Cal/gm | SG   | FSI | HGI    |
|--------|-----------|------|--------|------|------|-------|------|-----------|------|-----|--------|
| 625    | 1         | 8.9  | 4.1    | 39.3 | 19.4 | 37.2  | 0.24 | 3885      | 1.67 | 0   | 133    |
| 626    | 2         | 8.1  | 4.3    | 60.9 | -    | -     | 0.15 | -         | 2.00 | 0   | 83     |
| 627    | 3         | 6.9  | 10.1   | 33.8 | 19.0 | 37.1  | 0.23 | 3827      | 1.62 | 0   | 133    |
| 628    | 4         | 5.6  | 4.3    | 71.2 | -    | -     | 0.07 | -         | 2.15 | 0   | N.S.S. |
| 629    | 5         | 9.3  | 6.2    | 38.6 | 20.0 | 35.2  | 0.25 | 3553      | 1.70 | 0   | N.S.S. |
| 630    | 6         | 8.8  | 3.2    | 72.1 | -    | -     | 0.07 | -         | 2.20 | 0   | N.S.S. |
| 631    | 7         | 10.1 | 6.2    | 56.8 | -    | -     | 0.14 | -         | 1.94 | 0   | 81     |
| 632    | 8         | 12.0 | 4.0    | 72.0 | -    | -     | 0.08 | -         | 2.15 | 0   | 76     |
| 633    | 9         | 16.2 | 7.5    | 23.4 | 25.1 | 44.0  | 0.28 | 4531      | 1.61 | 0   | N.S.S. |
| 634    | 10        | 10.1 | 6.3    | 49.3 | -    | -     | 0.18 | -         | 1.82 | 0   | 98     |
| 648    | 11        | 10.1 | 7.1    | 14.3 | 24.4 | 54.2  | 0.40 | 5828      | 1.44 | 0   | 90     |
| 649    | 12        | 23.9 | 11.7   | 12.4 | 27.9 | 48.0  | 0.32 | 4835      | 1.56 | 0   | N.S.S. |
| 650    | 13        | 6.9  | 2.1    | 88.9 | -    | -     | 0.05 | -         | 2.44 | 0   | N.S.S. |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |

N.S.S. -Not Sufficient Sample

**Birtley Coal  
& Minerals Testing**

A DIVISION OF GREAT WEST STEEL INDUSTRIES LTD

CLIENT : BP EXPLORATIONS CANADA

PROJECT: SNTR-29 Samples

SAMPLES RECEIVED Oct. 16, 1981

RAW COAL ANALYSIS, a.d.b.

| Lab No | Sample No | ADM% | MOIST% | ASH% | VOL% | F.C.% | S%   | CV Cal/gm | SG   | FSI | HGI    |
|--------|-----------|------|--------|------|------|-------|------|-----------|------|-----|--------|
| 651    | 1         | 7.7  | 3.5    | 74.7 | -    | -     | 0.09 | -         | 2.19 | 0   | 66     |
| 652    | 2         | 18.2 | 6.1    | 22.4 | 24.9 | 46.6  | 0.22 | 4666      | 1.64 | 0   | N.S.S. |
| 653    | 3         | 6.8  | 4.2    | 6.4  | 27.7 | 61.7  | 0.31 | 6599      | 1.41 | 0   | 98     |
| 654    | 4         | 1.4  | 1.9    | 72.3 | -    | -     | 0.07 | -         | 2.15 | 0   | 95     |
| 655    | 5         | 27.6 | 6.8    | 25.7 | 25.9 | 41.6  | 0.15 | 4100      | 1.69 | 0   | 100    |
| 656    | 6         | 24.7 | 9.9    | 21.0 | 25.8 | 43.3  | 0.18 | 4447      | 1.61 | 0   | 83     |
| 657    | 7         | 17.7 | 7.6    | 15.5 | 25.8 | 51.1  | 0.18 | 5222      | 1.54 | 0   | 75     |
| 658    | 8         | 6.6  | 1.6    | 89.5 | -    | -     | 0.01 | -         | 2.48 | 0   | N.S.S. |
| 659    | 9         | 9.1  | 10.1   | 8.3  | 26.3 | 55.3  | 0.25 | 5743      | 1.46 | 0   | 79     |
| 660    | 10        | 11.4 | 4.4    | 50.5 | -    | -     | 0.15 | -         | 1.87 | 0   | 72     |
| 661    | 11        | 2.5  | 2.3    | 78.7 | -    | -     | 0.11 | -         | 2.28 | 0   | N.S.S. |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |
|        |           |      |        |      |      |       |      |           |      |     |        |

N.S.S. - Not Sufficient Sample

Birtley Coal & Minerals Testing  
A DIVISION OF GREAT WEST STEEL INDUSTRIES LTD.

CLIENT : BR. EXPLORATION CANADA LIMITED

PROJECT : SNTR SAMPLES Received Sept. 2/80

| LAB NO. | SAMPLE I.D. | ADM% | MOIST | PROXIMATE |      |       | S%   | FSI  | BTU/LB |      | HGI | S.G. | CALC BASIS |        |
|---------|-------------|------|-------|-----------|------|-------|------|------|--------|------|-----|------|------------|--------|
|         |             |      |       | ASH %     | VOL% | F.C.% |      |      |        |      |     |      |            |        |
| 5853    | 12-1        | 14.3 | 4.7   | 59.3      | -    | -     | -    | -    | -      | -    | NSS | -    | a.d.b.     |        |
|         | SNTR 12/1   |      | 18.3  | 50.8      | -    | -     | -    | -    | -      | -    | -   | -    | a.r.b.     |        |
|         |             |      |       |           | 62.2 | -     | -    | -    | -      | -    | -   | -    | -          | d.b.   |
| 5854    | 12-2        | 12.0 | 7.2   | 25.5      | 23.3 | 44.0  | 0.32 | N.A. | 8329   |      | 75  | 1.60 | a.d.b.     |        |
|         | SNTR 12/2   |      | 18.3  | 22.4      | 20.5 | 38.8  | 0.28 | -    | 7330   |      | -   | -    | -          | a.r.b. |
|         |             |      |       | 27.5      | 25.1 | 47.4  | 0.34 | -    | 8975   |      | -   | -    | -          | d.b.   |
| 5855    | 12-3        | 8.6  | 1.7   | 80.4      | -    | -     | -    | -    | -      |      | NSS | -    | a.d.b.     |        |
|         | SNTR 12/3   |      | 10.2  | 73.5      | -    | -     | -    | -    | -      |      | -   | -    | -          | a.r.b. |
|         |             |      |       |           | 81.8 | -     | -    | -    | -      | -    |     | -    | -          | -      |
| 5856    | 12-4        | 12.1 | 3.5   | 45.2      | 18.4 | 32.9  | 0.34 | N.A. | 6353   |      | 74  | 1.75 | a.d.b.     |        |
|         | SNTR 12/4   |      | 15.2  | 39.7      | 16.2 | 28.9  | 0.30 | -    | 5584   |      | -   | -    | -          | a.r.b. |
|         |             |      |       |           | 46.8 | 19.1  | 34.1 | 0.35 | -      | 6583 |     | -    | -          | -      |

NSS - Not Sufficient Sample

air dried basis - a.d.b.  
as received basis - a.r.b.  
dry basis - d.b.

Birtley Coal  
& Minerals Testing

A DIVISION OF CANADIAN WESTERN INDUSTRIES LTD



CLIENT : BP EXPLORATION CANADA LIMITED

PROJECT : SNTR SAMPLES Received Sept. 2/80

| LAB NO. | SAMPLE I.D. | ADM% MOIST | PROXIMATE |      |       | S%   | FSI  | BTU/LB | HGI  | S.G. | CALC BASIS |        |
|---------|-------------|------------|-----------|------|-------|------|------|--------|------|------|------------|--------|
|         |             |            | ASH %     | VOL% | F.C.% |      |      |        |      |      |            |        |
| 5837    | 12-5        | 7.5        | 1.9       | 82.0 | -     | -    | -    | -      | NSS  | -    | a.d.b.     |        |
|         | SNTR 12/5   |            | 9.3       | 75.9 | -     | -    | -    | -      | -    | -    | a.r.b.     |        |
|         |             |            |           |      | 83.6  | -    | -    | -      | -    | -    | -          | d.b.   |
| 5838    | 12-6        | 8.2        | 3.6       | 28.6 | 22.7  | 45.1 | 0.42 | N.A.   | 9308 | 65   | 1.56       | a.d.b. |
|         | SNTR 12/6   |            | 11.5      | 26.3 | 20.8  | 41.4 | 0.39 | -      | 8545 | -    | -          | a.r.b. |
|         |             |            |           |      | 29.7  | 23.5 | 46.8 | 0.44   | -    | 9656 | -          | -      |
| 5839    | 12-7        | 7.8        | 3.5       | 53.2 | -     | -    | -    | -      | -    | NSS  | -          | a.d.b. |
|         | SNTR 12/7   |            | 11.0      | 49.1 | -     | -    | -    | -      | -    | -    | -          | a.r.b. |
|         |             |            |           |      | 55.1  | -    | -    | -      | -    | -    | -          | -      |
| 5841    | 18-1        | 6.7        | 1.8       | 39.0 | 18.4  | 40.8 | 0.34 | N.A.   | 8360 | 65   | 1.66       | a.d.b. |
|         | SNTR 18/1   |            | 8.4       | 36.4 | 17.2  | 38.0 | 0.32 | -      | 7800 | -    | -          | a.r.b. |
|         |             |            |           |      | 39.7  | 18.7 | 41.6 | 0.35   | -    | 8513 | -          | -      |
| 5842    | 18-2        | 4.0        | 2.0       | 74.1 | -     | -    | -    | -      | -    | NSS  | -          | a.d.b. |
|         | SNTR 18/2   |            | 5.9       | 71.1 | -     | -    | -    | -      | -    | -    | -          | a.r.b. |
|         |             |            |           |      | 75.6  | -    | -    | -      | -    | -    | -          | -      |
| 5843    | 18-3        | 10.4       | 2.1       | 39.6 | 17.9  | 40.4 | 0.31 | 1/2    | 8350 | 99   | 1.65       | a.d.b. |
|         | SNTR 18/3   |            | 12.3      | 35.5 | 16.0  | 36.2 | 0.28 | -      | 7482 | -    | -          | a.r.b. |
|         |             |            |           |      | 40.4  | 18.3 | 41.3 | 0.32   | -    | 8529 | -          | -      |

NSS - Not Sufficient Sample

air dried basis - a.d.b.  
 as received basis - a.r.b.  
 dry basis - d.b.

Birtley Coal  
 & Minerals Testing

CLIENT : BP EXPLORATION CANADA LIMITED

PROJECT : SNTR SAMPLES Received Sept. 2/80

| LAB NO. | SAMPLE I.D. | ADM% MOIST% | PROXIMATE |      |       | S%   | FSI  | BTU/LB | HGI   | S.G.  | CALC * BASIS |        |        |
|---------|-------------|-------------|-----------|------|-------|------|------|--------|-------|-------|--------------|--------|--------|
|         |             |             | ASH %     | VOL% | F.C.% |      |      |        |       |       |              |        |        |
| 5844    | 18-4        | 8.3         | 1.7       | 73.2 | -     | -    | -    | -      | NSS   | -     | a.d.b.       |        |        |
|         | SNTR 18/4   |             | 9.9       | 67.1 | -     | -    | -    | -      | -     | -     | a.r.b.       |        |        |
|         |             |             |           |      | 74.5  | -    | -    | -      | -     | -     | -            | d.b.   |        |
| 5845    | 18-5        | 8.4         | 2.0       | 40.4 | 18.1  | 39.5 | 0.33 | 1/2    | 8174  | NSS   | 1.66         | a.d.b. |        |
|         | SNTR 18/5   |             |           | 10.2 | 37.0  | 16.6 | 36.2 | 0.30   | -     | 7487  | -            | -      | a.r.b. |
|         |             |             |           |      | 41.2  | 18.5 | 40.3 | 0.34   | -     | 8341  | -            | -      | d.b.   |
| 5846    | 18-6        | 8.3         | 2.0       | 81.5 | -     | -    | -    | -      | -     | NSS   | -            | a.d.b. |        |
|         | SNTR 18/6   |             |           | 10.1 | 74.7  | -    | -    | -      | -     | -     | -            | -      | a.r.b. |
|         |             |             |           |      |       | 83.2 | -    | -      | -     | -     | -            | -      | d.b.   |
| 5847    | 18-7        | 8.1         | 1.8       | 45.9 | 16.8  | 35.5 | 0.33 | N.A.   | 7329  | 61    | 1.73         | a.d.b. |        |
|         | SNTR 18/7   |             |           | 9.8  | 42.2  | 15.4 | 32.6 | 0.30   | -     | 6735  | -            | -      | a.r.b. |
|         |             |             |           |      | 46.7  | 17.1 | 36.2 | 0.34   | -     | 7463  | -            | -      | d.b.   |
| 5848    | 19-1        | 1.2         | 1.1       | 62.1 | -     | -    | -    | -      | -     | NSS   | -            | a.d.b. |        |
|         | SNTR 19/1   |             |           | 2.3  | 61.4  | -    | -    | -      | -     | -     | -            | -      | a.r.b. |
|         |             |             |           |      |       | 62.8 | -    | -      | -     | -     | -            | -      | d.b.   |
| 5849    | 19-2        | 8.5         | 3.8       | 20.0 | 25.2  | 51.0 | 0.49 | N.A.   | 10403 | 74    | 1.51         | a.d.b. |        |
|         | SNTR 19/2   |             |           | 12.0 | 18.3  | 23.1 | 46.6 | 0.45   | -     | 9519  | -            | -      | a.r.b. |
|         |             |             |           |      | 20.8  | 26.2 | 53.0 | 0.51   | -     | 10814 | -            | -      | d.b.   |
| 5850    | 19-3        | 10.8        | 2.5       | 65.0 | -     | -    | -    | -      | -     | NSS   | -            | a.d.b. |        |
|         | SNTR 19/3   |             |           | 13.0 | 58.0  | -    | -    | -      | -     | -     | -            | -      | a.r.b. |
|         |             |             |           |      | 66.7  | -    | -    | -      | -     | -     | -            | -      | d.b.   |

NSS - Not Sufficient Sample

\* air dried basis - a.d.b.  
 s received basis - a.r.b.  
 dry basis - d.b.

Birtley Coal & Minerals Testing

A DIVISION OF GREAT WESTERN INDUSTRIES LTD

CLIENT : BP EXPLORATION CANADA LIMITED

PROJECT : SNTR. SAMPLES Received Sept. 2/80

| LAB NO. | SAMPLE I.D. | ADM% | MOIST | PROXIMATE |      |       | S%   | FSI  | BTU/LB | HGI | S.G. | CALC * BASIS |
|---------|-------------|------|-------|-----------|------|-------|------|------|--------|-----|------|--------------|
|         |             |      |       | ASH %     | VOL% | F.C.% |      |      |        |     |      |              |
| 5851    | 19-4        | 9.8  | 2.9   | 7.8       | 29.9 | 59.4  | 0.36 | N.A. | 11894  | 90  | 1.41 | a.d.b.       |
|         | SNTR 19/4   |      | 12.4  | 7.0       | 27.0 | 53.6  | 0.32 | -    | 10728  | -   | -    | a.r.b.       |
|         |             |      |       | 8.0       | 30.8 | 61.2  | 0.37 | -    | 12249  | -   | -    | d.b.         |
| 5852    | 19-5        | 9.9  | 2.8   | 60.6      | -    | -     | -    | -    | -      | NSS | -    | a.d.b.       |
|         | SNTR 19/5   |      | 12.4  | 54.6      | -    | -     | -    | -    | -      | -   | -    | a.r.b.       |
|         |             |      |       | 62.3      | -    | -     | -    | -    | -      | -   | -    | -            |
| 5853    | 19-6        | 9.5  | 3.5   | 18.5      | 25.6 | 52.4  | 0.42 | N.A. | 10163  | 74  | 1.50 | a.d.b.       |
|         | SNTR 19/6   |      | 12.7  | 16.7      | 23.2 | 47.4  | 0.38 | -    | 9198   | -   | -    | a.r.b.       |
|         |             |      |       | 19.2      | 26.5 | 54.5  | 0.44 | -    | 10532  | -   | -    | d.b.         |
| 5854    | 19-7        | 12.2 | 6.7   | 7.3       | 29.1 | 56.9  | 0.36 | N.A. | 10862  | 98  | 1.46 | a.d.b.       |
|         | SNTR 19/7   |      | 18.1  | 6.4       | 25.5 | 50.0  | 0.32 | -    | 9537   | -   | -    | a.r.b.       |
|         |             |      |       | 7.8       | 31.2 | 61.0  | 0.39 | -    | 11642  | -   | -    | d.b.         |
| 5855    | 19-8        | 16.6 | 6.0   | 38.6      | 21.7 | 33.7  | 0.20 | N.A. | 6071   | 94  | 1.82 | a.d.b.       |
|         | SNTR 19/8   |      | 21.6  | 32.2      | 18.1 | 28.1  | 0.17 | -    | 5063   | -   | -    | a.r.b.       |
|         |             |      |       | 41.1      | 23.1 | 35.8  | 0.21 | -    | 6459   | -   | -    | d.b.         |
| 5856    | 19-9        | 10.9 | 7.4   | 14.8      | 26.2 | 51.6  | 0.38 | N.A. | 9700   | 97  | 1.52 | a.d.b.       |
|         | SNTR 19/9   |      | 17.5  | 13.2      | 23.3 | 46.0  | 0.34 | -    | 8643   | -   | -    | a.r.b.       |
|         |             |      |       | 16.0      | 28.3 | 55.7  | 0.41 | -    | 10475  | -   | -    | d.b.         |
| 5857    | 19-10       | 10.8 | 2.9   | 67.2      | -    | -     | -    | -    | -      | 78  | -    | a.d.b.       |
|         | SNTR 19/10  |      | 13.4  | 59.9      | -    | -     | -    | -    | -      | -   | -    | a.r.b.       |
|         |             |      |       | 69.2      | -    | -     | -    | -    | -      | -   | -    | -            |

NSS - Not Sufficient Sample

air dried basis - a.d.b.  
 as received basis - a.r.b.  
 dry basis - d.b.

Birtley Coal  
 & Minerals Testing

ADVISOR OF GREAT WESTERN INDUSTRIES LTD

CLIENT : BP EXPLORATION CANADA LIMITED

PROJECT : SNTR SAMPLES Received Sept. 2/80

| LAB NO. | SAMPLE I.D. | ADM% | MOIST | PROXIMATE |      |       | S%   | FSI  | BTU/LB | HGI | S.G. | CALC * BASIS |
|---------|-------------|------|-------|-----------|------|-------|------|------|--------|-----|------|--------------|
|         |             |      |       | ASH %     | VOL% | F.C.% |      |      |        |     |      |              |
| 5858    | 20-1        | 12.0 | 2.2   | 74.5      | -    | -     | -    | -    | -      | NSS | -    | a.d.b.       |
|         | SNTR 20/1   |      | 13.9  | 65.6      | -    | -     | -    | -    | -      | -   | -    | a.r.b.       |
|         |             |      |       | 76.2      | -    | -     | -    | -    | -      | -   | -    | -            |
| 5859    | 20-2        | 12.8 | 6.8   | 14.7      | 27.6 | 50.9  | 0.27 | N.A. | 9316   | 122 | 1.56 | a.d.b.       |
|         | SNTR 20/2   |      | 18.7  | 12.8      | 24.1 | 44.4  | 0.24 | -    | 8124   | -   | -    | a.r.b.       |
|         |             |      |       | 15.8      | 29.6 | 54.6  | 0.29 | -    | 9996   | -   | -    | -            |
| 5860    | 20-3        | 28.0 | 4.8   | 14.2      | 28.8 | 52.2  | 0.25 | N.A. | 10544  | NSS | 1.63 | a.d.b.       |
|         | SNTR 20/3   |      | 31.5  | 10.2      | 20.7 | 37.6  | 0.18 | -    | 7592   | -   | -    | a.r.b.       |
|         |             |      |       | 14.9      | 30.3 | 54.8  | 0.26 | -    | 11076  | -   | -    | -            |
| 5861    | 20-4        | 17.5 | 5.1   | 6.0       | 28.7 | 60.2  | 0.40 | N.A. | 11161  | 109 | 1.50 | a.d.b.       |
|         | SNTR 20/4   |      | 21.7  | 5.0       | 23.7 | 49.6  | 0.33 | -    | 9208   | -   | -    | a.r.b.       |
|         |             |      |       | 6.3       | 30.2 | 63.5  | 0.42 | -    | 11761  | -   | -    | -            |
| 5862    | 20-5        | 8.3  | 2.3   | 6.6       | 30.1 | 61.0  | 0.31 | N.A. | 12531  | 74  | 1.41 | a.d.b.       |
|         | SNTR 20/5   |      | 10.4  | 6.1       | 27.6 | 55.9  | 0.28 | -    | 11491  | -   | -    | a.r.b.       |
|         |             |      |       | 6.8       | 30.8 | 62.4  | 0.32 | -    | 12826  | -   | -    | -            |
| 5863    | 20-6        | 2.2  | 1.9   | 32.3      | 23.9 | 41.9  | 0.27 | N.A. | 9050   | 49  | 1.61 | a.d.b.       |
|         | SNTR 20/6   |      | 4.1   | 31.6      | 23.7 | 40.6  | 0.26 | -    | 8851   | -   | -    | a.r.b.       |
|         |             |      |       | 32.9      | 24.4 | 42.7  | 0.28 | -    | 9225   | -   | -    | -            |
| 5864    | 20-7        | 13.0 | 5.5   | 25.8      | 23.5 | 45.2  | 0.21 | N.A. | 8257   | 110 | 1.65 | a.d.b.       |
|         | SNTR 20/7   |      | 17.8  | 22.5      | 20.4 | 39.3  | 0.18 | -    | 7184   | -   | -    | a.r.b.       |
|         |             |      |       | 27.3      | 24.9 | 47.8  | 0.22 | -    | 8738   | -   | -    | -            |

NSS - Not Sufficient Sample

\* air dried basis - a.d.b.  
 as received basis - a.r.b.  
 dry basis - d.b.

**Birtley Coal  
& Minerals Testing**

A DIVISION OF GREAT WEST STEEL INDUSTRIES LTD

CLIENT : BP EXPLORATION CANADA LIMITED

PROJECT : SNTR SAMPLES Received Sept. 2/80

| AB NO. | SAMPLE I.D. | ADM% | MOIST | PROXIMATE |      |       | S%   | FSI  | BTU/LB | HGI | S.G. | CALC # BASIS |
|--------|-------------|------|-------|-----------|------|-------|------|------|--------|-----|------|--------------|
|        |             |      |       | ASH %     | VOL% | F.C.% |      |      |        |     |      |              |
| 5865   | 20-8        | 16.1 | 5.4   | 21.5      | 24.1 | 49.0  | 0.22 | N.A. | 8665   | 99  | 1.64 | a.d.b.       |
|        | SNTR 20/8   |      | 20.6  | 18.0      | 20.2 | 41.2  | 0.18 | -    | 7270   | -   | -    | a.r.b.       |
|        |             |      |       | 22.7      | 25.5 | 51.8  | 0.23 | -    | 9160   | -   | -    | d.b.         |
| 5866   | 20-9        | 16.7 | 7.0   | 5.0       | 28.1 | 59.9  | 0.29 | N.A. | 11014  | NSS | 1.45 | a.d.b.       |
|        | SNTR 20/9   |      | 22.5  | 4.2       | 23.4 | 49.9  | 0.24 | -    | 9174   | -   | -    | a.r.b.       |
|        |             |      |       | 5.4       | 30.2 | 64.4  | 0.31 | -    | 11843  | -   | -    | d.b.         |
| 5867   | 20-10       | 14.6 | 3.1   | 6.0       | 29.6 | 61.3  | 0.23 | N.A. | 11078  | NSS | 1.48 | a.d.b.       |
|        | SNTR 20/10  |      | 17.2  | 5.1       | 25.3 | 52.4  | 0.20 | -    | 9461   | -   | -    | a.r.b.       |
|        |             |      |       | 6.2       | 30.5 | 63.3  | 0.24 | -    | 11432  | -   | -    | d.b.         |
| 5868   | 20-11       | 7.1  | 1.8   | 78.3      | -    | -     | -    | -    | -      | NSS | -    | a.d.b.       |
|        | SNTR 20/11  |      | 8.8   | 72.7      | -    | -     | -    | -    | -      | -   | -    | a.r.b.       |
|        |             |      |       | 79.7      | -    | -     | -    | -    | -      | -   | -    | -            |
| 5869   | 20-12       | 18.0 | 3.7   | 12.3      | 27.1 | 56.9  | 0.31 | N.A. | 10744  | NSS | 1.48 | a.d.b.       |
|        | SNTR 20/12  |      | 21.0  | 10.1      | 22.2 | 46.7  | 0.25 | -    | 8810   | -   | -    | a.r.b.       |
|        |             |      |       | 12.8      | 28.1 | 59.1  | 0.32 | -    | 11157  | -   | -    | d.b.         |
| 5870   | 20-13       | 9.4  | 2.1   | 72.7      | -    | -     | -    | -    | -      | NSS | -    | a.d.b.       |
|        | SNTR 20/13  |      | 11.3  | 65.9      | -    | -     | -    | -    | -      | -   | -    | a.r.b.       |
|        |             |      |       | 74.3      | -    | -     | -    | -    | -      | -   | -    | -            |
|        |             |      |       |           |      |       |      |      |        |     |      |              |

NSS - Not Sufficient Sample

air dried basis - a.d.b.  
as received basis - a.r.b.  
dry basis - d.b.

Birtley Coal  
& Minerals Testing

A DIVISION OF GREAT WESTERN INDUSTRIES LTD

CLIENT : BP EXPLORATION CANADA

PROJECT : SNTR 18 SAMPLES RECEIVED OCT.30,1980

Service W.O.# 63205

| LAB NO. | SAMPLE I.D. | ADH% | MOIST | PROXIMATE |      |       | S%   | BTU/LB | HGI   | S.G. | CALC * BASIS |
|---------|-------------|------|-------|-----------|------|-------|------|--------|-------|------|--------------|
|         |             |      |       | ASH %     | VOL% | F.C.% |      |        |       |      |              |
| 6381    | Sample 13   | 0.8  | 1.0   | 38.0      | 15.9 | 45.1  | 0.40 | 8920   | 49    | 1.63 | a.d.b.       |
|         | SNTR 18/13  |      | 1.8   | 37.7      | 15.8 | 44.7  | 0.40 | 8849   | -     | -    | a.r.b.       |
|         |             |      |       |           | 38.4 | 16.1  | 45.5 | 0.40   | 9010  | -    | -            |
| 6382    | Sample 14   | 2.4  | 1.5   | 12.0      | 20.7 | 65.8  | 0.50 | 12601  | 70    | 1.42 | a.d.b.       |
|         | SNTR 18/14  |      | 3.9   | 11.7      | 20.2 | 64.2  | 0.49 | 12299  | -     | -    | a.r.b.       |
|         |             |      |       |           | 12.2 | 21.0  | 66.8 | 0.51   | 12793 | -    | -            |
| 6383    | Sample 15   | 5.7  | 1.9   | 23.3      | 25.5 | 49.3  | 0.40 | 10535  | 86    | 1.49 | a.d.b.       |
|         | SNTR 18/15  |      | 7.5   | 22.0      | 24.0 | 46.5  | 0.38 | 9935   | -     | -    | a.r.b.       |
|         |             |      |       |           | 23.8 | 26.0  | 50.2 | 0.41   | 10739 | -    | -            |
| 6384    | Sample 16   | 6.0  | 2.5   | 6.4       | 26.7 | 64.4  | 0.43 | 12739  | 78    | 1.38 | a.d.b.       |
|         | SNTR 18/16  |      | 8.4   | 6.0       | 25.1 | 60.5  | 0.40 | 11975  | -     | -    | a.r.b.       |
|         |             |      |       |           | 6.6  | 27.4  | 66.0 | 0.44   | 13066 | -    | -            |
| 6385    | Sample 17   | 8.3  | 3.4   | 8.4       | 26.9 | 61.3  | 0.35 | 12060  | 91    | 1.40 | a.d.b.       |
|         | SNTR 18/17  |      | 11.4  | 7.7       | 24.7 | 56.2  | 0.32 | 11059  | -     | -    | a.r.b.       |
|         |             |      |       |           | 8.7  | 27.8  | 63.5 | 0.36   | 12484 | -    | -            |
| 6386    | Sample 18   | 10.0 | 4.9   | 13.9      | 26.3 | 54.9  | 0.28 | 10433  | 96    | 1.49 | a.d.b.       |
|         | SNTR 18/18  |      | 14.4  | 12.5      | 23.7 | 49.4  | 0.25 | 9390   | -     | -    | a.r.b.       |
|         |             |      |       |           | 14.6 | 27.7  | 57.7 | 0.29   | 10971 | -    | -            |
| 6387    | Sample 19   | 4.8  | 2.7   | 61.4      | 13.0 | 22.9  | 0.17 | -      | 61    | 1.98 | a.d.b.       |
|         | SNTR 18/19  |      | 7.4   | 58.5      | 12.4 | 21.7  | 0.16 | -      | -     | -    | a.r.b.       |
|         |             |      |       |           | 63.1 | 13.4  | 23.5 | 0.17   | -     | -    | -            |

air dried basis - a.d.b.  
as received basis - a.r.b.  
dry basis - d.b.

Birtley Coal  
& Minerals Testing

A DIVISION OF CRAYNE STEEL INDUSTRIES LTD

CLIENT : BP EXPLORATION CANADA

PROJECT : SNTR 18 SAMPLES RECEIVED OCT. 30, 1980

Service W.O.# 63205

| LAB NO. | SAMPLE I.D. | ADM% | MOIST | PROXIMATE |      |       | S%   | BTU/LB | HGI | S.G. | CALC * BASIS |
|---------|-------------|------|-------|-----------|------|-------|------|--------|-----|------|--------------|
|         |             |      |       | ASH %     | VOL% | F.C.% |      |        |     |      |              |
| 6388    | Sample 20   | 13.1 | 7.6   | 9.9       | 25.3 | 57.2  | 0.21 | 10327  | 95  | 1.51 | a.d.b.       |
|         | SNTR-18/20  |      | 19.7  | 8.6       | 22.0 | 49.7  | 0.18 | 8974   | -   | -    | a.r.b.       |
|         |             |      |       | 10.7      | 27.4 | 61.9  | 0.23 | 11176  | -   | -    | d.b.         |
|         |             |      |       |           |      |       |      |        |     |      |              |
|         |             |      |       |           |      |       |      |        |     |      |              |
|         |             |      |       |           |      |       |      |        |     |      |              |
|         |             |      |       |           |      |       |      |        |     |      |              |
|         |             |      |       |           |      |       |      |        |     |      |              |
|         |             |      |       |           |      |       |      |        |     |      |              |
|         |             |      |       |           |      |       |      |        |     |      |              |
|         |             |      |       |           |      |       |      |        |     |      |              |
|         |             |      |       |           |      |       |      |        |     |      |              |
|         |             |      |       |           |      |       |      |        |     |      |              |
|         |             |      |       |           |      |       |      |        |     |      |              |
|         |             |      |       |           |      |       |      |        |     |      |              |
|         |             |      |       |           |      |       |      |        |     |      |              |
|         |             |      |       |           |      |       |      |        |     |      |              |

air dried basis - a.d.b.  
as received basis - a.r.b.  
dry basis - d.b.

CLIENT : B.P. EXPLORATION (ADA) LTD.

PROJECT : SN-80 CORE SAMPLES RECEIVED JULY 31, 1980.

| LAB NO. | SAMPLE I.D. | ADM% MOIST | PROXIMATE |      |       | S%   | FSI  | BTU/LB | HGI   | S.G.  | CALC BASIS |        |
|---------|-------------|------------|-----------|------|-------|------|------|--------|-------|-------|------------|--------|
|         |             |            | ASH %     | VOL% | F.C.% |      |      |        |       |       |            |        |
| 5548    | 1/1/1       | 0.9        | 1.1       | 24.7 | 17.8  | 56.4 | 0.37 | 1      | 10799 | 64    | 1.53       | a.d.b. |
|         | BP80-01/1/1 |            | 2.0       | 24.5 | 17.6  | 55.9 | 0.37 | -      | 10702 | -     | -          | a.r.b. |
|         |             |            |           |      | 25.0  | 18.0 | 57.0 | 0.37   | -     | 10919 | -          | -      |
| 5549    | 1/1/2       | 1.2        | 1.3       | 58.4 | -     | -    | -    | -      | -     | 53    | -          | a.d.b. |
|         | BP80-01/1/2 |            | 2.5       | 57.7 | -     | -    | -    | -      | -     | -     | -          | a.r.b. |
|         |             |            |           |      | 59.2  | -    | -    | -      | -     | -     | -          | -      |
| 5550    | 1/1/3       | 1.5        | 1.2       | 6.8  | 24.2  | 67.8 | 0.47 | 2      | 14495 | 54    | 1.33       | a.d.b. |
|         | BP80-01/1/3 |            | 2.7       | 6.7  | 23.8  | 66.8 | 0.46 | -      | 14278 | -     | -          | a.r.b. |
|         |             |            |           |      | 6.9   | 24.5 | 68.6 | 0.48   | -     | 14671 | -          | -      |
| 5551    | 1/1/4       | 2.3        | 1.2       | 7.5  | 26.2  | 65.1 | 0.39 | 5      | 13908 | 57    | 1.32       | a.d.b. |
|         | BP80-01/1/4 |            | 3.5       | 7.3  | 25.6  | 63.6 | 0.38 | -      | 13588 | -     | -          | a.r.b. |
|         |             |            |           |      | 7.6   | 26.5 | 65.9 | 0.39   | -     | 14077 | -          | -      |
| 5552    | 1/1/5       | 1.2        | 1.7       | 60.3 | -     | -    | -    | -      | -     | 58    | -          | a.d.b. |
|         | BP80-01/1/5 |            | 2.9       | 59.6 | -     | -    | -    | -      | -     | -     | -          | a.r.b. |
|         |             |            |           |      | 61.3  | -    | -    | -      | -     | -     | -          | -      |
| 5553    | 1/1/F       | 1.3        | 1.5       | 63.8 | -     | -    | -    | -      | -     | 50    | -          | a.d.b. |
|         | BP80-01/1/F |            | 2.8       | 63.0 | -     | -    | -    | -      | -     | -     | -          | a.r.b. |
|         |             |            |           |      | 64.8  | -    | -    | -      | -     | -     | -          | -      |
| 5554    | 1/1/R       | 1.0        | 1.4       | 90.6 | -     | -    | -    | -      | -     | NSS   | -          | a.d.b. |
|         | BP80-01/1/R |            | 2.4       | 89.7 | -     | -    | -    | -      | -     | -     | -          | a.r.b. |
|         |             |            |           |      | 91.9  | -    | -    | -      | -     | -     | -          | -      |

N.S.S. - Not sufficient sample

air dried basis - a.d.b.  
as received basis - a.r.b.  
dry basis - d.b.

Birtley Coal  
& Minerals Testing



CLIENT : B.P. EXPLORATION, ADA LIMITED

PROJECT : SN-80 CORE SAMPLES RECEIVED JULY 31, 1980.

| LAB NO. | SAMPLE I.D. | ADM% | MOIST | PROXIMATE |      |       | S%   | FSI   | BTU/LB | HGI | S.G. | CALC BASIS |
|---------|-------------|------|-------|-----------|------|-------|------|-------|--------|-----|------|------------|
|         |             |      |       | ASH %     | VOL% | F.C.% |      |       |        |     |      |            |
| 5555    | 1/2/1       | 0.9  | 1.5   | 4.4       | 19.9 | 74.2  | 0.44 | 1/2   | 14451  | 57  | 1.33 | a.d.b.     |
|         | BP80-01/2/1 |      | 2.4   | 4.4       | 19.7 | 73.5  | 0.44 | -     | 14321  | -   | -    | a.r.b.     |
|         |             |      |       | 4.5       | 20.2 | 75.3  | 0.45 | -     | 14671  | -   | -    | d.b.       |
| 5556    | 1/2/1       | 1.5  | 1.3   | 4.3       | 19.4 | 75.0  | 0.30 | 1/2   | 14432  | 56  | 1.33 | a.d.b.     |
|         | BP80-01/2/1 |      | 2.8   | 4.2       | 19.1 | 73.9  | 0.30 | -     | 14216  | -   | -    | a.r.b.     |
|         |             |      |       | 4.4       | 19.7 | 75.9  | 0.30 | -     | 14622  | -   | -    | d.b.       |
| 5557    | 1/2/2       | 5.3  | 1.1   | 57.4      | -    | -     | -    | -     | -      | 63  | -    | a.d.b.     |
|         | BP80-01/2/2 |      | 6.3   | 54.4      | -    | -     | -    | -     | -      | -   | -    | a.r.b.     |
|         |             |      |       | 58.0      | -    | -     | -    | -     | -      | -   | -    | -          |
| 5558    | 1/2/3       | 1.3  | 1.1   | 16.2      | 22.3 | 60.4  | 0.36 | 3     | 12741  | 58  | 1.40 | a.d.b.     |
|         | BP80-01/2/3 |      | 2.4   | 16.0      | 22.0 | 59.6  | 0.36 | -     | 12575  | -   | -    | a.r.b.     |
|         |             |      |       | 16.4      | 22.5 | 61.1  | 0.36 | -     | 12883  | -   | -    | d.b.       |
| 5559    | 1/2/4       | 0.6  | 1.2   | 33.5      | 18.2 | 47.1  | 0.34 | 1     | 9811   | 54  | 1.55 | a.d.b.     |
|         | BP80-01/2/4 |      | 1.8   | 33.3      | 18.1 | 46.8  | 0.34 | -     | 9752   | -   | -    | a.r.b.     |
|         |             |      |       | 33.9      | 18.4 | 47.7  | 0.34 | -     | 9930   | -   | -    | d.b.       |
| 5560    | 1/2/5       | 1.4  | 1.2   | 23.8      | 19.6 | 55.4  | 0.35 | 1 1/2 | 11298  | 58  | 1.48 | a.d.b.     |
|         | BP80-01/2/5 |      | 2.3   | 23.5      | 19.4 | 54.8  | 0.35 | -     | 11174  | -   | -    | a.r.b.     |
|         |             |      |       | 24.1      | 19.8 | 56.1  | 0.35 | -     | 11435  | -   | -    | d.b.       |
| 5561    | 1/2/R       | 2.7  | 1.5   | 88.1      | -    | -     | -    | -     | -      | NSS | -    | a.d.b.     |
|         | BP80-01/2.R |      | 4.2   | 85.7      | -    | -     | -    | -     | -      | -   | -    | a.r.b.     |
|         |             |      |       | 89.4      | -    | -     | -    | -     | -      | -   | -    | -          |

N.S.S. - not sufficient sample

air dried basis - a.d.b.  
as received basis - a.r.b.  
dry basis - d.b.

Birtley Coal  
& Minerals Testing

420000 2000 0000 0000 0000 0000 0000 0000

CLIENT : B.P. EXPLORATION CANADA LIMITED  
 PROJECT : SN-80 CORE SAMPLES RECEIVED JULY 31, 1980

| LAB NO. | SAMPLE I.D. | ADM% MOIST | PROXIMATE |      |       | S% FS1 | BTU/LB | HGT   | S.G.  | CALC BASIS |      |        |
|---------|-------------|------------|-----------|------|-------|--------|--------|-------|-------|------------|------|--------|
|         |             |            | ASH %     | VOL% | F.C.% |        |        |       |       |            |      |        |
| 5562    | 1/3/1       | 1.4        | 1.1       | 18.1 | 21.1  | 59.7   | 0.39   | 3 1/2 | 12355 | 63         | 1.42 | a.d.b. |
|         | BP80-01/3/1 |            | 2.5       | 17.8 | 20.8  | 58.9   | 0.38   | -     | 12182 | -          | -    | a.r.b. |
|         |             |            |           |      | 18.3  | 21.3   | 60.4   | 0.39  | -     | 12492      | -    | -      |
| 5563    | 1/3/2       | 0.8        | 1.6       | 84.8 | -     | -      | -      | -     | -     | NSS        | -    | a.d.b. |
|         | BP80-01/3/2 |            | 2.4       | 84.1 | -     | -      | -      | -     | -     | -          | -    | a.r.b. |
|         |             |            |           |      | 86.2  | -      | -      | -     | -     | -          | -    | -      |
| 5564    | 1/3/3       | 0.7        | 1.0       | 29.9 | 17.8  | 51.3   | 0.36   | 1     | 10367 | 63         | 1.54 | a.d.b. |
|         | BP80-01/3/3 |            | 1.7       | 29.7 | 17.7  | 50.9   | 0.36   | -     | 10294 | -          | -    | a.r.b. |
|         |             |            |           |      | 30.2  | 18.0   | 51.8   | 0.36  | -     | 10472      | -    | -      |
| 5565    | 1/3/F       | 1.1        | 1.4       | 51.0 | -     | -      | -      | -     | -     | 53         | -    | a.d.b. |
|         | BP80-01/3/F |            | 2.5       | 50.4 | -     | -      | -      | -     | -     | -          | -    | a.r.b. |
|         |             |            |           |      | 51.7  | -      | -      | -     | -     | -          | -    | -      |
| 5566    | 1/3/R       | 0.8        | 0.7       | 43.5 | 15.0  | 40.8   | 0.26   | 1     | 8244  | 48         | 1.67 | a.d.b. |
|         | BP80-01/3/R |            | 1.5       | 43.2 | 14.9  | 40.4   | 0.26   | -     | 8178  | -          | -    | a.r.b. |
|         |             |            |           |      | 43.8  | 15.1   | 41.1   | 0.26  | -     | 8302       | -    | -      |
|         |             |            |           |      |       |        |        |       |       |            |      |        |
|         |             |            |           |      |       |        |        |       |       |            |      |        |
|         |             |            |           |      |       |        |        |       |       |            |      |        |

air dried basis - a.d.b.  
 as received basis - a.r.b.  
 dry basis - d.b.

Birtley Coal & Minerals Testing

CLIENT : B.P. EXPLORATION CANADA LIMITED

PROJECT : SN-80 CORE SAMPLES Received August 5, 1980

| LAB NO. | SAMPLE I.D. | ADME | MOIST | PROXIMATE |      |       | S%   | FSI   | BTU/LB | HGI   | S.G. | CALC BASIS |        |
|---------|-------------|------|-------|-----------|------|-------|------|-------|--------|-------|------|------------|--------|
|         |             |      |       | ASH %     | VOL% | F.C.% |      |       |        |       |      |            |        |
| 5570    | 2-1-1       | 0.6  | 0.9   | 4.0       | 26.1 | 69.0  | 0.56 | 6 1/2 | 14679  | 64    | 1.30 | a.d.b.     |        |
|         | BP80-02/1/1 |      | 1.5   | 4.0       | 25.9 | 68.6  | 0.56 | -     | 14591  | -     | -    | a.r.b.     |        |
|         |             |      |       |           | 4.0  | 26.3  | 69.7 | 0.57  | -      | 14812 | -    | -          | d.b.   |
| 5571    | 2-1-2       | 0.5  | 0.6   | 9.1       | 27.0 | 63.3  | 0.51 | 8 1/2 | 14045  | 88    | 1.32 | a.d.b.     |        |
|         | BP80-02/1/2 |      | 1.1   | 9.1       | 26.9 | 62.9  | 0.51 | -     | 13975  | -     | -    | a.r.b.     |        |
|         |             |      |       |           | 9.2  | 27.2  | 63.6 | 0.51  | -      | 14130 | -    | -          | d.b.   |
| 5572    | 2-1-F       | 0.6  | 1.3   | 66.2      | -    | -     | -    | -     | -      | 50    | -    | a.d.b.     |        |
|         | BP80-02/1/P |      | 1.9   | 65.8      | -    | -     | -    | -     | -      | -     | -    | -          | a.r.b. |
|         |             |      |       |           | 67.1 | -     | -    | -     | -      | -     | -    | -          | -      |
| 5573    | 2-1-R       | 0.6  | 1.2   | 85.0      | -    | -     | -    | -     | -      | 46    | -    | a.d.b.     |        |
|         | BP80-02/1/R |      | 1.8   | 84.5      | -    | -     | -    | -     | -      | -     | -    | -          | a.r.b. |
|         |             |      |       |           | 86.0 | -     | -    | -     | -      | -     | -    | -          | -      |
| 5574    | 2-2-1       | 1.4  | 0.9   | 31.8      | 16.5 | 50.8  | 0.39 | 1     | 9823   | 73    | 1.59 | a.d.b.     |        |
|         | BP80-02/2/1 |      | 2.3   | 31.4      | 16.3 | 50.0  | 0.38 | -     | 9685   | -     | -    | a.r.b.     |        |
|         |             |      |       |           | 32.1 | 16.6  | 51.3 | 0.39  | -      | 9912  | -    | -          | d.b.   |
| 5575    | 2-2-2       | 1.4  | 0.3   | 63.7      | -    | -     | -    | -     | -      | 88    | -    | a.d.b.     |        |
|         | BP80-02/2/2 |      | 1.7   | 62.8      | -    | -     | -    | -     | -      | -     | -    | -          | a.r.b. |
|         |             |      |       |           | 63.9 | -     | -    | -     | -      | -     | -    | -          | -      |
| 5576    | 2-2-3       | 0.5  | 1.0   | 18.2      | 21.2 | 59.6  | 0.47 | 2 1/2 | 12153  | 62    | 1.43 | a.d.b.     |        |
|         | BP80-02/2/3 |      | 1.5   | 18.1      | 21.1 | 59.3  | 0.47 | -     | 12092  | -     | -    | a.r.b.     |        |
|         |             |      |       |           | 18.4 | 21.4  | 60.2 | 0.47  | -      | 12276 | -    | -          | d.b.   |

\* air dried basis - a.d.b.  
 as received basis - a.r.b.  
 dry basis - d.b.

Birtley Coal & Minerals Testing

4000 Highway 104, Birtley, N.B. Canada

CLIENT : B.P. EXPLORATION WADA LIMITED  
 PROJECT : SN-80-CORE, SAMPLES Received August 5, 1980

| LAB NO. | SAMPLE I.D. | ADM% MOIST | PROXIMATE |      |       | S%   | FSI  | BTU/LB | HGI   | S.G.  | CALC BASI |        |
|---------|-------------|------------|-----------|------|-------|------|------|--------|-------|-------|-----------|--------|
|         |             |            | ASH %     | VOL% | F.C.% |      |      |        |       |       |           |        |
| 5577    | 2-2-4       | 0.9        | 1.6       | 74.9 | -     | -    | -    | -      | 50    | -     | a.d.b.    |        |
|         | BP80-02/2/4 |            | 2.5       | 74.2 | -     | -    | -    | -      | -     | -     | a.r.b.    |        |
|         |             |            |           |      | 76.1  | -    | -    | -      | -     | -     | -         | d.b.   |
| 5578    | 2-2-5       | 0.8        | 1.0       | 24.0 | 19.4  | 55.6 | 0.36 | 1      | 11324 | 59    | 1.49      | a.d.b. |
|         | BP80-02/2/5 |            | 1.8       | 23.8 | 19.2  | 55.2 | 0.36 | -      | 11233 | -     | -         | a.r.b. |
|         |             |            |           |      | 24.2  | 19.6 | 56.2 | 0.36   | -     | 11438 | -         | -      |
| 5579    | 2-2-6       | 0.6        | 1.5       | 79.0 | -     | -    | -    | -      | -     | NSS   | -         | a.d.b. |
|         | BP80-02/2/6 |            | 2.1       | 78.5 | -     | -    | -    | -      | -     | -     | -         | a.r.b. |
|         |             |            |           |      | 80.2  | -    | -    | -      | -     | -     | -         | -      |
| 5580    | 2-2-7       | 0.6        | 1.1       | 8.6  | 26.5  | 63.8 | 0.43 | 8      | 13959 | 66    | 1.32      | a.d.b. |
|         | BP80-02/2/7 |            | 1.7       | 8.5  | 26.3  | 63.5 | 0.43 | -      | 13875 | -     | -         | a.r.b. |
|         |             |            |           |      | 8.7   | 26.8 | 64.5 | 0.43   | -     | 14114 | -         | -      |
| 5581    | 2-2-F       | 0.7        | 1.4       | 63.5 | -     | -    | -    | -      | -     | 51    | -         | a.d.b. |
|         | BP80-02/2/F |            | 2.1       | 63.1 | -     | -    | -    | -      | -     | -     | -         | a.r.b. |
|         |             |            |           |      | 64.4  | -    | -    | -      | -     | -     | -         | -      |
| 5582    | 2-2-R       | 0.7        | 1.3       | 69.7 | -     | -    | -    | -      | -     | 53    | -         | a.d.b. |
|         | BP80-02/2/R |            | 2.0       | 69.2 | -     | -    | -    | -      | -     | -     | -         | a.r.b. |
|         |             |            |           |      | 70.6  | -    | -    | -      | -     | -     | -         | -      |
| 5583    | 2-3-1       | 0.7        | 1.2       | 58.9 | -     | -    | -    | -      | -     | 53    | -         | a.d.b. |
|         | BP80-02/3/1 |            | 1.9       | 58.5 | -     | -    | -    | -      | -     | -     | -         | a.r.b. |
|         |             |            |           |      | 59.6  | -    | -    | -      | -     | -     | -         | -      |

N.S.S. - not sufficient sample

\* air dried basis - a.d.b.  
 as received basis - a.r.b.  
 dry basis - d.b.

Birtley Coal & Minerals Testing

| AB NO. | SAMPLE I.D. | ADM% MOIST | PROXIMATE |      |       | S%   | FSI  | BTU/LB | HGI   | S.G. | CALC BASIS |        |
|--------|-------------|------------|-----------|------|-------|------|------|--------|-------|------|------------|--------|
|        |             |            | ASH %     | VOL% | F.C.% |      |      |        |       |      |            |        |
| 5584   | 2-3-2       | 0.6        | 1.2       | 78.1 | -     | -    | -    | -      | 46    | -    | a.d.b.     |        |
|        | BP80-02/3/2 |            | 1.8       | 77.6 | -     | -    | -    | -      | -     | -    | a.r.b.     |        |
|        |             |            |           | 79.0 | -     | -    | -    | -      | -     | -    | d.b.       |        |
| 5585   | 2-3-3       | 0.6        | 1.3       | 46.1 | 17.0  | 35.6 | 0.49 | 4 1/2  | 7646  | 60   | 1.70       | a.d.b. |
|        | BP80-02/3/3 |            | 1.9       | 45.8 | 16.9  | 35.4 | 0.49 | -      | 7600  | -    | -          | a.r.b. |
|        |             |            |           | 46.7 | 17.2  | 36.1 | 0.50 | -      | 7747  | -    | -          | d.b.   |
| 5586   | 2-3-4       | 1.1        | 1.6       | 75.7 | -     | -    | -    | -      | -     | 46   | -          | a.d.b. |
|        | BP80-02/3/4 |            | 2.7       | 74.9 | -     | -    | -    | -      | -     | -    | -          | a.r.b. |
|        |             |            |           | 76.9 | -     | -    | -    | -      | -     | -    | -          | d.b.   |
| 5587   | 2-3-5       | 0.5        | 0.9       | 23.0 | 15.2  | 60.9 | 0.46 | 1      | 11269 | 70   | 1.53       | a.d.b. |
|        | BP80-02/3/5 |            | 1.4       | 22.9 | 15.1  | 60.6 | 0.46 | -      | 11212 | -    | -          | a.r.b. |
|        |             |            |           | 23.2 | 15.3  | 61.5 | 0.46 | -      | 11371 | -    | -          | d.b.   |
| 5588   | 2-3-6       | 0.5        | 1.1       | 18.4 | 25.9  | 54.6 | 0.34 | NA     | 10982 | 80   | 1.53       | a.d.b. |
|        | BP80-02/3/6 |            | 1.6       | 18.3 | 25.8  | 54.3 | 0.34 | -      | 10927 | -    | -          | a.r.b. |
|        |             |            |           | 18.6 | 26.2  | 55.2 | 0.34 | -      | 11104 | -    | -          | d.b.   |
| 5589   | 2-3-7       | 0.8        | 1.2       | 4.8  | 18.8  | 75.2 | 0.52 | 1 1/2  | 14455 | 72   | 1.35       | a.d.b. |
|        | BP80-02/3/7 |            | 2.0       | 4.8  | 18.6  | 74.6 | 0.52 | -      | 14339 | -    | -          | a.r.b. |
|        |             |            |           | 4.9  | 19.0  | 76.1 | 0.53 | -      | 14631 | -    | -          | d.b.   |
| 5590   | 2-3-8       | 0.5        | 1.1       | 9.0  | 20.3  | 69.6 | 0.62 | 1 1/2  | 13765 | 78   | 1.37       | a.d.b. |
|        | BP80-02/3/8 |            | 1.6       | 9.0  | 20.2  | 69.2 | 0.62 | -      | 13696 | -    | -          | a.r.b. |
|        |             |            |           | 9.1  | 20.5  | 70.4 | 0.63 | -      | 13918 | -    | -          | d.b.   |

air dried basis - a.d.b.  
as received basis - a.r.b.  
dry basis - d.b.

Birley Coal & Minerals Testing

CLIENT : B.P. EXPLORATION / CANADA LIMITED

PROJECT : SN-80 CORE SAMPLES Received August 5, 1980

| LAB NO. | SAMPLE I.D.                | ADM% MOIST | PROXIMATE |      |       | S%   | FSI  | BTU/LB | HGI  | S.G. | CALC BASIS |        |
|---------|----------------------------|------------|-----------|------|-------|------|------|--------|------|------|------------|--------|
|         |                            |            | ASH %     | VOL% | F.C.% |      |      |        |      |      |            |        |
| 5591    | 2-3-9<br>BP80-02/<br>3/9   | 1.3        | 1.1       | 64.7 | -     | -    | -    | -      | 50   | -    | a.d.b.     |        |
|         |                            |            | 2.4       | 63.9 | -     | -    | -    | -      | -    | -    | a.r.b.     |        |
|         |                            |            |           | 65.4 | -     | -    | -    | -      | -    | -    | -          | d.b.   |
| 5592    | 2-3-10<br>BP80-02/<br>3/10 | 0.8        | 1.1       | 36.3 | 19.1  | 43.5 | 0.45 | 5 1/2  | 9373 | 62   | 1.58       | a.d.b. |
|         |                            |            | 1.9       | 36.0 | 18.9  | 43.2 | 0.45 | -      | 9298 | -    | -          | a.r.b. |
|         |                            |            |           | 36.7 | 19.3  | 44.0 | 0.46 | -      | 9477 | -    | -          | d.b.   |
| 5593    | 2-3-11<br>BP80-02/<br>3/11 | 0.9        | 1.6       | 72.4 | -     | -    | -    | -      | -    | 50   | -          | a.d.b. |
|         |                            |            | 2.5       | 71.7 | -     | -    | -    | -      | -    | -    | -          | a.r.b. |
|         |                            |            |           | 73.6 | -     | -    | -    | -      | -    | -    | -          | d.b.   |
| 5594    | 2-3-12<br>BP80-02/<br>3/12 | 0.8        | 1.2       | 43.7 | 17.2  | 37.9 | 0.40 | 4 1/2  | 7900 | 58   | 1.67       | a.d.b. |
|         |                            |            | 2.0       | 43.4 | 17.1  | 37.5 | 0.40 | -      | 7837 | -    | -          | a.r.b. |
|         |                            |            |           | 44.2 | 17.4  | 38.4 | 0.40 | -      | 7996 | -    | -          | d.b.   |
| 5595    | 2-3-F<br>BP80-02/<br>3/F   | 0.9        | 1.5       | 70.0 | -     | -    | -    | -      | -    | 51   | -          | a.d.b. |
|         |                            |            | 2.4       | 69.4 | -     | -    | -    | -      | -    | -    | -          | a.r.b. |
|         |                            |            |           | 71.1 | -     | -    | -    | -      | -    | -    | -          | -      |

air dried basis - a.d.b.  
 as received basis - a.r.b.  
 dry basis - d.b.

Birley Coal  
 & Minerals Testing

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CLIENT : BP EXPLORATION CANADA  
 PROJECT: SH-80 COMPOSITE RAW COAL

LAB NO. 6614

SAMPLE NO. 1/1 - PG1

| RM% | ASH% | CALC BASIS |
|-----|------|------------|
| 1.1 | 9.3  | a.d.b.     |
|     | 9.4  | d.b.       |

BP-1  
 PUMP SEAM

| MINERAL ANALYSIS OF ASH |       |      |       |      |      |      |      |      |      |        |
|-------------------------|-------|------|-------|------|------|------|------|------|------|--------|
| SiO2                    | Al2O3 | TiO2 | Fe2O3 | CaO  | MgO  | Na2O | K2O  | P2O5 | SO3  | Undet. |
| 60.06                   | 26.06 | 0.94 | 1.39  | 2.08 | 0.79 | 1.21 | 1.19 | 3.29 | 1.10 | - 1.89 |

LAB NO. 6615

SAMPLE NO. 1/2 - PG2

| RM% | ASH% | CALC BASIS |
|-----|------|------------|
| 1.1 | 10.6 | a.d.b.     |
|     | 10.7 | d.b.       |

BP-1  
 GRIZZLY SEAM

| MINERAL ANALYSIS OF ASH |       |      |       |      |      |      |      |      |      |        |
|-------------------------|-------|------|-------|------|------|------|------|------|------|--------|
| SiO2                    | Al2O3 | TiO2 | Fe2O3 | CaO  | MgO  | Na2O | K2O  | P2O5 | SO3  | Undet. |
| 66.84                   | 21.73 | 1.28 | 1.18  | 0.89 | 0.63 | 1.04 | 1.13 | 2.69 | 0.63 | - 1.96 |

Birtley Coal  
 & Minerals Testing

A. J. BIRTLEY & SONS LTD. TORONTO, CANADA

LAB NO.: 5548 SAMPLE I.D. 1/1/1

| ASH FUSION TEMPERATURES (°F) |        |       |      |      |
|------------------------------|--------|-------|------|------|
| ATMOSPHERE                   | I.D.T. | S.T.  | H.T. | F.T. |
| OXIDIZING                    | 2800+  |       |      |      |
| REDUCING                     | 2790   | 2800+ |      |      |

LAB NO.: 5550 SAMPLE I.D. 1/1/3

| ASH FUSION TEMPERATURES (°F) |        |      |      |      |
|------------------------------|--------|------|------|------|
| ATMOSPHERE                   | I.D.T. | S.T. | H.T. | F.T. |
| OXIDIZING                    | 2260   | 2410 | 2520 | 2610 |
| REDUCING                     | 2200   | 2370 | 2480 | 2570 |

LAB NO.: 5551 SAMPLE I.D. 1/1/4

| ASH FUSION TEMPERATURES (°F) |        |      |      |      |
|------------------------------|--------|------|------|------|
| ATMOSPHERE                   | I.D.T. | S.T. | H.T. | F.T. |
| OXIDIZING                    | 2560   | 2680 | 2750 | 2800 |
| REDUCING                     | 2320   | 2580 | 2690 | 2780 |



PROJECT: SN-80 CORE SAMPLE Received July 31, 1980

LAB NO.: 5555 SAMPLE I.D. 1/2/1

| ASH FUSION TEMPERATURES (°F) |        |      |       |       |
|------------------------------|--------|------|-------|-------|
| ATMOSPHERE                   | I.D.T. | S.T. | H.T.  | F.T.  |
| OXIDIZING                    | 2600   | 2760 | 2800+ |       |
| REDUCING                     | 2520   | 2720 | 2760  | 2800+ |

LAB NO.: 5556 SAMPLE I.D. 1/2/2

| ASH FUSION TEMPERATURES (°F) |        |      |      |      |
|------------------------------|--------|------|------|------|
| ATMOSPHERE                   | I.D.T. | S.T. | H.T. | F.T. |
| OXIDIZING                    | 2370   | 2520 | 2640 | 2750 |
| REDUCING                     | 2320   | 2480 | 2570 | 2710 |

LAB NO.: 5558 SAMPLE I.D. 1/2/3

| ASH FUSION TEMPERATURES (°F) |        |       |       |      |
|------------------------------|--------|-------|-------|------|
| ATMOSPHERE                   | I.D.T. | S.T.  | H.T.  | F.T. |
| OXIDIZING                    | 2690   | 2800+ |       |      |
| REDUCING                     | 2570   | 2800  | 2800+ |      |

PROJECT: SN-SO CORE SAMPLE Received July 31, 1980  
LAB NO.: 5559 SAMPLE I.D. 1/2/4

| ASH FUSION TEMPERATURES (°F) |        |       |      |      |
|------------------------------|--------|-------|------|------|
| ATMOSPHERE                   | I.D.T. | S.T.  | H.T. | F.T. |
| OXIDIZING                    | 2720   | 2800+ |      |      |
| REDUCING                     | 2590   | 2800+ |      |      |

LAB NO.: 5560 SAMPLE I.D. 1/2/5

| ASH FUSION TEMPERATURES (°F) |        |       |       |      |
|------------------------------|--------|-------|-------|------|
| ATMOSPHERE                   | I.D.T. | S.T.  | H.T.  | F.T. |
| OXIDIZING                    | 2680   | 2800+ |       |      |
| REDUCING                     | 2560   | 2780  | 2800+ |      |

LAB NO.: 5562 SAMPLE I.D. 1/3/1

| ASH FUSION TEMPERATURES (°F) |        |      |       |       |
|------------------------------|--------|------|-------|-------|
| ATMOSPHERE                   | I.D.T. | S.T. | H.T.  | F.T.  |
| OXIDIZING                    | 2620   | 2770 | 2800+ |       |
| REDUCING                     | 2550   | 2720 | 2770  | 2800+ |

PROJECT: SN-50 CORE SAMPLE: Received July 31, 1980

LAB NO.: 5564 SAMPLE I.D. 1/3/3

| ASH FUSION TEMPERATURES (°F) |        |      |      |       |
|------------------------------|--------|------|------|-------|
| ATMOSPHERE                   | I.D.T. | S.T. | H.T. | F.T.  |
| OXIDIZING                    | 2570   | 2710 | 2780 | 2800+ |
| REDUCING                     | 2520   | 2680 | 2740 | 2800+ |

LAB NO.: 5566 SAMPLE I.D. 1/3/R

| ASH FUSION TEMPERATURES (°F) |        |       |      |      |
|------------------------------|--------|-------|------|------|
| ATMOSPHERE                   | I.D.T. | S.T.  | H.T. | F.T. |
| OXIDIZING                    | 2690   | 2800+ |      |      |
| REDUCING                     | 2640   | 2800+ |      |      |

LAB NO.: SAMPLE I.D.

| ASH FUSION TEMPERATURES (°F) |        |      |      |      |
|------------------------------|--------|------|------|------|
| ATMOSPHERE                   | I.D.T. | S.T. | H.T. | F.T. |
|                              |        |      |      |      |
|                              |        |      |      |      |

CLIENT : BP EXPLORATION CO. DA

PROJECT: SN-80 CORE SAMPLES

Received August 5, 1980

LAB NO.: 5570

SAMPLE I.D. 2/1/1

| ASH FUSION TEMPERATURES (°F) |        |      |      |      |
|------------------------------|--------|------|------|------|
| ATMOSPHERE                   | I.D.T. | S.T. | H.T. | F.T. |
| OXIDIZING                    | 2290   | 2420 | 2530 | 2700 |
| REDUCING                     | 2250   | 2390 | 2450 | 2620 |

LAB NO.: 5571

SAMPLE I.D. 2/1/2

| ASH FUSION TEMPERATURES (°F) |        |      |      |      |
|------------------------------|--------|------|------|------|
| ATMOSPHERE                   | I.D.T. | S.T. | H.T. | F.T. |
| OXIDIZING                    | 2260   | 2450 | 2560 | 2720 |
| REDUCING                     | 2220   | 2400 | 2480 | 2650 |

LAB NO.: 5574

SAMPLE I.D. 2/2/1

| ASH FUSION TEMPERATURES (°F) |        |       |      |      |
|------------------------------|--------|-------|------|------|
| ATMOSPHERE                   | I.D.T. | S.T.  | H.T. | F.T. |
| OXIDIZING                    | 2800+  |       |      |      |
| REDUCING                     | 2780   | 2800+ |      |      |

PROJECT: SN-80 CORE SAMPLE Received Aug. 5, 1980

LAB NO.: 5576 SAMPLE I.D. 2/2/3

| ASH FUSION TEMPERATURES (°F) |        |      |      |      |
|------------------------------|--------|------|------|------|
| ATMOSPHERE                   | I.D.T. | S.T. | H.T. | F.T. |
| OXIDIZING                    | 2800+  |      |      |      |
| REDUCING                     | 2800+  |      |      |      |

LAB NO.: 5578 SAMPLE I.D. 2/2/5

| ASH FUSION TEMPERATURES (°F) |        |      |       |       |
|------------------------------|--------|------|-------|-------|
| ATMOSPHERE                   | I.D.T. | S.T. | H.T.  | F.T.  |
| OXIDIZING                    | 2480   | 2700 | 2800+ |       |
| REDUCING                     | 2430   | 2630 | 2720  | 2800+ |

LAB NO.: 5580 SAMPLE I.D. 2/2/7

| ASH FUSION TEMPERATURES (°F) |        |      |       |       |
|------------------------------|--------|------|-------|-------|
| ATMOSPHERE                   | I.D.T. | S.T. | H.T.  | F.T.  |
| OXIDIZING                    | 2600   | 2790 | 2800+ |       |
| REDUCING                     | 2440   | 2750 | 2780  | 2800+ |

CLIENT : BP EXPLORATION CANADA

PROJECT: SN-80 CORE SAMPLES

Received August 5, 1980

LAB NO.: 5585 SAMPLE I.D. 2/3/3

| ASH FUSION TEMPERATURES (°F) |        |       |      |      |
|------------------------------|--------|-------|------|------|
| ATMOSPHERE                   | I.D.T. | S.T.  | H.T. | F.T. |
| OXIDIZING                    | 2800+  |       |      |      |
| REDUCING                     | 2730   | 2800+ |      |      |

LAB NO.: 5587 SAMPLE I.D. 2/3/5

| ASH FUSION TEMPERATURES (°F) |        |       |      |      |
|------------------------------|--------|-------|------|------|
| ATMOSPHERE                   | I.D.T. | S.T.  | H.T. | F.T. |
| OXIDIZING                    | - 2790 | 2800+ |      | --   |
| REDUCING                     | 2750   | 2800+ | ---  |      |

LAB NO.: 5588 SAMPLE I.D. 2/3/6

| ASH FUSION TEMPERATURES (°F) |        |      |      |      |
|------------------------------|--------|------|------|------|
| ATMOSPHERE                   | I.D.T. | S.T. | H.T. | F.T. |
| OXIDIZING                    | 2420   | 2430 | 2440 | 2460 |
| REDUCING                     | 2140   | 2230 | 2260 | 2330 |

CLIENT : BP EXPLORATION Y... ADA

PROJECT: SN-80 CORE SAMPLES Received August 5, 1980

LAB NO.: 5589 SAMPLE I.D. 2/3/7

| ASH FUSION TEMPERATURES (°F) |        |      |      |      |
|------------------------------|--------|------|------|------|
| ATMOSPHERE                   | I.D.T. | S.T. | H.T. | F.T. |
| OXIDIZING                    | 2200   | 2280 | 2380 | 2520 |
| REDUCING                     | 2160   | 2240 | 2320 | 2470 |

LAB NO.: 5590 SAMPLE I.D. 2/3/8

| ASH FUSION TEMPERATURES (°F) |        |      |      |      |
|------------------------------|--------|------|------|------|
| ATMOSPHERE                   | I.D.T. | S.T. | H.T. | F.T. |
| OXIDIZING                    | 2320   | 2550 | 2640 | 2760 |
| REDUCING                     | 2180   | 2260 | 2340 | 2440 |

LAB NO.: 5592 SAMPLE I.D. 2/3/10

| ASH FUSION TEMPERATURES (°F) |        |       |       |      |
|------------------------------|--------|-------|-------|------|
| ATMOSPHERE                   | I.D.T. | S.T.  | H.T.  | F.T. |
| OXIDIZING                    | 2620   | 2800+ |       |      |
| REDUCING                     | 2570   | 2780  | 2800+ |      |

PROJECT: SN-80 CORE SAMPLES      Received August 5, 1980

LAB. NO.: 5594      SAMPLE I.D. 2/3/12

| ASH FUSION TEMPERATURES (°F) |          |       |       |       |
|------------------------------|----------|-------|-------|-------|
| ATMOSPHERE                   | I. D. T. | S. T. | H. T. | F. T. |
| OXIDIZING                    | 2690     | 2800+ |       |       |
| REDUCING                     | 2570     | 2760  | 2790  | 2800+ |