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In reply please  
quote file:

Mr. Barry Ryan, Coal Geologist  
Geological Survey Branch  
Ministry of Employment and Investment  
1810 Blanshard Street  
Victoria, B.C. V8V 1X4

July 19, 1996

**Re: Assessment Report for Saddle Surface Geophysics Project**

Enclosed, please find a copy of the assessment report for the above project which was completed in 1993. Various components had to be added to Mr. Sharma's base report, which was produced for in-house use only, to create a more complete package.

Any questions about this material should be directed to me.

Thank You.

Yours truly,

Ted Hannah  
Senior Geologist  
(604) 425-3118



MAILING ADDRESS: P.O. BOX 2003, SPARWOOD, B.C., CANADA V0B 2G0 (604) 425-2555 FAX (604) 425-7144





# line creek resources ltd.

In reply please  
quote file:

Ministry of Employment and Investment  
Energy and Minerals Division  
525 Superior Street  
Victoria, B.C.  
V8V 1X4

Dear Sirs:

Re: Professional Verification of Report  
Entitled: Saddle (Ewin Pass) Surface Geophysics  
Kootenay Land District, B.C., 1993

Enclosed please find our report on the Saddle Surface Geophysics Project.

This report has been prepared by Mr. A. Sharma and Mr. T. Hannah, both of whom were employed by Crows Nest Resources Limited, now Line Creek Resources Ltd., as geologists.

Mr. A. Sharma, B.Sc., graduated in Geophysics from the University of Calgary in 1989. Prior to his graduation, Mr. Sharma worked as an assistant for a major coal company in the Crows Nest coalfields. Mr. Sharma was employed by Crows Nest Resources Limited as a Project Geologist from May 1989 until December 1993.

Mr. T. Hannah, B.Sc.P.Geol., graduated in Geology from the University of New Brunswick in 1972. Since graduation, Mr. Hannah has spent 24 years working for Shell Canada Ltd., Crows Nest Resources and Line Creek Resources on a wide variety of coal exploration projects in B.C. and Alberta. His present position is that of Senior Geologist, Engineering Group, Line Creek Mine.

In my opinion, these personnel are fully qualified, by training and experience to prepare this report.

Yours truly,

Line Creek Resources

R. Williams, P.Eng.  
Chief Engineer



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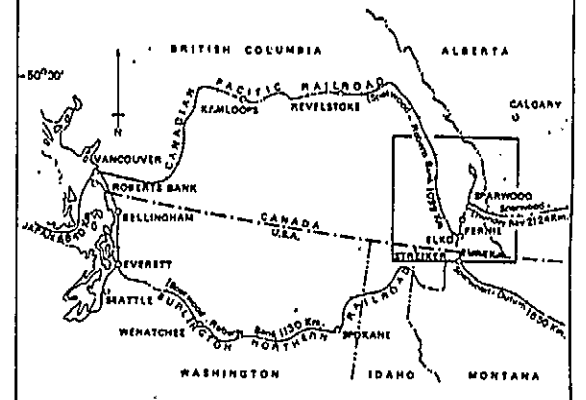
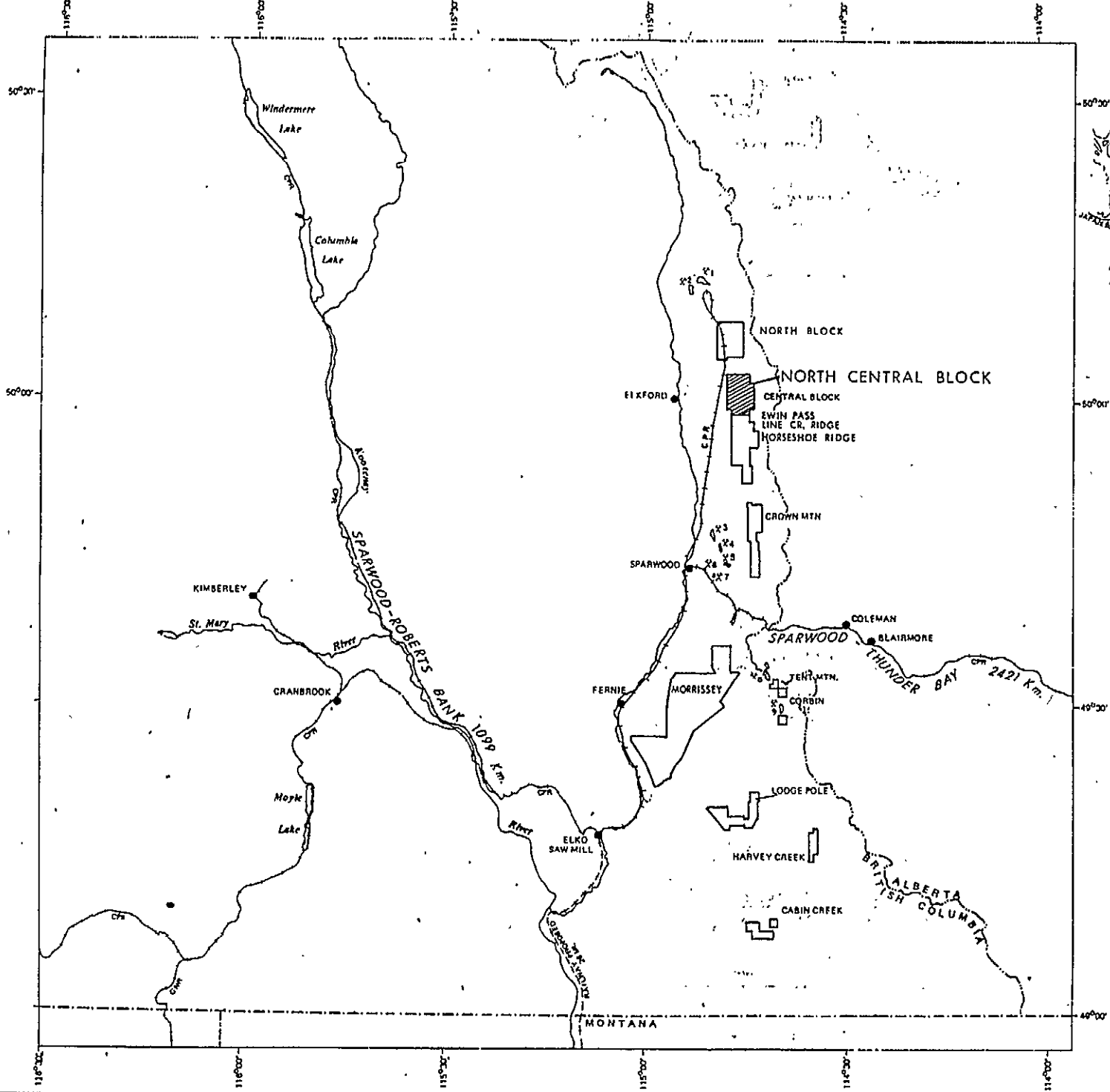
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- III. HLEM Survey Lines 400N, 800N, 1200N
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- V. Conductivity - Thickness of Massive Sulphide Bodies



**LEGEND**

- OPERATING MINES**
- 1 FORDING COAL LTD.
  - 2 CLODE PIT
  - 3 GREENHILL MT
  - KAIPER RESOURCES LTD.
  - 4 HARMER PITS 1 & 2
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  - 6 CAMPS & ADIT 6A PITS
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  - BYRON CREEK COLLIERIES LTD.
  - 10 CORBIN PIT
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- SHELL - CNRL

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SOUTHEAST B.C.  
LOCATION MAPS

**FIGURE 1.**

author: Mortonhegyi	scale: 1:200,000	ENCLOSURE NO.
DATE: Feb 11, 1979	REVISED	DRAWING NO. BA-233
To: Department		

## Objectives

The objectives of the 1993 Saddle (Ewin Pass) Area project were to experiment with Horizontal Loop Electro - Magnetics and use the obtained data to assist in the interpretation of the structural geology of the area.

## Location

### **Geographic Location**

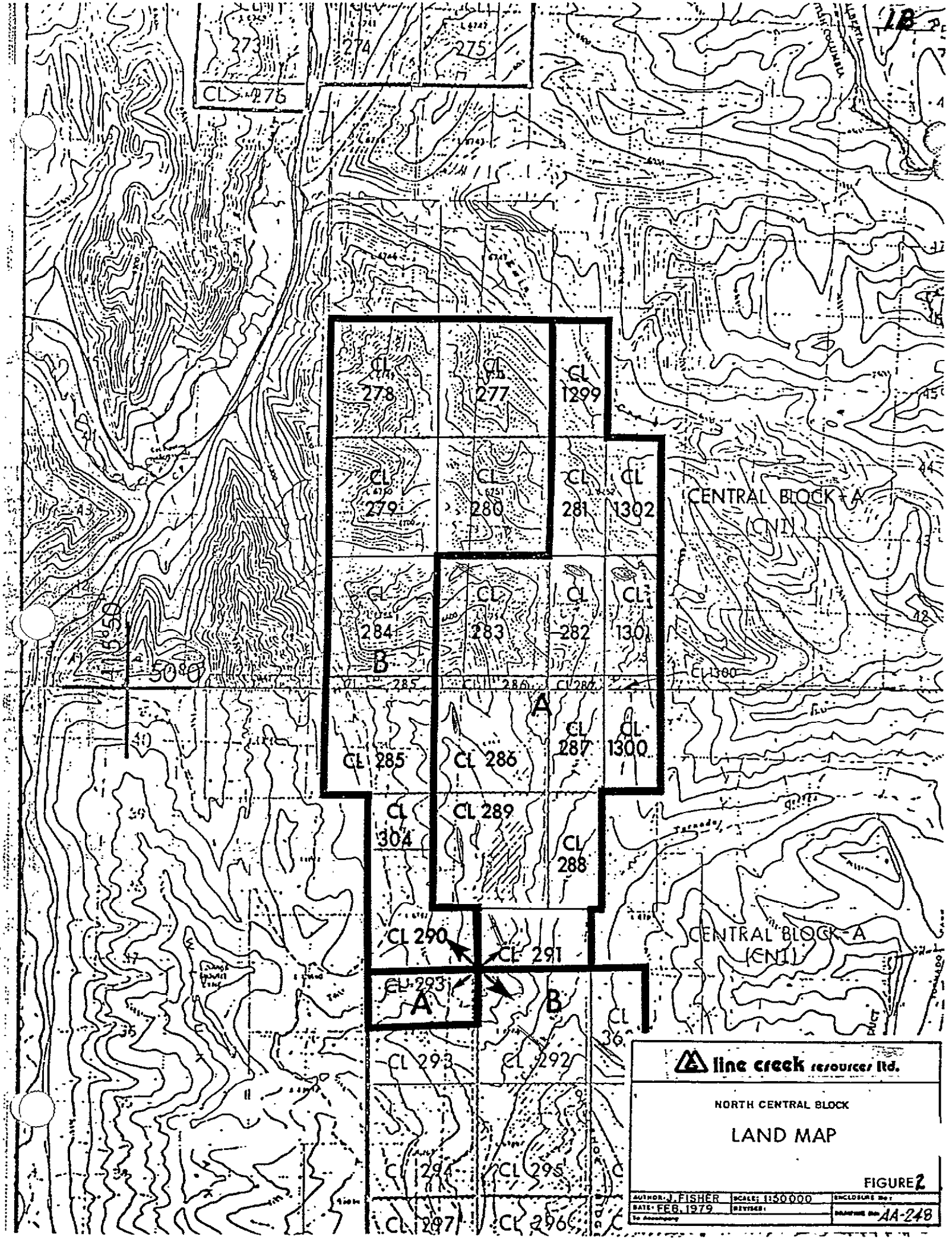
The property is located adjacent to the Elk River Valley in the Crowsnest Pass of the Rocky Mountains in the Southeastern British Columbia. The property is approximately 1150 kilometres east of Vancouver and 27 kilometres north of the town of Sparwood. (Figure No. 1)

The North Central Block is to be found on National Topographic System (NTS) map 82G, FERNIE ( 1: 250 000 ), 82G/15, TORNADO MOUNTAIN ( 1: 50 000), and 82J/2 FORDING RIVER ( 1: 50 000). It is encompassed by 49° 57' N, 50° 03' N, and 114° 44' W, 114° 48' W of the prime meridian, and comprises slightly more than 43 km<sup>2</sup>. (Figure No. 2)

### **Access**

The southern portion of the area is accessible from the south via the Line Creek Road. This road follows the valley floor, paralleling the North Central Block for approximately 2.7 km. It is necessary to climb the slopes from the valley - bottom road to the work area, on useable exploration roads.

Crows Nest industries Limited constructed a road, (CNI Road), from the valley floor to Ewin Pass Ridge in the late 1960's. This road has been maintained and is in fair condition. (Figure No. 3)



273 274 275

CL 276

CL 278 CL 277 CL 1299

CL 279 CL 280 CL 281 CL 1302

CL 284 CL 283 CL 282 CL 1301

CL 285 CL 286 CL 287 CL 1300

CL 304 CL 289 CL 288


CL 290 CL 291

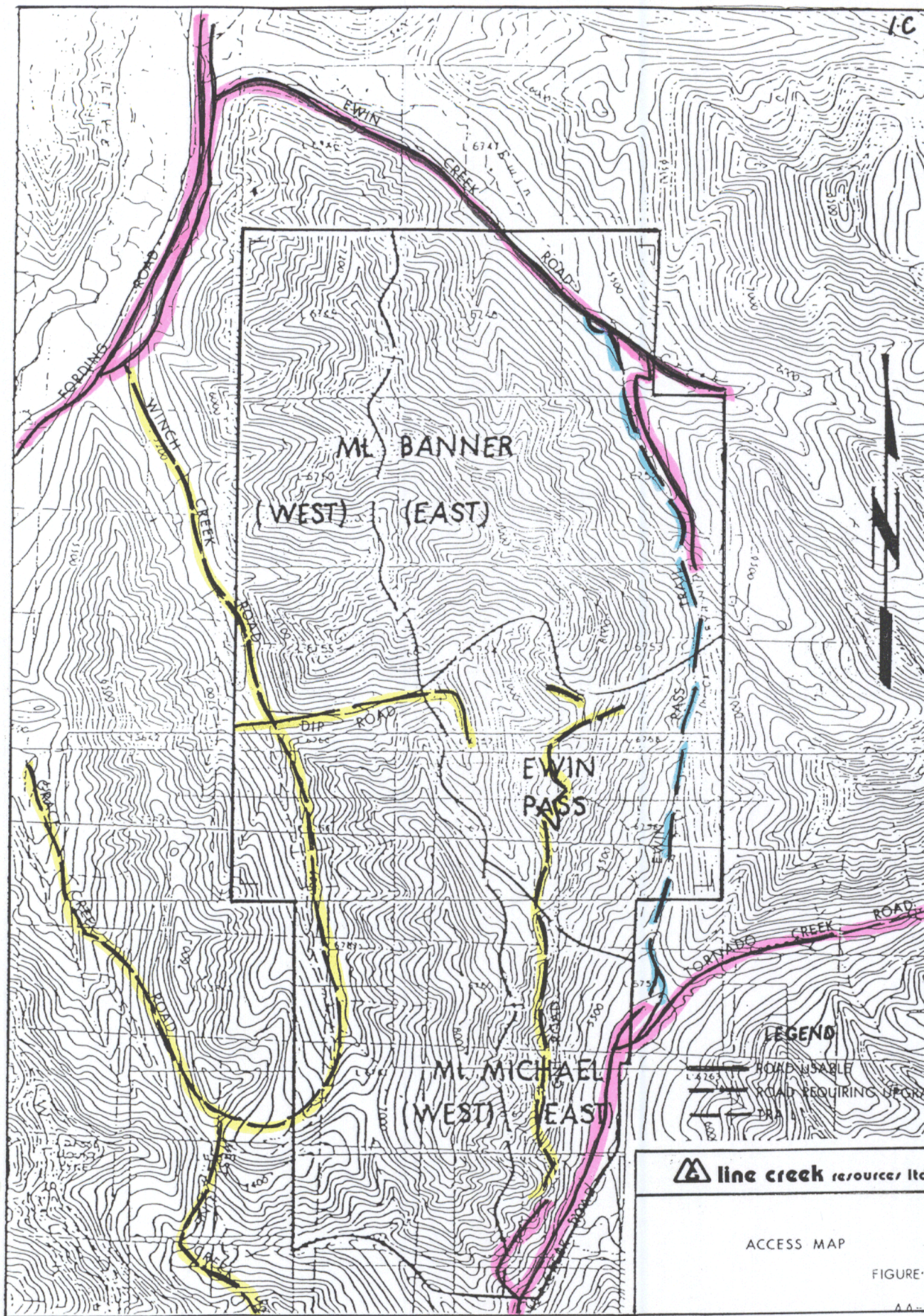
CL 293 CL 292

CL 294 CL 295

CENTRAL BLOCK A  
(ENL)

CENTRAL BLOCK A  
(ENL)

 <b>line creek resources ltd.</b>		
NORTH CENTRAL BLOCK LAND MAP		
<b>FIGURE 2</b>		
AUTHOR: J. FISHER DATE: FEB. 1979 To: Asst. Comm.	SCALE: 1:50000 REVISED:	ENCLOSURE NO: DRAWING NO: AA-248



**LEGEND**

ROAD USABLE

ROAD REQUIRING IMPROVEMENT

**line creek resources ltd.**

ACCESS MAP


FIGURE 4

AA-2



2A

Era	Period or Epoch	Group Formation	Lithology	Thickness (m)
M E S O Z O I C	Disconformity			
	Lower Cretaceous	Crowsnest Formation	Trachyte agglomerate, tuff, volcanic - rich sandstone; mudstone, conglomerate	28
	Lower Cretaceous May be younger		Trachyte, syenite, volcanic breccia.	
	Lower Cretaceous	Blairmore Group	Grey and greenish sandstone, arkosic sandstone, green and red mudstone; minor brown limestone.	100 - 208
	Disconformity			
	Jurassic and Cretaceous	Kootenay Formation	Dark grey, carbonaceous sandstone and conglomerate sandstone, siltstone, shale ; coal.	28 - 94
	Jurassic	Fernie Group	Grey calcareous shale, shaly limestone, silty limestone; dark grey shale, limestone; sandstone.	69
	Disconformity			
Triassic	Spray River Formation	Grey dolomitic siltstone and sandstone; brown siltstone and silty shale	17	



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*TABLE of FORMATIONS*  
*FIG. 4*

Dwn. by:	Date:
Chkd. by:	File no.:

## Geology

### **Regional Stratigraphy**

The Kootenay Formation of Upper Jurassic - Lower Cretaceous age is the coal - bearing sequence of south-eastern B.C. It is a thick sequence of clastic sediments representing delta progradation over marine shales, siltstone and sandstones of the Jurassic Fernie Formation.

(Figure No. 4)

Deposition was initiated by an epeirogenic uplift of the source area in early phases of the Columbian Orogeny in Late Jurassic time. The Kootenay section thickens from east to west; the source of sediments being southwest and the shoreline on the east and northeast. Its thickness within the Upper Elk Coal Field ranges up to 100..

The Kootenay Fm. can be subdivided into three main units. (Figure No. 5) A basal, cliff-forming "Moose Mountain Member" is composed predominately of sandstones and shales. It is a prograding sequence of delta front sheet sands, barrier bars and tidal channel deposits.


The middle "Coal - bearing Member" is generally in sharp contact with the underlying Moose Mountain sandstone. It consists of alternating beds of sandstone, shale, siltstone and coal representing prograding delta plain environments. The Coal - bearing Member is 245m - 860m thick, including 6m to 61m of coal in the south contained within two seams and up to 90m of coal in 23 seams on the north.

The upper portion of the Kootenay Fm., the "Elk Member", consists of alternating sandstone, siltstone, shale and conglomerates with minor lenticular coal beds. It represents progradation of the alluvial plain over the delta plain coal - forming environments.

The upper contact of the Kootenay is an erosional surface. It is overlain by the Cretaceous Blairmore Group, beginning with rejuvenated piedmont-plain deposits of the Cadomin Formation (Cadomin Conglomerate).

Only erosional remnants of the Kootenay Formation are preserved in the south of the Fording Syncline. A 10° north plunge on the syncline preserves an increasing thickness of

Norris 1959 Alberta		Newmarsh 1953 British Columbia		Jansa 1972 Alberta - B.C.		Gibson Alberta - B.C.	
Cadomin Fm.				Cadomin Fm.			
		Elk Formation	K O O T E N A Y Fm	Elk Member	K O O T E N A Y Fm	Pocaterre Mbr.	
						Elk Member	
K O O T E N A Y Fm.	Mutz Member	Kootenay Formation	K O O T E N A Y Fm	Coal Bearing Member	K O O T E N A Y Fm	Coal Bearing Member	
	Hillcrest Member						
	Adnac Member						
	Moose Mtn. Mbr	Moose Mtn Mbr	Moose Mtn. Mbr	Basal Sandstone Unit A _____ Unit B _____			
Fernie Fm.				Fernie Fm.			
<p>Nomenclature chart illustrating and comparing the main Kootenay and stratigraphically adjacent formations and members recognized.</p> <p>Figure no.</p>							

 <b>line creek resources ltd.</b>	
<i>KOOTENAY FORMATIONS</i>	
<b>FIG. 5</b>	
Drawn by:	Date:
Checked by:	File no.:

Kootenay section to the north. Faulting and folding has caused some repetitions of the section and thickening of the coal seams.

Shales are generally dark gray to black, slightly calcareous, lensey and thin. Two notable exceptions occur persistently at 12m and 16m below the top of the Moose Mountain Member. The thickness ranges from 0.2m to 1.0m and lithology varies from carbonaceous shale to bright coal. These beds appear as two slightly recessive layers in the Moose Mountain Member outcrops, especially noticeable along the west side of the ridge.

The lower contact of the Moose Mountain Member is transitional into Passage Beds (Ferne Formation) while the upper contact is generally sharp below the #10A seam of the Coal-bearing Member.

The middle Coal-bearing Member is an interbedded sequence of shale siltstones, sandstones and coal.

Shales range from carbonaceous to silty and dark gray to black in color. Thin laminae of siltstone and coaly stringers of wisps are common throughout the section. In road cuts (constructed between 1968 and 1971) the carbonaceous shales are almost completely sloughed over whereas the silty shales are often still partially exposed.

Siltstones are interbedded with shales and sandstones or occur in transition from one to the other. Roadcut occurrences are often still well exposed.

Sandstones are fine - to medium grained and tend to become coarser down section. Laminar bedding, crossbedding and soft sediment deformation are seen throughout. The lower 75m of the Coal-bearing Member (below #8 seam) has a higher proportion of thick, persistent sandstone units, some of which are easily correlated in drill holes. Above #8 seam, sandstones in the Coal-bearing Member are less common, thinner, and more variable. Their upper and lower contacts tend to be gradational, compared with the relatively sharp sandstone contacts below #8 seam. Petrographic analysis of the cliff-forming quartzite between #8 and #9 seams (G. Wilson, 1976) is as follows:

Quartz & Chert	73%
Cement - Silica	20%
Matrix	7%
Accessory Minerals	<u>Trace</u>
	100%

Coal seams are numbered from the top #1, #2, #3, #4, #5, #6, #7, #8, #9, #10B, #10A, with 45% of the coal thickness occurring in the lower four seams. The main mineable seams are:

- #4, two coal seams separated by a shale parting

Average thickness is 8.0 m.

- #6, two coal seams separated by a shale parting which ranges in thickness from zero to 13.0 m.

Average thickness is 2.4 m.

- #7, maintains a regular thickness of about 6.0 m.

- #8, is the thickest seam, averaging 12.5 m. Its stratigraphic and geophysical characteristics are very consistent. Thickness variations are probably due to structural disturbances ( faulting and / or folding ).

- #9, maintains a regular thickness (average 4,5 m) except where faulted. Its upper contact is interbedded carbonaceous shale and shaly coal and is therefore not as sharp as the basal contact.

- #10A, maintains a regular thickness (average 2.8 m). Its basal contact is often a sandy coal or coaly sandstone.

### **Regional Structure**

The Coal-bearing Kootenay Formation occurrences of southeastern B.C. are preserved in north - south trending synclines referred to as the East Kootenay Coalfields. High structural relief of Paleozoic rocks surrounding the coalfields fades out in relatively incompetent rocks of the Fernie and Kootenay formations. The structure within the syncline is complicated to varying

degrees by thrust faults and their associated folds, and also by normal faults. The complexity of this structure increases towards the thinner, east side of the coalfields where they have been thrust against the underlying Paleozoics.

The East Kootenay Coalfields can be subdivided into three coal-bearing areas. From south to north they are the Flathead Coalfield, the Fernie Coalfield and the Upper Elk Coalfield. Since they are all part of the same depositional complex, the subdivision is based on erosional boundaries and structural boundaries. (Figure No. 6, found in pocket)

### **Upper Elk Coalfield**

The Upper Elk Coalfield is an elongated basin composed of two major synclines (Greenhills and Fording) separated by an anticline and the northern extension of the Erickson normal fault. The eastern, Fording syncline, can be traced northwards from Alexander Creek to the Kananaskis Lakes. At its south end, it is symmetric with moderate to steep dips on both limbs. To the north it becomes more asymmetric with a west dipping axial plane, vertical strata on the west limb and moderately dipping strata on the east limb.

On the west side of the Erickson Fault, the Greenhills syncline has been downthrown approximately 900 m. It can be traced up the Elk River Valley from Fording Mountain to where it is cut off by the Elk River Thrust. The Greenhills Syncline is slightly asymmetric with a west dipping axial plane.

### **Structure Saddle (Ewin Pass) Area**

In the Saddle (Ewin Pass) Area we have the benefit of results from 9 drill holes to give us a better understanding of the dip and nature of the coal seams.

In this area there is strong evidence for faulting along the trend of the synclinal axis. The sudden change in magnitude of the dip of the strata on the east limb from the horizontal to approximately 65° in a few tens of metres indicates that the fault continues northwards along the axial fold line.

The Fording River thrust fault is present in the North Central Block and is mapped from the southernmost portion of Mt. Michael into the Saddle (Ewin Pass) sector. The dip of the beds in the east limb of the syncline generally decrease as one moves from the south to the north. In the Saddle (Ewin Pass) sector the measurement of dip ranges from 30° - 40° W. The dip of the coal seams in this area are almost coincident with the slope of the ground, presenting an advantageous situation for an open pit mining operation.

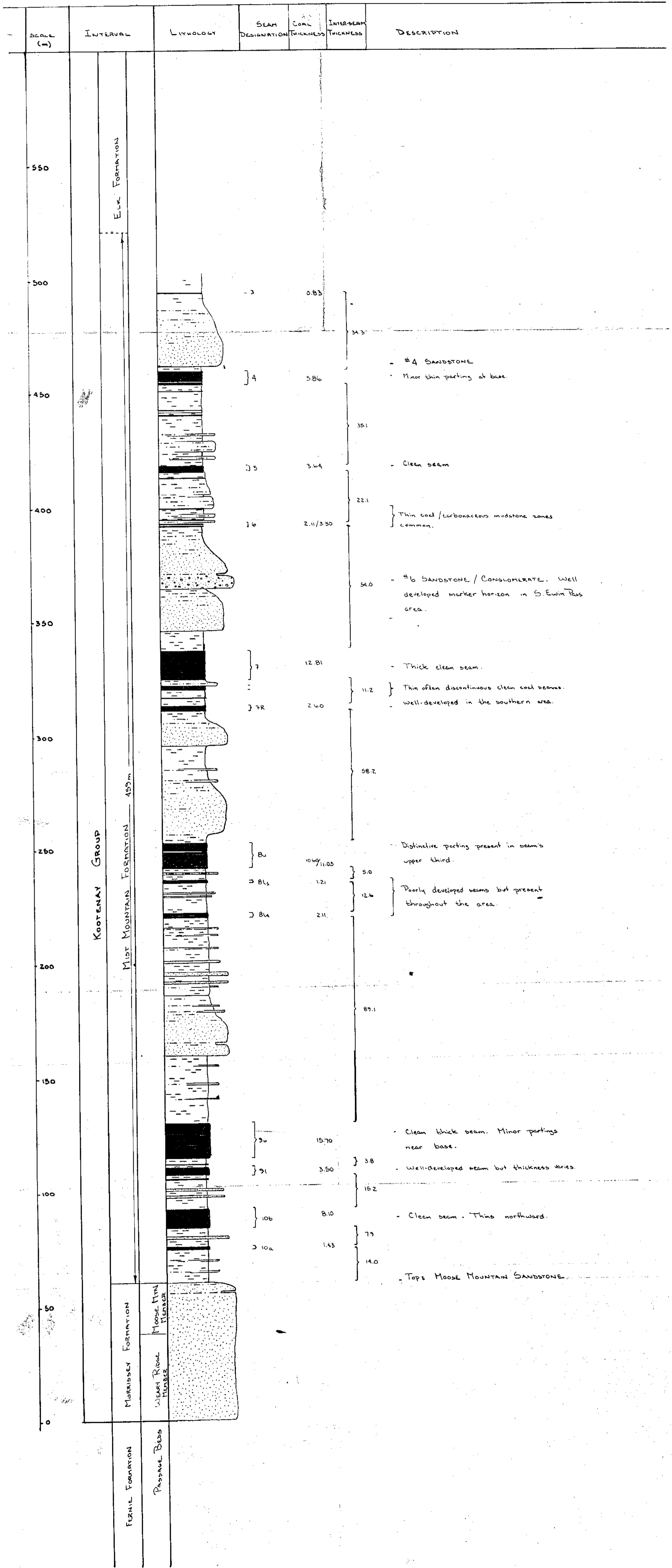
Thrust faulting along bedding planes has resulted in a marked thickening and repetition of coal seams. In the Saddle (Ewin Pass) sector the #8 seam displays an increase in thickness indicative of fault action. The remainder of this block contains nine seams with a thickness greater than 1.5 m. The aggregate thickness is 51.8 m. These figures, (CNI's) do not include the 10B and 10A seams. The inclusion of these seams may raise the aggregate thickness to 59m.

Seams no. 5, 6, 7, 8, 9, 10B, and 10A extend northwards from the area drilled by CNI Ltd., and increases the possibility of extending the mineable area in that direction. This block deserves further detailed exploration and mapping.

STRATIGRAPHIC SECTION

EWIN PASS SOUTH (N 400 N / 500 W)

Scale: 1:10,000 1,000

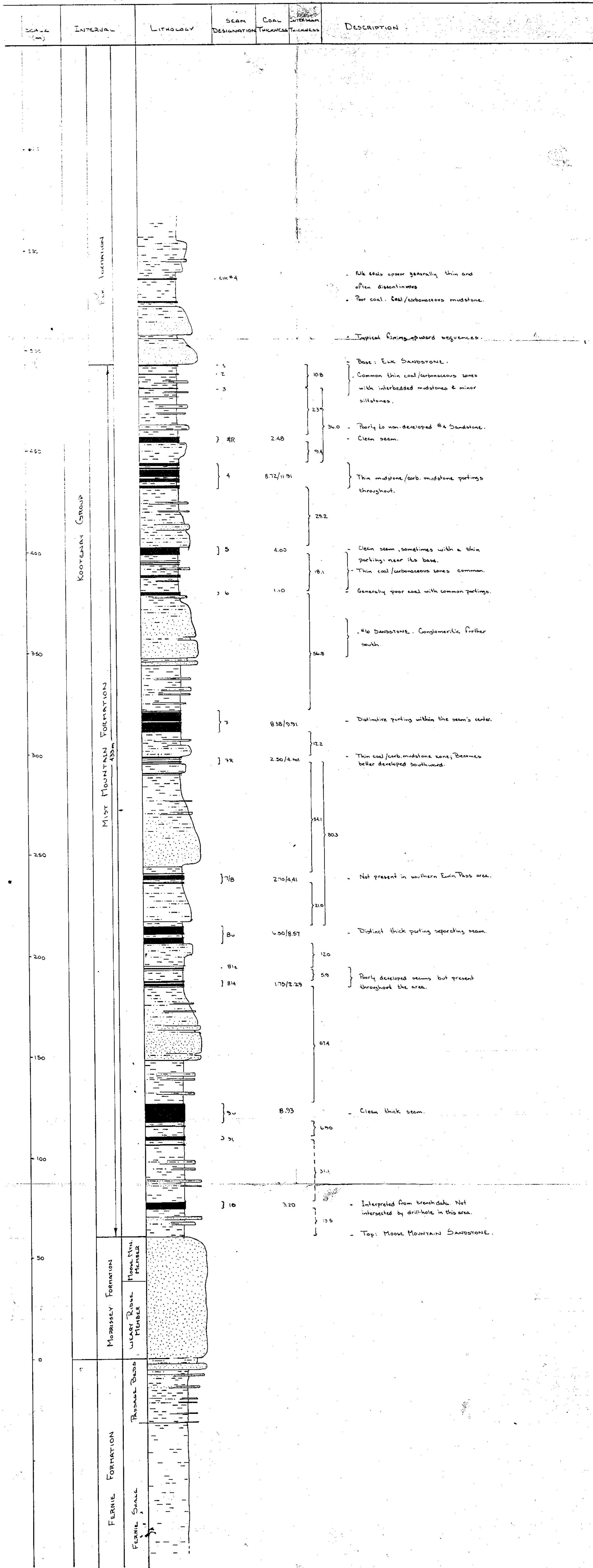




STRATIGRAPHIC SECTION

ELWIN PASS - CENTRAL (N 2200 N / 500 W)

SCALE: 1:100000 1:200



## INTRODUCTION:

This report presents the results of a surface geophysical program that was carried out in the Saddle Area, at the Line Creek Mine in August, 1993. The geophysical technique used was Horizontal Loop Electro-Magnetics (HLEM). Data Acquisition, processing and interpretation was carried out by LCRL and Manalta personnel. The objective of the program was to assist in the structural mapping of the area.

## THEORY:

Electro-Magnetic surveys respond to contrasts in conductivity within the subsurface. Geological structures such as faults, fractures, fold axis, etc. will generally have a higher iron oxide and moisture content, and perhaps more clay minerals than the surrounding rock. This will result in a relatively higher conductivity for that zone and will yield a definitive geophysical response.

Basic EM theory states that if an alternating dipole magnetic field (produced by an AC current flowing in a wire coil transmitter) is introduced to the subsurface it will create or induce a secondary dipole alternating magnetic field around any conductive zone within range. HLEM equipment consists of a transmitter; emitting a fixed primary magnetic field, having a specific frequency, phase, amplitude and intensity. And a receiver which detects the combined primary and secondary fields. The transmitter/receiver pair are connected by a reference cable (60m in this survey) which serves as a communication link and as a means of keeping a constant distance between the transmitter and receiver. The strongest response occurs when the conductor is at the midpoint of the cable. As stated before the receiver detects the combined primary and secondary fields, however the data is more useful if the secondary field can be plotted by itself. Therefore the receiver applies a compensating signal, which is equal to the primary signal but 180 degrees out of phase, to the combined detected signal. The receiver now displays only the secondary field, this field is separated into two components the quadrature (out-of-phase) and the real (in-phase). A phase shift of 90 (quadrature) to 180 degrees (real) occurs to the secondary field, relative to the phase of the primary field. An excellent conductor will produce a secondary field consisting of only a real component. The majority of conductors will produce a field with both components. Close analysis and

modelling of this two component data will define conductor characteristics such as dip of conductor, depth to conductor, and conductivity. The magnitude of the data is shown as a percent of the primary field intensity. Erroneous signals such as those produced from topography, incorrect coil orientations and spacing effect the real component only.

#### DATA ACQUISITIONS AND LOGISTICS:

There were 7 lines that were geophysically surveyed. The lines had an azimuth of 103/283 they were located 400m apart and ranged in length from 980m to 2160m. Cumulative line distance was 11.3km. Each line was characterised by steep-rough topography with slopes often reaching 35-40 degrees.

Due to poor road access endpoints of each line were located and surveyed using helicopter support. Lines were then slashed by a local contractor at a rate of 450m/manday. Stations were then located every 20m thru the length of the line, a piece of flagging every 20m and a short stake every 100m was used for station identification. The slope angle between each station was also measured, this angle was used for applying topographic corrections to the data. Station spacing preceded at the rate of 1.4 km/manday. Geophysical data was acquired at 3 different primary field frequencies; 56,320hz, 14080hz, 1760hz. It took approx. 30sec. to obtaining the secondary field data at each station, data acquisition occurred at the rate of 1.13 km /manday.

The UTM coordinates for the endpoints of each line are listed below:

LINE	EAST END POINT(m)	WEST END POINT(m)
L400N	5539380N 661080E	5539580N 660145E
L800N	5539765N 661225E	5540070N 659800E

○ L1200N	5540165N 661268E	5540457N 659885E
L1600N	5540580N 661235E	5540875N 659865E
L2000N	5540960N (put in by hipchain) 661370E	5541340N 659615E
L2400N	5541340N 661508E	5541765N 659545E
○ L2800N	5541780N 661365E	5542140N 659680E

When L2800N was being chained a large cliff was encountered near the valley bottom at station 1240, the line was broken and restarted at the top of the cliff. The second half of L2800N went from station 1260 to 1780, it was stopped approx. 70m short of the west end point because of the large cliffs near the top of the west ridge. Due to the breakage in the line survey control in the second half of L2800N became very poor. The Motorola Global Positioning System (GPS) was used successfully to help establish this control.

#### INTERPRETATION:

○ Interpretation was relatively straightforward on each line. Response lows on both the quadrature and real components indicated the prescense of a conductor. The magnitude of the response was a function of the type of conductor and amount of overburden present. Since

the real component is effected by slight variations in coil orientation and spacing the real-profile was "noisy" therefore the quadrature component was used almost exclusively for conductor location. Conductor characteristics such as dip, depth, and conductivity could not be determined since these computations require "clean" real and quadrature profile. Appendix 3 shows typical real and quadrature profiles over conductors in a laboratory and in a real environment. Appendix 1 shows the anomalies that occurred on each line. Field investigations were made to every anomaly that fell at or near an outcrop to determine the exact cause of the anomaly.

Flowing subsurface water at L800N, stn. 1450 gave an excellent response as did a flowing peizometer hole at L800N, stn. 470. A large positive response occurs at L1200N, stn. 810 this is in the middle of a large land slide, and the anomaly may be due to water "pockets" within the slide or the overburden being conductive. The Elk Sandstone horizon gave an anomalous response on every line it crossed, with the exception of L400N. This horizon is yielding a response either because it is acting as a retardent to water flow or due to a higher iron content. Field mapping showed this sandstone to be highly oxidized and bright yellow in colour. Coal seams that outcropped on the west limb of the Ewin Syncline on L2800N, stns. 910 and 970 showed a weak response, these were the only coal seams that were interpreted with a relatively high degree of confidence. Two weak signals on L2000N, stns. 1580 and 1690 may also have been caused by coal seams.

Outcrops that showed signs of faulting were located at: L400N, stn. 850; L800N, stns. 1210 and 1340; L1200N, stns. 950; L2800, stn. 1620 and 1370. At L2800N, stn. 620 the bedding was observed to be near horizontal, this is the approximate location of the Ewin Syncline fold axis. All of these locations gave strong geophysical responses. Every anomaly including those listed above are plotted (Appendix II.)

After plotting the anomalies onto the geological map an attempt was made to correlate between the lines. This correlations was difficult for several reasons; signals that occurred along the

conductor did not always match, this is more than likely due to the depth and nature of the overburden varying along the strike of the conductor. A line spacing of 400m is too large for confident correlations. After filtering out signals that were that were due to groundwater and lithological units, faults and fold axis were correlated from line to line. The Ewin Syncline and Anticline were traced for the entire length of the survey, as was the Ewin Anticline Thrust Fault. A high degree of confidence is attached to the location of these three structures.

The Ewin Thrust Fault showed on L2400N and L2800N but then it trends too far west to be picked up on the more southern lines. Two other prominent structures also showed on L800N thru to L2800N between the Ewin Anticline and the Ewin Anticline Thrust Fault.

The east portion of the valley shows a peculiar lack of anomalies. Anomalies that do occur are weak and questionable. In the author's opinion this is because of the dip slope geology on the east side. Bedding and structures are intersecting the topography at a very low angle, whereas on the west side this intersection is near perpendicular.

The reader must keep in mind that this interpretation has been based on a reconnaissance geophysical program. Infill lines are needed for a more confident interpretation of the weaker conductors.

#### CONCLUSIONS AND RECOMMENDATIONS:

The Horizontal Loop Electro-Magnetic method has been field proven to delineate conductive zones within the subsurface. These zones may be groundwater, lithological units, faults, fractures, and fold axis. Careful field investigations should be made after each profile has been interpreted, to filter out erroneous signals. It is highly recommended that a surface geophysics program be carried out after comprehensive field mapping has been done, field mapping data is

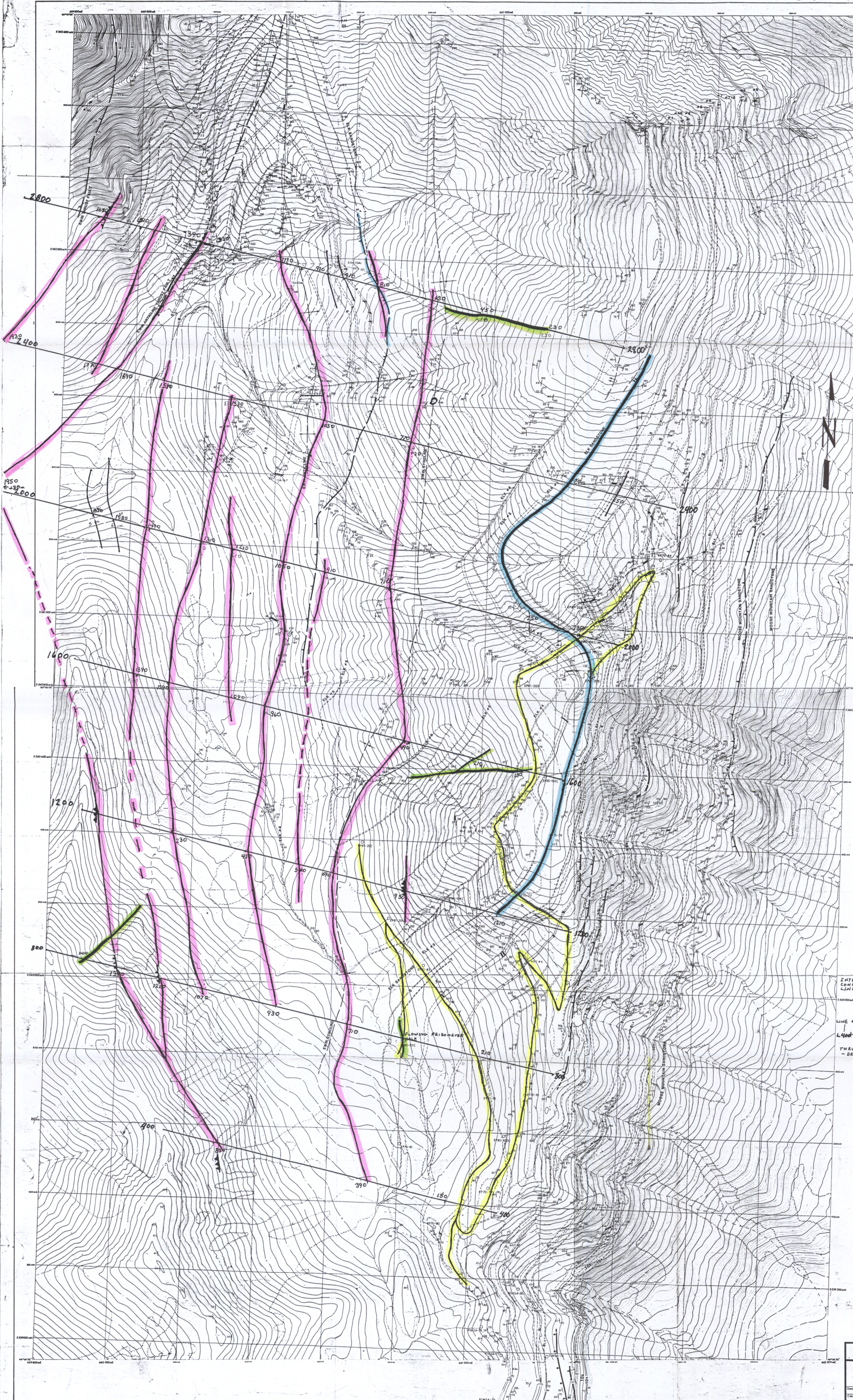
near mandatory to do a proper interpretation of geophysical data. Grid layout should be designed to fill in "holes" which appear to exist in the structural model. Tight grids (100m line spacing, and 10m stations spacing) over shorter areas will yield a more confident interpretation.

#### ACKNOWLEDGEMENTS;

Doug Walilko – Manalta Coal Ltd.

Gordon Zurowski – Line Creek Resources Ltd.

Terry Stickney – Line Creek Resources Ltd.



**LEGEND**

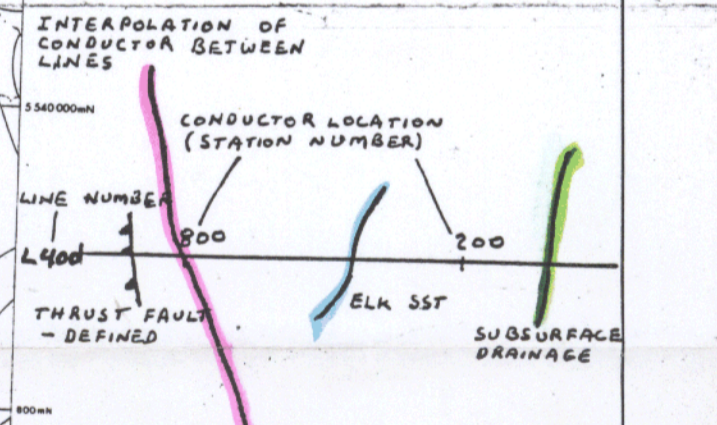
- DRILL HOLE WITH DIRECTIONAL DEVIATION PROJECTION
- COAL SEAM - DEFINED
- COAL SEAM - APPROXIMATE
- COAL SEAM - ASSUMED
- THRUST FAULT - DEFINED
- THRUST FAULT - APPROXIMATE/INTERPRETED
- NORMAL FAULT - DEFINED
- NORMAL FAULT - APPROXIMATE/INTERPRETED
- ANTICLINE
- ANTICLINE - OVERTURNED
- SYNCLINE
- SYNCLINE - OVERTURNED
- BEDDING ATTITUDE - OVERTURNED
- TRENCH
- ADIT WITH PROJECTION FROM ENTRY
- CONGLOMERATE
- SANDSTONE
- COAL
- 3.55/4.85 TRUE THICKNESS: COAL / ROCK
- 7.11 TRUE THICKNESS: COAL ONLY

SCALE 1:2 000  
 CONTOUR INTERVAL: 2 METRES  
 DATE OF PHOTOGRAPHY: JUNE/JULY 1978

**line creek resources ltd.**

**LEGEND**

- DRILLHOLE WITH DIRECTIONAL DEVIATION PROJECTION
- COAL SEAM - DEFINED
- COAL SEAM - APPROXIMATE
- COAL SEAM - ASSUMED
- THRUST FAULT - DEFINED
- THRUST FAULT - APPROXIMATE/INTERPRETED
- NORMAL FAULT - DEFINED
- NORMAL FAULT - APPROXIMATE/INTERPRETED
- ANTICLINE
- ANTICLINE - OVERTURNED
- SYNCLINE
- SYNCLINE - OVERTURNED
- BEDDING ATTITUDE - OVERTURNED
- TRENCH
- ADIT WITH PROJECTION FROM ENTRY
- CONGLOMERATE
- SANDSTONE
- COAL
- 3.55/4.85 TRUE THICKNESS: COAL / ROCK
- 7.11 TRUE THICKNESS: COAL ONLY
- MAIN ROAD



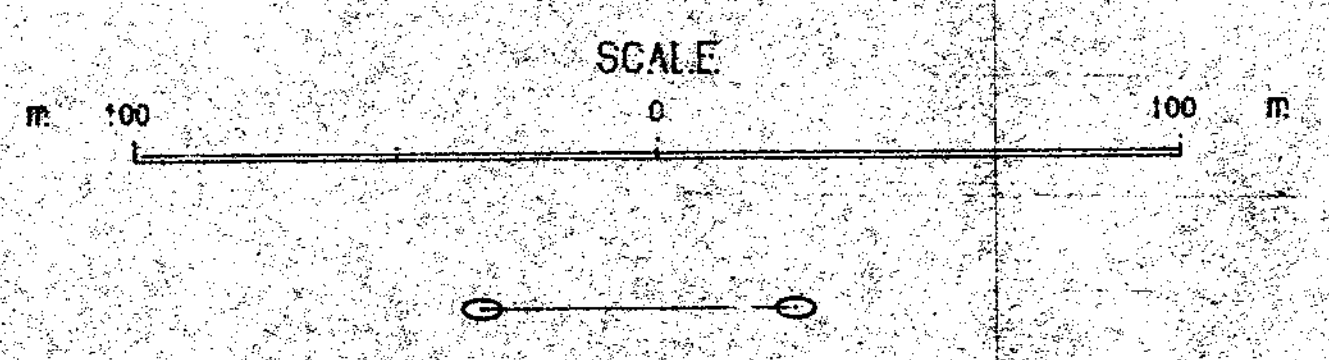
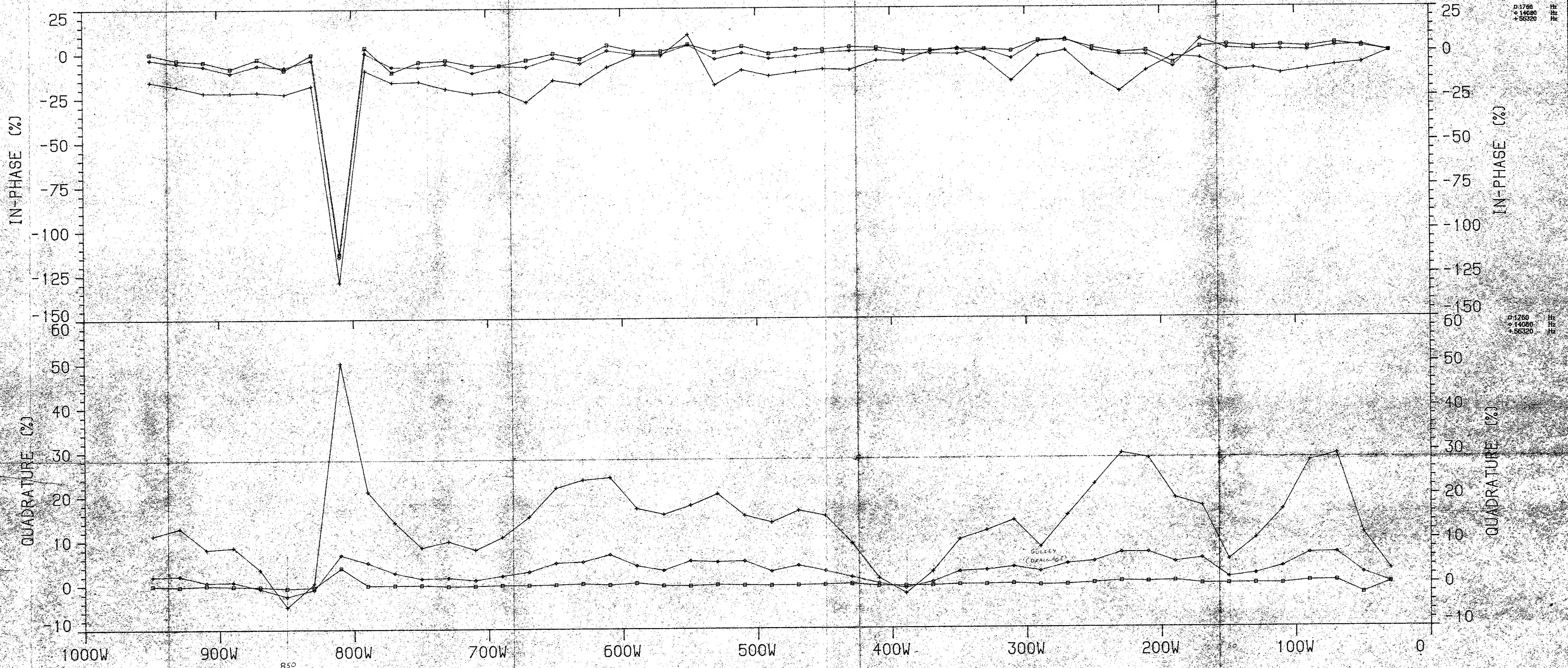
SCALE 1:5 000  
 CONTOUR INTERVAL: 2 METRES  
 DATE OF PHOTOGRAPHY: JUNE/JULY 1978

**line creek resources ltd.**

**HLEM SURVEY**

Drawn by: M.L.E. Date: AUG. 1983  
 Check by: A.L. File no.: 21772



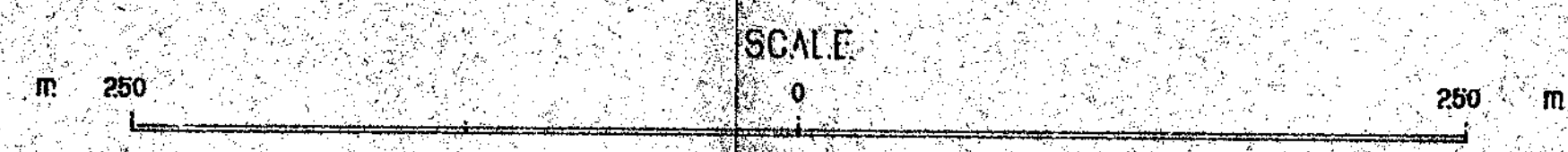
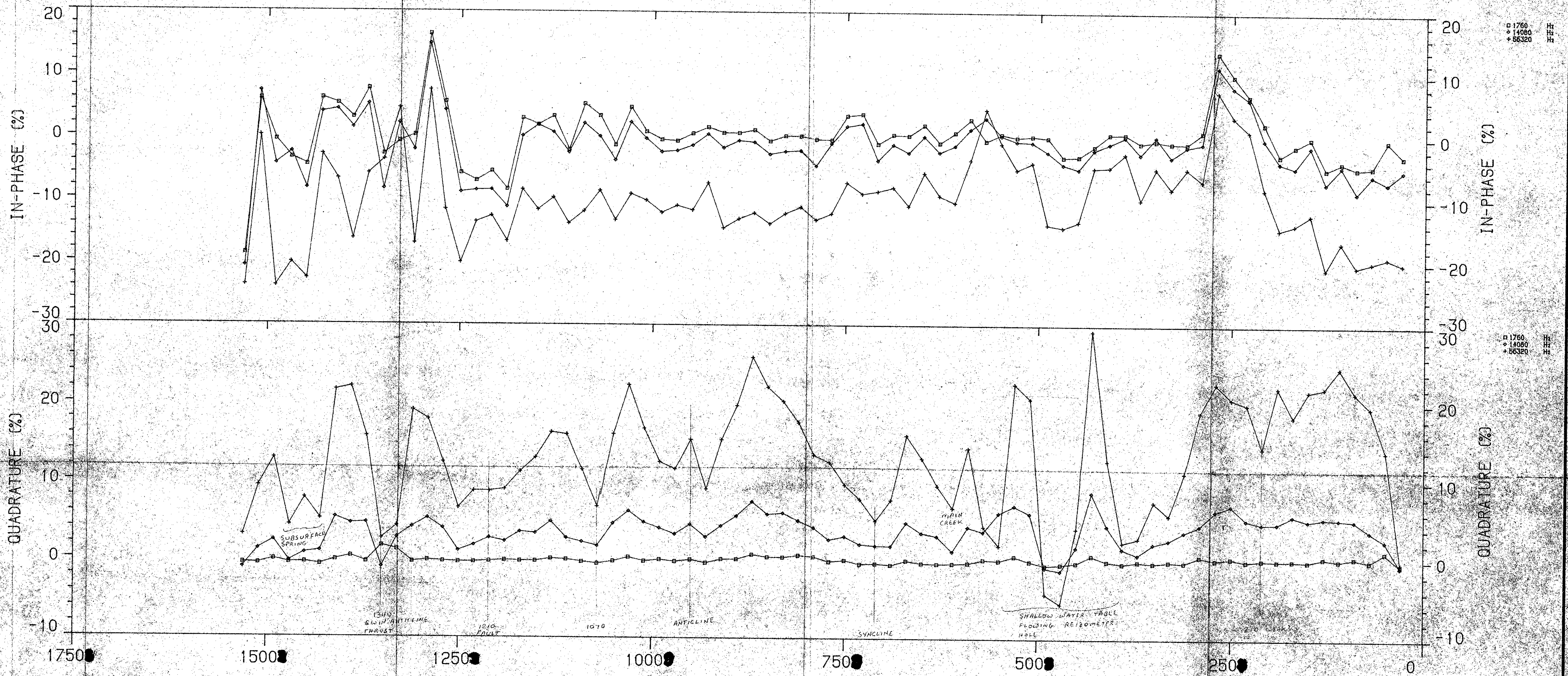


SCALE = 1:1456

for: LINE CREEK RESOURCES LTD.	
by: Line Creek Resources Ltd.	
Data Set: L400B	Date: AUG. 1993
Equipment: MAXMIN EQUIPME	Sounding: 400N

HELM SURVEY  
 SADDLE EXPLORATION AREA  
 S.E. BRITISH COLUMBIA  
 Azimuth: 103/283

LINE 400N

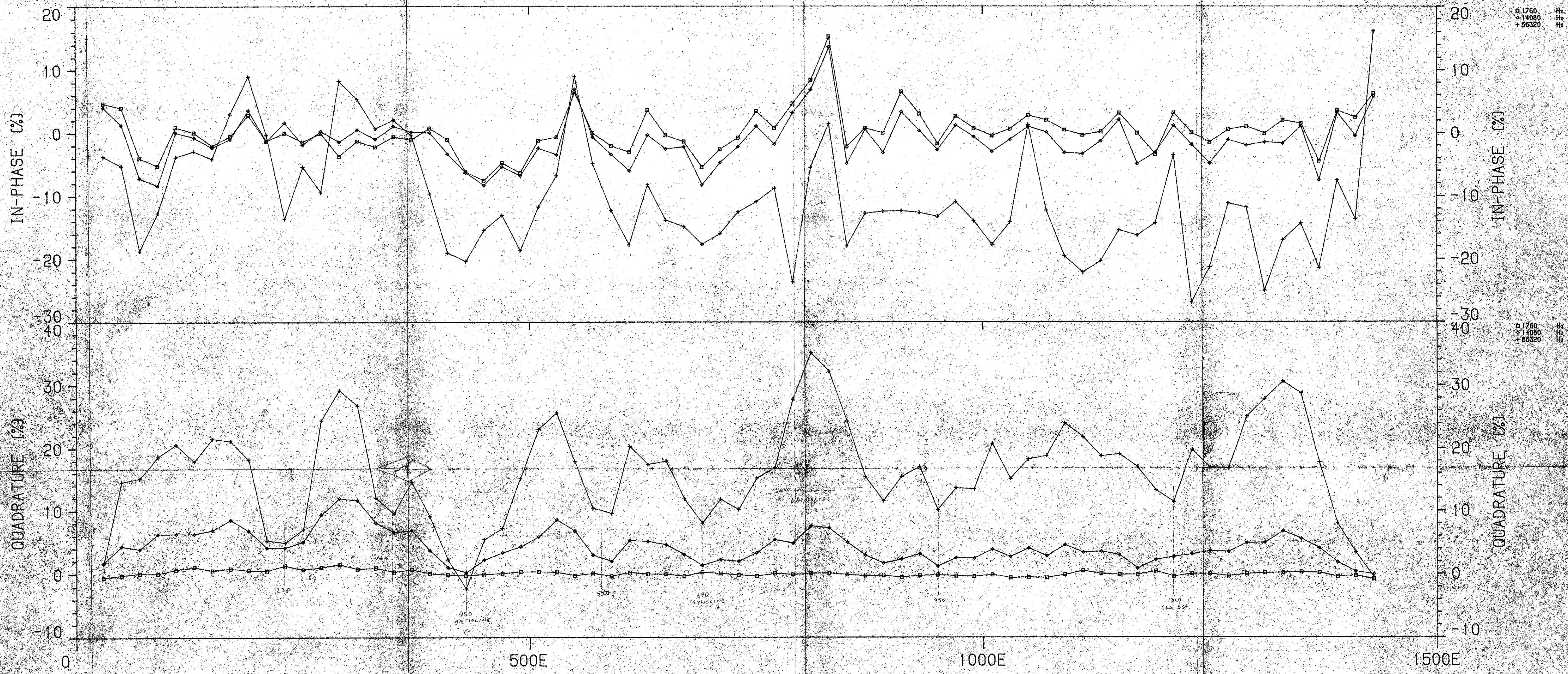


SCALE

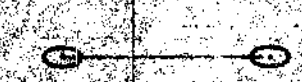
SCALE = 1:2000

for: LINE CREEK RESOURCES LTD.		HLEM SURVEY	
by: Line Creek Resources Ltd.		SADDLE EXPLORATION AREA	
Data Set: L810B	Date: AUG., 1993	SOUTHEAST B.C.	
Equipment: APEX MAXMIN	Sounding: 800N	Azimuth: 103/283	

LINE 800N



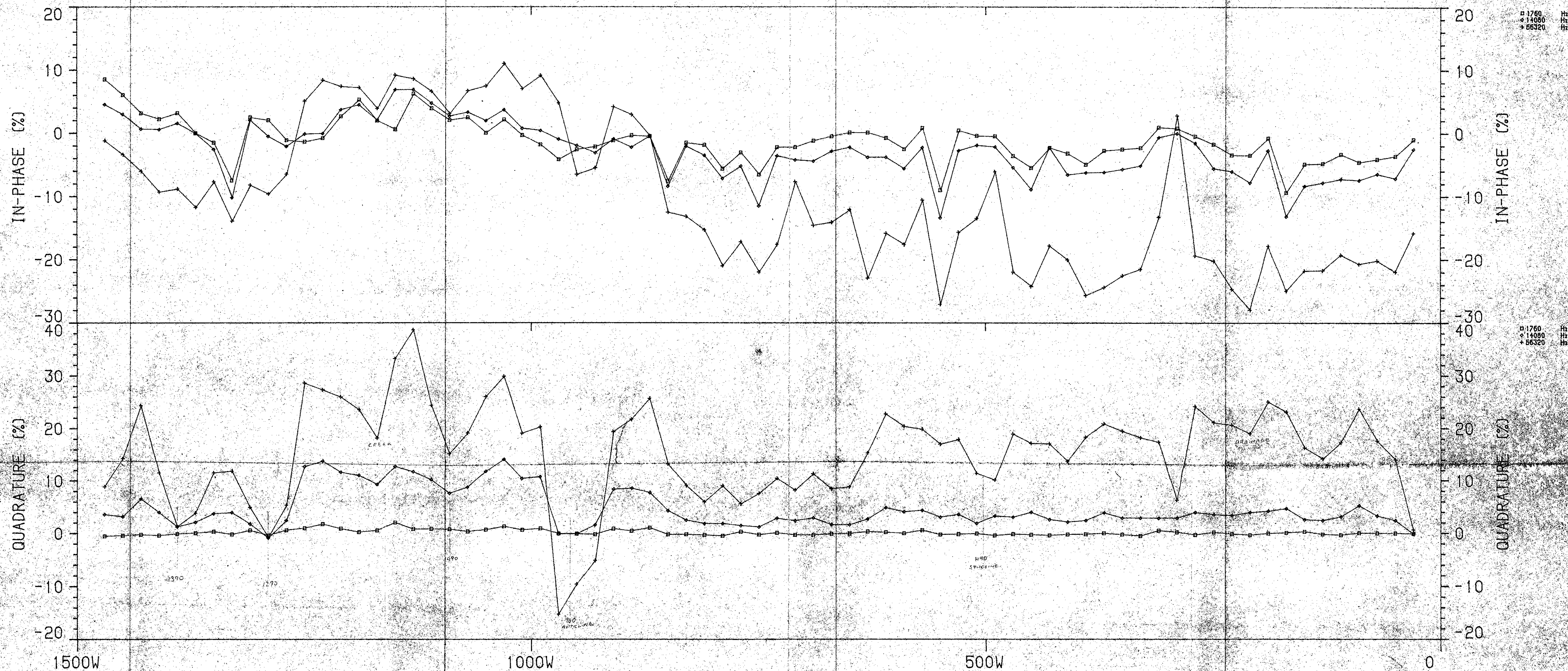
SCALE  
0  
1



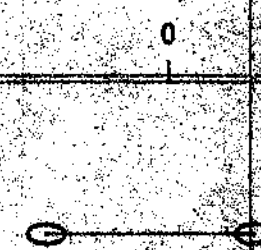
SCALE = 1:2167

for: LINE CREEK RESOURCES LTD.	
by: Line Creek Resources Ltd.	
Data Set: L1200	Date: AUG. 1993
Equipment: MAXMIN EQUIPME	Sounding: 1200N

LINE 1200N
HLEM SURVEY
SADDLE EXPLORATION AREA S.E. BRITISH COLUMBIA
Azimuth: 103/283



SCALE

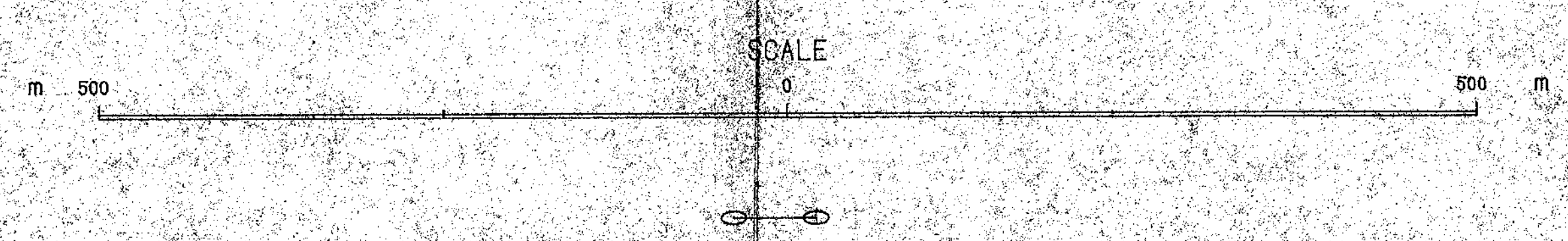
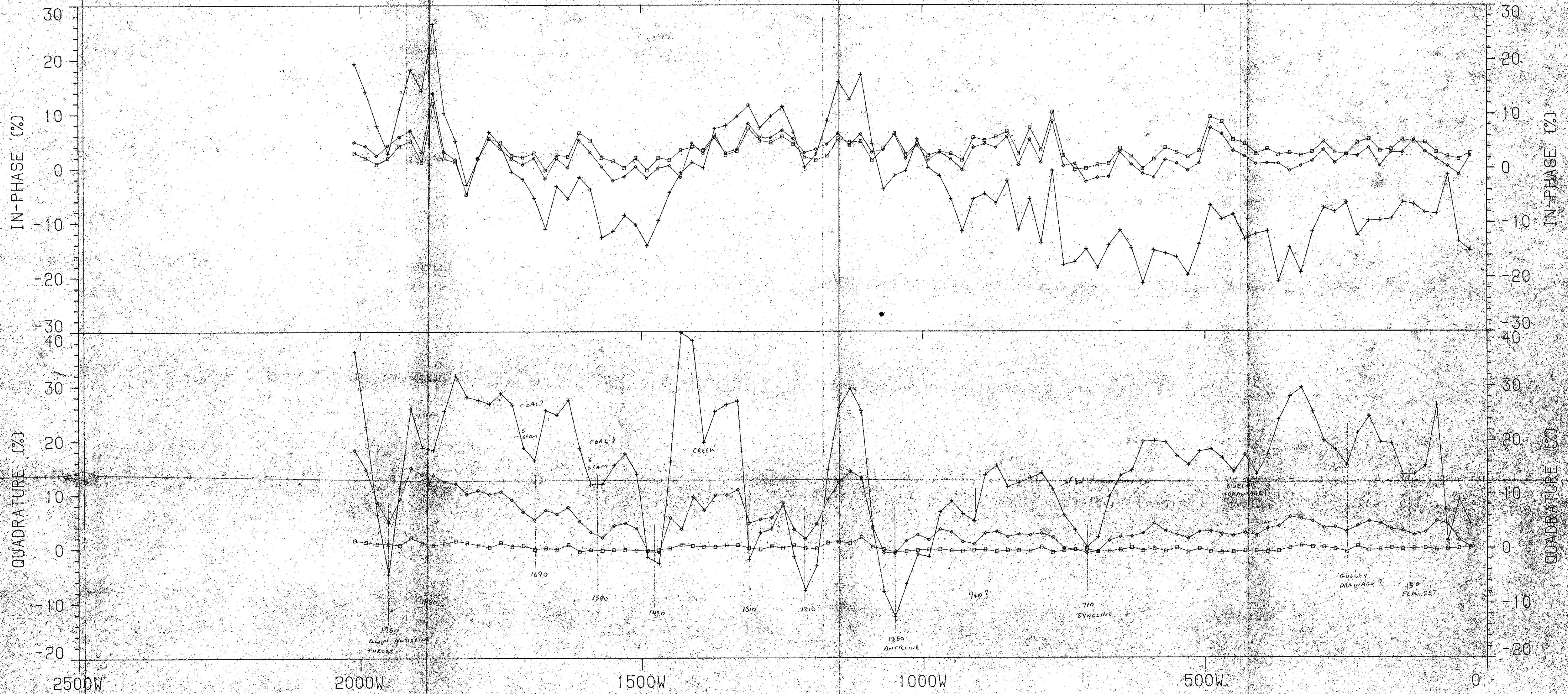


SCALE = 1:2107

for: LINE CREEK RESOURCES LTD.	
by: Line Creek Resources Ltd.	
Data Set: 16000	Date: AUG. 1993
Equipment: MAXMIN EQUIPME	Sounding: 1600N

HLEM SURVEY
SADDLE EXPLORATION AREA
S.E. BRITISH COLUMBIA
Azimuth: 103/283

LINE 100N

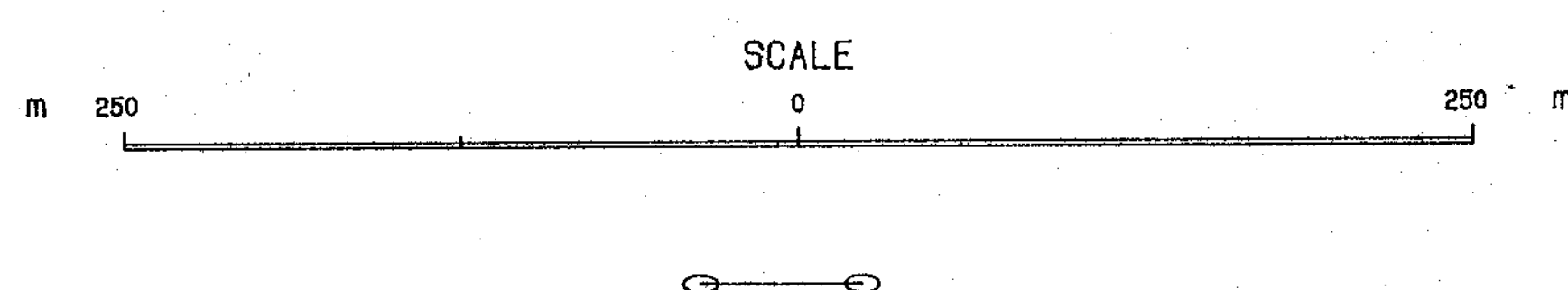
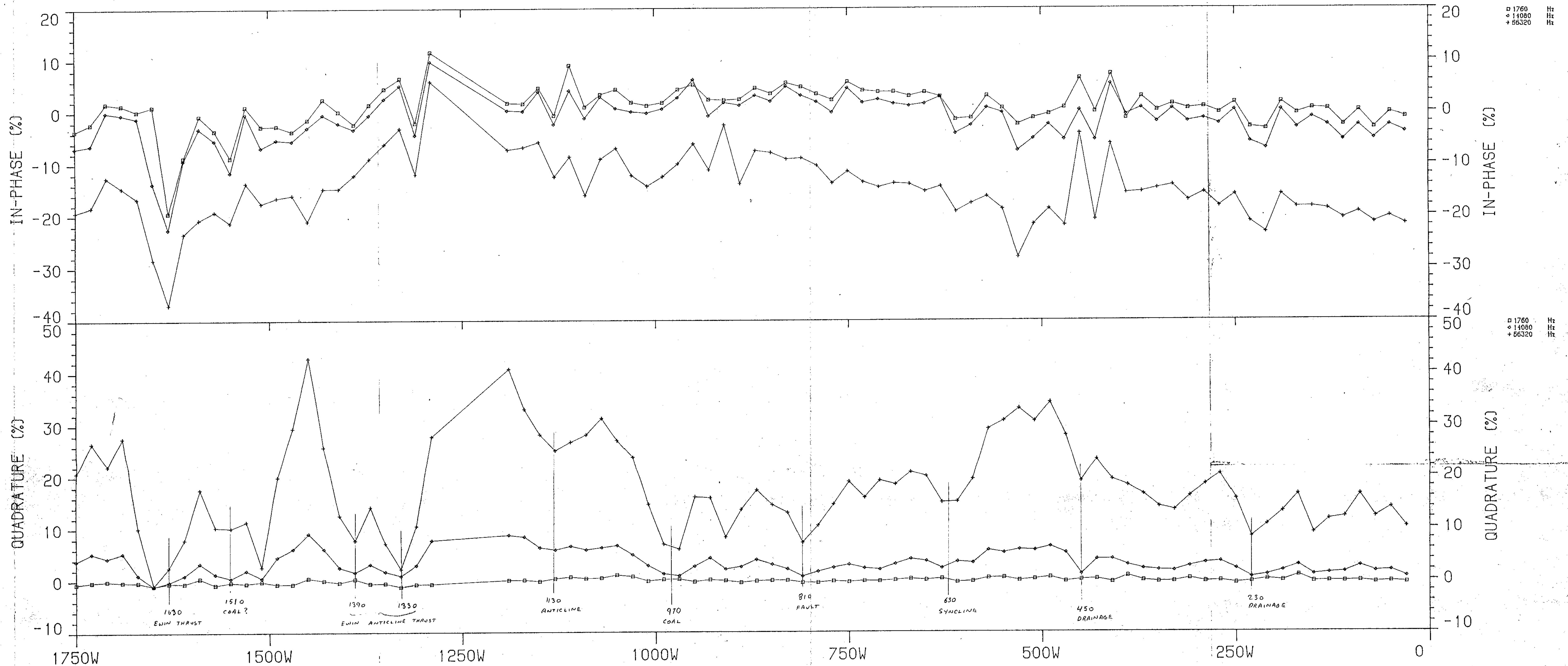


SCALE = 1:3645

for: LINE CREEK RESOURCES LTD.	
by: Line Creek Resources Ltd.	
Data Set: L2000	Date: AUG. 1993
Equipment: MAXMIN EQUIPME	Sounding: 2000N

HELM SURVEY	
SADDLE EXPLORATION AREA	
S.E. BRITISH COLUMBIA	
Azimuth: 103/283	

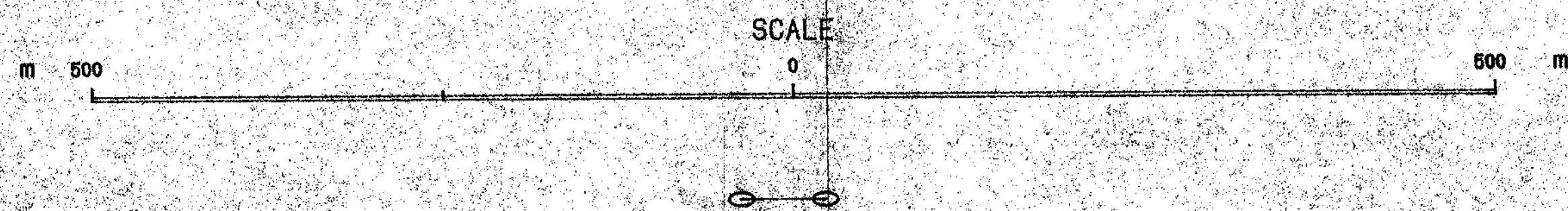
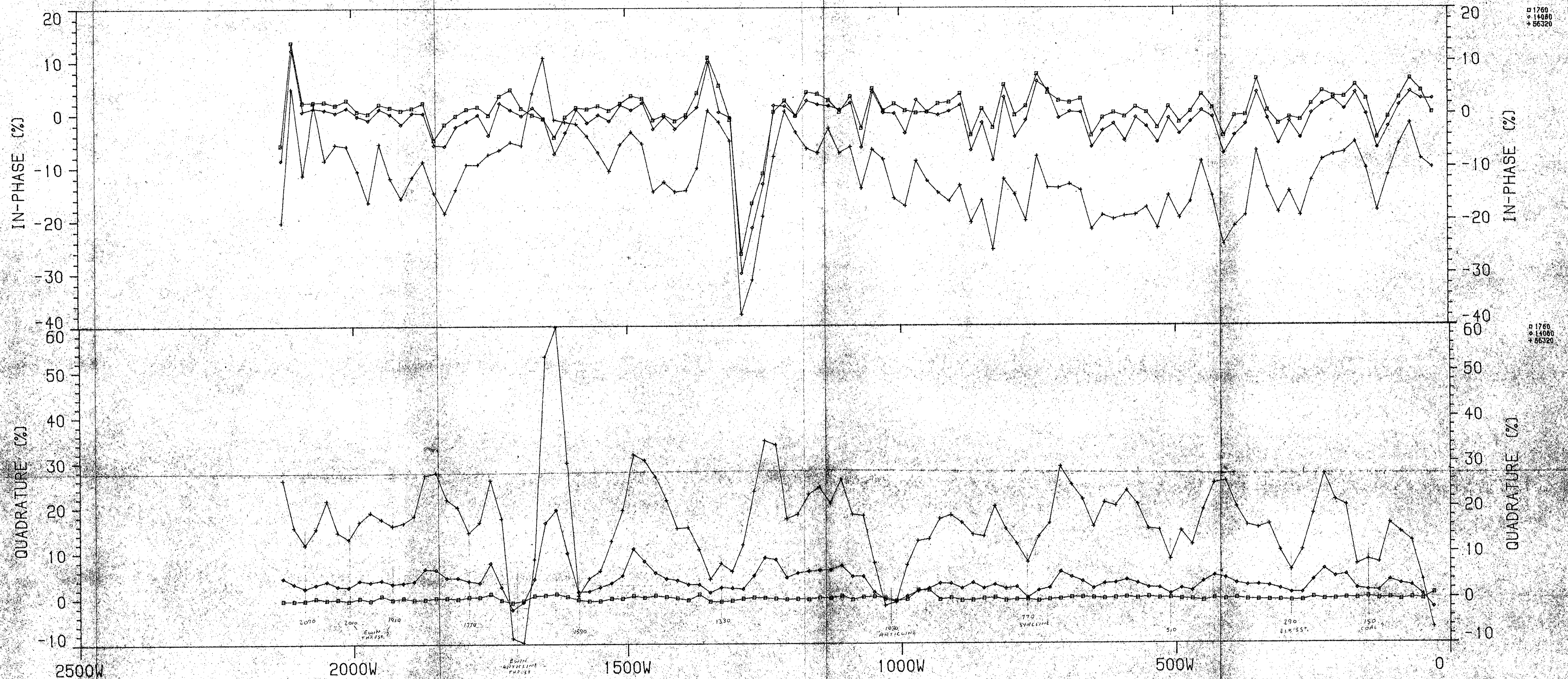
LINE  
CON



SCALE = 1: 2552

for: LINE CREEK RESOURCES		HLEM SURVEY SADDLE AREA EXPLORATION S.E. BRITISH COLUMBIA Azimuth: 103/283
by: Line Creek Resources Ltd.		
Data Set: L2800	Date: AUG. 1993	
Equipment: MAXMIN EQUIPME	Sounding: 2800N	

LINE  
2800N



SCALE = 1:3645

for: LINE CREEK RESOURCES LTD.

by: Line Creek Resources Ltd.

Data Set: L2400

Date: AUG. 1993

Equipment: MAXMIN-EQUIPME

Sounding: 2400N

HLEM SURVEY

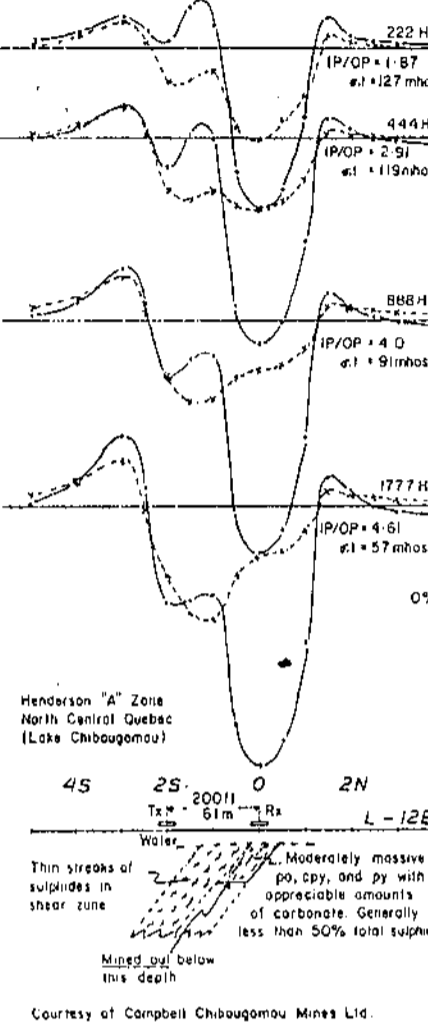
SADDLE EXPLORATION AREA  
S.E. BRITISH COLUMBIA

Azimuth: 103/283

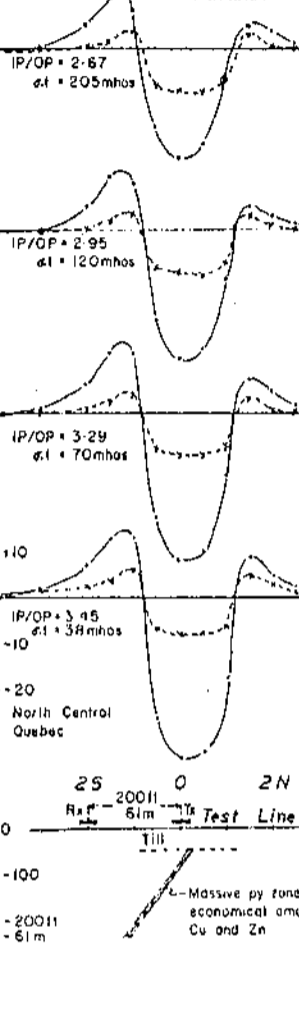
LINE  
2400N

# CONDUCTIVITY-THICKNESS STUDIES OF MASSIVE SULPHIDE BODIES

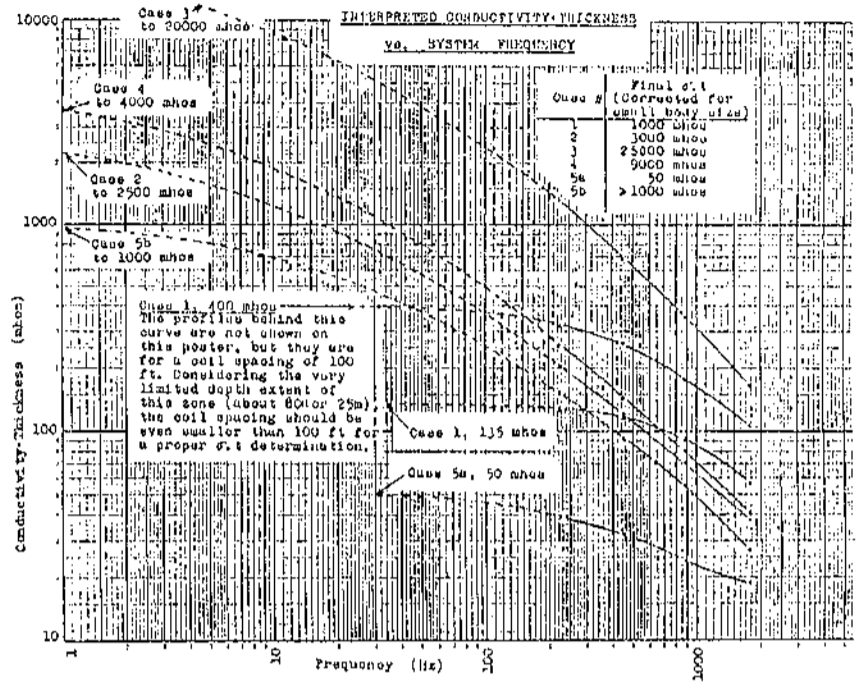
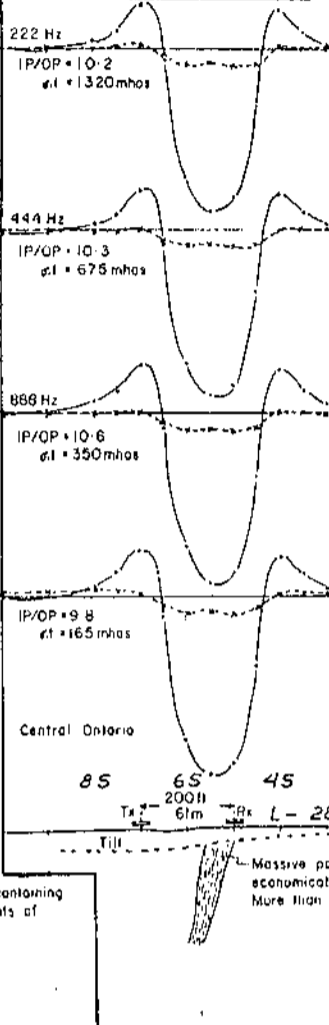
**CASE 1 - SHEAR ZONE REPLACEMENT**  
Cu-Zn OREBODY



**CASE 2 - VOLCANOGENIC**  
Cu-Zn OREBODY

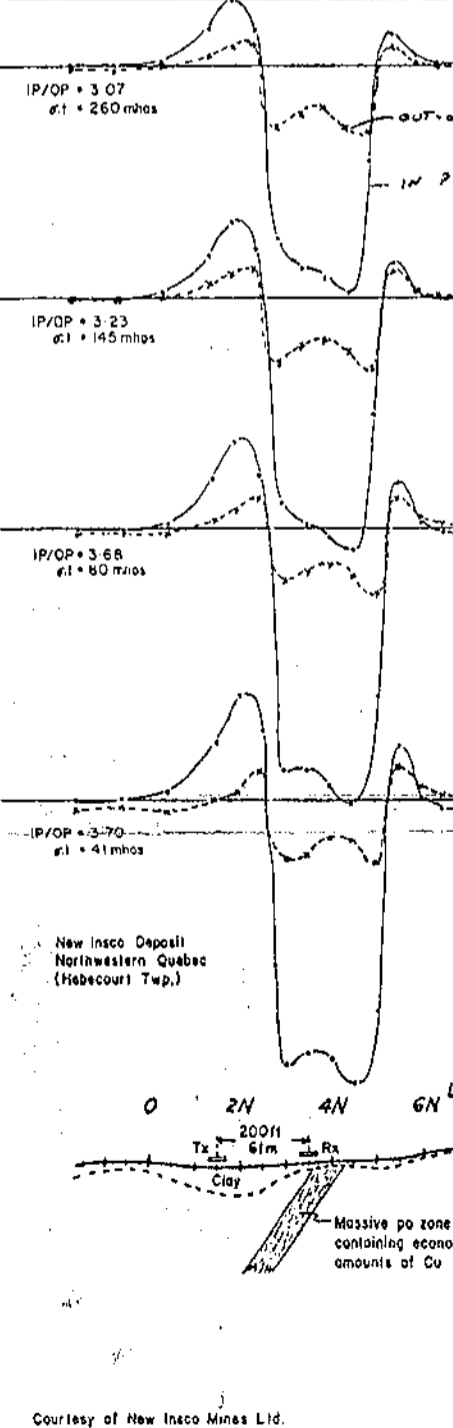


**CASE 3 - BASIC INTRUSIVE**  
Cu-Ni OREBODY

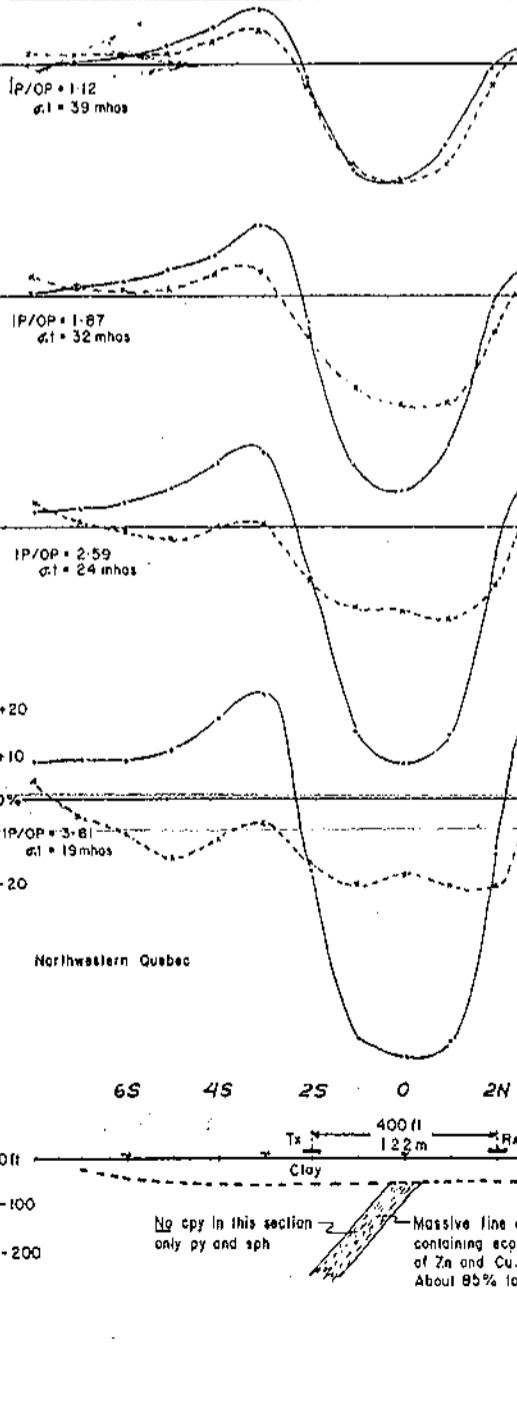


Note: The conductivity thickness ( $\rho_t$ ) determinations are made from curves derived from laboratory scaled modeling on "inductively thin" conductive dikes in an infinitely resistive environment (free space). In nature, effects known as "current gathering" and "thickness" cause the  $\rho_t$  determination to be too small, when using interpretive curves derived from thin dike modeling. These effects decrease, and the  $\rho_t$  determinations become more accurate, with decreasing system frequency. (See Poster 2 for a fuller description of these effects.) By determining a value of  $\rho_t$  at several frequencies, and extrapolating to the region of very low frequencies, a more accurate value of  $\rho_t$  can be derived. The extrapolated  $\rho_t$  value can still be too small if the conductor size is "finite" compared to the coil spacing used, i.e. if the strike length is less than three times and the depth extent is less than twice the coil spacing, or if the traverse is run close to one end of the conductor. However, by making frequency extrapolated  $\rho_t$  determinations of more than one coil spacing, it is possible to extrapolate to the region very short coil spacings to get a more accurate estimate of the true  $\rho_t$ . Although not all of the data is shown here, this procedure was followed in all cases, except 5b, to get the final corrected  $\rho_t$  values shown in table in the upper right corner of this poster.

**CASE 4 - VOLCANOGENIC Cu OREBODY**



**CASE 5a - VOLCANOGENIC Zn-Cu OREBODY**



**CASE 5b - VOLCANOGENIC Zn-Cu OREBODY**

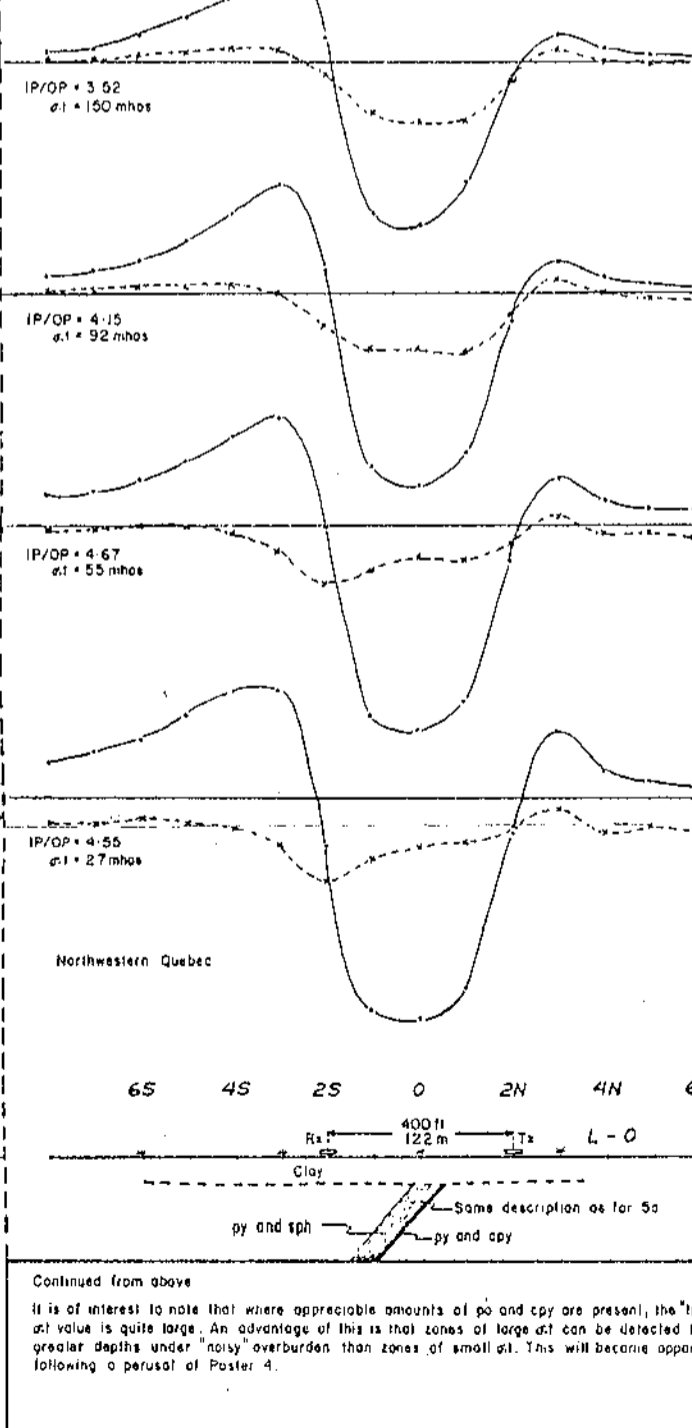




FIG. 2

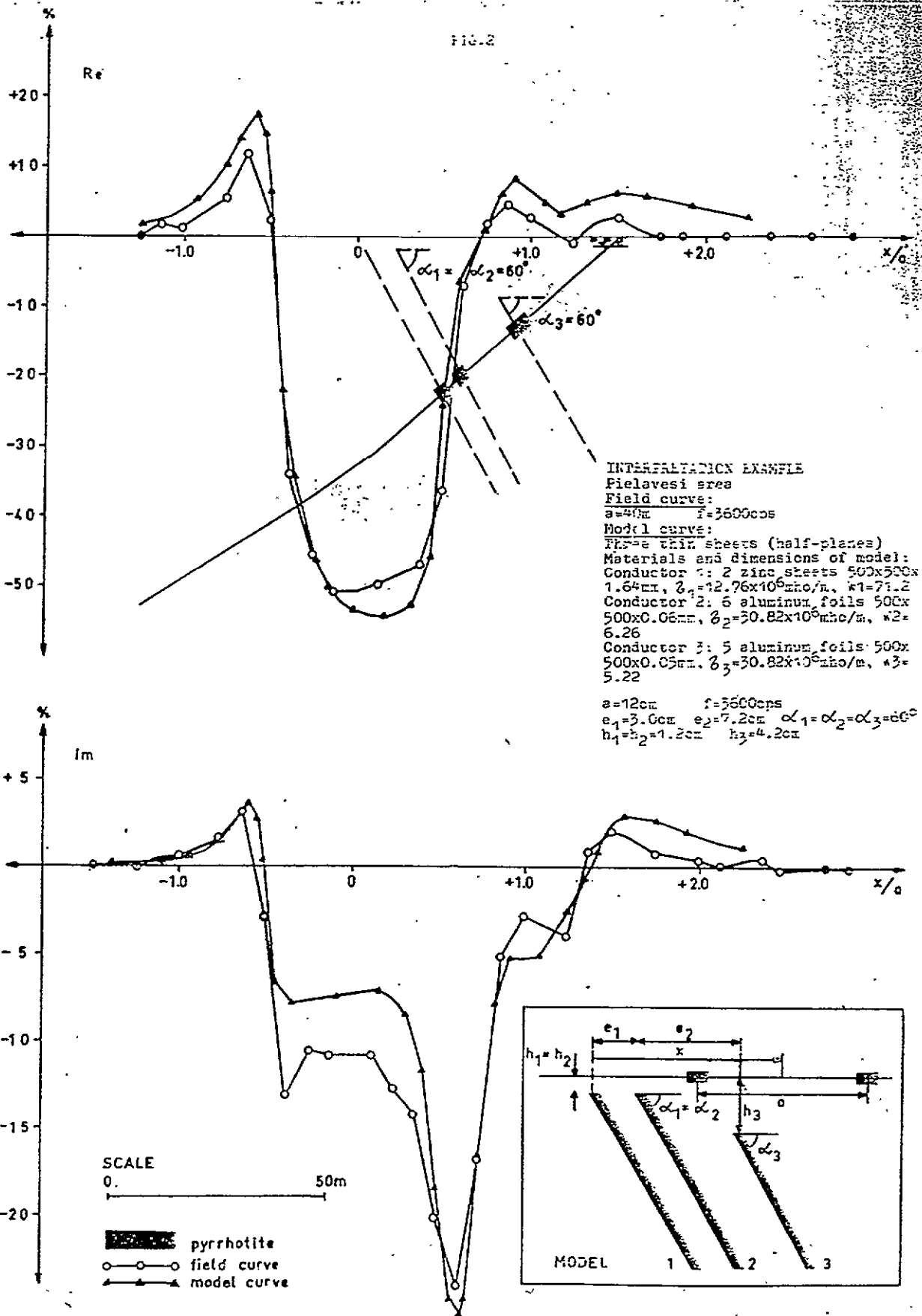


FIG. 3

