GEOLOGIC SUMMARY AND THERMAL COAL POTENTIAL OF THE BOWROÑ RIVER COAL PROPERTY OF NORCO RESOURCES LTD. PRINCE GEORGE, B. C.



by

Ruben Verzosa, P. Eng.

December 31, 1981

1



# TABLE OF CONTENTS

1

1.0	INTR	ODUCTION	1
2.0	SUMM	ARY AND CONCLUSIONS	2
3.0	PROP	ERTY DESCRIPTION	3
	3.1 3.2 3.2	Location and Access Size Physiography	3 3 3
4.0	HIST	ORY	6
5.0	PREV	IOUS EXPLORATION	7
	5.1 5.2	Borehole Drilling Adits and Bulk Sampling	7 8
6.0	GEOL	OGY	8
	6.1 6.2	General Setting Stratigraphy	8 8
		<pre>6.2.1 Antler Formation</pre>	9 9
	6.3 6.4	Structure Coal Seams	10 12
		<pre>6.4.1 Lower Seam 6.4.2 Upper Seam</pre>	12 13
7.0	COAL	QUALITY	13
	7.1 7.2 7.3	Proximate Analysis and Washability Tests Petrography Amber Resin	13 14 14
8.0	COAL	RESERVES	15
	8.1	Measured Reserves	15
		8.1.1 Computation Method and Parameters	15
	8.2	Potential Reserves	19
9.0	RECO	MMENDATIONS	20
	9.1 9.2 9.3	Borehole Drilling Bulk Sampling Coal Analysis	20 20 20

Page

ł

i

## LIST OF ILLUSTRATIONS

Page

1

ł

Figure	1:	Property Location Map	4
Figure	2:	Coal Licence Map	5
Figure	3:	Borehole and Adit Location Map	(Pocket)
Figure	4: 1	Interpretive Geology of the Bowron River Coal Property	(Pocket)
Figure	5:	Typical Stratigraphic Section of Bowron River (Modified from DDH 77-19)	11
Figure	6:	Structure Contour Map at the Base of the Lower Seam	(Pocket)
Figure	7: 🗸	Location Map of Proposed Boreholes	(Pocket)
Fig. 8-1	1 to 8-21	Cross Sections	(Pocket) 🗸

## LIST OF TABLES

Table 1:	Summary	of	Borehole	Drilling	• • • • • • • • • •	7
Table 2:	Summary	of	Coal Res	erve Comp	utation	17

# LIST OF APPENDICES

Drill Core Analytical Results ..... Appendix I Bulk Sampling Analytical Results .... Appendix II

## 1.0 INTRODUCTION

The Bowron River coal property of Norco Resources Ltd. is an Upper Cretaceous Tertiary coal deposit located near Prince George, B. C. Coal has been known in the area since before the turn of the century, although it was not until the early 1960's that serious exploration was started. To date some 26,075 metres in 95 boreholes, both diamond and rotary, have been drilled. In addition, two adits were driven, originally for the purpose of extracting coal for the local market and later serving as access for bulk sampling. The drilling programmes from 1967 onwards are of particular importance since the results are adequately documented. Geophysical logging of boreholes was incorporated in the 1980 and 1981 programmes and provided valuable data.

This report summarizes the results of exploration work carried out on the property. It briefly describes the general geology of the deposit, particularly as it relates to its coal potential. It also includes a computation of coal reserves of the "measured" category, as well as an estimate of additional coal reserves outside the drilled area.

Since the property is extensively covered by alluvium and glacial till, the interpretation of the local geology is based almost entirely on the results of borehole drilling. Other interpretations, particularly on regional structure, were interpolated from published government maps and reports.

- 1 -

#### 2.0 SUMMARY AND CONCLUSIONS

The Bowron River coal property of Norco Resources Ltd., near Prince George, B. C., comprises 51 coal licences, of which only 6 licences have been extensively explored. Exploration to date, mainly by borehole drilling, has confirmed the presence of thick coal seams in the southwest sector of what appears to be a northwesterly elongated sedimentary basin. The coal seams occur in the lower half of the Upper Cretaceous and Early Tertiary Bowron River coal measures which, in the drilled area, attain thicknesses exceeding 700 metres. The closely spaced drilling has delineated an area 4.5 km long and 1.5 km wide, from which 49,904,280 tonnes of in-place raw coal from two seams have been calculated.

C

The average analysis of the raw coal on an air-dry basis is as follows:

Moisture	3.63%
Ash	35.70%
Volatile Matter	26.69%
Fixed Carbon	33.98%
Sulphur	1.33%
BTU/1b	8,154

The coal is non-coking.

Limited tests indicate that the coal can be satisfactorily washed to specified ash levels with relatively high product yields. Additional tests are required to confirm this assumption.

It is anticipated that additional drilling outside the delineated area will appreciably increase the presently known reserves.

- 2 -

#### 3.0 PROPERTY DESCRIPTION

1

#### 3.1 Location and Access

The Bowron River coal property lies approximately 60 km east of Prince George, B. C. (Figure 1). It is accessible from Prince George by some 50 km of paved road on Highway 16 and thence by 10 km of all-weather gravel road. The closest access to rail would be Hansard, a distance of 35 km to the north. Prince George is a large industrial and commercial hub in north central B. C., with daily scheduled commercial jet transportation. It also serves as a major staging point for both B. C. Rail and the C. N. R.

## 3.2 Size

The Bowron River coal property of Norco Resources Ltd. comprises a total of 51 coal licences (Figure 2). Of this total, only six licences (C.L. 148, 162, 163, 4459, 4462, and 4464) have been explored by borehole drilling. The licences more or less follow and straddle the northwestflowing Bowron River along a distance of nearly 34 km.

## 3.3 Physiography

The most notable physiographic feature of the area is the narrow northwest trending valley that contains the mature flood plain of the Bowron River. Except for a few gravel terraces the valley is relatively flat with elevations averaging about 750 metres above sea level. The dominant surficial materials are river gravels which, over a wide area, average 30 metres to bedrock. The valley rises on each flank to elevations exceeding 1,200 metres above sea level.



( )



.

4

#### 4.0 HISTORY

Coal in the area was discovered by G. M. Dawson of the GSC in 1870. Prior to 1960 several small companies hand-sorted coal from small underground workings and sold it locally in In 1960 Northern Coal Mines Ltd. acquired Prince George. coal licences covering a large area and, between 1964 and 1966, drilled 32 boreholes, ranging in depth from 50 to 150 metres. All the core from the drilling was neglected and destroyed. In 1967, 10 diamond drill holes were completed under the supervision of Dr. S. M. Black. The results of this drilling were well documented and the core is reportedly still intact. It was during this same period that two adits were driven, apparently for the purpose of exploring the coal seam. In 1971 Northern Coal Mines optioned their property to Bethlehem Copper Mines which completed 5 diamond drill holes under the supervision of Dr. Kucera.

6 -

In 1973 Zulu Explorations Ltd. staked mineral claims in the area and drilled 10 boreholes. The results of the drilling are poorly documented. Shortly thereafter, Northern Coal Mines was reorganized and renamed Norco Resources Ltd. Norco sampled one of the adits and shipped 12 tons to the Department of Energy, Mines & Resources, and to Cyclone Engineering, both of Edmonton, Alberta, for testing. In 1977 a major diamond drilling programme comprising 25 diamond drill holes was completed under the direction of Kerr, Dawson & Associates. The results of this programme are very well documented. Further borehole drilling, both diamond and rotary, was carried out in 1980 and 1981 under the direction of I. Borovic, P. Eng. During both years a total of 10,894 metres in 24 boreholes was completed.

#### 5.0 PREVIOUS EXPLORATION

## 5.1 Borehole Drilling

The surface geology of the Bowron River coal property is obscured by a thick mantle of alluvium and glacial till. Limited rock exposures are found only along the banks of the Bowron River and on higher elevations on both sides of the Bowron River Valley. Consequently, past exploration programmes have been limited mainly to borehole drilling. During the 1980 and 1981 exploration programmes, rotary drilling was introduced specifically to penetrate the thick overburden. A summary of borehole drilling carried out on the property since 1964 is shown below in Table 1.

#### TABLE 1

Year	No. of Holes	Total Length
1967	32	5,220.4 m
1971	5	2,517.5 m
1973	9	1,746.9 m
1977	25	5,701.6 m
1980	14	5,328.8 m <sup>°</sup>
1981	10	5,564.7 m
		<u> </u>
	95	26,075.9 m
	=	

#### SUMMARY OF BOREHOLE DRILLING

## 5.2 Adits and Bulk Sampling

Two old adits are present on the property, both of which were driven for the purpose of mining coal. These adits were later utilized for bulk sampling. The first bulk sampling was carried out in 1968 by the DEMR and consisted of 727 kg of coal. The second bulk sampling was carried out by H. S. Haslam & Associates in 1976 and consisted of a 12 tonne sample. The results from the bulk samplings are appended to this report and are discussed in the section on coal quality.

## 6.0 GEOLOGY

#### 6.1 General Setting

The Bowron River coal deposit is situated in a narrow northwesterly elongate basin at the northern end of the Cariboo Mountain range. The basin is mainly comprised of the Upper Cretaceous or Early Tertiary Bowron River coal measures, which unconformably overlie the Mississippian Antler Formation. A few outcrops of the Bowron River coal measures occur over a strike length of 11 km along a narrow band bounded by rocks of the Antler Formation (Figure 4). Published government aeromagnetic maps indicate that the basin could be as much as 19 km long with an average width of 2.5 km. The structural trend of the basin appears consistent with the northwesterly regional strike of the surrounding older formations.

## 6.2 Stratigraphy

The following summary of the stratigraphy of the property is based mainly on borehole information and limited government publications. The rock units comprising the Bowron River coal measures are characterized by rapid changes in lithology indicative of rapidly changing depositional environment. The stratigraphy is therefore complex and correlation would only be possible on a local basis. A typical stratigraphic section of the property is shown in Figure 5.

- 8 -

#### 6.2.1 Antler Formation

The oldest rock on the property is the Mississippian Antler Formation that belongs to the Slide Mountain group. The formation is comprised of pillow basalt, breccia, tuff, minor diorite and gabbro, chert, argillite and lithic sandstone. It is regional in distribution and appears to have been subjected to the same degree of deformation as the surrounding sedimentary rocks. The majority of the boreholes drilled on the property bottomed in volcanics and tuffaceous sandstone of the Antler Formation.

## 6.2.2 Bowron River Coal Measures

Resting unconformably on the Antler Formation are the Upper Cretaceous or Early Tertiary Bowron River coal measures, chiefly comprised of conglomerate, breccia, shale, sandstone, and coal. The deepest hole on the property, DDH 81-22, penetrated close to 1,150 metres of Bowron River coal measures, representing a total true thickness of at least 700 metres.

A distinct feature of the sedimentary environment of the area is the frequent, although irregular, appearance of conglomeratic units varying from less than a metre to greater than 18 metres in thickness throughout the entire stratigraphic succession. The conglomerates, which rarely include coal beds, are interbedded with dominantly carbonaceous and coaly shales and sandstones.

- 9 -

The lateral distribution of the conglomerates is not well understood although there are indications that they thicken eastward. The dominant rock types of the Bowron River coal measures are carbonaceous shales and siltstones. Although they occur throughout the stratigraphic sequence, they appear to predominate in the Lower half of the section. They are the main units that envelope the major coal seams.

## 6.3 Structure

A structure contour map, drawn at the base of the Lower Seam, is shown in Figure 5. The map details the structure of a part of the basin and shows a small, south-plunging syncline terminated by a northeast transverse fault. The syncline has an average width of 1,200 metres. It is symmetrical, with its flanks dipping an average of 35 degrees. South of the transverse fault, the dips progressively steepen southwards to a maximum of 65 degrees west of DDH No. 22.

Evidence is lacking to support the suggestion of previous writers that the basin is graben-modified where the Bowron River coal measures are in fault contact with the Antler Formation. Borehole data indicates that the occasional truncation of the coal measures by the Antler Formation could be due to an initial topography at the start of sedimentary deposition. The steep dips on the southwest flank of the basin appears consistent with the tight folding that characterizes the structural profile of the rocks to the east and southeast.

- 10 -



Τſ

#### 6.4 Coal Seams

A simplified depositional model of the Bowron River coal measures suggests predominant swamp environment which was frequently interrupted by alternating and/or interacting lagoonal and fluviatile conditions. Most of the swamp developments, particularly in the upper part of the section, were short-lived, as they were either inundated during periods of marine incursions or destroyed by meandering streams.

Several coal seams occur throughout the Bowron River coal measures, either as discrete individual coal beds or as zones comprising a number of coal beds. Only two coal zones appear to be important.

#### 6.4.1 Lower Seam

The Lower Seam is actually a coal zone that occurs within 50 to 100 metres above the Antler Formation and is generally comprised of several closely spaced coal beds separated by rock bands. The zone includes coal beds ranging widely in thickness to as much as 6.7 metres. The rock bands range from laminae to a thickness of 1 In places the seam is comprised of only metre. one coal bed with thicknesses of as much as 5 In general, the seam is comprised of metres. interbedded coal and rock with thicknesses of up to 15 metres. At section 27 + 00 N, a rock band in the Lower Seam develops and, as it progresses southeastward, thickens and divides the seam into an upper and lower split with each split maintaining appreciable thicknesses.

The Lower Seam is persistent and correlatible over long distances.

# 6.4.2 Upper Seam

The Upper Seam occurs within 50 metres above the Lower Seam. It is less developed and less persistent although, like the Lower Seam, it includes a number of rock bands. Typically, the Upper Seam comprises two coal beds separated by a rock band nearly one metre thick. The maximum aggregate thickness of coal and rock observed in the Upper Seam was 4.75 metres. The seam appears better developed on the west flank of the basin.

#### 7.0 COAL QUALITY

#### 7.1 Proximate Analysis and Washability Tests

The coal from Bowron River has always been considered a thermal coal. However, additional laboratory tests are required to establish its quality. From the 1977 drilling programme, 30 core samples were submitted for Proximate Analyses and returned the following averages on an air-dry basis:

Moisture	3.63%
Ash	35.70%
Volatile Matter	26.79%
Fixed Carbon	33.98%
Sulphur	1.33%
BTU/lb	8,154

No washability tests were carried out on any of the above samples. The original laboratory results are found in Appendix I. Two composited coal samples from the 1981 drilling programme were submitted for float and sink analysis, the results of which are included in Appendix I. It would appear from these meagre results that the coal can be cleaned to less than 10% ash at product yields between 60% and 70%.

The results of washability tests on the two bulk samples are inconclusive and inadequate. The results can be found in Appendix II.

Additional analyses will be required to establish coal quality, as it would affect a mining plan as well as the proper design of a washplant.

## 7.2 Petrography

A petrographic study of a coal seam (presumably the Lower Seam) was carried out by the Geological Survey of Canada in 1972. The results indicate that the bright coal is principally comprised of vitrain and clarain almost in equal proportion. The maximum average reflectance for the whole seam is 0.65%.

#### 7.3 Amber Resin

Unique to Bowron River coal is the random occurrence of amber resin in the form of blebs, stringers, and disseminations, which amounts to as much as 4% of the coal by weight.

#### 8.0 COAL RESERVES

## 8.1 "Measured" Reserves

Exploratory borehole drilling has delineated appreciable reserves of high volatile bituminous coal over a part of the Bowron River coal property. These reserves occur in coal seams in the lower half of the Upper Cretaceous to Early Tertiary Bowron River coal measures. Figure 6 illustrates the relationship of the delineated reserve area with respect to the basin as a whole. It also illustrates the density of borehole drilling which provided closely spaced data that enabled a high degree of geological confidence in the interpretation of the structure and the correlation of seams. The calculated reserves confined within the drilled area are, therefore, of the "measured" category.

A summary of the "measured" coal reserves by seam is as follows:

Lower Seam (lower split) ..... 40,540,272 tonnes Lower Seam (upper split) ..... 7,970,136 tonnes Upper Seam ..... 1,393,872 tonnes

TOTAL 49,904,280 tonnes

#### 8.1.1 Computation Method and Parameters

5

The cross-section method of reserve computation was used. Cross sections were drawn to accommodate as many boreholes as possible at 300 metre spacings. In the closer spaced drilling the spacings were at 150 metres. In the computation of tonnage from each section the following formula was used: 

- Where: SL = seam length as measured from cross section
  W = Width of cross section which is the cross
  section spacing
  - T = Average seam true thickness from bore hole intersections
  - SG = Specific Gravity of the coal (assumed uniform at 1.60)

It must be noted that the seam thickness is the aggregate total true thickness of each coal bed within a seam and <u>does not</u> include the rock bands within the seam. The true <u>mining</u> thickness would therefore be the seam thickness (as used in the computation of reserves) plus the interseam rock bands. These rock bands would constitute the inseam dilution in the calculation of future mining reserves.

The assumed Specific Gravity of 1.60 is estimated to be near the true value for an average head ash of 35.70% for Bowron River coal. Several specific gravity measurements from coal samples would be required to establish a true specific gravity figure.

In cross sections where no borehole data is available, average seam thicknesses were borrowed from adjacent cross sections.

A summary of the computation of coal reserves is shown in Table 2.

# TABLE 2 - SUMMARY OF COAL RESERVE COMPUTATION

Lower Seam (Lower Split)

Se	ect	tio	<u>n</u>	Seam Length (Metres)	<u>Width</u>	Average Thickness	<u>S.G.</u>	Tonnes
9	+	00	s	1,850	300	4.42	1.60	3,924,960
6	+	00	s	1,720	300	3.67	1.60	3,029,952
3	+	00	S	1,650	30,0	3.67	1.60	2,906,640
0	÷	00		1,650	300	3.67	1.60	2,906,640
3	+	00	N	1,420	300	4.84	1.60	3,298,944
6	+	00	Ŋ	2,000	300	3.84	1.60	3,686,400
9	+	00	N	1,950	300	3.84	1.60	3,594,240
12	÷	00	N	1,860	225	4.05	1.60	2,711,880
13	+	50	N	1,890	150	4.33	1.60	1,964,088
15	+	00	N	1,150	225	6.95	1.60	2,877,300
18	+	00	N	1,200	300	5.73	1,60	3,300,480
21	+	00	N	1,160	300	3.08	1.60	1,714,944
24	' <b>+</b>	00	N	1,120	225	3.49	1.60	1,407,168
25	+	50	N	690	150	1.86	1.60	308,016
27	÷	00	N	850	150	2.98	1.60	607,920
28	÷	50	N	750	150	5.00	1.60	900,000
30	÷	00	N	750	150	3.11	1.60	559,800
31	+	50	N	680	150	5.02	1.60	512,040
33	+	00	N	540	150	4.06	1.60	328,860

TOTAL:

40,540,272

/

11

\_

# Lower Seam (Upper Split)

13	+	50	N	1,350	150	2.83	1.60	916,920
15	+	00	N	900	225	4.92	1.60	1,594,080
18	+	00	N	480	300	6.43	1.60	1,481,472
21	Ŧ	00	N	580	300	5.64	1.60	1,570,176
24	+	00	N	940	225	3.12	1.60	1,055,808
25	+	50	N	540	150	5.80	1.60	751,680
27	+	00	N	500	150	5.00	1.60	600,000

TOTAL: 7,970,136

# Upper Seam

24	+	00	N	340	225	1.97	1.60	241,128
25	+	00	N	300	150	1.12	1.60	80,640
27	+	00	N	820	150	1.13	1.60	222,384
28	+	50	N	740	150	1.33	1.60	236,208
30	+	00	N	710	150	1.69	1.60	287,976
31	+	50	N	820	150	0.92	1.60	181,056
33	+	00	N	350	150	1.72	1.60	144,480

TOTAL:

TOTAL TONNAGE IN UPPER AND LOWER SEAMS:

- 18 -

į

1

.

ł

**}-**`

ł

} --

49,904,280

ł

1

1,393,872

## 8.2 Potential Reserves

The drilled area from which measured coal reserves have been calculated comprises only a small portion of the Bowron River sedimentary basin. The distribution of outcrops, even if sparse, and aeromagnetic data support the interpretation that rocks of the Bowron River coal measures underlie the whole basin. Based on this interpretation, it is therefore possible to make an order of magnitude estimate of the coal potential of the remaining area outside the drilled area.

In the following calculation only the Lower Seam is considered:

Total Area	37,530,000	sq.	m
Average Seam Thickness			
(Assumed minimum)		. 4	m
Specific Gravity (Assumed)		1	• 6

Thus:  $37,530,000 \ge 4 \ge 1.6 = 240,192,000$  tonnes.

It is obvious that the above estimated tonnage must be moved to a more realistic figure consistent with the level of confidence in the geological interpretation. This confidence level may be expressed as a geologic factor which, in the case of the insufficient data in the above calculation, is set at 40%. The potential reserve calculation, based on the above assumptions, would therefore be:

 $37,530,000 \ge 4 \ge 1.6 \ge 0.40 = 96,076,800$  tonnes

- 19 -

#### 9.0 RECOMMENDATIONS

## 9.1 Borehole Drilling

Figure 8 shows the location of proposed drill holes. The proposed drilling programme has the following objectives:

- (a) to verify specific structural interpretations.
- (b) to extend the presently known reserves.
- (c) to identify other areas for more detailed drilling.

# 9.2 Bulk Sampling

Bulk samples should be taken either from old adits or from a new adit to provide sufficient material for the following tests:

- (a) pilot plant washability
- (b) combustion (clean coal)
- (c) attrition (raw coal and rock)

## 9.3 Coal Seam Logging, Sampling and Analysis

In the event that a core drilling programme is initiated, a comprehensive procedure should be drawn on coal seam logging, sampling, and laboratory analysis. Washability tests should be included where core recoveries are high and the flow sheet should be designed to ultimately provide simulated plant yields.

December 31, 1982

#### SELECTED REFERENCES

# APPENDIX I

ł

.

•

ł

# DRILL CORE ANALYTICAL RESULTS

ţ

PROJECT: Bowron River HOLE #: 77-1 Footage: 632.0 - 637.5

	<u>Air-dry Basis</u>	Dry Basis
Ash %	19.13	19.95
R.M. %	4.07	
V.M. %	32.42	33.79
F.C. %	44.38	46.26
S. %	1.24	1.29
BTU/15.	10,720	11,170

Estimated Amber Resin Content:

0.4%

CYCLONE ENGINEERING SALES LTD.

PROJECT: Bowron River HOLE #: 77-1 Footage: 639.0 - 647.5

	<u>Air-dry Basis</u>	<u>Dry Basis</u>
Ash %	27.74	28.83
R.M. %	3.77	
V.M. %	29.39	30.54
F.C. %	39.10	40.63
S. %	2.11	2.19
BTU/15.	9,370	9,740

Estimated Amber Resin Content: 0.3%

CYCLONE ENGINEERING SALES LTD.

t

PROJECT: Bowron River HOLE #: 77-1 Footage: 651.5 - 659.0

	<u>Air-dry Basis</u>	Dry Basis
Ash %	34.02	35.23
R.M. %	3.43	
V.M. %	28.11	29.11
F.C. %	34.44	35.66
S. %	2.87	2.97
BTU/16.	8,690	9,000

Estimated Amber Resin Content: 0.6%

CYCLONE ENGINEERING SALES LTD.

PROJECT: Bowron River

HOLE: DDH 77-2

Footage: 623' - 628'

	Air-dry basis	Dry basis
Ash %	30.57	31.83
R.M. %	3.95	
V.M. %	29.94	31.17
F.C. %	35.54	37.00
S. %	1.37	1.43
B.T.U./15.	9,140	9,520

Estimated Amber Resin Content: 0.8%

CYCLONE ENGINEERING SALES LTD.

ł

PROJECT: Bowron River

HOLE: DDH 77-3

Footage: 765' - 77**4**'

	<u>Air-dry basis</u>	<u>Dry basis</u>
∧sh %	50.98	52.54
R.M. %	2.97	
V.M. %	22.89	23.59
F.C. %	23.16	23.87
S. %	0.79	0.81
B.T.U./1b.	6,310	6,500

Estimated Amber Resin Content: 0.1%

CYCLONE ENGINEERING SALES LTD.

X.

PROJECT: Bowron River

HOLE: 77-4

Footage: 756' - 765'

	<u>Air-dry basis</u>	Dry basis
Ash %	34.88	35.97
R.M. %	3.03	
V.M. %	27.85	28.72
F.C. %	34.24	35.31
S %	1.32	1.36
BTU/16.	8,120	8,370

Estimated Amber Resin Content:

# CYCLONE ENGINEERING SALES LTD.

0.1%

PROJECT:	Bowron River
HOLE:	77-4
Footage:	765' - 773'

	Air-dry basis	Dry basis
Ash %	42.26	43.31
R.M. %	2.42	
V.I. %	25.79	26.43
F.C. %	29.53	30.26
S %	0.76	0.78
BTU/15.	7,090	7,270

Estimated Amber Resin Content: 0.09%

CYCLONE ENGINEERING SALES LTD.

;

PROJECT: Bowron River HOLE: 77-4 Footage: 773' - 778'

	Air-dry basis	Ury basis
Ash %	28.16	29.09
R.M. %	3.19	
V.M. %	31.90	32,95
F.C. %	36.75	37.96
S %	0.73	0.75
BTU/16.	9,280	9,590

Estimated Amber Resin Content: 0.1%

CYCLONE ENGINEERING SALES LTD.

1

PROJECT: Bowron River HOLE# 77-5 Footage: 893' - 909'

	<u>Air-dry basis</u>	<u>Dry basis</u>
Ash %	33.36	34.37
R.M. %	2.95	
V.M. %	31.20	32.15
F.C. %	32.49	33.48
S. %	1.11	1.14
BTU/15.	8,350	8,600

Estimated Amber Resin Content: 0.09%

CYCLONE ENGINEERING SALES LTD.

PROJECT:	Bowron Ri	ver
HOLE:	77-5	
Footage:	912' - 91	91

----

\_\_\_\_

	<u>Air-dry basis</u>	Dry basis
Ash %	33.25	34.27
R.M. %	2.98	
V.M. %	30.37	31.30
F.C. %	33.40	34.43
s.	2.01	2.01
BTU/15.	8,600	8,860

Estimated Amber Resin Content: 0.23%

CYCLONE ENGINEERING SALES LTD.

3

;

PROJECT: Bowron River HOLE: #77-6 Footage: 695.5' - 709.5

	<u>Air-dry basis</u>	Dry basis
Ash %	36.08	37.05
R.M.%	2.62	
V.M.%	33.04	33.93
F.C. %	28.26	29.02
S. %	0.82	0.84
BTU/15.	7,820	8,030

Estimated Amber Resin Content: 0.16%

CYCLONE ENGINEERING SALES LTD.

-
PROJECT: Bowron River

HOLE: 77-7

÷

Footage: 528.5' - 538'

	Air-dry basis	Dry basis
Ash %	23.65	24.62
R. M. %	3.93	
V. M. %	36.08	37.56
F. C. %	36.34	37.83
S. %	1.13	1.18
ВТU/1Ъ.	9,940	10,350

Estimated Amber Resin Content: 0.26 %

CYCLONE ENGINEERING SALES LTD.

CABLE ADDRESS COMTEC( TELEX 04-35269

# COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 228 NORTH LA SALLE STREET, CHICAGO, ILLINOIS 60801 - AREA CODE 312 728-8434

Please address all correspondence to: 147 Riverside Dr., North Vancouver, B.C. V7H 116



Office: Tel. (604) 929-2228

September 15, 1977

WRIGHT ENGINEERS LTD. Ste. #100 - 1444 Alberni St. VANCOUVER, BC V6G 2Z4

Report No. 64-16093 - 101

Sample Identification:

77-8	471-478'	77-11	988-997'
77-8	478-485'	77-11	1038-1045'
77-9	835-839.5'	77-12	919-927.5'
77-10	1262.5-1271'	77-13	958.5-962.5
		77-15	697.5-707'

	PROXIMATE ANALYSES								
Sample No.		As Received	Dry Basis						
77-8 471-478'	<pre>% Moisture % Ash % Volatile % Fixed Carbon</pre>	$ \begin{array}{r} 4.77 \\ 24.52 \\ 29.33 \\ \underline{41.38} \\ 100.00 \end{array} $	xxxxx     25.75     30.80     43.45     100.00						
	Btu	9481	9956						
	% Sulphur	1.73	1.82						
77-8 478-485'	<pre>% Moisture % Ash % Volatile % Fixed Carbon</pre>	5.0725.6929.3039.94100.00	xxxxx 27.06 30.86 42.08 100.00						
	Btu	9297	9794						
	% Sulphur	1.46	1.54						
77-9 835-839.5'	<pre>% Moisture % Ash % Volatile % Fixed Carbon</pre>	$ \begin{array}{r} 4.32\\ 21.84\\ 30.33\\ \underline{43.51}\\ 100.00 \end{array} $	xxxxx 22.83 31.70 <u>45.47</u> 100.00						
	Btu	9976	10426						
	<pre>% Sulphur</pre>	2.71	2.83						

Continued Page 2/ ...



Jere Free

Sample No.		As Received	Dry Basis
77-10 1262.5-1271'	<pre>% Moisture % Ash % Volatile % Fixed Carbon</pre>	3.29 41.23 22.57 32.91 100.00	xxxxx 42.63 23.34 34.03 100.00
	Btu	7267	7514
	% Sulphur	1.17	1.21
77-11 988-997'	<pre>% Moisture % Ash % Volatile % Fixed Carbon</pre>	3.2242.1322.9431.71100.00	xxxxx 43.53 23.70 <u>32.77</u> 100.00
	Btu	7134	7371
	% Sulphur	1.65	1.70
77-11 1038-1045'	<pre>% Moisture % Ash % Volatile % Fixed Carbon</pre>	4.36 29.81 26.38 <u>39.45</u> 100.00	xxxxx 31.17 27.58 41.25 100.00
	Btu	8763	9163
	% Sulphur	1.22	1.28
77-12 919-927.5'	<pre>% Moisture % Ash % Volatile % Fixed Carbon</pre>	3.36 46.94 19.93 29.77 100.00	xxxxx 48.57 20.62 30.81 100.00
	Btu	6307	6526
	% Sulphur	0.83	0.86
77-13 958.5-962.5'	<pre>% Moisture % Ash % Volatile % Fixed Carbon</pre>	4.64 20.89 32.12 42.35 100.00	xxxxx 21.91 33.68 44.41 100.00
	Btu	10012	10499
	% Sulphur	0.96	1.01

Wright Engineers Ltd. Continued Page 2

September 15, 1977

Continued Page 3/ ...

- (

COMMERCIAL TESTING & ENGINEERING CO.

Wright Engin Page 3	eers Ltd. Continue	ed	September 15, 1977
Sample No.		As Received	Dry Basis
77-15 697.5-707'	<pre>% Moisture % Ash</pre>	4.33 34.37	xxxxx 35.93
	<pre>% Volatile % Fixed Carbon</pre>	26.35 <u>34.95</u> 100.00	$\frac{36.53}{100.00}$
	Btu	8125	8493
	% Sulphur	1.34	1.40

Respectfully submitted, COMMERCIAL TESTING & ENGINEERING CO. ſ

Łø C. D. Saville Manager

js

COMMERCIAL TESTING & ENGINEERING CO. <u>র হ</u> চ

CABLE ADDRESS COMTE

### COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 228 NORTH LA SALLE STREET, CHICAGO, ILLINOIS 60601 · AREA CODE \$12 728-8434

Please address all correspondence to: 147 Riverside Dr., North Vancouver, B.C. V7H 1T6



Office: Tel. (604) 929-2228/

WRIGHT ENGINEERS LTD. Ste. #100 - 1444 Alberni St. VANCOUVER, BC V6G 224

Report No. 64-16148 - 50

September 27, 1977

Attention: Dr. L. S. Gormely, Mr. N. R. Krpan

Sample Identification:

DDH WL-3 846-859' DDH 77-17 1109-1114.5' DDH 77-17 1048.5-1057'

Sample NO.			As Received	Dry Basis	
WL-3	ક	Moisture	4.49	XXXXX	
846-859'	8	Ash	41.37	43.32	
	8	Volatile	24.72	25.88	
	8	Fixed Carbon	29.42	30.80	
			100.00	100.00	
		BTU	6646	6958	
	g	Sulphur	0.96	1.00	
77-17	8	Moisture	3.68	xxxxx	
1109-	8	Ash	35.07	36.41	
1114.5'	ક્ષ	Volatile	25.99	26.98	
	₹	Fixed Carbon	35.26	36.61	-
			100.00	100.00	
		BTU	8095	8404	
	£	Sulphur	1.09	1.13	
77-17	<del>.</del>	Moisture	2.92	xxxxx	
1048.5-	8	Ash	55.83	57.51	
1057'	€	Volatile	19.90	20.50	
	8	Fixed Carbon	21.35	21.99	
			100.00	100.00	
		BTU	5103	5256	
	8	Sulphur	0.50	0.51	
				<del></del>	~

Continued Page 2/ ...



ſ

# COMMERCIAL TESTING & ENGINEERING CO.

. 1

GENERAL OFFICES: 228 NORTH LA BALLE BTREET, CHICAGO, ILLINDIB 80801 - AREA CODE 312 728-0434

rside Dr., North Vancou	ver, B.C. V7H 1T6		Office: Tel. (604)
	Sth.	"Öctober 12	, 1977
WRIGHT ENGI Ste. #100 - VANCOUVER, V6G 224	NEERS LTD. 1444 Alberni Street BC	Report No.	64-16162-64
Attention:	Dr. L. S. Gormely Mr. N. R. Krpan		
Sample Iden	tification:	DDH 77-18	1145 - 1158.5' 1161 - 1167.5' 1169 - 1175'
	PROXIMAT	TE ANALYSIS	
SAMPLE NO.		AS RECEIVED	DRY BASIS
DDH 77-18	% Moisture	3.42	xxxxx
1145-1158.5'	% Ash	47.86	49.56
	<pre>% Volatile</pre>	22.66	23.46
	<pre>% Fixed Carbon</pre>	26.06	26.98
		100.00	100.00
	BTU	6194	6413
	% Sulphur	1.06	1.10
DDH 77-18	<pre>% Moisture</pre>	3.03	
1161-1167.5'	% Ash	47.90	49.40
	<pre>% Volatile</pre>	23.85	24.60
	<pre>% Fixed Carbon</pre>	25.21	_26.00
		100.00	100.00
	BTU	6132	6324
	% Sulphur	1.23	1.27
DDH 77-18	<pre>% Moisture</pre>	3.93	XXXXX
1169-1175'	% Ash	36.30	37.79
	<b>% Volatile</b>	27.48	28.60
	% Fixed Carbon	32.29	33.61
		100.00	100.00
	BTU	7883	8205
	<b>%</b> Sulphur	1.58	1.64

DENSITY: DDH 77-18 1161 - 1167.5' = 98.3 lbs/cu ft.

Respectfully submitted, COMMERCIAL TESTING & ENGINEERING CO.

> C. D. Saville Manager

-

LLINGS, MT + BIRMINGHAM, AL + CHARLESTON, WY + CLARKSBURG, WY + CLEVELAND, OH + DENVER, CO + GOLDEN, CO + HENDERSON, KY + MIDDLESBORO, KY + NORFOLK, VA + SOUTH HOLLAND

- -.

···. ·· ·· ·· ·· · · ·

jр

CABLE ADDRESS CO TELEX D

### COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 228 NORTH LA SALLE STREET, CHICAGO, ILLINOIS 60601 - AREA CODE 312 728-8434

Please address all correspondence to: 147 Riverside Dr., North Vancouver, B.C. V7H 116



Office: Tel. (604) 929-2

October 12, 1977

WRIGHT ENGINEERS LTD. Ste. #100 - 1444 Alberni Street VANCOUVER, BC V6G 2Z4 Report No. 64-16211-13 Attention: Dr. L. S. Gormely Mr. N. R. Krpan Sample Identification: DDH 77-19 1015.5 - 1027'1027 - 1040' 1040 - 1047' PROXIMATE ANALYSIS SAMPLE NO. AS RECEIVED DRY BASIS DDH 77-19 % Moisture 3.53 XXXXX 1015.5-1027' % Ash 40.69 42.18 % Volatile 19.22 19.92 % Fixed Carbon 36.56 37.90 100.00 100.00 BTU 7278 7544 % Sulphur 1.34 1.39 DDH 77-19 % Moisture 3.04 XXXXX 1027-1040' % Ash 49.84 51.40 % Volatile 19.42 20.03 % Fixed Carbon 27.70 28.57 100.00 100.00 BTU 5828 6011 Sulphur 1.42 1.46

DDH 77-19 1040-1047'



4.21

34.73

19.16

41.90

1,28

8104

C. D. Saville Manager

XXXXX

36.26

20.00

43.74

1.34

8460

jр

LINGS, MT + BIRMINGHAM, AL + CHARLESIDA, WY + CLARKSBURG WY + CLEVELANY DH + CENED OD N CONDEN OF A PROFESSION OF

% Moisture

% Volatile

% Fixed Carbon.

& Ash

BTU

% Sulphur



# **COMMERCIAL TESTING & ENGINEERING CO.**

GENERAL OFFICES: 228 NORTH LA SALLE STREET, CHICAGO, ILLINOIS 60601 AREA CODE 312 726-8434



PLEASE ADDRESS ALL CORRESPONDENCE TO: 16130 VAN DRUNEN RD., P.O. BOX 127 SOUTH HOLLAND, IL 60473 OFFICE TEL. (312) 264-1173

NORCO RESOURCES LTD. 412-200 Granville Street Vancouver, B.C., Canada V7C 1S4

\_ \_ ~ ~

Kind of sample

reported to us

Sample taken at

Sample taken by

Date sampled

Date received

Coal from D.H. #2

Norco Resources Ltd.

Norco Resources Ltd.

June 11, 1981

Sample identification by Norco Resources Ltd.

> Composite of "A" samples. Samples crushed to 6 mm x 0.

Analysis of Raw Coal Head Sample.

Analysis report no. 71-71962

Dry Basis

XXXXX

25.42

37.68

36.90

10020

1.82

Oxidizing

XXXX

XXXX

XXXX

XXXX

°F

°F

٩F

°۴

100.00

#### PROXIMATE ANALYSIS

As Received

3.48

24.54

36.37

35.61

9671

1.76

Reducing

XXXX

XXXX

XXXX °F

XXXX °F

٩F

°F

100.00

% Moisture % Ash % Volatile % Fixed Carbon

> Btu/lb. % Sulfur

> > FUSION TEMPERATURE OF ASH

Initial Deformation	
Softening $(H = W)$	
Softening $(H = \frac{1}{2}W)$	
Fluid	

THEN THE LACE DED.

17 - 1755

Respectfully submitted, COMMERCIAL TESTING & ENGINEERING CO.

H == Cone Height W == Cone Width

Original Copy Watermarked For Your Protection

١.

DENSIER CO. C

R. A. HOUSER, Manager, Midwest Division

BALTIMORE, MD + BILLINGS, MT + BIRMINGHAM, AL + BYESVILLE, OH + CHARLESTON, WV + CLARKSRURG, WV + CLEVELAND, OH + CONNEAUT, OH Charter Member SERVER LY DEVICTOR TY REPER

### NORCO RESOURCES LTD. Vancouver, B.C.

D.H. #2 Composite of "A" samples Sample crushed to 6 mm x 0 Analysis Report No. 71-71963 - 71967

June, 1981

### FLOAT & SINK ANALYSIS

SPECIFIC	GRAVITY			FRACTION	ANALYSIS,	DRY BASIS	
SINK	FLOAT	₹WT.	*ASH	€SUL.	BTU	₹VOL.	%F.C.
<b></b>	1.40	51.6	5.22	1.59 -	13236	41.63	53.15
1.40	1.50	11.4	16.69	2.85	11439	38.38	44.93
1.50	1.60	6.1	27.35	3.12	9800	34.53	38.12
1.60	1.70	4.9	36.26	2.83	8425	31.68	32.06
1.70		26.0	64.97	1.46	3421	27.23	7.80
			CUMULATIVE	RECOVERY			
			(FLO	AT)			
—	1.40	51.6	5.22	1.59	13236	41.63	53.15
1.40	1.50	63.0	7.30	1.82	12911	41.04	51.66
1.50	1.60	69.1	9.07	1.93	12636	40.47	50.46
1.60	1.70	74.0	10.87	1.99	12357	39.89	49.24
1.70		100.0	24.93	1.85	10034	36.59	38.48
			CUMULATIV	E REJECT			
			(SIN	K)			
	1.40	100.0	24.93	1.85	10034	36.59	38.48
1.40	1.50	48.4	45.95	2.14	6620	31.23	22.82
1.50	1.60	37.0	54.97	1.92	5135	29.02	16.01
1.60	1.70	30.9	60.42	1.68	4215	27.94	11.64
1.70		26.0	64.97	1.46	3421	27.23	7.80

Respectfully submitted,

COMMERCIAL TING & ENGINEERING CO.

waw 0

R. A. Houser, Manager, Midwest Division

RAH/đh

COMMERCIAL TESTING & ENGINEERING CO.



# Li-

# COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 228 NORTH LA SALLE STREET, CHICAGO, ILLINOIS 60601 AREA CODE 312 726-8434



PLEASE ADDRESS ALL CORRESPONDENCE TO: 16130 VAN DRUNEN RD., P.O. BOX 127 SOUTH HOLLAND, IL 60473 OFFICE TEL. (312) 264-1173

NORCO RESOURCES LTD. 412-200 Granville Street Vancouver, B.C., Canada V7C 1S4

Kind of sample

reported to us

Sample taken at

Sample taken by

Date sampled

Date received

Coal from D.H. #4

Norco Resources Ltd.

Norco Resources Ltd.

462

June 11, 1981

Sample identification by Norco Resources Ltd.

> Composite of "B" samples. Samples crushed to 6 mm x 0.

Analysis of Raw Coal Head Sample.

Analysis report по. 71-71968

PROXIMATE ANALYSIS

As Received Dry Basis 3.06 XXXXX % Moisture 34.06 35.14 % Ash 28.26 29.15 % Volatile 34.62 35.71 % Fixed Carbon 100.00 100.00 8375 8639 Btu/lb. 1.04 1.07 % Sulfur

#### FUSION TEMPERATURE OF ASH

	Reducing	Oxidizing	
Initial Deformation	xxxx °F	xxxx °F	
Softening $(H = W)$	XXXX °F	XXXX °F	H Cone Height
Softening $(H = \frac{1}{2}W)$	xxxx ∘ <sub>F</sub>	xxxx °F	W == Cone Width
Fluid	xxxx °F	xxxx °F	

Respectfully submitted, COMMERCIAL PESTING & ENGINEERING CO.

Charter Member

Original Copy Watermarked For Your Protection

R. A. HOUSER, Manager, Midwest Division BALTIMORE, MD - BILLINGS, MT - BIRMINGHAM, AL - BYESVILLE, OH - CHARLESTON, WV - CLARKSBURG, WV - CLEVELAND, OH - CONNEAUT, OH

### NORCO RESOURCES LTD. Vancouver, B.C.

D.H. #4 Composite of "B" samples Sample crushed to 6 mm x 0 Analysis Report No. 71-71969 - 71973

June, 1981

#### FLOAT & SINK ANALYSIS

SPECIFIC	GRAVITY		FR	ACTION A	NALYSIS,	DRY BASIS	
SINK	FLOAT	8WT.	&ASH	*SUL.	BTU	&VOL.	%F.C.
	1.40	45.1	4,54	1.26	13189	40.48	54,98
1.40	1.50	9.1	16.29	2.67	11376	37.75	45.96
1.50	1.60	3.2	28.41	1.78	9568	33.24	41.35
1.60	1.70	2.3	37.95	1.38	8140	30.15	31.90
1.70		40.3	78.85	0.45	1842	17.63	3.52
		CUMU	LATIVE RE	COVERY			
		<u> </u>	(FLOAT)				
	1.40	45.1	4.54	1.26	13189	40.48	54.98
1.40	1.50	54.2	6.5L	1.50	12885	40.02	53.47
1.50	T.00	5/.4	7.73	T. DT	12700	39.04	52.03
1.60	1.70	59./	8,90	1.51	12524	39.28	51.82
1.70		100.0	37.09	1.08	8219	30.55	32.36
		CUM	ULATIVE R (SINK)	EJECT			
 1.40	1.40 1.50	100.0 54.9	37.09 63.83	1.08 0.93	8219 4136	30.55 22.40	32.36 13.77
1.50	1.60	45.8	73.27	0.59	2698	19.35	7.38
1,60	1.70	42.6	76.64	0.50	2182	18.31	5.05
1.70		40.3	78.85	0.45	1842	17.63	3.52
~* • •				~ • • • •			

Respectfully submitted,

COMMERCIAL TESTING & ENGINEERING CO.

R. A. Houser, Manager, Midwest Division

RAH/dh

COMMERCIAL TESTING & ENGINEERING CO.



Original Copy Watermarked For Your Protection

}-

CLIENT : NORCO RESOURCES LIMITED

PROJECT: DRILLHOLE CORE 81-22 COMPOSITE OF 13 INTERVALS from 1171.27 to 1183.35 = 12.2

LAB NO.: 8310

HEAD RAW ANALYSIS

Ī	MOIST%	ASH%	VOĽ%	F.C.%	S%	CALC. BASIS
Ī	0.9	55.0	22.1	22.0	0.67	<u>a.d.b.</u>
		55.5	22.3	22.2	0.68	a.p.

SIZE CONSIST: RAW COAL CRUSHED TO - 1 1/2"

SIZE FRACTION	WT%	CUM WT%
1 1/2" x 3/8 "	88.1	88.1
3/8 " x 28M	11.3	99.4
28M x 0	0.6	100.0

SINK-FLOAT ANALYSIS, adb: 1 1/2"x0									
SG FRACTION	WT%	RM%	ASH%	VOL%	F.C.%	S%	C.V. Cal/gm	CUMULA WT%	ASH%
- 1.40	23.7	1.5	7.9	39.1	51.5	1.07	7245	23.7	7.9
1.40- 1.50	4.7	1.5	23.9	33.4	41.2	1.13	5842	28.4	10.5
1.50- 1.60	5.5	1.2	30.9	31.3	36.6	0.88	5202	33.9	13.8
1.60- 1.70	5.5	1.2	40.4	26.5	31.9	1.30	4415	39.4	17.6
+1.70	60.6	0.6	79.4	-	-	-	-	100.0	55.0

ANALYSIS OF COMPOSITE FLOATS @ 1.60 S.G.

	ULTIMATE ANALYSIS, adb							
Γ	H20%	С%	H%	N%	S%	ASH%	O(by dif	HGI
	1.50	69.16	4.28	1.30	1.02	13.74	9.00	53

ASH FUSION TEMPERATURES(OF)							
ATMOSPHERE	I.D.T.	S.T.	Н.Т.	F.T.			
OXIDIZING	2120	2280	2320	2400			
REDUCING	2040	2140	2220	2340			

Birtley Coal & Minerals Testing

1

ī.

APPENDIX II

- - -

BULK SAMPLING ANALYTICAL RESULTS

Bowron River Mines

TABLE 1. ANALYSIS OF FEED SAMPLE

PROXIMATE ANALYSIS:

Ash %	36.10
R.M. %	2.24
V.M. %	30.99
F.C. %	30.67

ULTIMATE ANALYSIS:

Ash %	36.10
Carbon %	48.59
Hydrogen %	3.75
Nitrogen %	0.90
Sulphur %	0.97
Oxygen % (by difference)	9.69

TOTAL 100.00

1

í

# Bowron River Mines

TABLE 1. ANALYSIS OF FEED SAMPLE continued

# MINERAL ANALYSIS OF ASH:

SiO <sub>2</sub>	%	63.76
A12 <sup>0</sup> 3	o/ 70	18.88
Ca0	0% 10	1.92
Mg0	0/ /0	1.18
<sup>Fe</sup> 2 <sup>0</sup> 3	%	5.49
Na20	%	1.33
к <sub>2</sub> 0	%	0.53
Ti0 <sub>2</sub>	%	0.56
P2 <sup>0</sup> 5	%	0.33
50 <sub>ع</sub>	%	1.67

ASH FUSIBILITY:

	Atmosphere	Atmosphere
Initial Deformation Temperature	2320 <sup>0</sup> F.	2400 <sup>0</sup> F.
Softening Temperature (Spherical)	2480 <sup>0</sup> F.	2560 <sup>0</sup> F.
Softening Temperature (Hemispherical)	2540 <sup>0</sup> F.	2600 <sup>0</sup> F.
Fluid Temperature	2700 <sup>0</sup> F	2800 <sup>0</sup> F.

# **OTHER TESTS:**

Calorific Value	8,310	BTU/16.
FSI	N.A.	
HGI	58.0	

. . . . . . . . . . . . .

Bowron River Mines

# TABLE 2. ANALYSIS OF PRODUCTS AFTER WASHING AT EMR PILOT PLANT

# A. <u>CLEAN COAL AND MIDDLING</u>

# PROXIMATE ANALYSIS:

	<u>Clean Coal</u>	Middling
Ash %	9.79	35.00
R.M. %	2.54	2.11
V.M. %	34.93	26 <b>.9</b> 9
F.C. %	52.74	35.90

### ULTIMATE ANALYSIS:

Ash %	9.79	35.00
Carbon %	67.89	47.48
Hydrogen %	4.91	3.66
Nitrogen %	1.15	0.87
Sulphur %	0.90	0.87
Oxygen % (by difference)	15.36	12.12
TOTAL	100.00	100.00

Ţ

MINERAL ANALYSIS OF ASH:

Bowron Mines Ltd.

# TABLE 2. ANALYSIS OF PRODUCTS AFTER WASHING AT EMR PILOT PLANT continued

#### Clean Coal Middling Si0<sub>2</sub> % 58.60 65.76 A1203 % 16.98 18.96 5.77 CaO % 1.37 1.78 1.18 Mg0 % 6.23 5.37 Fe203 % Na20 % 1.35 1.37 0.66 K<sub>2</sub>0 % 0.53 Ti0<sub>2</sub> % 0.51 0.55 0.26 0.31 P205 % 4.26 1.12 so<sub>3</sub> %

ASH FUSIBILITY:	CLEAN (	COAL	MIDDLING	
	Reducing <u>Atmosphere</u>	Oxidizing Atmosphere	Reducing Atmosphere	Oxidizing ' <u>Atmosphere</u>
Initial Deformation Temp.	2140 <sup>0</sup> F	2260 <sup>0</sup> F	2320 <sup>0</sup> F	2480 <sup>0</sup> F
Softening Temp. (Spherical)	2260 <sup>0</sup> F	2340 <sup>0</sup> F	2520 <sup>0</sup> F	2600 <sup>0</sup> F
Softening Temp. (Hemispherical)	2340 <sup>0</sup> F	2400 <sup>0</sup> F	2600 <sup>0</sup> F	2660 <sup>0</sup> F
Fluïd Temperature.	2600 <sup>0</sup> F	2700 <sup>0</sup> F	2720 <sup>0</sup> F	2760 <sup>0</sup> F

OTHER TESTS:	CLEAN COAL	MIDDLING
Calorific Value (BTU/1b)	12,360	8,630
FSI	1/2	N.A.

}-

Bowron River Mines

TABLE 2. ANALYSIS OF PRODUCTS AFTER WASHING AT EMR PILOT PLANT continued

B. <u>REJECTS</u>:

	Coarse <u>Reject</u>	Fine <u>Reject</u>
Ash %	68.67	37.40
Calorific Value (BTU/15.)	4,580	8,050

### TABLE 3. SIZE CONSIST OF PRODUCTS

, , , , , , , , , , , , , , , , , , ,		WT. %						
SIZE	Clean Coal	Middling	Coarse Reject	Fine Reject				
+ 3/8"	.00	1.42	1.32	0.00				
3/8" x 28 mesh	49.85	94.76	89.46	15.18				
28 m x 150 mesh	42.90	3.56	8.95	74.96				
150 m x 0	7.25	0.26	0.27	9.86				
TOTAL	100.00	100.00	100.00	100.00				

Bowron River Mines

TABLE 4. FLOAT-SINK ANALYSIS OF + 28 MESH FRACTIONS OF PRODUCTS

	WT. %						
SP. GR.	CLEAN COAL	MIDDLING	COARSE REJECT	FINE REJECT			
- 1.25	0.44 (1.16)			0.19 (1.16)			
1.25 - 1.30	18.07	22.71	3.23	2.40			
1.30 - 1.35	63.51	15.91	4.32	15.92			
1.35 - 1.40	7.42	0.31	5.53	6.32			
1.40 - 1.50	5.67	7.28	0.47	9.16			
1.50 - 1.60	1.87	2.14	3.36	9.41			
1.60 - 1.80	1.28	5.04	6.78	16.68			
1.80 - 2.00	0.62	7.35	7.90	15.66			
+ 2.00	1.12 (2.33)	39.26 (2.44)	68.41 (2.38)	24.26 (2.34)			
TOTAL	100.00	100.00	100.00	100.00			

Figures in Parenthesis are the Sp.Gr. of the fractions.

January 13, 1977

1

CYCLONE ENGINEERING SALES LTD.

Bowron River Mines

TABLE 5. FLOAT-SINK ANALYSIS OF 28 MESH x 150 MESH FRACTIONS OF PRODUCTS

	WT.%					
SP. GR.	CLEAN COAL	MIDDLING	COARSE COAL	FINE COAL		
- 1.25	0.49 (1.15)	0.73 (1.20)	0.33 (1.14)	0.35 (1.14)		
1.25 - 1.30	29.45	24.78	10.03	2.59		
1.30 - 1.35	43.66	24.49	14.45	21.82		
1.35 - 1.40	8.84	5.83	2.17	8.20		
1.40 - 1.50	5.33	4.37	2.17	6.64		
1.50 - 1.60	3.89	3.50	2.34	8.59		
1.60 - 1.80	2.36	4.66	3.68	8.16		
1.80 - 2.00	1.56	4.96	5.68	7.17		
+ 2.00	4.42 (2.45)	26.68 (2.34)	59.15 (2.23)	36.48 (2.34)		
TOTAL	100.00	100.00	100.00	100.00		

Figures in Parenthesis are the Sp. Gr. of the fractions.

TABLE 6. ASHES OF 150 M × 0 FRACTIONS OF PRODUCTS							
		CLEAN COAL	MIDDLING	COARSE REJECT	FINE REJECT		
ASH %		30.12	22.29	38.94	33.87		

January 13, 1977

CYCLONE ENGINEERING SALES LTD.

5

#### 9.0 RECOMMENDATIONS

#### 9.1 Borehole Drilling

Figure 8 shows the location of proposed drill holes. The proposed drilling programme has the following objectives:

- (a) to verify specific structural interpretations.
- (b) to extend the presently known reserves.
- (c) to identify other areas for more detailed drilling.

### 9.2 Bulk Sampling

Bulk samples should be taken either from old adits or from a new adit to provide sufficient material for the following tests:

- (a) pilot plant washability
- (b) combustion (clean coal)
- (c) attrition (raw coal and rock)

### 9.3 Coal Seam Logging, Sampling and Analysis

In the event that a core drilling programme is initiated, a comprehensive procedure should be drawn on coal seam logging, sampling, and laboratory analysis. Washability tests should be included where core recoveries are high and the flow sheet should be designed to ultimately provide simulated plant yields.

S. Verie

Ruben Verzosa, P. Eng.

December 31, 1982



.

400	1600	1800	2000	2200	2400	GEOLOGY:       R.S.V. 1981         DRAWN BY:       P.S.H.         N.T.S. GRID:       93H/13 (W)         SCALE:       1:5000         DATE:       31 Dec. 1981
						SECTION 34+50N
						786
				1		





.

- -

	1600	1800	, 2000	2200	2400	GEOLOGY:       R.S.V. 1981         DRAWN       BY:         P.S.H.         N.T.S.       GRID:         93H/13 (W)         SCALE:         1:5000         BATE:         31 Dec.         1981
						SECTION 33+00N
						NORCO BOWRON COALFIELD
						786
:						•
1						
						-





.....

						786
						NORCO BOWRON COALFIELD
						SECTION 31+50N
						GEOLOGY: R.S.V. 1981 DRAWN BY: P.S.H.
0	1600	1800	2000	2200	2400	N.T.S. GRID:         93H/13 (W)         FIG. No.           SCALE:         1:5000         8-3           DATE:         31 Dec. 1981         8-3



(M3)



----

1400	1600	1800	2000	2200	2400	GEOLOGY:       R.S.V. 1981         DRAWN       BY:       P.S.H.         N.T.S.       GRID:       93H/13 (W)         SCALE:       1:5000       8-4         DATE:       31 Dec. 1981       8-4
						SECTION 30+00N
						NORCO RESOURCES LTD BOWRON COALFIELD
						786
ι.						
ł						
2						

(MM)





\* \*

•

.

				-		-
						$\neg$
						NORCOL BOWPON COALELE
						SECTION 28+50N
100	1600	1800	2000	2200	2400	GEOLOGY:         R.S.V. 1981           DRAWN BY:         P.S.H.           N.T.S. GRID:         93H/13 (W)           SCALE:         1:5000









1						
					-	(FM)
	3					
?						
						-
		•				_
						786
						RESOURCES LTD BOWRON COALFIELD
						GEOLOGY: R.S.V. 1981
0	1600	1800	2000	2200	2400	DRAWN         BY:         P.S.H.           N.I.S.         GRID:         93H/13(W)         FIG. No.           SCALE:         1:5000         8-7









						(ro)
÷						
ł						
		3				- -
?						
						786
						NORCO RESOURCES LTD BOWRON COALFIELD SECTION 22+50N
				-		GEOLOGY: R.S.V. 1981 DRAWN BY: P.S.H.
00	1600	1800	2000	2200	2400	N.I.S. GRID:     93H7 I3 (W)     FIG. No.       SCALE:     1:5000     8-9       DATE:     31 Dec. 1981     8-9









![](_page_68_Figure_0.jpeg)

![](_page_68_Picture_3.jpeg)

![](_page_69_Figure_0.jpeg)

•

.

•

![](_page_69_Picture_5.jpeg)

![](_page_70_Figure_0.jpeg)

.

1	1		3		ann ta ann an	MIY
						-
						, ,
						-
						786
			ł			NORCO RESOURCES LTD BOWRON COALFIELD
						GEOLOGY: R.S.V. 1981
400	1600	1800	2000	2200	2400	DRAWN BT         P.S.H.           NT.S. GRID:         93H/13 (W)           SCALE:         1: 5000           DATE:         31 Dec. 1981

![](_page_70_Picture_2.jpeg)

![](_page_71_Figure_0.jpeg)

•

**\*** 

······

![](_page_71_Picture_3.jpeg)




















•

•

.

•



—









## --- 5964000 N

— 5963000 N

1



