

Most of Appendix II, Sections 1 & 2 of this report contains coal quality data, and remains confidential under the terms of the *Coal Act Regulation*, Section 2(1). It has been removed from the public version.

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QUINTETTE COAL LIMITED

TRANSFER AREA

GEOLOGICAL REPORT

724



**Quintette
Coal
Limited**

P. O. Box 1500
Tumbler Ridge, B.C., Canada
V0C 2W0

Tel. (604) 242-3221

DENISON MINES LIMITED
MANAGER

April 13, 1987

File No. 4.2.1
No. 6.1.1.6

VIA COURIER

Mr. P. Hagen,
Coal Administrator
Ministry of Energy, Mines and
Petroleum Resources
412, 617 Government Street
Victoria, British Columbia
V8V 1X4

Re: Technical Assessment Report: Quintette Coal Limited 1986 Exploration

Dear Mr. Hagen:

Enclosed please find the "Transfer Area Geological Report" which is submitted in support of previously documented expenditures amounting to \$777,193.84. The costs were incurred from exploration on Quintette Coal Licences during 1986 coal licence year. It would be appreciated if you would forward the report to A. Matheson after your review.

Sincerely yours,

QUINTETTE COAL LIMITED

G.P. Gormley
Chief Mine Geologist

GPG/ccw

Attachment(s)

cc: A. Matheson
J.H.H. Chamberlin

CONFIDENTIAL



DENISON MINES LIMITED
MANAGER

P. O. Box 1500
Tumbler Ridge, B.C., Canada
V0C 2W0
Tel. (604) 242-3221

June 25, 1987

File No. 6.1.1.6

Mr. A. Matheson
Resource Data & Analysis Section
Ministry of Energy, Mines and
Petroleum Resources
105, 525 Superior Street
Victoria, B.C.
V8V 1X4

Dear Alex:

Re: Transfer Area Geophysical Logs:

As per your request please find copies of the geophysical logs completed during our 1984, 1985 and 1986 programmes in the Transfer Area at Quintette Coal Limited.

Sincerely yours,

QUINETTE COAL LIMITED

G.P. Gormley
Chief Mine Geologist

GPG/ccw

Enclosures

cc: J.H.H. Chamberlin

LOG NO: 0629	RD. 4
ACTION:	
FILE NO:	

COPY #1

QUINTETTE COAL LIMITED

TRANSFER AREA

GEOLOGICAL REPORT

TEXT

MARCH 1987

PREFACE

During 1986, geological exploration on Quintette Coal Limited property was undertaken in the following areas:

1. Transfer Area
2. Shikano
3. Mesa Extension

This report and its related appendices introduces all geological data and assessments of the geological structure, stratigraphy, coal quality and reserves of the first area only. Previous geological interpretation of the Shikano and Mesa Extension deposits resulted in their inclusion in the Quintette Coal Limited Development Plan Revision 2, in April, 1986. Results of the 1986 geological exploration in the Mesa Extension are presented in a separate report. Results of rotary drilling in Shikano have been incorporated into ongoing production planning for the mine which commenced operation in October of 1986.

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1.0 SUMMARY

Objectives of Transfer Area Exploration and Work Completed

The purpose for exploration in the Transfer Area is to develop mineable open pit reserves which may prove more economically attractive than certain portions of Quintette Coal Limited's current long term mining plan. Drilling completed to date in the two primary areas covered by this report is summarized as follows:

Summary of Transfer Area Drilling

	<u>Number of Diamond Drill Holes</u>	<u>Number of Rotary Drill Holes</u>
Transfer	8 ✓	--
Grizzly	3 ✓	7

Although drilling is limited at this stage of development, extensive surface geological mapping has confirmed the basic structural interpretation of the two primary anticlines in the Transfer and Grizzly Areas.

Structure

Resources have been estimated on anticline limbs in both the Transfer and Grizzly Area. These structures are similar in nature to the Shikano Anticline currently being mined, their limbs generally dip from 35° to 65° with northwesterly plunges from 0° to 30°. The larger resource potential estimated in the Transfer Area can be mainly attributed to near surface Middle Gates Formation combined with an abnormally flat axial plunge over a strike distance of about 1 kilometre.

Coal Seam Thickness

Seam D, E, F, G, J, K1 and K2, have been identified from drilling to date and are readily correlated to the Shikano deposit coal seams. In both anticlines, thin and or poorly developed intersections have been found in D and E coal seams resulting in their exclusion from current resource evaluation. Seams F and G are well developed, forming single, thick mining sections in both structures. The interseam partings between J, K1 and K2 are variable in thickness such that this zone may be a single mining section (including all partings) or two mining sections.

Thickness range and average values are compared to Shikano as follows:

Seam	Average Mining Section Thickness			Shikano
	Grizzly	Transfer		
D	-	-		2.81
E	-	-		2.12
F	3.52	4.05		4.05
G	3.19	3.70		3.27
J	-	-		4.65
J+K1	6.11	7.13		-
K1	-	-		0.87
K1+K2	-	1.12		-

Coal Quality and Yields

Coal samples taken from drill core were subjected to a full range of testing procedures which generally confirmed its acceptability as metallurgical feed to the wash plant. The plant feed ash values and subsequent plant yield predicted in the preliminary evaluation of resource potential are compared to Shikano as follows:

Seam	Grizzly		Transfer		Shikano	
	Met Plant Feed Ash %	Met Plant Yield %	Met Plant Feed Ash %	Met Plant Yield %	Met Plant Feed Ash %	Met Plant Yield %
D	-	-	-	-	21.8	78.0
E	-	-	-	-	29.3	59.7
F	20.65	75.5	27.23	64.8	21.7	73.1
G	43.27	50.6	40.48	53.4	42.1	48.3
J	-	-	-	-	30.4	65.2
J+K1	27.09	70.1	32.58	62.7	-	-
K1	-	-	-	-	38.4	53.90
K1+K2	-	-	33.59	59.3	-	-
Wt. Avg	29.7	66.0	33.4	60.7	30.9	63.10

Resources

The resource potential of both structures is currently being assessed. Preliminary estimates indicate a total resource of 27.9 million tonnes of product coal. These resources are derived as follows:

	Grizzly Preliminary Pit "C"	Transfer Preliminary Pit "A"	Combined Pits
Product Met (M tonnes)	5.992	20.766	26.758
Product Thermal (M tonnes)	0.337	0.772	1.109

Conclusions and Recommendations

The results of work to date satisfy the objectives of exploration at Quintette Coal Limited in that establishing more attractive long term mine plan reserve alternatives appears probable in the area explored. To this end, further exploration efforts plus initial geotechnical and environmental concerns is recommended during 1987 in order to expedite the areas development.

1.2 INTRODUCTION

One of Quintette Coal Limited's primary long term geological objectives is to develop new reserve alternatives to those included in current long term mining plans providing both stripping ratio and capital (infrastructure) requirements can be reduced. To this end, the Transfer Area, which is named due to its proximity to the Transfer Point on the Company's overland conveyor system is being explored. The Quintette Coal Limited Development Plan - Revision 2 completed in April, 1986 referenced the Transfer Area as follows:

"Recommendations and Further Improvements

During 1985, exploratory efforts in areas within 3 km of the existing conveyor belt have indicated the possibility of developing substantial reserves at a strip ratio lower than certain portions of the Wolverine deposit. Funds have been budgeted to conduct exploration and drilling during 1986 in this area (Transfer)."

1.3 LOCATION, ACCESS AND PHYSIOGRAPHIC FEATURES

1.3.1 Location

Regional and local maps illustrating Quintette Coal Limited's location are provided as Figure 1.3.1 and Figure 1.3.2. The location of the Transfer Area relative to the properties primary infrastructure is illustrated in Figure 1.3.3. As can be seen from this illustration, the area contains a number of potential reserve areas which have had various levels of exploration completed to date. The focus of recent exploration activity (1985/86) and this report is in three relatively distinct geological structures which are listed in order of resource size as follows:

1. Transfer
2. Grizzly
3. Gething

1.3.2 Access

The 1986 Exploration Programme established 4-wheel drive access routes from existing roads into the Transfer, Grizzly and Gething areas. The location of these routes are schematically illustrated in Figure 1.3.4 and plotted in detail on the respective areas geological maps presented in Section 2.0.

The current road distance from the Preparation Plant and Mine Service Complex to the three target areas are listed as follows:

Transfer Area Current Road Access Distances

From	To	Distance (km)
Transfer	Preparation Plant	21.5
	Mine Service Complex	13.0
Grizzly	Preparation Plant	7.2
Gething	Preparation Plant	18.5
	Mine Service Complex	10.0

Although open pit mine limits are not finalized at present, possible road routes (at approximately 7% grade) from the deposits to the overland conveyor, Preparation Plant and Service Complex are illustrated in Figure 1.3.5 and summarized as follows:

**Transfer Area
Future Road Access Distances**

From	To	Distance (km)
Transfer	Overland Conveyor (Transfer Bldg)	5.6
	Mine Service Complex	9.2
	Preparation Plant	14.7
Grizzly	Overland Conveyor (Transfer Bldg)	1.2
	Mine Service Complex	11.4
	Preparation Plant	10.3
Gething	Overland Conveyor (Transfer Pt)	7.2
	Mine Service Complex	10.8
	Preparation Plant	16.3
Mesa Pit*	Mine Service Complex	6.7
	Preparation Plant	23.1
Wolverine Pit*	Mine Service Complex	6.9
	Preparation Plant	23.3

*Mesa and Wolverine Pits are listed to provide a reference to current travel distances.

1.3.3 Physiography

Both the Transfer and Grizzly Areas are located below tree line in sparsely merchantable stands of Spruce and Pine with Cottonwood and Poplar. The Gething Area is located above tree line in a sub-alpine environment. The range in elevation for each area is as follows:

**Transfer Area
Maximum and Minimum Elevations Above Sea Level**

Area	Maximum Elevation (m)	Minimum Elevation (m)
Transfer	1650	850
Grizzly	1150	850
Gething	1650	1450

The drainage patterns and natural topographic slopes peripheral to each area in which future waste dumps will be considered are illustrated schematically in Figure 1.3.6. A summary of each "Slope Study Area" is listed as follows:

TRANSFER AREA NATURAL TOPOGRAPHIC SLOPE STUDY (PERCENTAGE OF PLAN AREA)				
NATURAL SLOPE (DEGREES)	GETHING (%)	TRANSFER (%)	GRIZZLY (%)	CATEGORY
0 to 10	17.11	31.22	18.72	Gentle
10 to 20	35.62	44.91	43.92	Moderate
20 to 30	34.54	19.42	26.63	Steep
30 to 90	12.73	4.45	10.73	Very Steep
	100	100	100	

More detailed maps of the slope study are provided in Appendix 1.1

1.4 COAL LICENCES

The location of coal licences covering the Transfer Area is illustrated in Figure 1.4.1. As development of the licences progresses, an application for a coal lease will be made to establish tenure required for mine development. A preliminary list of those licences likely to be included in this application are presented as follows:

Licence Number*	Area (ha)	Licence No.	Area (ha)
3618	297	7845	75
3660	297	3339	223
7849	297	3343	297
7848	297	3336	297
7847	297	3335	297
3346	297		
3662	297	TOTAL	3864
3661	149		

* Legal Description of the licences is presented in Appendix 1.2

1.5 EXPLORATION HISTORY

A summary of key exploration activity undertaken in the Transfer Area to the end of the 1986 field season is presented in Table 1.5.1.

1.5.1 Exploration Programmes Prior to 1986

Regional scale or geological mapping (1:5000) aided by aerial photograph interpretation was the only form of geological assessment undertaken in the Transfer Area prior to 1976 when the first three helicopter supported diamond drill holes were completed (QJD 7641, 7642, 7643.). The next phase of work involved the completion of 1 rotary drill hole (QJR8001) in 1980 to test Gates Member coal thickness in the remnant syncline structure referred to as the Hermann Syncline (see attached Figure 1.5.1). This structure had been accessed during the fall of 1980 when Nabors Drilling Limited completed a gas well (B.P. ET AL MURRAY d-83-J-93-I-14) for British Petroleum through the structure in encountering a potentially productive gas bearing horizon well below the coal measures. During 1982, six rotary drill holes (QHR8201-8206) were completed, on the forenoted well site access road, to test coal bearing thickness of both the Hermann Syncline as well as the Hermann North area where a steeply dipping Gates section extends south easterly from the Marmot subpit in the Mesa Mine. Results of this programme led to the completion of 5 rotary drill holes QHR8301-8305 in 1983 plus access road construction and detailed geological mapping at 1:2500 scale, in Hermann North. In 1984, a further 12 rotary holes and trenching were undertaken in the Hermann Syncline plus 6 rotary holes and 3 diamond holes in Hermann North. This season also saw the completion of 6 rotary holes in the Gething Area and the first rotary (6) and diamond (1) holes in the Hermann South area which is now referred to as the Grizzly Area. In 1985 limited mapping and the first 2 diamond drill holes were placed in the Transfer Anticline.

1.5.2 1986 Exploration Programme

The primary objectives of the 1986 exploration programme were:

- (1) To complete detailed geological mapping of all naturally exposed outcrop as well as outcrop exposed by access route and trench construction.

- (2) To complete sufficient diamond and rotary drilling to supplement the above noted mapping such that a preliminary determination of resources could be made within approximate pit limits (unscheduled mine area).

1.5.3 Project Management and Primary Contractors

Project Management

All exploration activity, planning, interpretation and report compilation has been managed by the Long Range section of Quintette Coal's Technical Services Department. Assistance in the field and office during 1985 and 1986 has been provided by the geological staff of Mitsui Mining Overseas Company. Staff involved in the preparation of this report are listed as follows:

Quintette Coal Limited Staff

H. Bartle	Geologist
G. P. Gormley	Chief Mine Geologist, Denison Mines
G. Holmlund	Geological Technician
W. R. Leeder	Manager of Product Services, Denison Mines
L. Pendleton	Geological Technician
P. Roussy	Geological Technician
P. Taylor	Geological Technician
Y. Tainaka	Geologist
K. Vandenameele	Draftsperson
B. Wong	Geological Engineer

Mitsui Mining Overseas Company Limited

I. Kakizaki	Chief Geologist
H. Wada	Geologist

Primary Contractors

Table 1.5.2 lists all contractors involved in the most significant aspects of exploration since the commencement of field activity in 1976.

1.5.4 Standards and Procedures

1.5.4.1 Geophysical Logging

Rotary and diamond drill holes have been logged by down hole geophysical methods since the commencement of drilling in 1976. However, in some instances, the caving of drill holes has either prevented the completion of geophysical logs or required the holes to be logged through the drill stem. The types of geophysical logs completed include the following:

1. Gamma
2. Neutron
3. Density
4. Caliper
5. Deviation

All mining section thickness data points used in the resource calculation from rotary drill holes were taken directly from geophysical logs and corrected for seam dip from local structural interpretation. In the case of diamond drill holes, the geophysical logs were used to confirm missing intervals within the mining sections, and as an overall apparent thickness subsequent to dip corrections made from actual core measurements. Copies of all geophysical logs are available in the administration building of Quintette Coal Limited.

1.5.4.2 Rotary Drilling

The contract rotary drill companies have drilled only vertical holes with both down hole hammer and conventional reverse circulation equipment. Through past experience, it has been found that rotary sampling does not provide representative samples of the coal seams because of contamination inherent in the drilling procedure. In some instances however, where near surface intersections have been made, samples normally taken at one meter intervals have been used to provide an indication of seam oxidation through Free Swelling Index tests.

1.5.4.3 Diamond Drilling

Diamond drilling contractors have mostly drilled vertical holes of H.Q. core size (64 mm diameter) using conventional wireline recovery equipment. Each drill hole was geophysically logged followed by detailed visual core descriptions and complete sampling of all mineable coal sections. Approximately 5 kilograms of coal sample was taken from each metre of mineable section and sent to "off site" laboratories for washability and related analyses as described in the following section.

The graphical presentation of all core holes is provided in correlation charts found in Section 2.0

1.5.4.4 Drill Core Analysis

Drill core samples of the mining sections in which +80% core recovery has been achieved normally provide the primary data points for the assessment of in-place ash content, washability yield predictions, and other physical and chemical tests. Normal procedures involve the segregation of any selected mining section into various sample components associated with in-seam rock partings. These samples are then combined into a single sample representing the actual section to be mined. In some instances, it is necessary to substitute equivalent components from other seams due to poor core recovery. Flow diagrams relating the types of laboratory work undertaken on the Transfer Area drill core are presented on Figures 1.5.2 and 1.5.3. Detailed sampling descriptions and test results from the drill core sampling are presented in Appendix 2.

1.5.4.5 Cartography and Survey Control

At present the topographic map coverage for the Transfer Area has been derived by enlarging the "regional" 1:5000 sheets (with 5 metre contour) to a 1:2500 horizontal scale. The "regional" topographic coverage was completed by Burnet Resource Surveys Ltd. using photography taken on September 6th, 1975 from which cartography was completed May 19, 1976. Primary survey control used in the regional work is referenced as follows:

SURVEY NOTE

The Horizontal and Vertical Co-ordinates were established by Burnett Resource Surveys Ltd. under the supervision of D.C. Zelmer, P. Eng. and H.F.H. Neumann, M.L.S., S.L.S., using MRA3 Tellurometers, Hewitt-Packard Distance Meter and DKM2A Theodolites. Horizontal Co-ordinates are derived from Trig. Station 2494 Lat.55°03'54.000"Long.121°05'43.150" which is within the same trig. network as Quintette E.(2374). Lat. 54°51'30.330" Long.120°52'38.310". Elevations are above Mean Sea Level and derived from Trig. Station 2494, elev.=1357.3m and were established by trig. levelling, vertical angles being read at both ends of each course simultaneously. The field survey was made between 1973 and 1976."

It was acknowledged at the start of the 1986 field season that new 1:2500-2 metre contour mapping and the required additional survey control would be necessary to support detailed mine planning and related development as is the case in Quintette's three operating areas, Mesa, Wolverine and Shikano. Considering the early stage of resource quantification it was decided to use enlarged regional mapping for 1986 and to utilize both access routes and drill sites to provide the majority of control points required to complete the new mapping early in 1987.

The 1986 field survey was completed exclusively by Stables and Associates of Dawson Creek, British Columbia. A series of "geological survey control points" were established prior to field mapping to facilitate the "tie-in" of geological field traverses. All drill holes and trench sites were also surveyed during the program. A listing of survey coordinates and details of the survey traverses and control used for these primary points is provided in Appendix 1.3.

1.5.4.6 Geological Mapping

Prior to 1986, only regional scale geological mapping (1:5000) supported by air photo interpretation was available in the Grizzly, Transfer and Gething Areas. One of the objectives of the 1986 Exploration Programme was to map outcrops in the areas of immediate interest as well as those outcrops created during road and trench construction. This objective was accomplished using a modified plane table system controlled by pre-surveyed reference points. The results of this work are included in the geological maps presented for each area in Section 2.0.

1.6 FUTURE DEVELOPMENT SCHEDULE

Geological Exploration/Development and Related Activity

It is anticipated that two more phases of exploration/development will be required to support the ultimate decision to proceed with mining in the Transfer Area. Primary objectives of the 1987 programmes will be to:

1. Obtain bulk samples from test adits driven in the mineable coal seams to further assess washability and to undertake pilot scale carbonization tests.
2. Undertake in-fill drilling to confirm seam continuity throughout each deposit.
3. Confirm the extent of overburden in the south eastern portion (Murray River Valley) of the Grizzly deposit.

In 1988, a small drilling programme will likely be required to confirm any areas where structural interpretation may be weak within the mine plan area.

Mine Planning and Governmental Approvals

A preliminary assessment of the possible mining areas, production levels, waste dumps and primary haulage route accessing the deposits is underway at the present time the results of which it is hoped will support a "Prospectus for mining". Geotechnical, hydrological and environmental field studies will be implemented this year in concert with the exploration programme. The first detailed mine plan will be developed subsequent to the evaluation of the 1987 geological data and preferred routing and infrastructure selected. These studies would support a "Stage 1" submission to the Government of British Columbia. This mine plan will also confirm any additional geological, geotechnical and environmental requirement necessary to obtain Government approvals, which, when met, will result in the submission of a "Stage 2" report thereafter. A tentative development schedule is depicted in Figure 1.5.4.

Table 1.5.1

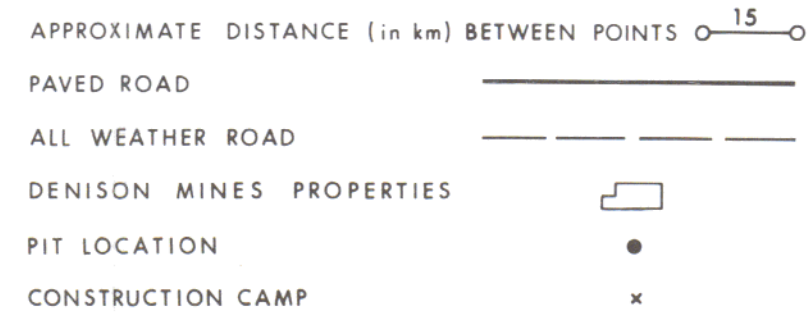
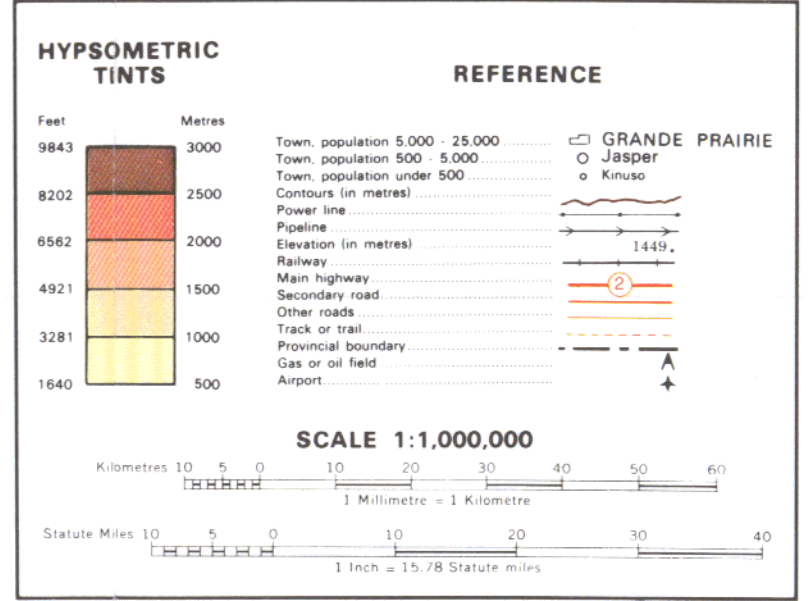
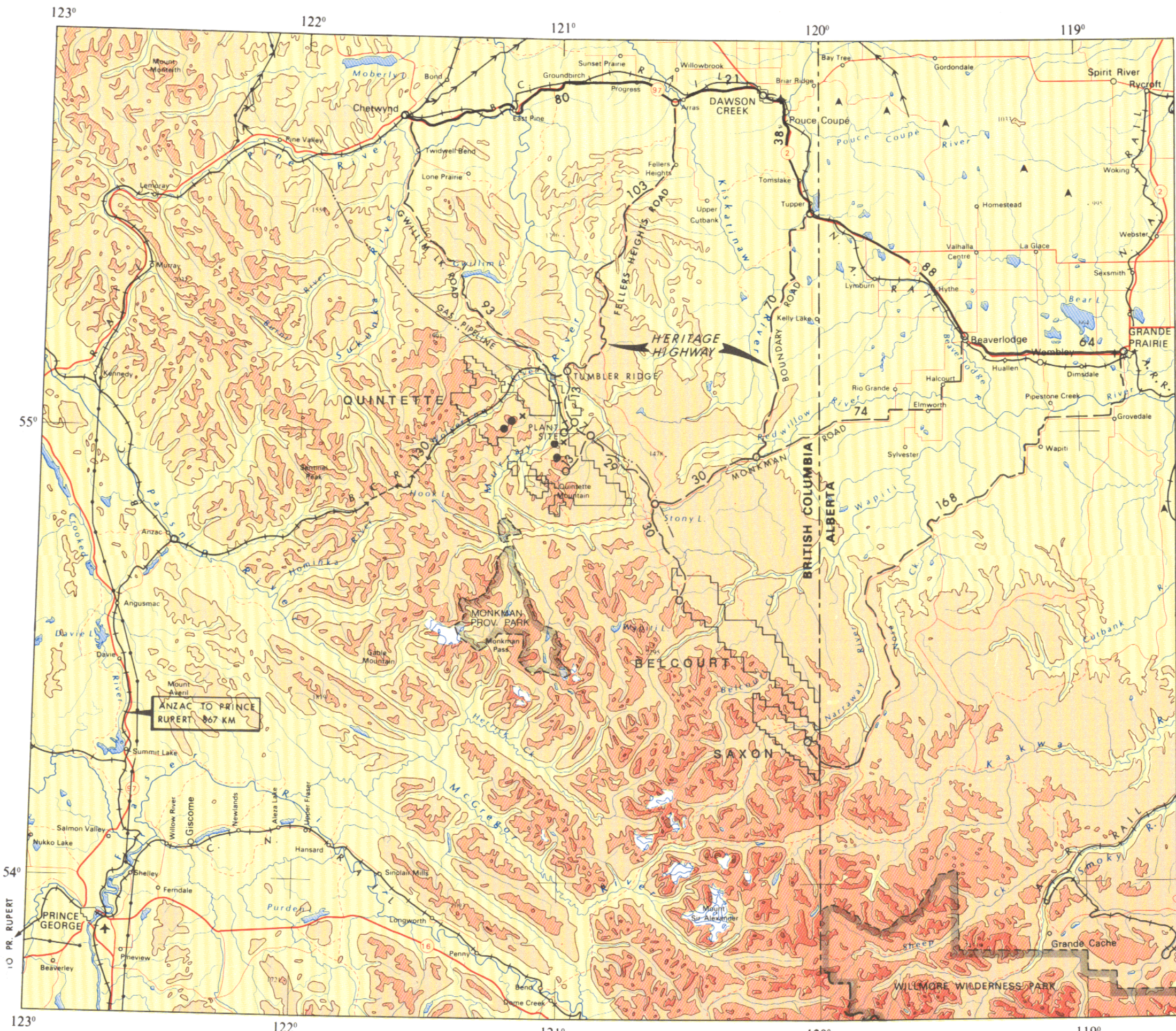
QUINETTE COAL LIMITED
HISTORY OF PRIMARY EXPLORATION ACTIVITY
TRANSFER AREA
1976 - 1986

Location	Year	Rotary Drilling		Diamond Drilling		Road Construction
		Number of Holes Completed	Metres of Drilling	Number of Holes Completed	Metres of Drilling	Kilometres of Access
Hermann Syncline	1980	1	124	----	----	----
	1982	4	259	----	----	----
	1984	12	560	----	----	.5
	TOTAL	17	943	----	----	.5
Gething	1976	----	---	1	183	----
	1984	6	241	----	----	1.8
	1986	(37)	3,360	(1)	81	4.0
	TOTAL	43	3,601	2	264	5.8
Hermann North	1982	2	131	----	----	----
	1983	5	773	----	----	1.3
	1984	6	509	3	573	1.1
	TOTAL	13	1,413	3	573	2.4
Grizzly (Formerly Hermann South)	1983	1	211	----	----	----
	1984	6	686	1	110	1.5
	1986	---	---	(2)	268	1.5
	TOTAL	7	897	3	378	3.0
Transfer	1985	---	---	2	302	----
	1986	---	---	(6)	952	6.1
	TOTAL	---	---	8	1,254	6.1
	GRAND TOTAL	80	6,854	16	2,469	17.8


Table 1.5.2

**QUINETTE COAL LIMITED
PRIMARY EXPLORATION CONTRACTORS
TRANSFER AREA
1976 - 1986**

NATURE OF ACTIVITY	COMPANY	YEAR OF WORK
Road and Drill Site Construction	Lee's Ventures Ltd.	1982
	Quintette Coal Ltd.	1983
	Loiselle Contracting Ltd.	1984,1986
	Murray River Construction Ltd.	1986
Diamond Drilling	Tonto Drilling Ltd.	1976
	Acadia Drilling Ltd.	1984
	Canadian Longyear Ltd.	1985,1986
Rotary Drilling	Bertram Drilling Ltd.	1980
	Northern Wireline Coring and Grouting Ltd.	1982
	S.D.S. Drilling Ltd.	1983,1984,1986
Surveying	D. Watson & Associates	1976
	Quintette Coal Limited	1982,1983
	McElhanney Group Ltd.	1984
	Stables, Tryon and Associates	1986
Geophysical Logging	Roke Oil Enterprises	1976,1980,1982
	Quintette Coal Ltd.	1982,1983,1984
	B.P.B. Instruments Ltd.	1985,1986
Laboratory Analysis	Cyclone Engineering Sales Ltd.	1976,1985,1986
	Quintette Coal Limited	1982,1983
	General Testing Laboratories	1982,1984

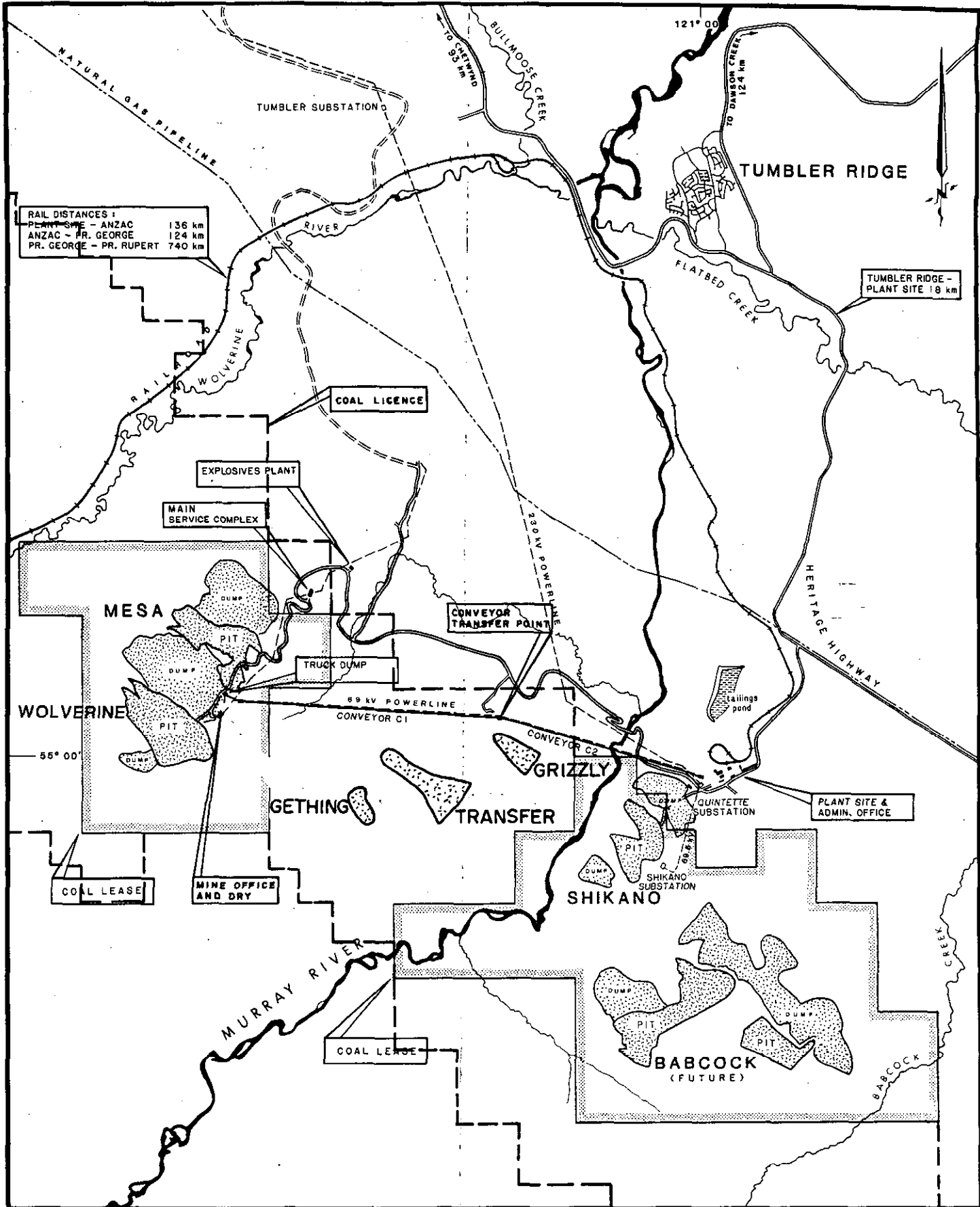


DENISON MINES LIMITED
(COAL DIVISION)
VANCOUVER BRITISH COLUMBIA



NORTHEAST B.C. PROPERTIES

OCTOBER 1982



RAIL DISTANCES:
 PLANT SITE - ANZAC 136 km
 ANZAC - PR. GEORGE 124 km
 PR. GEORGE - PR. RUPERT 740 km

TUMBLER RIDGE -
 PLANT SITE 18 km

COAL LEASE

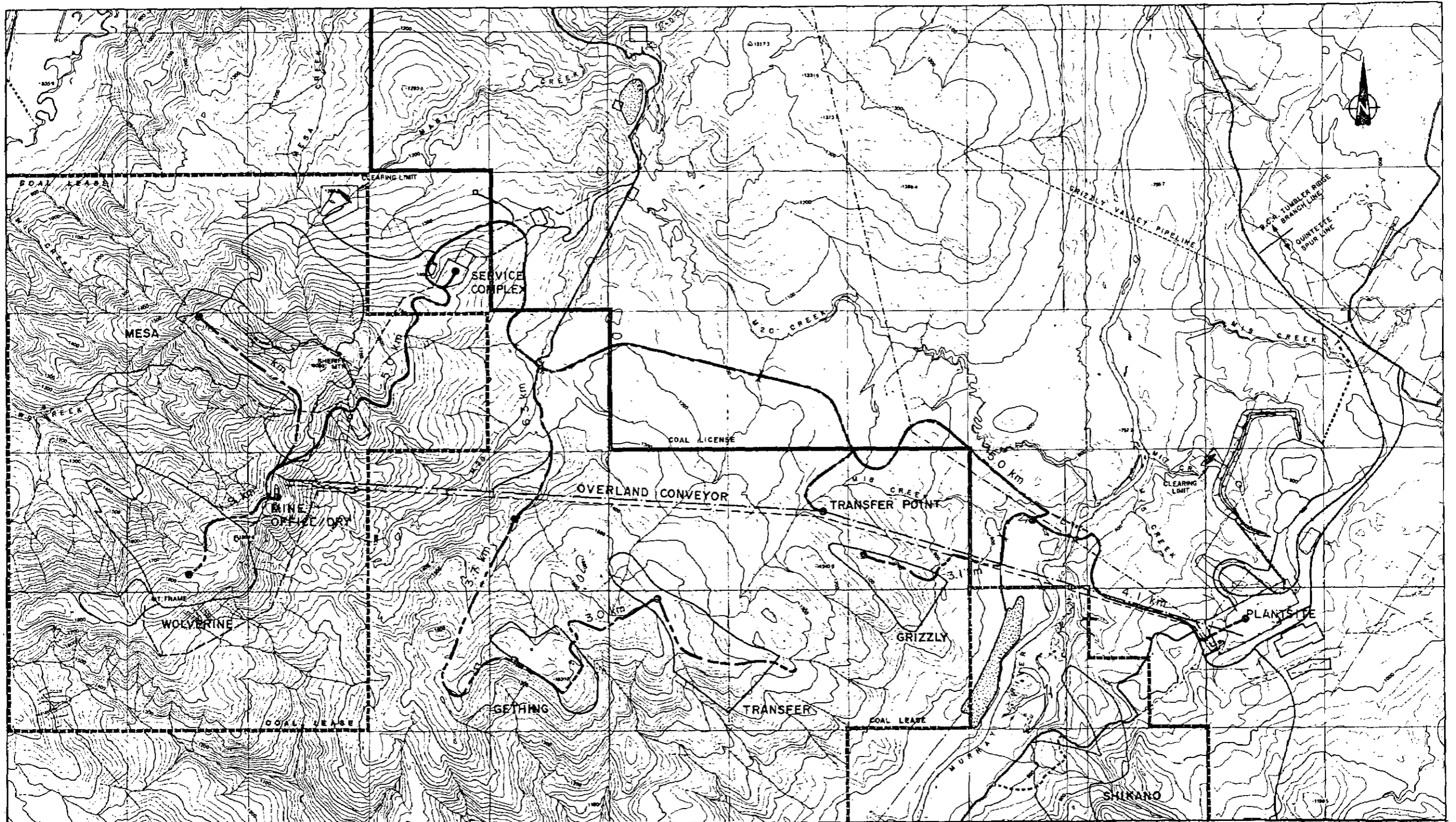
MINE OFFICE
 AND DRY

COAL LEASE

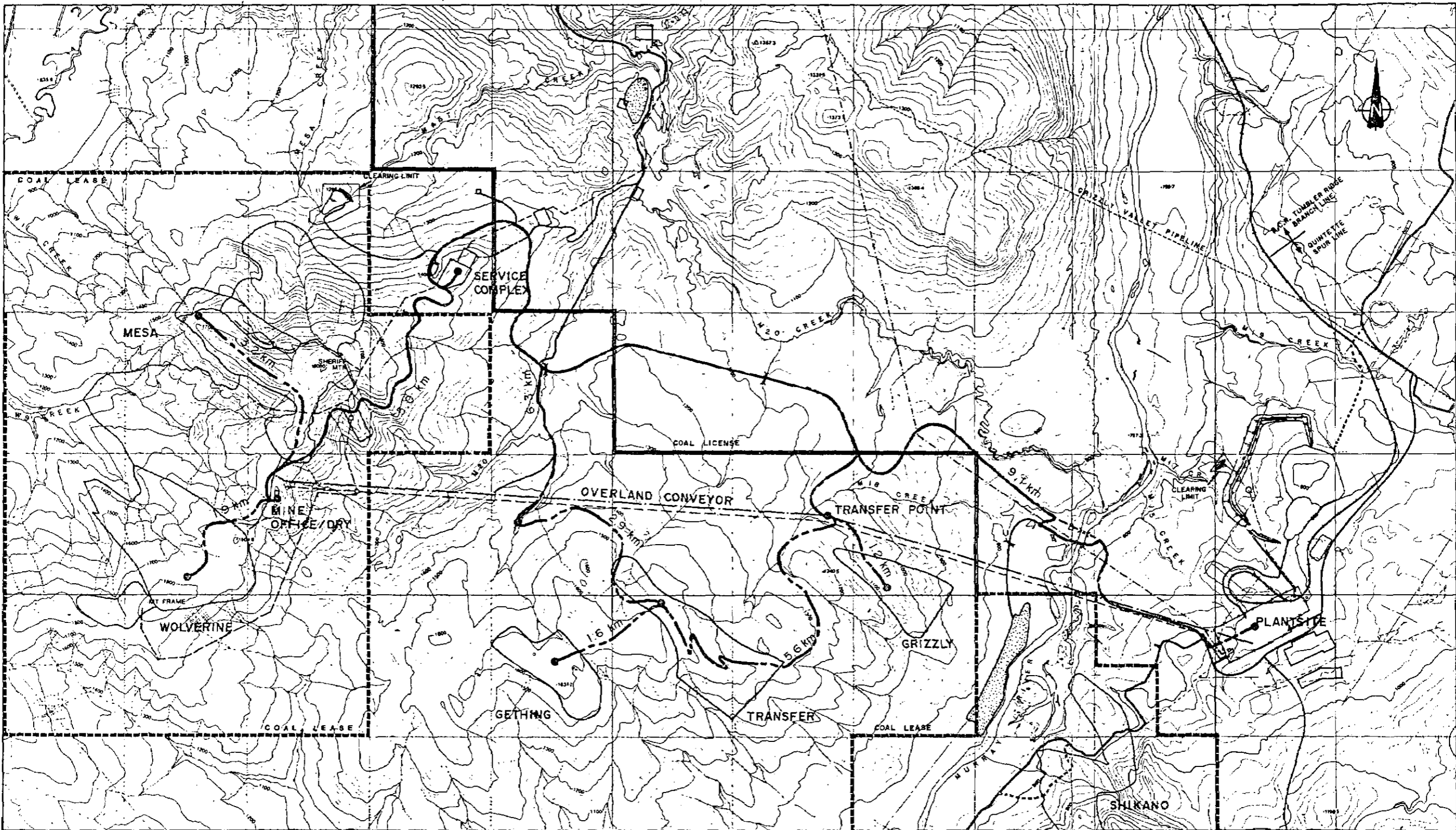
PLANT SITE &
 ADMIN. OFFICE



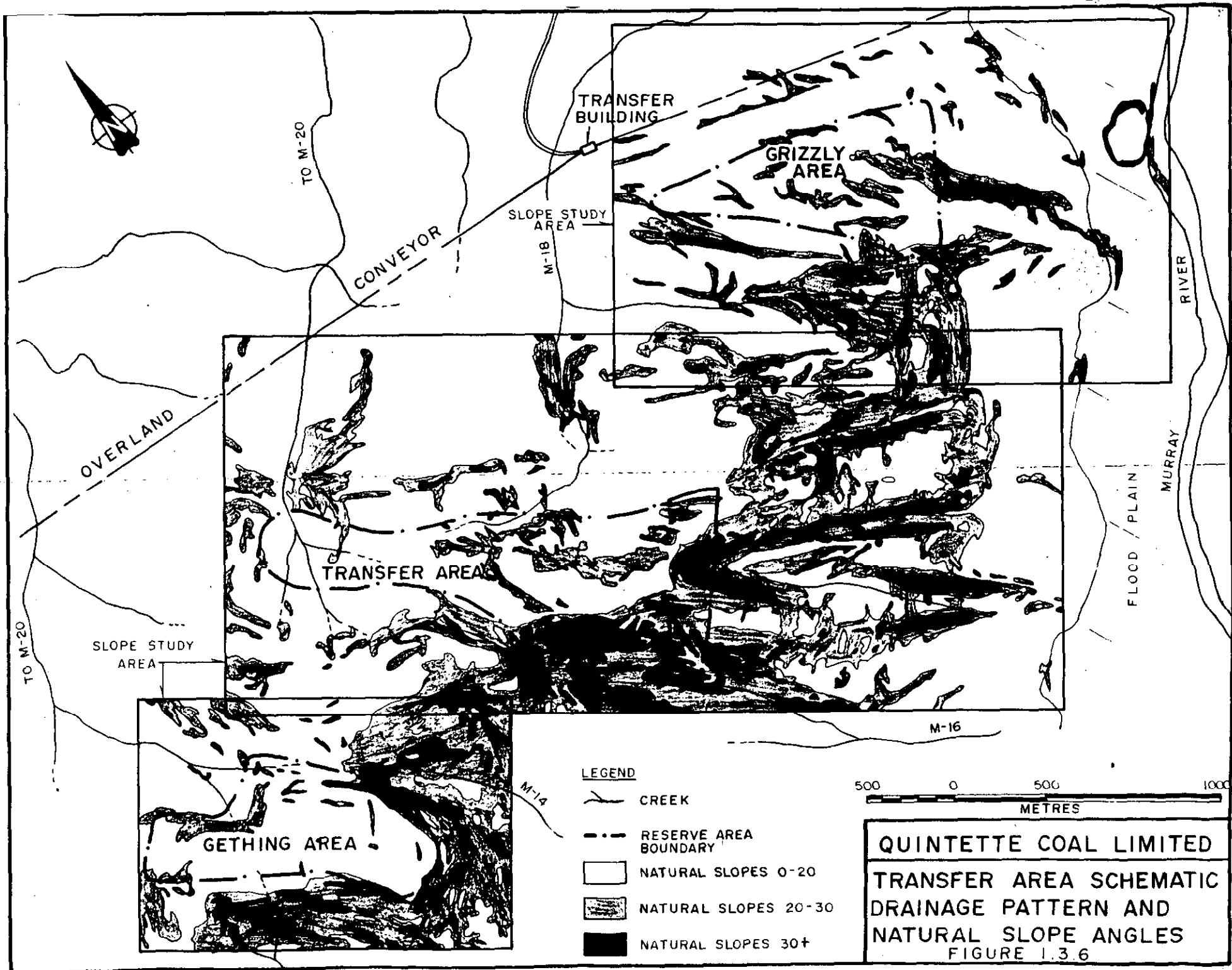
QUINTETTE COAL LIMITED
SITE INFRASTRUCTURE
 FIGURE 1.33



Q 090387	ORIGINAL DRAFT	KJV	GPG	GPG
Rev. D. M. V.	Revision Description	Drn.	Des.	App.
QUINTETTE COAL LIMITED				
Project Manager				
DENISON MINES LIMITED				
COAL DIVISION				
Area		Category		
Drawing Title				
TRANSFER AREA				
CURRENT ROAD ACCESS ROUTES AND DISTANCES				
Scale	Drawing No.	Rev.		
	FIGURE 1.3.4			0



O 090387	ORIGINAL DRAFT	KJV	GPG	GPG
Rev. D M Y	Revision Description	Drn.	Des.	App.
QUINTETTE COAL LIMITED				
Project Manager:				
DENISON MINES LIMITED				
COAL DIVISION				
Area		Category		
Drawing Title				
TRANSFER AREA				
FUTURE ROAD ACCESS ROUTES AND DISTANCES				
Scale	Drawing No.	Rev.		
	FIGURE 1.3.5			0



TRANSFER BUILDING

GRIZZLY AREA

SLOPE STUDY AREA

CONVEYOR

M-18

TO M-20

RIVER

OVERLAND

MURRAY

TRANSFER AREA






SLOPE STUDY AREA

FLOOD / PLAIN

TO M-20

M-16

LEGEND

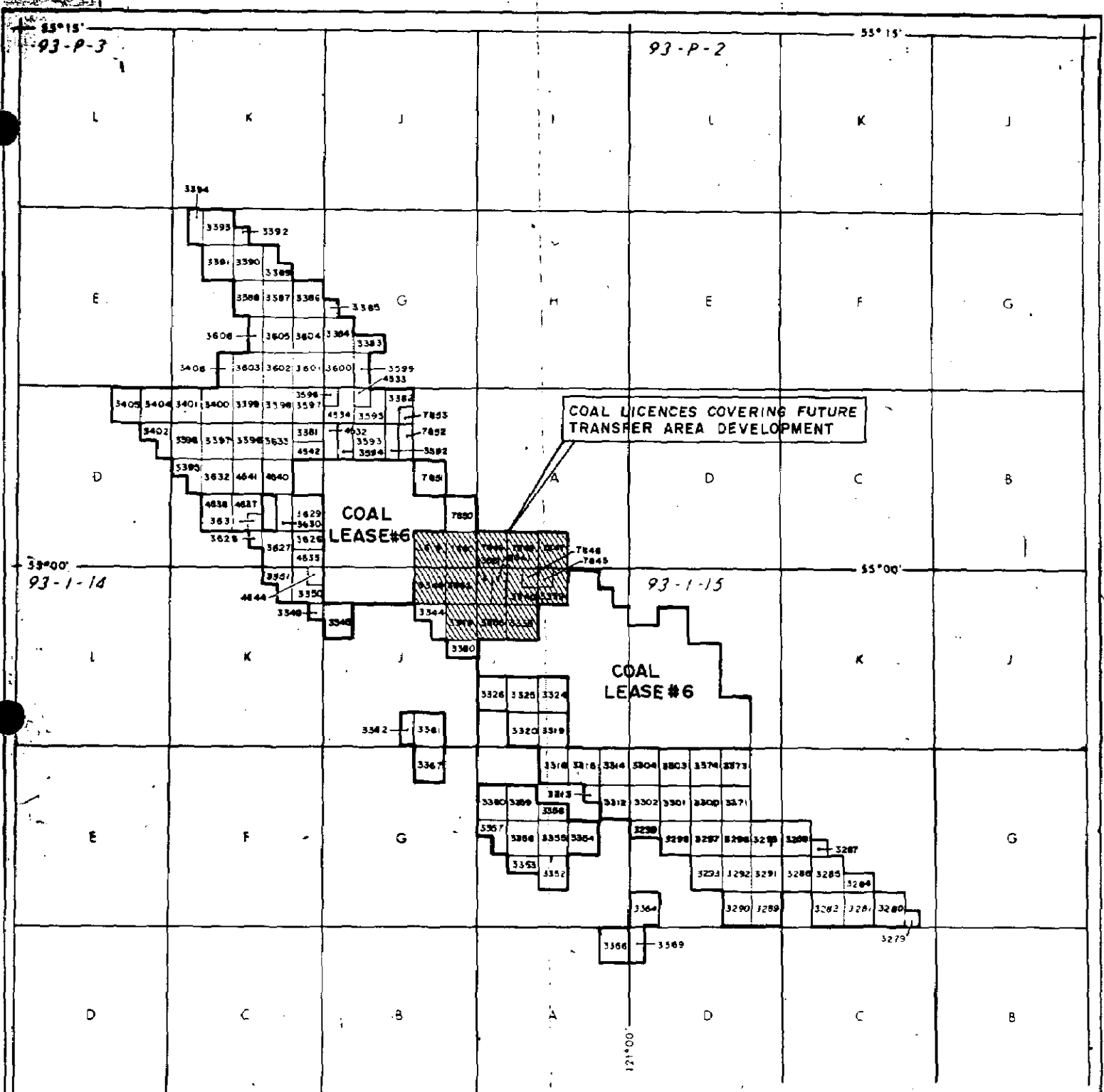
-  CREEK
-  RESERVE AREA BOUNDARY
-  NATURAL SLOPES 0-20
-  NATURAL SLOPES 20-30
-  NATURAL SLOPES 30+



QUINTETTE COAL LIMITED
TRANSFER AREA SCHEMATIC
DRAINAGE PATTERN AND
NATURAL SLOPE ANGLES
FIGURE 1.3.6

GETHING AREA

M-14



DENISON MINES LIMITED
 COAL DIVISION
 VANCOUVER BRITISH COLUMBIA



QUINTETTE
 COAL LICENSES

FIGURE 1.4.1

DRAWN BY: E.T.	DATE: 10/81	SCALE:
DESIGNED BY: E.T.	DATE: 10/81	DRAWING NUMBER:
APPROVED BY: E.T.	DATE: 10/81	QNTT 75-0563-R02

COAL LICENSE

OVERLAND CONVEYOR

M 18 CREEK

TRANSFER POINT

HERMANN NORTH (NABORS)

QHDB4001

QHRB3002 QHRB3003 QHRB3004 QHRB3005 QHRB206 QHD84003 QHRB205

QHRB3001 QHD84002

QHD86003

QHRB4014 QHRB4015

QHD86002

QHD86001

QHD86002

QHRB4016 QHRB4025

QHRB6024 QJD7643

QHD86008

GRIZZLY

QHRB201 QHRB4026 QHRB4005

QHRB4012 QHRB4013 QHRB6036 QHRB6037 QHRB6033 QHRB6034 QHRB6032 QHRB6031 QHRB6029 QHRB6020 QHRB6003

QHRB6023 QHRB6022

QHD86006

QHRB204

QHRB6026 QHRB6025 QHRB6022 QHRB6003

QHRB6021

QHD85001

QHD86007

QHRB4027 QHRB4030 QHRB4029

QHRB4028 QHRB4017 QHD84004 QHRB4018

QHRB4011

QHRB4010

QHRB202

QJD7641

QHRB4006 QHRB4007 QHRB4008 QHRB4009 QHRB4010 QHRB4011 QHRB4012 QHRB4013 QHRB4014 QHRB4015 QHRB4016 QHRB4017 QHRB4018 QHRB4019 QHRB4020 QHRB4021 QHRB4022 QHRB4023 QHRB4024 QHRB4025 QHRB4026 QHRB4027 QHRB4028 QHRB4029 QHRB4030 QHRB6001 QHRB6002 QHRB6003 QHRB6004 QHRB6005 QHRB6006 QHRB6007 QHRB6008 QHRB6009 QHRB6010 QHRB6011 QHRB6012 QHRB6013 QHRB6014 QHRB6015 QHRB6016 QHRB6017 QHRB6018 QHRB6019 QHRB6020 QHRB6021 QHRB6022 QHRB6023 QHRB6024 QHRB6025 QHRB6026 QHRB6027 QHRB6028 QHRB6029 QHRB6030 QHRB6031 QHRB6032 QHRB6033 QHRB6034 QHRB6035 QHRB6036 QHRB6037 QHRB6038 QHRB6039 QHRB6040

GETHING

QHRB4020

QHRB6005

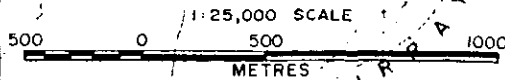
QHD86005

QHD86004

TRANSFER

COAL LEASE

HERMANN SYNCLINE



QUINTETTE COAL LIMITED

TRANSFER AREA
DRILL HOLE LOCATION MAP
1976 - 1986
FIGURE 1.5.1

QUINTETTE COAL LIMITED

1984 DRILL CORE ANALYSIS FLOW DIAGRAM

(+40% Core Recovery)

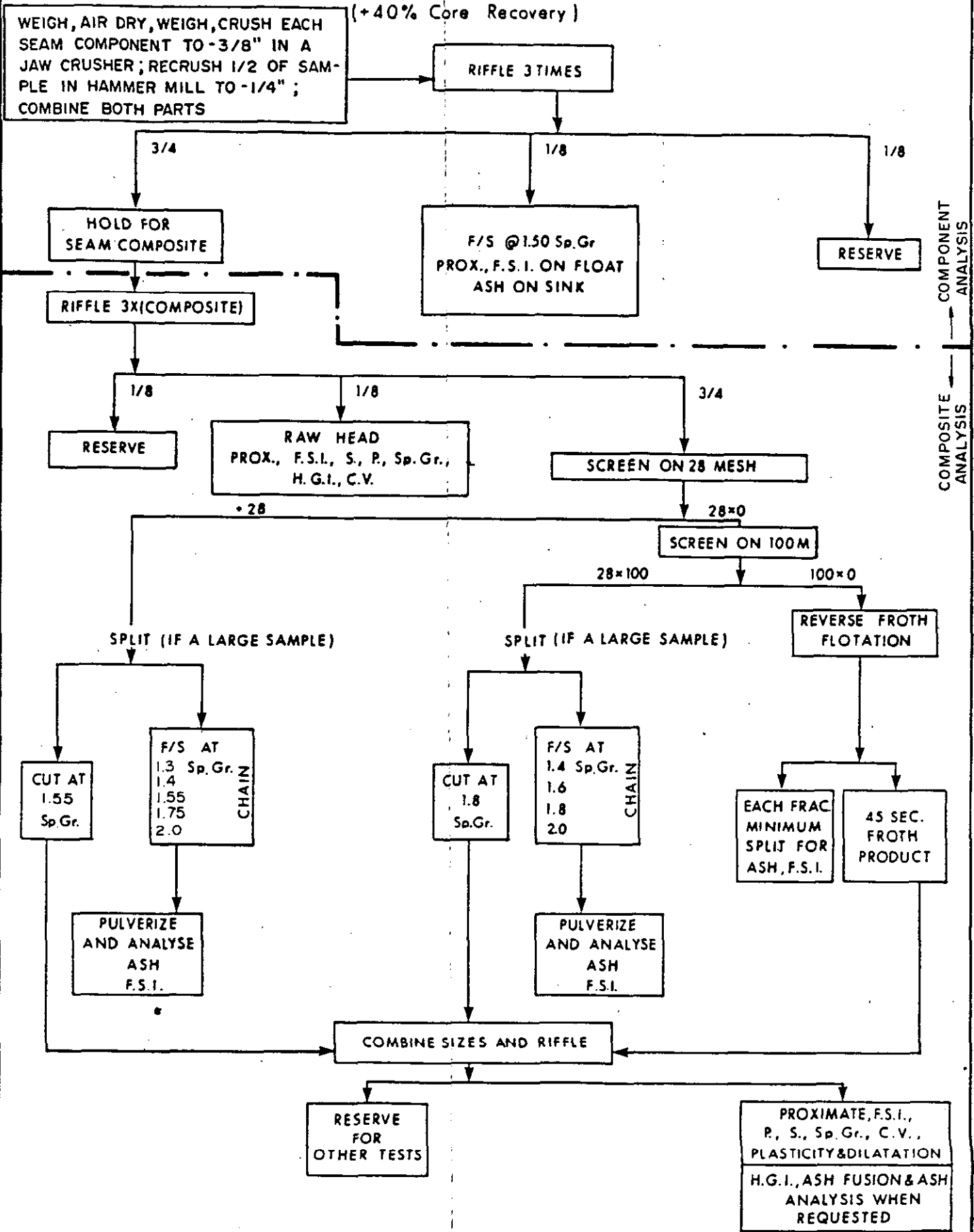


FIGURE I.5.2

QUINTETTE COAL LIMITED

1985/86 DRILL CORE ANALYSIS FLOW DIAGRAM

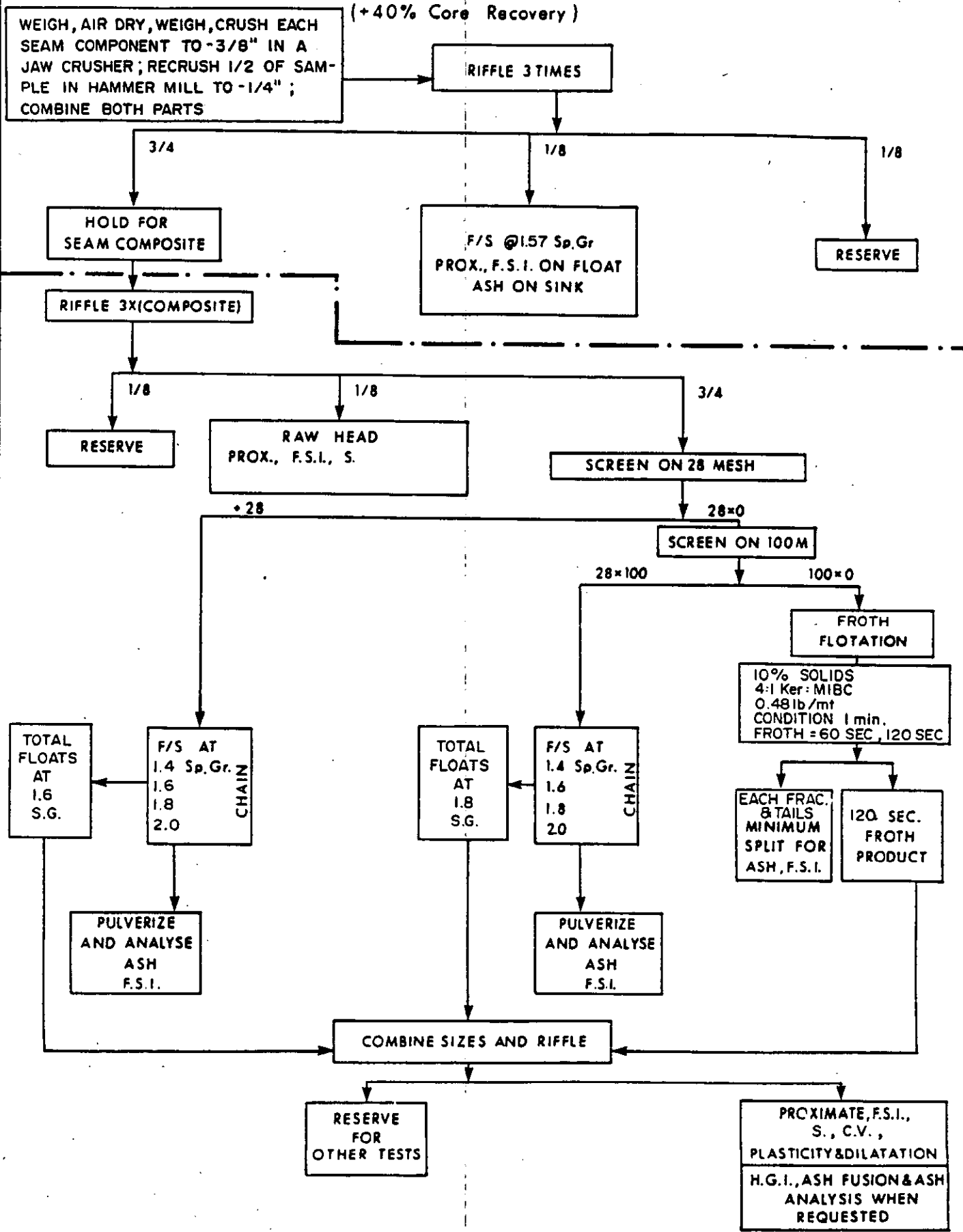


FIGURE 1.5.3

TENTATIVE MINE DEVELOPMENT SCHEDULE OF TRANSFER AREA DEPOSITS

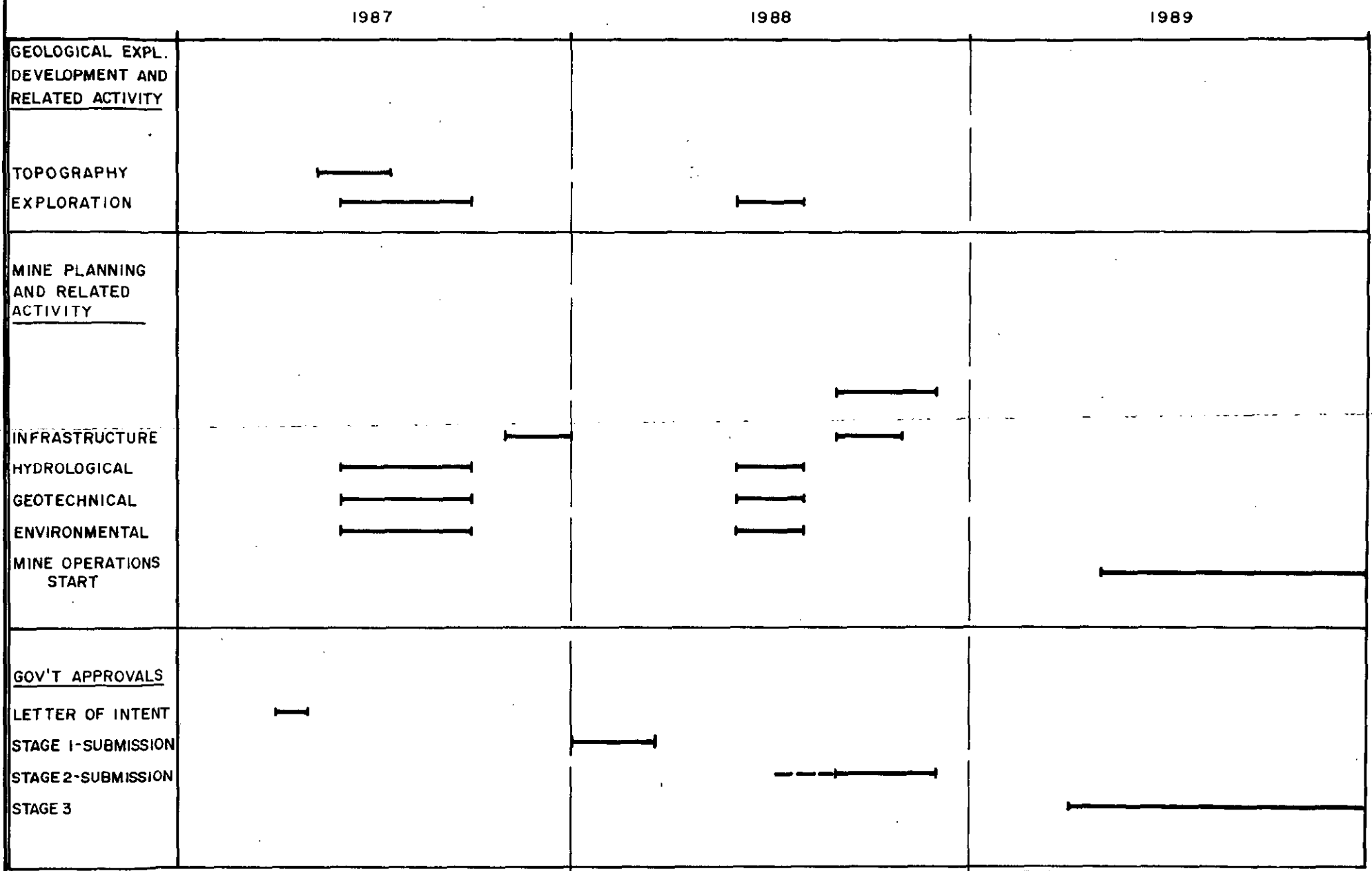


FIGURE I.5.4

2.0 STRATIGRAPHY AND STRUCTURE

2.1 REGIONAL STRATIGRAPHY

The stratigraphic succession exposed on the Quintette property ranges from Upper Jurassic to Lower Cretaceous in age. It consists of inter-tonguing shales and sands of both marine and continental origin. The table of formations for the area is outlined in Figure 2.1 and indicates general formation thickness ranges and coal zones as encountered over 16 years of exploration. The coal seams of economic thickness and quality are found in the Gates and Gething Formations. The regional distribution of these formations is illustrated in Figures 2.2 and 2.3.

2.2 LOCAL STRATIGRAPHY

2.2.1 Transfer Anticline Stratigraphy

The Transfer Area is underlain by the Boulder Creek Formation, the Hulcross Formation, and the economically coal-bearing Gates Formation. The Transfer geology map (Figure 87-903-20-001 Sheets 1 & 2) and correlation charts (Figures 86-903-26-003 & 004) illustrate the distribution of these stratigraphic units and the outcrop of the coal seams.

Boulder Creek Formation

The Boulder Creek Formation, the uppermost unit exposed in the Transfer Area, is distributed in the northeast limb of the Transfer Anticline and in the west corner of the area. This formation consists mainly of massive sandstone and conglomerate with minor shale and thin inferior coal seams, and is known as a ridge forming formation in this region. In the Transfer Area a ridge, formed by the lower part of the Boulder Creek Formation, is dominant and is easily traced both in the field and on the map. The formation thickness is estimated at approximately 130 metres.

Hulcross Formation

The Hulcross Formation is conformably overlain by the Boulder Creek Formation, and is composed mostly of medium to dark grey shale with laminations of siltstone and thin beds of bentonite. Within the top and bottom 5 metres of the formation, siltstone is dominant with interbeds of shale. Along the access road from the Gething to the Transfer Area provides good continuous exposures of the Hulcross Formation. The base of the formation is marked by a thin bed of pebbly conglomerate or coarse sandstone. The formation thickness is about 90 metres.

Gates Formation

The Gates Formation contains the economic coal seams in this area, and is widely distributed in both limbs of the Transfer Anticline. The formation can be divided into three members. These are termed the Upper, Middle and Lower. Though each of the members contains coal, seam thickness of economic interest occur only in the Middle Gates Member. The total thickness of the formation is 260 metres.

(i) Upper Gates Member

The Upper Gates Member is defined from the bottom of the Hulcross Formation to the bottom of the conglomerate just above D seam. The upper half of the member is made up mainly of shale, with sandstone beds and coal zones. In other areas of the property, usually three coal zones designated as A, B, and C seams are found in this upper portion, but these are "uneconomical" because of their thin inconsistent development. In the Transfer Area, as well as other areas, three coal or carbonaceous zones are presented in this portion. Two of them (A and C), however, are poorly developed only to be seen as carbonaceous shale. The thickness of B seam is 0.88 metres with no parting (QHD 85002).

In the lower half of the member, very fine and fine sandstone are predominant with subordinate amounts of shale and siltstone.

At the middle of this portion a tuffaceous horizon is recognized, which is used as a good marker for stratigraphic correlation. The conglomerate at the bottom of the member is stratigraphically equivalent to the so called "caprock" in the Mesa, Wolverine, and Shikano pits. The thickness of the conglomerate is relatively thin compared to other areas and ranges from 2.75 metres in the southwest of the area (QHD 86005) to less than 1 metre (0.95 - 0.15) in the rest of the area. The Upper Gates Member is approximately 75 metres thick.

(ii) Middle Gates Member

The lower limit of the Middle Gates Member is marked by the floor of K2 seam. The member contains six coal seams (D, E, F, G, J and K in descending order), these seams are directly correlated to the coal seams at the Shikano Pit. (See Fig. 2.3). Only the last four coal seams, however, should be termed "mineable" in the Transfer Area, because D and E seams have poorly developed thickness and quality, abruptly changing from hole to hole.

Interseam strata is composed mainly of shale with minor sandstone and siltstone, or of alternating beds of shale and sandstone. In some places, discontinuous channel sandstone are found at different horizons creating variations in interseam thickness (ie; between D and E in QHD 86003, and F and G in QHD 86008). The thickness ranges and general lithologies of the interseam strata are summarized on Table 2.1. The Middle Gates Member ranges in thickness from 98 to 105 metres.

(iii) Lower Gates Member

The boundary between the Lower Gates Member and underlying Moosebar Formation is the bottom of a light or pale greenish massive sandstone, below which finer facies such as shale and siltstone are predominant (Moosebar Formation). The upper part of the Member consists of fine to

medium sandstone with minor shale. The lower part of this member is made up of alternating beds of sandstone, siltstone and shale. One thin coal seam designated as L seam is found in this section. The thickness of the Lower Gates Member is approximately 95 metres.

2.2.2 GRIZZLY STRATIGRAPHY

The stratigraphy underlying the Grizzly Area is identical to that of the Transfer Area. That is, the Boulder Creek, Hulcross, Gates, and Moosebar Formations in descending order. Four coal seams of mining interest, F, G, J and K seams, are found in the Middle Gates Member. Basically, the development of the Middle Gates Member is the same as that of the Transfer Area, with the following being primary differences:

- i) a thick conglomerate and sandstone bed ranging from 21 to 25 metres is present between F and G seams, and the interval between these two seams is thicker than that of the Transfer area.
- ii) the interseam thickness between J and K1 is relatively thin (0.38 - 0.58 metres) for most of the area.
- iii) the interval between K1 and K2 is thick (3.0 - 3.7 metres) compared to that of the Transfer area.

The thickness ranges and general lithologies of the interseam strata are summarized on Table 2.2. The distribution of the various stratigraphic units is also illustrated on the Grizzly Geology Map Fig. 86-905-30-001 and the correlation charts previously noted.

2.2.3 Gething Stratigraphy

The Gething area is underlain by the Gething Formation, which is stratigraphically located about 180 meters below the Middle Gates Member. In this region, it is known that the Gething Formation contains economical coal seams at several horizons, the most prominent being termed in descending order as Bird, Skeeter and Chamberlain. The formation can be divided into two sections designated as the Upper and Lower. The thickness of the formation has not been confirmed in this area, however, judging from a core hole drilled in a nearby area, (QHD86010) it is considered that the Gething Formation is at least 280 meters in thickness. (See Gething Area General Correlation Drawing No. 86-605-26-002).

(i) Upper

The upper Gething is defined from the bottom of a thin glauconitic sandstone at the base of the Moosebar Formation to the bottom of a thin glauconitic sandstone conglomerate bed just above GT1 seam. The upper section is composed mainly of conglomerate and sandstone with shale and coal. At the top of this portion, a coal seam designated as the Bird seam is exposed in the northeast end of the area. Its thickness and the extent of its distribution have not yet been well defined because of structural complexity. The thickness of the Upper Gething is estimated at about 130 meters.

(ii) Lower

The lower Gething is predominantly shale with coal and siltstone, and contains minor sandstone and conglomerate. Two coal seams of mining interest found in this section are designated as GT1 and GT2. It is possible that these seams correlate to Skeeter and Chamberlain seams of the Gething Formation. The thickness of this section is more than 150 meters.

2.2.4 Transfer Coal Seam Development and Correlations

As mentioned in the description on stratigraphy, six coal seams are present in the Middle Gates Member in the Transfer Area, although only four of these (F, G, J and K seams) are currently termed "mineable".

Both D and E seams are split into thin coal portions by partings and designated as "non-mineable" for most of the area. In some drill holes, however, these seams have a mineable thickness of more than 1 metre ie; D seam in QHD86005 and E seam in QHD86003, and further exploration may delineate areas in which D and or E seams are recoverable. Coal seam development and corresponding mining thickness are illustrated on the detailed seam correlation charts (Drawing # 86-903-26-001 & 002). The seam thickness variations are summarized on Table 2.3.

F Seam

F seam is well developed in thickness throughout the Transfer Area with an average of more than 4 metres. The columnar section depicted in Figure 2.5 shows a typical F seam development. The seam is generally divided into three portions designated as F1, Parting and F2 from Upper to Lower. In the vicinity of QHD86003, F1 is not present and the parting F1 forms the top portion of F seam (see correlation chart). In the rest of the area, F1 ranges in thickness from 0.73 to 0.92 with an average of 0.84 metres. The parting between F1 and F2 is composed mainly of high ash coal and carbonaceous shale, with a thickness range from 0.23 to 0.68 metres. F2 comprises the major portion of the seam, and consists mainly of low ash coal with two to four discontinuous thin partings. The thickness of those partings are normally less than 10 centimetres, but the parting developed at the middle of F2 is relatively thick and reaches a thickness of 26 centimeters in QHD85001. F2 ranges in thickness from 2.92 to 4.13 metres. The roof and floor of the seam consist of shale or carbonaceous shale, with coal stringers. The mining section of F seam ranges in thickness from 3.97 to 4.25 with an average of 4.15 metres.

G Seam

G seam is characterized by two major continuous partings, and divided into five portions. As seen in Figure 2.6, the three coal portions are identified as G1, G2 and G3, with the two partings denoted as G2P and G3P, in descending order. G1 ranges in thickness from 0.80 to 0.98 metres with little or no partings. G2P is composed of shale, carbonaceous shale, and inferior coal, with a thickness range from 0.10 to 0.30 metres. G2 ranges in thickness from 0.76 to 1.13 metres and occasionally contains one or two very thin partings in the lower half. G3P is composed of shale and siltstone, but in some places (QHD86001, 86007) this parting consists entirely of siltstone with very thin bands of shale at the top and bottom. The thickness of G3P ranges from 0.33 to 0.46 metres. G3 is characterized by a group of partings near the seam's floor, and ranges in thickness from 0.74 to 1.33 metres. The total collection of the above portions comprises the G seam mining section, and ranges in thickness from 2.94 to 3.76 with an average of 3.45 metres. The roof material is shale, occasionally with a thin carbonaceous layer at the bottom. The floor consists of carbonaceous shale or shale with coal stringers.

J Seam

J seam is well developed in thickness throughout the area with an average of more than 4.5 metres. Figure 2.7 shows a typical J seam section. Though no major parting appears in J seam, many thin inferior coal bands (Fusinite?) usually less than 5 centimetres thick, are found. The roof material is shale or carbonaceous shale, and the floor consists of carbonaceous shale with coal bands. J seam ranges in thickness from 3.92 to 6.04 with an average of 4.61 metres.

K Seam

K seam comprises two separate sub-seams identified as K1 for the Upper and K2 for the lower. A typical K seam section is shown in Figure 2.8.

(i) K1 Seam

K1 seam is characterized by alternating thin beds of coal and carbonaceous shale in the upper portion of the seam. The seam grades to carbonaceous shale in some areas and is therefore excluded from coal mining sections. The thicknesses of K1 Seam range from 0.84 to 1.32 metres.

For most of the Transfer Area, the interval between J and K1 is less than 1 metre, and since the structures dip is more than 30°, mining selectivity constraints will likely dictate its extraction together with J Seam. In this case, the combined mining thicknesses range from 5.63 to 8.23 metres.

(ii) K2 Seam

K2 seam may have one or two discontinuous thin partings, and ranges in thickness from 0.79 to 1.28 with an average of 1.09 metres. The interseam strata between K1 and K2 consist of shale, siltstone, and carbonaceous shale with coal stringers. In the east part of the area, sandstone appears in this section. The thickness of the interseam is normally more than 1 metre and at the east end of the area it reaches 3.5 metres (QHD86007). However, in the vicinity of QHD85001 and 85002, it is less than 1 metre (0.7 - 0.8 metres). Given constraints on mining selectivity mentioned previously, the sequence from J to K2 Seam may form a single mining section in the above area.

The cumulative mineable coal seam thickness (F, G, J, K1 and K2) in the Transfer Area is 14.34 metres.

2.2.5 Grizzly Coal Seam Development and Correlation

The characteristics of each mineable coal seam in the Grizzly Area are very similar to that of the Transfer; therefore only points of significant difference are described here. (Detailed seam correlation charts previously listed, illustrate the seams development).

F Seam

The thickness of F seam is relatively thin compared to the Transfer, ranging from 3.28 to 3.66 with an average of 3.51 metres.

G Seam

In the northeast limb of the Grizzly Structure, the thickness of the lower parting (G3P) thickens to .81 metres.

G seam is overlain directly by a thick conglomerate and sandstone bed.

The overall seam thicknesses ranges from 2.97 to 3.34 with an average of 3.20 metres.

J Seam

J seam ranges in thickness from 4.02 to 4.82 with an average of 4.41 metres.

K1 Seam

The thicknesses of K1 seam range from 0.90 to 1.38 with an average of 1.19 metres.

K1 seam may be mined together with J seam in a single mining section owing to thin interval between J and K1 seams.

K2 Seam

K2 seam is thinner, having a thickness of 0.51 to 0.72 metres.

K2 seam may not be mined in this area because of its poor thickness development and the thick interval between K1 and K2 seams.

The cumulative mineable coal seam thickness (excluding K2) is 12.31 metres in average.

2.2.6 Gething Coal Seam Development and Correlation

The southern part of the Gething Area, which was previously known as the Hermann Gething area is presently designated as Gething Flat. In this area, it had been recognized that two coal seams of mining interest, identified as GT1 and GT2, were present at shallow depth (1976 drill hole QJD7642). In 1986 drilling further confirmed this potential and in addition the above area northwest of Gething Flat was drilled and mapped. (See Gething Geological Map Drawing No. 86-605-30-001 and Cross Sections at the end of this section). The development and extent of these coal seams are not yet fully understood in the recently explored area because of the structural complexity encountered.

The columnar sections of GT1 and GT2, which are taken from diamond holes and a trench, are shown on the detailed seam correlation chart (drawing #86-605-26-001) and coal intersections in rotary holes are seen in the geophysical correlation charts, (provided in Appendix 1). The following is a description of GT1 and GT2 Seams in the Gething Flat Area.

i) GT-1 Seam

GT1 Seam is found just below the conglomerate - sandstone bed which forms a flat table like topography in the Gething Flat Area. GT1 Seam is generally divided into two portions designated as the Upper and Lower. Figure 2.9 illustrates GT1 Seam development in a backhoe trench where bulk sampling was undertaken. The Upper GT1 is characterized by a group of partings in the Lower half, which is composed mainly of shale and carbonaceous shale. The thickness of the parting zone ranges from 0.90 to 1.34 meters in the northwest area, but toward the south it thins to be about 0.2 meters (QHR84020, 84020, 84021, 86009, 86010). Upper GT1 has only a few thin partings and is about 4 meters in thickness. Total thickness of GT1 Seam ranges from 5.06 to 7.53 with an average of 6.44 meters.

ii) GT-2 Seam

The interval between GT1 and GT2 is about 10 meters in the northwest of the area and thins toward the south to 3 meters. GT2 Seam is generally clean coal, although a very thin carbonaceous parting is occasionally present. The seam ranges in thickness from 0.74 to 0.94 meters (Figure 2.10).

2.3 REGIONAL STRUCTURE

The regional geologic structure over the Transfer - Grizzly area is best illustrated in Figures 2.2 & 2.4. As shown in these figures, the area is characterized by northwesterly trending folds and southeasterly dipping thrust faults between the Shikano - Babcock area situated on the opposite side of the Murray River. Three pairs of folds arranged in parallel are found. These are identified as the Shikano Anticline and Syncline, the M-9 Anticline and Syncline, and the Transfer Anticline and Syncline from north to south. The Transfer area is located on the Transfer Anticline and the Grizzly area is located on the Shikano Anticline.

2.4 LOCAL STRUCTURE

2.4.1 Transfer Structure

The dominant structure in the Transfer area is the northwest-southeast trending Transfer Anticline that plunges gently ($0-20^{\circ}$) to the northwest. The coal-bearing Gates Formation is widely distributed on both limbs of the anticline. Dips on the northeast limb of the anticline are 35° to 40° in the west half of the limb, and are getting steeper toward the southeast, with a maximum of 57° at the east end of the area. On the southwest limb, dips are relatively steep and range from 50° to 60° . No major faults have been confirmed in the area, however, minor faults should be expected with more detailed drilling density. The Transfer, Grizzly and Gething Area Structure is illustrated on geological cross sections at the end of this section and structure contour maps provided in Appendix 1

2.4.2 Grizzly Structure

The geologic structure of the Grizzly area is entirely controlled by the Shikano Anticline plunging ($10-30^{\circ}$) to the northwest. This anticline has a broad or box-like top of about 100 meters in width. The strata dip 55° to 65° on the northeast limb of the anticline and about 45° on the southwest limb. No major faults have been found in the area, but one minor fault with a displacement of less than 10 meters is interpreted in the vicinity of the anticline axis. As in the case of the Transfer Area, further minor faults will likely be confirmed with increased drill density.

2.4.3 Gething Structure

i) Gething Flat Area

The Gething Flat Area is a "nappe" or overthrust sheet which was lifted up by a low angle thrust fault (see cross-section 29800). The northeast limit of the area is cut by the above fault. The structure in the area is simple and gentle, with a 10° plunge to the southeast and dips of 8 to 18° (see structure contour of GT1 and GT2). Only one minor fault has been interpreted in this area, resulting in thinned intersections of GT1 in holes QHR 86008 and QHR 84022.

ii) Remaining Area

The structure, peripheral to the flat area, is complicated by folding and faulting. The block below the Gething Flat Area has a highly complicated structure and dips of strata abruptly change from a few degrees to vertical. More than 10 faults have been interpreted in the area, and it would be expected that further exploration would result in even more structural complications.

Table 2.1

SUMMARY OF INTERSEAM STRATA IN THE MIDDLE GATES MEMBER
TRANSFER

<u>Interval</u>	<u>Approximate Thickness Range (m)</u>	<u>General Lithology</u>
D seam to E seam	13 - 27	Mainly shale with minor very fine sand and channel sandstone
E seam to F seam	17 - 23	Southwest limb of Transfer Anticline - dominant sandstone with shale North limb of Transfer - Anticline - shale with minor sandstone and sandy shale
F seam to G seam	17 - 33	Alternating beds of shale and sandstone, channel sandstone
G seam to metres J seam	13 - 21	Shale, sandstones, a 3-4 sandstone zone occurs at 3 meters above J seam
J seam to K seam	0.6 - 1.1	Shale, carbonaceous shale

Table 2.2

SUMMARY OF INTERSEAM STRATA IN THE MIDDLE GATES MEMBER
GRIZZLY

<u>Interval</u>	<u>Approximate Thickness Range (m)</u>	<u>General Lithology</u>
F seam to G seam	28 - 34	Conglomerate and fine sandstone, shale with fine sandstone bed for upper 6 - 9 m
G seam to J seam	14 - 18	Alternating beds of shale, siltstone and fine sandstone
J seam to K1 seam	< 0.5	Carbonaceous shale and siltstone
K1 seam to K2 seam	3 - 4	Shale with very fine to fine sandstone beds

Table 2.3

**SEAM THICKNESS SUMMARY
TRANSFER**

<u>Seam</u>	Thickness (m)		<u>Range</u>	<u>Mathematical Average Thickness (m)</u>
	<u>Minimum</u>	<u>Maximum</u>		
F	3.97	4.25	0.28	4.15
G	2.94	3.76	0.82	3.45
J	3.92	6.04	2.12	4.61
K1	0.84	1.32	0.48	1.04
K2	0.79	1.28	0.49	<u>1.09</u>
			Total	<u><u>14.34</u></u>

Table 2.4

**SEAM THICKNESS SUMMARY
GRIZZLY**

<u>Seam</u>	Thickness (m)		<u>Range</u>	<u>Mathematical Average Thickness (m)</u>
	<u>Minimum</u>	<u>Maximum</u>		
F	3.28	3.66	0.28	3.51
G	2.97	3.34	0.37	3.20
J	4.02	4.82	0.80	4.41
K1	0.90	1.38	0.48	1.19
K2	0.51	0.72	0.21	<u>0.60</u>
			Total	<u><u>14.34</u></u>

Hulcross Formation

The Hulcross Formation is conformably overlain by the Boulder Creek Formation, and is composed mostly of medium to dark grey shale with laminations of siltstone and thin beds of bentonite. Within the top and bottom 5 metres of the formation, siltstone is dominant with interbeds of shale. Along the access road from the Gething to the Transfer Area provides good continuous exposures of the Hulcross Formation. The base of the formation is marked by a thin bed of pebbly conglomerate or coarse sandstone. The formation thickness is about 90 metres.

Gates Formation

The Gates Formation contains the economic coal seams in this area, and is widely distributed in both limbs of the Transfer Anticline. The formation can be divided into three members. These are termed the Upper, Middle and Lower. Though each of the members contains coal, seam thickness of economic interest occur only in the Middle Gates Member. The total thickness of the formation is 260 metres.

(i) Upper Gates Member

The Upper Gates Member is defined from the bottom of the Hulcross Formation to the bottom of the conglomerate just above D seam. The upper half of the member is made up mainly of shale, with sandstone beds and coal zones. In other areas of the property, usually three coal zones designated as A, B, and C seams are found in this upper portion, but these are "uneconomical" because of their thin inconsistent development. In the Transfer Area, as well as other areas, three coal or carbonaceous zones are presented in this portion. Two of them (A and C), however, are poorly developed only to be seen as carbonaceous shale. The thickness of B seam is 0.88 metres with no parting (QHD 85002).

In the lower half of the member, very fine and fine sandstone are predominant with subordinate amounts of shale and siltstone.

At the middle of this portion a tuffaceous horizon is recognized, which is used as a good marker for stratigraphic correlation. The conglomerate at the bottom of the member is stratigraphically equivalent to the so called "caprock" in the Mesa, Wolverine, and Shikano pits. The thickness of the conglomerate is relatively thin compared to other areas and ranges from 2.75 metres in the southwest of the area (QHD 86005) to less than 1 metre (0.95 - 0.15) in the rest of the area. The Upper Gates Member is approximately 75 metres thick.

(ii) Middle Gates Member

The lower limit of the Middle Gates Member is marked by the floor of K2 seam. The member contains six coal seams (D, E, F, G, J and K in descending order), these seams are directly correlated to the coal seams at the Shikano Pit. (See Fig. 2.3). Only the last four coal seams, however, should be termed "mineable" in the Transfer Area, because D and E seams have poorly developed thickness and quality, abruptly changing from hole to hole.

Interseam strata is composed mainly of shale with minor sandstone and siltstone, or of alternating beds of shale and sandstone. In some places, discontinuous channel sandstone are found at different horizons creating variations in interseam thickness (ie; between D and E in QHD 86003, and F and G in QHD 86008). The thickness ranges and general lithologies of the interseam strata are summarized on Table 2.1. The Middle Gates Member ranges in thickness from 98 to 105 metres.

(iii) Lower Gates Member

The boundary between the Lower Gates Member and underlying Moosebar Formation is the bottom of a light or pale greenish massive sandstone, below which finer facies such as shale and siltstone are predominant (Moosebar Formation). The upper part of the Member consists of fine to

medium sandstone with minor shale. The lower part of this member is made up of alternating beds of sandstone, siltstone and shale. One thin coal seam designated as L seam is found in this section. The thickness of the Lower Gates Member is approximately 95 metres.

2.2.2 GRIZZLY STRATIGRAPHY

The stratigraphy underlying the Grizzly Area is identical to that of the Transfer Area. That is, the Boulder Creek, Hulcross, Gates, and Moosebar Formations in descending order. Four coal seams of mining interest, F, G, J and K seams, are found in the Middle Gates Member. Basically, the development of the Middle Gates Member is the same as that of the Transfer Area, with the following being primary differences:

- i) a thick conglomerate and sandstone bed ranging from 21 to 25 metres is present between F and G seams, and the interval between these two seams is thicker than that of the Transfer area.
- ii) the interseam thickness between J and K1 is relatively thin (0.38 - 0.58 metres) for most of the area.
- iii) the interval between K1 and k2 is thick (3.0 - 3.7 metres) compared to that of the Transfer area.

The thickness ranges and general lithologies of the interseam strata are summarized on Table 2.2. The distribution of the various stratigraphic units is also illustrated on the Grizzly Geology Map Fig. 86-905-30-001 and the correlation charts previously noted.

2.2.3 Gething Stratigraphy

The Gething area is underlain by the Gething Formation, which is stratigraphically located about 180 meters below the Middle Gates Member. In this region, it is known that the Gething Formation contains economical coal seams at several horizons, the most prominent being termed in descending order as Bird, Skeeter and Chamberlain. The formation can be divided into two sections designated as the Upper and Lower. The thickness of the formation has not been confirmed in this area, however, judging from a core hole drilled in a nearby area, (QHD86010) it is considered that the Gething Formation is at least 280 meters in thickness. (See Gething Area General Correlation Drawing No. 86-605-26-002).

(i) Upper

The upper Gething is defined from the bottom of a thin glauconitic sandstone at the base of the Moosebar Formation to the bottom of a thin glauconitic sandstone conglomerate bed just above GT1 seam. The upper section is composed mainly of conglomerate and sandstone with shale and coal. At the top of this portion, a coal seam designated as the Bird seam is exposed in the northeast end of the area. Its thickness and the extent of its distribution have not yet been well defined because of structural complexity. The thickness of the Upper Gething is estimated at about 130 meters.

(ii) Lower

The lower Gething is predominantly shale with coal and siltstone, and contains minor sandstone and conglomerate. Two coal seams of mining interest found in this section are designated as GT1 and GT2. It is possible that these seams correlate to Skeeter and Chamberlain seams of the Gething Formation. The thickness of this section is more than 150 meters.

2.2.4 Transfer Coal Seam Development and Correlations

As mentioned in the description on stratigraphy, six coal seams are present in the Middle Gates Member in the Transfer Area, although only four of these (F, G, J and K seams) are currently termed "mineable".

Both D and E seams are split into thin coal portions by partings and designated as "non-mineable" for most of the area. In some drill holes, however, these seams have a mineable thickness of more than 1 metre ie; D seam in QHD86005 and E seam in QHD86003, and further exploration may delineate areas in which D and or E seams are recoverable. Coal seam development and corresponding mining thickness are illustrated on the detailed seam correlation charts (Drawing # 86-903-26-001 & 002). The seam thickness variations are summarized on Table 2.3.

F Seam

F seam is well developed in thickness throughout the Transfer Area with an average of more than 4 metres. The columnar section depicted in Figure 2.5 shows a typical F seam development. The seam is generally divided into three portions designated as F1, Parting and F2 from Upper to Lower. In the vicinity of QHD86003, F1 is not present and the parting F1 forms the top portion of F seam (see correlation chart). In the rest of the area, F1 ranges in thickness from 0.73 to 0.92 with an average of 0.84 metres. The parting between F1 and F2 is composed mainly of high ash coal and carbonaceous shale, with a thickness range from 0.23 to 0.68 metres. F2 comprises the major portion of the seam, and consists mainly of low ash coal with two to four discontinuous thin partings. The thickness of those partings are normally less than 10 centimetres, but the parting developed at the middle of F2 is relatively thick and reaches a thickness of 26 centimeters in QHD85001. F2 ranges in thickness from 2.92 to 4.13 metres. The roof and floor of the seam consist of shale or carbonaceous shale, with coal stringers. The mining section of F seam ranges in thickness from 3.97 to 4.25 with an average of 4.15 metres.

G Seam

G seam is characterized by two major continuous partings, and divided into five portions. As seen in Figure 2.6, the three coal portions are identified as G1, G2 and G3, with the two partings denoted as G2P and G3P, in descending order. G1 ranges in thickness from 0.80 to 0.98 metres with little or no partings. G2P is composed of shale, carbonaceous shale, and inferior coal, with a thickness range from 0.10 to 0.30 metres. G2 ranges in thickness from 0.76 to 1.13 metres and occasionally contains one or two very thin partings in the lower half. G3P is composed of shale and siltstone, but in some places (QHD86001, 86007) this parting consists entirely of siltstone with very thin bands of shale at the top and bottom. The thickness of G3P ranges from 0.33 to 0.46 metres. G3 is characterized by a group of partings near the seam's floor, and ranges in thickness from 0.74 to 1.33 metres. The total collection of the above portions comprises the G seam mining section, and ranges in thickness from 2.94 to 3.76 with an average of 3.45 metres. The roof material is shale, occasionally with a thin carbonaceous layer at the bottom. The floor consists of carbonaceous shale or shale with coal stringers.

J Seam

J seam is well developed in thickness throughout the area with an average of more than 4.5 metres. Figure 2.7 shows a typical J seam section. Though no major parting appears in J seam, many thin inferior coal bands (Fusinite?) usually less than 5 centimetres thick, are found. The roof material is shale or carbonaceous shale, and the floor consists of carbonaceous shale with coal bands. J seam ranges in thickness from 3.92 to 6.04 with an average of 4.61 metres.

K Seam

K seam comprises two separate sub-seams identified as K1 for the Upper and K2 for the lower. A typical K seam section is shown in Figure 2.8.

(i) K1 Seam

K1 seam is characterized by alternating thin beds of coal and carbonaceous shale in the upper portion of the seam. The seam grades to carbonaceous shale in some areas and is therefore excluded from coal mining sections. The thicknesses of K1 Seam range from 0.84 to 1.32 metres.

For most of the Transfer Area, the interval between J and K1 is less than 1 metre, and since the structures dip is more than 30°, mining selectivity constraints will likely dictate its extraction together with J Seam. In this case, the combined mining thicknesses range from 5.63 to 8.23 metres.

(ii) K2 Seam

K2 seam may have one or two discontinuous thin partings, and ranges in thickness from 0.79 to 1.28 with an average of 1.09 metres. The interseam strata between K1 and K2 consist of shale, siltstone, and carbonaceous shale with coal stringers. In the east part of the area, sandstone appears in this section. The thickness of the interseam is normally more than 1 metre and at the east end of the area it reaches 3.5 metres (QHD86007). However, in the vicinity of QHD85001 and 85002, it is less than 1 metre (0.7 - 0.8 metres). Given constraints on mining selectivity mentioned previously, the sequence from J to K2 Seam may form a single mining section in the above area.

The cumulative mineable coal seam thickness (F, G, J, K1 and K2) in the Transfer Area is 14.34 metres.

2.2.5 Grizzly Coal Seam Development and Correlation

The characteristics of each mineable coal seam in the Grizzly Area are very similar to that of the Transfer, therefore only points of significant difference are described here. (Detailed seam correlation charts previously listed, illustrate the seams development).

F Seam

The thickness of F seam is relatively thin compared to the Transfer, ranging from 3.28 to 3.66 with an average of 3.51 metres.

G Seam

In the northeast limb of the Grizzly Structure, the thickness of the lower parting (G3P) thickens to .81 metres.

G seam is overlain directly by a thick conglomerate and sandstone bed.

The overall seam thicknesses ranges from 2.97 to 3.34 with an average of 3.20 metres.

J Seam

J seam ranges in thickness from 4.02 to 4.82 with an average of 4.41 metres.

K1 Seam

The thicknesses of K1 seam range from 0.90 to 1.38 with an average of 1.19 metres.

K1 seam may be mined together with J seam in a single mining section owing to thin interval between J and K1 seams.

K2 Seam

K2 seam is thinner, having a thickness of 0.51 to 0.72 metres.

K2 seam may not be mined in this area because of its poor thickness development and the thick interval between K1 and K2 seams.

The cumulative mineable coal seam thickness (excluding K2) is 12.31 metres in average.

2.2.6 Gething Coal Seam Development and Correlation

The southern part of the Gething Area, which was previously known as the Hermann Gething area is presently designated as Gething Flat. In this area, it had been recognized that two coal seams of mining interest, identified as GT1 and GT2, were present at shallow depth (1976 drill hole QJD7642). In 1986 drilling further confirmed this potential and in addition the above area northwest of Gething Flat was drilled and or mapped. (See Gething Geological Map Drawing No. 86-605-30-001 and Cross Sections at the end of this section). The development and extent of these coal seams are not yet fully understood in the recently explored area because of the structural complexity encountered.

The columnar sections of GT1 and GT2, which are taken from diamond holes and a trench, are shown on the detailed seam correlation chart (drawing #86-605-26-001) and coal intersections in rotary holes are seen in the geophysical correlation charts, (provided in Appendix 1). The following is a description of GT1 and GT2 Seams in the Gething Flat Area.

i) GT-1 Seam

GT1 Seam is found just below the conglomerate - sandstone bed which forms a flat table like topography in the Gething Flat Area. GT1 Seam is generally divided into two portions designated as the Upper and Lower. Figure 2.9 illustrates GT1 Seam development in a backhoe trench where bulk sampling was undertaken. The Upper GT1 is characterized by a group of partings in the Lower half, which is composed mainly of shale and carbonaceous shale. The thickness of the parting zone ranges from 0.90 to 1.34 meters in the northwest area, but toward the south it thins to be about 0.2 meters (QHR84020, 84020, 84021, 86009, 86010). Upper GT1 has only a few thin partings and is about 4 meters in thickness. Total thickness of GT1 Seam ranges from 5.06 to 7.53 with an average of 6.44 meters.

ii) GT-2 Seam

The interval between GT1 and GT2 is about 10 meters in the northwest of the area and thins toward the south to 3 meters. GT2 Seam is generally clean coal, although a very thin carbonaceous parting is occasionally present. The seam ranges in thickness from 0.74 to 0.94 meters (Figure 2.10).

2.3 REGIONAL STRUCTURE

The regional geologic structure over the Transfer - Grizzly area is best illustrated in Figures 2.2 & 2.4. As shown in these figures, the area is characterized by northwesterly trending folds and southeasterly dipping thrust faults between the Shikano - Babcock area situated on the opposite side of the Murray River. Three pairs of folds arranged in parallel are found. These are identified as the Shikano Anticline and Syncline, the M-9 Anticline and Syncline, and the Transfer Anticline and Syncline from north to south. The Transfer area is located on the Transfer Anticline and the Grizzly area is located on the Shikano Anticline.

2.4 LOCAL STRUCTURE

2.4.1 Transfer Structure

The dominant structure in the Transfer area is the northwest-southeast trending Transfer Anticline that plunges gently ($0-20^\circ$) to the northwest. The coal-bearing Gates Formation is widely distributed on both limbs of the anticline. Dips on the northeast limb of the anticline are 35° to 40° in the west half of the limb, and are getting steeper toward the southeast, with a maximum of 57° at the east end of the area. On the southwest limb, dips are relatively steep and range from 50° to 60° . No major faults have been confirmed in the area, however, minor faults should be expected with more detailed drilling density. The Transfer, Grizzly and Gething Area Structure is illustrated on geological cross sections at the end of this section and structure contour maps provided in Appendix 1

2.4.2 Grizzly Structure

The geologic structure of the Grizzly area is entirely controlled by the Shikano Anticline plunging ($10-30^\circ$) to the northwest. This anticline has a broad or box-like top of about 100 meters in width. The strata dip 55° to 65° on the northeast limb of the anticline and about 45° on the southwest limb. No major faults have been found in the area, but one minor fault with a displacement of less than 10 meters is interpreted in the vicinity of the anticline axis. As in the case of the Transfer Area, further minor faults will likely be confirmed with increased drill density.

2.4.3 Gething Structure

i) Gething Flat Area

The Gething Flat Area is a "nappe" or overthrust sheet which was lifted up by a low angle thrust fault (see cross-section 29800). The northeast limit of the area is cut by the above fault. The structure in the area is simple and gentle, with a 10° plunge to the southeast and dips of 8 to 18° (see structure contour of GT1 and GT2). Only one minor fault has been interpreted in this area, resulting in thinned intersections of GT1 in holes QHR 86008 and QHR 84022.

ii) Remaining Area

The structure, peripheral to the flat area, is complicated by folding and faulting. The block below the Gething Flat Area has a highly complicated structure and dips of strata abruptly change from a few degrees to vertical. More than 10 faults have been interpreted in the area, and it would be expected that further exploration would result in even more structural complications.

Table 2.1

SUMMARY OF INTERSEAM STRATA IN THE MIDDLE GATES MEMBER
TRANSFER

<u>Interval</u>	<u>Approximate Thickness Range (m)</u>	<u>General Lithology</u>
D seam to E seam	13 - 27	Mainly shale with minor very fine sand and channel sandstone
E seam to F seam	17 - 23	Southwest limb of Transfer Anticline - dominant sandstone with shale North limb of Transfer Anticline - shale with minor sandstone and sandy shale
F seam to G seam	17 - 33	Alternating beds of shale and sandstone, channel sandstone
G seam to metres J seam	13 - 21	Shale, sandstones, a 3-4 sandstone zone occurs at 3 meters above J seam
J seam to K seam	0.6 - 1.1	Shale, carbonaceous shale

Table 2.2

SUMMARY OF INTERSEAM STRATA IN THE MIDDLE GATES MEMBER
GRIZZLY

<u>Interval</u>	<u>Approximate Thickness Range (m)</u>	<u>General Lithology</u>
F seam to G seam	28 - 34	Conglomerate and fine sandstone, shale with fine sandstone bed for upper 6 - 9 m
G seam to J seam	14 - 18	Alternating beds of shale, siltstone and fine sandstone
J seam to K1 seam	< 0.5	Carbonaceous shale and siltstone
K1 seam to K2 seam	3 - 4	Shale with very fine to fine sandstone beds

Table 2.3

**SEAM THICKNESS SUMMARY
TRANSFER**

<u>Seam</u>	Thickness (m)		<u>Range</u>	<u>Mathematical Average Thickness (m)</u>
	<u>Minimum</u>	<u>Maximum</u>		
F	3.97	4.25	0.28	4.15
G	2.94	3.76	0.82	3.45
J	3.92	6.04	2.12	4.61
K1	0.84	1.32	0.48	1.04
K2	0.79	1.28	0.49	<u>1.09</u>
			Total	<u><u>14.34</u></u>

Table 2.4

**SEAM THICKNESS SUMMARY
GRIZZLY**

<u>Seam</u>	Thickness (m)		<u>Range</u>	<u>Mathematical Average Thickness (m)</u>
	<u>Minimum</u>	<u>Maximum</u>		
F	3.28	3.66	0.28	3.51
G	2.97	3.34	0.37	3.20
J	4.02	4.82	0.80	4.41
K1	0.90	1.38	0.48	1.19
K2	0.51	0.72	0.21	<u>0.60</u>
			Total	<u><u>14.34</u></u>

LOWER CRETACEOUS

FORT ST. JOHN GROUP

SHAFTESBURY
FORMATION
(82+ m)

BOULDER
CREEK
FORMATION
(122 - 140 m)

HULCROSS
FORMATION
(75 - 105m)

GATES FORMATION (262 - 274 m)	UPPER
	MIDDLE
	LOWER

MOOSEBAR
FORMATION
(120 - 215 m)

BULLHEAD GROUP
GETHING
FORMATION
(120 - 200m)

CADOMIN 15-45 m

MINNES
GROUP
(~ 2100m)



Interbedded gray shale and mudstone.

Sandstone, conglomerate and shale with carbonaceous materials.

Marine shale with sideritic concretions and mudstones.

Thin coals

Babcock Member

Coal Zone

Torrens Member

Cyclic alternation of interbedded gray shale and coarse to fine grain sandstone, conglomerate and coal.

Marine shale with sideritic concretions, glauconitic sandstone at base.

Bird

Skeeter - Chamberlain

Middle Coal Zone

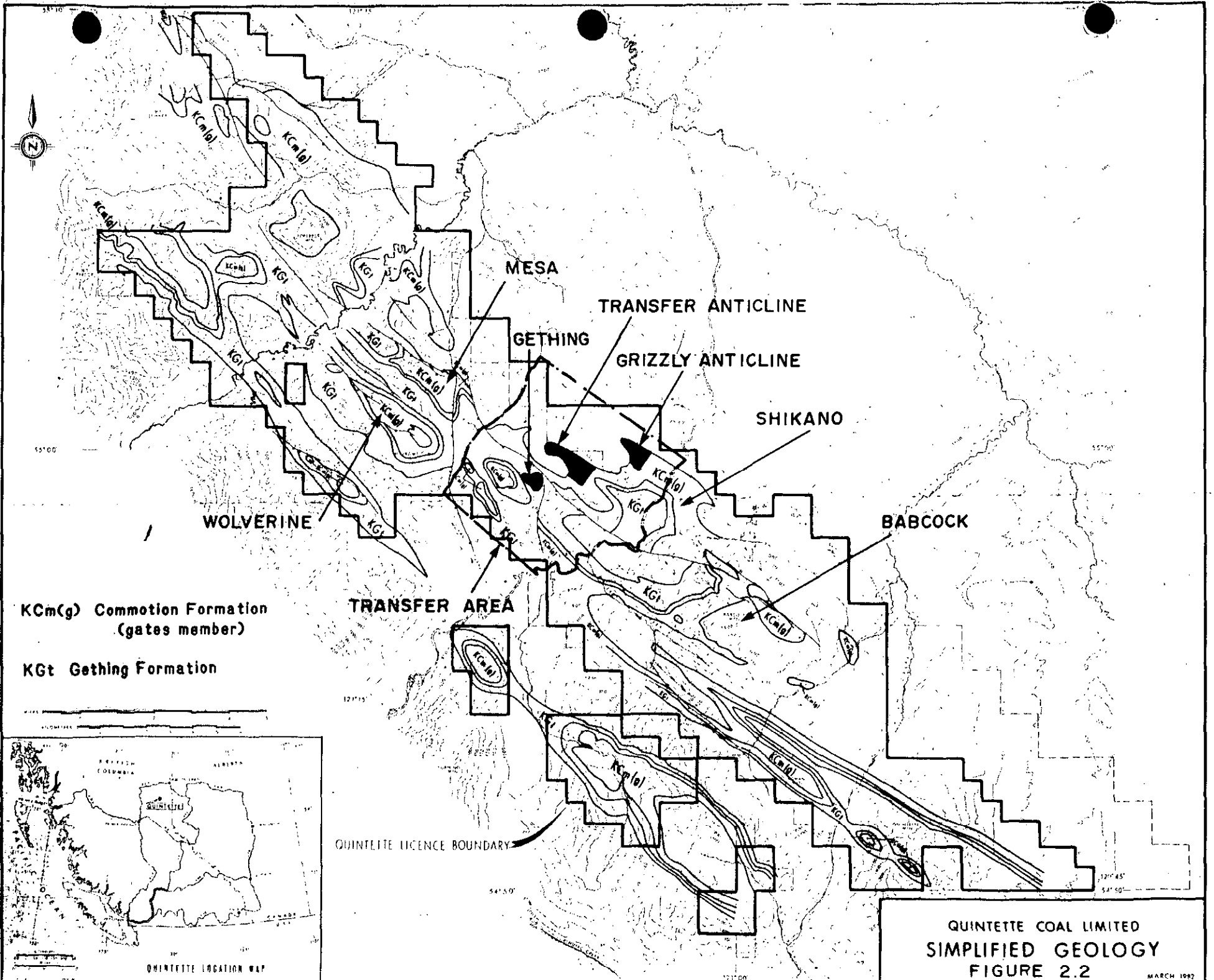
Basal conglomerate.

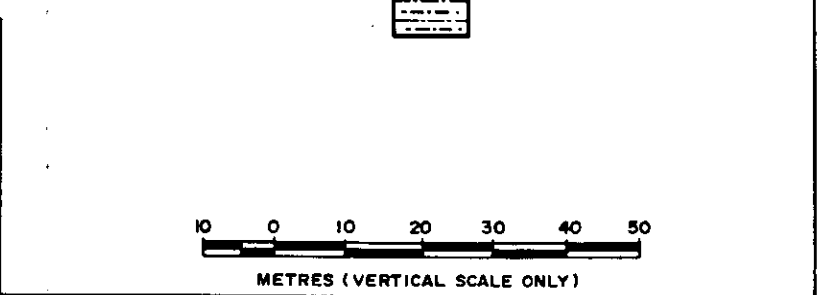
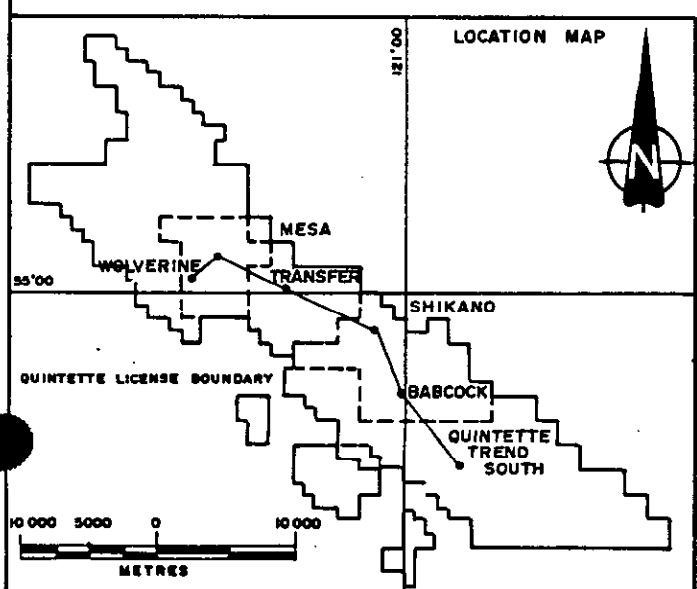
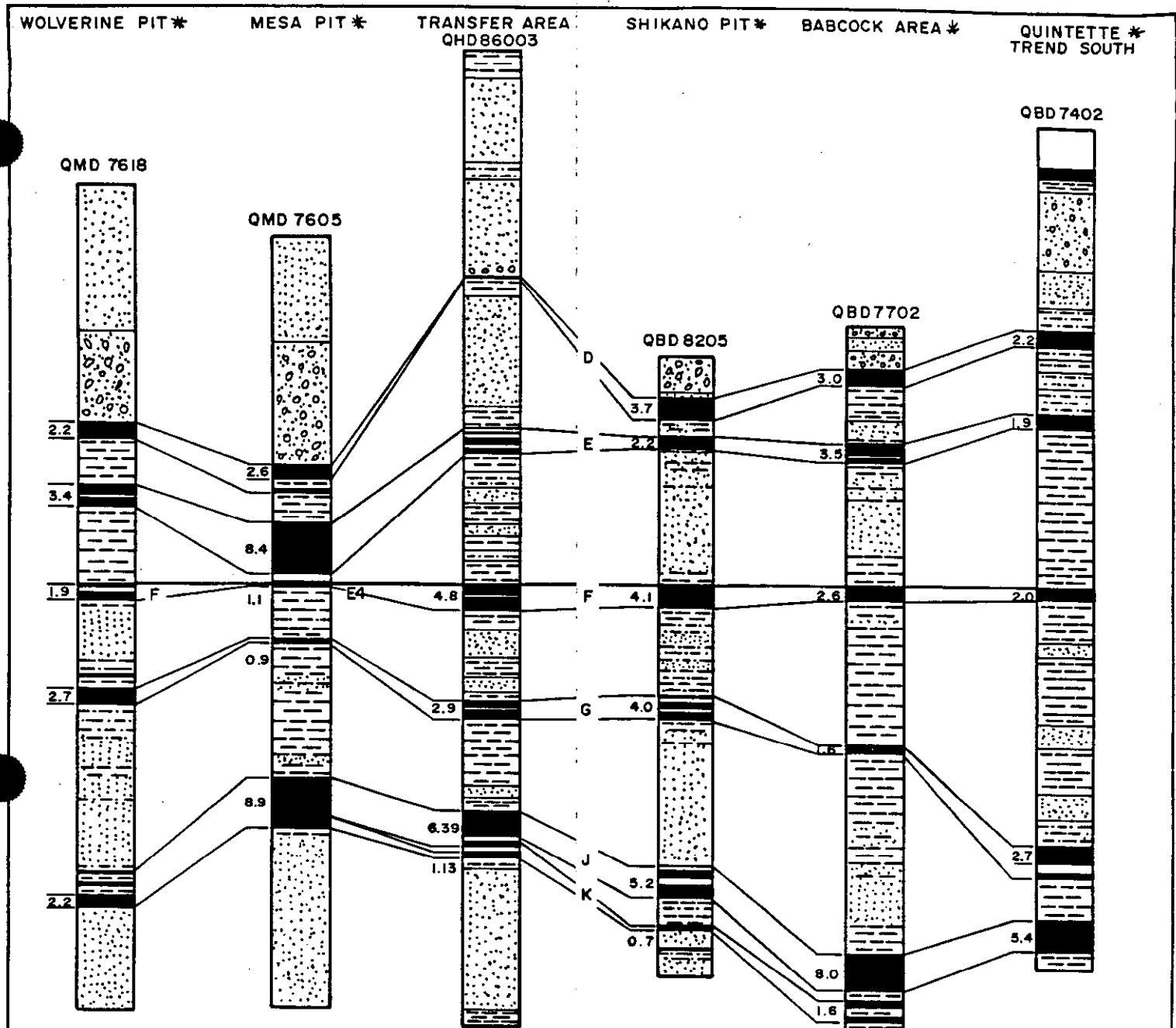
Siltstones, shales, some sandstone and coaly shale.

UPPER
JURASSIC

QUINTETTE COAL LIMITED GENERAL STRATIGRAPHIC SECTION

FIGURE 2.1



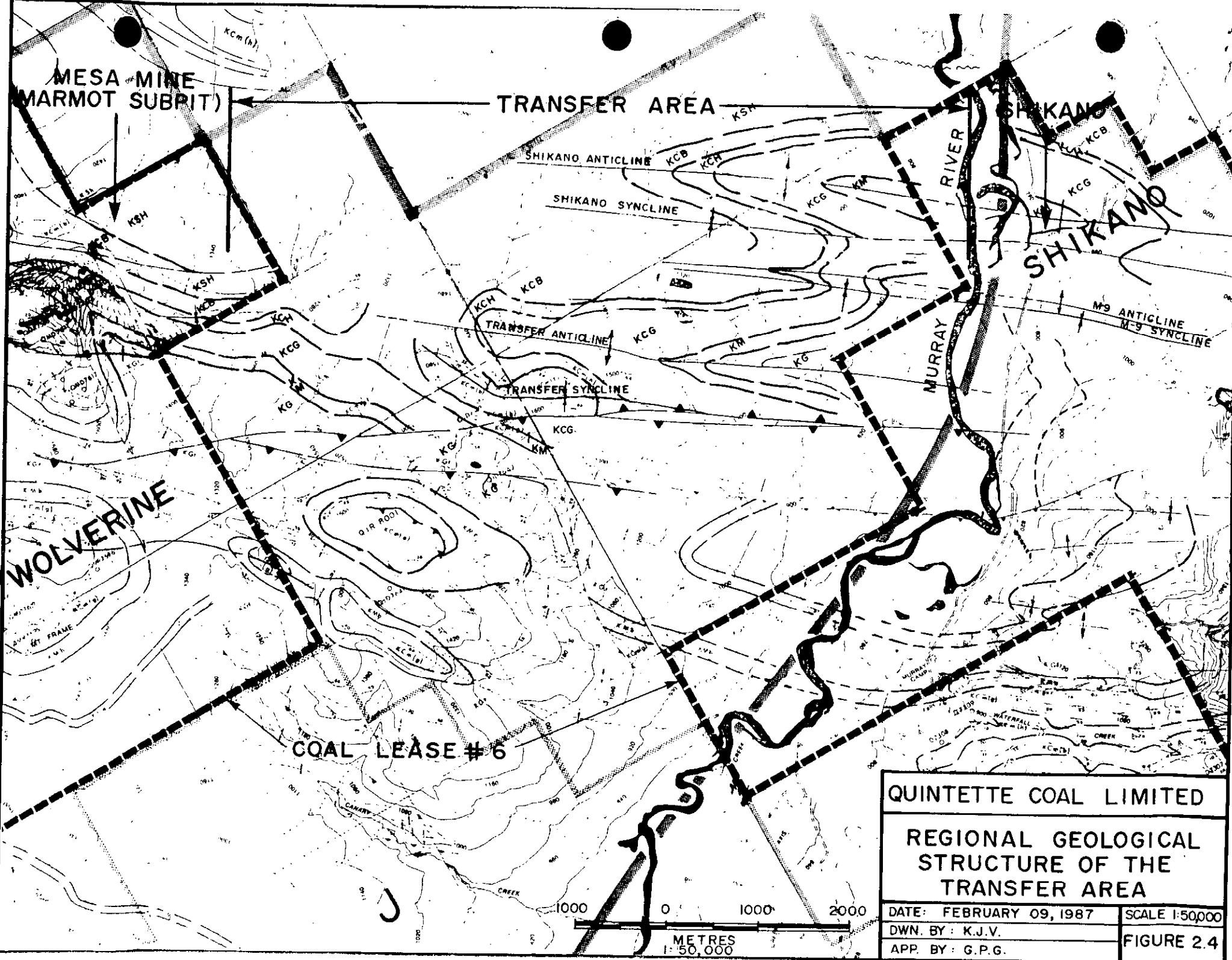


QUINTETTE COAL LIMITED

MIDDLE GATES FORMATION

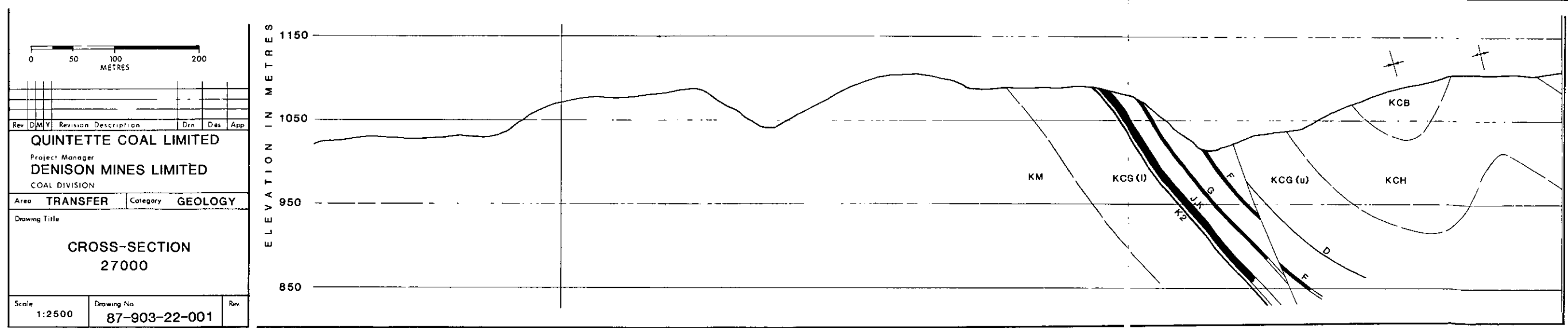
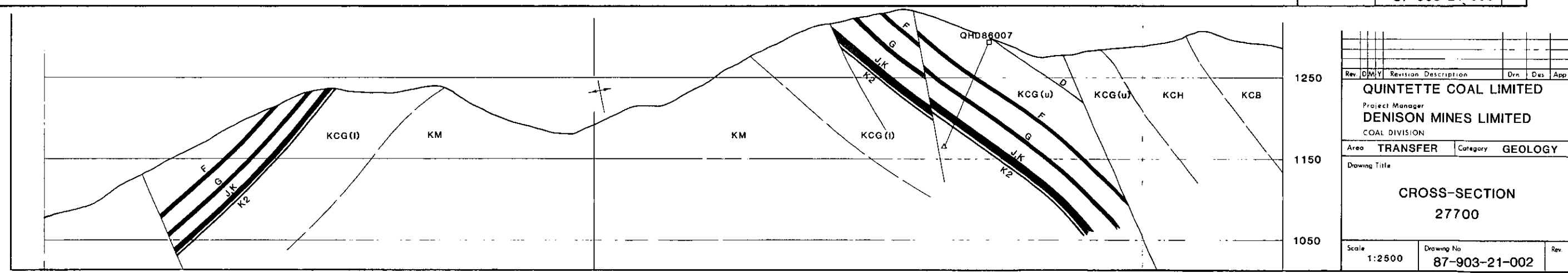
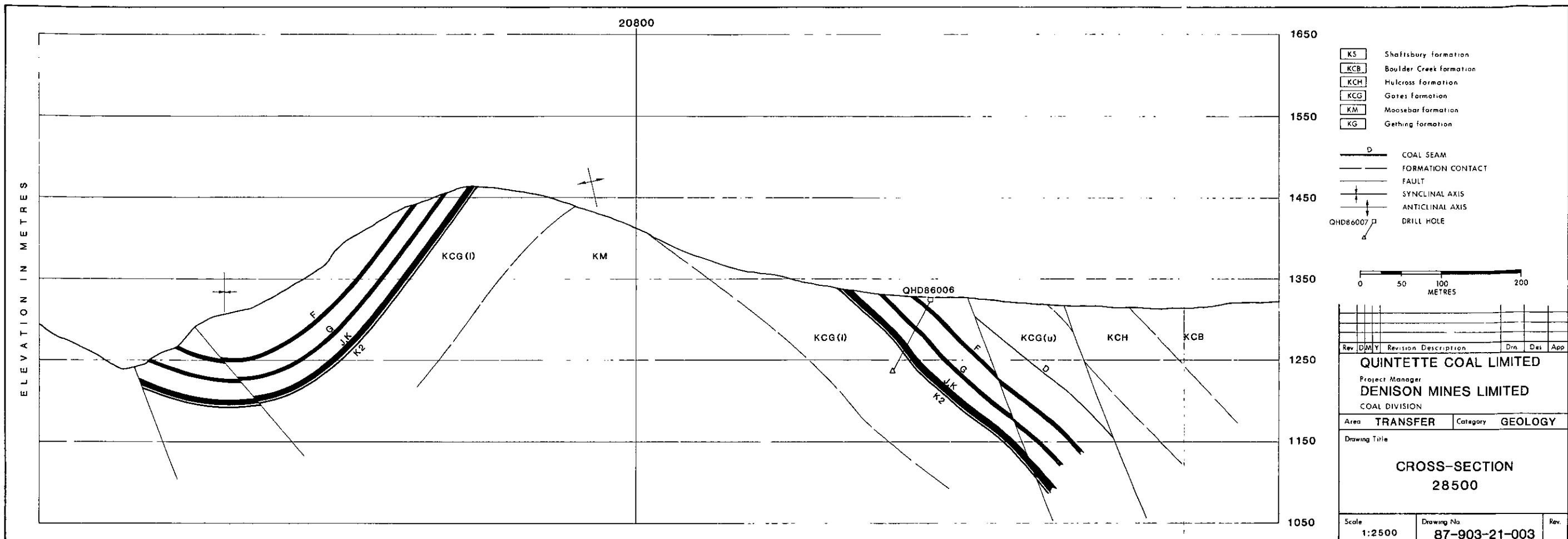
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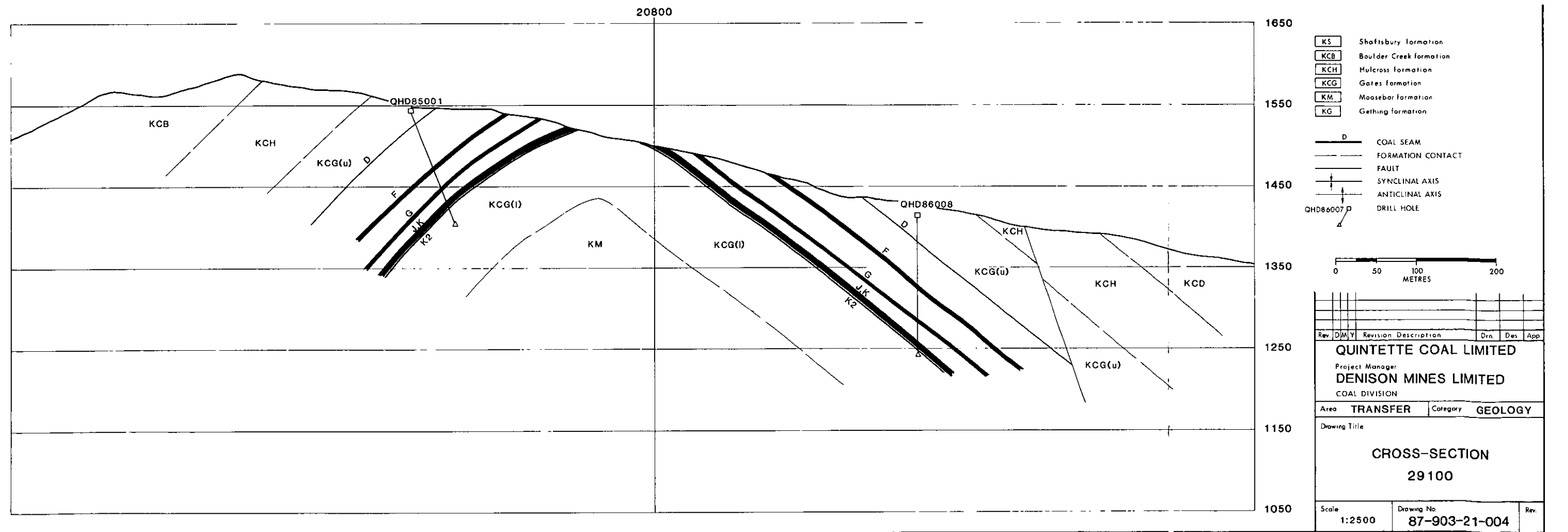
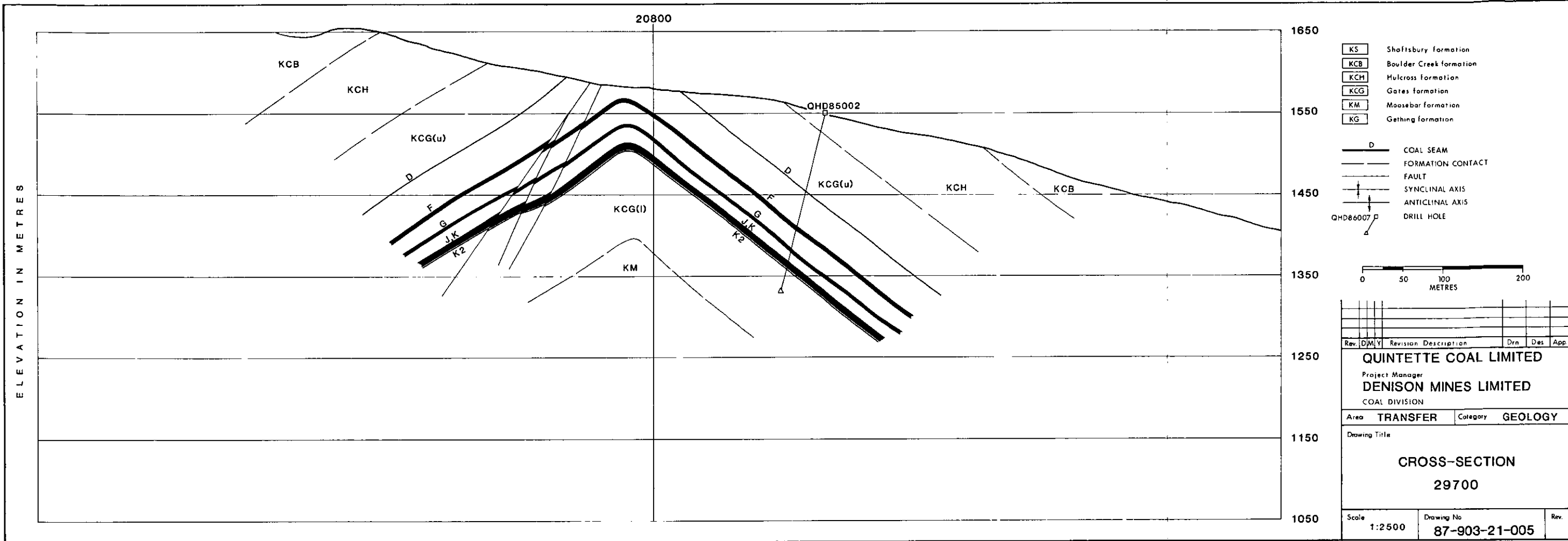
FIGURE 2.3

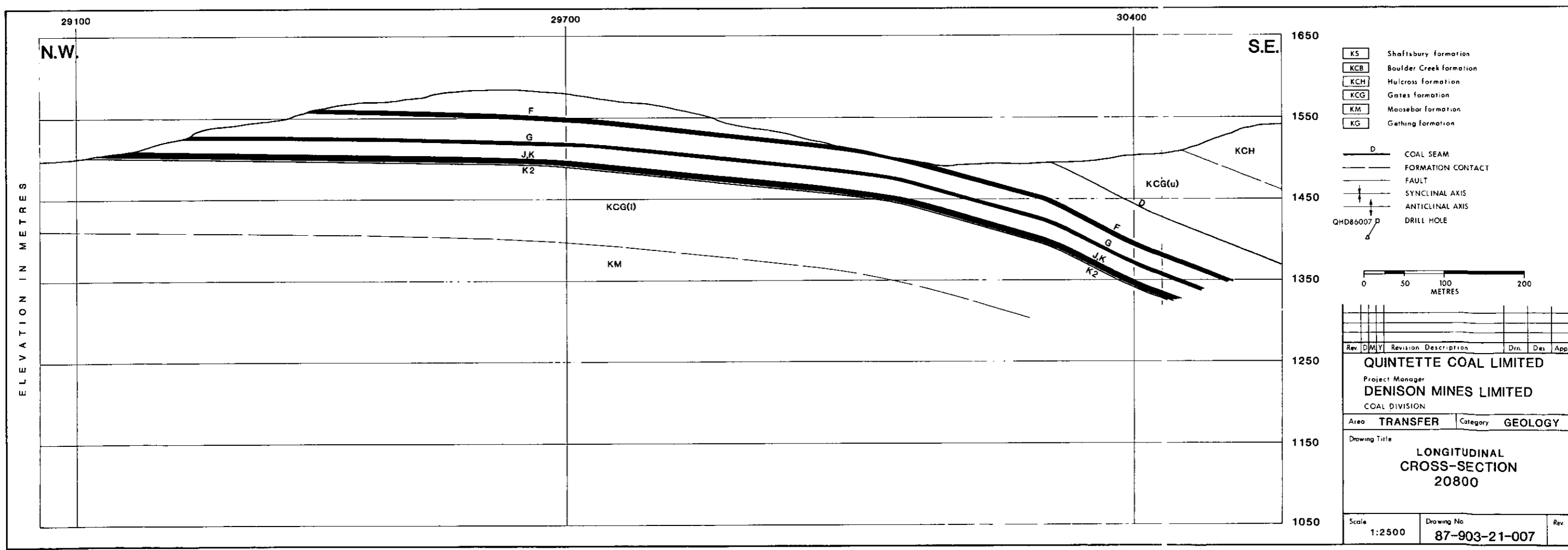
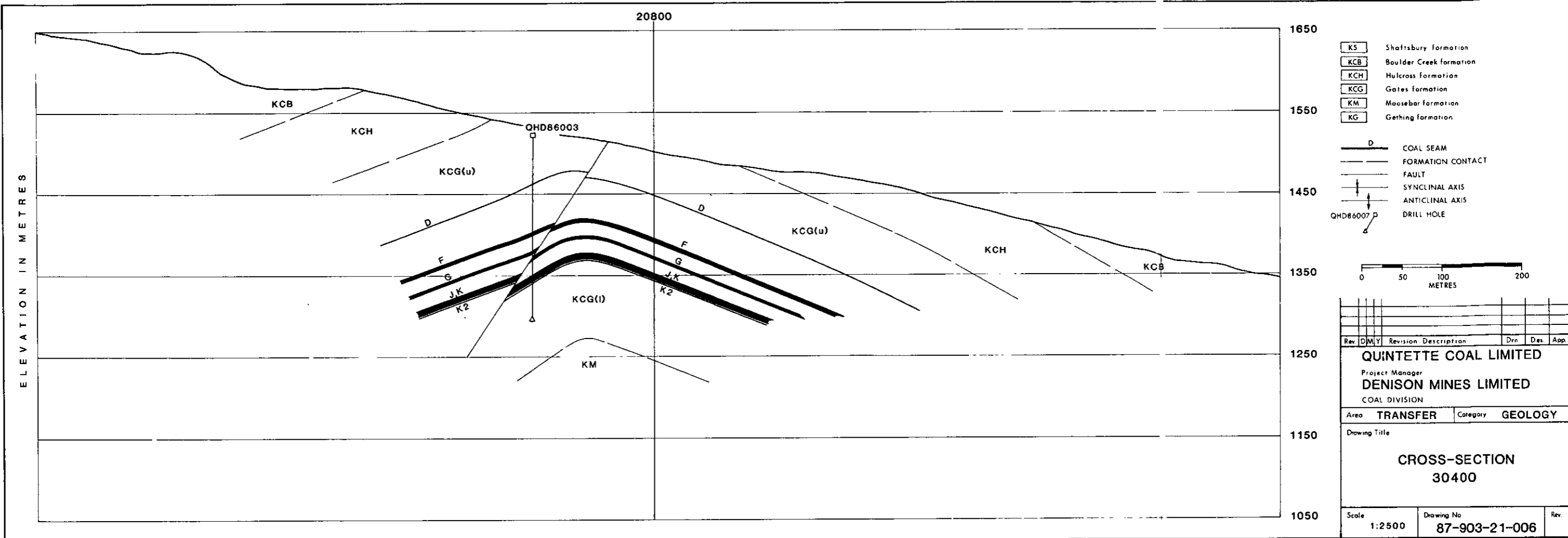


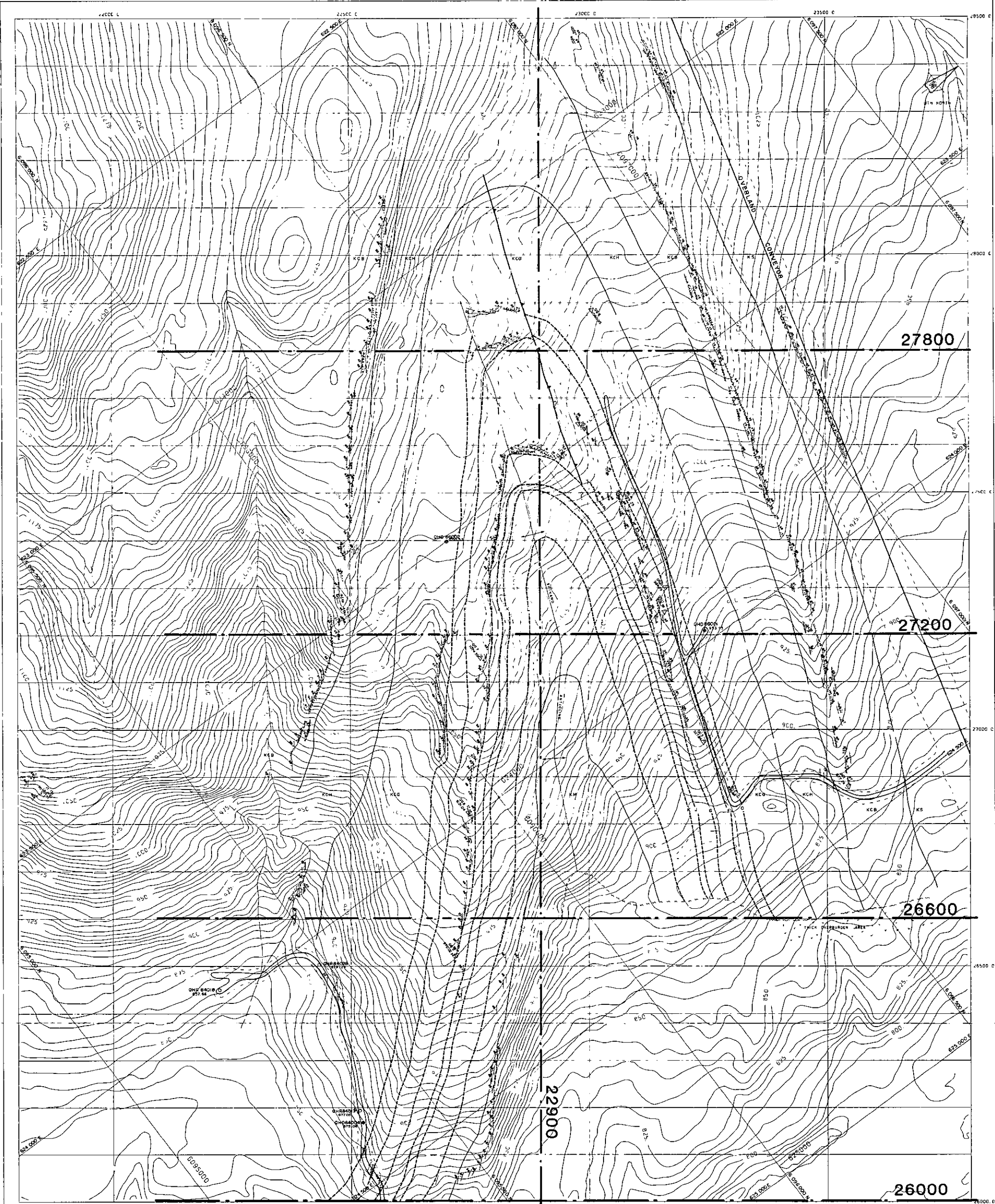
QUINTETTE COAL LIMITED
REGIONAL GEOLOGICAL
STRUCTURE OF THE
TRANSFER AREA
 DATE: FEBRUARY 09, 1987 SCALE 1:50,000
 DWN. BY: K.J.V.
 APP. BY: G.P.G. **FIGURE 2.4**











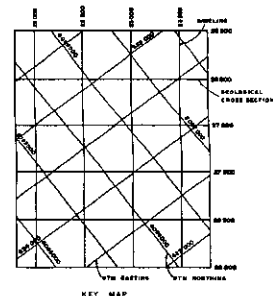
GEOLOGIC FORMATIONS

- KS** SHAFTSBURY
- KCB** BOULDER CREEK
- KCH** MULCROSS
- KCG** GATES
- KM** MOOSEBAR
- KQ** GETMING
- KCD** CADOMIN

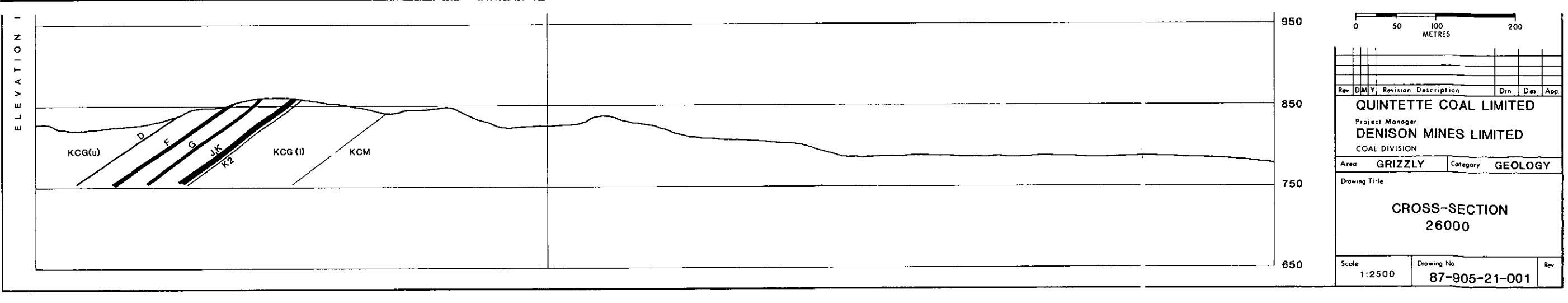
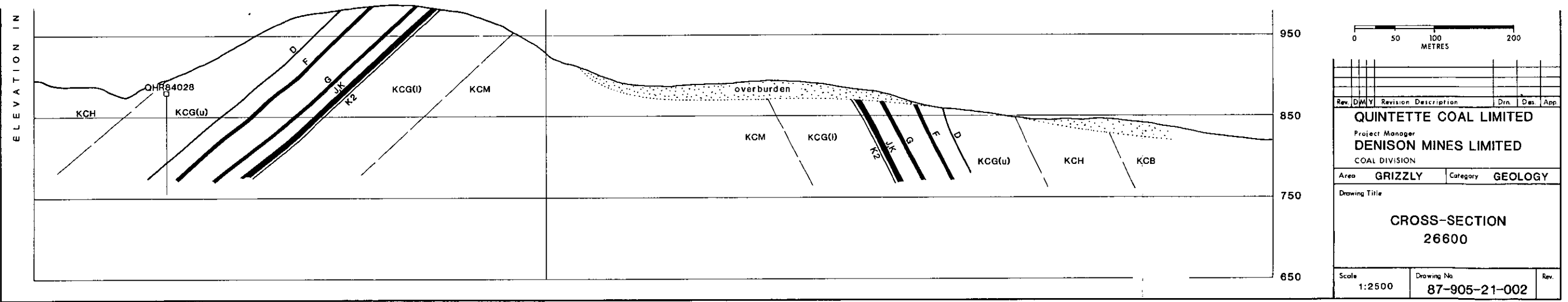
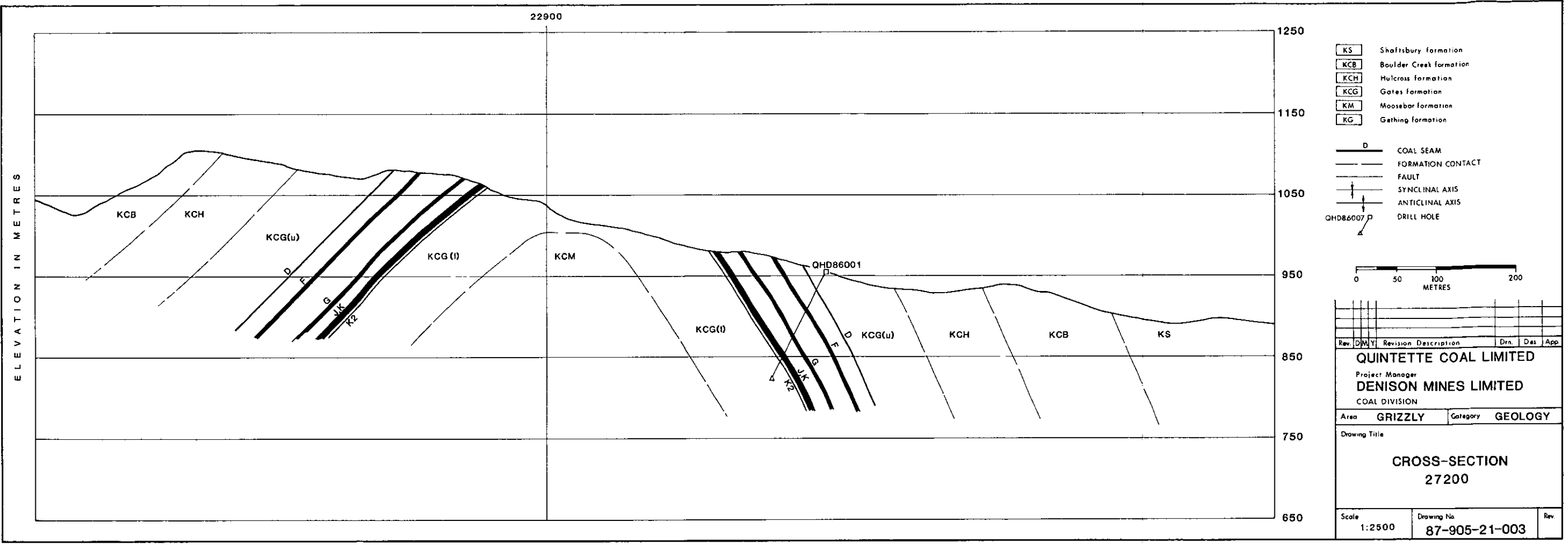
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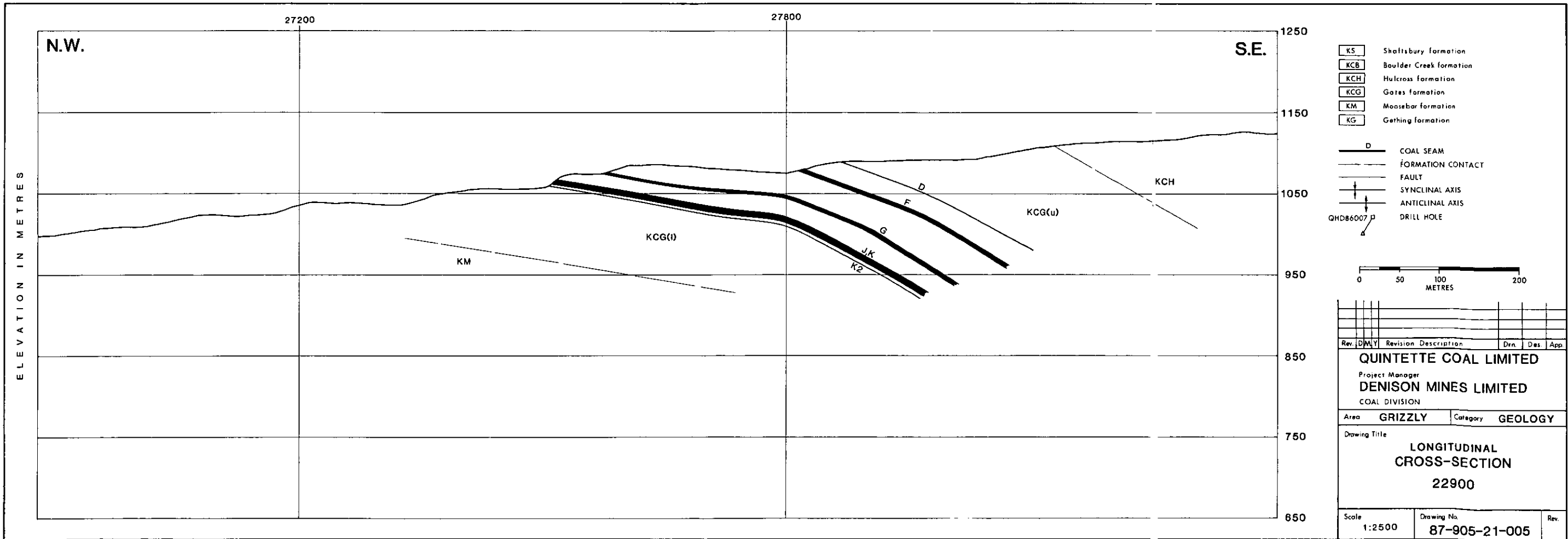
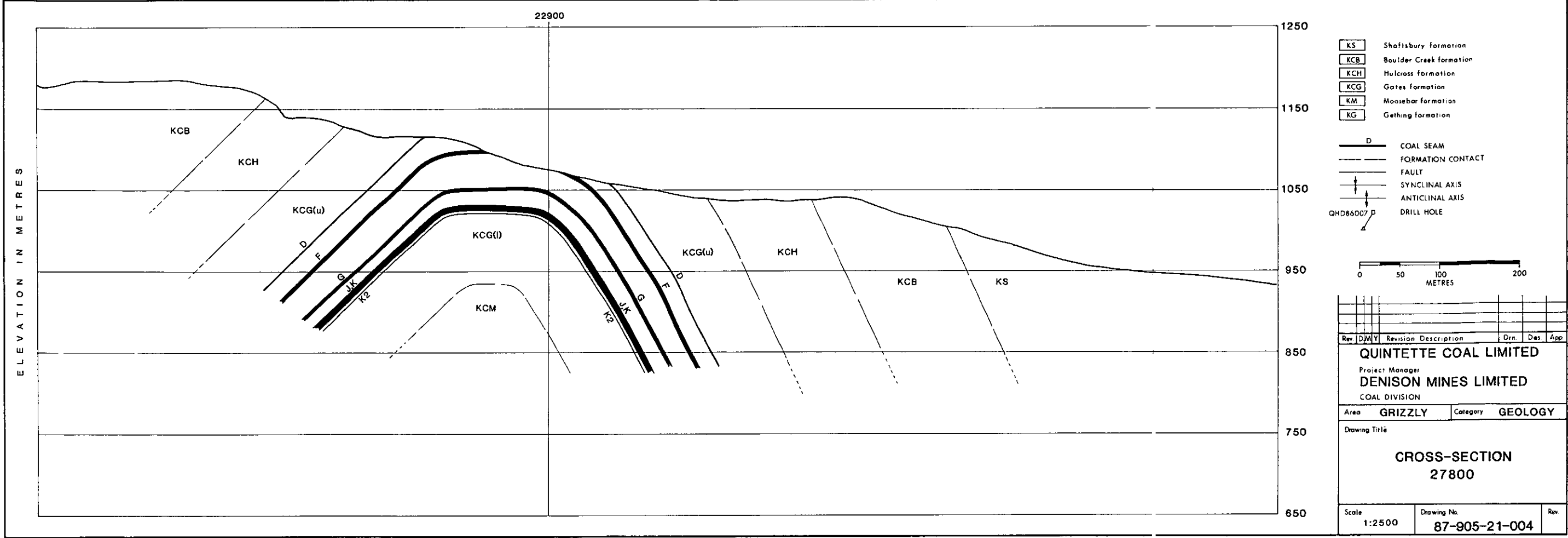
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- ROADS
- TRENCH
- ROTARY DRILL HOLE
- DIAMOND DRILL HOLE
- THRUST FAULT
- ANTICLINE
- SYNCLINE
- GEOLOGIC CONTACT
- COAL SEAM OUTCROP

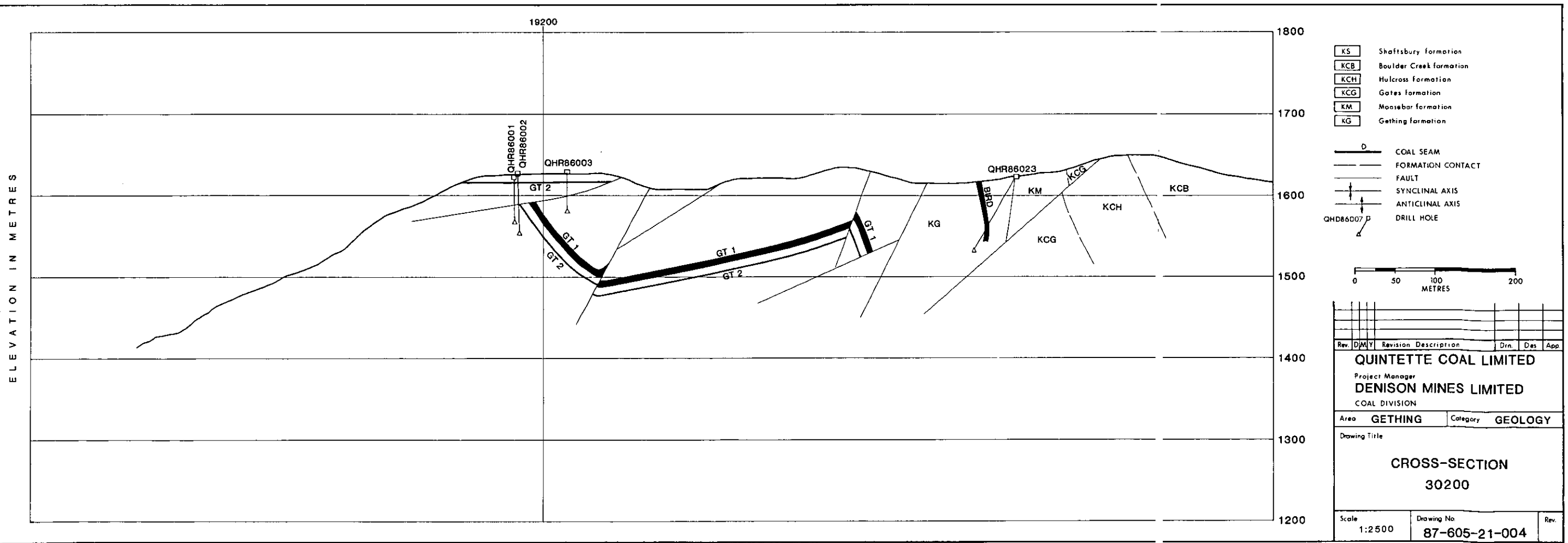
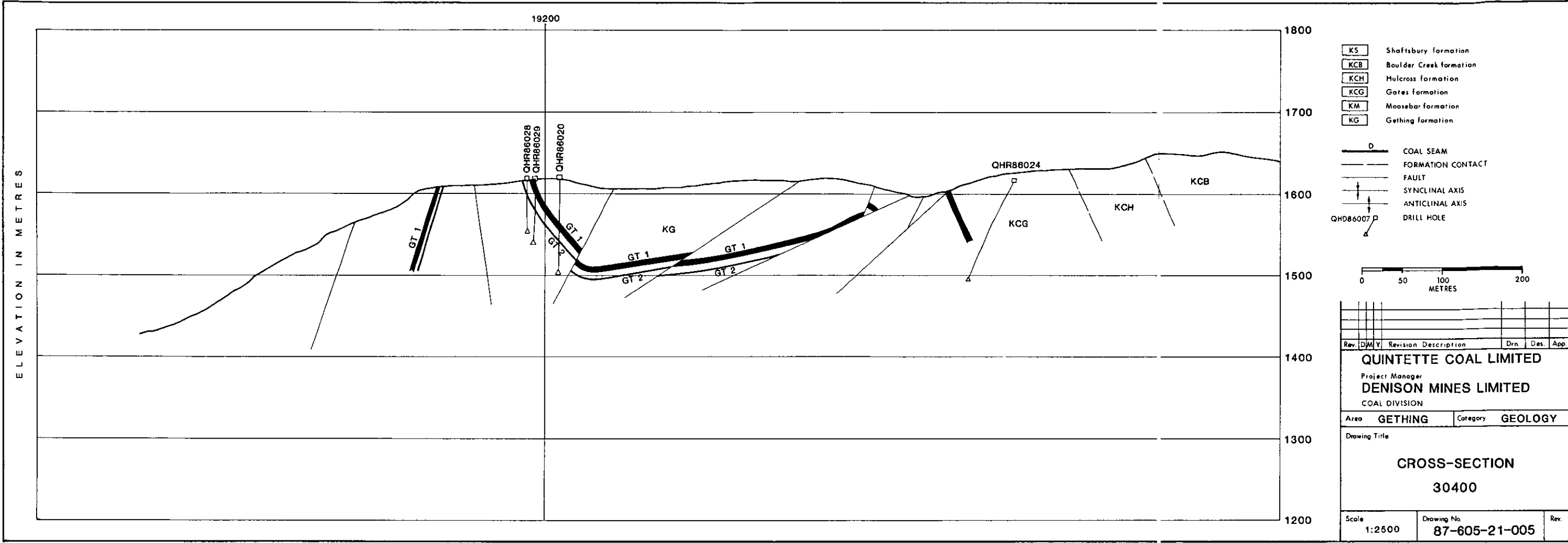
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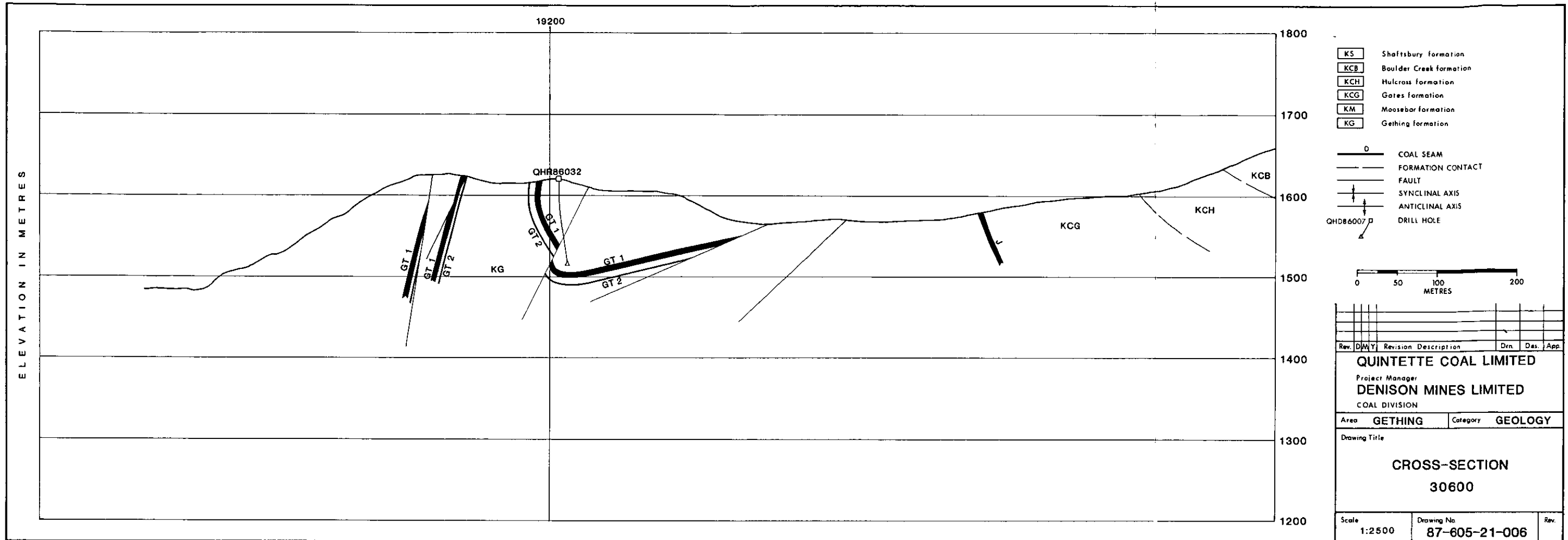


QUINTETTE COAL LIMITED			
PROJECT NUMBER DENISON MINES LIMITED			
EPR. DIVISION			
NO. GRIZZLY	CATEGORY	TOPOGRAPHY	
DRAWING TITLE			
GRIZZLY AREA GEOLOGY			
SCALE	DRAWING FILE 86-905-30-001		









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SH 0.06
MR 0.04

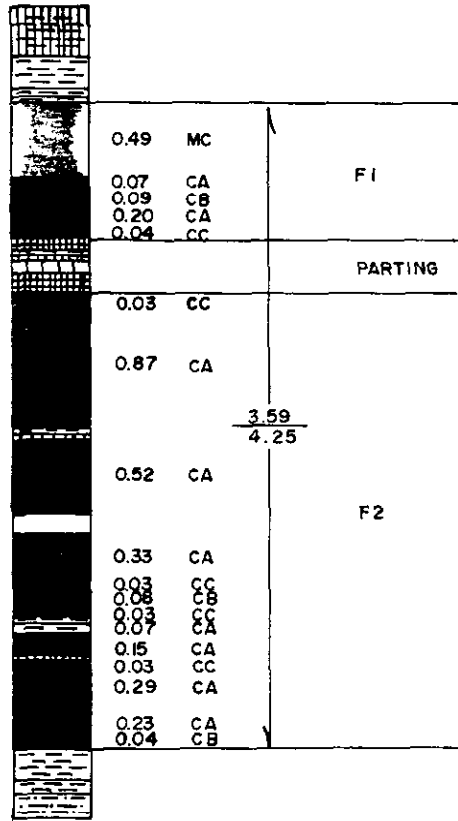
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CSH 0.02

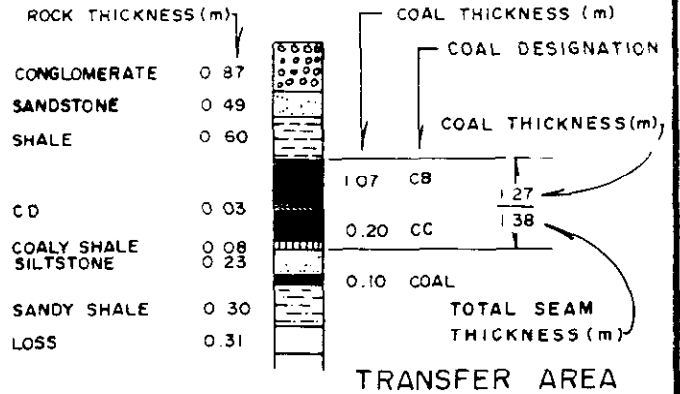
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GRSH 0.20
CRSH 0.09
SSH 0.17



LEGEND



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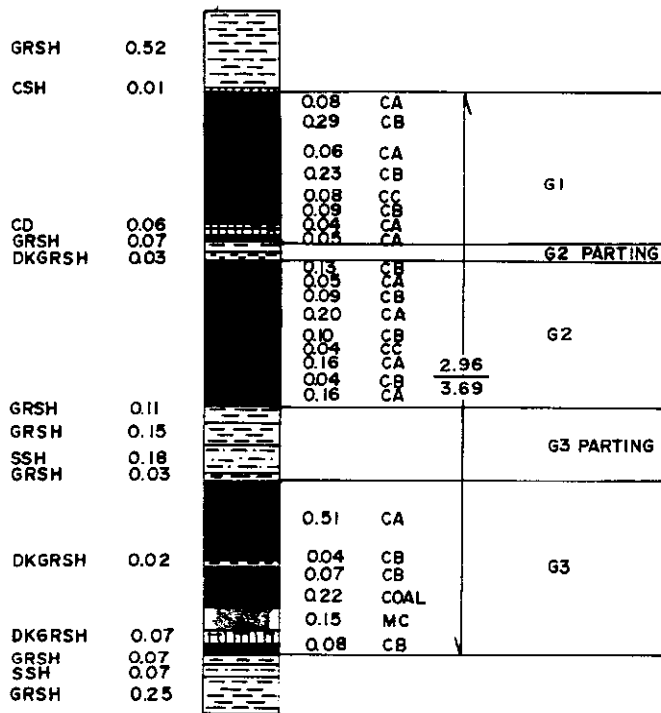
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OF F SEAM

TAKEN FROM QHD 86008

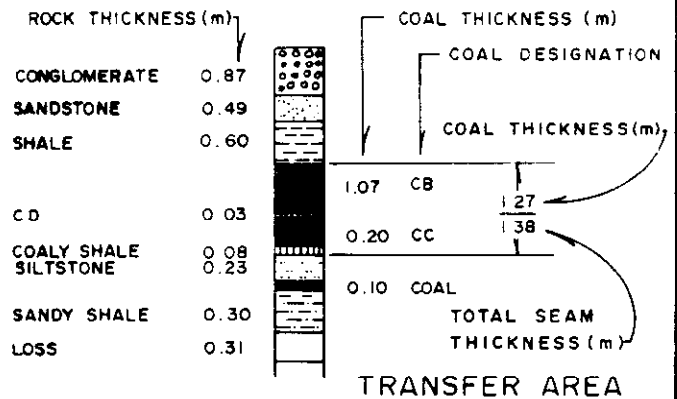
FIGURE 2.5

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BCIL 742 OCL



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Scale: 1:50 (VERT.)

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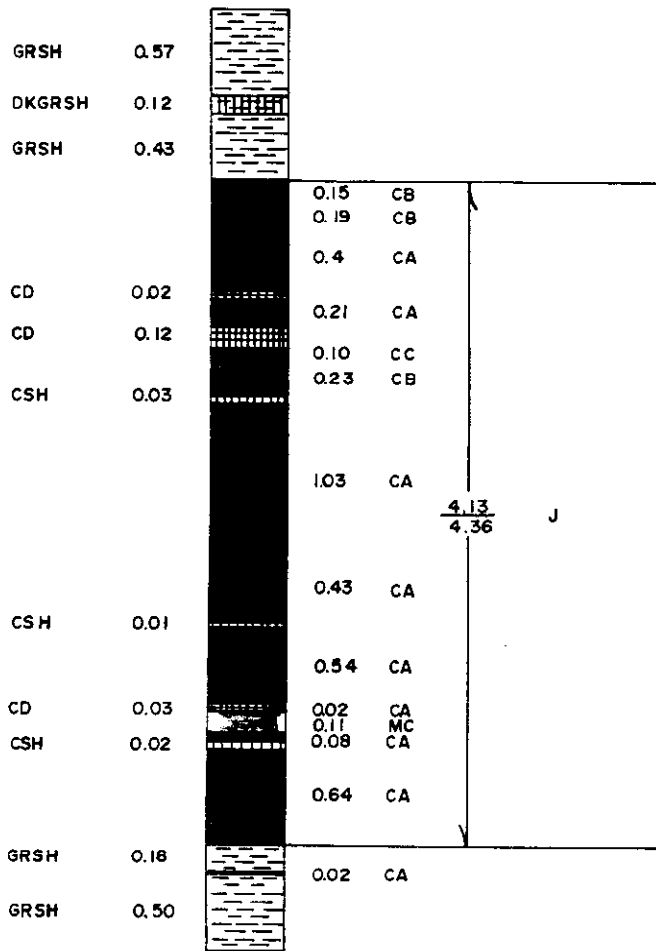
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OF G SEAM

TAKEN FROM QHD 86008

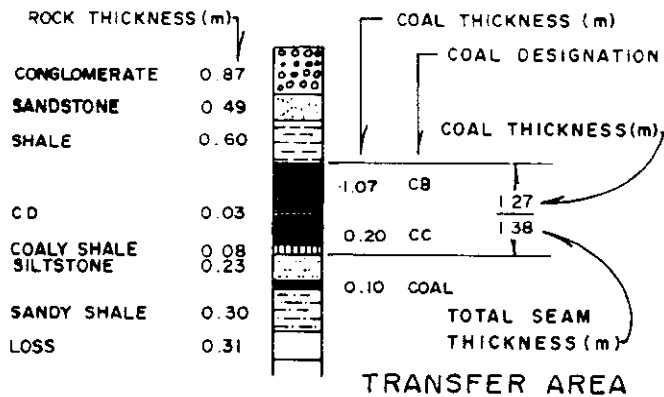
FIGURE 2.6

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BCIL 7742 DCL



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Drawn: KJV

Scale: 1:50 (VERT.)

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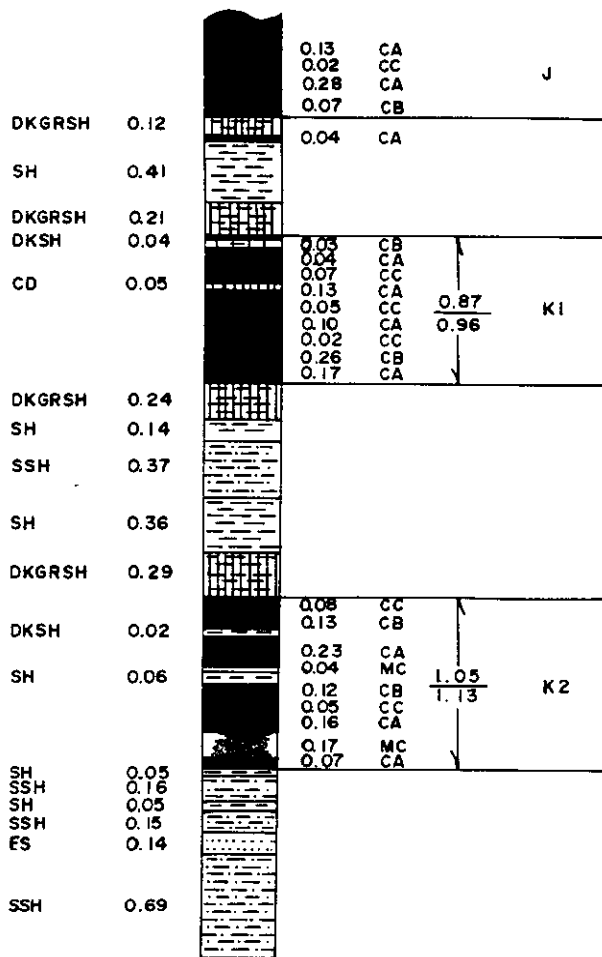
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TAKEN FROM QHD 85002

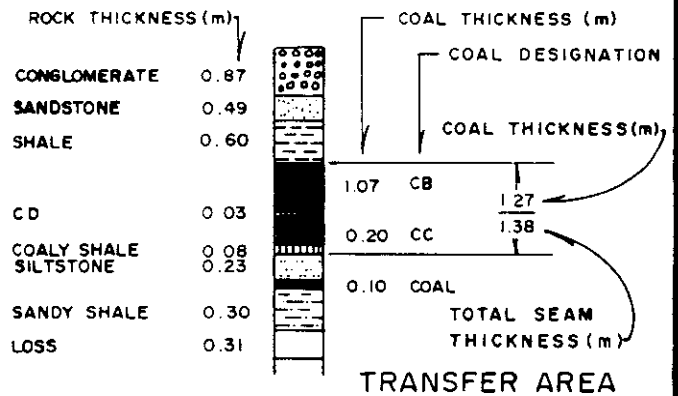
FIGURE 2.7

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BCIL 7742 OCL



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TYPICAL SECTION

OF K SEAM

TAKEN FROM QHD 86003

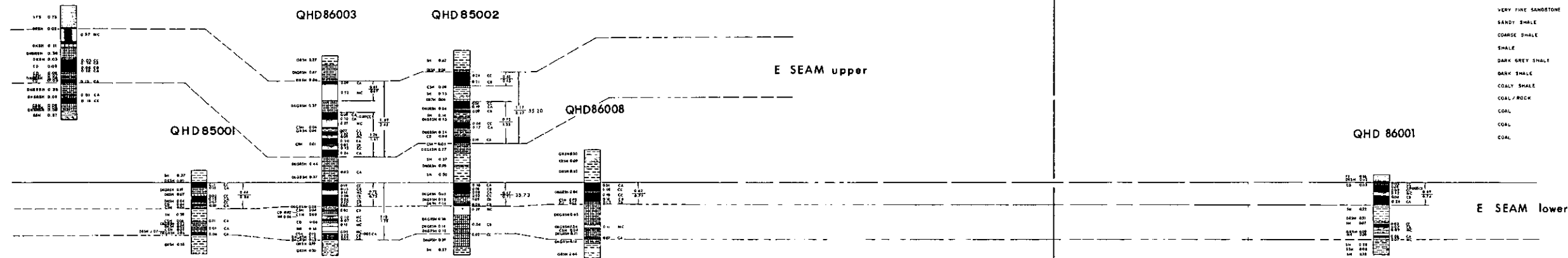
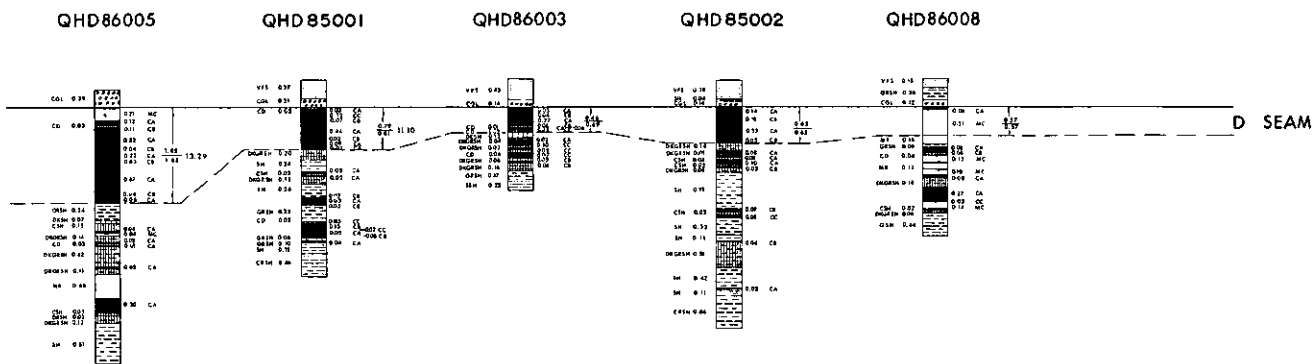
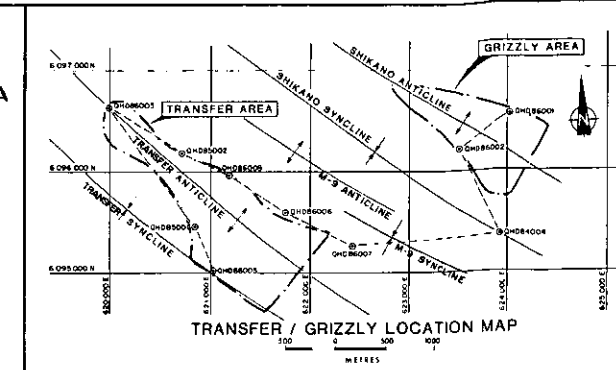
FIGURE 2.8

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BCIL 7/42 OCL

TRANSFER AREA

GRIZZLY AREA

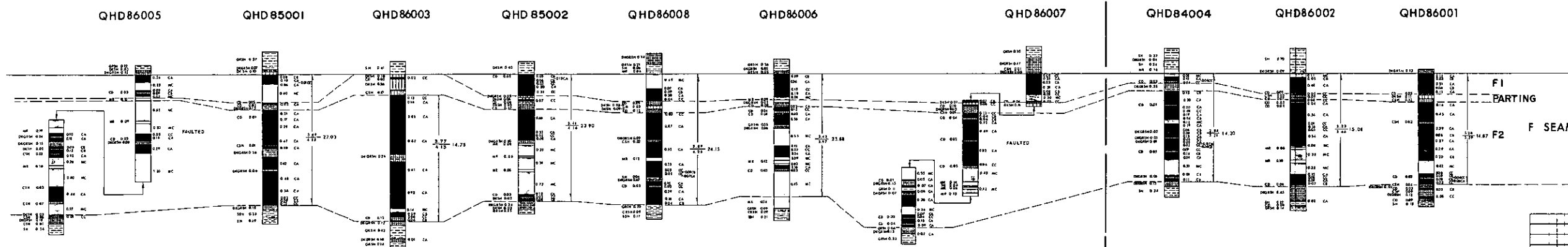


LITHOLOGIC SYMBOLS

CONGLOMERATE	CSL
CLARSE SANDSTONE	CS
MEDIUM SANDSTONE	MS
FINE SANDSTONE	FS
VERY FINE SANDSTONE	VFS
SANDY SHALE	SSM (SILTSTONE)
COARSE SHALE	CRSH (SILTY CLAYSTONE)
SHALE	SH (CLAYSTONE)
DARK GREY SHALE	DGRSH (CARBONACEOUS > 80% ASH)
DARK SHALE	DKSH (20-40% ASH)
COALY SHALE	CSH (40-50% ASH)
COAL / ROCK	CR (30-45% ASH)
COAL	CC (20-30% ASH)
COAL	CB (10-20% ASH)
COAL	CA (< 10% ASH)

LEGEND

ROCK THICKNESS (m)	COAL THICKNESS (m)
CONGLOMERATE 0.67	CONGLOMERATE 0.67
SANDSTONE 0.49	SANDSTONE 0.49
SHALE 0.80	SHALE 0.80
CD 0.03	CD 0.03
COALY SHALE 0.29	COALY SHALE 0.29
SANDY SHALE 0.30	SANDY SHALE 0.30
LOSS 0.31	LOSS 0.31
	COAL THICKNESS (m)
	1.07 CB
	0.20 CC
	0.10 COAL
	11.04 - ASH CONTENT % * LIVE QTY BASIS * adjusted for missing core
	TOTAL SEAM THICKNESS (m)

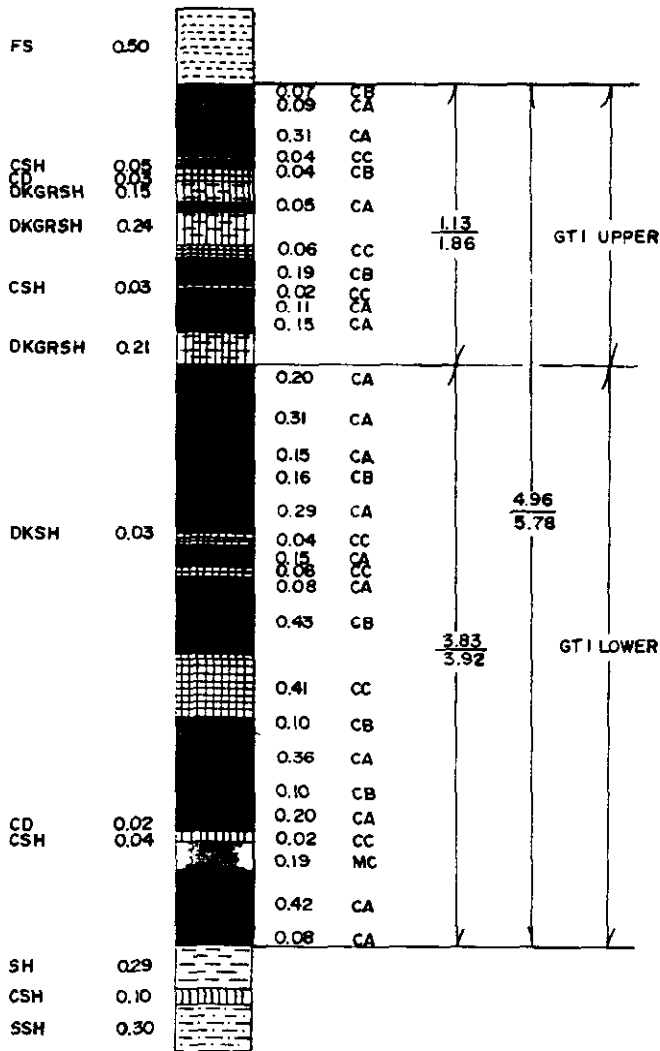


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Rev	0	M	Revision Description	Drn.	Des.	App

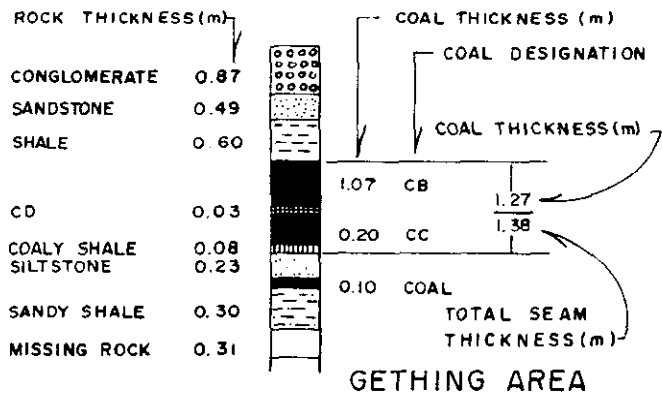
QUINETTE COAL LIMITED
Project Manager:
DENISON MINES LIMITED
COAL DIVISION

Area: TRANSFER/GRIZZLY Category: CORRELATION
Drawing Title:
**TRANSFER / GRIZZLY AREA
DETAILED SEAM CORRELATION
D, E, AND F SEAMS**

Scale	Drawing No	Rev
1:50 (vert.)	86-903-26-001	0



LEGEND



Date: MARCH 09, 1987

Design: HTB

Drawn: DKL

Scale: 1: 50 (VERT)

QUINTETTE COAL LIMITED

Project Manager

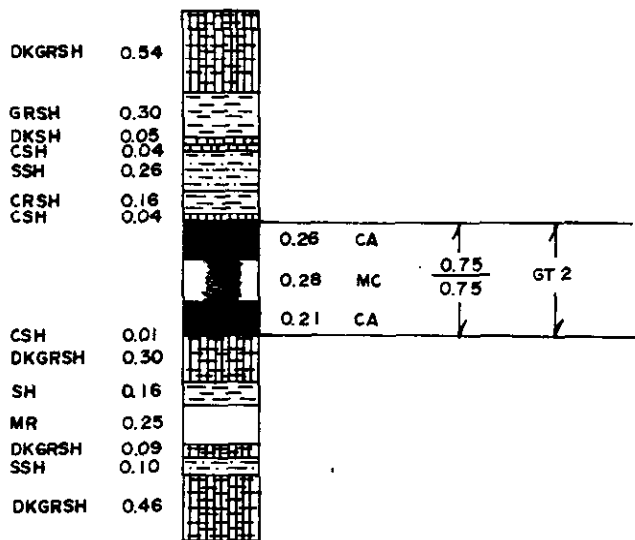
DENISON MINES LIMITED

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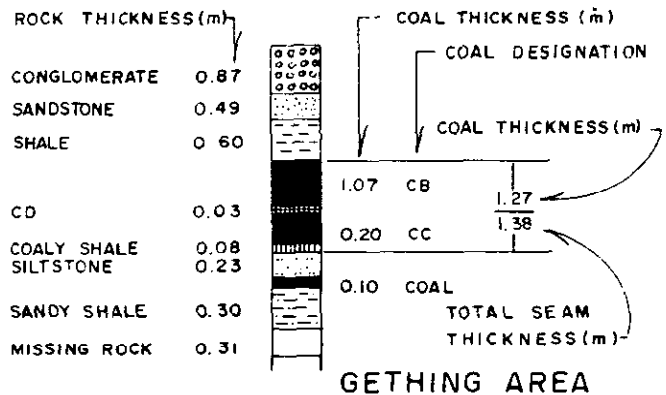
TYPICAL SECTION
OF GTI SEAM
TAKEN FROM QJD 7642

Drawing No.
FIGURE 2.9

Rev.
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LEGEND



Date: MARCH 09, 1987

Design: HTB

Drawn: DKL

Scale: 1: 50 (VERT.)

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TYPICAL SECTION
OF GT 2 SEAM
TAKEN FROM QJD 7642

Drawing No.
FIGURE 2.10

Rev.
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3.0 COAL QUALITY

3.1 INTRODUCTION AND SUMMARY

During the course of the exploration work on the Grizzly/Transfer area, a number of coal samples were collected from drill cores. Laboratory analysis and washability studies were carried out on these samples in order to evaluate their properties, primarily as a source of coking coal. This section will review and discuss the results of these testing programs.

Table 3.1 summarizes the number of drill cores that have been taken from each seam in the Grizzly/Transfer area and used in the evaluation of quality. The prime criterion for the use of drill core results was usually 80% or greater core recovery. Where possible, extensive analytical studies were conducted on all samples and analysis included the following:

- Proximate Analysis
- Sulphur Content
- Ash Analysis
- Calorific Value
- Ash Fusibility
- Free Swelling Index (F.S.I.)
- Dilatation and Gieseler Fluidity
- Hardgrove Grindability Index
- Petrographic Analysis
- Washability Testing

Samples were from about 60 mm diameter core samples. Analyses have been performed on coal from all seams included in the potential mineable resources of the Grizzly/Transfer area.

The coal seams within the deposit can be ranked according to the ASTM method of coal classification as low volatile bituminous class. Using vitrinite reflectance, a more reliable method of classifying coal rank where a reflectance of 1.51 separates mvb and lvb coals, all seams but K can be classified as mvb, and K as lvb coal. On a seam-by-seam basis, Grizzly/Transfer coal is a little higher in ASTM rank than the Mesa, Wolverine or Babcock deposits and is more similar to Shikano deposits. Table 3.2 summarizes these results for each pit using vitrinite mean maximum reflectance as the prime measure of coal rank.

As might be expected, the rank of the coal increases slightly towards the basal level J and K seams, K seam being a low volatile bituminous (lvb) rank in Grizzly/Transfer.

Table 3.3 summarizes the current Quintette product specifications and compares them to expected Grizzly/Transfer average product quality. On an average basis the Grizzly/Transfer production meets the Quintette product quality specifications, except possibly for volatile matter which is close but slightly lower than specification. This would not be a problem overall as production specifications will be met since at no time will coal from any one seam comprise the plant feed. Grizzly/Transfer would be developed in conjunction with other pits and fed to the plant in a blend from a number of pits. Slight variations in product coal quality may occur but such variations are controlled by blending at the plant or port, to ensure cargo quality specifications are met.

Washability data was used with a wash plant simulator computer program to predict metallurgical coal yields. Since yield is a function of both seam washability characteristics and the ash content of the coal, equations were derived to relate the calculated yield to the plant feed ash level for each seam in each pit. Similar equations have been derived for coals currently mined in the Mesa and Wolverine deposits and are being used successfully to predict actual plant results. The empirical relationships between yield and ash for each seam permit straight forward calculation of expected yields where ash levels of feed are known, and permits easy adjustment for out-of-seam dilution, partings, breaker rejects, etc. Another advantage to this approach is that more reliable ash data are available than reliable float/sink data. The resulting increased density of yield results should lead to more reliable forecasting and is also amenable to advanced computer geostatistical averaging techniques such as Kriging.

3.2 GRIZZLY/TRANSFER RAW COAL QUALITY

Mean values of drill-core raw coal quality are summarized in Table 3.4 from detailed results in Appendix I, Section 3.1. Analyses summarized include proximate residual moisture (RM), ash and volatile matter (VM), free swelling index (FSI), sulphur (S), phosphorous (P), calorific value (CV), and Hardgrove Grindability Index (HGI).

Raw coal residual moisture values appear to be in line with those expected throughout the Quintette pits, about 0.5 to 0.7%. Volatile matter on a DMMF basis indicates the weighted average Grizzly/Transfer coal is a low volatile bituminous coal as ranked by ASTM. FSI levels are lower than would be expected for clean coal, since the excessive amount of ash in the samples depresses the FSI. Sulphur in D seam is higher than the other seam, but since it is not part of the reserves, this will not represent a problem. HGI values are in line with other experience in Quintette and indicate a relatively soft coal, somewhere between the hardness of Coal Valley and the Southeast BC coals. Phosphorous content in the two seams of raw coal analyzed appeared to be acceptable.

3.3 GRIZZLY/TRANSFER CLEAN COAL ANALYSES

This section will concentrate on examining the mean clean coal analysis of the drill core samples. Lab scale work was conducted at two commercial analytical laboratories, General Testing Laboratories and Cyclone Engineering Sales Limited. Drill core samples were used to produce a clean coal product by combining the same float-sink fractions from each sample to create the clean coal (see earlier section on procedures). This often resulted in a clean coal ash that was less than the current 9.5% Quintette specification.

3.3.1 Proximate and Ultimate Analyses

Proximate, sulphur and a few phosphorous analyses were conducted on drill core simulated clean coal. Table 3.5 contains mean values of these results.

Residual moistures (RM) of the clean coal samples was close to those currently being experienced in Quintette and found in other pits - around 0.5 to 0.7%. Mean ash level of the clean coal samples was slightly lower than the final specifications for Quintette coal. The volatile matter, on a DMMF basis, agreed with the raw coal values and indicated that these coals were all low volatile bituminous as classified by ASTM. The sulphur content of D seam was over the 0.5% quality specification of the product; however, since it will not be mined it will have no effect on the product quality.

3.3.2 Thermal Rheology

Gieseler fluidity, dilatation and free swelling index (FSI) thermal rheological testing was conducted on many of the drill cores taken from the proposed pit area. Details of these analyses appear in Appendix I, Section n3.1. A summary of the results appears in Table 3.6.

Inspection of the mean thermal rheology values for each seam in Table 3.6 indicates that the seams have caking (swelling and plastic) properties that would result in coking characteristics of these coals during the carbonization process. The weighed average maximum fluidity (12 ddpm) is similar to Canadian production coals with higher reflectance. It appears from review of the data from the Babcock, Mesa and Shikano pits, that the Grizzly/Transfer FSIs, fluidities and dilatations also tend to decrease towards the basal J and K seams.

Projections of coking properties of Grizzly/Transfer coal blended with the existing QCL product indicate that coking quality will be at least equivalent and probably better than the existing met product.

3.3.3 Ash Analysis, Ash Fusion and Calorific Value

Mean seam values of ash analysis and ash fusion appear in Tables 3.7 and 3.8. Detailed calorific values (which appear in Appendix I, Section 3.1) and ash content relationship, are seen graphically in Figure 3.1.

The results in Table 3.7 indicate that the base-to-acid ratio varies between seams in Grizzly/Transfer. The low base-to-acid weighted average ratio indicates that slagging is unlikely to be a problem at normal combustion furnace operating temperatures. Fouling should not be a problem as the $\text{Na}_2\text{O} + \text{K}_2\text{O}$ content in the ash is less than 2.0%.

Results in Table 3.8 show some variation in coal ash fusibility temperatures between seams in the Grizzly/Transfer area. However, on a weighted average fusibility of coal ash should not represent a problem in normal combustion furnace operations.

The calorific value results seen in Figure 3.1, indicate the usual linear relationship found between coal ash level and calorific value. The solid line in Figure 3.1 is a historical regression line derived from samples taken from a number of Quintette pits. Inspection of the figure indicates that the Grizzly/Transfer values are perhaps 100 kilocalories per kilogram higher than those for the average Quintette values. This is expected because of the slightly higher rank (ie. more carbon content) of the Grizzly/Transfer coals as compared to the other pits at Quintette. Normally oxidized (weathered) coal product would have calorific values up to 500 kilocalories per kilogram less than metallurgical coal value, which is represented by the solid line in the figure. Actual thermal coal production quality would occur somewhere between the solid and dashed line for the Grizzly/Transfer pits. Since the coal will be blended with other coals from Quintette, it is expected that the calorific value of the Grizzly/Transfer material clean coal will have no noticeable effect on the overall calorific value of the QCL clean coal product.

All regression equations had high levels of confidence (i.e. high correlation coefficient) and there were reasonable data points for F, G, J+K1 and K1K2, although not for D, or J alone. Only drill cores with about 80% recovery or greater were used in the regressions. The limit of confidence in the yield results is on average about ± 2 yield percent units.

On the figures, both the drill core and plant simulated ash/yield points fell together and were regressed together. Consequently, the regressions can be used to calculate either clean coal directly from insitu coal, or expected plant yield and clean coal using the mine planning procedure. In deriving the mine planning procedure results, the following criteria were used: 30 cm of 87% ash OSD; 30 cm loss of the mining section at $\leq 30\%$ ash; and breaker rejects as a percentage of ROM material) = $0.5 \times \text{OSD} + 0.1 \times \text{insitu ash}$. Rejects were estimated at 80% ash.

Yields projected in these figures are for metallurgical coal and the thermal plant yield is estimated by subtracting 9 yield percent units from the calculated metallurgical yield for a given plant feed ash. The 9% recognizes the fact that the fines (minus 0.15 mm) are currently sent to tailings as they have too high an ash to be recovered into the product.

3.5 GETTING COAL QUALITY

3.5.1 Raw Coal

Raw coal residual moisture appeared to be higher in the bulk sample than found throughout Quintette, 0.5 to 0.7%, and also higher than the QHD 86009 drill core results. Normally, higher residual moisture is associated with oxidized coal and it is probable that the bulk sample was weathered to some degree. Volatile matter on a d.a.f. basis indicates the coal is a low volatile bituminous coal as ranked by ASTM. FSI levels are lower than for Gates clean coals because of the excessive inerts (ash and inert macerals) in the samples. Sulphur was high in the raw (QHD 86009) sample at over 1%, although low in the other two samples. HGI is similar to Gates coal, indicating a relatively soft coal somewhere between the hardness of Coal Valley and South East BC coals. (See Table 3.12).

Raw samples were analyzed for ash fusion and ash mineral composition to complete the evaluation of the use of these coals in the thermal markets. The low volatile content restricts use of this coal in the power generation thermal coal market as nearly all thermal stations are designed to use high volatile coals however a few plants do blend such high calorific, low volatile coals and a few plants are specifically designed for low volatile coals. The calorific value of the raw GTA sample was excellent at 7641 cal/gm (db) or as received at 8% moisture of about 6030 cal/gm (net). The ash fusibility and mineral composition results on GT-A or GT-Combined indicate that slagging is unlikely to be a problem at normal combustion furnace operating temperature. However, fouling would be a problem as (Na₂ + K₂) content in the ash is over 2.0% in most samples and blending before combustion may be required. The best marketing potential of the raw coal

is likely in the cement industry that is not concerned with ash levels up to 15% or so, or ash mineral composition, but rather with as received calorific value. For GT-A, the calorific value compares favourably with previous QCL thermal cargoes that average about 7400 ± 100 cal/gm (adb), or 6900 ± 93 cal/gm (9% moisture) at 11% ash, the ash level of the GT-A raw sample. These cargoes were well received because of the good calorific value, low moisture and ease of pulverization. (See Table 3.13A).

3.5.2 Washability Results and Conclusions

Attached is a table (3.11) of regression coefficients and a graph (Fig. 3.8) relating ash and yield. GT-2 had only 1 result which fell into the GT-1 results and consequently it was regressed with GT-1 data. Both the drill core and plant simulated ash/yield data fell together and was regressed together so that the regressions can be used to calculate either clean coal directly from insitu coal or expected plant ash. Details are included on Table 3.11(a).

Table 3.11

GETHING YIELD / ASH PREDICTION EQUATION

Theoretical Yield = A + B x (ash) - R
 where A & B = regression constants

Expected Yield = Theoretical Yield x Plant Efficiency*

Seam	A	B	R. Factor	
			met	thermal
GT-1	114.186	-1.44	0	9
GT-2	114.186	-1.44	0	9

* Targeted at 92% for 1987 and onwards unless actual performance indicated it should be changed. Actual 1986 plant efficiency was about 91.8%.

Table 3.11 (a)

GETHING ACTUAL DRILL CORE ASH AND ESTIMATED PLANT FEED ASH VERSUS THEORETICAL YIELD

Seam	I.D.	DRILL CORE		ESTIMATED	
		Ash	Theoretical Yield	Plant Feed Ash	Plant Theoretical Yield
GT-1	GTA-Trench (lower)	9.63	99.15	17.98	92.13
	GTB-Trench (upper)	35.37	59.76	45.05	46.49
	GT-Comb.	18.07	84.02	21.91	86.22
	QHD 86009 GT1-L	11.85	95.10	17.20	91.43
	GT1-U	45.24	52.59	55.97	38.87
	GT1-U&L	22.84	81.82	23.02	80.94
GT-2	QHD 86009	55.36	30.98	60.80	25.09

Table 3.12

**GETHING
RAW COAL QUALITY**

Seam	Drill Hole	#/ID	Proximate			FSI	c/gm	%	HGI
			RM	Ash	VM				
GT-1	GT-A Trench		1.82	11.06	19.58	1	7641	.51	62
	GT-B Trench		2.40	36.25	18.47	1.5	5128	.41	67
	GT-Comp		1.92	18.88	18.54	1	6882	.47	63
	QHD 86009	GT1-U	.79	42.61	12.7	1		1.31	
		GT1-L	.91	12.81	18.44	1		.85	
		Comb, T31	.47	22.35	15.97	1.5		1.02	74
GT-2	QHD 86009	T32	0.60	48.25	14.82	1.5		.28	71

GRIZZLY/TRANSFER CV/ASH RELATIONSHIP

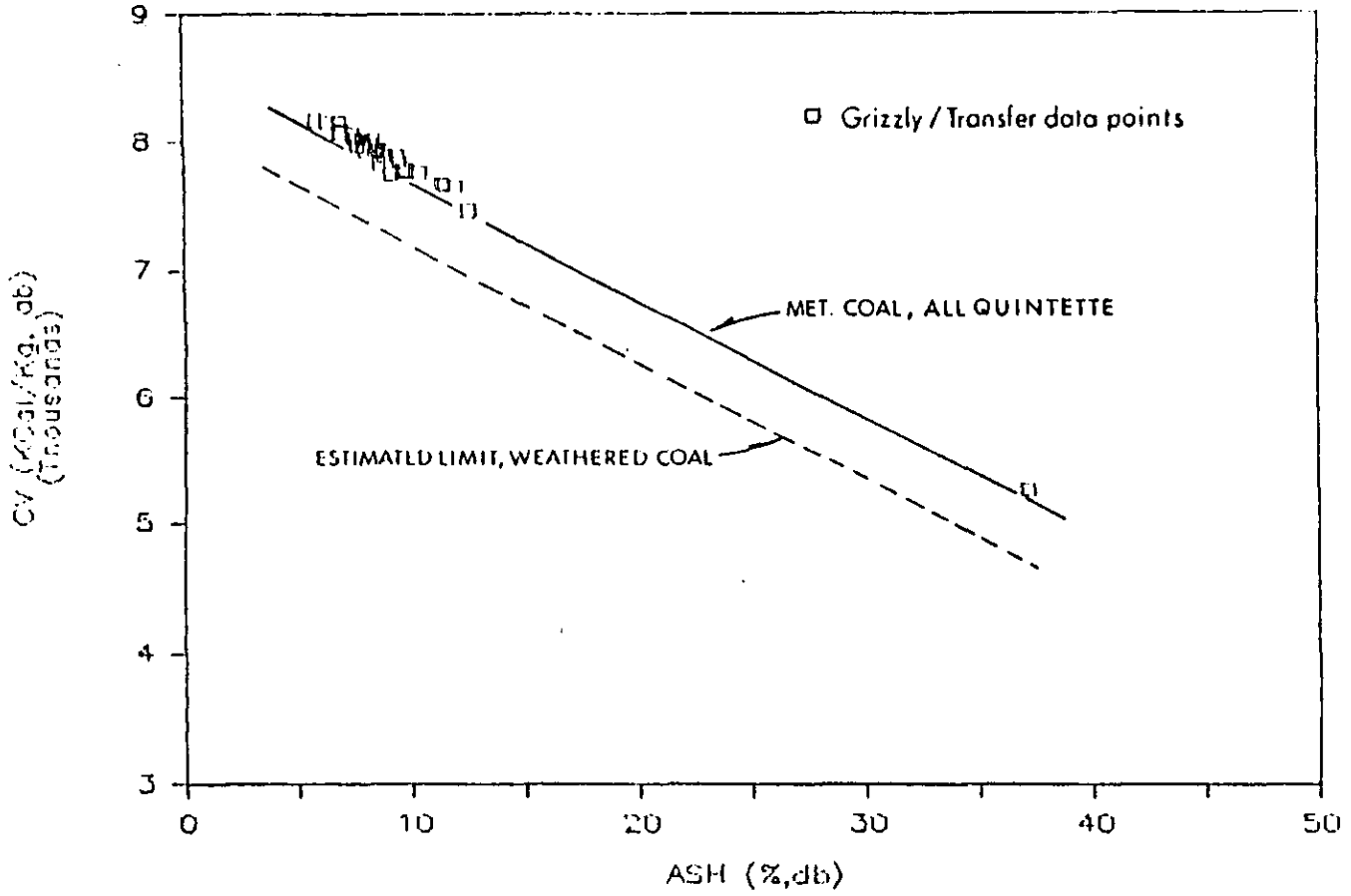
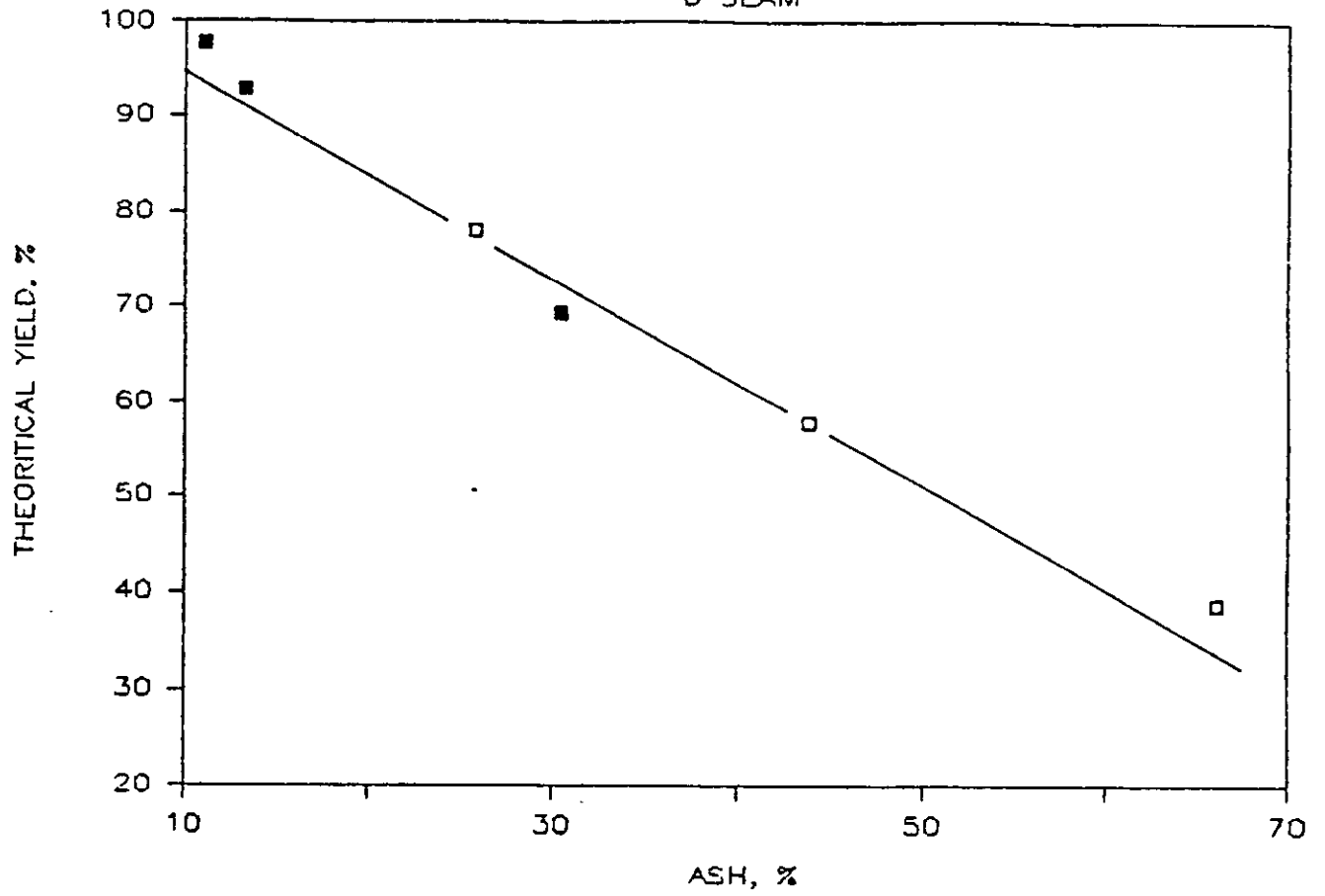


FIGURE 3.1

GRIZZLY/TRANSFER

D SEAM



- drill core insitu ash/yield
- estimated plant feed ash/plant yield using mine planning calculations

FIGURE 3.2

GRIZZLY/TRANSFER F SEAM

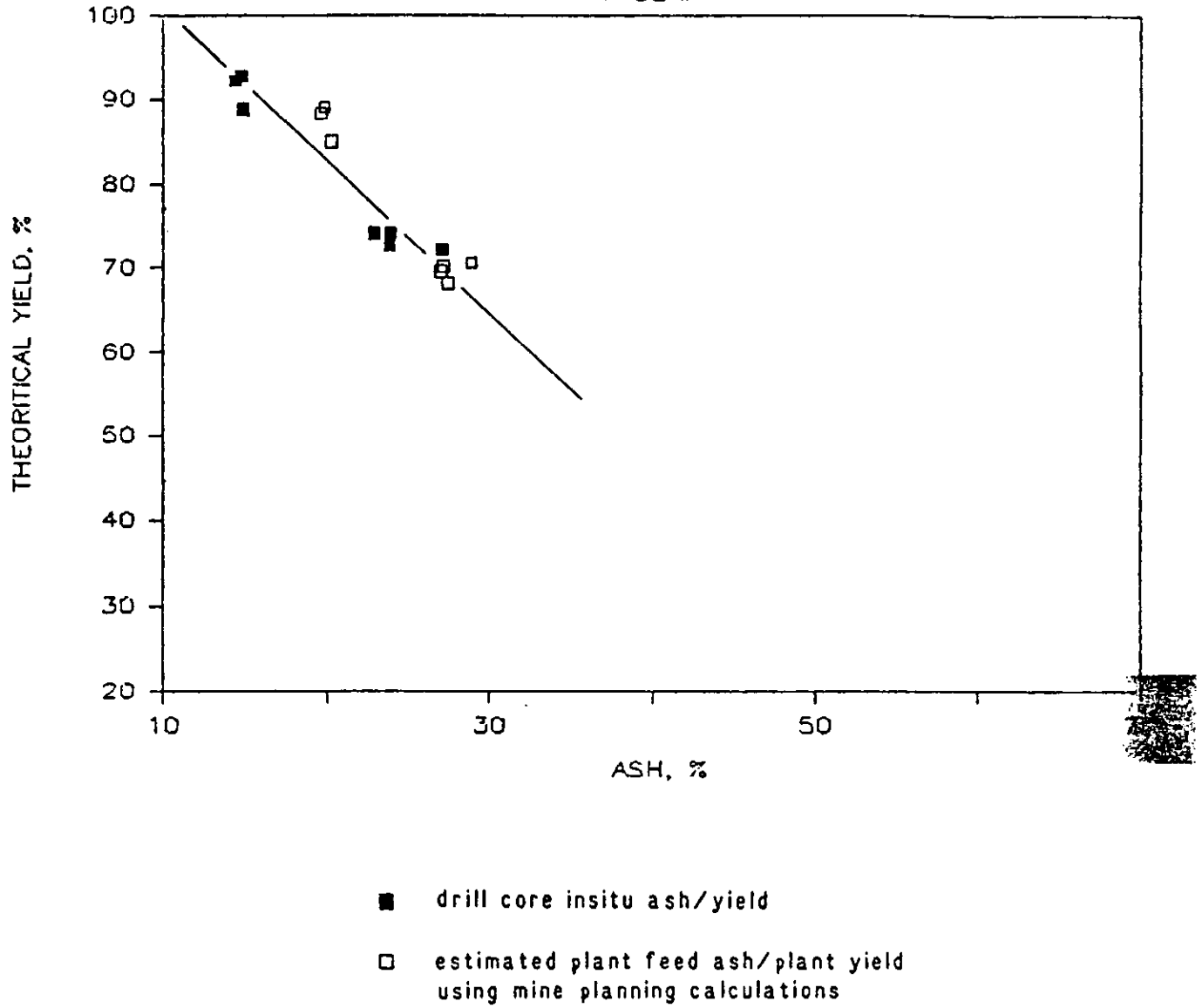


FIGURE 3.3

GRIZZLY/TRANSFER G SEAM

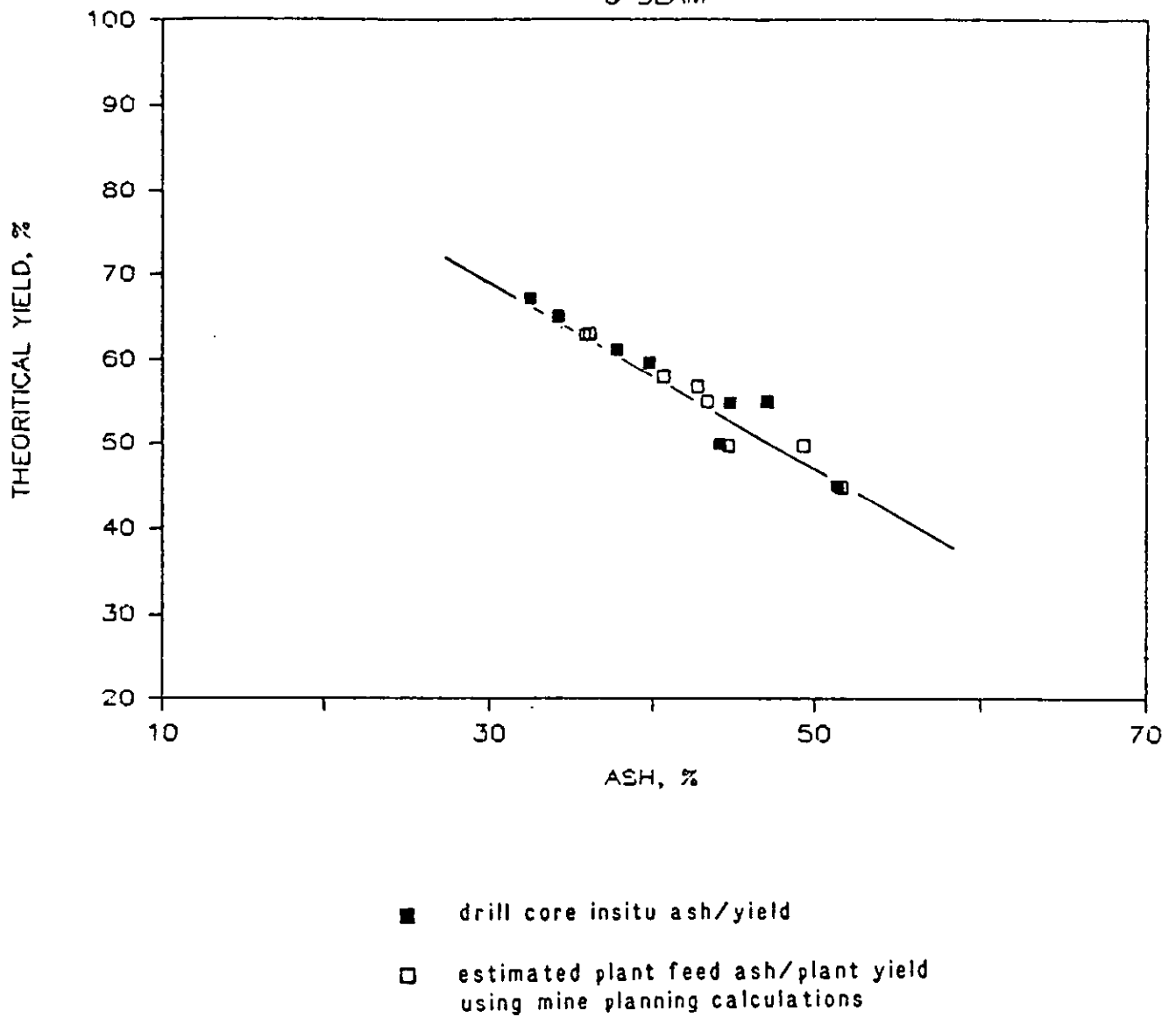


FIGURE 3.4

GRIZZLY / TRANSFER

J SEAM

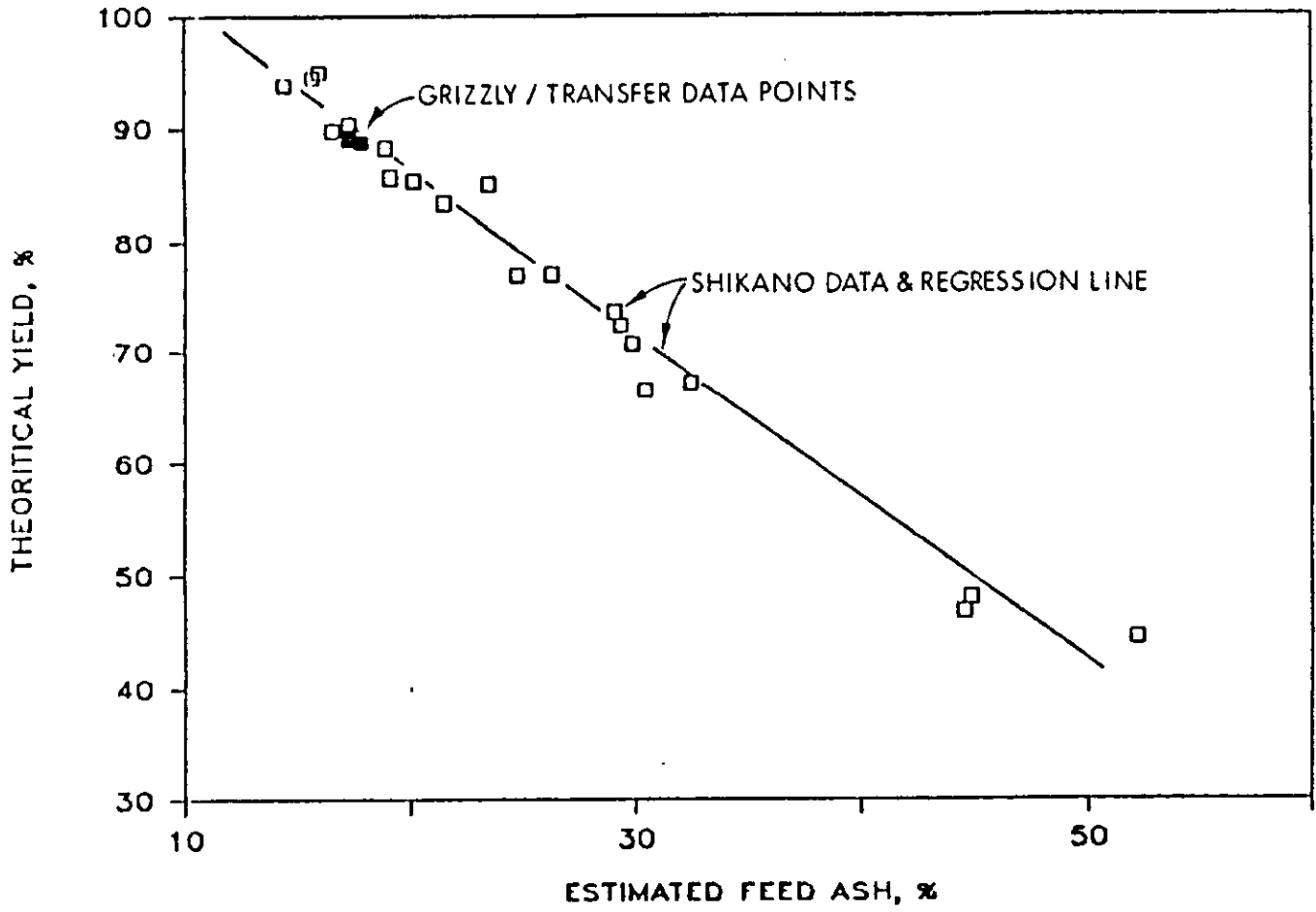
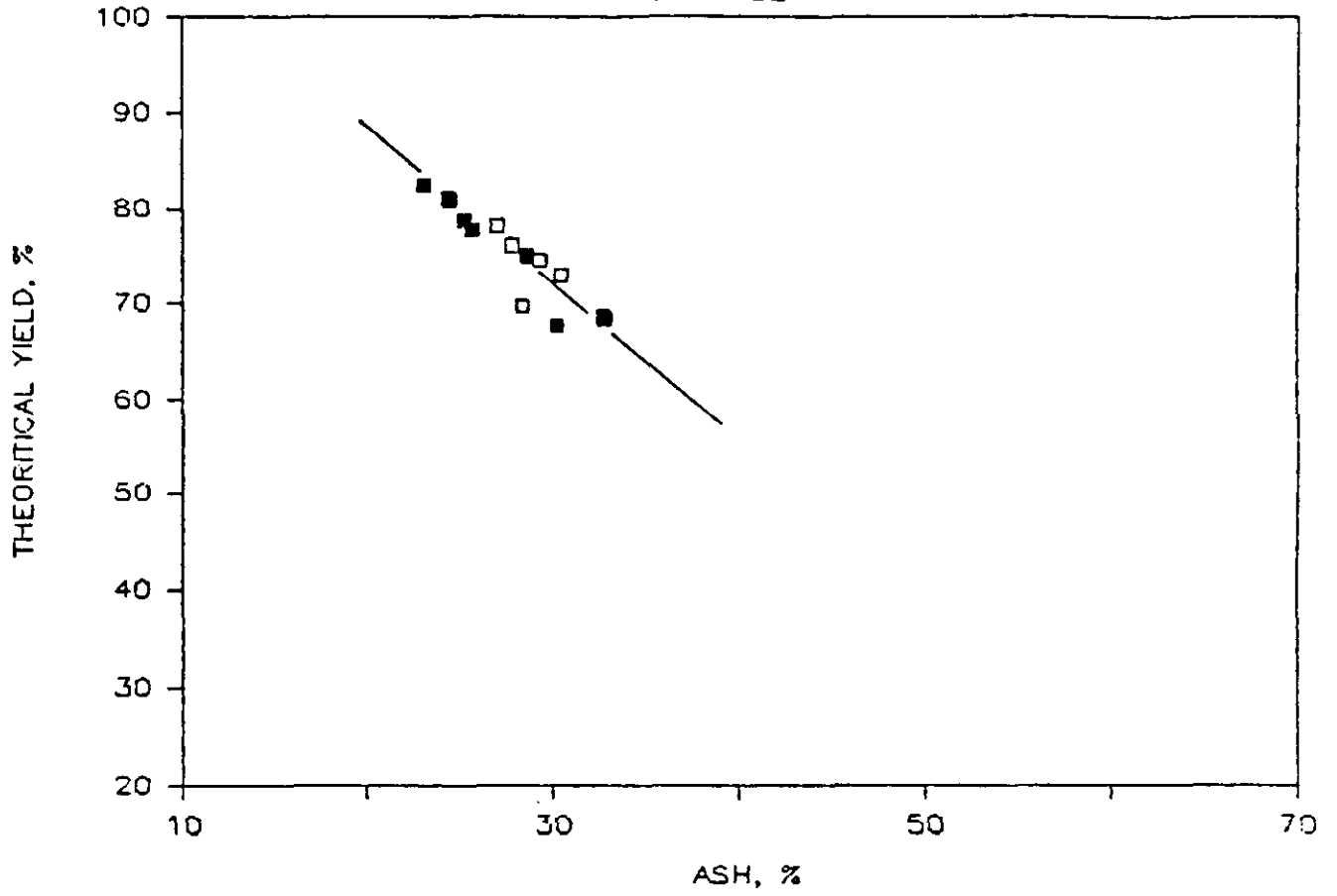


FIGURE 3.5

GRIZZLY/TRANSFER

J+K1 SEAM

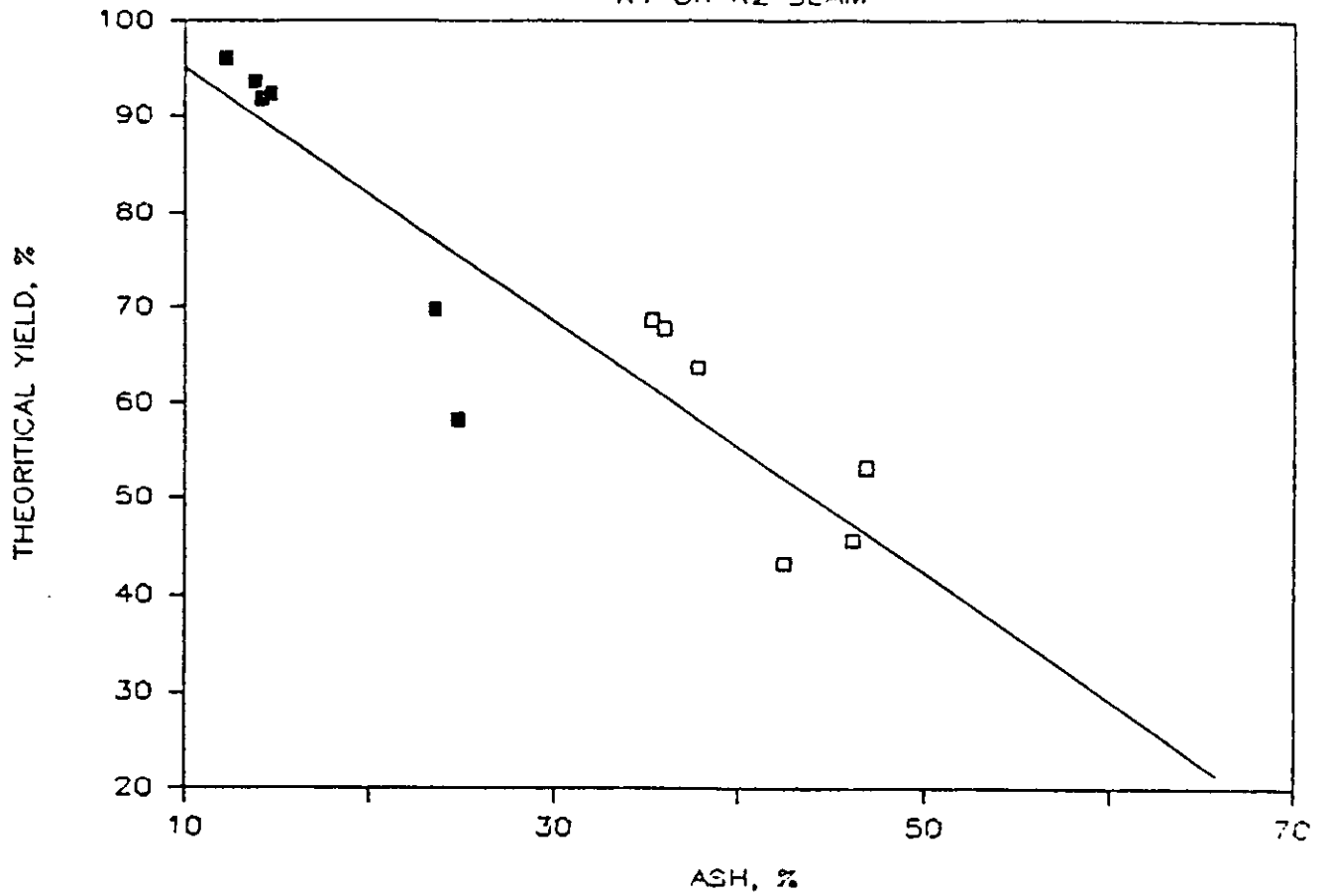


- drill core insitu ash/yield
- estimated plant feed ash/plant yield using mine planning calculations

FIGURE 3.6

GRIZZLY/TRANSFER

K1 OR K2 SEAM

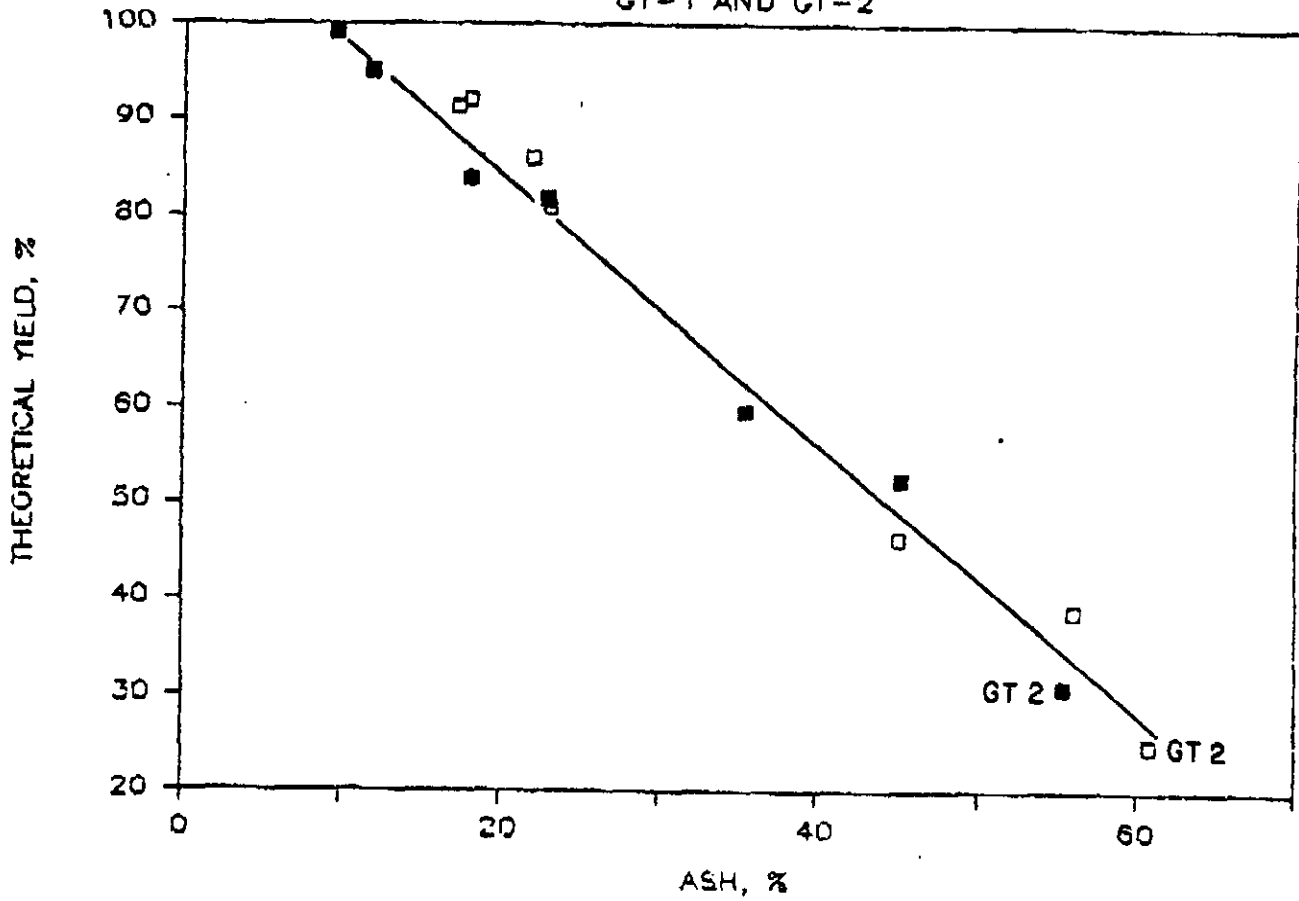


- drill core insitu ash/yield
- estimated plant feed ash/plant yield using mine planning calculations

FIGURE 3.7

GETHING

GT-1 AND GT-2



- drill core in situ ash/yield
- estimated plant feed ash/plant yield using mine planning calculations

Figure 3.8

GETHING ASH/FSI RELATIONSHIP

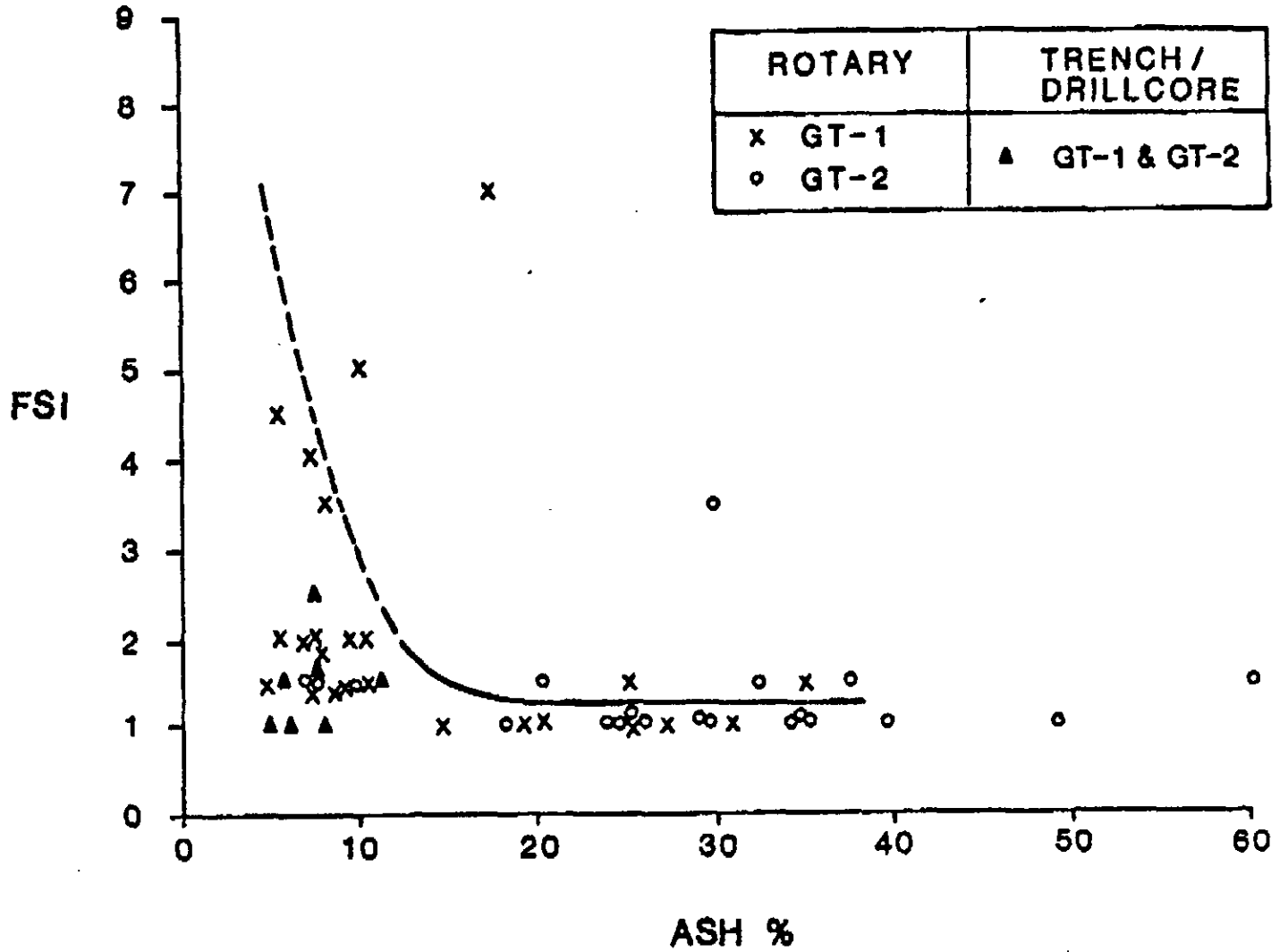


Figure 3.9

CHANGE IN COKE STRENGTH (DI 30/15)
FOR CARBONIZED BLENDS OF RAW GTA
WITH A SAMPLE OF QCL MET PRODUCT

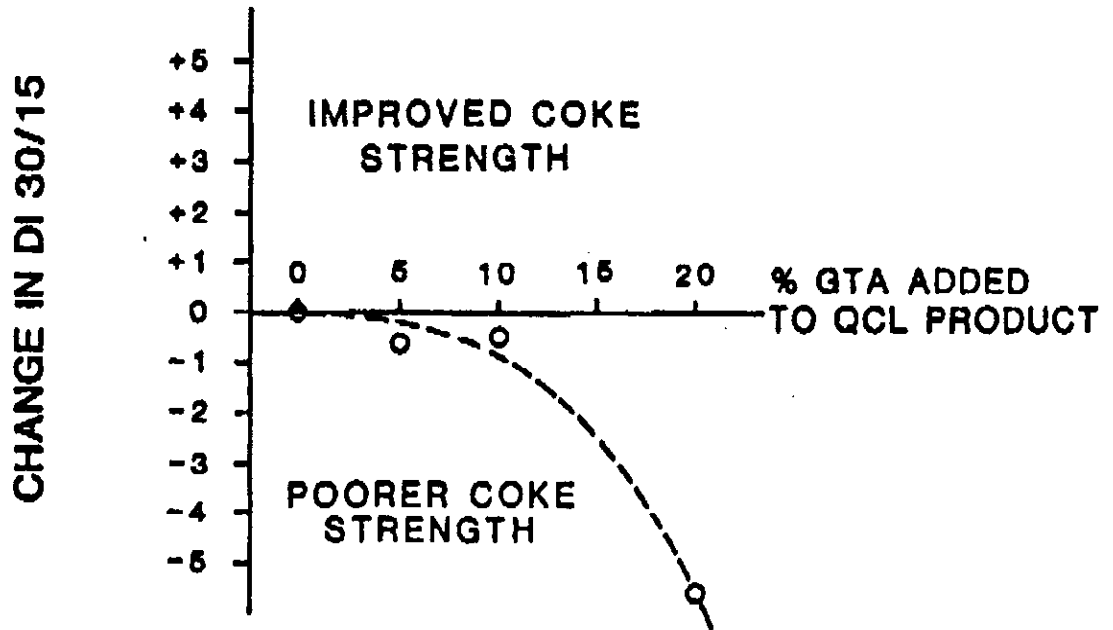
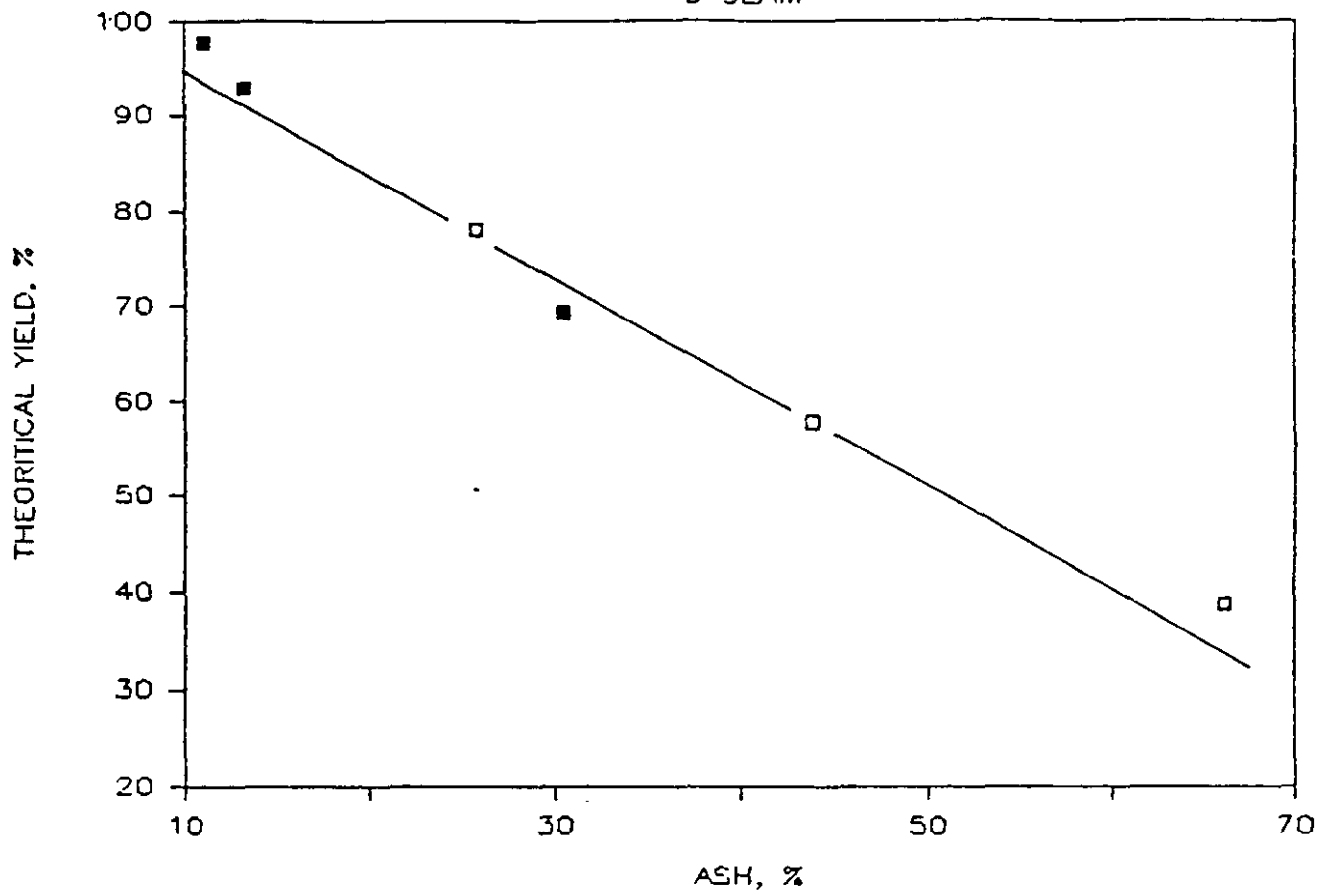


Figure 3.10

GRIZZLY/TRANSFER

D SEAM



- drill core insitu ash/yield
- estimated plant feed ash/plant yield using mine planning calculations

FIGURE 3.2

GRIZZLY/TRANSFER F SEAM

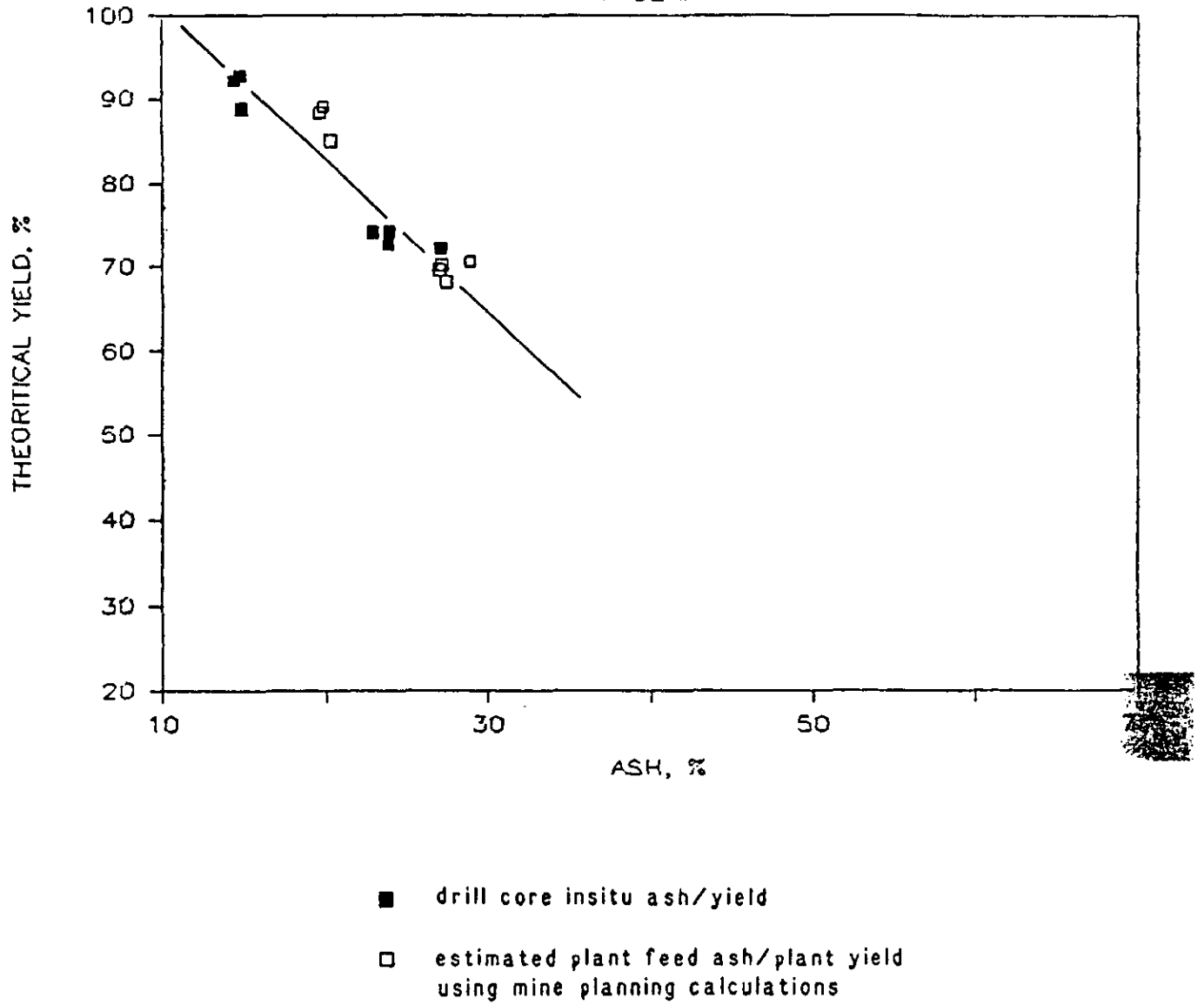
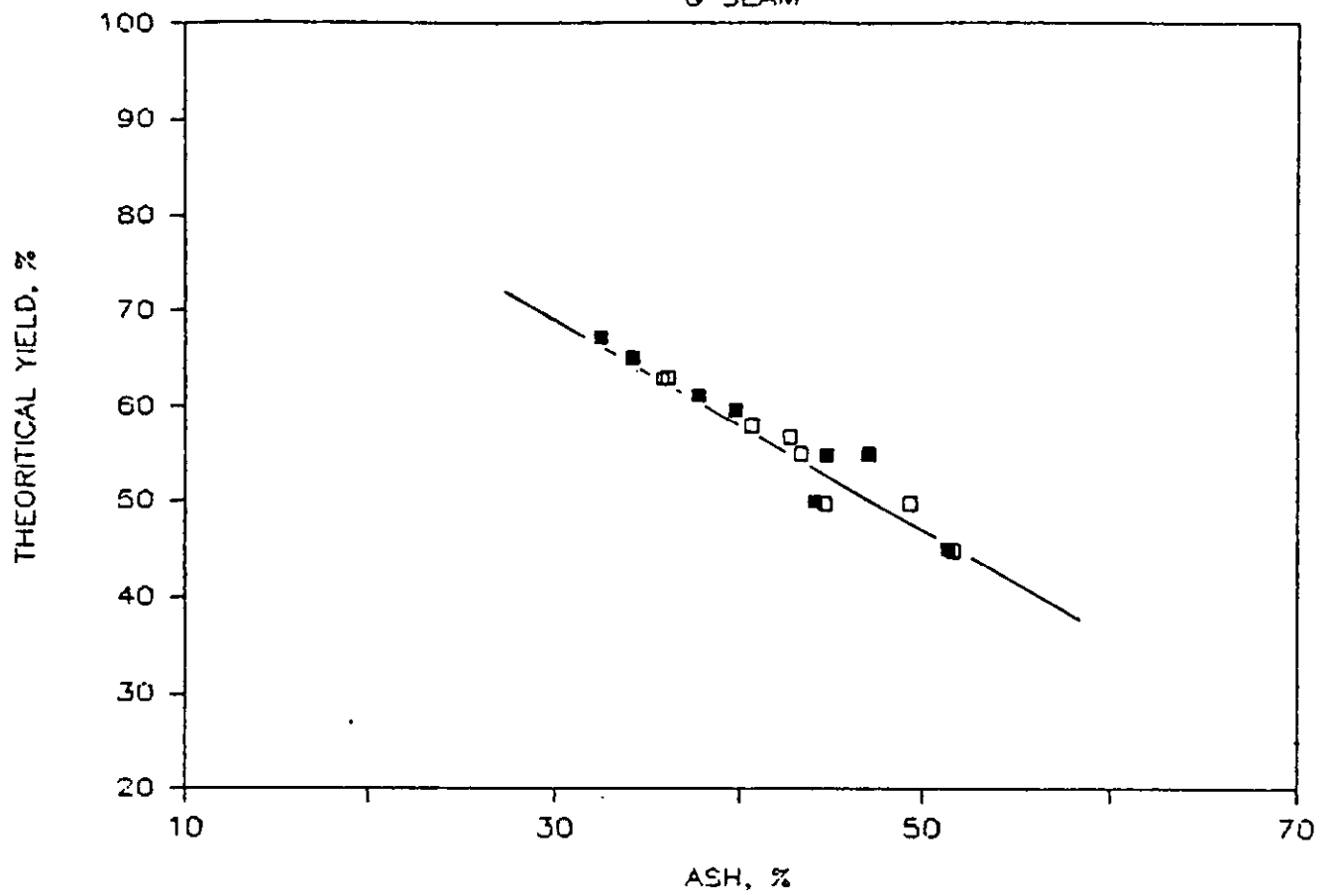


FIGURE 3.3

GRIZZLY/TRANSFER

G SEAM



- drill core insitu ash/yield
- estimated plant feed ash/plant yield using mine planning calculations

FIGURE 3.4

GRIZZLY/TRANSFER

J SEAM

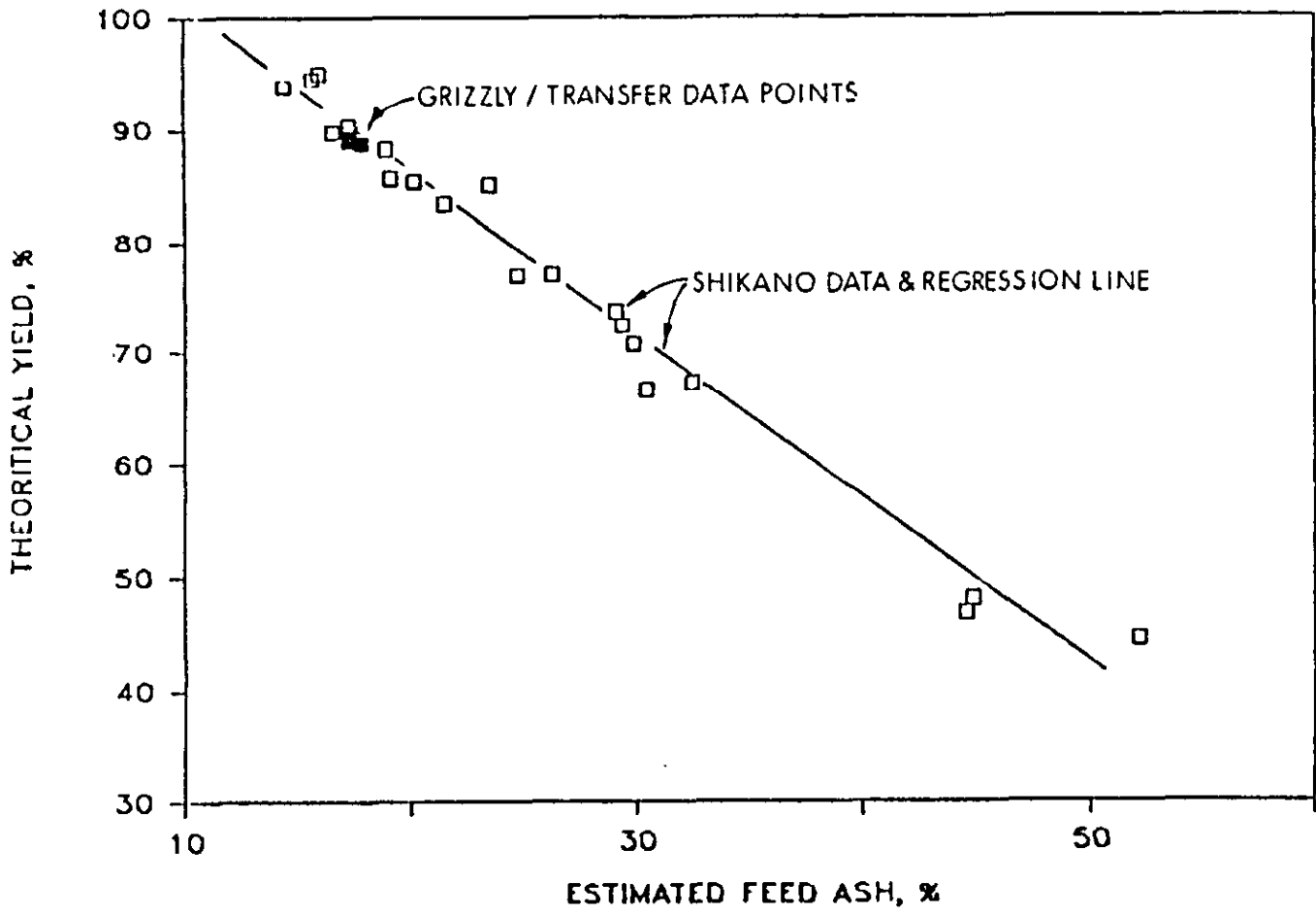
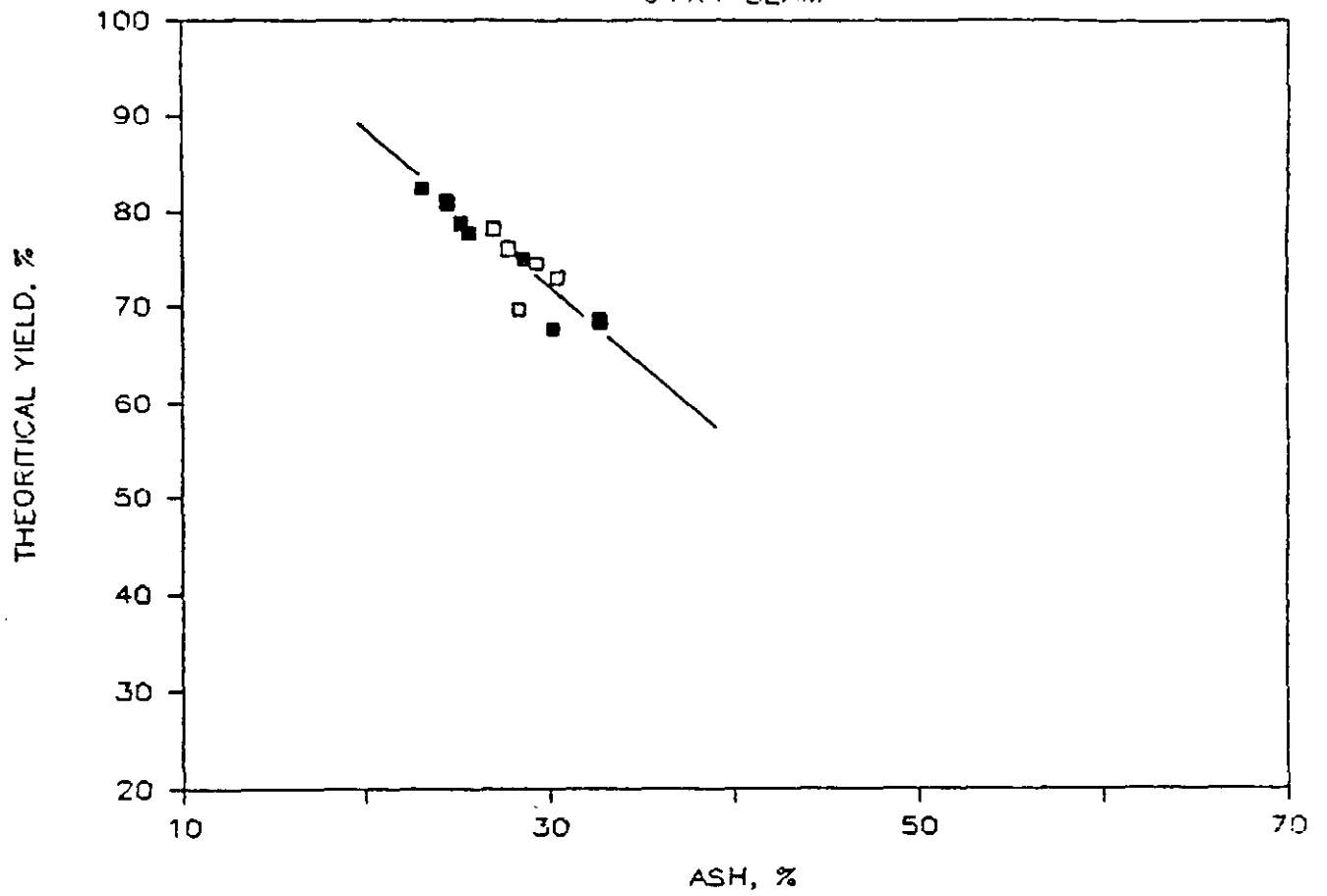


FIGURE 3.5

GRIZZLY/TRANSFER

J+K1 SEAM

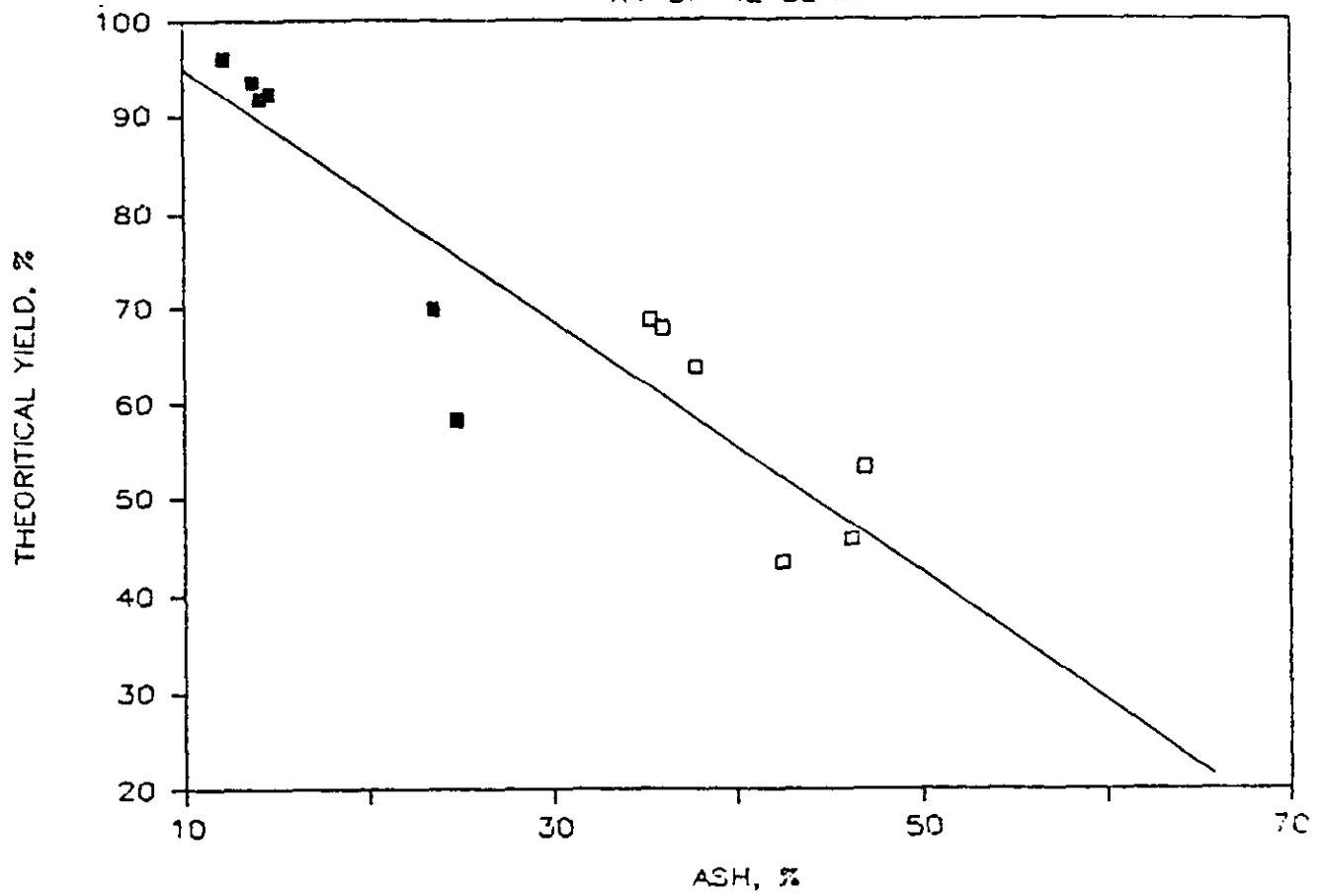


- drill core insitu ash/yield
- estimated plant feed ash/plant yield using mine planning calculations

FIGURE 3.6

GRIZZLY/TRANSFER

K1 OR K2 SEAM

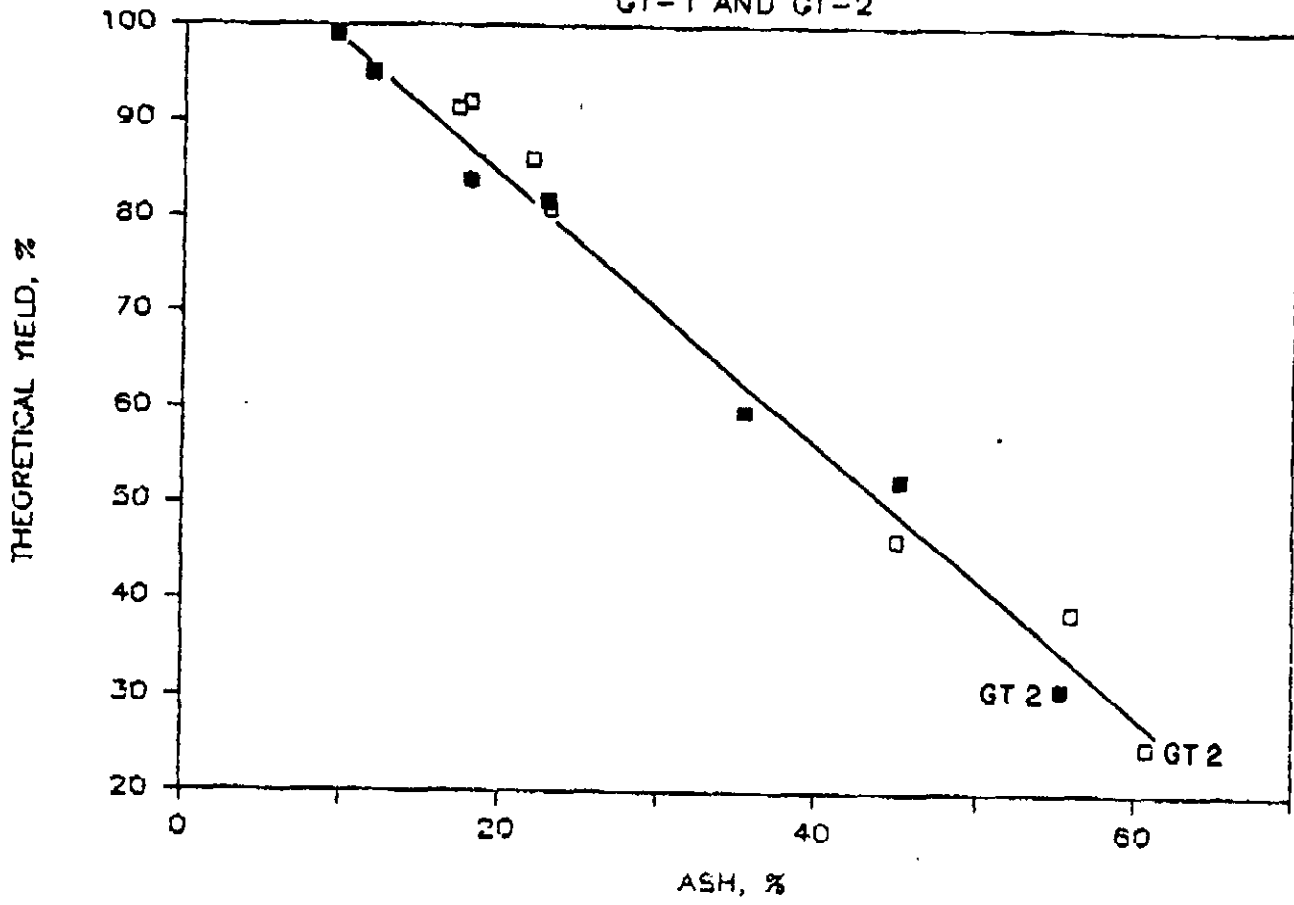


- drill core insitu ash/yield
- estimated plant feed ash/plant yield using mine planning calculations

FIGURE 3.7

GETHING

GT-1 AND GT-2



- drill core in situ ash/yield
- estimated plant feed ash/plant yield using mine planning calculations

Figure 3.8

GETHING ASH/FSI RELATIONSHIP

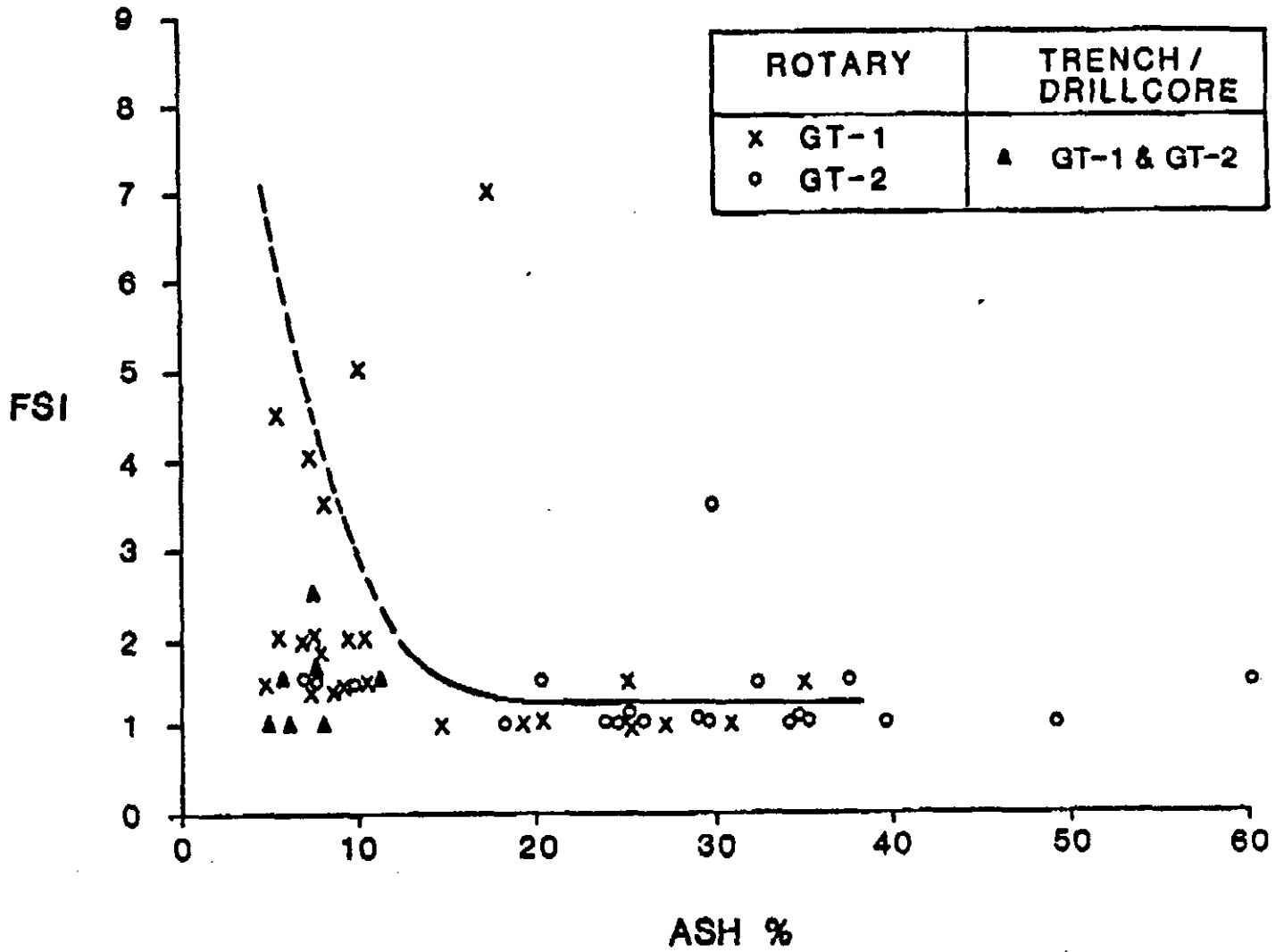
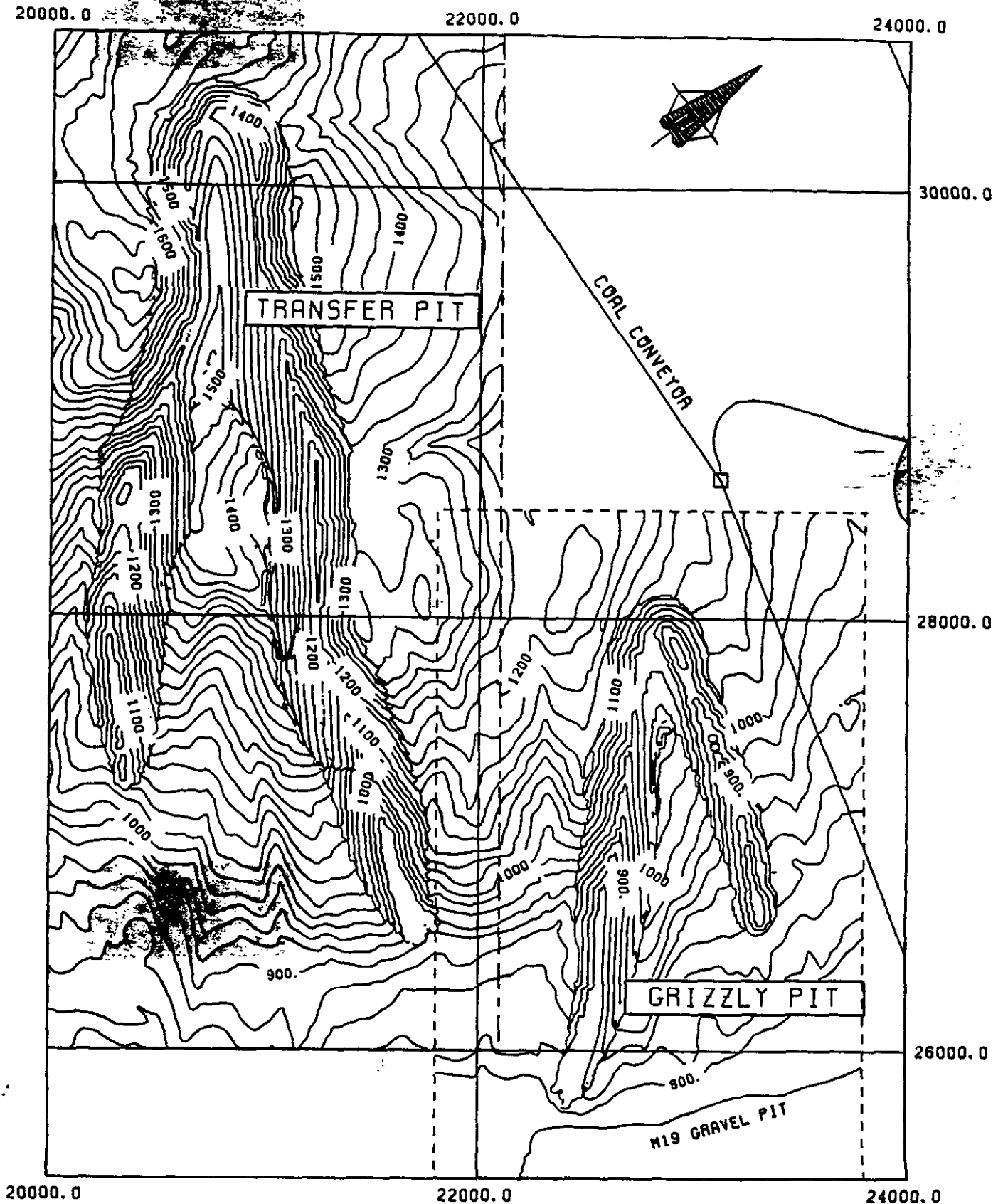


Figure 3.9

QUINETTE COAL LIMITED GRIZZLY-TRANSFER MINE AREA



11-MAR-87

SCALE 1:25000

FIGURE 4.1

5.0 CONCLUSIONS & RECOMMENDATIONS

5.1 CONCLUSIONS

- ° A preliminary evaluation of structure, coal seam development, quality, washability, and resources quantity have been made possible through the 1986 exploration programme in the Transfer and Grizzly Areas.
- ° The results of the work in the Transfer and Grizzly Area further supports the premise that a substantial resource potential, with stripping ratio lower than certain portions of the long term Wolverine mine plan, is probable. These resources appear to have similar quality to those of the Shikano deposit.
- ° During 1986, exploration work in the Gething Area allowed for the further delineation of the limits of the Gething Flat Area and for the assessment of the quality of the target seam (GT-1).
- ° Initial drilling, peripheral to the Flat Area, provided indications of extremely complicated structure at depths generally precluding the possibility of strip ratios of current interest.
- ° Most geological mapping information has now been obtained in the three target areas. future mapping information will be primarily restricted to exposure through road construction.

5.2 RECOMMENDATIONS

- ° During 1987, undertake exploration work consisting of diamond and rotary drilling to both "infill" existing drill sites and to "step out" from the currently drilled areas particularly in the vicinity of the Murray River valley in order to extend the limbs of both anticline structures.
- ° Obtain bulk samples through adits to be driven in each of the mining sections in the Transfer and Grizzly structures such that pilot scale washability and carbonization testing can be completed.
- ° Assess market potential for low tonnage supply of Gething Flat Area coal based on current quality results prior to undertaking any further field work.

QUINTEITE COAL LIMITED

TRANSFER AREA

GEOLOGICAL REPORT

**TRANSFER AREA
GEOLOGICAL REPORT**

COPY#7

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CONFIDENTIAL

APPENDIX 1

Section 1.0

APPENDIX 1
Section 1.1
Transfer Area
Natural Topographic Slope Study

APPENDIX 1

Section 1.2

**Legal Description of
Transfer Area Coal Licences**

APPENDIX 1.2

QUINTETTE COAL LIMITED

LEGAL DESCRIPTION OF TRANSFER AREA COAL LICENCES

LICENCE NO.	DATE ISSUED	SERIES	BLOCK	UNITS	AREA
3618	May 27/75	93 P /3	B	3,4,13,14	297
3660	Sept.27/76	93 P /3	B	1,2,11,12	297
7849	Aug.24/84	93 P /3	A	9,10,19,20	297
7848	Aug.24/84	93 P /3	A	7,8,17,18	297
7847	Aug.24/84	93 P /3	A	5,6,15,16	297
3346	Oct.16/74	93 I /14	J	83,84,93,94	297
3662	Sept.27/76	93 I /14	J	81,82,91,92	297
3661	Sept.27/76	93 I /14	I	90,100	149
3341	Oct.16/74	93 I /14	I	89,99	149
3340	Oct.16/74	93 I /14	I	87,88,98	223
7846	Aug.24/84	93 I /14	I	97	75
7845	Aug.24/84	93 I /14	I	96	75
3339	Oct.16/74	93 I /14	I	85,86,95	223
3343	Oct.16/74	93 I /14	J	61,62,71,72	297
3336	Oct.16/74	93 I /14	I	69,70,79,80	297
3335	Oct.16/74	93 I /14	I	67,68,77,78	297
					3,864

APPENDIX 1

Section 1.3

**Transfer Area Survey Data Tables
and Traverse Maps**

GETTING AREA

Survey Station	Description	UTM Co-ordinates		Elevations
		Northing	Easting	
QHR 86001	Rotary D.H	6095072.96	619155.10	1622.56
QHR 86002	" "	6095099.77	619125.94	1627.00
QHR 86003	" "	6095150.35	619159.36	1629.31
QHR 86004	" "	6095032.93	619326.07	1626.41
QHR 86005	" "	6095046.12	619429.14	1604.78
QHR 86006	" "	6094973.74	619423.22	1609.04
QHR 86007	" "	6094890.93	619317.76	1612.87
QHR 86008	" "	6094839.27	619347.20	1604.45
QHR 86009	" "	6094639.77	619466.96	1570.38
QHR 86010	" "	6094697.29	619424.93	1579.44
QHR 86011	" "	6094963.40	619513.03	1587.50
QHR 86012	" "	6095003.00	619492.57	1586.51
QHR 86013	" "	6094731.10	619550.24	1564.92
QHR 86014	" "	6094802.80	619712.02	1539.35
QHR 86015	" "	6094829.61	619729.99	1538.60
QHR 86016	" "	6094996.27	619685.96	1557.95
QHR 86017	" "	6094751.07	619775.69	1515.45
QHR 86018	" "	Casing not found, location by chain & compass		
QHR 86019	" "	6095364.04	619450.87	1632.26
QHR 86020	" "	6095229.27	619033.47	1619.51
QJD 7642	Diamond D.H.	6094987.64	619293.20	1627.00
QHD 86009	" "	6094896.09	619455.14	1598.15
GTT 1	Trench	6095044.10	619220.0	1620.5
GTT 2	"	6095035.0	619227.0	1625.0
GGT 1	"	6095031.5	619221.9	1621.9
QTT 86001	Trench	6095645.473	619370.128	1620.12
QTT 86002	"	6095644.367	619278.974	1603.70
QTT 86003	"	6095720.156	619215.938	1596.21

GETHING AREA

Survey Station	Description	UTM Co-ordinates		Elevations
		Northing	Easting	
QTT 86004	Trench	6095793.886	619148.717	1574.37
QHR 86021	Rotary D.H.	6095285.770	619571.301	1610.81
QHR 86022	" "	6095522.735	619535.391	1620.59
QHR 86023	" "	6095599.208	619483.754	1622.70
QHR 86024	" "	6095732.913	619306.290	1626.43
QHR 86025	" "	6095165.472	618870.375	1610.18
QHR 86026	" "	6095288.466	618712.019	1628.64
QHR 86027	" "	6095438.991	618548.523	1649.64
QHR 86028	" "	6095199.822	619006.590	1618.35
QHR 86029	" "	6095232.411	618979.294	1618.19
QHR 86030	" "	6095268.876	618888.320	1613.15
QHR 86031	" "	6095315.091	618910.638	1615.17
QHR 86032	" "	6095379.648	618825.777	1620.62
QHR 86033	" "	6095463.003	619070.240	1616.82
QHR 86034	" "	6095501.148	618908.476	1604.73
QHR 86035	" "	6095625.501	618674.980	1613.90
QHR 86036	" "	6095553.821	618447.732	1605.34
QHR 86037	" "	6095582.881	619180.654	1604.72

GRIZZLY AREA

Survey Station	Description	UTM Co-ordinates		Elevations
		Northing	Easting	
QG 1	Geol. Cont. Pt.	6096601.02	624420.00	877.74
QG 2	" " "	6096403.28	624295.71	893.84
QG 3	" " "	6096413.42	624161.95	927.84
QG 4	" " "	6096593.84	623644.90	1029.75
QG 5	" " "	6096609.47	623468.87	1055.48
QG 6	" " "	6096775.26	623293.48	1060.95
QG 7	" " "	6096147.85	623738.40	1074.35
QG 8	" " "	6095929.33	623986.12	1021.04
QG 9	" " "	6095727.33	624210.08	970.02
QG 10	" " "	6096546.92	623852.07	984.69
QG 11	" " "	6096514.02	623892.70	982.38
QHD 86001	Diamond D.H.	6096557.33	623975.75	953.93
QHD 86002	" " "	6096236.98	623500.76	1095.53*

T R A N S F E R A R E A

Survey Station	Description	UTM Co-ordinates		Elevations
		Northing	Easting	
QHS 86001	Geol. Cont. Pt	6095804.90	620020.69	1619.10
QHS 86002	" " "	6095450.28	620623.85	1629.90
QHS 86003	" " "	6095236.20	621314.87	1475.59
QHS 86004	" " "	6095297.30	621153.98	1489.26
QHS 86005	" " "	6095442.51	620986.15	1526.35
QHS 86006	" " "	6095402.32	620958.73	1512.97
QHS 86007	" " "	6095611.08	620851.21	1549.12
QHS 86008	" " "	6095356.76	620619.56	1618.75
QHS 86009	" " "	6095233.87	620549.12	1570.08
QHS 86010	" " "	6095158.50	620648.23	1548.13
QHS 86011	" " "	6095204.48	621464.98	1456.00
QHS 86012	" " "	6095096.77	621555.57	1413.06
QHS 86013	" " "	6095124.88	621616.91	1427.92
QHS 86014	" " "	6095221.62	621620.67	1444.50
QHS 86015	" " "	6096359.58	620912.84	1504.38
QHS 86016	" " "	6094350.33	621321.77	1279.49
QHS 86050	" " "	6095077.41	621037.70	1335.92
QHS 86051	" " "	6094873.12	621069.58	1249.33
P 1	" " "	6096077.83	620508.79	1583.18
P 2	" " "	6096047.04	620425.87	1578.46
P 3	" " "	6096018.64	620374.79	1591.61
P 4	" " "	6095985.80	620333.40	1597.10
P 5	" " "	6095858.73	620215.57	1621.54
P 6	" " "	6095621.11	619892.57	1648.75
P 7	" " "	6095669.14	619555.28	1640.56
P 8	" " "	6095503.39	619520.19	1617.54
P 9	" " "	6095244.54	619607.75	1597.42
P 10	" " "	6095058.71	619547.24	1584.59

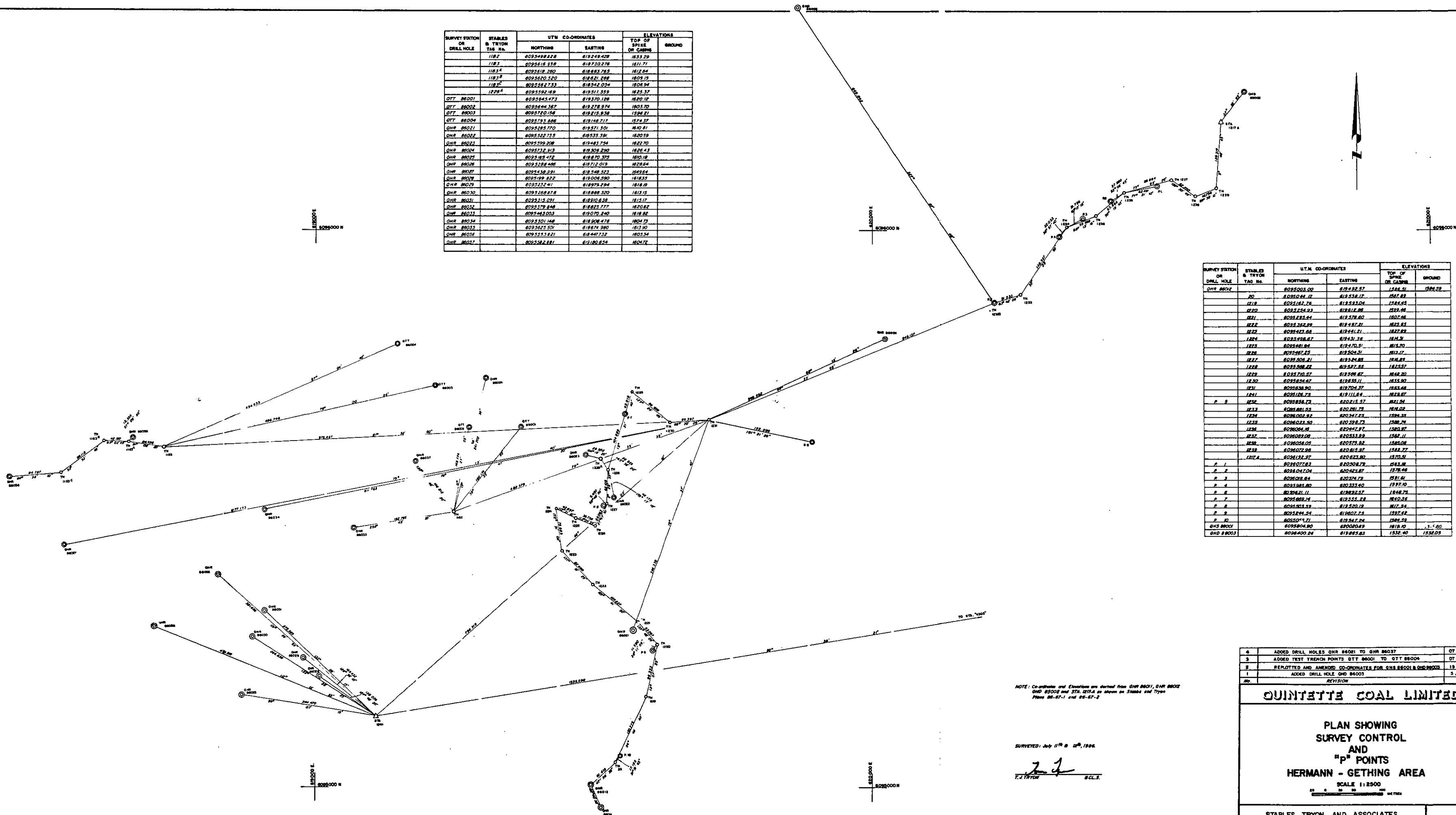
T R A N S F E R A R E A

Survey Station	Description	UTM Co-ordinates		Elevations
		Northing	Easting	
QHD 85001	Diamond D.H.	6095479.72	620842.46	1543.20
QHD 85002	" "	6096247.89	620665.99	1549.97
QHD 86003	" "	6096400.24	619865.63	1532.40
QHD 86004	" "	6095039.71	621025.49	1328.95
QHD 86005	" "	6095040.51	621025.89	1329.25
QHD 86006	" "	6095648.46	621718.59	1325.06
QHD 86007	" "	6095276.73	622427.33	1292.95
QHD 86008	" "	6095971.61	621225.68	1413.39

S O U T H G E T H I N G

Survey Station	Description	UTM Co-ordinates		Elevations
		Northing	Easting	
QGS 86001	Geol. Cont. Pt.	6093913.03	616744.15	1434.07
QGS 86002	" " "	6094537.28	616643.70	1369.73
QGS 86003	" " "	6093739.15	616643.79	1396.26
QGS 86004	" " "	6094297.63	616431.63	1323.83
QGS 86005	" " "	6092987.61	617366.42	1388.84
QGS 86006	" " "	6093317.78	617396.83	1373.12

SURVEY STATION OR DRILL HOLE	STABLES OR TRYON TAG No.	UTM CO-ORDINATES		ELEVATIONS	
		NORTHING	EASTING	TOP OF SPIKE OR CASING	GROUND
118.2	8095498.828	619249.428	1633.29		
118.3	8095416.838	618730.278	1611.71		
118.3 ^A	8095418.282	618853.782	1612.84		
118.3 ^B	8095520.520	618621.288	1609.15		
118.3 ^C	8095522.733	618542.054	1608.94		
1228 ^A	8095592.189	619311.359	1625.37		
OTT 86001	8095645.473	619370.128	1620.12		
OTT 86002	8095644.367	619278.974	1603.70		
OTT 86003	8095720.156	619215.938	1596.21		
OTT 86004	8095793.886	619148.717	1574.37		
QHR 86021	8095185.770	619371.301	1610.81		
QHR 86022	8095322.735	619535.391	1620.59		
QHR 86023	8095359.208	619483.754	1622.70		
QHR 86024	8095732.913	619308.290	1626.43		
QHR 86025	8095182.472	618870.373	1610.18		
QHR 86026	8095218.486	618712.019	1628.64		
QHR 86027	8095438.591	618548.523	1649.64		
QHR 86028	8095199.822	619006.580	1618.33		
QHR 86029	8095232.411	618978.294	1618.19		
QHR 86030	8095288.878	618888.320	1613.15		
QHR 86031	8095315.021	618910.638	1613.17		
QHR 86032	8095379.848	618825.777	1620.82		
QHR 86033	8095463.003	619070.240	1618.82		
QHR 86034	8095301.148	618508.478	1604.73		
QHR 86035	8095425.501	618674.980	1613.90		
QHR 86036	8095553.821	618447.732	1603.34		
QHR 86037	8095582.881	619180.854	1604.72		



SURVEY STATION OR DRILL HOLE	STABLES OR TRYON TAG No.	UTM CO-ORDINATES		ELEVATIONS	
		NORTHING	EASTING	TOP OF SPIKE OR CASING	GROUND
QHR 86038	8095001.02	619482.27	1586.31	1586.29	
20	8095044.12	619538.12	1587.82		
1219	8095182.76	619593.04	1584.43		
1220	8095254.93	619618.88	1593.98		
1221	8095293.44	619578.60	1602.46		
1222	8095352.99	619497.21	1623.83		
1223	8095423.88	619441.21	1627.82		
1224	8095498.67	619431.38	1616.31		
1225	8095481.84	619470.51	1615.70		
1226	8095467.25	619504.51	1613.17		
1227	8095508.21	619524.83	1616.83		
1228	8095588.22	619527.54	1623.57		
1229	8095710.57	619598.67	1648.30		
1230	8095854.67	619635.11	1653.90		
1231	8095836.90	619704.37	1663.68		
1231	8095126.73	619111.84	1618.67		
P 8	8095858.73	620213.57	1641.04		
1232	8095881.53	620281.79	1618.02		
1233	8095902.92	620267.23	1598.31		
1234	8096023.50	620298.73	1598.74		
1235	8096064.18	620447.97	1580.97		
1236	8096089.04	620533.89	1582.11		
1237	8096258.05	620575.82	1586.08		
1238	8096272.88	620612.97	1584.27		
1238 ^A	8096134.97	620623.80	1570.51		
P 1	8096177.82	620608.79	1648.30		
P 2	8096047.04	620442.87	1578.58		
P 3	8096081.84	620375.79	1581.61		
P 4	8095981.80	620332.60	1577.10		
P 5	8096211.11	619823.47	1648.75		
P 6	8095881.14	619555.28	1640.56		
P 7	8096033.13	619520.19	1617.54		
P 8	8095844.54	619802.73	1597.82		
P 9	8095504.71	619542.24	1596.58		
QHS 86001	8095804.80	620000.89	1618.10	15.60	
QHD 86003	8096400.24	619865.83	1532.40	1532.09	

NOTE: Co-ordinates and Elevations are derived from QHR 86021, QHR 86022, QHD 85002 and STA. 227-A as shown on Stables and Tryon Plans 86-67-1 and 86-67-2

SURVEYED: July 11th & 12th, 1966

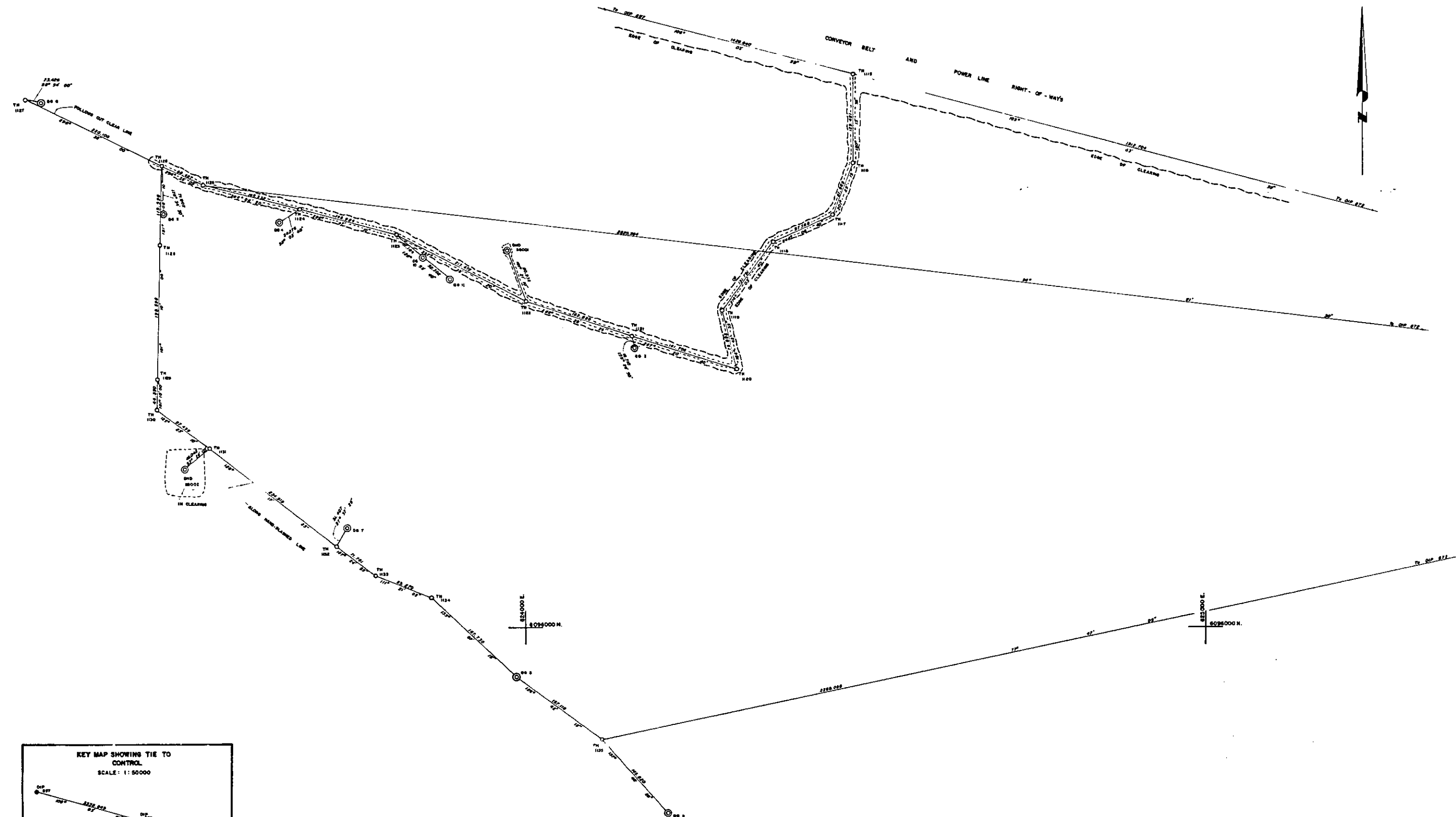
T. J. Tryon
T. J. TRYON B.C.L.S.

4	ADDED DRILL HOLES QHR 86021 TO QHR 86027	07 / 10 / 66
3	ADDED TEST TRENCH POINTS OTT 86001 TO OTT 86004	07 / 10 / 66
2	REPLOTTED AND AMENDED CO-ORDINATES FOR QHR 86001 & QHR 86002	12 / 8 / 66
1	ADDED DRILL HOLE QHD 84003	3 / 8 / 66
REV.	REVISION	DATE

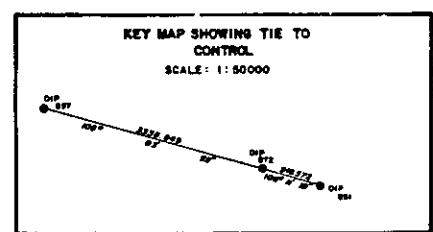
QUINTETTE COAL LIMITED

PLAN SHOWING
SURVEY CONTROL
AND
"P" POINTS
HERMANN - GETTING AREA

SCALE 1:2500



SURVEY STATION OR DRILL HOLE	STABLES & TRYON TAG NO.	U.T.M. CO-ORDINATES		ELEVATIONS	
		NORTHING	EASTING	TOP OF SPIKE OR CASING	GROUND
OP 857	1115	8097182.84	823105.77		
	1116	8098812.23	824482.80	858.84	
OP 872	1117	8098315.21	824329.18	850.34	
	1118	8098882.80	824482.31	857.88	
	1117	8098608.35	824452.29	872.21	
	1118	8098587.08	824363.11	873.27	
	1119	8098827.21	824288.72	888.11	
	1120	8098380.87	824310.38	893.33	
	1121	8098429.06	824158.09	892.30	
	1122	8098480.87	824001.82	931.24	
	1123	8098379.11	823816.30	932.29	
	1124	8098148.81	823778.74	1022.86	
	1125	8098851.83	823529.24	1044.84	
	1126	8098880.42	823487.10	1050.23	
	1127	8098778.88	823270.34	1081.82	
	1128	8098584.87	823484.81	1071.89	
	1129	8098386.35	823480.77	1087.00	
	1130	8098322.02	823459.87	1101.83	
	1131	8098265.37	823259.32	1081.88	
	1132	8098180.03	823233.84	1082.32	
	1133	8098078.44	823280.62	1039.04	
	1134	8098033.22	823283.72	1052.31	
	1135	8098855.80	824111.21	1003.45	
OG 1		8098802.02	824420.00	877.74	877.82
OG 2		8098403.88	824255.71	881.84	882.84
OG 3		8098413.42	824161.32	927.84	927.84
OG 4		8098153.84	823864.90	1028.72	
OG 5		8098809.47	823488.87	1052.48	
OG 6		8098773.88	823283.88	1080.26	
OG 7		8098147.85	823238.40	1074.32	
OG 8		8098329.33	823388.12	1011.04	
OG 9		8098127.33	824200.08	850.02	
OG 10		8098148.82	823854.07	844.82	
OG 11		8098514.02	823894.70	848.28	
Q.M. 88001		8098557.33	823973.79	923.23	
Q.M. 88002		8098226.88	823800.76		1022.32
OP 851		8098058.11	827211.23		



- NOTES:
- 1) Coordinates and Bearings are derived from M'Elhenny Coordinates for Stations 851 and 857.
 - 2) Elevations are derived from M'Elhenny Bench Mark 1003. Elevation = 850.31
 - 3) OG Points are Marked by O.B.I. & O.D. Rebar.

Surveyed:
July 22nd to July 25th, 1986.

T.J. TRYON S.C.L.S.

QUINTETTE COAL LIMITED

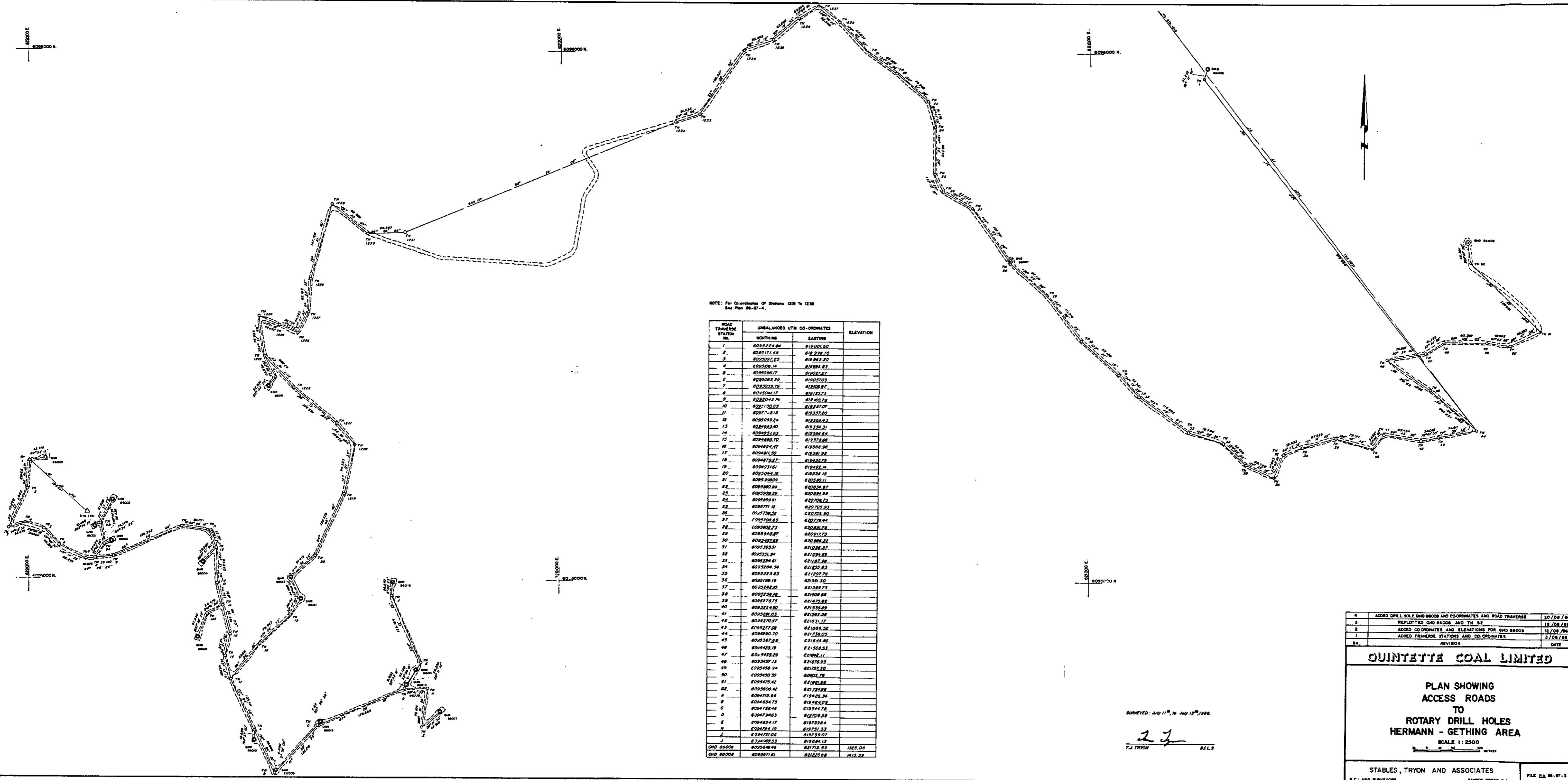
**PLAN SHOWING
SURVEY CONTROL
AND
ROTARY DRILL HOLES
GRIZZLY AREA**

SCALE 1:2500

STABLES, TRYON AND ASSOCIATES

B.C.L.A.M. 93 DAWSON CREEK, B.C.

P.L.P. No. 84-87-5



NOTE: For Coordinates Of Stations 1219 To 1236 See Plan 88-67-4.

ROAD TRAVERSE STATION No.	UNBALANCED UTM CO-ORDINATES		ELEVATION
	NORTHING	EASTING	
1	6095224.84	619001.50	
2	6095171.48	618998.70	
3	6095097.25	618962.20	
4	6095066.14	618983.83	
5	6095026.17	619027.27	
6	6095063.39	619027.03	
7	6095039.79	619006.97	
8	6095041.17	619133.73	
9	6095043.14	619190.24	
10	6095100.03	619141.07	
11	6095112.13	619332.80	
12	6095058.24	619354.13	
13	6095033.40	619354.31	
14	6095051.93	619364.84	
15	6095025.70	619374.88	
16	6095054.41	619388.94	
17	6095011.50	619381.92	
18	6095076.27	619433.73	
19	6095039.91	619532.24	
20	6095048.12	619538.12	
21	6095080.09	620580.11	
22	6095080.89	620634.97	
23	6095008.59	620894.98	
24	6095059.81	620706.72	
25	6095077.12	620705.83	
26	60950736.52	620725.80	
27	6095008.69	620778.44	
28	6095008.23	620881.24	
29	6095044.87	620917.12	
30	6095052.89	620908.24	
31	6095093.51	621058.37	
32	6095331.94	621094.83	
33	6095294.81	621182.98	
34	6095264.54	621258.83	
35	6095223.83	621297.78	
36	6095198.19	621351.30	
37	6095242.10	621389.73	
38	6095258.98	621408.88	
39	6095278.73	621470.88	
40	6095294.90	621530.24	
41	6095281.05	621582.98	
42	6095270.27	621631.17	
43	6095277.08	621664.52	
44	6095290.70	621738.05	
45	6095367.88	621845.80	
46	6095423.19	621968.83	
47	6095433.29	621982.11	
48	6095487.13	621678.25	
49	6095456.94	621797.10	
50	6095490.80	621803.78	
51	6095475.43	621948.88	
52	6095406.44	621794.84	
A	6094715.98	619426.81	
B	6094634.73	619484.02	
C	6094726.44	619544.78	
D	6094794.63	619704.58	
E	6094854.17	619739.84	
H	6094794.10	619731.32	
J	6094721.05	619739.07	
K	6094854.13	619804.13	
QHD 88008	6095448.44	621718.59	1325.08
QHD 88009	6095971.81	621823.88	1412.32

SURVEYED: July 11th to July 13th 1988.

T.J. TRYON S.C.L.S.

4	ADDED DRILL HOLE QHD 88008 AND COORDINATES AND ROAD TRAVERSE	20/08/88
3	REPLOTTED QHD 88008 AND TH 51	19/08/88
2	ADDED COORDINATES AND ELEVATIONS FOR QHD 88008	12/08/88
1	ADDED TRAVERSE STATIONS AND CO-ORDINATES	3/08/88
NO.	REVISION	DATE

QUINTETTE COAL LIMITED

**PLAN SHOWING
ACCESS ROADS
TO
ROTARY DRILL HOLES
HERMANN - GETTING AREA**

SCALE 1:2500

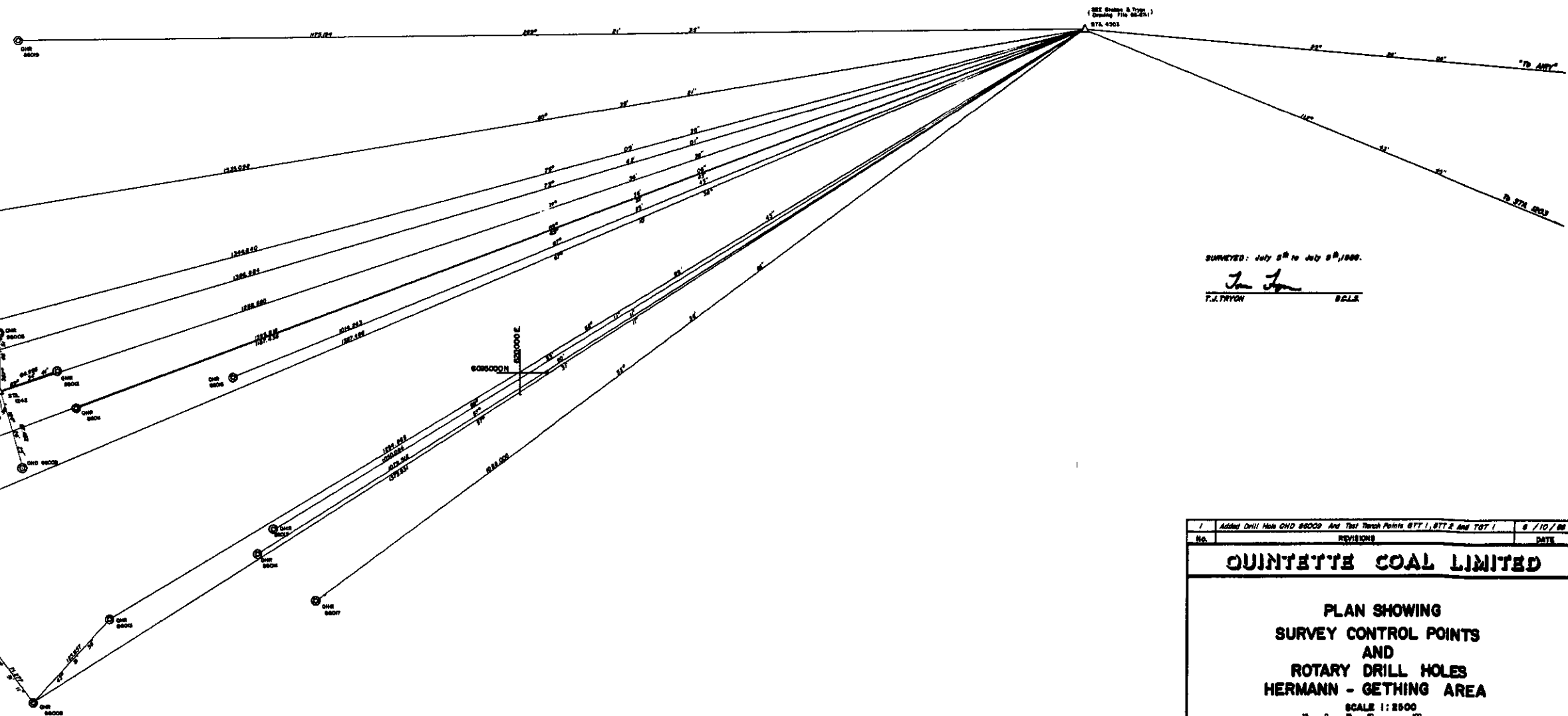
0 10 20 METRES

818000 E
809000 N

809000 N
809000 E

SURVEY STATION OR DRILL HOLE	STABLES & TRYON TAG No.	U.T.M. CO-ORDINATES		ELEVATION	
		NORTHING	EASTING	TOP OF IRON BAR OR GAMING	GROUND
4307		8093377.20	820625.43	1823.77	
4341		8094226.73	819111.84	1823.87	
4342		8094280.33	819431.68	1828.59	
QHR 80001		8094072.36	819153.10	1822.26	1822.31
QHR 80002		8094029.77	819123.24	1822.00	1822.50
QHR 80003		8094150.35	819152.38	1823.31	1823.07
QHR 80004		8094032.83	819328.07	1822.51	1822.71
QHR 80005		8094046.12	819428.14	1824.78	1824.80
QHR 80006		8094173.74	819443.22	1829.04	1828.22
QHR 80007		8094200.83	819312.78	1818.87	1818.70
QHR 80008		8094232.27	819347.20	1824.43	1824.22
QHR 80009		8094333.77	819468.26	1820.38	1820.24
QHR 80010		8094427.22	819424.24	1822.42	1822.28
QHR 80011		8094461.80	819314.03	1827.80	1827.30
QHR 80012		8094000.000	819432.27	1828.87	1828.29
QHR 80013		8094731.10	819550.24	1824.82	1824.67
QHR 80014		8094802.80	819712.02	1819.33	1819.18
QHR 80015		8094828.81	819729.22	1818.80	1818.44
QHR 80016		8094826.27	819883.26	1827.84	1827.80
QHR 80017		8094751.07	819773.80	1813.43	1813.28
QHR 80018					
QHR 80019		8094364.07	819450.87	1822.28	1822.02
QHR 80020		8094222.27	819033.67	1818.51	1818.44
QHD 7812		8094222.24	819222.20	1822.00	1822.00
QHD 80029		8094222.24	819455.14	1822.15	1822.15
BT 1		8093044.10	819210.0	1820.5	
BT 2		8093033.0	819217.0	1822.0	
BT 3		8093031.3	819217.9	1821.9	

818000 E
809000 N



SURVEYED: July 5th to July 8th, 1986.

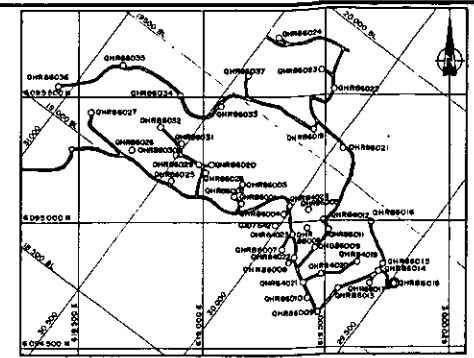
F. J. Fryon
F. J. FRYON B.E.L.

1. Added Drill Hole QHD 80029 And Test Trench Points BT 1, BT 2 and BT 3		6/10/86
No.	REVISIONS	DATE
QUINETTE COAL LIMITED		
PLAN SHOWING SURVEY CONTROL POINTS AND ROTARY DRILL HOLES HERMANN - GETTING AREA SCALE 1:2500 <small>0 10 20 METERS</small>		
STABLES, TRYON AND ASSOCIATES		86-87-2
<small>S.D. LAM</small>	<small>ORS</small>	<small>CARSON CREEK, S.C.</small>

APPENDIX 1

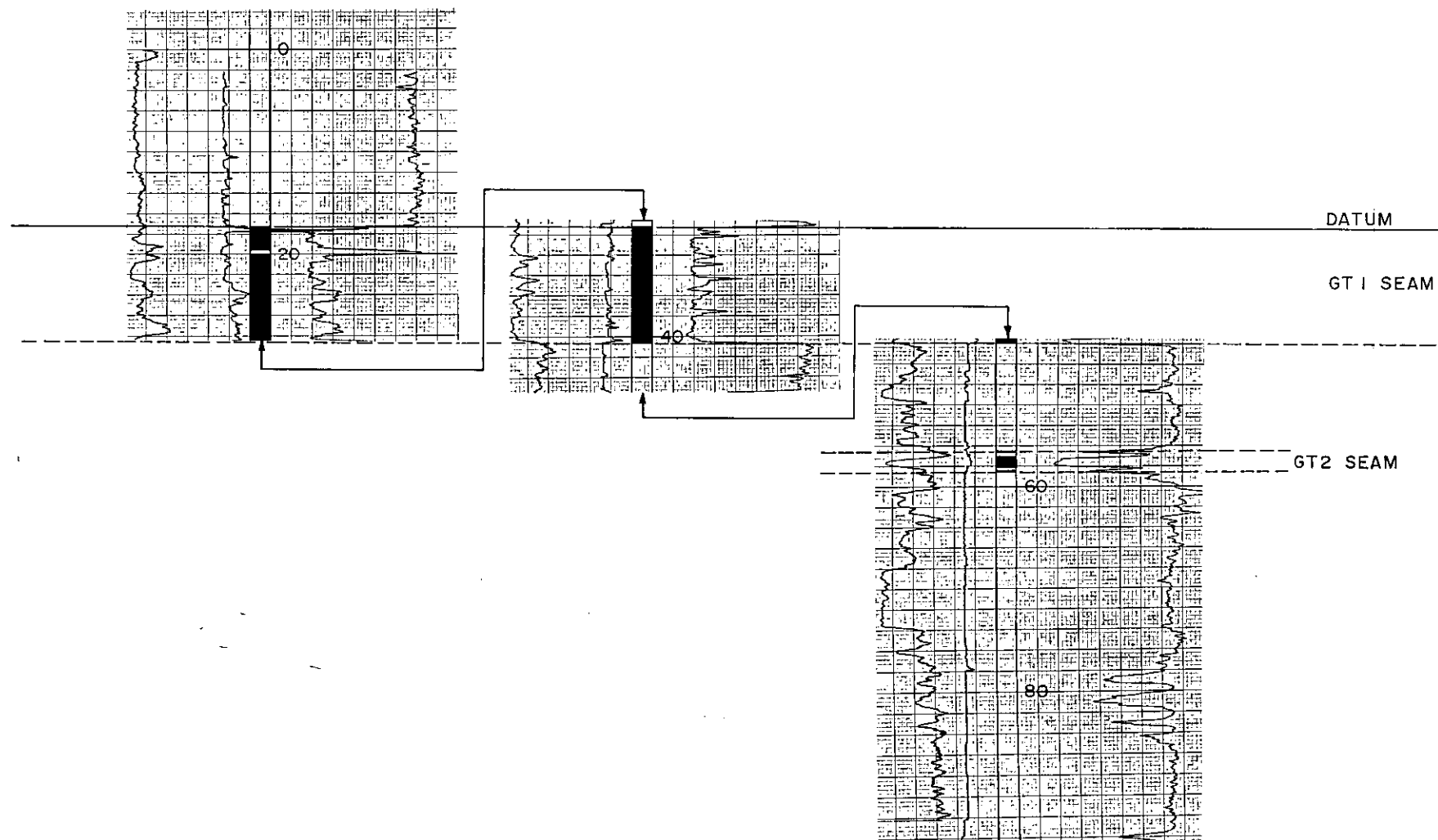
Section 2.1

**Gething Area Geophysical
Drill Hole Geophysical Log Correlation
of Coal Bearing Section**

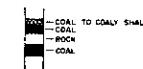


GETHING AREA LOCATION MAP
1:10000 SCALE

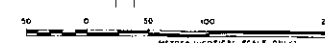
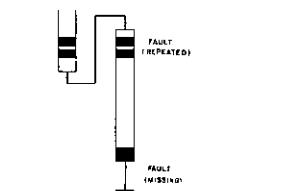
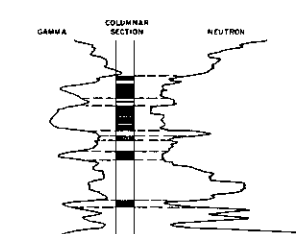
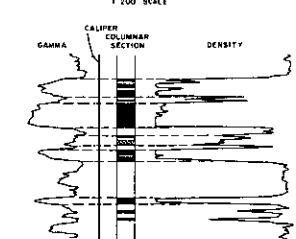
QHR 86018



LEGEND



GEOPHYSICAL LOGS
1:200 SCALE



NOTE: 1) ALL THICKNESSES ARE APPARENT.
2) ADDITIONAL BOREHOLE GEOPHYSICAL DATA IS AVAILABLE FOR MOST HOLES.
3) GAMMA/NEUTRON LOGS USED ONLY WHEN DENSITY LOG IS NOT AVAILABLE.

Rev.	D	M	Y	Revision Description	HB	HW
0	28	11	84	ORIGINAL DRAFT		

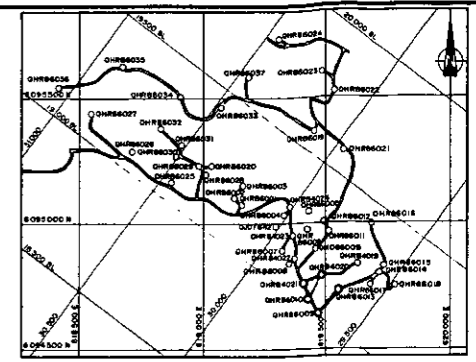
QUINTETTE COAL LIMITED
Project Manager
DENISON MINES LIMITED
COAL DIVISION

Area: **GETHING** Category: **CORRELATION**

Drawing Title:
**GETHING AREA
DRILL HOLE GEOPHYSICAL LOG
CORRELATION OF COAL-BEARING
SECTION**

Scale: **1:200(VERT.)**
Drawing No.: **86-605-26-011**
Rev.: **0**

SHEET 1 of 12



GETHING AREA LOCATION MAP
1:10000 SCALE

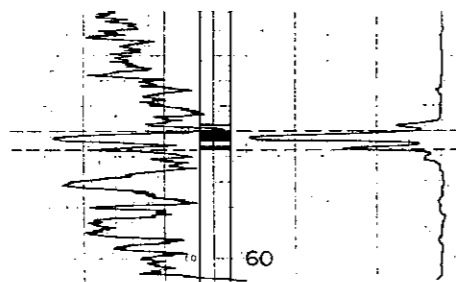
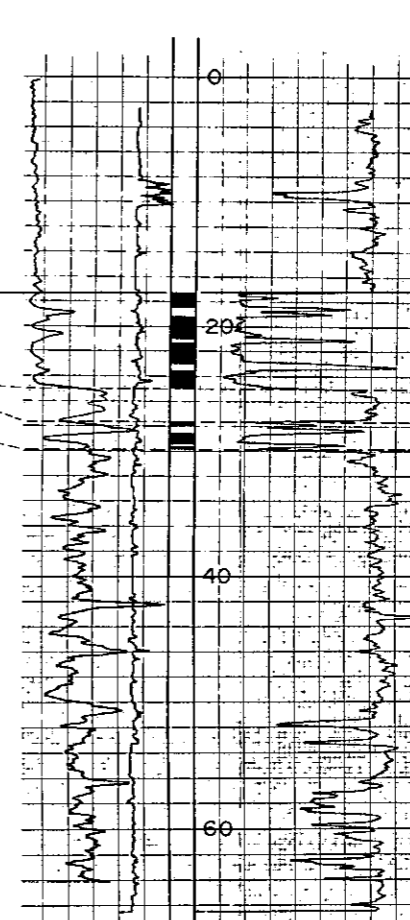
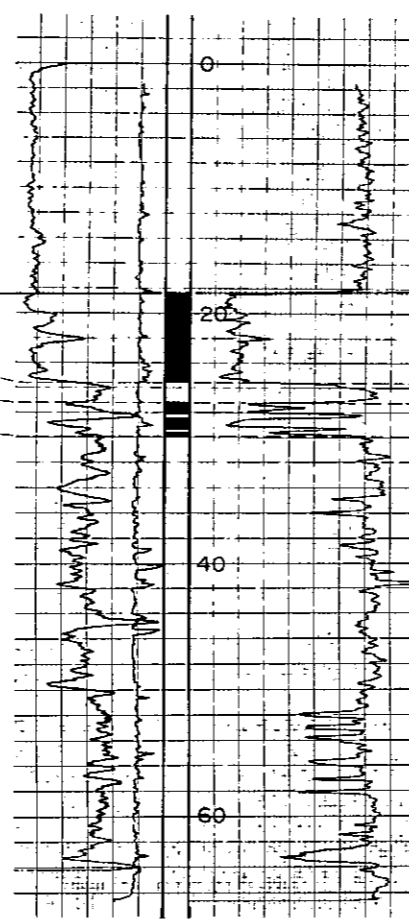
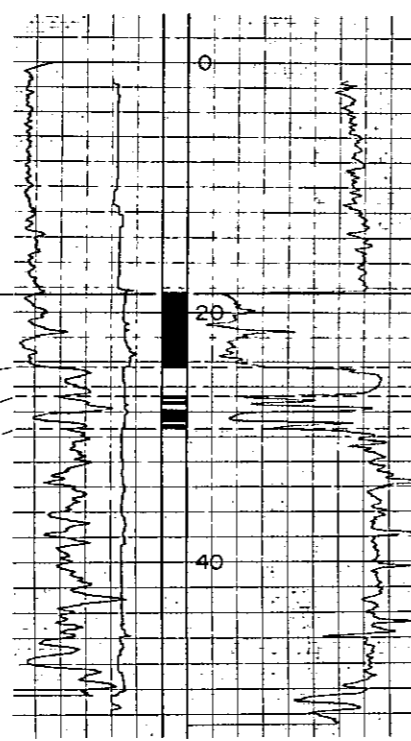
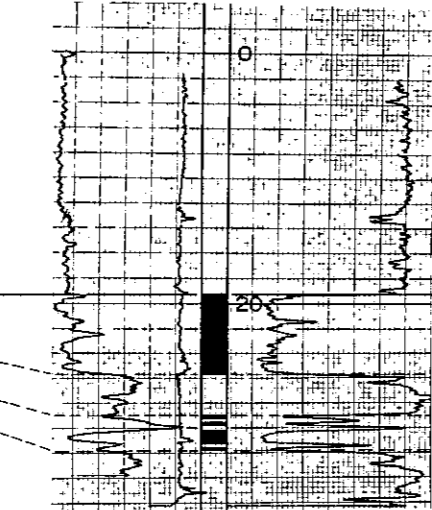
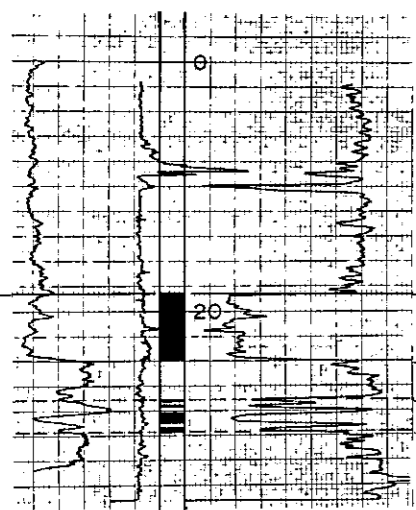
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QHR 84020

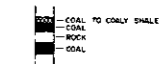
QHR 86010

QHR86009

QHR86013



LEGEND

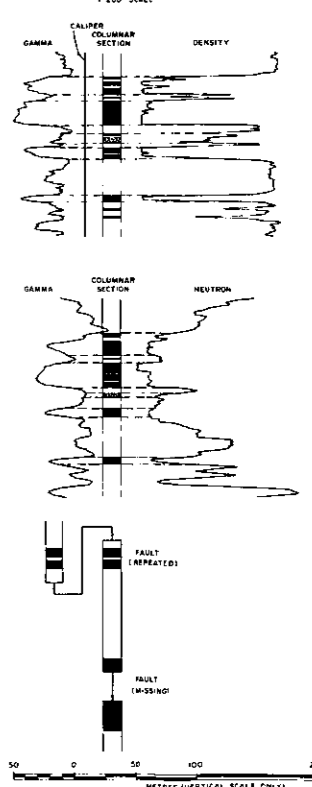


DATUM

GT1 SEAM

GT2 SEAM

GEOPHYSICAL LOGS
1:200 SCALE



NOTE: 1) ALL THICKNESSES ARE APPARENT
2) ADDITIONAL BOREHOLE GEOPHYSICAL DATA IS AVAILABLE FOR MOST HOLES
3) GAMMA/NEUTRON LOGS USED ONLY WHEN DENSITY LOG IS NOT AVAILABLE

Rev.	D.	M.	Y.	Revision Description	Drn.	Des.	App.
0	28	11	88	ORIGINAL DRAFT			

QUINTETTE COAL LIMITED
Project Manager
DENISON MINES LIMITED
COAL DIVISION

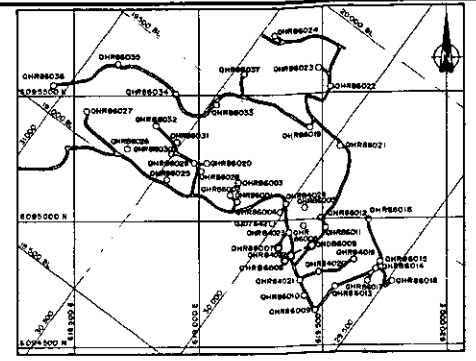
Area: **GETHING** Category: **CORRELATION**

Drawing Title:
**GETHING AREA
DRILL HOLE GEOPHYSICAL LOG
CORRELATION OF COAL-BEARING
SECTION**

Scale: 1:200(VERT)
HORIZONTAL NOT TO SCALE

Drawing No. 86-605-26-013
Rev. 0

SHEET 3 of 12



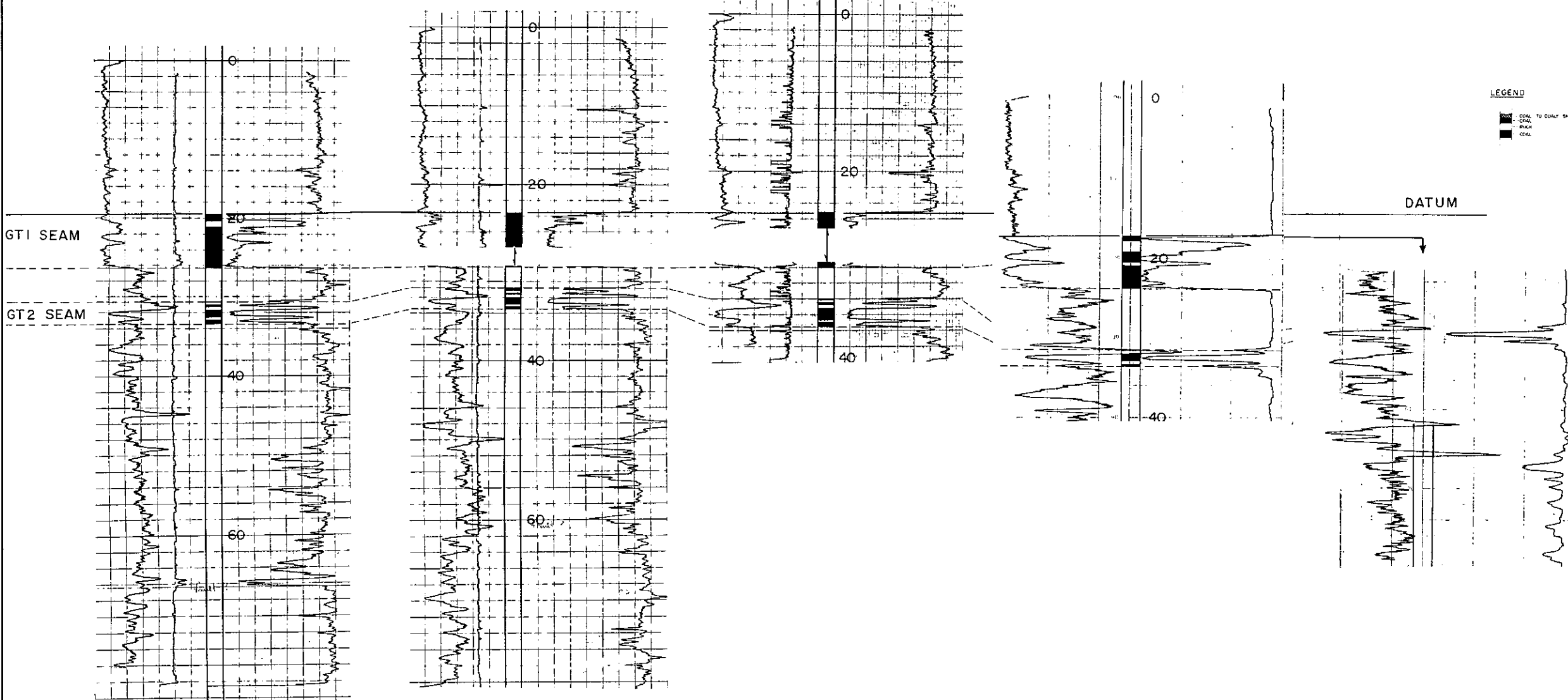
GETHING AREA LOCATION MAP
1:10000 SCALE

QHR 86007

QHR 86008

QHR 84022

QHD 86009



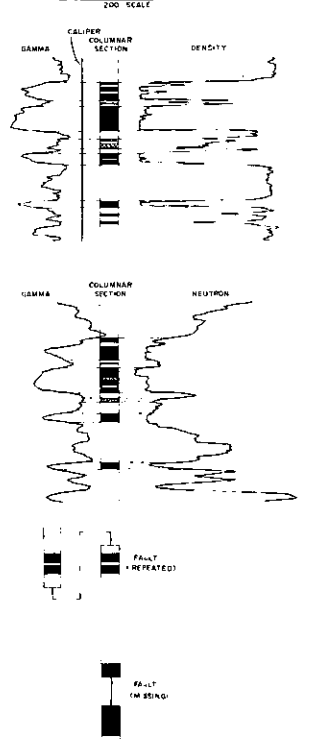
GT1 SEAM

GT2 SEAM

LEGEND

- COAL TO COALY SHALE
- COAL
- SHALE
- COAL

GEOPHYSICAL LOGS



NOTE: ALL THICKNESSES ARE APPROXIMATE
 1. ALLY MAX. HOLEWIRE LOGGING DATA IS AVAILABLE
 2. FOR UP TO 100m
 3. GAMMA NEUTRON LOGS USED ONLY WHEN DENSITY LOG IS NOT AVAILABLE

Rev.	Dr.	Des.	App.
1	DMY		

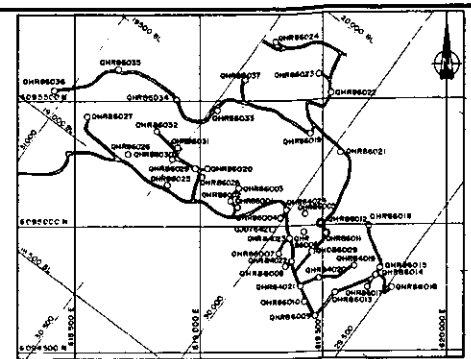
QUINTETTE COAL LIMITED
 Project Manager
DENISON MINES LIMITED
 COAL DIVISION

Area: **GETHING** Category: **CORRELATION**

Drawing Title
GETHING AREA
DRILL HOLE GEOPHYSICAL LOG
CORRELATION OF COAL-BEARING
SECTION

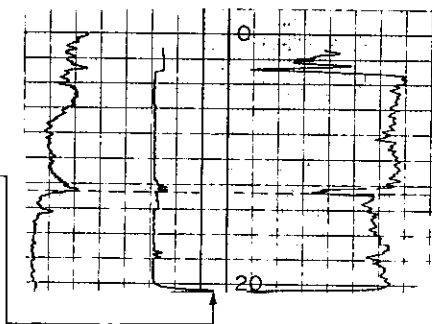
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 Drawing No: **86-605-26-014**
 Rev: **0**

SHEET 4 of 12

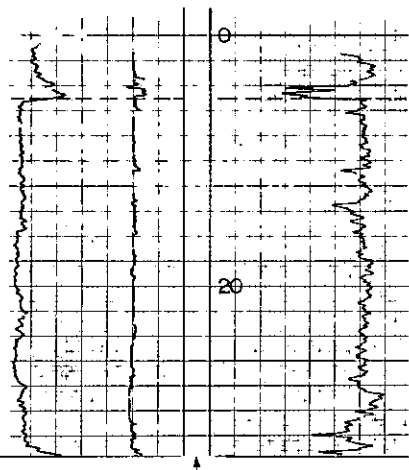


GETHING AREA LOCATION MAP
1:10000 SCALE

QHR 86012



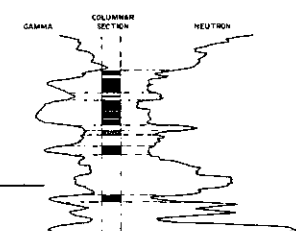
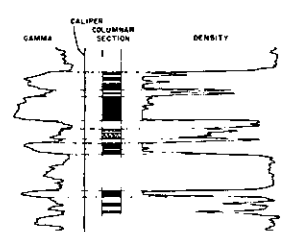
QHR 86011



LEGEND

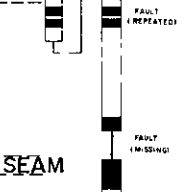
- COAL TO COALY SHALE
- COAL
- ROCK
- COAL

GEOPHYSICAL LOGS



GT1 SEAM

GT2 SEAM



0 50 100 200
METRES (VERTICAL SCALE ONLY)

NOTE: 1) ALL THICKNESSES ARE APPARENT
2) ADDITIONAL BOREHOLE GEOPHYSICAL DATA IS AVAILABLE FOR MOST HOLES
3) GAMMA/NEUTRON LOGS USED ONLY WHEN DENSITY LOG IS NOT AVAILABLE

Rev.	Date	Description	By	App.
0	28/1/86	ORIGINAL DRAFT	JHB	NW

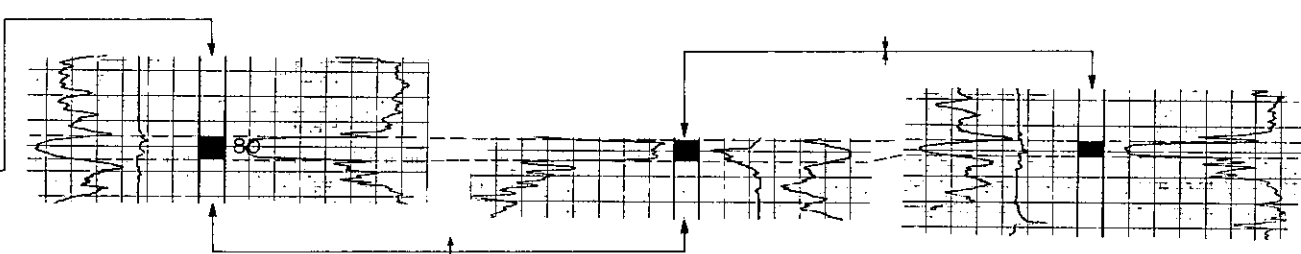
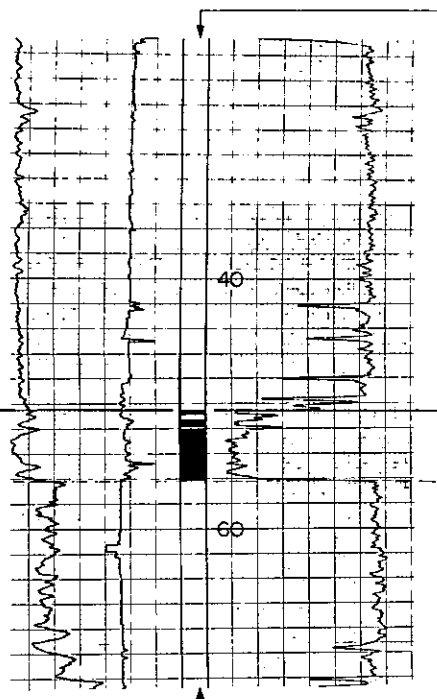
QUINTETTE COAL LIMITED
Project Manager
DENISON MINES LIMITED
COAL DIVISION

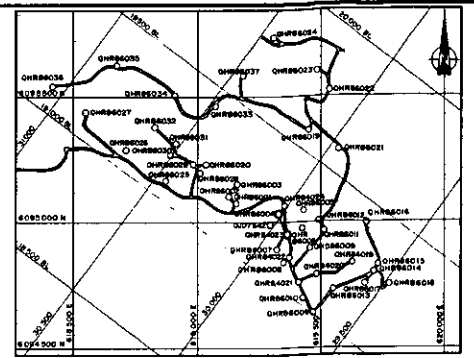
Area: GETHING Category: CORRELATION

Drawing Title
GETHING AREA
DRILL HOLE GEOPHYSICAL LOG
CORRELATION OF COAL-BEARING
SECTION

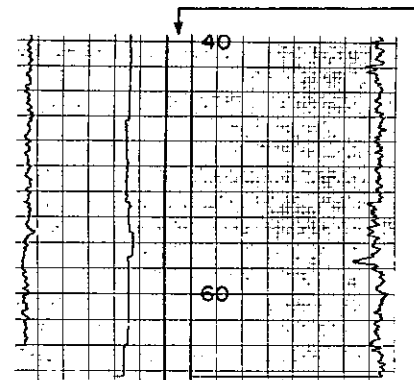
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Drawing No.: 86-605-26-015
SHEET 3 of 12
Rev. 0

DATUM

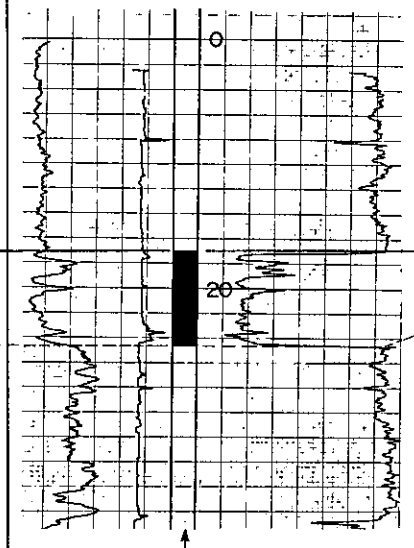




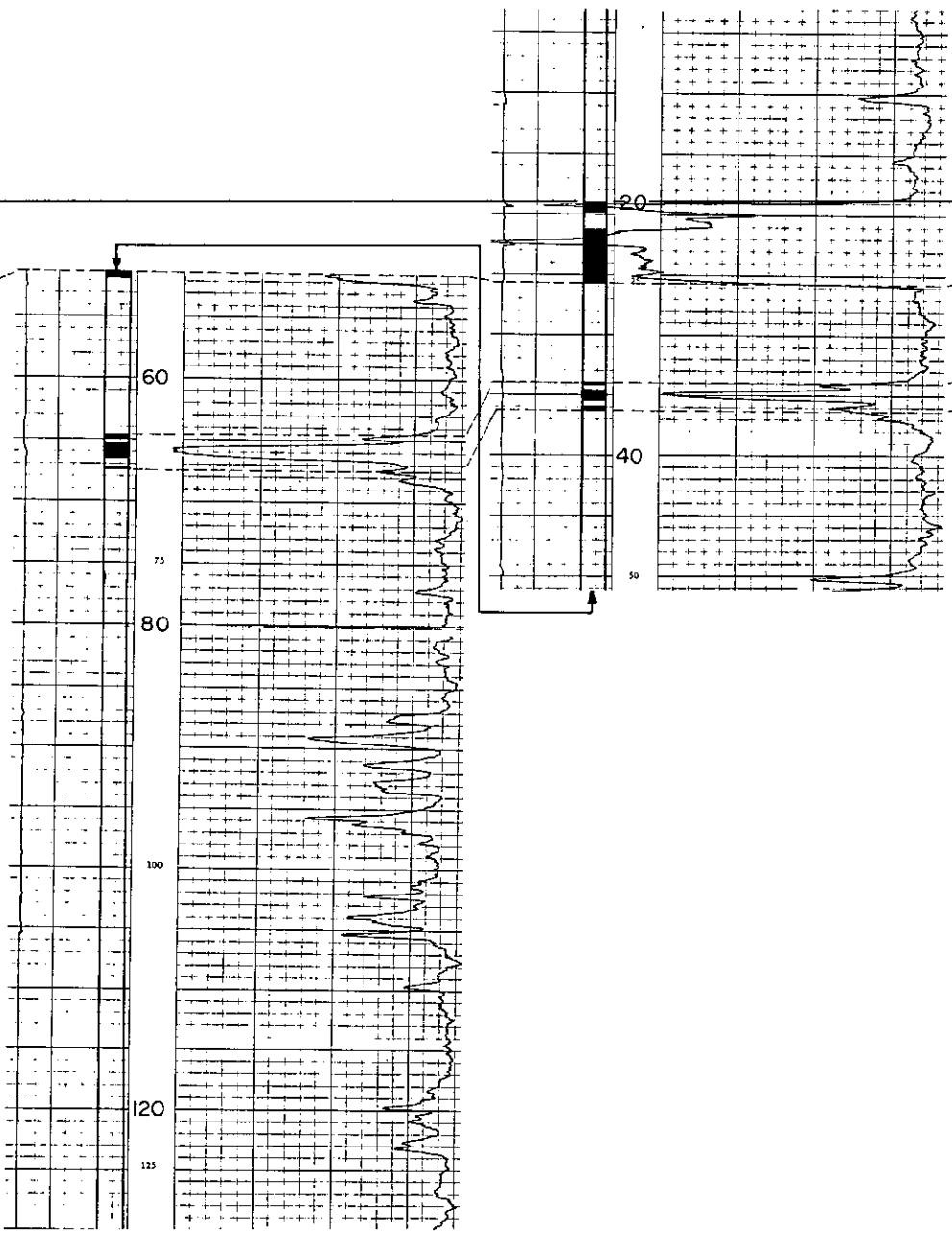
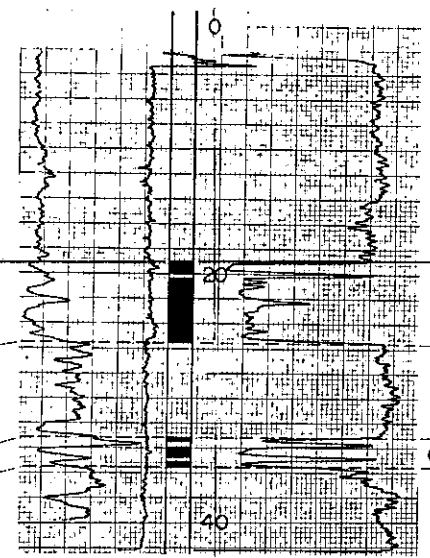
GETHING AREA LOCATION MAP
1:10000 SCALE



QHR 86004

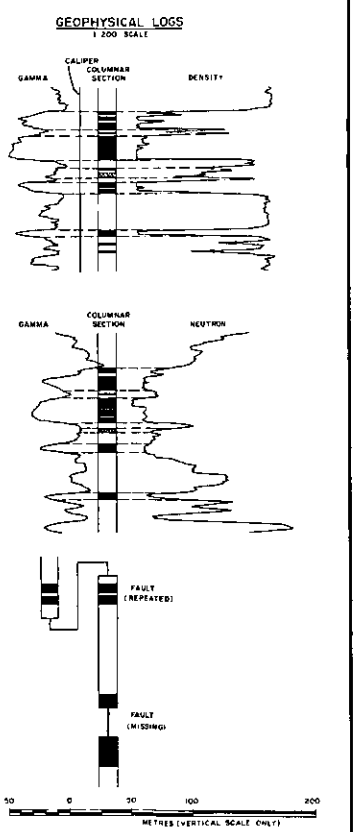


QHR 84023



LEGEND
 [Symbol] COAL TO COAL SHALE
 [Symbol] COAL
 [Symbol] ROCK
 [Symbol] COAL

DATUM
 GT1 SEAM
 GT2 SEAM



NOTE: 1. ALL THICKNESSES ARE APPARENT
 2. SQUIGGLING: BOREHOLE GEOPHYSICAL DATA IS AVAILABLE FOR MOST HOLES
 3. GAMMA / NEUTRON LOGS USED ONLY WHEN DENSITY LOG IS NOT AVAILABLE

Rev.	D	M	V	Revision Description	Dr.	Des.	App.
0	25	11	04	ORIGINAL DRAFT	HW	HW	

QUINTETTE COAL LIMITED
 Project Manager
DENISON MINES LIMITED
 COAL DIVISION

Area: **GETHING** Category: **CORRELATION**

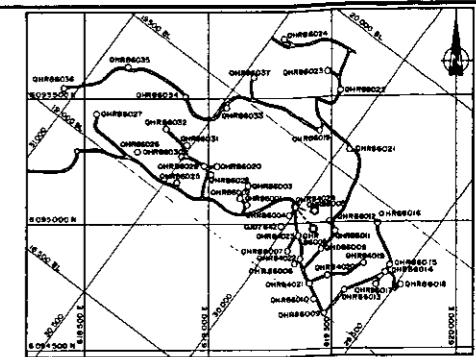
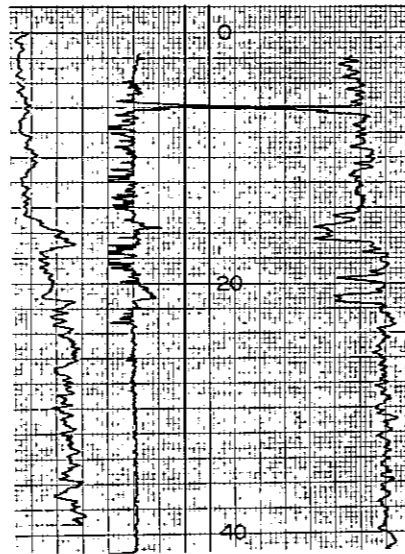
Drawing Title:
**GETHING AREA
 DRILL HOLE GEOPHYSICAL LOG
 CORRELATION OF COAL-BEARING
 SECTION**

Scale: 1:200(VERT)
 HORIZONTAL NOT TO SCALE

Drawing No.: 86-605-26-016
 Rev. 0

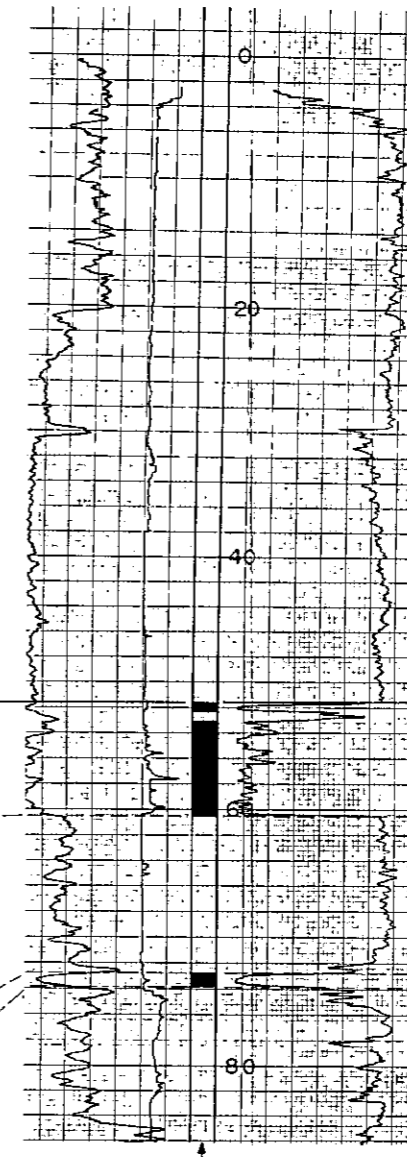
SHEET 8 of 12

QHR 84024

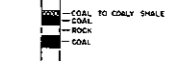


GETHING AREA LOCATION MAP
1:10000 SCALE

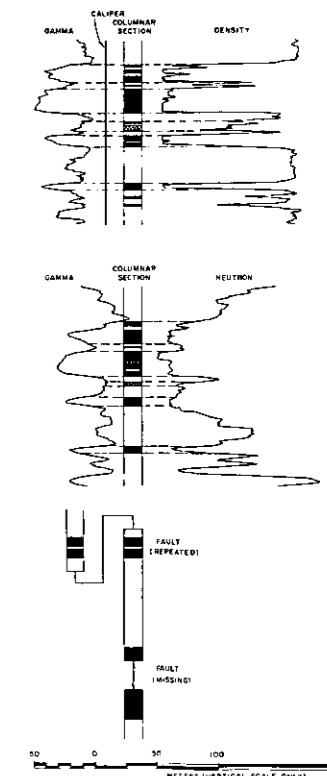
QHR 86005



LEGEND



GEOPHYSICAL LOGS
1:200 SCALE

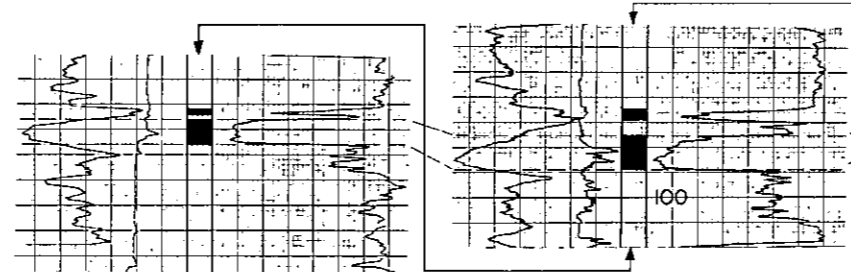
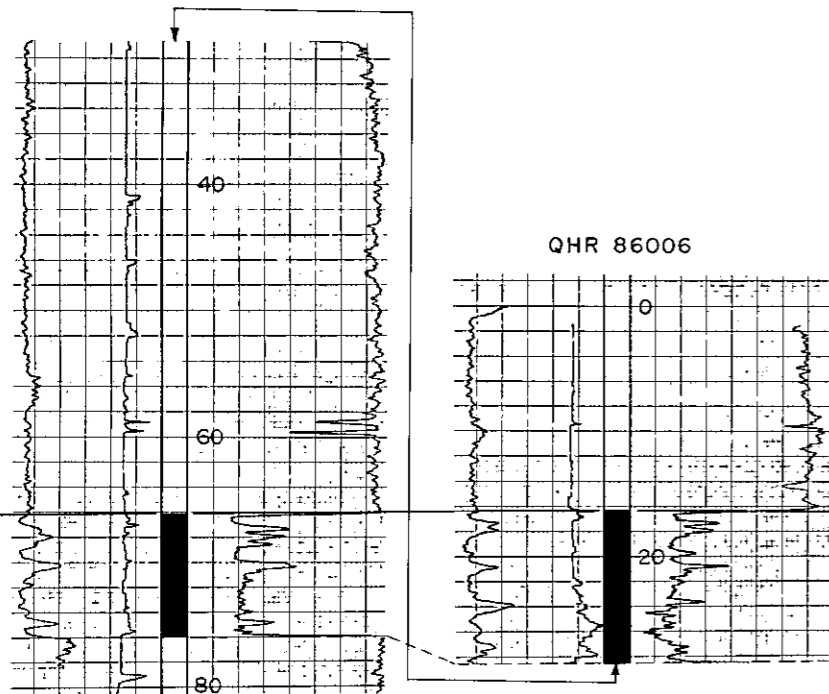


DATUM

GT 1 SEAM

GT 2 SEAM

QHR 86006

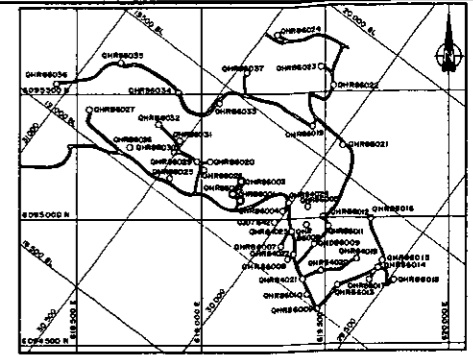


NOTE: 1) ALL THICKNESSES ARE APPARENT
2) ADDITIONAL BOREHOLE GEOPHYSICAL DATA IS AVAILABLE FOR MOST HOLES
3) GAMMA/NEUTRON LOGS USED ONLY WHEN DENSITY LOG IS NOT AVAILABLE

Rev.	D.	M.	Y.	Revision Description	Drn.	Des.	App.
0	28	11	86	ORIGINAL DRAFT	H.B.	H.W.	

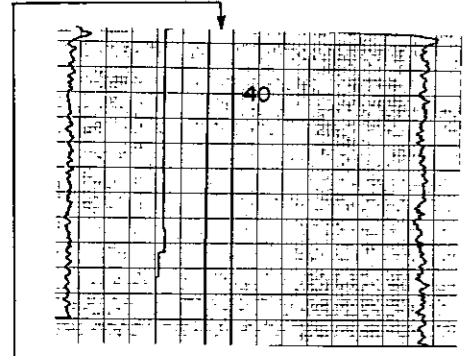
QUINETTE COAL LIMITED
Project Manager
DENISON MINES LIMITED
COAL DIVISION

Area	GETHING	Category	CORRELATION
Drawing Title			
GETHING AREA			
DRILL HOLE GEOPHYSICAL LOG			
CORRELATION OF COAL-BEARING SECTION			
SHEET 7 of 12			
Scale	1:200(VERT.)	Drawing No.	86-605-26-017
Rev.			0



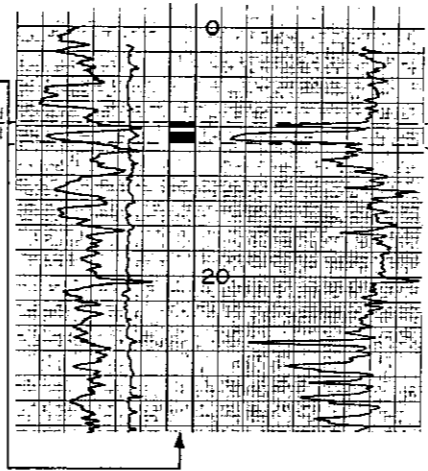
GETHING AREA LOCATION MAP
1:10000 SCALE

QHR 86003

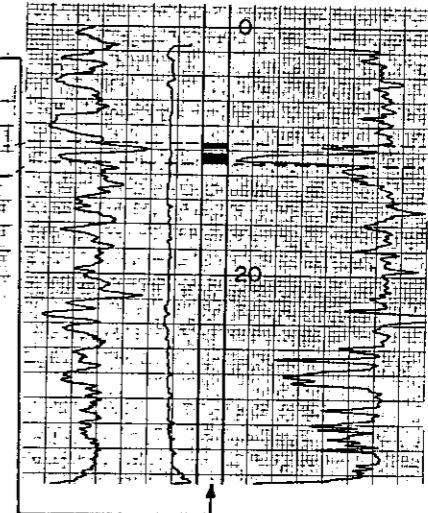


GT 1 SEAM

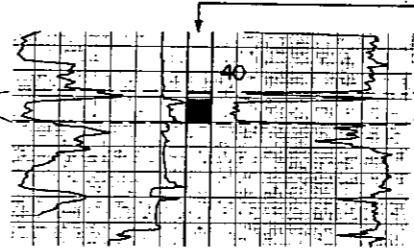
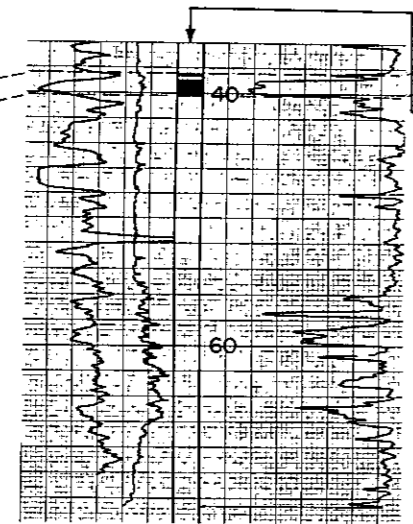
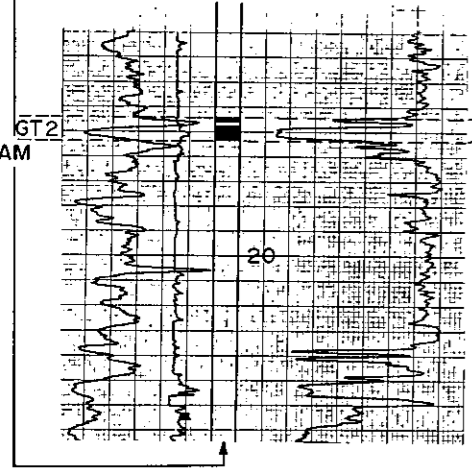
QHR 86002



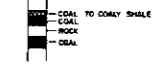
QHR86001



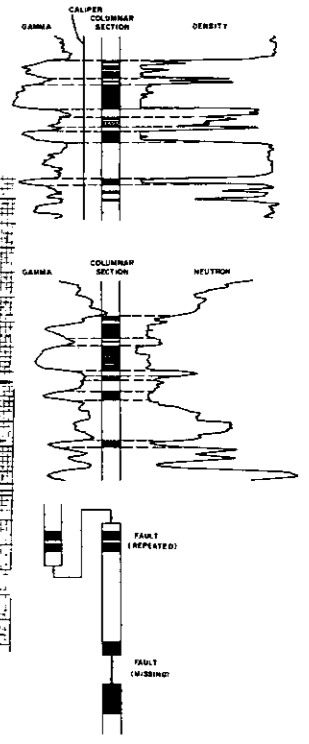
GT2 SEAM



LEGEND



GEOPHYSICAL LOGS
1:200 SCALE



50 0 50 100 200
METRES (VERTICAL SCALE ONLY)

NOTE: 1) ALL THICKNESSES ARE APPARENT
2) ADDITIONAL BOREHOLE GEOPHYSICAL DATA IS AVAILABLE FOR MOST HOLES
3) GAMMA/NEUTRON LOGS USED ONLY WHEN DENSITY LOG IS NOT AVAILABLE

Rev.	Date	Description	By	App.
0		ORIGINAL DRAFT	HW	HW

QUINTETTE COAL LIMITED
Project Manager
DENISON MINES LIMITED
COAL DIVISION

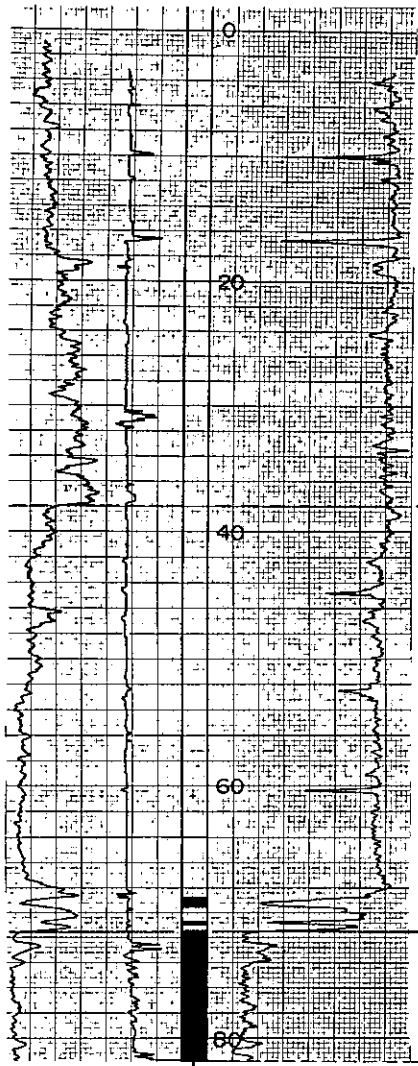
Area: GETHING Category: CORRELATION

Drawing Title
**GETHING AREA
DRILL HOLE GEOPHYSICAL LOG
CORRELATION OF COAL-BEARING
SECTION**

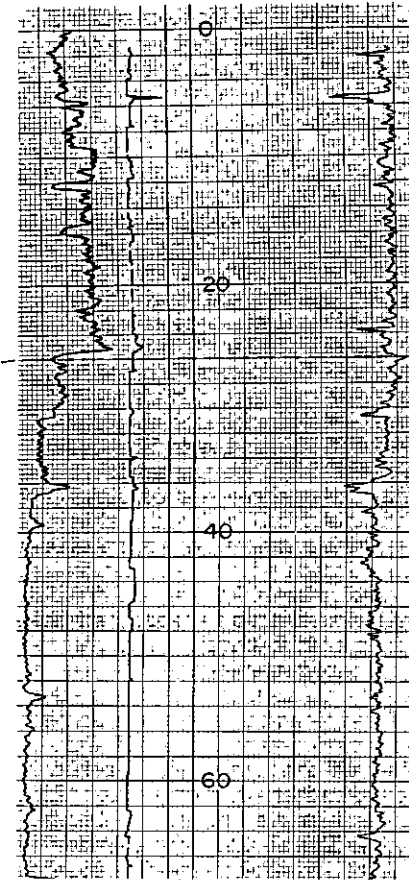
Scale: 1:200(VERT)
Drawing No.: 86-605-26-018
Rev.: 0

SHEET 8 of 12

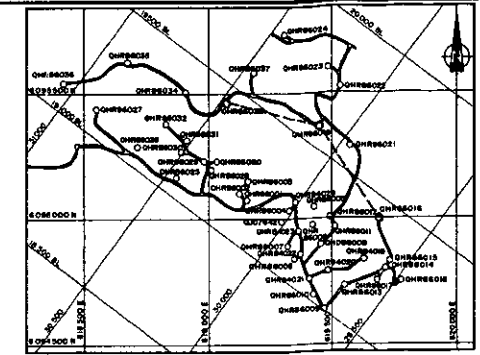
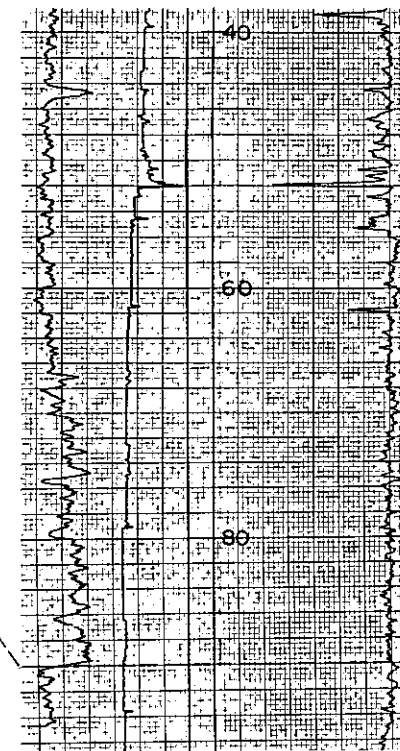
QHR 86033



QHR 86019

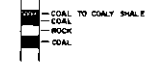


QHR 86016

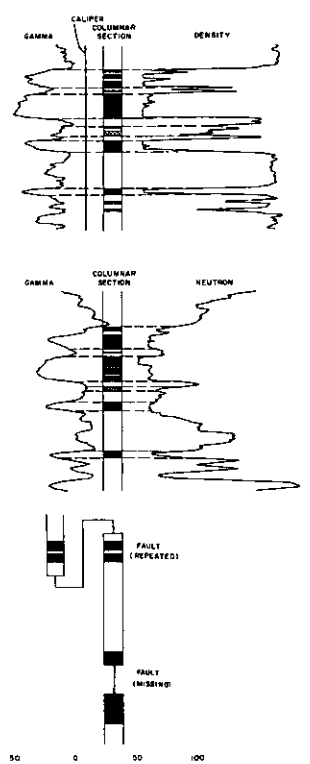


GETHING AREA LOCATION MAP
1:10000 SCALE

LEGEND



GEOPHYSICAL LOGS
1:200 SCALE



NOTE: 1) ALL THICKNESSES ARE APPARENT
 2) ADDITIONAL BOREHOLE GEOPHYSICAL DATA IS AVAILABLE FOR MOST HOLES
 3) GAMMA/NEUTRON LOGS USED ONLY WHEN DENSITY LOG IS NOT AVAILABLE

Rev.	Date	Description	Drn.	Des.	App.
0		ORIGINAL DRAFT			

QUINTETTE COAL LIMITED
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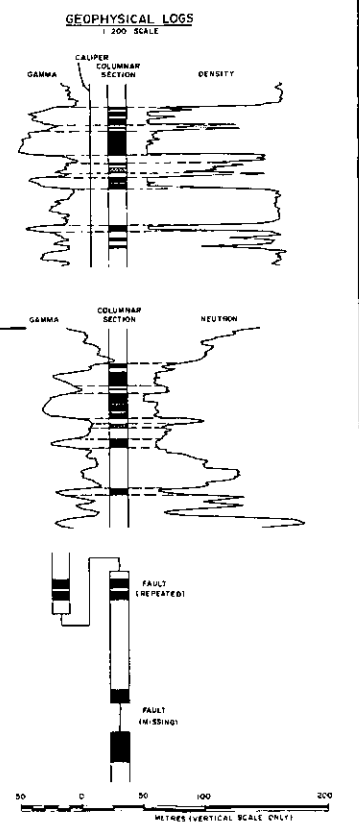
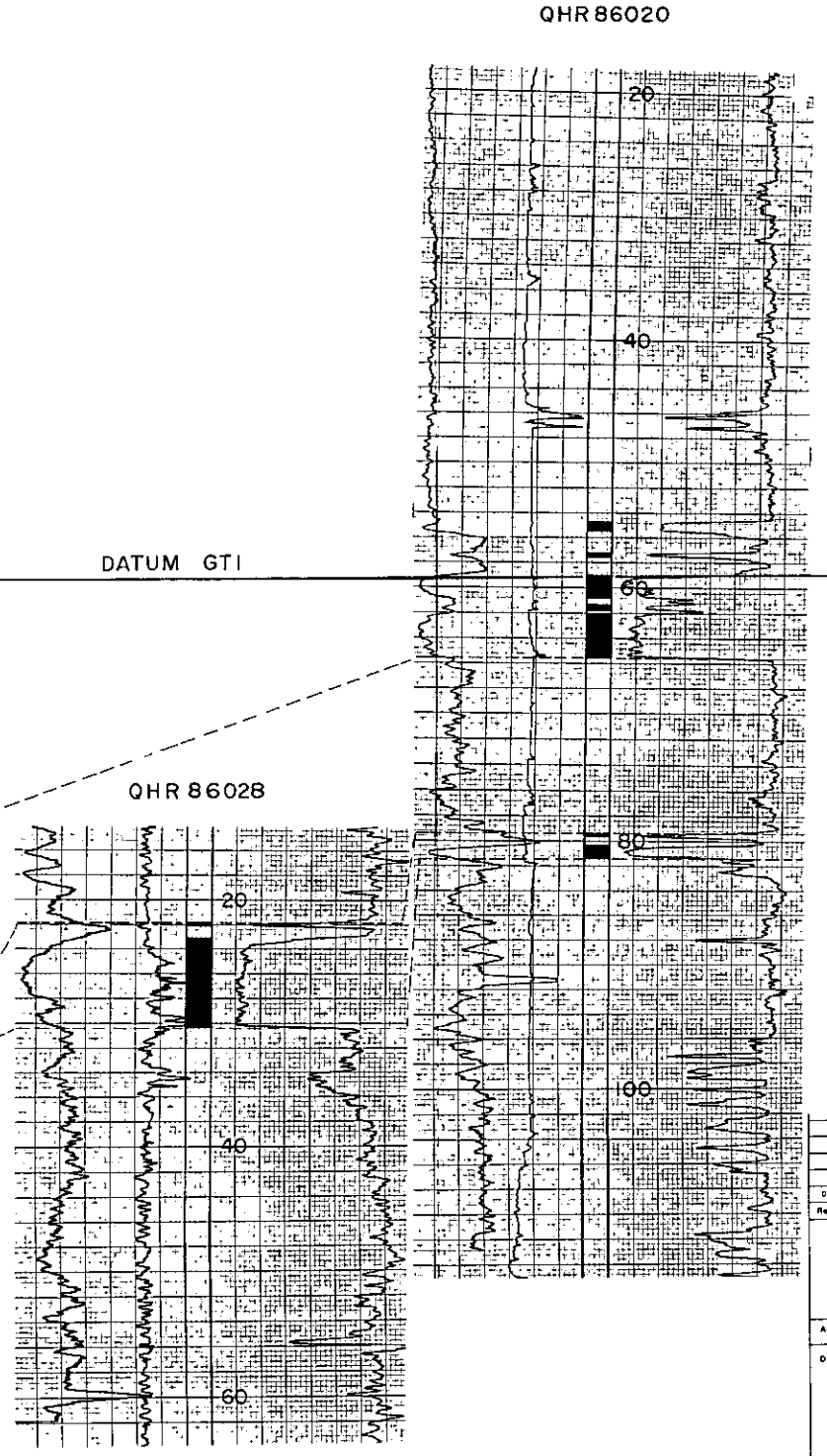
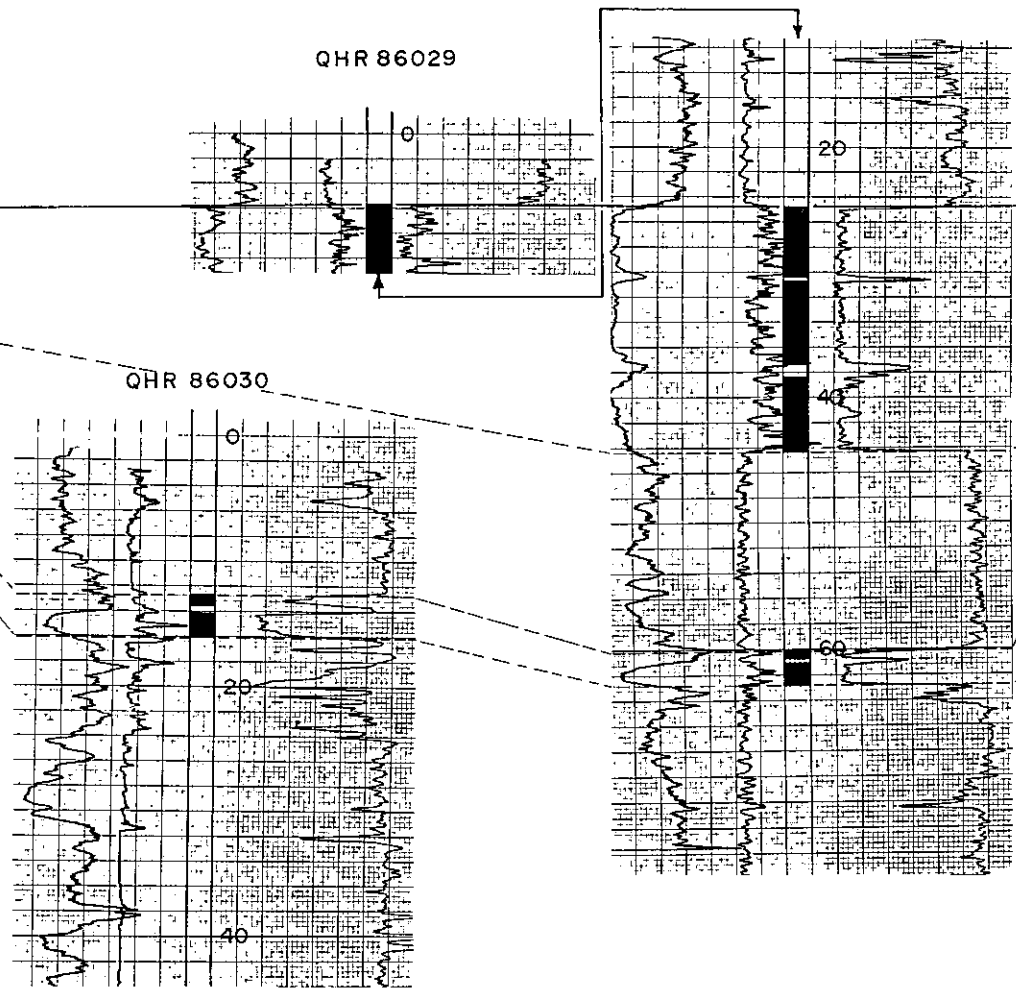
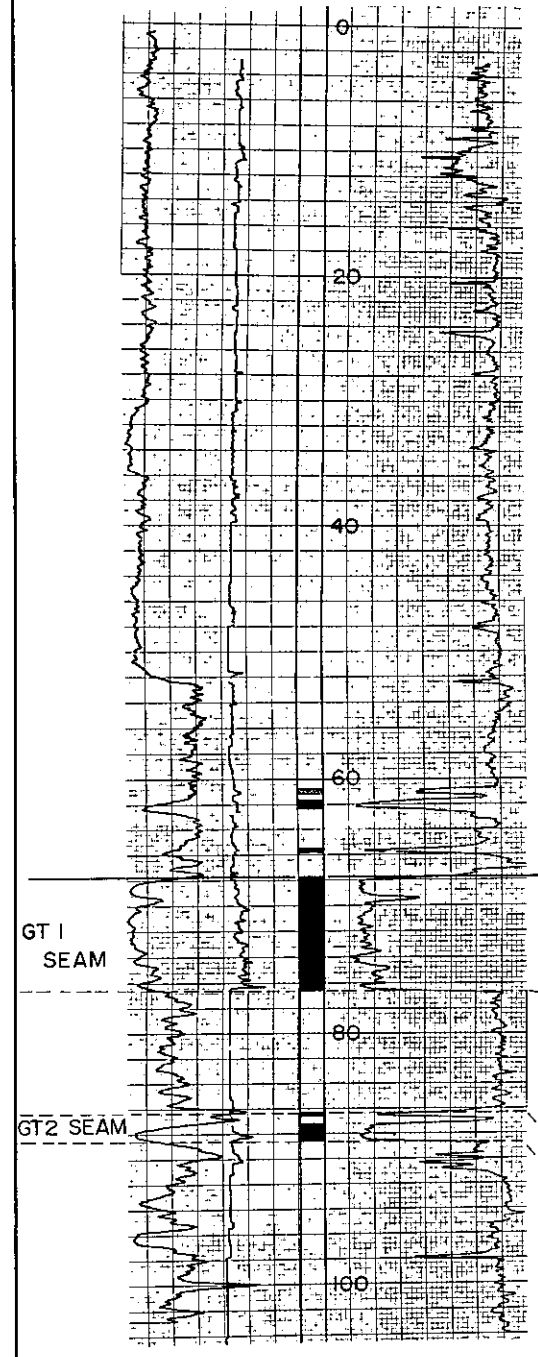
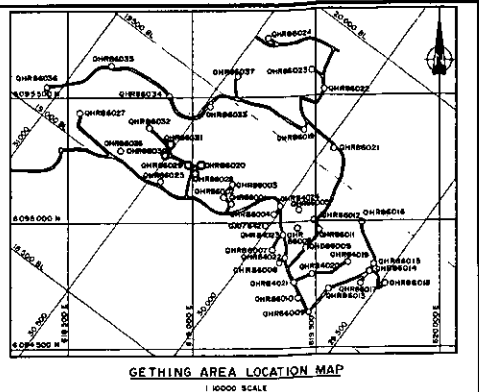
Area: **GETHING** Category: **CORRELATION**
 Drawing Title:
GETHING AREA
DRILL HOLE GEOPHYSICAL LOG
CORRELATION OF COAL-BEARING SECTION

Scale: 1:200 (VERT.) Drawing No. 85-605-26-019 Rev. 0
 SHEET 2 of 12

GT1 SEAM

GT2 SEAM

QHR 86031



NOTE: 1) ALL THICKNESSES ARE APPARENT
2) ADDITIONAL BOREHOLE GEOPHYSICAL DATA IS AVAILABLE FOR MOST HOLES
3) GAMMA/NEUTRON LOGS USED ONLY WHEN DENSITY LOG IS NOT AVAILABLE

Rev.	D	M	Y	Revision Description	Drn.	Des.	App.
0	28	11	86	ORIGINAL DRAFT	HS	H	

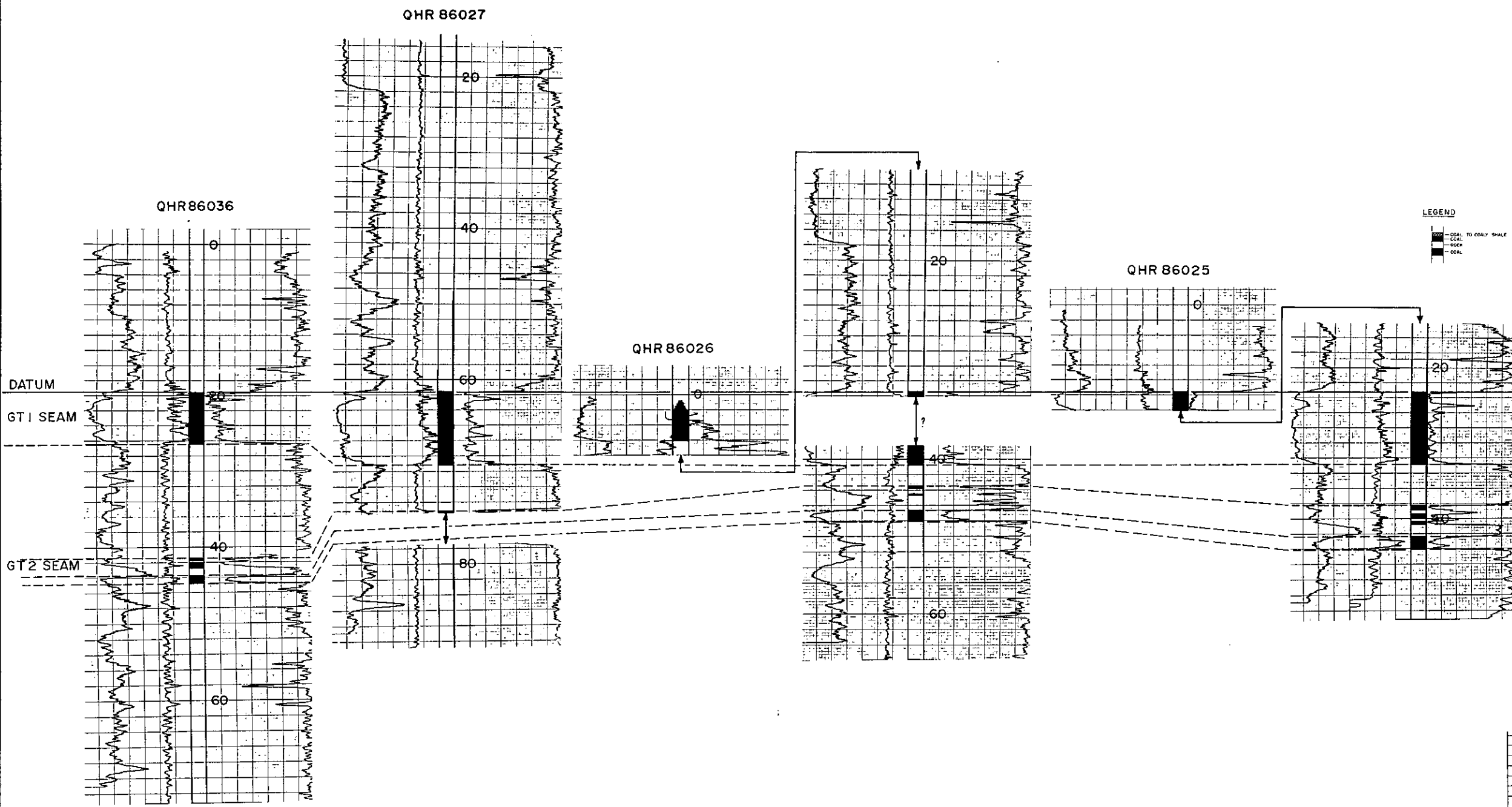
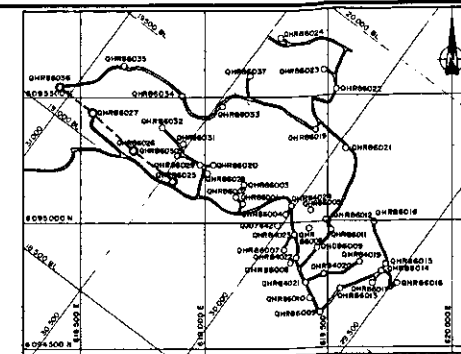
QUINTETTE COAL LIMITED
Project Manager
DENISON MINES LIMITED
COAL DIVISION

Area: GETHING Category: CORRELATION

Drawing Title:
**GETHING AREA
DRILL HOLE GEOPHYSICAL LOG
CORRELATION OF COAL-BEARING
SECTION**

Scale: 1:200(VERT.)
Drawing No.: 86-605-26-020
Rev.: 0

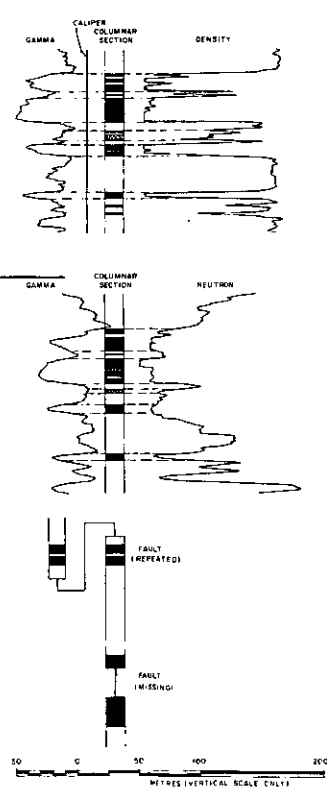
SHEET 20 OF 18



LEGEND

- COAL TO COALY SHALE
- COAL
- ROCK
- COAL

GEOPHYSICAL LOGS



NOTE: 1. ALL THICKNESSES ARE APPARENT
2. ADDITIONAL BOREHOLE GEOPHYSICAL DATA IS AVAILABLE FOR MOST HOLES
3. GAMMA/NEUTRON LOGS USED ONLY WHEN DENSITY LOG IS NOT AVAILABLE

Rev	Date	Description	Drn.	Des.	App.
0	26/11/86	ORIGINAL DRAFT	HB	HW	

QUINTETTE COAL LIMITED
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COAL DIVISION

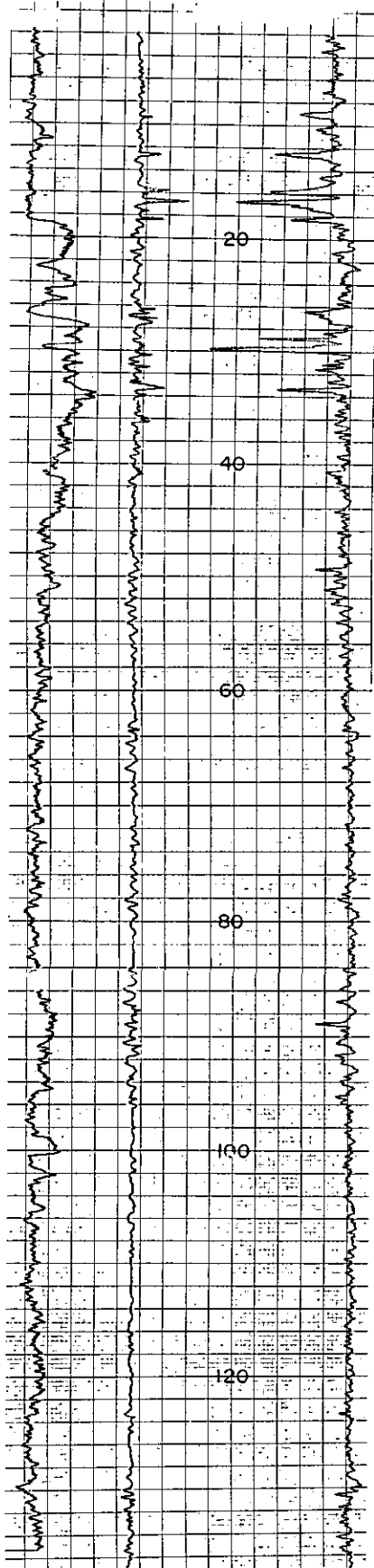
Area: GETHING Category: CORRELATION

Drawing Title:
**GETHING AREA
DRILL HOLE GEOPHYSICAL LOG
CORRELATION OF COAL-BEARING
SECTION**

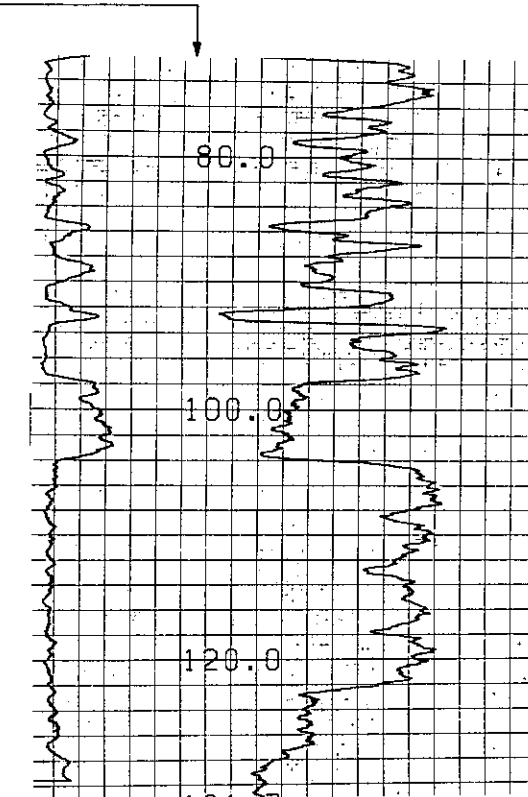
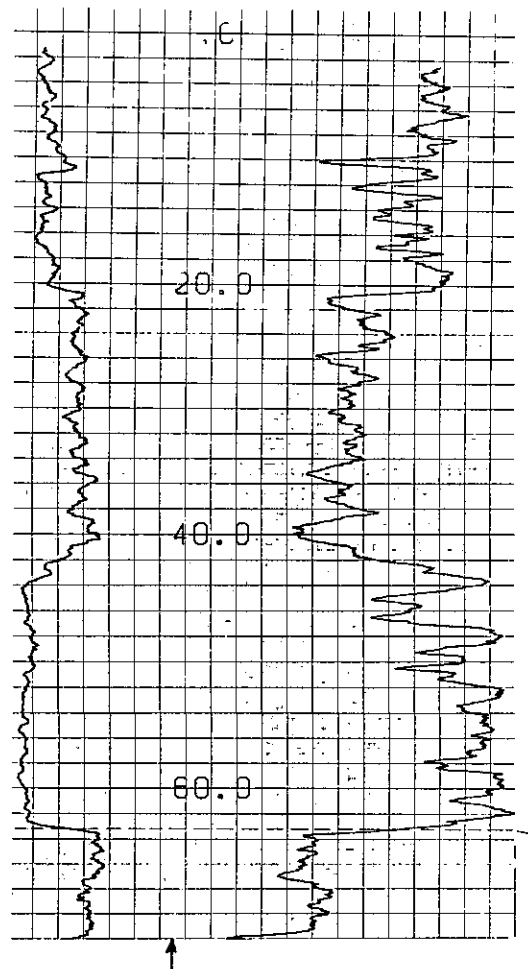
Scale: 1:200 (VERT.) Drawing No.: 86-605-26-021 Rev.: 0
(HORIZONTAL, NOT TO SCALE)

SHEET 11 of 12

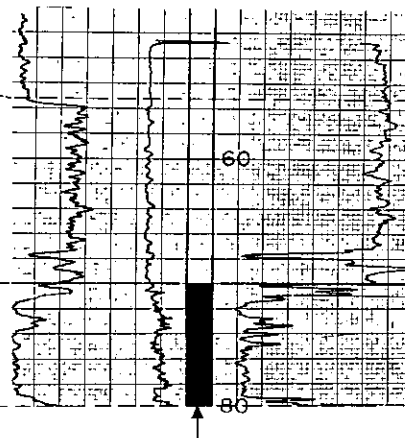
QHR 86037



QHR 86035

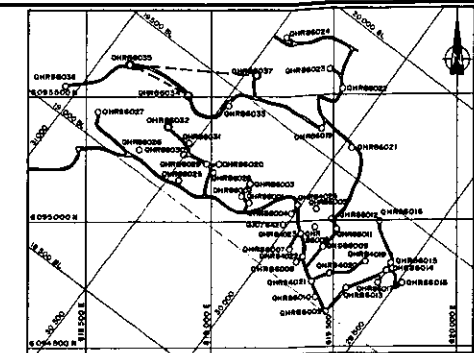


QHR 86034



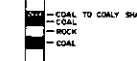
DATUM

GT I SEAM

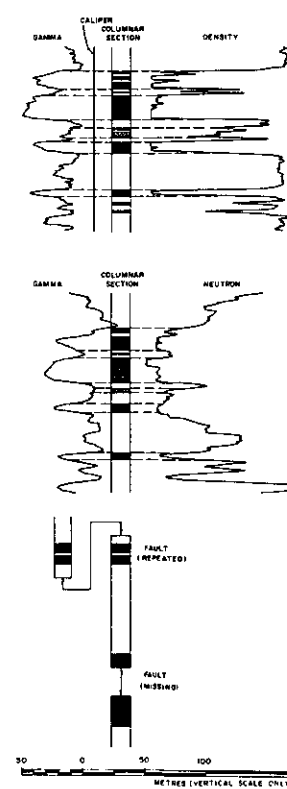


GETHING AREA LOCATION MAP
1:10000 SCALE

LEGEND



GEOPHYSICAL LOGS
1:200 SCALE



NOTE 1) ALL THICKNESSES ARE APPARENT
2) ADDITIONAL BOREHOLE GEOPHYSICAL DATA IS GIVEN ONLY FOR MOST HOLES
3) SIGMA/NEUTRON LOGS USED ONLY WHEN DENSITY LOG IS NOT AVAILABLE

Rev.	Q	M	Y	Revision Description	Dr.	Des.	App.
0	28			ORIGINAL DRAFT			

QUINTETTE COAL LIMITED
Project Manager
DENISON MINES LIMITED
COAL DIVISION

Area: **GETHING** Category: **CORRELATION**

Drawing Title:
**GETHING AREA
DRILL HOLE GEOPHYSICAL LOG
CORRELATION OF COAL-BEARING
SECTION**

Scale: 1:200 (VERT.)
Drawing No.: 86-605-26-022
Rev.: 0

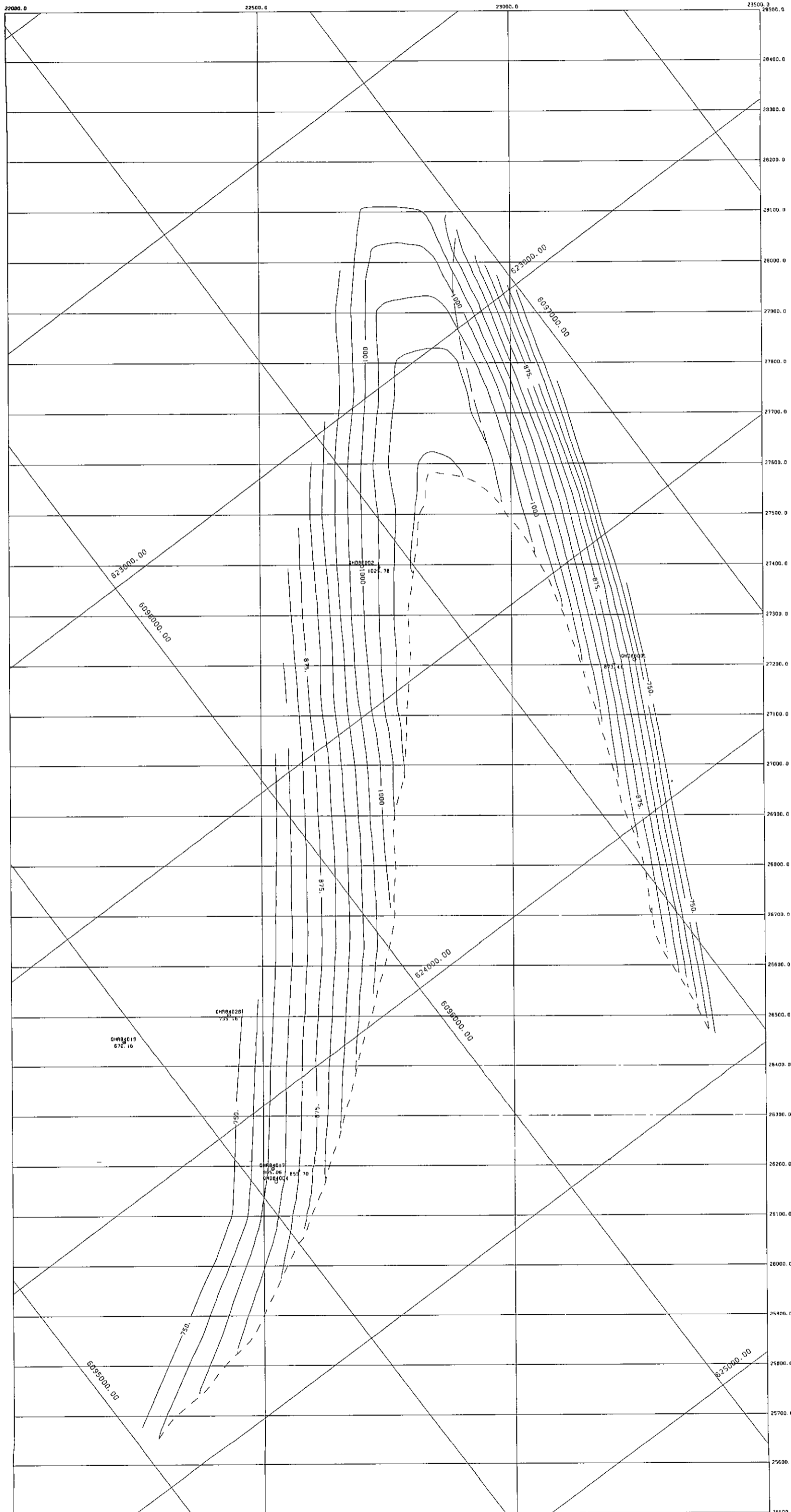
APPENDIX 1

Section 2.2

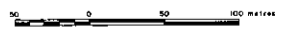
Grizzly Area

Structure Contour Maps

Seam F, G and J



NOTE:
 - - - - - SUBCROP
 - - - - - FAULT TRACE
 - - - - - STRUCTURE CONTOUR
 - - - - - DATASET (DRILLHOLES, TRENCHES)
 CHN0001 - 1027.70
 CHN0002 - 1027.70
 CHN0003 - 893.41
 CHN0004 - 893.41
 CHN0005 - 735.16
 CHN0006 - 735.16
 CHN0007 - 855.70
 CHN0008 - 855.70
 CHN0009 - 855.70
 CHN0010 - 855.70



DATE	202507	ORIGINAL DRAFT	KJV	DPL	G.G.
REV	01	REVISION DESCRIPTION	DN	DES	APP
QUINETTE COAL LIMITED PROJECT NUMBER DENISON MINES LIMITED					
AREA	GRIZZLY	CATEGORY	GEOLOG		
DRAWING TITLE					
GRIZZLY MINE AREA STRUCTURE CONTOUR PLOT G SEAM					
SHEET	1:2500	DRAWING FILE	87-905-22-002	REV	0

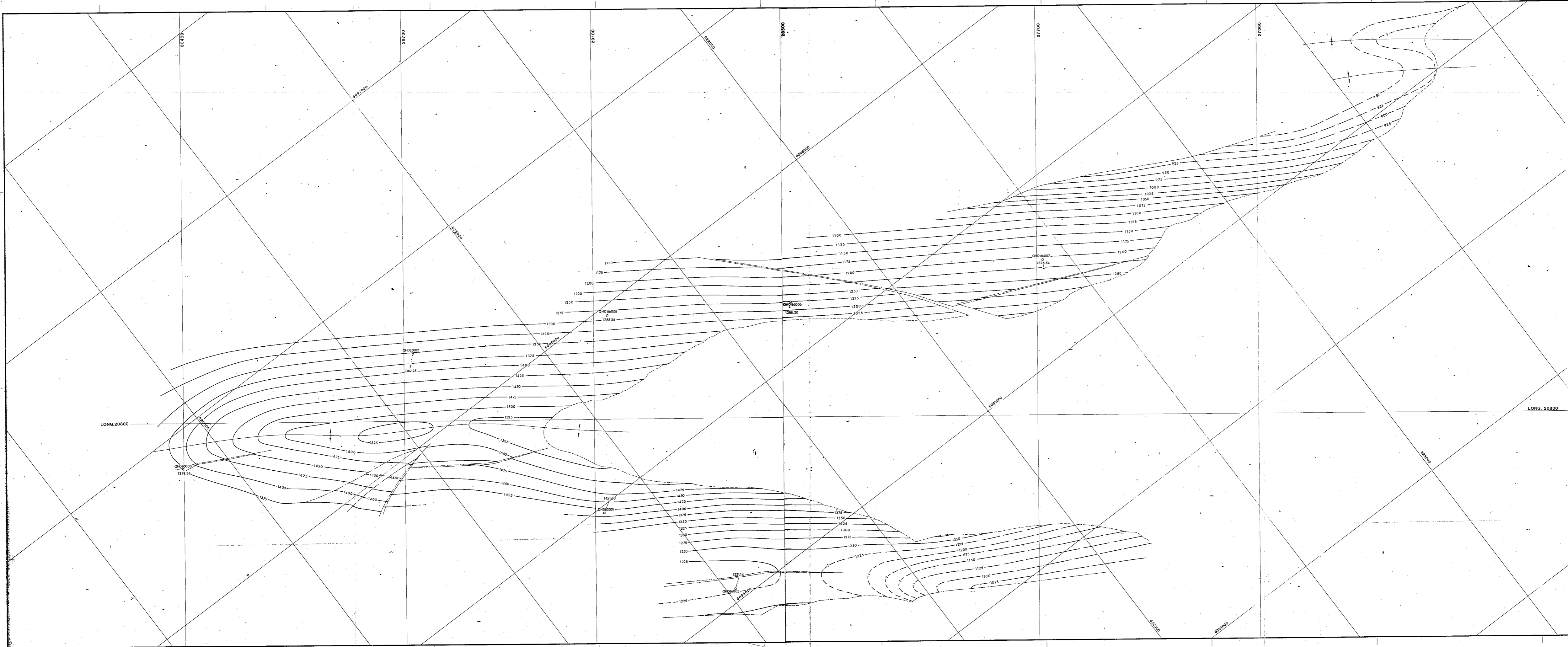
APPENDIX 1

Section 2.3

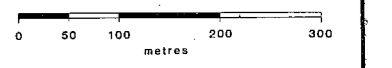
Transfer Area

Structure Contour Maps (6)

Seam F, G and J



- SEAM OUTCROP
- FAULT INTERSECTION
- STRUCTURE CONTOUR (25m INTERVAL)
- QHD 86002
1251.2
ELEVATION OF SEAM TOP
DOLLAR
- ELEVATION OF SEAM TOP
- SYNCLINE
- ANTICLINE



Rev.	Drawn	Checked	Revision Description	Est.	App.

QUINTETTE COAL LIMITED
 Project Manager
DENISON MINES LIMITED
 COAL DIVISION

Area: TRANSFER Category: STRUCTURES

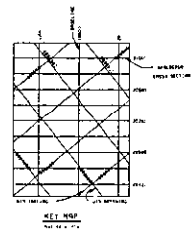
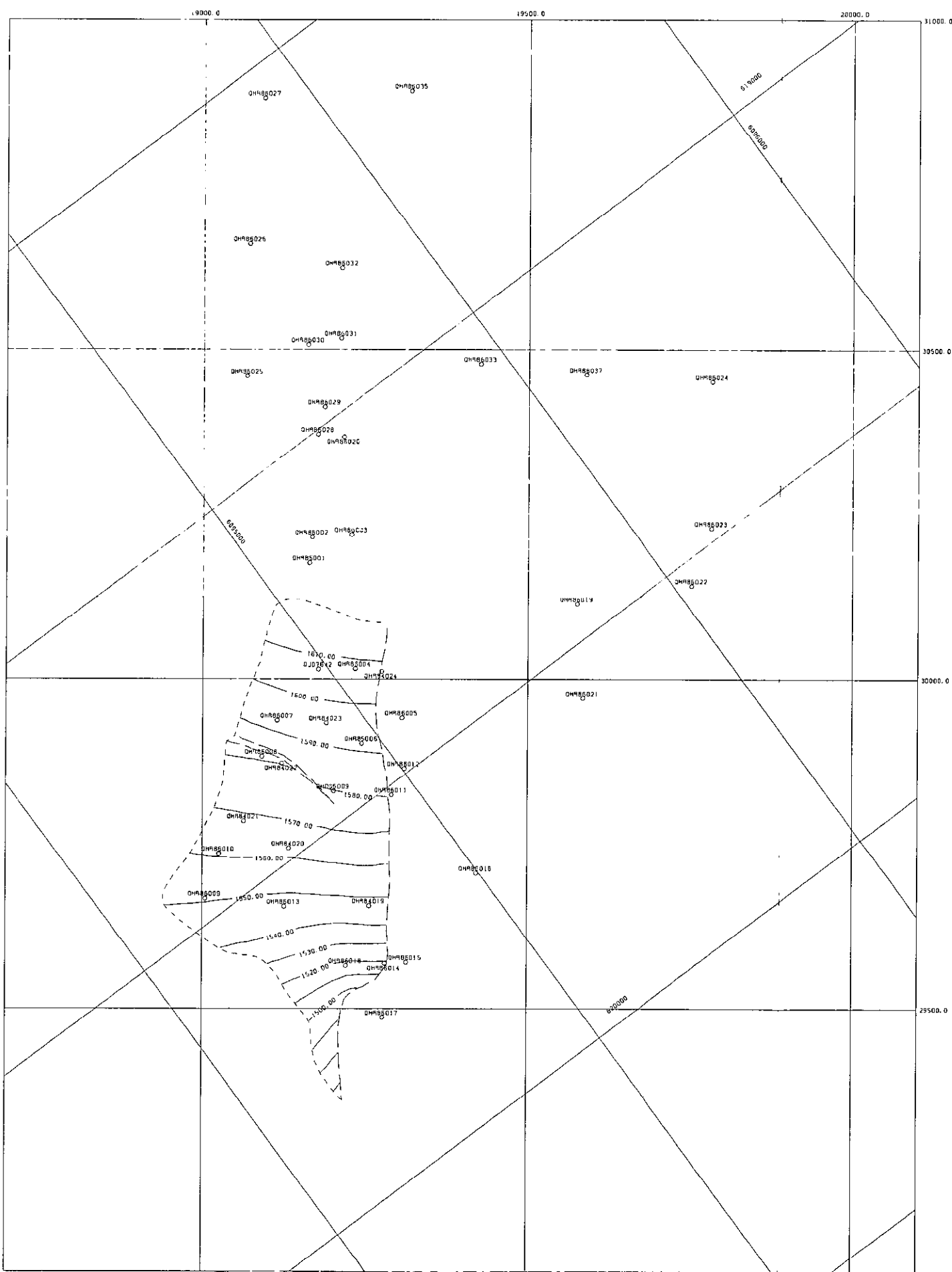
Drawing Title:
TRANSFER AREA
STRUCTURE CONTOURS
G SEAM

Scale: 1:2500 Drawing No.: 87-903-22-002 SHEET 1 of 2

APPENDIX 1

Section 2.4

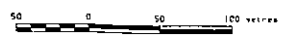
**Gething Area
Structure Contour Maps
Seam GT.1 and GT.2**



UTM NORTH

LEGEND

- 01485019 DATASET (DRILLHOLES, TRENCHES)
- 01485018 ELEVATION OF SEAM TOP
- 1670.00 STRUCTURE CONTOUR (10m contour interval)
- SEAM OUTCROP TRACE
- FAULT CONTACT

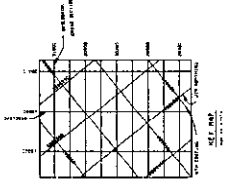


NO.	REVISION	DESCRIPTION	DATE	BY	CHECKED
01		ORIGINAL DRAFT			
02		REVISION			

QUINTEITE COAL LIMITED
 Project Manager
 DENISON MINES LIMITED
 COAL DIVISION

Area: **GETHING** Category: **STRUCTURE CONTOUR**
 Drawing Title: **GETHING AREA
GT1 SEAM
TOP OF SEAM STRUCTURE CONTOUR**

Scale: 1:2500 Drawing File: 87-605-22-001 Rev: 0

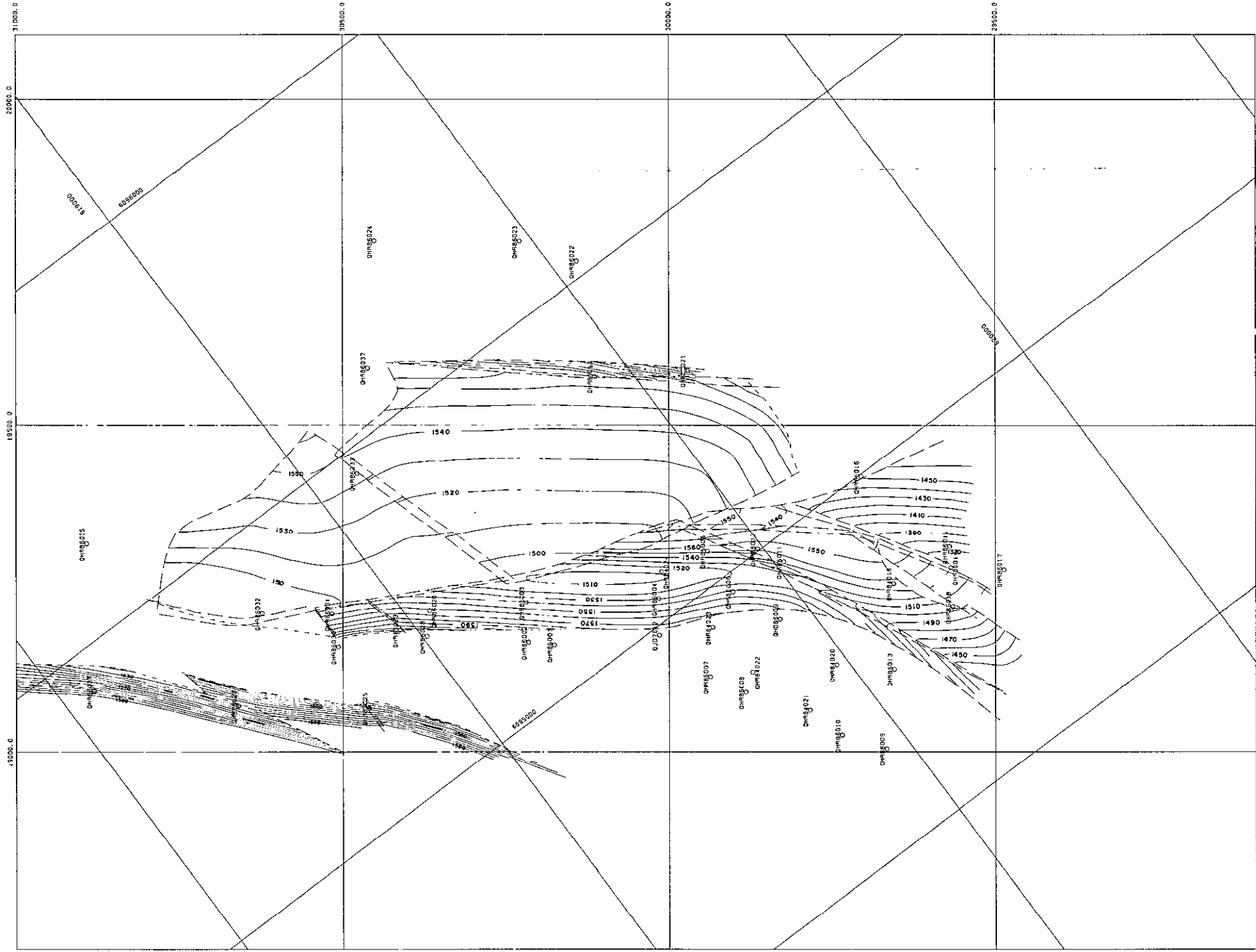


UTM NORTH

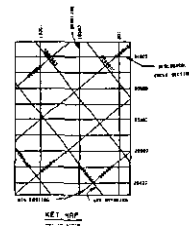
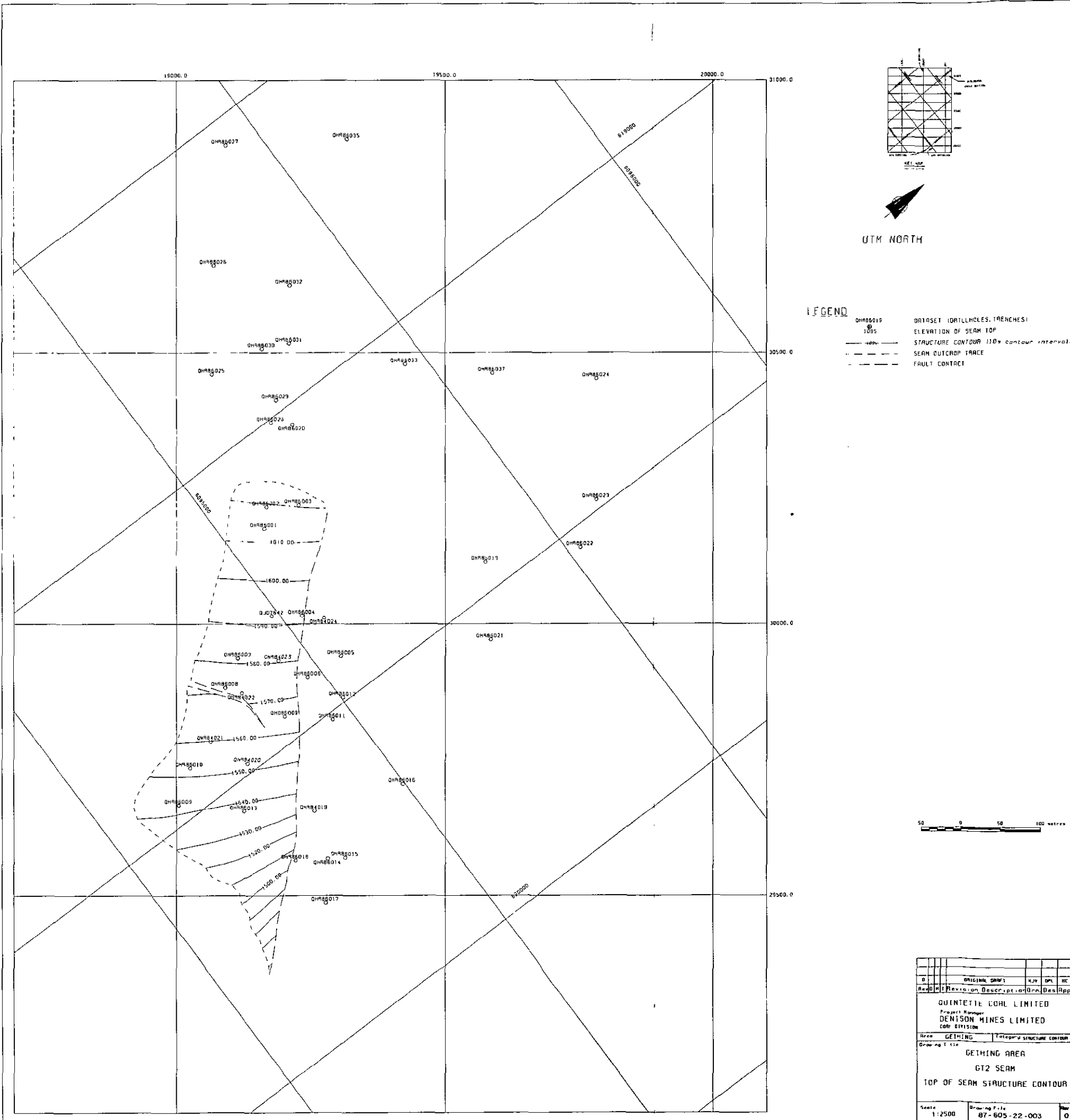
LEGEND

01M85G019
1075
1485

DATASET (DAILHOLES, TRENCHES)
ELEVATION OF SEAM TOP
STRUCTURE CONTOUR (10m contour interval)
SEAM OUTCROP TRACE
FAULT CONTACT



NO.	REVISION	DESCRIPTION	DATE	BY	CHK
0					
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4					
5					
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7					
8					
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10					
11					
12					



LEGEND

- DHR85019
○
1085 DATASET (DRILLHOLES, TRENCHES)
- 1085 ELEVATION OF SEAM TOP
- 100 — STRUCTURE CONTOUR 100m contour interval
- SEAM OUTCROP TRACE
- - - FAULT CONTACT



REV	NO	DATE	BY	CHKD	APP
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100					

QUINTETTE COAL LIMITED
 Project Manager
 DENISON MINES LIMITED
 COAL DIVISION
 Area: GETTING Topography STRUCTURE CONTOUR
 Drawing Title:
 GETTING AREA
 G12 SEAM
 TOP OF SEAM STRUCTURE CONTOUR
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APPENDIX 1

Section 3.0

Appendix I, Section 3 of this report contains coal quality data, and remains confidential under the terms of the *Coal Act Regulation*, Section 2(1). It has been removed from the public version.

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APPENDIX 1

Section 4.0

QUINTEITE COAL LIMITED

TRANSFER AREA

GEOLOGICAL REPORT

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**TRANSFER AREA
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Most of Appendix II, Sections 1 & 2 of this report contains coal quality data, and remains confidential under the terms of the *Coal Act Regulation*, Section 2(1). It has been removed from the public version.

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