ESSO RESOURCES CANADA LTD. SUMMARY REPORT ON FIELD INVESTIGATIONS OF COAL MINE WASTE DUMPS IN THE NANAIMO AREA VANCOUVER ISLAND

> PREPARED FOR : ESSO RESOURCES CANADA LTD.

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DATE: October, 1983

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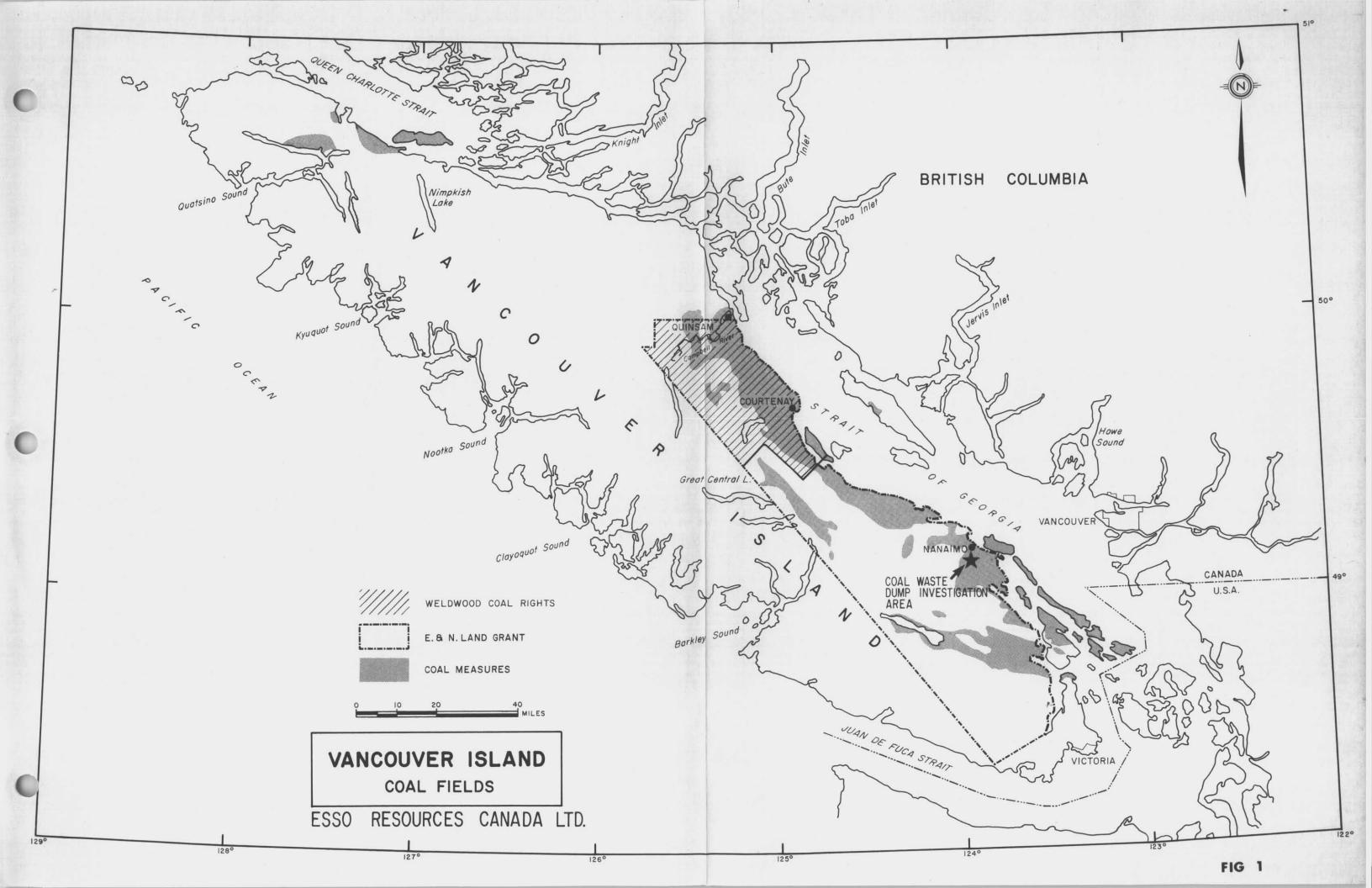
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SECTION 1.

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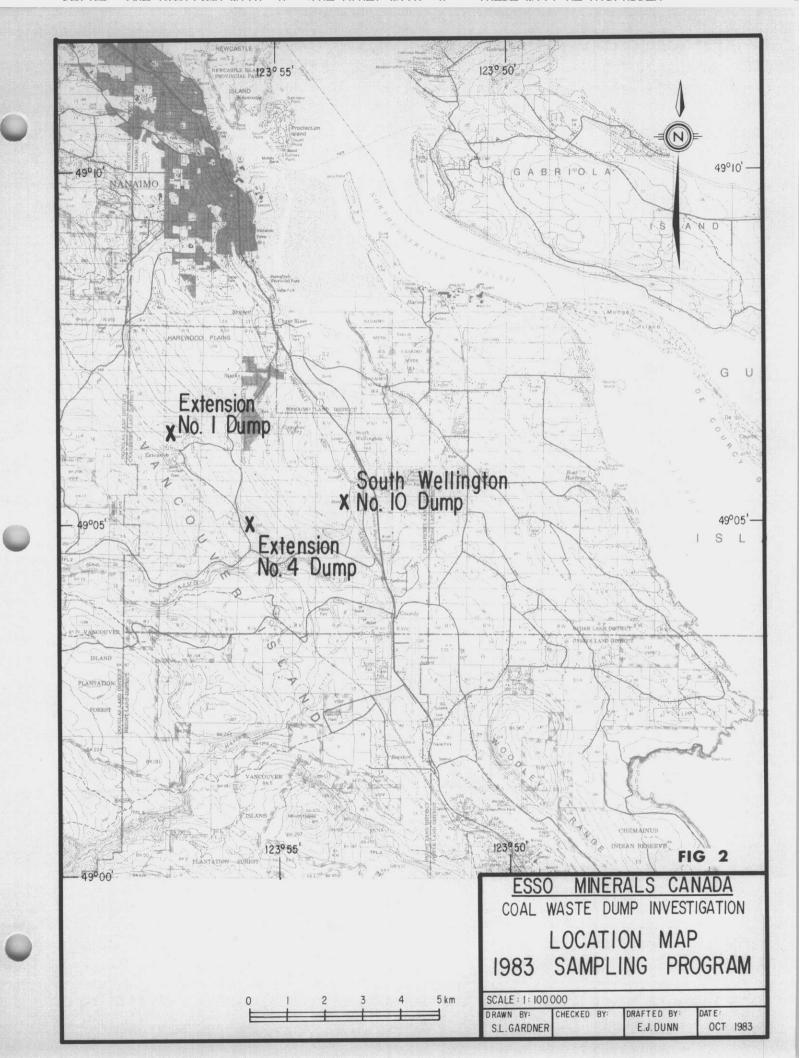
1.0 INTRODUCTION

Between 5 and 10 million tonnes of coal mine tailings occurs in the Nanaimo area of southeastern Vancouver Island. This tailings material is contained in a number of waste dumps varying in size from a few thousand to as much as 500,000 cubic meters. These dumps are located near the abandoned mine headings that are scattered around the suburban Nanaimo area.

Preliminary analytical work, consisting mainly of grab samples taken from random locations, indicated that the dumps contain between 50 to 60% ash on an as-received basis, with 8 - 10% moisture, and 3,500 to 5,000 BTU/lb. This preliminary testing prompted Countryside Coal Processing Ltd. to secure options on the piles from the various land owners.

In September, 1983 Esso Resources Ltd. entered into an agreement with Countryside to investigate the waste dumps in greater detail and evaluate the economics of processing the dumps in order to recover clean coal product. Three of the larger and more accessible dumps were chosen for the initial investigation.

This report describes the field methods chosen for the sampling of each of the dump sites and outlines the field program undertaken by the author on behalf of Esso Resources Ltd.



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1.1 Location of Coal Waste Dumps Selected for Initial Investigations

Figure 2 shows the location of the three waste dumps selected for initial sampling work. These are the South Wellington No. 10 Mine Dump, the Extension No. 1 Mine Dump, and the Extension No. 4 Mine Dump. They are located within an ll km. road distance of each other and are 12 km. road distance of tidewater.

The South Wellington No. 10 Dump is located on a 22.7 hectare parcel of land owned by Mr. Mac Smith, a local equipment contractor. The Extension No. 1 and No. 4 Mine Dumps are both located on MacMillan Bloedel Ltd. surface rights. All three dumps are situated outside of the city limits of Nanaimo and as such fall within the jurisdiction of the Regional District of Nanaimo.

SECTION 2.

2.0 BRIEF HISTORY OF COAL MINING - NANAIMO AREA

During the period 1852 to 1964, approximately 55 million short tons of coal was produced from the Nanaimo coalfield. Of this 55 million tons, 18 million tons was produced from the Wellington Seam horizon (the lowermost seam). Of the remaining 37 million tons, approximately 20 million tons was produced from the No. 1 Mine near Nanaimo harbour and other mines within the vicinity of downtown Nanaimo (the Douglas Seam Horizon). The other 17 million tons were produced from scattered locations in the Nanaimo coalfield.

Most of the mines washed their raw coal with a simple Vissac Jig wash plant. Jig plant efficiency for the various mines ranged from 71 to 80 %. In general, the Douglas Seam mines on the south end of the field had the lowest plant yields (71 to 73 %). This was because the Douglas Seam in this area was subjected to a great amount of stress resulting in areas of pinch and swell, which yielded a great amount of fines. The Jig plants had difficulty recovering the fines fraction, and these fines were difficult to market in the domestic and bunkering trades.

Most of the coal waste in the harbour and downtown Nanaimo areas had been disposed of due to urban developments. On the outskirts of the city, however, numerous waste dumps ranging from a few thousands of tons to hundreds of thousands of tons still remain.

Using the approximate total output figures for the Nanaimo coalfield of 55 million tons minus the 20 million tons from the harbour area, a figure of 35 million tons for the outlying mines is estimated. By employing an average jig plant yield of 75 %, and assuming that all of the coal was washed, an estimate of 8.75 million tons of coal waste may be present in the Nanaimo district. Table 1. illustrates some washery data for the typical coal sizes produced from Nanaimo mines.

TABLE 1. COAL WASHERY DATA, NANAIMO COALFIELD

WASHED COAL SIZES	% RECOVERY % RECOVERY		
Classification inches	millimeters	Wellington Seam	Douglas Seam
No. 1 Nut -24+14	-64+38	13.85	4.96
No. 2 Nut -11/2+7/8	-38+22	10.45	7.12
Pea -7/8+3/16	-22+05	20.00	21.91
Washed Smalls -3/16 -	-05	25.61	32.26
Boiler Smalls -3/16	-05	6.64	6.04
Refuse -3/16	-05	23.45	27.71
	- San an	Y K	V.

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3.0 PREVIOUS SAMPLING WORK

Previous analytical work on the waste dumps consists of work conducted by the author in 1979 on two of the most extensive dumps: the South Wellington No. 10 Mine Dump and the Extension No. 4 Mine Dump. This work is tabulated in the following tables. Sample No. 1 is a composite sample of the No. 1 Extension Dump located approximately 11 km. southwest of the Nanaimo city centre. The sample labelled Sample No. 2 is a composite sample of the South Wellington No. 10 Mine Dump, located approximately 8 km. south of the city centre.

The 1979 sampling involved the use of a tractor-mounted backhoe. The backhoe was able to ascend the sides of the piles in both cases, utilizing the tipple ramps. Holes were spaced randomly up the ramps and around the base of the piles. In most cases, the backhoe penetrated 2 to 3 meters into the material before a sample was collected. Approximately 350 kg. of dump material was composited from the various trench sites for each sample. The composite was then coned and quartered several times to reduce the shipped sample weight to approximately 50 kg. for each sample.

Dry screening and float-sink testing was conducted on each sample. The results are documented in the following tables.

Results of the dry screening are tabulated in Table 2. It should be noted that between 11 and 14 % of the total sample is greater than the 1 in. (25 mm.) size. Also, approximately 1/3 of the total samples are smaller than 10 mesh. (1.7

The dry screen analysis was performed in order to determine whether a particular size range would have a greater or lesser coal content. The data shows that the ash percent of all size fractions is quite similar, except a slight decrease in ash in the finer sizes. Screening does little to enhance

SIZE F INCHES	RANGE MM	DIR WT. %	ECT ASH %	% WT. ASH OF TOTAL	CUM. WT. % ASH	CUMULATIV WT. %	E OVERSIZE ASH %
SAMPLE#1 +2 +1 + $\frac{1}{2}$ + $\frac{1}{2}$ + $\frac{1}{4}$ + 1/8 + 1/16 - 1/16	Extensic +50 +25 +13 +6 +3 +1.5 -1.5	n) 4.43 9.43 9.30 14.21 14.71 16.71 31.22	80.69 75.44 67.19 62.49 63.99 66.08 66.16	3.16 7.11 6.25 8.88 9.41 11.04 20.66	3.16 10.27 16.52 25.40 34.81 45.85 66.51	4.43 13.86 23.16 37.37 52.08 68.79 100.01	71.33 74.10 71.34 67.97 66.84 66.65 66.51
SAMPLE #2 +2 +1 + $\frac{1}{2}$ + $\frac{1}{2}$ + 1/8 + 1/16 - 1/16	+50 +25 +13 +6 +3	11ingtor 4.71 6.85 10.20 14.80 14.92 15.22 33.32) 67.08 72.08 57.21 55.89 55.98 57.26 58.11	3.16 4.94 5.84 8.27 8.35 8.71 19.36	3.16 8.10 13.94 22.21 30.56 39.27 58.63	4.71 11.56 21.76 36.56 51.48 66.70 100.02	67.09 70.06 64.06 60.75 59.36 58.88 58.63

TABLE 2. - SIZE DISTRIBUTION ANALYSIS

7.

GENERAL TESTING LABORATORIES

DIVISION: SUPERINTENDENCE COMPANY (CANADA) LTD. 1001 EAST PENDER STREET, VANCOUVER, B.C., CANADA V6A 1W2

PHONE (804) 254-1647 TELEX 04-507514 CABLE SUPERVISE

CERTIFICATE OF ANALYSIS

No.:	7907-1014		3.070
FILE:		August 10,	1919

TABLE 3.

WE HEREBY CERTIFY that we have analyzed the submitted samples herein described and report as follows:

Samples marked # 1 and # 2

AS RECEIVED BASISY

TO:

Mr. Steven L. Gardner

V9R 5K3

273 Westwood Road,

R.R. # 3 - Site S.

Nanaimo, B.C.

Volatile Matter Total Moisture Fixed Carbon Ash Sample # 1 9.29% 61.27% 17.79% 11.65% 8.15% 54.86% Sample # 2 19.95% 17.04% Residual Volatile Fixed AIR DRY BASIS: Fraction Ash Sulphur Moisture Matter Carbon % % % % % % 1.66 66.43 19.36 12.55 # 1 Original 0.19 1.78 80.69 14.08 3.45 + 2" 4.43 0.10 75.44 15.83 7.27 1" 9.43 1.46 0.13 + 18.58 + 1/2" 9.30 1.44 67.19 12.79 0.17 + 1/4" 62.49 20.06 15.92 14.21 1.53 0,20 19.83 14.56 + 1/8" 1.62 14.71 63.99 0.20 18.53 66.08 + 1/16" 1.68 13.71 0.18 16.71 - 1/16" 31.22 1.84 66.16 18.54 13.46 0.19 18.19 1.57 58.79 21.45 0.48 #2 Original 67.08 18.31 1.51 13.10 0.49 + 2" 4.71 1.31 17.05 9.56 + 1" 6.85 72.08 0.27 + 1/2" 1.42 57.21 22.05 19.32 0.35 10.20 55.89 + 1/4" 14.80 1.57 22,50 20.04 0.48 1.59 21.96 20.47 + 1/8" 14.92 55.98 0.45 1.60 57.26 21.74 19.40 0.45 + 1/16" 15.22 58.11 21.17 19.05 1.67 0.53 - 1/16" 33.32

Calorific Value on Original Sample # 1 (air dry basis) 3582 BTU/1b. Calorific Value on Original Sample # 2 (air dry basis) 5033 BTU/1b.

Calorific Value and Specific Gravity on Fractions with lowest Ash (air dry basis) Sample # 1 - 1/4" 4111 BTU/1b. Specific Gravity 1.99 g/cm³ Sample # 2 - 1/4" 5485 BTU/1b. Specific Gravity 1.87 g/cm³

NOTE:

Specific Gravity was determined on air dry basis pulps -60 mesh.

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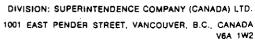
L. Lakosik

THIS COMPANY ACCEPTS NO RESPONSIBILITY EXCEPT FOR THE DUE PERFORM-ANCE OF INSPECTION AND/OR ANALYSIS IN GOOD FAITH AND ACCORDING TO THE RULES OF THE TRADE AND OF SCIENCE. L. Lakosil - Chief Coal Chemist.

Analytical and Consulting Chemists, Bulk Cargo Specialists, Surveyors, Inspectors, Samplers, Weighers

MEMBER: American Society For Testing Materials - The American Oil Chemists' Society - Canadian Testing Association REFEREE AND: OR OFFICIAL CHEMISTS FOR National Institute Of Oilseed Products - The American Oil Chemists' Society OFFICIAL WEIGHMASTERS FOR Vancouver Board Of Trade

GENERAL TESTING LABORATORIES



PHONE (604) 254-1647 TELEX 04-507514 CABLE SUPERVISE

CERTIFICATE OF ANALYSIS

No.:	7908-0905	DATE:
FILE:		August 27, 1979

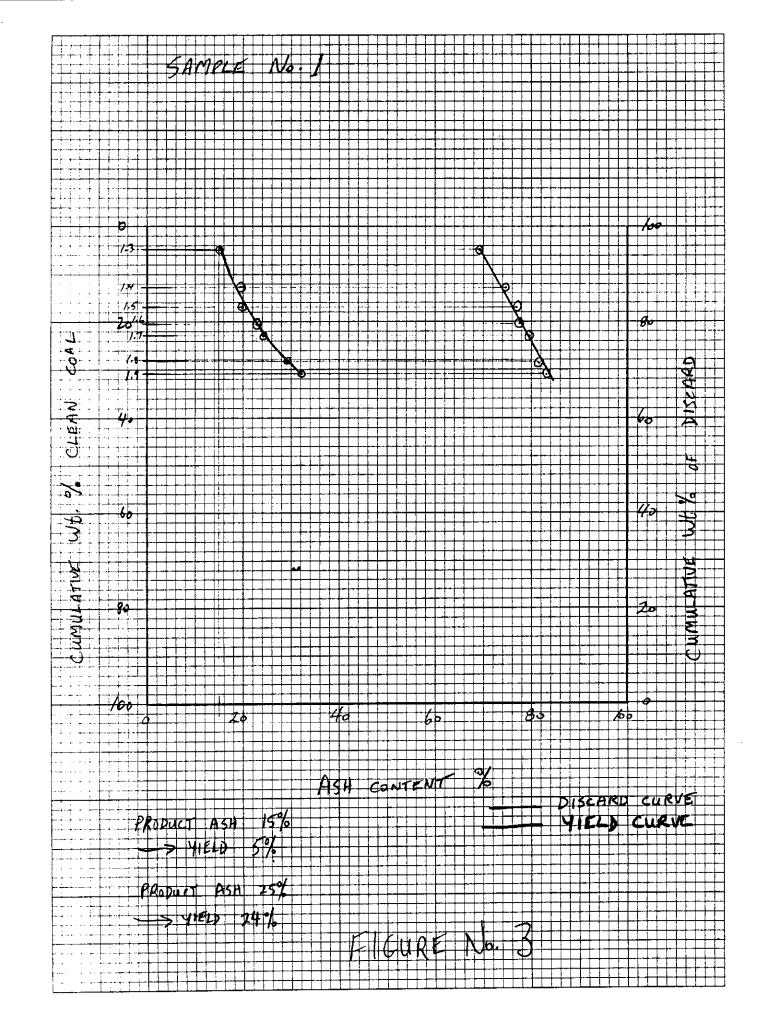
<u># 1 FEED:</u> Air D: SPECIFIC GRAVIT				
	ry asn 00.4 <i>37</i> 0 -	Dry Ash 67.55%		
SECTETC GUNATI.	•	•	SIN	K
<u></u>	- Yield %	Dry Ash %	Yield %	Dry Ash %
1.3	4.53	15.15	95.47	69.16
1.4	12.39	19.26	87.61	74.46
1.5	16.83	19.43	83.17	76.91
1.6 1.7	20.20 23.01	23.12 24.14	79.80 76 .99	77.65 79.59
1.8	28.33	28.85	71.67	81.82
1.9	31.19	32.03	68.81	83.10
1.4 1.5 1.6 1.7 1.8 1.9	18.36 26.94 30.25 34.16 40.23 43.42	11.04 16.94 18.27 19.87 25.30 27.06	81.64 73.06 69.75 65.84 59.77 56.58	70.31 74.37 76.65 79.10 81.01 82.92
			Brihanson	1

Analytical and Consulting Chemists, Bulk Cargo Specialists, Surveyors, Inspectors, Samplers, Weighers

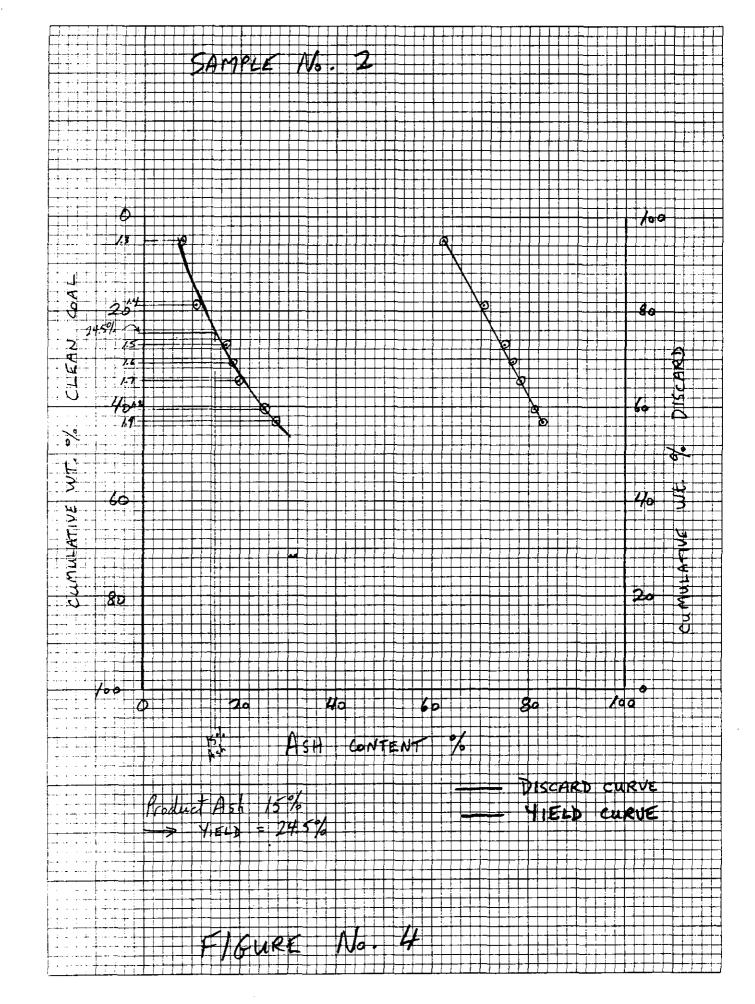
MEMBER: American Society For Testing Materials - The American Oil Chemists' Society - Ganadian Testing Association REFEREE AND/OR OFFICIAL CHEMISTS FOR: National Institute Of Oilseed Products - The American Oil Chemists' Society OFFICIAL WEIGHMASTERS FOR: Vancouver Board Of Trade

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TO: MR. STEVEN L. GARDNER 27月 Westwood Road, R.R. 着 3 - Site S. Nanaimo, B.C. V9R 5K3



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MADE IN U. S. A.

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Section 3.0 (continued)

the quality of the sample, no matter what sieve size is employed.

Float-sink testing was performed on each sample at Relative Density separations of 1.3 to 1.9, on.l increments. The results are tabulated in Table 4. Figures 3 and 4 are graphs showing predicted yields using the float-sink data. Figure 4 (sample No. 2), which is the No. 10 South Wellington Dump, shows a good performance: if product ash is specified at 15%, then the yield can be expected to be 24.5%. The difference in yields between Sample No. 2 and Sample No. 1 is guite apparent when Figures 3 and 4 are compared. Sample No. 1 will hardly produce a 15% ash product and this is cause for concern. One important limiting factor when assessing the validity of the 1979 data is that the material in the composite samples was not separated into size fractions prior to float-sink testing. However, the dry screening data indicates that this should not impact the results to a great extent.

Additional analytical work has been performed by Countryside Coal Processing in 1982 and 1983, however, sampling methods and analyitical procedures are not in the author's possession. Presumably these results will be made available to Esso Resources Ltd.

SECTION 4.

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4.0 DESCRIPTION OF THE RECENT SAMPLING PROGRAM

4.1 Scope of Work

Because of time constraints, Esso Resources Ltd. decided to limit their investigation to the three aforementioned dumps, while at the same time realizing that additional tailings dumps are controlled by Countryside Coal Processing and available for testing.

The two important factors that the initial sampling program was designed to confirm are:

a) The volumes of coal dump material in place in each of the three initial dumps.

b) The relative uniformity, or conversely, the relative variance of the quality of the material within each dump.

In addition to these factors, samples would be used to provide more information on the actual make-up of the dump material and its cleaning characteristics.

4.2 Methods of Sampling

Two major sampling methods were employed in the course of the program - drillhole sampling and trenching. Each method is described below:

1. Drillhole sampling: Because of the height of the piles (up to 45 meters) and the diverse nature of the material within the piles, which ranged from the normal coal tailings to a collection of mine timbers, peices of scrap metal and other articles, an augur system, which would have been more preferable in terms of size range of material collected, was ruled out. The alternative was drilling. An air-rotary rig equipped with a casing hammer was selected. The casing hammer equipment was necessary for three reasons:

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Section 4.2 (continued)

a) it prevented up-hole caving by setting casing immediately behind the drill bit, thus assuring the catchment of representative samples through the entire depth of the pile,

b) it allowed the casing to be driven through obstructions such as timbers, which were common occurrences in the course of the drilling, and

c) it allowed for the complete catchment of drill samples by discharging the entire amount of sample material through a 6 meter long flexible spout.

Samples were collected in 3 meter intervals in all of drillholes. The tailings material was discharged from the spout assembly into metal pails, then transferred directly to properly-labelled large fibre shipping bags. As instructed by Esso Resources Ltd., no coning and quartering was done prior to shipment. No water or other circulation additives were added to the air-flushing system, so that as-received moistures reflect the total moisture contents of each sample.

The biggest drawback of the drilling technique is that it alters the size consist of the material by the action of the drill bit. This alteration of the size consist and its ramifications on coal quality and ash content of the individual reporting size fractions was not forecast to be great, considering the relatively uniform distribution of ash through all size ranges (see Table 2).

2. Trench Sampling: In order to provide a comparison of unaltered sample material with the crushed drill cuttings samples, a number of trenches were dug and sampled. A tractor-mounted backhoe was employed for this work. Selected trench locations included the collars of the drillholes so that the trench samples could be directly compared to the upper sample intervals of the drillholes. Other trench sample locations included random trenches

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Section 4.2 (continued)

around the toe of the dump piles. The backhoe trenched in to maximum digging depth before the sample was collected. These samples were transferred directly into large, properly labelled fibre shipping bags of the type used for the drillhole samples. Again, no coning and quartering of the sample was done proir to shipment, as instructed by Esso Resources Ltd.

4.3 Surveying

As part of the sampling program, initial survey work on both the Extension No. 1 Mine Dump and the South Wellington No. 10 Mine Dump was conducted. This consisted of stadia traverses that tied in the drillhole and trench sample locations, and provided elevations and survey control on the dumps. Contour drawings of the dump sites on a scale of 1:500 were then produced.

This type of detailed survey work was not undertaken on the Extension No. 4 dump site, however in order to effect some measurements on the volume of material in this dump, chainages and elevations were measured around the toe and the top of the slope with the aid of a rod, level and chain. A 1:500 scale plan was also produced for this dump (see Appendix III).

4.4 The South Wellington No. 10 Mine Dump

Investigations of the South Wellington No. 10 Mine Dump near Beck Lake consisted of four drillholes and five trench locations. The four drillholes, labelled SW-83-01 to SW-83-04 inclusively, were completed in 26 operating hours. A total of 101 drilled meters were completed. The deepest hole was SW-83-02, which ended in brown peat at 29.5 meters.

A surface trench to a maximum depth of 5 meters was

4.4 (continued)

completed by the backhoe beside the collar of each drillhole. In addition, one surface trench at the toe of the dump on the west side was dug.

Appendix I consists of plans and sections of the South Wellington No. 10 Mine Dump, with drillhole locations and section lines shown.

Table 5. details volume calculations for the South Wellington Mine Dump. These volumes were calculated by section according to the sections drawn up in Appendix I. Total volume of material for this dump is estimated at 220,000 cubic meters (288,000 Cu. Yds.). Assuming an average Relative Density of 1.87 g/cc. as documented in Table 3., the total tonnage works out to 412,000 tonnes.

Table 6. lists the sample inventory for the South Wellington Dump as shipped to General Testing Laboratories in Vancouver for analysis.

In general, the tailings material in the South Wellington No. 10 Dump was quite uniform in all the holes. However, holes SW-83-01 and SW-83-04 intersected a lot of timber. A strong smell of gas occurred right at the base of the dump directly above the water table in holes 01, 02 and 03. TABLE 5. - SOUTH WELLINGTON No. 10 DUMP

SECTION No.	AREA (m²)	D	VOLUME (m ³)
510 N	0	0	
JIC N	0	20	2,100
490 N	210	20	8,420
470 N	632	20	8,420
470 M	032	20	19,210
450 N	1289	20	30,140
430 N	1725	20	50,140
		20	37,550
410 N	2030	20	36,530
390 N	1623		
		20	34,810
370 N	1858	20	32,070
350 N	1349		
		20	16,390
330 N	290	20	2,900
310 N -	0		

220,120 m³ (288,357 cu.yd.)

=411,600 tonnes

(453,583 short tons)

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HOLE NO./TRENCH No.	SAMPLE NO.	SAMPLE INTERVAL	No. of BAGS
SW-83-01	<u></u>	(meters)	2
	1	0 - 3.0	2
11	2	3.0 - 6.0	1
n	3	6.0 - 9.0	2
11	4	9.0 - 12.0	2
	5	12.0 - 15.0	2
	6	15.0 - 18.0	2
11	7	18.0 - 21.0	2
	8	21.0 - 24.0	2
	9	24.0 - 25.5	
	10	25.0 - 27.0	i î
11	11	1	
		27.0 - 28.0	L _
SW-83-02	1	0 — 3.0	2
n	2	3.0 - 6.0	2
11	3	6.0 - 9.0	3
	4	9.0 - 12.0	3
	5	12.0 - 15.0	3
11	6	15.0 - 18.0	3
	7	18.0 - 21.0	3
- 11	8	21.0 - 24.0	3
	9		3
		24.0 - 27.0	3
••	10	27.0 - 29.5	3
SW-83-03	1	0 - 3.0	2
	2	3.0 - 6.0	2
IT	3	6.0 - 9.0	3
11	4	9.0 - 12.0	3
u	5	12.0 - 15.0	3
n	6	15.0 - 18.0	3
"	7	18.0 - 21.0	3
11	8	21.0 - 24.0	3
10	9	24.0 - 25.5	1
5. C			- -
SW-83-04	1	0 - 3.0	2
P	2	3.0 - 6.0	
IŤ	3	6.0 - 9.0	1 2
71	4	9.0 - 12.0	3
	5	12.0 - 15.0	3
11	6	15.0 - 17.0	3
		10.0 17.0	
SW-83-01(TRENCH)	1	-	4
SW-83-02 (TRENCH)	1	1 _	4
SW-83-03 (TRENCH)	1	_	4
SW-83-03 (TRENCH) SW-83-04 (TRENCH)	1	_	4
SW = 83 = 04 (TRENCH) SW = 83 = 05 (TRENCH)			4
SW-03-03(TRENCH)	1 +	-	7

Total No. of Samples: 41

4.5 The Extension No. 1 Mine Dump

Investigations of the Extension No. 1 Mine Dump consisted of three drillholes and four trench locations. The three drillholes, labelled EX-83-01 to EX-83-03 inclusively, for a total of 113.5 meters, were completed in 31 operating hours. The deepest of these holes was EX-83-01, which ended in brown peat and gravel at 51 m.

A trench, labelled EX-83-04 TRENCH, was located in the road cut beside drillhole EX-83-02 but above the collar. A second trench was completed beside the collar of drillhole EX-83-03 (labelled EX-83-05 TRENCH). Trenches labelled EX-83-06 TRENCH and EX-83-07 TRENCH were completed at the toe of the dump on the west side.

Appendix II consists of plans and sections of the Extension No. 1 Mine Dump, with drillhole locations and section lines shown.

Table 7. details volume calculations for the Extension No. 1 Mine Dump. These volumes were calculated by section according to the sections drawn up in Appendix II. Total volume of material for this dump is estimated at 369,000 cubic meters (483,000 cu. yds.). Assuming an average Relative Density of 1.99 g/cc. as documented in Table 3., the total tonnage works out to 734,000 tonnes. Some additional tonnage occurs under the approach road to the dump area, which is an old railway grade built of tailings.

In general, the tailings material sampled in the drillholes and trenches on the Extension No. 1 Mine Dump appeared dirty with abundant shale material throughout. Some lenses of red clinker and burned shale were encountered in both the backhoe trenches and in the drillholes, especially near the base of the pile in holes EX-83-01 and EX-83 -02. It is not known whether this burned material was dumped on the site or whether it burned in place.

Table 8. lists the sampleinventory for this dump as shipped to General Testing Labs for analysis.

TABLE 7. - EXTENSION No. 1 DUMP VOLUME CALCULATIONS

0 827 2700 3514 3620	20 20 20 20 20 20	8270 35270 62140 71340 67140
2700 3514 3620	20 20 20	35270 62140 71340
3514 3620	20 20	62140 71340
3514 3620	20	71340
3620		
	20	67140
3094	20	52810
2187		
1596	20	37830
	20	23010
705	20	9070
202	20	2020
o		
	1596 705 202 0	1596 20 705 20 202 20

TOTAL:

368,900 m³ (483,259 cu.yd.)

Assume an S.G. of 1.99 gm/cm³ (see Table 3) 734,111 tonnes

(808,990 short tons)

TABLE 8. - SAMPLE INVENTORY - EXTENSION No. 1 DUMP

HOLE NO./TRENCH NO.	SAMPLE No.	SAMPLE INTERVAL (meters)	No. of BAGS
EX-83-01	l	0 - 3.0	2
	2	3.0 - 6.0	2
11	3	6.0 - 9.0	3
п	4	9.0 - 12.0	3
п	5	12.0 - 15.0	3
	6	15.0 - 18.0	3
	7	13.0 - 18.0 18.0 - 21.0	3
11	8	21.0 - 24.0	3
	9	24.0 - 27.0	3
	10	27.0 - 30.0	3
11	11	30.0 - 33.0	3
п	12	33.0 - 36.0	3
91	13	36.0 - 39.0	3
11	14	39.0 - 42.0	3
11	15	42.0 - 45.0	3
"	16	45.0 - 48.0	3
11	17	48.0 — 51.0	3
EX-83-02	1	0 - 3.0	3
"	2	3.0 - 6.0	3
"	3	6.0 - 9.0	3
n	4	9.0 - 12.0	3
п	5	12.0 - 15.0	3
	6	15.0 - 18.0	3
90	7	18.0 - 21.0	3
"	8	21.0 - 24.0	3
11	9	24.0 - 27.0	3
п	10	27.0 - 30.0	3
0	11	30.0 - 33.0	3
п	12		
		33.0 - 35.0	3
	13	35.0 - 37.5	1
EX-83-03	1	0 - 3.0	2
"	2	3.0 - 6.0	3
11	3	6.0 - 9.0	3
11	4	9.0 - 12.0	3
и	5	12.0 - 15.0	3
н	6	15.0 - 18.0	3
n	7	18.0 - 21.0	3
n	8	21.0 - 24.0	3
п	9	24.0 - 27.0	1
EX-83-04 TRENCH	1	_	4
EX-83-05 TRENCH	1		4
EX-83-06 TRENCH	1	_	3
EX-83-07 TRENCH	1	_	3
EX-03-07 IRENCH	±		5

TABLE 9	. –	EXTENSION	No.	4	DUMP	VOLUME	CALCULATIONS
---------	-----	-----------	-----	---	------	--------	--------------

SECTION No.	AREA (m²)	ΔD	VOLUME (m ³)
0+260	0	45	11,228
0+215	499	106	57,770
0+109	591	61	30,897
0+048	422	56	11,816
0-008	0		

TOTAL:

111,711 m³
(146,341 cu. yd.)

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Assume an S.G. of 1.87 gm./cc.*

208,900 tonnes total material (230,208 short tons)

* Equivalent to S.G. of No. 10 South Wellington Dump, which appears to be of similar coal content.

4.6 The Extension No. 4 Mine Dump

No drilling was performed on the Extension No. 4 Mine Dump, however a total of six backhoe trenches on the dump were completed, with approximately 150 kg. of material shipped from each trench. Only thesouth end of the dump was investigated, as there was some question as to surface rights ownership (the owner of a house located near the northwest end of the dump came over during the sampling program and claimed that the north end of the dump was on his property).

Appendix III consists of plan and sections of the Extension No. 4 Mine Dump, with trench locations and section lines shown.

Table 9. details volume calculations for this dump. These volumes were calculated by section according to the drawings in Appendix III. Total volume of material for this dump is estimated at 112,000 cubic meters, or 147,000 cu. yds.. Assuming a Relative Density of 1.87 g/cc. (equivalent to the South Wellington Dump, which appears of similar quality), the total tonnage works out to about 209,000 tonnes.

Table 10 lists the sample inventory for the Extension No. 4 Mine Dump, as shipped to General Testing Labs-

		Labe)		_	No. of Bags
No.	4	Dump	Trench	No.	l	4
No.	4	Dump	Trench	No.	2	4
No.	4	Dump	Trench	No.	3	4
No.	4	Dump	Trench	No.	4	4
No.	4	Dump	Trench	No.	5	4
No.	4	Dump	Trench	No.	6	4

TABLE 10. : SAMPLE INVENTORY, EXTENSION No. 4 DUMP

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5.0 SUMMARY AND CONCLUSIONS

On-site investigations of three major coal tailings dumps in the Nanaimo area of Vancouver Island were conducted by Esso Resources Ltd. in September of 1983. These on-site investigations were designed to estimate volumes of dump material in place and to determine the relative uniformity of tailings throughout each tailings pile. Samples of the tailings from each site would be used to evaluate the cleaning characteristics of the coal tailings, with a view to determining the economic viability of recovering clean coal product from the dumps.

Two sampling techniques were employed in the course of the program - drillhole sampling and trench sampling. The drillhole sampling would provide information on the coal content of the tailings through the entire thickness of dump material by sampling on 3 meter intervals. Because the drilling method crushed the top sizes of material, a number of backhoe trenches located in various spots on and around the piles would provide an undisturbed sample for comparisons with the drillhole data.

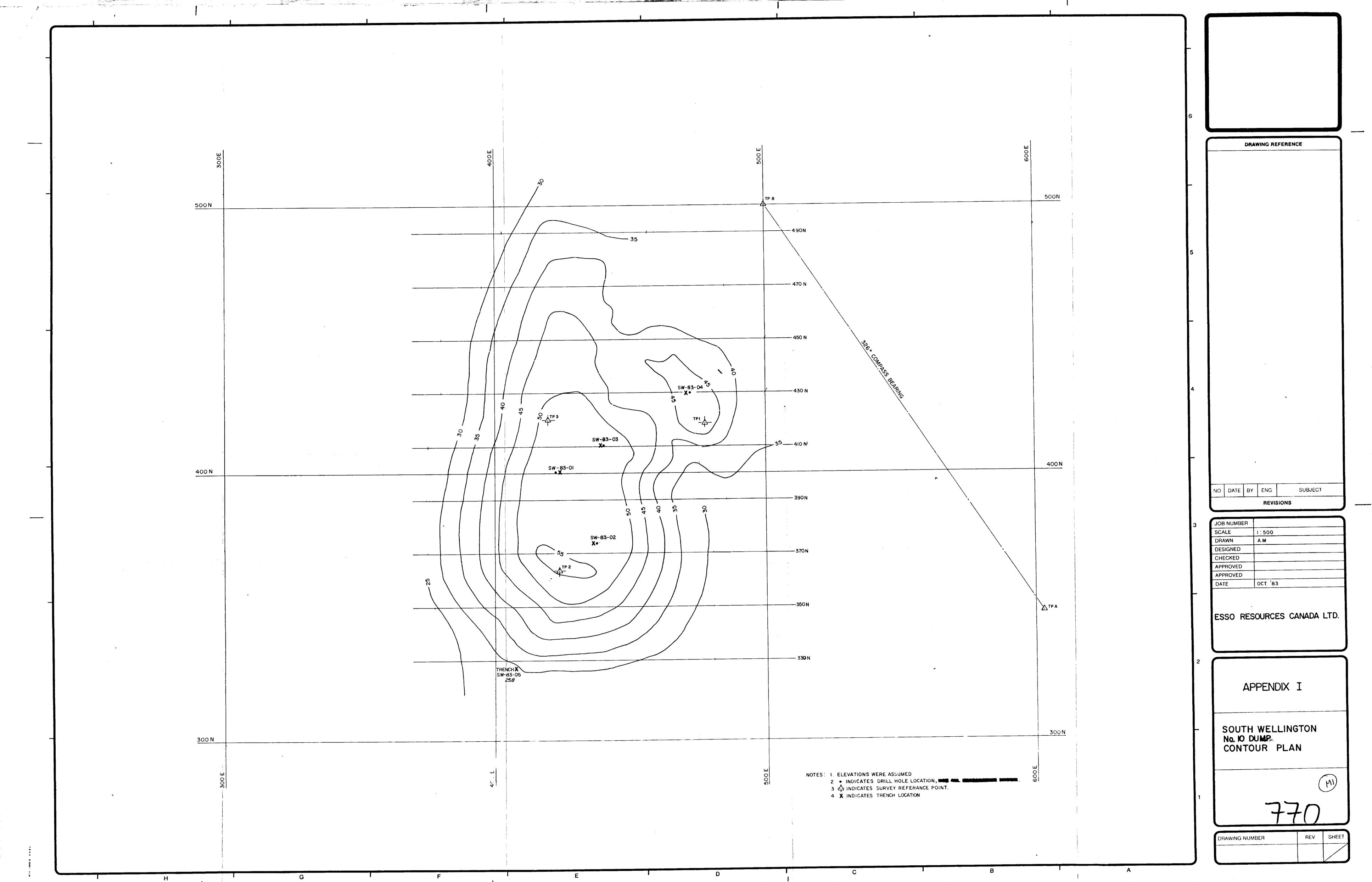
Volume calculations as a result of the survey work identified a total of 701,000 cubic meters of tailings material, of which 220,000 cubic meters is contained in the South Wellington No. 10 Mine Dump, 369,000 cubic meters in the Extension No. 1 Mine Dump, and 112,000 cubic meters in the Extension No. 4 Mine Dump. Additional volumes of material can be found in numerous other dump sites in the Nanaimo area, which were not part of this study.

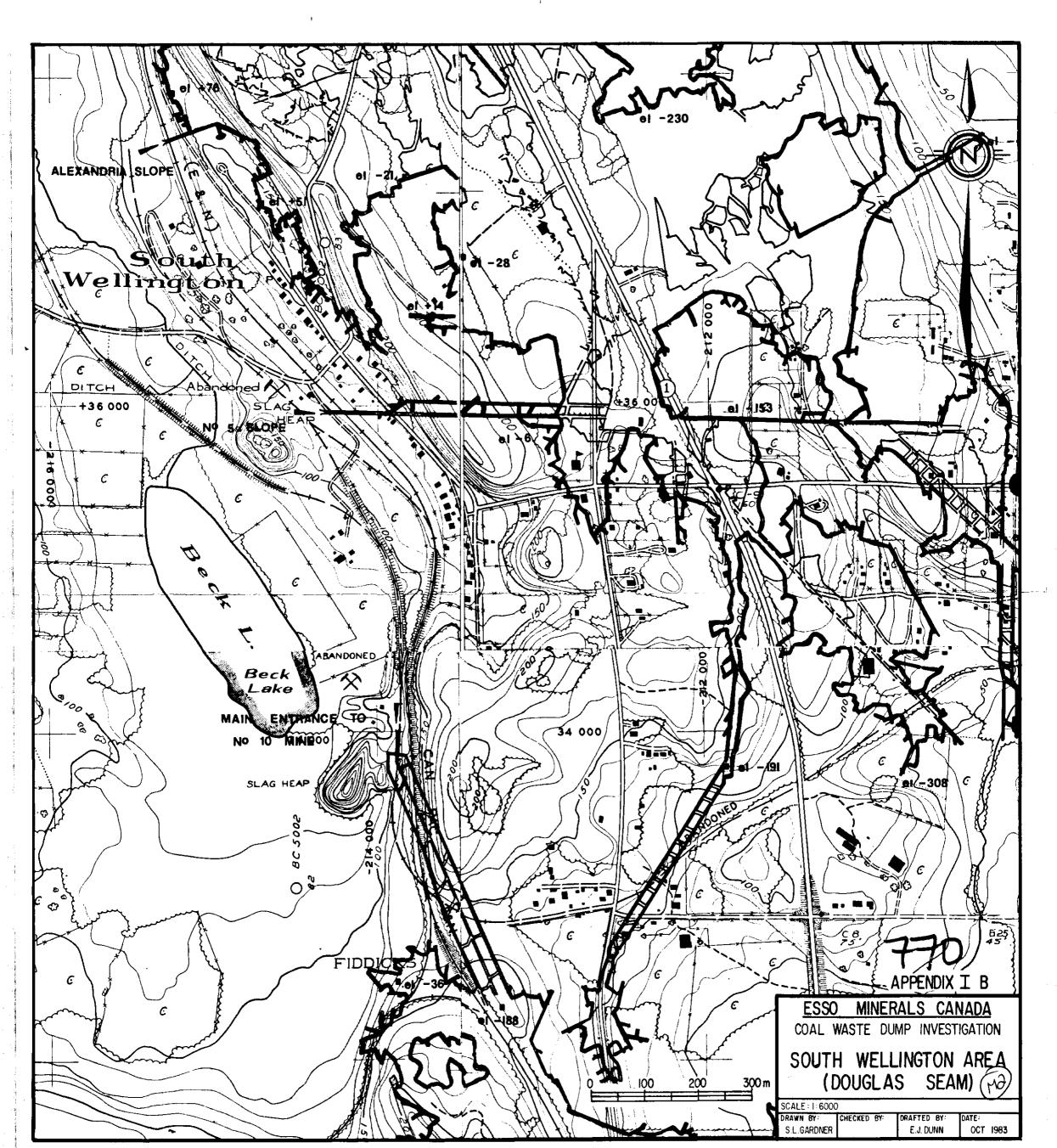
A total of seven drillholes and seventeen backhoe trenches were completed on the dump sites for an approximate total cost of \$ 20,000.00. This work resulted in the collection of 90 samples for shipment to the laboratory for analytical work.

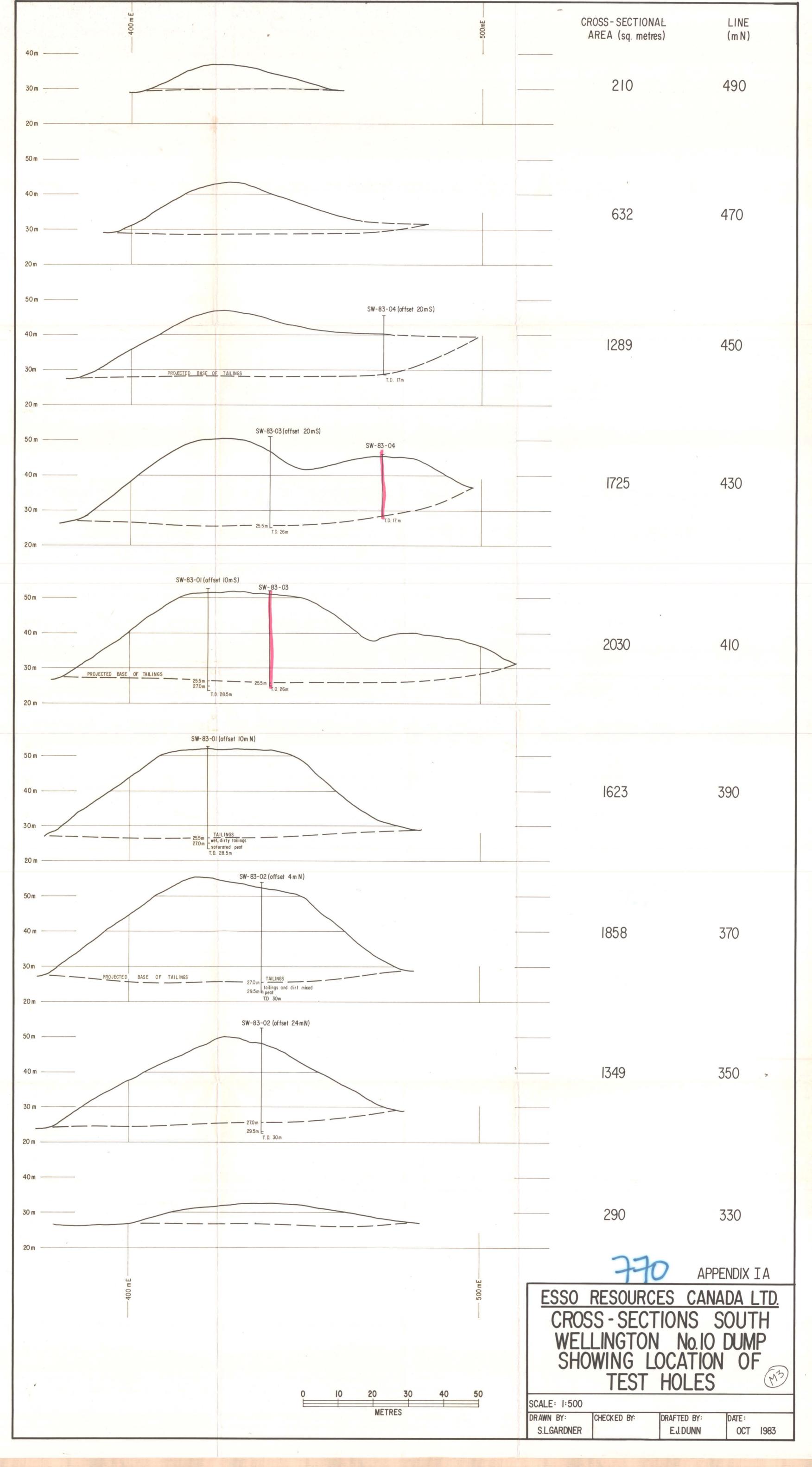
APPENDIX I.

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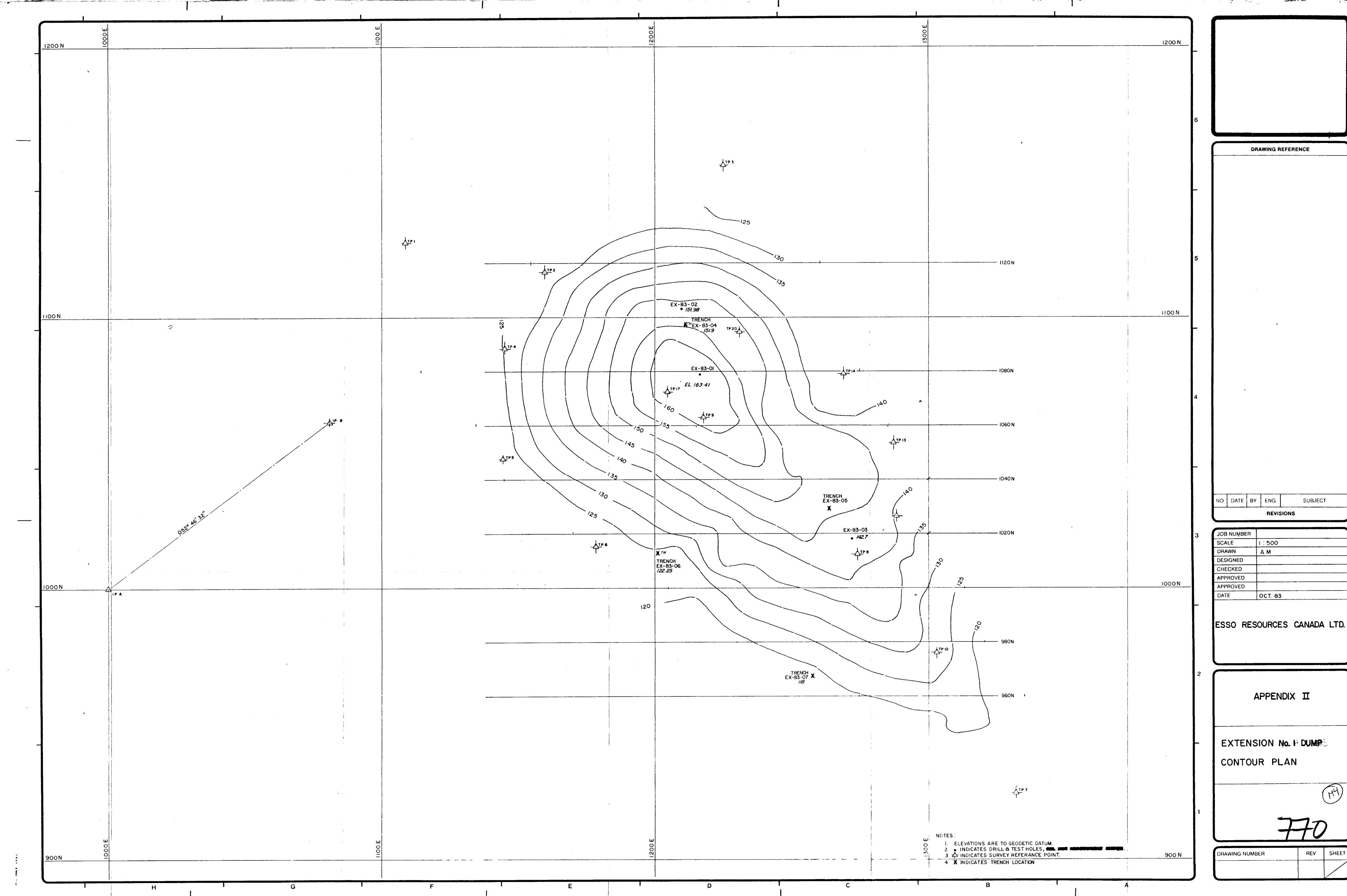


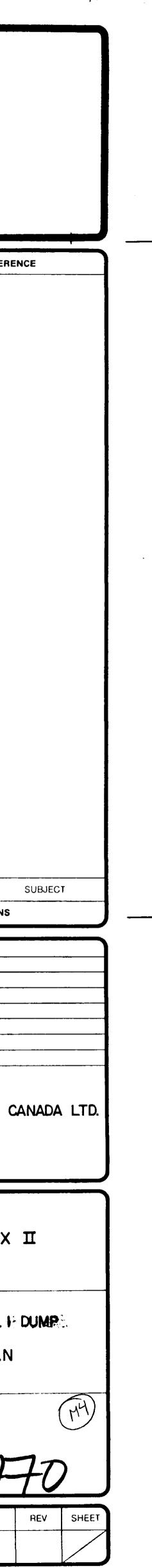


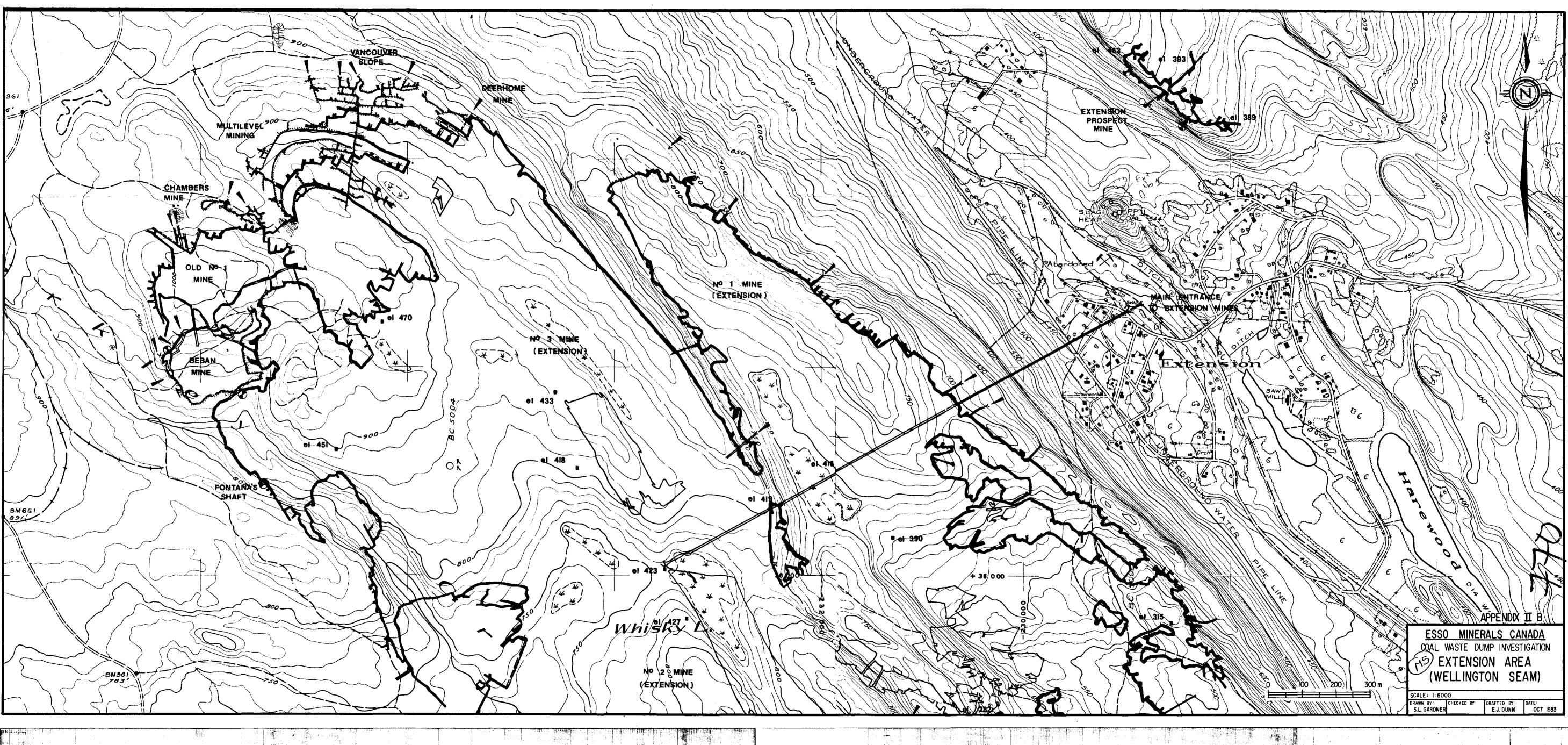


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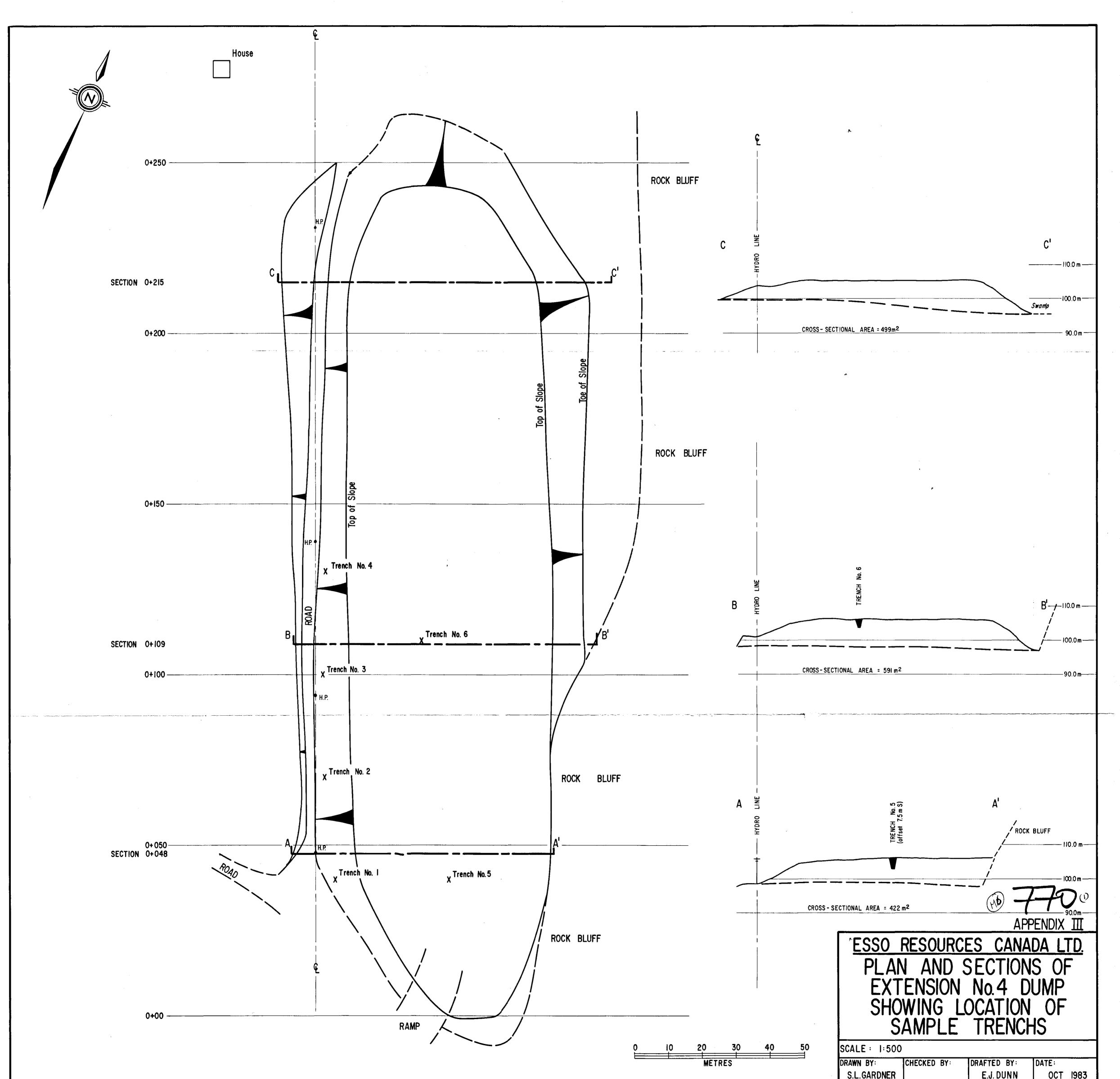
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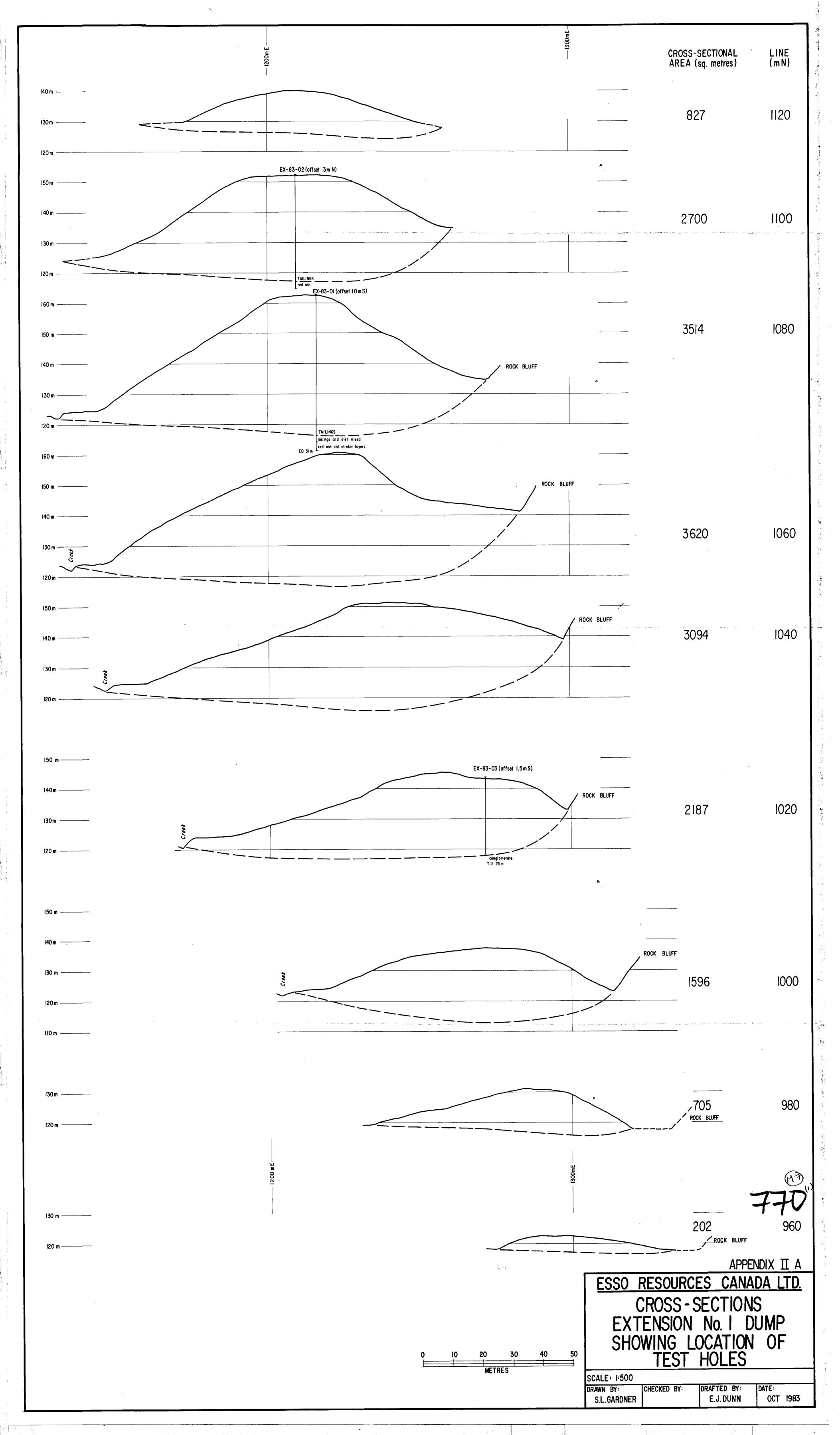






i.





NANAIMO STOCKPILE - OCTOBER 1983

DRILL HOLE SAMPLES

LABORATORY REPORTS

ERCL

ESSO MINERALS CANADA A DIVISION OF ESSO RESOURCES CANADA LTD. 237-4TH AVENUE S.W. - CALGARY - ALBERTA T2P OH6 EXPLORATION MANAGER : MR. HUGH JONES

ANALYTICAL WORK ACCORDING TO ASTM PERFORMED BY : GENERAL TESTING LABORATORIES A DIVISION OF SGS SUPERVISION SERVICES INC. 1707 FRANKLIN ST - VANCOUVER B.C. - CANADA - V5L 1P6 TELEX : 04-507514 - PHONE : (604) 254-2148 CHIEF CHEMIST : L.M. LAKOSIL

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L. Lakosil Styphen L. Gardner то 🗟 GENERAL TESTING LABS oper Esso Resources VANCOUVER B.C. Nanaimo B.C. SUBJECT SAMPLE INVENTORY - EXTENSION DUMP - HOLE EX-83-01 Sept. 25 19 **B**Z. DATE SAMP INTERVAL (m) No. - F Bags (MTERVAL (m) No. of Bag SAMPLE No. NP 0-3.0 m. 2 33.0-36.0 m. 3 12 2 3.0-6.0 m. 36.0 - 39.0 m. 3. 13 14 3 3 6.0 - 9.0 m. 39. o - 42. o m. 3 42.0-45.0 m. 3 4 15 9.0- 12.0m 3 3 12.0 - 15.0 m. 45.0 - 48.0 .. 5 16 3 3 48.0 -51.0m 6 17 15.0 - 18.0 m. 3 TOTAL BAGS 49 180-21.0 $\mathcal B$ 21.0 - 24.0 3 9 3 24.0 - 27.0 3 10 27.0 - 30.0 30.0 - 33.0 3. SIGNED

AREDILETTER

Stephen L. Gardner 10 h. LeposIL GENERAL TESTING LABS PER ESSO RESOURCES KTIP VANCOUVER B.C. NANAIMO B.C. IUBJECT SAMPLE INVENTORY - EXTENSION HOLE EX-83-02 Sept. 27 19 83 DATE SAMPLENO. INTERNAL (M.) NO. of BAGS 0 - 3.03, 3' - 6.0 3.0 3. 9.0 6.0 3 9.0 4 - 12,0 Ŝ, 5 12.0 - 15.0 3. 18.0 6 15.0 2 3-21,0 18.0 \mathscr{B} 3-21,0 - 24.0 3-9 24.0 - 27.0 27.0 3 30.0 10 MM 30.D ||_________ 33.0 35.0 SIGNED 12 SOASE MOORE RUSINESS FORMS

(REDI-LETTER)

L. LQKOSTL STEPHEN L GARDNER GENERAL TESTING LABS PER ESSO RESOURCES LAP TO L. LakosTL VANCOUVER BC. NANAEMO B.C. SUBJECT SAMPLE INVENTORY - EXTENSION HOLE EX-B3-03 .19 **83** Sept. 28 DATE INTERVAL (M.) NO. of BAGS SAMPHE NO. 2 0-3.0 3.0-60 3 6.0 - 9.0 3 9.0 - 12.0 3 3 12.0 -15.0 3 18:0 6 15.0 -21.0 3 18.0 \mathcal{B} 24.0 21.0 -27.0 9 24.0 EDIFORM 45065E MOORE BUSINESS FORMS 3

AREDI-LETTER

TO L. Lakosil Styphen L. Gardner 6 40 ESSO RESOURCES GENERAL TESTING LABS NANAIMO, B.C. VANCOUVER, B.C. SUBJECT SAMPLE INVENTORY: South Wallington Dump: Hok 5W-83-01 DATE Sept. 23 198 1983 Number of Bags INTERVAL (m.) SAMPLE No. 0-3.0 2 t 3.0-6.0 2 6.0 -9.0 3 2 2 4 9.0 - 12.0 2 12.0 - 15.0 15.0 -18.0 2-18.0 -21.0 2 7 21.0-24.0 в 24.0-25.5 9 25.5 - 27.0 10 27.0 - 28.0 (Total 18 bags) 11 SIGNED EDIEGRIA ASORSE MOORE BUSINESS FORMS 3

AREDI-LETTER

TOI / Lakosil Stephen L. Gardner GENERAL TESTING LABS o per/ ESSO RESOURCES LTD. NANAIMO B.C. VANCOUVER B.C. SUBJECT SAMPLE INVENTORY : South Wellington Dump: Hole SW-83-02 DATE Sept. 24 1983 Number of Bags SAMPLE No. INTERVAL (m.) 0-3.0 3.0-6.0 6.0 - 9.0 3 9.0 - 12.0 4 3 12.0 - 15.0 15.0 - 18.0 3 3 18.0 - 21.0 3 21.0 - 24.0 3 24.0 - 27.0 27.0 - 29.5 b 28 TOTAL SIGNED DOW ENVELOPE DIFORM 45065E MOORE BUSINESS FORMS 3

(REDI-LETTER)

TOT L. Lakosil Staphen L. Gardner 0 274 Westwood Rd. GENERAL TESTING LABS Nanaimo, B.C. VANCOUVER, B.C. SUBJECT ESSO RESOURCES WASTE DUMP, NUESTIGATION - SAMPLE INVENDAY Sept. 24 19 83 DATE Hole 5w- 83-03 No. of Bays SAMPLE No. INTERVAL (m.) 0-3.0 2 2 3.0-6.0 3 3 6.0-9.0 3 4 9.0-12.0 3 12.0-15-0 3 15.0-18.0 3 18.0 -21.0 71.0 -24.0 3 в 24.0-25.5 m 23 TOTAL SIGNED EDIFORM ASDREE MOORE BUSINESS FORMS 3

(REDI-LETTER)

L. Lakosil Stephen L. Gardner . TO 📑 o pur/ESSO RESOURCES GENERAL TESTING LABS JANCOUVER, B.C. NANAIMO, B.C. BUBJECT SAMPLE INVENTORY - HOLE SW- 83-04 DATE Sept. 25 19 834 No. of Bags INTERVAL (m) SAMPLE No. 0-3.0 3.0-6.0 6.0-9.0 Ŀ 3 4 9.0 -12.0 3 12.0 -15.0 3_ 15.0 - 17.0 TOTAL 14 SIGNED EDIFORM 45065E MOORE BUSINESS FORMS 3 **REDI-LETTER**

General Testing Laboratories A Division of SGS Supervision Services Inc.



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TO: Attn: Mr. Hugh Jones ESSO MINERALS CANADA A Division of ESSO RESOURCES CANADA LTD., 237-4th Avenue S.E. T2P OH6 Calgary, Alberta,

1001 East Pender Street. Vancouver, B.C. Canada V6A 1W2 Telephone: (604) 254-1647 Telex: 04-507514 Cable: Supervise

CERTIFICATE OF ANALYSIS

No.	DATE:	
FILE: 8310-1858C	NOV. 3	. 1983

WE HAVE ANALYZED the herein described submitted sample, and report as follows: NANAIMO COAL DUMPS DESCRIPTION:

Marked as below

LAB I.D.	DRILL HOLE	ASH	CUBIC FOOT WEIGHT	SPECIFIC GRAVITY
	NUMBER	& AIR DRY	KG	Grams/cm ³
EH 3	EX83-01- 3	65.07	38.15	1.92
EH 13	-13	72.43	38.80	2.04
EH 19	EX83-02- 2	62.92	36.10	1.92
EH 29	-12	75.77	40.80	2.18
EH 31	EX83-03- 1	69.42	36.10	2.06 2.08
EH 38	- 8	71.75	39.60	
EH 41	SW83-01- 2	56.70	34.90	1.84
EH 47	- 8	70.40	40.60	2.08
EH 51	SW83-02- 1	59.61	37.00	1.89
EH 60	-10	64.60	34.90	1.93
EH 63	SW83-03- 3	62.12	36.85	1.94
EH 68	- 8	62.33	35.50	1.91
EH 70	SW83-04- 1	56.05	34.50	1.81
EH 75	- 6	59.91	36.30	1.79

1. All cubic foot weight tightly packed in the container, NOT free NOTES: loaded.

2. Specific gravity determined by water displacement method.

THIS COMPANY ACCEPTS NO RESPONSIBILITY EXCEPT FOR THE DUE PERFORMANCE. OF INSPECTION AND/OR ANALYSIS IN GOOD FAITH AND ACCORDING TO THE RULES OF THE TRADE AND OF SCIENCE

L. Lakosil - Chief Coal Chemist

Lakor

SIGNATURE AND TITLE

Analytical and Consulting Chemists, Bulk Cargo Specialists, Surveyors, Inspectors, Samplers, Weighers MEMBER American Society For Testing Materials - The American Oil Chemists Society - Canadian Testing Association REFEREE AND OR OFFICIAL CHEMISTS FOR - National Institute of Oilseed Products - The American Oil Chemists Society OFFICIAL WEIGHMASTERS FOR Vancouver Board of Trade

=							
SAMPLE	+1" <u>%</u>	1"x2" 	2"x2" 	オ"x28M 	28Mx100M 7	100Mx0	
EX-83-03-1	none	none	12.43	49.80	22.16	15.61	
EX-83-03-2	none	none	25.56	46.61	16.95	10.88	
SW-83-03-1	none	none	6.07	49.68	27.04	17.21	
SW-83-03-2	none	none	6.39	44.52	29.43	19.66	

PRELIMINARY SIEVE ANALYSIS ON SELECTED DRILL HOLE SAMPLES

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ESSO - EX-83-01

DRILL HOLES - Total Moisture, Proximate

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	SMPL	MOIST A.D.		BASIS	R.M.	ASH	V.M.	F.C.
	NO	X.	Z Z		7	%	74	%
a mini	EX-83-01-1 EH 1	2.90	3.40	A.D. DRY	0.52	62.48 62.81	19.81 19.92	17.19 17.27
	EX-83-01-2 EH 2	4.08	4.60	A.D. DRY		66.11 66.47		14.57 14.65
a na	EX-83-01-3 EH 3	3.61	4.19	A.D. DRY		65,07 65.47		
~	EX-83-01-4 EH 4	3.66	4.11	A.D. DRY		68.68 69.00		
	EX-83-01-5 EH 5	з.90	4.39	A.D. DRY		65.84 66.17		14.82 14.90
•	EX-83-01-6 EH 6	3.43	3.88	A.D. DRY		67.42 67.74		13.49 13.55
-	EX-83-01-7 EH 7	3.82	4.29	A.D. DRY		66.26 66.58		14.08 14.16
-	EX-83-01-8 EH 8	3.81	4.23	A.D. DRY	0.44 -		18.38 18.46	13.64 13.70
-	EX-83-01-9 EH 9	3.81	4.32	A.D. DRY	0.53	71.17 71.55		11.35 11.41
	EX-83-01-10 EH 10	з . 98	4.31	A.D. DRY	0.34 -	73.07 73.31	17.21 17.27	
	EX-83-01-11 EH 11	4.05	4.35	A.D. DRY	0.31		16.91 16.96	
	EX-83-01-12 EH 12	4.40	4.70	A.D. DRY	0.31		15.69 15.74	10.60 10.64

ESSO - EX-83-01

DRILL HOLES - Total Moisture, Proximate

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	SMPL NO	MOIS A.D.	TURE T.M.	BASIS	R.M.	ASH	V.M.	F.C.
	140	%	%		%	7.	7.	X
	EX-83-01-13 EH 13	4.15	4.49	A.D. DRY	0.35	72.43 72.69	17.17 17.23	10.05 10.08
	EX-83-01-14 EH 14	3.65	3.96	A.D. DRY	-0.32	72.66 72.89	18.83 18.89	8.19 8.22
	EX-83-01-15 EH 15	7.65	8.00	A.D. DRY	0.38 -	73.86 74.14	11.68 11.72	14.08 14.14
	EX-83-01-16 EH 16	8.40	9.07	A.D. DRY	0.73	79.12 79.70	10.53 10.61	9.62 9.69
a ilini)	EX-83-01-17 EH 17	14.50	16.93	A.D. DRY	2.84	73.16 75.30	12.24 12.60	11.76 12.10

ESSO - EX-83-02

	SMPL NO	MOIST A.D.	URE T.M.	BASIS	R.M.	ASH	V.M.	F.C.
-		%	7		7.	7	7	%
_	EX-83-02-1 EH 18	3.30	3.98	A.D. DRY	0.70	69.70 70.20		12.91 12.99
	EX-83-02-2 EH 19	2.51	2.98	A.D. DRY	0.48	62.92 63.23	19.77 19.87	16.83 16.90
	EX-83-02-3 EH 20	3.89	4.33	A.D. DRY	0.46		18.73 18.82	13.10 13.16
-	EX-83-02-4 EH 21	4.03	4.45	A.D. DRY	0.44	70.23 70.54		12.34 12.39
-	EX-83-02-5 EH 22	3.92	4.32	A.D. DRY	0.42	70.27 70.56	17.04 17.11	12.27 12.33
	EX-83-02-6 EH 23	3.80	4.25	A.D. DRY	0.47	71.27 71.61		11.63 11.69
-	EX-83-02-7 EH 24	3.90	4.41	A.D. DRY	0.53	71.17 71.55	16.34 16.43	11.96 12.02
-	EX-83-02-8 EH 25	3.97	4.45	A.D. DRY	0.50	68.39 68.74		13.45 13.52
-	EX-83-02-9 EH 26	4.42	4.84	A.D. DRY	0.44 	71.59 71.90	16.65 16.72	11.32 11.38
_	EX-83-02-10 EH 27	3.72	4.03	A.D. DRY	0.32	68.79 69.01	16.42 16.47	14.47 14.52
-	EX-83-02-11 EH 28	5.44	6.26	A.D. DRY	0.87	80.60 81.31	8.70 8.78	9.83 9.91
	EX-83-02-12 EH 29	4.79	5.58	A.D. DRY	0.83	75.77 76.40	11.90 12.00	11.50 11.60
	EX-83-02-13 EH 30	5.11	5.68	A.D. DRY	0.60	96.19 96.77		0.18 0.18

ESSO - EX-83-03

-	SMPL NO	MOIST A.D.	T.M.	BASIS			V.M.	
		%	%		%	%	%	7
	EX-83-03-1 EH 31	4.36	5.74	A.D. DRY	1.44	69.42 70.43	16.95 17.19	12.19 12.38
	EX-83-03-2 EH 32	3.50	4.79	A.D. DRY	1.34	73.57 74.57	16.85 17.08	
-	EX-83-03-3 EH 33	2.91	3.99	A.D. DRY	1.11 -	73.45 74.28	15.44 15.61	10.00 10.11
	EX-83-03-4 EH 34	2.77	3.79	A.D. DRY	1.05	74.41 75.20	15.51 15.67	
-	EX-83-03-5 EH 35	2.71	3.75	A.D. DRY	1.07	73.73 74.52	16.61 16.79	
	EX-83-03-6 EH <i>3</i> 6	2.48	3.51	A.D. DRY	1.06	69.77 70.51	17.12 17.30	12.05 12.19
-	EX-83-03-7 EH 37	3.92	4.34	A.D. DRY	0.44 	73.05 73.38	16.28 16.35	10.23 10.27
-	EX-83-03-8 EH 38	4.48	4.91	A.D. DRY	0.45 -	71.75 72.07	16.49 16.57	11.31 11.36
-	EX-83-03-9 EH 39	3.23	4.64	A.D. DRY	1.46	76.75 77.89	13.27 13.46	

	SMPL NO			BASIS	R.M.	ASH	V.M.	F.C.
-	NL	A.D. %			χ.	7	7.	%
	SW-83-01-1 EH 40	0.91	2.59	A.D. DRY			21.42 21.79	18.85 19.18
	SW-83-01-2 EH 41	2.36	3.81	A.D. DRY			22.95 23.30	18.87 19.15
	SW-83-01-3 EH 42	4.59	5.24				23.70 23.86	
-	SW-83-01-4 EH 43	3.34	3.94				20.46 20.59	13.73 13.81
-	SW-83-01-5 EH 44	4.15	4.62					
-	SW-83-01-6 EH 45	4.14	4.61				20.40 20.51	
	SW-83-01-7 EH 46	3.51	3.97				22.11 22.22	
-	SW-83-01-8 EH 47	3.39	3.90	A.D. DRY			17.86 17.96	
-	SW-83-01-9 EH 48	3.33	3.76	A.D. DRY			19.96 20.04	
-	SW-83-01-10 EH 49	4.33	4.80	A.D. DRY			20.20 20.30	
	SW-83-01-11 EH 50	4.43	4.99				20.04 20.16	

-	SMPL NO		Т.М.	BASIS	R.M. %	ASH %	∨.m. %	F.C. %
-	SW-83-02-1 EH 51	4.52	4.90	A.D. DRY	0.40	59.61 59.85		18.23 18.30
	SW-83-02-2 EH 52	2.31	2.68	A.D. DRY		60.83 61.06		17.29 17.36
	SW-83-02-3 EH 53	3.79	4.17	A.D. DRY			20.79 20.87	
-	SW-83-02-4 EH 54	4.29	4.64	A.D. DRY		64.33 64.57		15.39 15.45
-	SW-83-02-5 EH 55	3.97	4.33	A.D. DRY		62.85 63.09	21.72 21.80	15.05 15.11
-	SW-83-02-6 EH 56	4.63	5.43	A.D. DRY		59.82 60.33		18.21 18.36
-	SW-83-02-7 EH 57	4.86	5.29	A.D. DRY		61.19 61.47	20.97 21.07	17.39 17.46
	SW-83-02-8 EH 58	4.59	4.68	A.D. DRY			18.46 18.60	
-	SW-83-02-9 EH 59	5.12	5.62	A.D. DRY				15.34 15.43
	SW-83-02-10 EH 60	5.41	6.01			64.60 65.01	19.45 19.58	15.32 15.41

	SMPL NO		JRE T.M.	BASIS	R.M.	ASH	V.M.	F.C.
-		× ×	%		X	Z	7	%
-	SW-83-03-1 EH 61	4.28	6.08	A.D. DRY	1.88	61.07 62.24	19.68 20.05	17.37 17.71
-	SW-83-03-2 EH 62	3.92	5.69	A.D. DRY	1.84 -	60.14 61.27	20.22 20.60	17.80 18.13
	SW-83-03-3 EH 63	3.97	4.60	A.D. DRY	0.66			16.89 17.00
-	SW-83-03-4 EH 64	4.36	4.99	A.D. DRY	0.66	61.03 61.44	21.26 21.40	17.05 17.16
-	SW-83-03-5 EH 65	4.32	4.83	A.D. DRY	0.53	64.77 65.12	19.85 19.96	14.85 14.92
-	SW-83-03-6 EH 66	3.61	4.09	A.D. DRY	0.50	71.77 72.13	16.97 17.05	10.76 10.82
	SW-83-03-7 EH 67	3.40	4.11	A.D. DRY				11.27 11.35
-	SW-83-03-8 EH 68	3.87	4.71	A.D. DRY	0.87	62.33 62.88	20.44 20.62	16.36 16.50
-	SW-83-03-9 EH 69	4.62	5.76	A.D. DRY	1.19 -	58.37 59.07	22.14 22.41	18.30 18.52

DRILL HOLES - Total Moisture, Proximate

-

	SMPL	MOIST		BASIS	R.M.	ASH	V.M.	F.C.
	NO	A.D. %	T.M. %		%	7.	%	7.
	SW-83-04-1 EH 70	3.78	4.32	A.D. DRY	0.56			21.44 21.56
-	SW-83-04-2 EH 71	3.64	4.15	A.D. DRY	0.53 -	58.44 58.75	21.81 21.93	19.22 19.32
	SW-83-04-3 EH 72	4.05	4.61	A.D. DRY	0.58		22.09 22.21	17.37 17.48
	SW-83-04-4 EH 73	3.91	4.45	A.D. DRY	0.56		21.38 21.50	15.00 15.08
	SW-83-04-5 EH 74	4.16	4.80	A.D. DRY	0.67	64.78 65.21	19.28 19.41	15.14 15.38
-	SW-83-04-6 EH 75	3.77	4.52	A.D. DRY	0.78 -	59.91 60.38	21.13 21.30	18.18 18.32



COAL, COKE AND WATER TESTING a specialized service of GENERAL TESTING LABORATORIES

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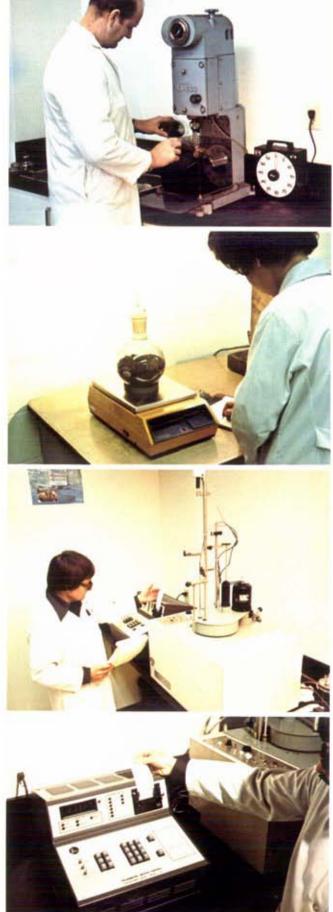
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 - Froth flotation
 - Chlorine
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 - Water soluble alkalis
- Float-sink analysis (producing washability curves)
- Ash analysis (trace elements by spectrographic or neutron activation procedures)

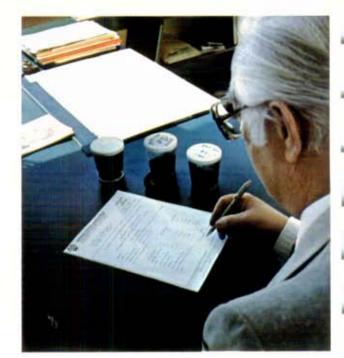
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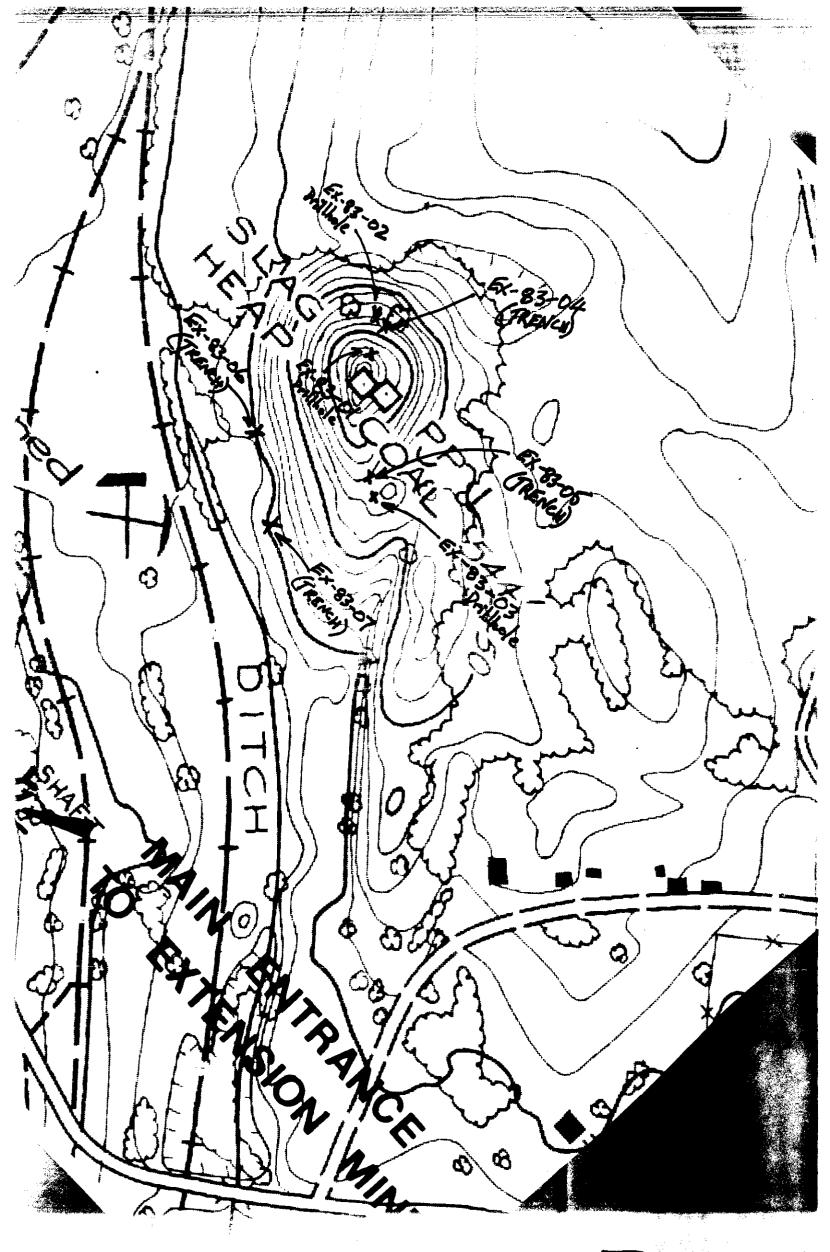


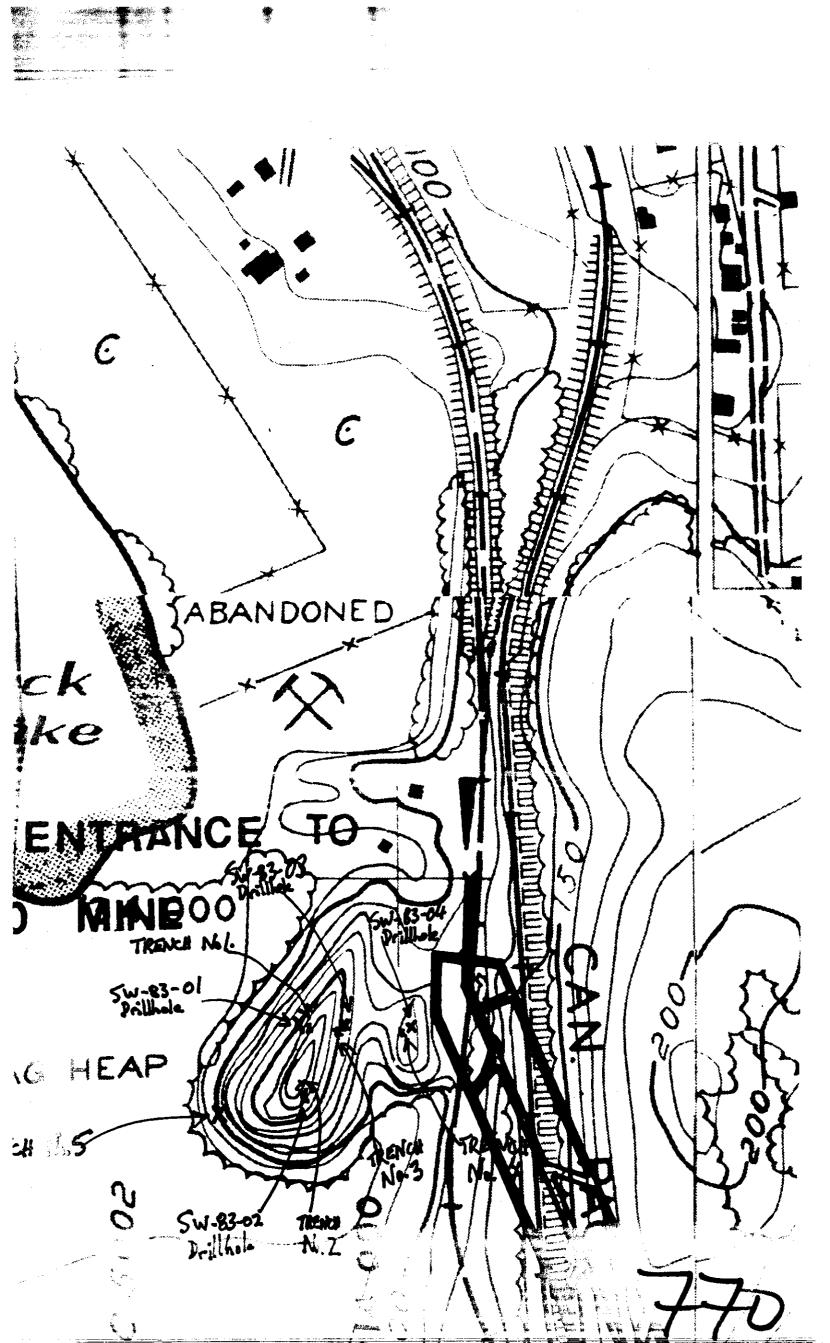
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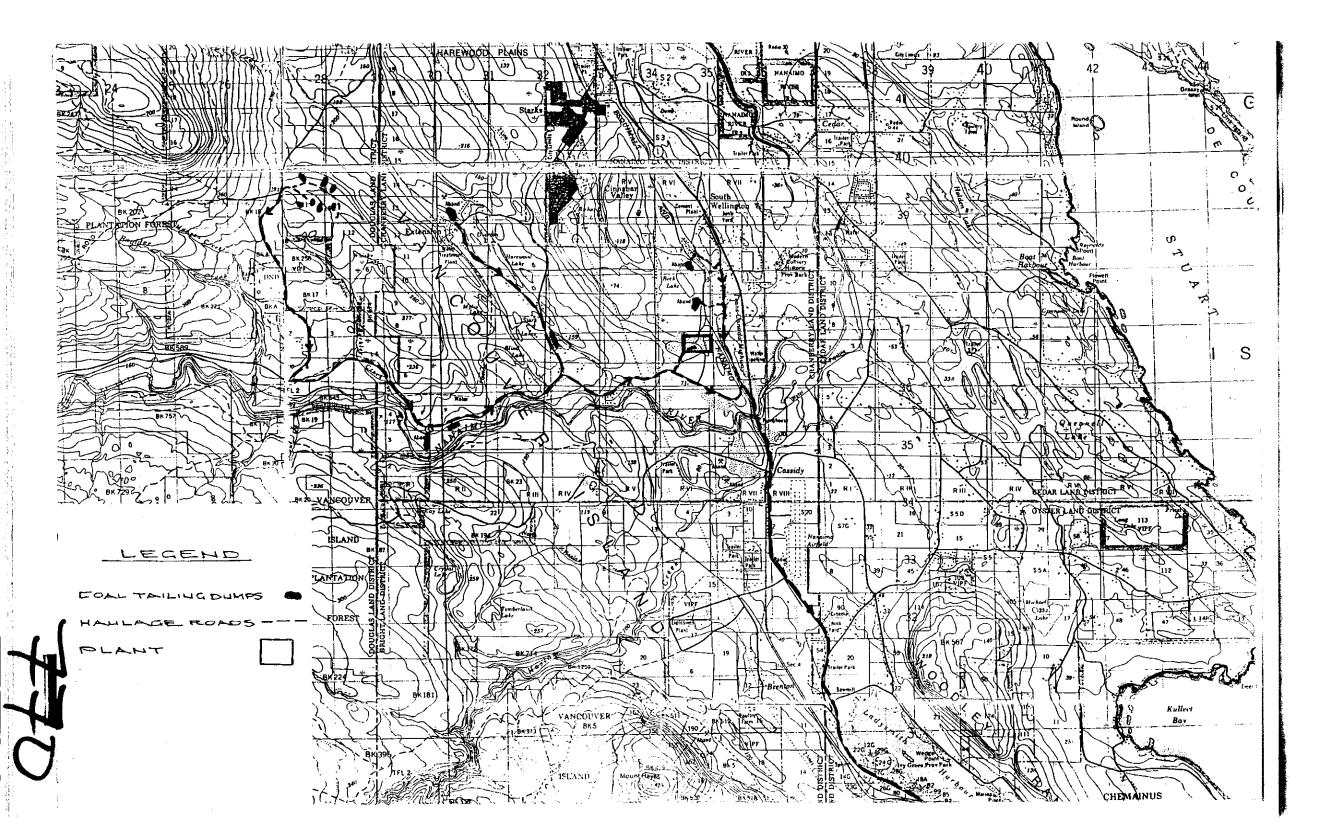
Coal, coke and water testing facilities located at:

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NANAIMO STOCKPILE - OCTOBER 1983

TRENCH SAMPLES

LABORATORY REPORTS

ESSO MINERALS CANADA A DIVISION OF ESSO RESOURCES CANADA LTD. 237-4TH AVENUE S.W. - CALGARY - ALBERTA T2P OHG EXPLORATION MANAGER : MR. HUGH JONES

ANALYTICAL WORK ACCORDING TO ASTM PERFORMED BY : GENERAL TESTING LABORATORIES A DIVISION OF SGS SUPERVISION SERVICES INC. 1707 FRANKLIN ST - VANCOUVER B.C. - CANADA - V5L 1P6 TELEX : 04-507514 - PHONE : (604) 254-2148 CHIEF CHEMIST : L.M. LAKOSIL

77

TO L. Lakosil Stephen . Gard R O M GENERAL TESTING LABS ESSO RESAURCES 4D per VANCOUVER, B.C. SUBJECT TRENCH SAMPLE INVENTORY SOUTH WELLINGTON DWW 1983 DATE Dear Liba: Please Find the following trench samples : 5w-83-01 (Trench) 4 bays 5w-03-02 (French) 4 kgs SW-83-03 (Trunch) 4 bays 4 bays Sw-83-04 (Trench) 4 bays 5W-83-05 (Tranch EX-83-06 (Trench) 30AGS EX-83-07 (Truch)_364675 2 Pro Ki 15 smples SIGNED DIFORM 4S065E MOORE BUSINESS FORMS 3

TO L. Lakosil Stophen L. Gardner GENERAL TESTING LABS " par/ ESSO KESOURCES VANCOUVER, B.C. NANAIMO B.C. SUBJECT RE: TRENCH SAMPLE INVENTORY 19 83 27 DATE SEIT Dear Liba: Please Find enclosed a number of Samples marked (TRENCH) are not These the same as drill hole samples and you will be supplied with a different set of instruction These TRENCH) - 4 bays - 83 - 6 Ex. 05 (TRENCH) -4 bags EX - 83-No. 4 DUMP (TRENCH #1)-4 bys -4 bags No. 4 DUMP (TREACH #2) L te # #4 11 le 10 (r # 51 10 lt #6) le R DIFORM 45055E MOORE BUSINESS FORMS 3

AREDI-LETTER

ESSO - TRENCH

RAW COAL (CALCULATED)

SAMPLE NO - ESSD : EX-83-05(T) - GTL : ET 1

YIELD ASH V.M. F.C. T.S. C.V. 2 2 2 2 2 CAL/(FRACTION CAL/G % 7. + 4 INCH 6.49 (KEPT ASIDE) 6.39 (CRUSHED TO -1 INCH) + 1 INCH 77.01 65.23 18.38 16.39 0.26 2216 +28 MESH +100 MESH 14.06 68.27 -100 MESH 8.93 73.86 18.78 12.95 1645 0.29 8.93 73.86 16.58 9.56 0.23 1381 - 66.43 18.28 15.29 0.26 2061 RAW COAL

ESSO	 TRENCH

RAW COAL (CALCULATED)

RAW COAL

SAMPLE NO - ESSO : SW 83-03(T) - GTL : ET 2

YIELD V.M. F.C. T.S. C.V. FRACTION ASH % Z 7. % 7 CAL/G + 4 INCH 8.72 (KEPT ASIDE) + 1 INCH 12.40 (CRUSHED TO -1 INCH) 71.58 21.89 21.00 2851 +28 MESH 57.11 0.46 22.55 18.07 57.61 19.84 0.47 2626 +100 MESH 10.35 60.75 20.35 18.90 0.56 2599 -100 MESH

57.58 21.85 20.57

0.47

RAW COAL (CALCULATED)

SAMPLE NO - ESSO : #4 DUMP T6 - GTL : ET 3

-

ASH V.M. F.C. T.S. C.V. FRACTION YIELD 7 7 7 7. 7 CAL/G + 4 INCH 10.97 (KEPT ASIDE) + 1 INCH 16.50 (CRUSHED TO -1 INCH) +28 MESH 84.87 53.84 23.18 22.98 0.28 3226 +100 MESH 9.40 48.51 26.23 25.26 0.30 3456 -100 MESH 5.73 53.74 23.71 22.55 0.30 3212 RAW COAL

53.33 23.49 23.18 0.28

RAW COAL (CALCULATED)

RAW COAL

SAMPLE NO - ESSO : EX-83-06(T) - GTL : ET 4

ASH V.M. F.C. T.S. C.V. FRACTION YIELD 7 7 7 Z % CAL/G 2.34 (KEPT ASIDE) + 4 INCH + 1 INCH 14.00 (CRUSHED TO -1 INCH) 69.24 69.76 16.08 1598 +28 MESH 14.16 0.16 +100 MESH 20.90 66.83 18.16 15.01 0.19 1847 -100 MESH 9.86 69.72 16.99 13.29 0.23 1480

69.14 16.60 14.26 0.17

RAW COAL (CALCULATED)

RAW COAL

SAMPLE ND - ESSO : SW-83-02(T) - GTL : ET 5

YIELD ASH V.M. F.C. T.S. C.V. Z Z Z Z Z Z CAL/(FRACTION 7 7 7 7. 7 CAL/G 8.34 (KEPT ASIDE) + 4 INCH 9.09 (CRUSHED TO -1 INCH) + 1 INCH 68.67 57.48 21.74 20.78 0.52 2904 +28 MESH +100 MESH 19.26 56.89 23.13 19.99 -100 MESH 12.07 62.79 21.09 16.12 0.54 2724 0.63 2596

58.01 21.93 20.06 0.54

RAW COAL (CALCULATED)

RAW COAL

SAMPLE NO - ESSO : #4 DUMP T1 - GTL : ET 6

-

ASH V.M. F.C. T.S. C.V. % % % % CAL/(FRACTION YIELD χ CAL/G 1.57 (KEPT ASIDE) + 4 INCH + 1 INCH 12.30 (CRUSHED TO -1 INCH) +28 MESH 75.21 60.91 20.76 18.33 0.23 2522 59.08 21.40 17.90 0.22 19.51 2530 +100 MESH -100 MESH 6.89 56.92 24.97 18.11 0.26 2831

60.30 21.17 18.53 0.23

SAMPLE NO - ESSO : EX-83-05(T) GTL : ET 1

- FRACTION : +28 MESH
- FRACTIONAL

V.M. F.C. T.S. C.V. S.G. BASIS YIELD R.M. ASH % 7. % 7 7 72 CAL/G 7408 1.40 A.D. 7.88 36,94 53.98 0.57 ----1.20 17.04 DRY 7.98 37.39 54.63 0.57 7498 1.50 A.D. 1.08 22.39 33.17 43.36 0.56 6044 ----3.54 DRY 22.63 33.54 43.83 0.56 6110 •••• 1.60 A.D. -1.14 32.84 30.11 35.91 0.53 5130 2.53 DRY 33.22 30,46 36.32 0.54 5189 -----1.70 A.D. _ 1.06 41.92 26.68 30.34 0.43 4322 2.92 42.37 26.97 DRY 30.66 0.44 4368 -1.80 A.D. -1.17 50.50 23.72 24.61 0.35 3556 DRY 3.44 51.10 24.00 24.90 0.35 3598 -**** ---A.D. 1.60 82.65 11.78 3.97 0.14 474 DRY 70.53 -83.99 11.97 4.04 0.14 481

S.G.	YIELD %	ASH Z		F.C.	T.S. %	C.V. CAL/G
1.60 1.70 1.80	17.04 20.58 23.11 26.03 29.47 100.00	7.98 10.50 12.99 16.28 20.35 65.23	36.72 36.04 35.02 33.73	50.97	0.57 0.57 0.57 0.55 0.53 0.26	7498 7260 7033 6734 6368 2216

ESSO - TRENCH SAMPLE NO - ESSO : SW 83-03(T) GTL : ET 2 FRACTION : +28 MESH FRACTIONAL YIELD ASH V.M. F.C. T.S. C.V. S.G. BASIS R.M. CAL/G 7 Z % Z 7 7 52.00 0.62 7217 1.40 A.D. 1.41 8.63 37.96 -----21.94 8.75 38.51 52.74 0.63 7320 DRY ----44.59 0.62 20.35 33.99 6081 1.50 A.D. 1.07 -----4.59 45.07 0.62 6147 20.57 34.36 DRY _ 31.36 37.80 0.62 1.60 A.D. 0.94 29.90 5230 0.62 DRY 4.27 30.18 31.65 38.17 5279 ----39.04 28.33 31.72 0.63 4411 1.70 A.D. ----0.91 3.55 28.59 32.01 0.63 4452 39.40 DRY ----47.78 25.34 25.93 0.62 3694 1.80 A.D. ----0.95 3.54 48.23 25.59 26.18 0.63 3730 DRY ----**** A.D. 1.44 79.11 13.63 5.82 0.35 710 -62.11 -80.27 13.83 5.90 0.35 720 DRY

P	S.G.	YIELD %	ASH %	∨.M. %	F.C. %		C.V. CAL/G
•	1.40 1.50 1.60 1.70 1.80	21.94 26.53 30.80 34.35 37.89	8.75 10.80 13.48 16.16 19.16	38.51 37.79 36.94 36.08 35.10	51.41 49.58 47.76	0.63 0.63 0.63 0.63 0.63	7320 7117 6863 6613 6344
	****	100.00	57.11		21.00	0.46	2851

ES	30 -	- TRE	ENCH	-1					
SAMPLE NO - ESSO : #4 DUMP T6 GTL : ET 3									
FRACT	ION	: +28 ME	SH						
FRACT	IONAL								
S.G.	BASIS	YIELD Z	R.M. %	ASH %		F.C. %			
1.40									
1.50		4.37							
1.60		_ 5.73							
1.70		7.50							
1.80	A.D. DRY	- 8.05			23.89 24.38				
****		- 55.74							

 S.G.	YIELD Z	ASH %		F.C. %		C.V. CAL/G
1.40 1.50 1.60 1.70 1.80 ****	44.26	8.35 11.07 15.36 20.96 26.35 53.84	37.21 35.94 34.30 32.49	48.70 44.74	0.51 0.49 0.47 0.44	7399 7148 6761 6270 5790 3226

	ES	50 -	- TRE	ENCH	4				
	SAMPL	_E NO -	ESSO : GTL :		06(T)				
_	FRAC	FION :	: +28 ME	SH					
	FRAC	FIONAL							
	S.G.	BASIS	YIELD %			V.M. Z			
	1.40		5.82						
	1.50		- 5.22						
-	1.60		_ 3.51						
	1.70		_ 2.74						
_	1.80		_ 2.46						
	****	A.D.		1.99	80.20	12.48	5.33	0.09	

80.25 - 81.82 12.73

C.V. CAL/G

6868 7044

6007 6288

5271 5503

4421 4529

3505 3606

554

565

5.45 0.09

CUMULATIVE - BASIS : DRY

DRY

-	S.G.	YIELD %	ASH %	V.M. Z	F.C. %	T.S. %	C.V. CAL/G
-	1.40 1.50 1.60 1.70 1.80 ****	5.82 11.04 14.55 17.29 19.75 100.00	7.17 9.93 13.25 16.92 20.74 69.76	33.15 31.79 30.74 29.68		0.48 0.47 0.42	7044 6687 6401 6104 5793 1598

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ESSO - TRENCH
SAMPLE NO - ESSO : SW-83-02(T)
          GTL : ET 5
FRACTION : +28 MESH
FRACTIONAL
                       ASH V.M. F.C. T.S. C.V.
S.G. BASIS
         YIELD
                 R.M.
            %
                 7
                       7
                             7
                 3.76
                      8.92
1.40 A.D.
            -
           25.82
                      9.27
     DRY
                 ---
```

50.77 0.56 7126 36.55 37.97 52.76 0.59 7405 1.23 21.40 33.96 43.41 0.74 6049 1.50 A.D. ----4.66 34.38 43.96 0.75 DRY 21.66 6125 37.23 0.74 29.90 31.53 5279 1.60 A.D. 1.34 ----37.74 0.75 30.30 31.96 5351 DRY 4.05 4487 29.07 31.02 0.86 A.D. ----1.17 38.74 1.70 31.38 0.87 4541 3.O9 39.20 29.42 DRY **** 26.49 25.48 0.95 3791 A.D. 1.23 46.80 1.80 ----2.92 47.38 26.82 25.80 0.97 3838 DRY -----3.07 0.41 393 **** A.D. 1.55 83.21 12.17 -----84.52 12.36 3.12 0.42 399 DRY 59.46 ****

CAL/G

7

7

•	S.G.	YIELD Ž	ASH Z	V.M. X	F.C. %	T.S. %	C.V. CAL/G
-	1.70	25.82 30.48 34.53 37.62 40.54 100.00	11.16 13.41	37.97 37.42 36.78 36.18 35.50 21.74	51.42 49.81 48.29 46.68	0.59 0.61 0.63 0.65 0.67 0.52	7405 7209 6991 6790 6577 2904

- SAMPLE NO ESSO : #4 DUMP T1 GTL : ET 6
- FRACTION : +28 MESH
- FRACTIONAL

S.G. BASIS YIELD R.M. ASH V.M. F.C. T.S. C.V. 7 7 7 Z CAL/G Ζ Z 8.21 38.13 52.41 0.51 7221 1.40 A.D. •••• 1.25 DRY 14.63 8.31 38.62 53.07 0.52 7313 ----A.D. 19.68 32.29 46.72 0.48 6083 1.50 ---1.31 2.88 DRY 19.94 32.72 47.34 0.48 6164 -1.60 A.D. 1.50 28.70 30.73 39.07 0.43 5269 ---DRY 4.28 ---29.14 31.19 39.67 0.44 5350 29.29 1.70 A.D. 1.50 38.53 30.68 0.39 4461 ---5.10 39.12 29.73 31.15 0.39 4529 DRY -1.49 47.50 24.82 1.80 A.D. 26.19 0.32 3704 ----5.05 48.22 25.20 26.58 0.32 DRY 3760 ----**** A.D. 76.86 14.45 6.58 898 2.11 0.13 -----DRY 68.06 ----78.52 14.76 6.72 0.13 917

1.50 17.51 10.22 37.65 52.13 0.51 71 1.60 21.79 13.94 36.38 49.68 0.50 67 1.70 26.89 18.71 35.12 46.17 0.48 63 1.80 31.94 23.38 33.55 43.07 0.45 59	II .	S.G.	YIELD X	ASH %		F.C. %		C.V. CAL/G
**** 100.00 60.91 20.76 18.33 0.23 25	-	1.50 1.60 1.70	17.51 21.79 26.89	10.22 13.94 18.71	37.65 36.38 35.12	52.13 49.68 46.17	0.51 0.50 0.48	7313 7124 6775 6349 5940
		****	100.00	60.91	20.76	18.33	0.23	2522

- ESSO TRENCH
- SAMPLE ND ESSO : EX-83-05(T) - GTL : ET 1
 - FRACTION : +100 MESH
 - FRACTIONAL

	S.G.	BASIS	YIELD %	R.M. %	ASH %	V.M. Z	F.C. %	s %	C.V. CAL/G
		001/					F 4 F 7		
	1.40	DRY	5.82	-	8.05	37.39	54.56	0.75	7313
	1.50	DRY	5.43		16.91	35.27	47.82	0.74	6129
	1.60	DRY	2.92		31.95	29.03	39.02	0.59	5114
	1.70	DRY	5.74	-	44.13	28.36	27.51	0.42	3239
	1.80	DRY	1.01		46.01	26.80	27.19	0.43	3096
	****	A.D.	-	3.83	76.55	14.52	5.10	0.19	631
L		DRY	79.08	-	79.60	15.10	5.30	0.20	656

-	S.G.	BASIS	YIELD %	R.M. %	ASH %	V.M. %	F.C. %	s %	C.V. CAL/G
-	1.40	A.D. DRY	_ 5.82	3.01 _	7.81 8.05			0.73 0.75	7093 7313
عتبته	1.50	A.D. DRY	11.25		11.85 12.33	34.96 36.37	49.31 51.30	0.72 0.75	6480 6742
	1.60	A.D. DRY	- 14.17		15.67 16.37		46.70 48.77		6133 6406
-	1.70	A.D. DRY	 19.91		23.79 24.37		41.60 42.65		5360 5493
	1.80	A.D. DRY	20.92	3.13	24.62 25.42	31.66 32.69	40.59 41.89	0.60 0.62	5209 5377
	****	DRY	100.00		68.27	18.78	12,95	0.29	1644

- ESSO TRENCH
- SAMPLE NO ESSO : SW 83-03(T) - GTL : ET 2
 - FRACTION : +100 MESH
 - FRACTIONAL

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S.G.	BASIS	YIELD	R.M.	ASH	V.M.	F.C.	S	C.V.
		Χ.	%	%	Z	7	%	CAL/G
1.40	DRY	6.82		9.22	37.12	53.66	0.60	7209
1.50	DRY	8.03	-	17.98	36.31	45.71	0.57	6420
1.60	DRY	6.29	-	26.28	35.29	38.43	0.60	5380
1.70	DRY	6.83		32.39	30.40	37.21	0.58	4553
1.80	DRY	6.72	-	42.12	27.34	30.54	0.52	3239
****	A.D.	-	3.58	72.10	16.20	8.12	0.40	1110
	DRY	65.31		74.78	16.80	8.42	0.41	1152

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CUMULATIVE

	S.G.	BASIS	YIELD %	R.M. %	ASH %	V.M. Z	F.C. %	S %	C.V. CAL/G
•	1.40	A.D. DRY	- 6.82	2.64	8.98 9.22	36.14 37.12	52.24 53.66	0.58 0.60	7018 720 9
•	1.50	A.D. DRY	_ 14.85		13.55 13.96	35.61 36.68		0.57 0.58	6583 6782
	1.60	A.D. DRY	_ 21.14		17.01 17.62		44.50 46.11		6143 6365
-	1.70	A.D. DRY	_ 27.97	3.87 -	20.41 21.23	33.49 34.84	42.23 43.93	0.56 0.59	5693 5923
	1.80	A.D. DRY	- 34.69	4.44 -	24.16 25.28	31.90 33.38	39.50 41.34	0.55 0.57	5163 5403
	****	DRY	100.00	-	57.61	22.55	19.84	0.47	2626

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- SAMPLE NO ESSO : #4 DUMP T6 - GTL : ET 3
 - FRACTION : +100 MESH

- - -

FRACTIONAL

S.G.	BASIS	YIELD X	R.M. %	ASH %	V.M. %	F.C. %	s %	C.V. CAL/G
1.40	DRY	19.54		8.15	37.19	54.66	0.55	7285
1.50	DRY	7.36		19.85	34.26	45.89	0.49	6222
1.60	DRY	5.13		32.60	34.07	33.33	0.50	4883
1.70	DRY	8.32	-	35.17	32.74	32.09	0.48	4478
1.80	DRY	7.58	-	45.65	32.31	22.04	0.33	3312
****	A.D.		3.14	69.57	17.71	9.58	0.13	1302
	DRY	52.07		71.82	18.29	9.89	0.13	1344

CUMULATIVE

•	S.G.	BASIS	YIELD %	R.M. %	ASH %	V.M. %	F.C. %	S %	C.V. CAL/G
	1.40	A.D. DRY	_ 19.54		7.92 8.15	36.15 37.19	53.13 54.66		7081 7285
-	1.50	A.D. DRY	26.90	2.88		35.34 36.39	50.76 52.26		6793 6994
	1.60	A.D. DRY	- 32.03		14.32 14.75	34.96 36.02	47.79 49.23		6461 6656
_	1.70	A.D. DRY	_ 40.35	3.46	18.31 18.96	34.12 35.34		0.50 0.52	5992 6207
	1.80	A.D. DRY	_ 47.93	3.94	22.27 23.18		40.30 41.96		5523 5749
•	***	DRY	100.00	-	48.51	26.23	25.26	0.30	3456

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- ESSO TRENCH
- SAMPLE NO ESSO : EX-83-06(T) - GTL : ET 4
 - FRACTION : +100 MESH
 - FRACTIONAL

S.G.	BASIS	YIELD	R.M.	ASH	V.M.	F.C.	S	C.V.
		%	%	%	7	%	7	CAL/G
1.40	DRY	2.51	-	6.81	36.88	56.31	0.57	6981
1.50	DRY	5.79		12.46	33.57	53.97	0.52	5968
1.60	DRY	5.08	-	18.26	33.13	48.61	0.48	5411
1.70	DRY	4.04		29.43	32.20	38.37	0.41	4346
1.80	DRY	2.90		45.96	31.49	22.55	0.33	3336
****	A.D.	-	3.46	75.71	13.80	7.03	0.12	931
	DRY	79.68		78.42	14.30	7.28	0.12	965

CUMULATIVE

	S.G.	BASIS	YIELD %	R.M. %	ASH %	V.M. %	F.C. %	S %	C.V. CAL/G
	1.40	A.D. DRY	2.51	3.51 -	6.57 6.81	35.58 36.88	54.34 56.31	0.55 0.57	6736 6981
	1.50	A.D. DRY	- 8.30	3.50	10.38 10.75	33.36 34.57		0.51 0.53	6055 6275
_	1.60	A.D. DRY	- 13.38	3.73	13.10 13.60	32.75 34.02		0.49 0.51	5725 5947
	1.70	A.D. DRY		3.75	16.63 17.27	32.34 33.60	47.28 49.13	0.47 0.49	5367 5576
	1.80	A.D. DRY	20.32	3.69	20.58 21.37	32.07 33.30	43.66 45.33	0.45 0.47	5062 5256
	****	DRY	100.00	-	66.83	18.16	15.01	0.19	1837

- ESSO TRENCH
- SAMPLE NO ESSO : SW-83-02(T) - GTL : ET 5
 - FRACTION : +100 MESH
 - FRACTIONAL

S.G.	BASIS	YIELD %	R.M. %	ASH %	V.M. Z	F.C. %	s %	C.V. CAL/G
1.40	DRY	11.45	-	10.71	37.62	51.67	0.68	7205
1.50	DRY	7.97	-	21.58	32.84	45.58	0.66	6210
1.60	DRY	5.85		28.67	32.84	38,49	0.67	5286
1.70	DRY	6.43	-	38.68	33.22	28.10	0.67	4419
1.80	DRY	7.11	-	40.8 9	32.81	26.30	0.73	3787
****	A.D.	-	3.83	73.67	15.42	7.08	0.44	851
	DRY	61.19	-	76.60	16.03	7.37	0.46	884

CUMULATIVE

	S.G.	BASIS	YIELD %	R.M. %	ASH %	∨.M. %	F.C. %	S %	C.V. CAL/G
	1.40	A.D. DRY		2.14	10.48 10.71		50.57 51.67	0.67 0.68	7051 7205
-	1.50	A.D. DRY	_ 19.42		14.80 15.17	34.79 35.66			6632 6797
	1.60	A.D. DRY	- 25.27	2.45	17.85 18.29	34.15 35.01			6289 6447
	1.70	A.D. DRY		2.77	21.81 22.43	33.68 34.64			5868 6035
	1.80	A.D. DRY		3.21 _	24.98 25.81	33.21 34.31	38.60 39.88	0.66 0.68	5443 5624
	****	DRY	100.00		56.89	23.13	19.99	0.54	2724

- SAMPLE NO ESSO : #4 DUMP T1 - GTL : ET 6
 - FRACTION : +100 MESH
 - FRACTIONAL

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S.G.	BASIS	YIELD %	R.M. %	ASH %	V.M. %	F.C. %	s %	C.V. CAL/G
1.40	DRY	10.67		6.83	38.56	54.61	0.63	7348
1.50	DRY	4.54		19.20	33.71	47.09	0.48	5916
1.60	DRY	6.12		24.00	33.47	42.53	0.46	5479
1.70	DRY	6.59		33.65	29.13	37.22	0.37	4464
1.80	DRY	5.93	****	69.12	21.58	9.30	0.18	1734
****	A.D.	-	4.54	71.72	15.17	8.57	0.10	1076
	DRY	66.15		75.13	15.89	8.98	O.11	1127

CUMULATIVE

Î	S.G.	BASIS	YIELD Z	R.M. %	ASH Z	V.M. Z	F.C. %	S %	C.V. CAL/G
	1.40	A.D. DRY	 10.67		6.63 6.83	37.41 38.56	52.99 54.61		7130 7348
	1.50	A.D. DRY	15.21			36.17 37.11			
	1.60	A.D. DRY	21.33			34.97 36.07			6310 6507
-	1.70	A.D. DRY	27.92	4.38	18.10 18.93		44.60 46.64		5761 6025
	1.80	A.D. DRY	- 33.85	4.37	26.51 27.73	30.77 32.18	38.35 40.09	0.43 0.45	5043 5273
	****	DRY	100.00	-	59.08	21.40	19.51	0.22	2530

ESSO - TRENCH

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FRACTION : -100 MESH

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-	SMPL NO	BASIS	YIELD X	R.M. %	ASH Z	V.M. Z	F.C. Z	T.S. %	
	ET 1 EX-83-05(T)		8.93	4.51	70.53 73.86		9.13 9.56	0.22 0.23	
	ET 2 SW 83-03(T)				58.38 60.75		18.16 18.90	0.54 0.56	
	ЕТ З #4 DUMP T6		5.73	3.57		-		0.29 0.30	3098 3212
-	ET 4 EX-83-06(T)						12.75 13.29	0.22 0.23	141 9 1480
	ET 5 SW-83-02(T)			2.56	61.19 62.79	20.55 21.09	15.70 16.12		2530 2596
	ET 6 #4 DUMP T1	A.D. DRY		2.12	55.71 56.92	24.44 24.97	17.73 18.11	0.25 0.26	2771 2831

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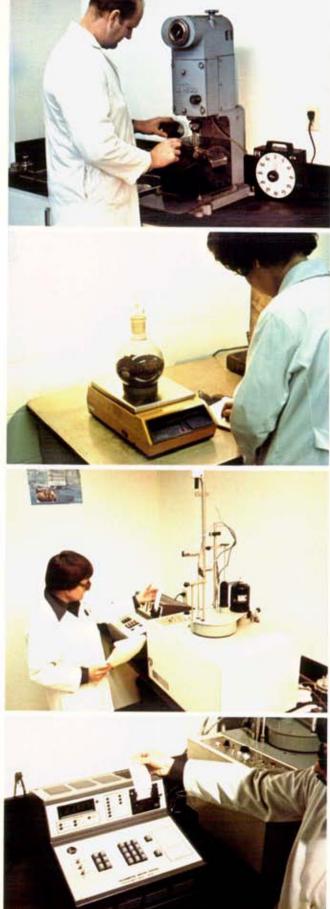
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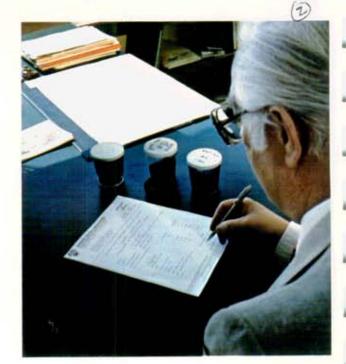
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