EWIN CREEK COAL LICENCES

(260, -263, 2221)

EXPLORATION PROGRESS REPORT

February, 1982

Kootenay Land District
N.T.S. Sheet 82 J/2
Centering approx. - 5,547,350 N, 659, 350 E (UTM).
Held and operated by B.C. Coal Ltd.
For Work Completed Dec., 1981

B.C. COAL LTD.

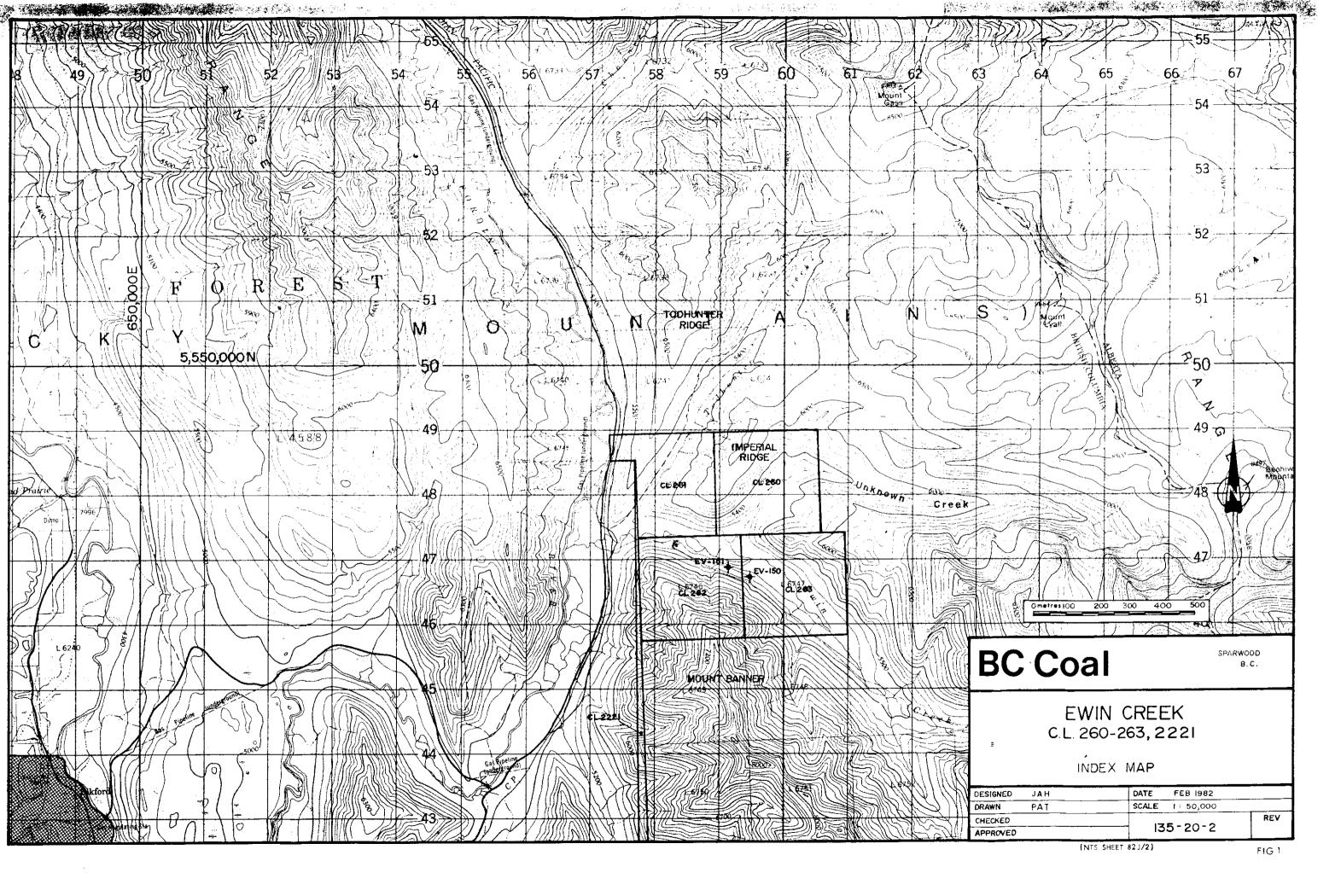
John A. Huryn Geologist

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INTRODUCTION

Location and Access

The Ewin Creek coal licences (260-263,2221) are located in the Fording River Valley of southeastern British Columbia. They are approximately 11 kilometres northeast of Elkford, B.C. and about 43 kilometres north of Sparwood, B.C. (Fig. 1).

A paved highway, connecting Elkford to the Fording Coal surface mine, and secondary logging roads, allow easy access to the licences. A Crowsnest Forest Products (CNFP) logging road runs along the bottom of the Ewin Creek valley, with exploration roads leading off to the drillholes and adit sites.

Topography, Climate and Vegetation

Ewin Creek has a gradient of about 23 metres per kilometre and flows through the centre of the licences in a flat valley bottom that in places, is up to 400 metres wide. Two streams, Todhunter Creek and Unknown Creek, with gradients of about 38 metres per kilometre flow through the licences into Ewin Creek from the northeast. These creeks drain an area of approximately 80 square kilometres and carry large volumes of water during spring run-off.

Prominent mountains rise sharply from the valley floor. On the south side of Ewin Creek is the north end of Mount Banner which reaches an elevation of about 2,235 metres within the licences, some 680 metres above the valley floor. This slope has ephemeral streams carrying run-off during the spring and early summer. The vegetation is primarily conifer with thick brush undergrowth in the drainages. The top of the ridge is more open grassland with sparse conifers.

Between Unknown Creek and Todhunter Creek is Imperial Ridge reaching an elevation of about 2,045 metres, some 495 metres above the valley floor. The southeast facing slope has few ephemeral streams and is primarily open grassland and deciduous vegetation. The northwest facing slope has some ephemeral streams, and the vegetation is primarily conifer, with thick brush in the drainages.

Other topographic features in the licences include the south end of Todhunter Ridge which is mainly open grassland with deciduous and conifer vegetation at lower elevations. Between Ewin Creek and Unknown Creek there is another ridge reaching an elevation of about 1900 metres in the licences. It is mainly conifer with deciduous vegetation at lower elevations.

The climate and weather conditions in the Ewin Creek area are similar to that of Sparwood and Elkford, having pleasant summers and falls, rainy and wet springs and cold winters with moderate to high amounts of snow.

Utilities

The nearest electrical power source is the Greenhills mine site to the west of Ewin Creek. B.C. Tel maintains a telephone exchange to service Elkford and the mines in the area. A Canadian pacific Railway spur, connecting Sparwood with the Fording Coal operations and the Greenhills mine, runs near the west licence boundary. A natural gas pipeline near the west licence boundary services the Fording Coal mine.

Land Description and Ownership

During February of 1968, Kaiser Resources Ltd., acquired the coal rights on 43, 725 hectares of coal-bearing lands from Crowsnest Industries Ltd. The Ewin Creek licences were part of the acquisition and cover 980 hectares, of which about 63% or 608 hectares are coal-bearing.

In October of 1980 Kaiser Resources Ltd. was acquired by the British Columbia Resources Investment Corporation (B.C.R.I.C.) and in February of 1981 became B.C. Coal Ltd., a member of the B.C. Resources Group.

EXPLORATION WORK

A summary of exploration work completed to date is contained in Table 1. Reports detailing past exploration work are listed in the bibliography.

Exploration Work - 1981

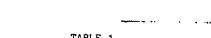
From October 24 to November 12 of 1981 two diamond drillholes were drilled on coal licences 262 and 263. The holes E.V.-150 and E.V.-151 reached depths of 348.8 metres and 391.8 metres respectively. The drill rig used was a Longyear 44 utilizing H.Q. drill rods and a triple-tube wireline core-barrel. The drill used a mud/water drilling fluid with mud tanks set up beside the rig and water pumped from Ewin Creek. The drill is owned and operated by D.W. Coates Enterprises 1td. of Richmond, B.C.

Core samples were collected from both holes and taken to Sparwood where it was logged, photographed and stored. Copies of the lithology logs for E.V.-150 and E.V.-151 are contained in Appendix I and Ia respectively. Strip logs for each hole plotted at 1:1000 scale are contained in a pocket. Coal seams recovered from the drillholes were sampled and taken to the B.C. Coal lab for analysis. The results of the analyses are contained in Appendix II and IIa. Gamma, Neutron and Density logs as well as borehole deviation surveys were done on both holes by Roke Oil Enterprises Ltd. of Calgary, Alberta. Copies of these logs are contained in a pocket. Location surveys for each drillhole were done by B.C. Coal surveyors.

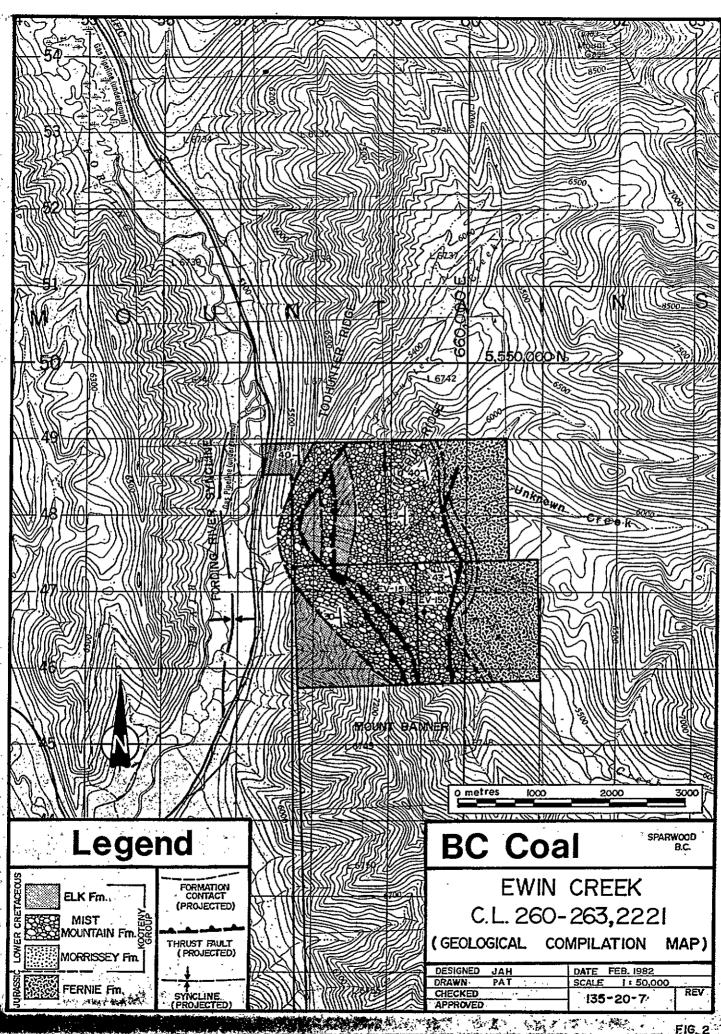
Prior to moving the rig on the licences the access road was upgraded and the drillpads were constructed by dozer. Two D-8H Caterpillar dozers were used in road upgrading, site preparation and rig moving.

RECLAMATION

Reclamation work on the licences included slashing the upgraded access road and slashing and general cleanup of the drillsites. One dozer was used to bury all existing adit portals within the licences.



τ		SUR	TABLE 1	ORK COMPLETED		
Type of Work	1967	1972	1978	1979	1980	1981
Bulldozer work - Main Access - Sec. Access						
Roads Upgraded						
Drill Sites					road to adits up⊸ graded	Road to drillsites
Adit Sites		•		2 Adit sites	•	2
Drilling - Rotary; to of holes - : total matres - Core : no of holes : total metres	,					2 holes
Adits:	·					740.6m
: no of Adits : total metres					2 adits #28,#29	
Adit Reentry	Six adits re- opened and bulk sampled	•			81.5 m including X-Cuts.	
Survey			Underhill Eng. Set survey points	Hand Trenches were surveyed	Survey of adits	Survey bore-holes
Geology /		Reconaissance mapping on licences "-400"	4 months of 1:5000 detailed surface mapping. Coal was hand trenched	Trenching on Tod Hunter ridge Completion of surface mapping 1:5000	· · /	Log drill core



GENERAL GEOLOGY

Figure 2 is a geologic compilation map of the licences. More detailed geologic data is shown on the 1:5,000 scale surface geology map and cross-sections in a pocket.

Stratigraphy

The major stratigraphic units within the Ewin Creek licences are the Jurassic Fernie Formation and the Jurassic-Cretaceous Kootenay Group.

a) Jurassic-Fernie Formation

Outcrops of the Fernie Formation were observed in the northwest end of Imperial Ridge. No detailed work was conducted on the outcrop. The formation has been described by various authors in other areas.

The lower part of the Fernie Formation is composed of dark grey silty shale which contains thin layers of ankeritic siltstone (Price, 1966).

The upper part is composed of rhythmically interbedded, fine-grained sandstone, siltstone and shale. Sandstones in the upper part are ankeritic or calcareous and are commonly laminated. Beds up to 30 centimetres in thickness occur, but are more commonly 1 to 8 centimetres thick (Jansa, 1972)

b) Jurassic-Cretaceous - Kootenay Group The Kootenay Group was proposed by Gibson (1979). It is divided into three formations: the Morrissey, the Mist Mountain and the Elk.

(i) Morrissey Formation

The Morrissey Formation is further divided into the lower Weary Ridge Member overlain by the Moose Mountain Member. In E.V.-150 the Morrissey Formation appears in excess of 50 metres thick. Only the upper contact of the Moose Mountain member was mapped, no detailed measurements were done on the formation other than core description. The upper three metres of the member consists of uniform, thickly bedded, clean, coarse-grained quartz-chert sandstone. Below this it becomes more thinly bedded and varies

in grain size. Occasional thin shale bands and carbonaceous stringers occur. In outcrop it is a prominent cliff-forming sandstone on Imperial Ridge. It can be found on the ridge between Ewin and Unknown Creeks and in a drainage on Mount Banner.

(ii) Mist Mountain Formation

The Mist Mountain Formation appears in excess of 700 metres thick on Imperial Ridge and 1100 metres thick on Mount Banner. The anomolous thickness on Mount Banner is due to thrust faulting. The thickness on Imperial Ridge was obtained by projecting the total thickness of the Mount Banner section excluding the effects of faults.

The formation consists of interbedded conglomerate, coarse-to-fine-grained sandstones, siltstone, mudstone and coal. Drawing 135-20-10 shows a correlation between the two drillholes and the Imperial Ridge section.

Conglomerate bands occur as localized zones, usually associated with sandstones. The sandstones vary in thickness from 1 to 20 metres, are coarse-to-fine-grained, are usually cross-bedded and often contain silt and mudstone interbeds. The siltstone beds are usually laminated and show occasional cross-bedding. The mudstones range from grey to black in colour. The darker shades usually have plant detritus preserved along bedding planes. Coal seams of commercial quality and thickness occur within the formation.

(iii) Elk Formation

The contact between the Mist Mountain Formation and the overlying Elk Formation has been placed at the base of the first major sandstone or conglomerate overlying the uppermost major coal seam in the Mist Mountain Formation (Gibson, 1979). On Mount Banner the base of the Elk Formation has been placed at the base of a large sandstone unit above Adit 8 seam. It can be projected up the ridge to the licence boundary and down to Todhunter Ridge and the licence boundary to the north. On Imperial Ridge the contact has been projected on the southwest facing slope. The formation consists of interbedded conglomerate, medium—to—coarse—grained

sandstones with silt and shale interbeds. Thin lenses of needle coal occur in the Elk Formation.

Structure

The Ewin Creek coal licences lie on the east limb of the Fording River syncline. The beds dip between 30 and 50 degrees to the west and strike approximately north-south. Four thrust faults have been projected through the licence area.

Fault 1 (F₁):

A fault zone was intersected by E.V.-150 between 155.6 metres and 180.3 metres and is characterized by zones of angular breccia and healed fractures. By comparing E.V.-150 with E.V.-151 this fault was found to be a thrust dipping to the west approximately 35° and displacing the section some 80 metres. The surface trace has been projected south to the licence boundary and north to the Fernie Formation. Cross-section B-B' illustrates this fault through the drillhole.

Fault 2,3 (F₂, F₃)

These are thrust faults suggested by D. Grieve of the B.C. Ministry of Energy, Mines and Petroleum Resources. They were projected from Mount Banner and help explain the thickening of the Mist Mountain Formation.

They are thought to dip about 45 degrees to the west. F_2 has a projected stratigraphic displacement of 135 metres, F3 has a projected stratigraphic displacement of 50 metres. They are illustrated in sections A-A' and B-B'. The surface trace is shown on the surface geology map.

Fault 4 (F₄)

This fault is also a thrust proposed to explain the thickening of Elk Formation between Todhunter Ridge and Imperial Ridge. It is projected with a west dip and displaces the section some 240 metres stratigraphically. Section C-C' illustrates this fault.

ECONOMIC GEOLOGY

The two drillholes intersected a total of five different major seams. These seams were sampled and a summary of the results for each hole are shown in Tables 2 and 3. The complete lab analyses are shown in Appendix II and IIa. Quality information on the seams from the adits is outlined previous reports listed in the bibliography.

3 Seam

Three seam is the lowest major seam in the section and occurs about 10 metres above the top of the Moose Mountain Member. A comparison of 3 seam in the two drillholes and Imperial Ridge is shown on drawing 135-20-12. The seam has been divided into 3 seam and 3 Lower seam due to a rock split which occurs. In trench G on Imperial Ridge 3 seam is 2.17 metres thick including some thin rock bands. The Imperial Ridge trench locations are shown on the Surface Geology map. The split is 0.89 metres of mudstone and 3L seam is 1.40 metres thick with some thin rock bands. In E.V.-150 3 seam is 3.95 metres thick. The split is 2.42 metres of sandstone and mudstone and 3L seam is 2.49 metres thick in this hole. seam is 3.56 metres thick with some thin bands of rock. The split is 0.59 metres of mudstone and 3L seam is 3.12 metres including some thin mudstone bands. Three and 3L seams are low volatile bituminous (lvb) coals with a volatile matter (V.M.) on a dry, ash-free (d.a.f.) basis ranging from 19.8-20.8% and a dry, ash-free fixed carbon (F.C. d.a.f.) ranging from The FSI ranges from 6 1/2 to 7 on a clean basis and the 79.4 to 80.2%. reflectance Ro is 1.41 for 3L and 1.45 for 3 seam in E.V.-150. Three seam makes up about 15% of the total estimated reserves for the licences, 45% of this or 33,855,974 tonnes is under less than 750 metres of cover.

4 Seam

Four seam occurs about 37 metres above the top of the Moose Mountain member. Drawing 135-20-13 is a comparison of 4 seam in the two drillholes and Imperial Ridge. In trench F on Imperial Ridge 4 seam is 4.11 metres thick with occasional mudstone bands. In E.V.-150 the seam is 5.64 metres thick. In E.V.-151 it is 4.74 metres thick and appears to have a small rider seam developing in the hanging wall. Four seam is a low volatile bituminous (lvb) coal with a V.M. (d.a.f.) ranging from 20.8 to 21.2% and

an F.C. (d.a.f.) ranging from 78.9-79.2%. The FSI is around 5 and the maximum mean reflectance in oil (Ro) is 1.40. Four seam makes up about 13% of the total estimated reserves and of this about 47% or 29,758,670 tonnes is under less than 750 metres of cover.

5 Seam

Five seam is the thickest seam encountered in the Ewin Creek licences. It occurs about 130 metres above the Moose Mountain Member. 135-20-14 is a comparison of 5 seam in the two drillholes and Imperial Drawing 135-20-11 is a hanging wall structure contour map of 5 seam projected from drillhole and outcrop information. In E.V.-150 the total thickness of 5 seam is 14.63 metres. The upper 2.86 metres has numerous mudstone splits and was sampled separately. In E.V.-151 the total thickness of 5 seam is 15.27 metres with the upper 2.26 metres containing numerous mudstone splits. The thickness decreases to the north and in the two trenches it appears the upper zone of muddy coal encountered in the drillholes has become carbonaceous mudstone. In trench E on Imperial Ridge 5 seam is 10.36 metres thick with a few thin mudstone In trench J on Imperial Ridge the seam is about 8.31 metres thick with some thin mudstone bands. The FSI is 7 and the maximum mean reflectance in oil (Ro) is around 1.32. Five seam is a medium volatile bituminous (m.v.b.) coal with a V.M. (d.a.f.) range between 22.8 and 25.3 and an F.C. (d.a.f.) range of 74.7-77.2%. Five seam makes up about 32% of the total estimated reserves and of this about 48% or 76,564,604 tonnes is under less than 750 metres of cover.

6 Seam

Six seam occurs about 185 metres above the top of the Moose Mountain Member. It was trenched on Imperial Ridge (trench D) and is 4.42 metres thick including a 1.07 metre rock split. The seam appears to pinch out to the south and is less than 1 metre thick when encountered in the two drillholes. The reserves for six seam were calculated for the Imperial block and included the rock split. It makes up about 4% of the total estimated reserves.

7 Seam

Seven seam occurs about 265 metres above the top of the Moose Mountain Member. In trench C on Imperial Ridge it is 4.29 metres thick. In E.V.-151 it is 2.95 metres thick. It makes up about 9% of the total estimated reserves in the licences.

8 Seam

Eight seam is 3.43 metres thick in trench B on Imperial Ridge and 5.30 metres thick in Adit 29. It accounts for about 9% of the total estimated reserves of which 86% or 38,980,000 tonnes is under less than 750 metres of cover.

10 Seam

Ten seam is 5.05 metres thick on Imperial Ridge and 5.12 metres thick in Adit 28. It accounts for about 10% of the total estimated reserves of which about 86% or 86,250,000 tonnes is under less than 750 metres of cover.

Upper Seams

Five seams greater than 1.50 metres thick occur above 10 seam. They each have adits driven in them and range in thickness from 1.77 metres to 3.91 metres. The combined total of estimated reserves for the upper seams accounts for about 4% of the total estimated reserves on the licences.



THOL	<u> </u>
COAL QUALIT	Y SUMMARY
D.D.H. E.V	150

Seam Intercepts	Seam No.	True Thickness	Core	Raw	Coal				Clean (Coal	· · · · · · · · · · · · · · · · · · ·		Hoot day 14 3	
(m)			1, 19 100001	Ash	FSI	Ash	V.M.	V.M. (daf)	F.C.	FSI	\$	DDM's	Heating Value cal/g	Rŏ
59.60- 62.90	5	2.86	70	57.8	1	10.4	22.5	25.1	67.1	7	0.52	778.1	7,836	1.24
62.90- 76.49	5	11.77	85.0	17.4	6	8.1	20.4	22.2	71.5	7	0.34	32.7	7,970	1.32
251.49-257.71	4	5.64	71.6	24.5	2	7.7	19.2	20.8	73.1	5	0.42	1.6	7,918	1.44
277.77-282.16	3	3.95	68.1	32,6	2	8.8	18.1	19.8	73.1	6.5	0.51	23.9	7,982	1.45
284.85-287.62	3L	2.49	50.5	14.1	2	7.9	19.2	20.8	72.9	6,5	0.38	60.1	7,995	
293.35-293.90		0.49	00	13.0	7.5	8.3	19.7	21.5	72.0	7.5	0.50	245:2	7,953	1.41
97.04-297.80	М	0.68	76.0	14.4	3.5	7.6	21.7	23.5	70.7	7	0.53	992.4	8,108	1.44

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TABLE 3
COAL QUALITY SUMMARY
D.D.H. E.V. - 151

Seam	Scan		Core.	Raw Coal			Clean	Coal				Heating Values	75 m
Intercepts	No.	Thickness	Recovery	Astı FSI	Ash	V.M.	V.M.	F.C.	FSI	S	DDM's	cal/g	Rö
							(daf)	•				,	
7.29- 11.65	. 8	3.88	42.7	17.7 6.5	6.1	25.3	26.9	68.6	6.5	0.55	9,8	8,056	1.13
17.01- 21.16	8L	3.70	41.9	50.8 5.5	8.5	25.9	28.3	65.6	7	0.62	435.9	7,901	1.13
29.27- 30.18		0.81	100	23.8 6	7.6	25.1	27.2	67.3	7.5	0.94	563.4	7,987	
44,13- 44.88		0.61	65.2	20.4 7	8.7	24.3	26.6	67.0	7.5	0.84		7,861	1.17
64.63- 65.24		0.53	85.0	19.9 7.5	6,1	24.7	26.3	69.2		1.07			1.22
82.20~ 85.43	7,	2.95	39.6	21.6 6	9.3	22.2	24.5	68,5		0.60	176 k	8,107	1.18
97.59- 98.84	•	1.07	100	15.3 2.5	8.5	20.0	21.9	71.5			175.4	7,657	1.18
59.82-170.73	6	0.82	80.0	41.3 4	8.5	21.7	23.7			0.68		7,228	1.22
16.55-218.96	5	2.26	- •	41.4 1.5				69.8		0,81	3.0	7,935	1.16
18.96-232.81	_	13.01	01 1		8.2	20.2	22.0	71.6	7	0.54	19.7	7,905	1.30
	,		81.4	22.9 2.5	8.3	21.5	23.4	70.2	6	0.35	7.3	7,925	1.35
26.92-327.56		0.67	100	37.9 1	6.4	19.2	20.5	74.4	6	0.58		8,154	1.43
28.26-333.45	tt	4.74	79.4	19.1 3	7.4	19.5	21.1	73.1	5.5	0.43	7.7	8,009	1.40
53.72-357.62	3	3.56	88.3	32.3 2	9.5	18.6	20.6	71.9	7	0.42	51.8	7,883	1.44
58.26-361.68	3L	3.12	88.4	19.4 7	8.4	21.1	23.0	70.5		0.55	264.5		
63.50-364.39		0.72	100	9.8 5.5	6.9	18.7	20.1	74.4		0.45	#04.7	7,924	1.44
					=			1911	•	V.40		8,123	1.44

COAL RESERVES

The estimated total coal in place reserves for the Ewin Creek licences is about 500 million tonnes. Of this approximately 60% or 300 million tonnes occurs under less than 750 metres of cover. Table 4 shows the breakdown by seam of the reserve estimate. Three, 4 and 5 seams account for about 60% of the total reserves with about 47% of the reserves for each seam occuring under less than 750 metres of cover.

Method of Reserve Estimate

The licences were divided into three blocks and bounded as shown on the surface geology map. The coal seams in each block were bounded by outcrop, 750m coverline, licence boundary or fault boundaries.

The surface area of each seam was measured using the 1:5000 scale map and a planimeter. The vertical thickness was taken from surface measurements or borehole thickness. The area times the vertical thickness gives a volume. The volume is multiplied by Specific Gravity to get tonnes.

· S.G. is calculated by the following:

S.G. = 1.250 + 0.011 (% raw ash of seam) (Samuelson, 1981)

This formula was derived by Samuelson as additional work to studies done by Taylor on Ash related to Volume coal conversion. The raw data for Samuelson's derivation was taken from Greenhills samples.

The raw ash data was taken from borehole, adit and trench data.

For the Imperial Block the vertical thicknesses and raw ash was taken from trench data. The seams are bounded by outcrop, the licence boundary and the 750 metre coverline.

For the Valley block the thicknesses were averaged between the drillholes and trenches, the raw ash data was taken from the drillholes for seams they intersected and adits or trenches for the other seams

For the Banner Block the vertical thicknesses and ash data were taken from the drillholes for seams they intersected. The other seam data was taken from adit or trench data.

Classification of Reserves

<u>Proven</u> - Proven reserves are tonnes of coal in place computed from observations (i.e. drill holes, adits outcrops, mine workings, etc.) spaced at intervals of 0.8 km or less in areas of good geological continuity. Seams should be greater than 1.5m thick and under less than 750 metres of cover.

Partially Explored - Partially explored reserves are tonnes of coal in place computed partially from observations spaced at intervals of 0.8 km to 2.4 km apart and partially from reasonable geological projections. Seams should be greater than 1.5 m thick and under less than 750 m of cover.

<u>Projected</u> - Projected reserves are tonnes of coal in place where little direct evidence is available but where geological studies have indicated continuity of the coal bearing measures. Coal seams and seam thicknesses are projected from adjacent areas.

The majority of the reserves in the Ewin Creek licences are considered to be projected. The Banner Block, where the majority of exploration work has occured can be considered as partially explored reserves.

TABLE 4

EWIN CREEK COAL LICENCES PROJECTED RESERVE ESTIMATE

TONNES OF COAL

	Seam No.	Vert. th (m)	S.G. gm/cc	Reserves to 750 m cover	Total Coal In Place
			1 20 '	E 600 010	11: 190 En6
Imperial Block	1	3.84	1.39 1.41	5,622,214 4,142,421	14,173,536 10,105,604
	* 2	2.73 4.65	1.51	7.569.482	18, 129, 841
•	3 4	5.73	1.43	9,065,327	20,930,808
		13.52	1.50	24,268,576	50,064,209
•	5 6	5.77	1.46	10,648,014	20,169,856
	7	5.60		12,284,384	21,762,881
	8	4.48	1.73 1.63	9,307,787	15,754,244
	10		-	11,091,051	17,707,803
	10	6.59	1.33		11,101,002
				93,999,256 Total	188,798,780 Total
Valley Block	3	6.59	1.44	11,769,477	15,826,281
•	4	5.71	1,49	9,418,247	12,459,747
	5	15.56	1.53	17,783,680	24,901,913
	7	4.42	1.49	5,202,732	5,202,782
	8	5.64	1.44	6,012,914	6,012,014
	10	6.59	1.33	5,896,398	5,896,398
				50,772,59\$ Total	70,299,135 Total
Banner Block	3	7.56	1.44	14,517,015	39,193,762
	4	5.71	1.49	11,275,096	30, 154, 126
	5	16.58	1.53	34,512,348	84,892,004
	7	4.42	1.49	19,770,571	19,770,571
	8	5.64	1.44	23,660,251	23,660,251
	10	6.59	1.33	24,510,435	24,510,485
				118,098,%% Total	222,181,200 Total
Upper Seams	Adit #1_	3 . 56 -	1.38	7,281,998	7,281,998
	Adit #2	1.77	1.45	3,430,770	3,430,770
	Adit #5	2.20	1.41	2,415,583	2,415,663
	Adit-#7	3.91	1.41	3,725,477	3,725,477
	Adit #8	2.85	1.48	2,636,251	2,636,251
	* * * *		•	19,490,779	19,490,179

Total Reserve Estimate to 750 m cover: 297,817,800 tonnnes

Total Coal In Place Estimate: 500.769,290 tonnes

Conclusions and Recommendations

The two drillholes in the licences indicate there is good quality metallurgical coal of significant volume in the lower part of the Mist Mountain Formation. Seams 3, 4 and 5 seams make up the bulk of the estimated reserves in the area. Five seam is the thickest of the seams in the licences and preliminary quality analysis indicates it to be good metallurgical coal, very much like the 10 seam coal presently being mined at Balmer Operations.

The structural geology of the area is very complex. The present interpretation is based largely upon projection. Further exploration by way of drillholes is required to help understand the structure of the area. An adit in number 5 seam in the Banner Block is recommended to obtain a reliable bulk sample and analysis of this seam. Adits in 3 and 4 seam in the same area would also prove useful in obtaining reliable quality data.

EWIN CREEK C.L. 260-263, 2221 STATEMENT OF COSTS

ON PROPERTY COSTS

	Salaries (geologists, supervision, core logging, surveying).	· \$	14,830.40
		•	
•	2 D8H Dozers @ \$95.76 per hr. (c/w angle blade and ripper)		
	All Found Rate	•	13,693.68
	D.W. Coates Enterprises Ltd. (Contract Drilling)	•	80,185.68
	Roke Oil Ltd. (Contract downhole logging)		4,684.77
,	Applied Reclamation Costs		3,601.26
	Sampling and Testing		8,102.99
	Freight (dozer transport)		677.46
	Truck Rental (1 for 30 days)		655.00
	Radio Communications	*	53.19
	Materials and Supplies		38.63
			~~

OFF PROPERTY COSTS .

Report Preparation	:			
(geological interpretation	, drafting,	• •	•	•
report writing)	•		•	6,732.84

TOTAL COSTS

\$ 133,265.90

R. REGIER
MANAGER, MINES ACCOUNTING

-fws/5/

STATEMENT OF QUALIFICATIONS

J.A. Huryn:

B.SC. Geology, University of Calgary Calgary, Alberta 1979

Practical: 3 summers coal mapping experience as a student and 3 years in coal mapping, structural interpretations, reserve estimation and licence evaluation with Kaiser Resources Ltd. and B.C. Coal Ltd.

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1973 Ewin Creek Licences Progress Report, March 1973. Kaiser Resources Ltd. Exploration Geology Report.

Samuelson, L.B.,

Ash related Volume to Weight Coal Conversion. Additional work to a report of the same title by G. Lynn Taylor, 1982.

Taylor, G.L., 1980

Ash Related Volume to Weight Coal Conversion.

BCCoal Ooteg ELEV.

HOLE No: EV-150 LOGGED BY: J.A. HURYN DATE: Oct 27/81 PAGE: 1 OF: 19 ELJIN CREEK HOLE NO. AREA LAT. O.B. m CASING WALER ANG. AZIM DOH 1510 EWNICK 40151514161713161917101016151914171717171612181210 48.78 274 START FIN. Doy, Mo., Year SIZE 10 ~. SIZE GEO. LOG co. CO. GEOL. 24/10/81.01 ROKTAH 3 4 81718 OF BED PRIMARY CONTROL ROCK I CHARACTERISTICS ROCK II **STRUCTURE** CORE RECOVERY MAJOR GUALIFYING MATERIAL MINOR QUALIFYING MATERIAL COLOUR MUNSELL SYSTEM **FRACTURES** FOOTAGE OF C-B ANGLE MEASUREMENT ROCK NAME CORE RECOVERY ROCK NAME TEXTURE ANGLE SORTING GRAIN SIZE SPHERICITY ROUNDNESS SECONDARY JOINT ANGLE LENGIH PRIMARY JOINT ANGLE RELIABILITY CORE FOOTAGE AMOUNT MA RELATION TENTHS AMOUNT AMOUNT NAME NAME C-8 9 10 11 12 13 14 15 36 17 38 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 46 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 10% B 9 46. ... RAW CLEAN DEPTH REC % SEAM V.M.(DAF) VERTICAL THICKNESS FS1 SULF D. D. M. AIEFD B.T. U.

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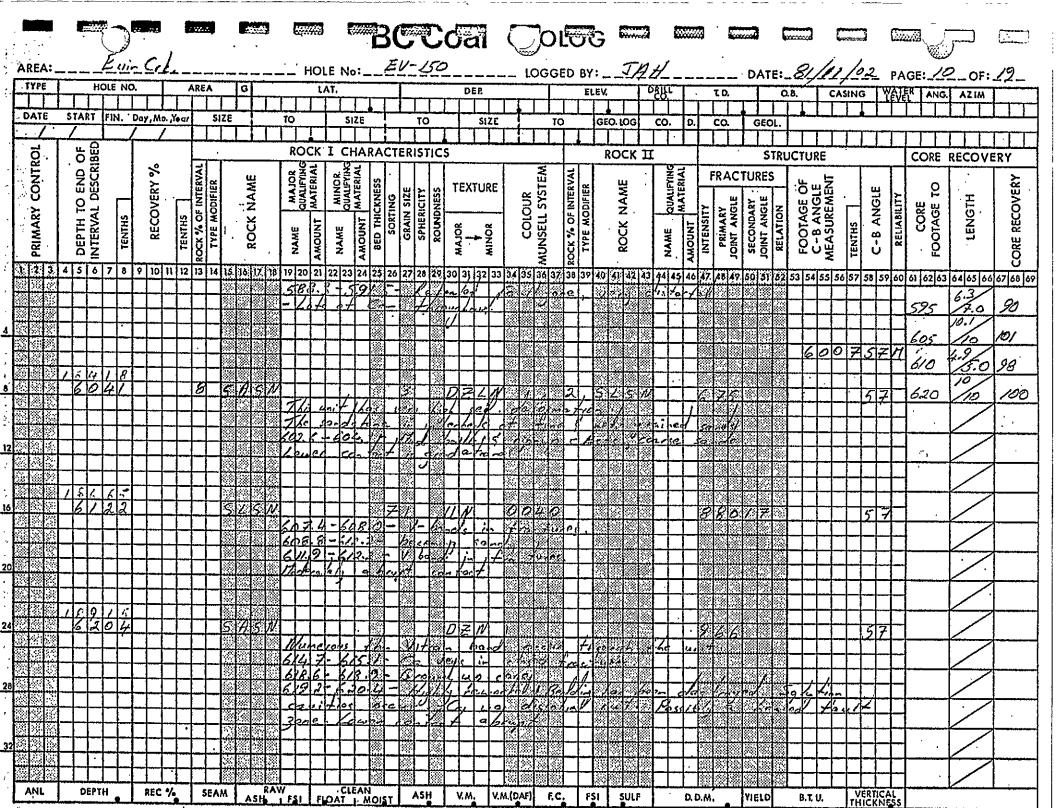
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TYPE HOLE NO. AREA LAT. DEP. CASING T, D. WAJEK ANG. AZIM DATE START FIN. Day, Mo., Year SIZE TO SIZE ΤQ SIZE GEO. LOG TO CO. ₽. COL GEOL. PRIMARY CONTROL DEPTH TO END OF INTERVAL DESCRIBED ROCK I CHARACTERISTICS ROCK II **STRUCTURE** CORE RECOVERY ROCK % OF INTERVAL
TYPE MODIFIER MAJOR QUALIFYIHG MATERIAL MINOR QUALIFYING MATERIAL COLOUR MUNSELL SYSTEM ROCK % OF INTERVAL **FRACTURES** FOOTAGE OF C-B ANGLE MEASUREMENT ROCK NAME BED THICKNESS
SORTING CORE RECOVERY CORE FOOTAGE TO RECOVERY ROCK NAME **TEXTURE** GRAIN SIZE SPHERICITY C-B ANGLE ROUNDNESS LENGTH SECONDARY JOINT ANGLE PRIMARY JOINT ANGLE RELIABILITY RELATION AMOUNT TENTHS MINOR AMOUNT AMOUNT TENTHS NAME NAME 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 34 37 38 39 40 41 42 43 44 45 46 47 46 49 50 57 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 73% 82.5 4.0 4.9/ 741. RAW CLEAN
ASH FSI FLOAT | MOIST ANL DEPTH REC % **SEAM** VERTICAL THICKNESS , ASH V.M. V,M,(DAF) F, C. F51 SULF D. D. M. YIELD B.T. U.

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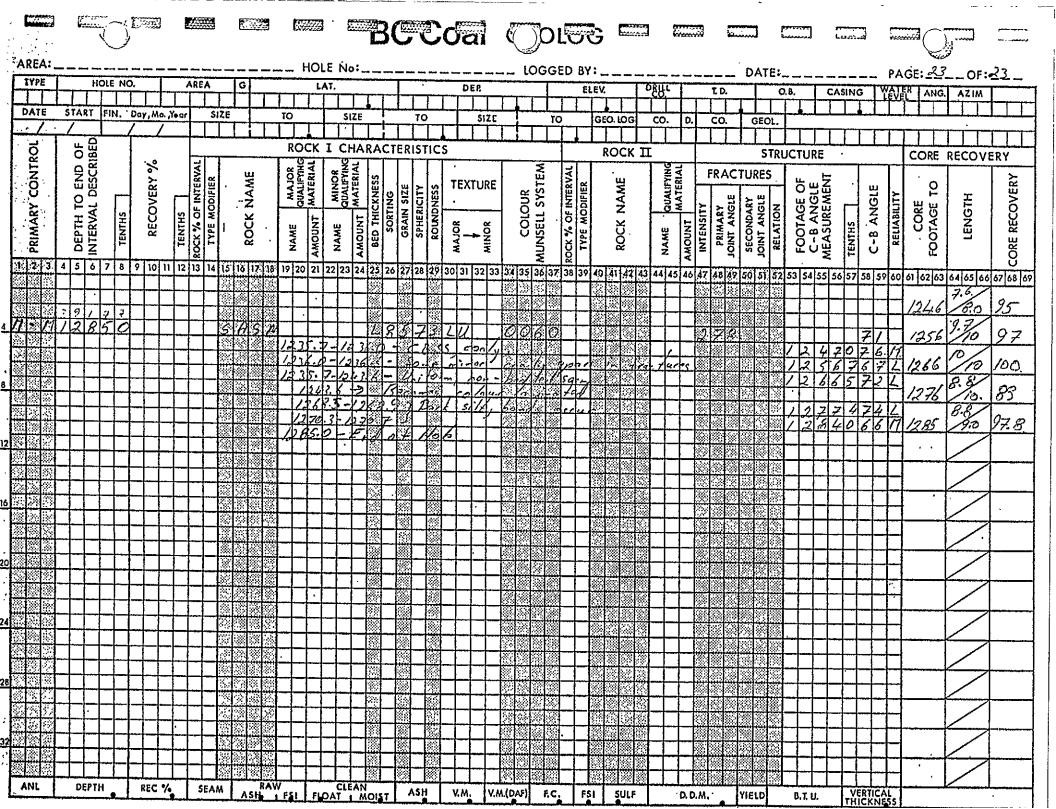
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The proximate analyses, washability tests and petrographic examinations of the coal seams sampled from diamond drillholes E.V.-150 and E.V.-151 were performed in the B.C. Coal Ltd. laboratory located in Sparwood, British Columbia.

A Geisler Plastometer was used in conducting fluidity tests on the samples. A Ruhr dilatometer was used for the dilatation tests.

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	PRILL HOLE: EVISO (CORE) SEAN VERTICAL THICKNESS -0.76 DIP ANGLE RECEIVED: ON H	0/00/00 8 00 YY	INTERCEPT LATTIVE WEIGHT COMPOSITE:	13.81- 14.5 3546736.970 H 0.00 KG	IT INICPT DEPARTURE WOISTURE RECOVERY	THICKNESS 0. 659471.970 X 0.0 X 94.0 %	74 TRUE THIC ELEVATION COMPLETES	MXIBS 0.70 X 1 1411.170 H 20/00/00 EN DD YY
	PROXIMATE ANALYSIS (DRY BASIS) RAU ICLEAN	i GIESEL	ER FLASTICI	iy, DATE RUN O)/00/00 	DILATATION (RUHR) DATE RUP	00/00/00
	PROXINATE ANALYSIS (DRY BASIS) X OF 1/8' X O 0.00 0.00 0.00 ASH X 0.00 0.00 0.00 F.C. X 0.00 0.00 F.C. X 0.00 0.00 F.S.I. X TOTAL SULF, 0.00 0.00 0.00 GROSS CAL, VALUE BTU/LB 0. 0.0 V.M. X (DAF) * (-1/8'+0 COAL FLOATED AT 1.50 S.G.) SCREEN ANALYSIS (COAL CRUSHED TO 1/4') SIZE WT.X ASHX WT.X ASHX -1/4'+ 28M 0.0 0.0 0.0 0.0 -60M + 60M 0.0 0.0 0.0 0.0	START FUSION WAX FI FINAL SOLID	i Tenp. LNID TEMP. FLUID TEMP IFICATION TO	00 00 00 00 00 00 EHF. 00	1.0	II - SOFT, TEM III - MAX, CONTI IIII - MAX, DILA CONTRACTIO	r. RACTION TEMP. TATION TEMP. ON	3 0.0 60 0.0 60 0.0
63	% 101AL SULF. 0.00 0.00 0.00 1	MAXIM	vo Kande. Di Fluidity	09/X hr . 0	1	withiniti		<i>5</i>
	V.K. X (DAF) 0.0 1 * (-1/8'+0 COAL FLOATED AT 1.50 S.G.)	PETROGI	RAPHIC CATA	DATE COMPL	ETER 00/00.	/00 PELLET NIN	MBER O	
 	SCREEN AMALYSIS (COAL CRUSHED TO 1/4')	- V-TYF I TYPE	'ES REAL ' T	CTIVE COMPONENT OTAL VIYRIHOID FACTOUS OF 111	3 . 0,0 2) 0.0	INERT COMPONENT INERT SF. (1/	(2) 0.0 3	
	SIZE WT.X ASHX WT.X ASHX	! 0 ! 0	0.0 E)	XINOID & RESIN	0.0	FUSINCIDS HINERAL HATTE	0.0 ER 0.0	
F33	-1/47 22M 0.0 0.0 0.0 0.0 0.0 -28M + 60M 0.0 0.0 0.0 0.0 0.0	I 0	0.0 TOTA	AL REACTIVES "	0.0	TOTAL INERTS	0.0	
	-60N + 0	MAX. P	0.0 SEAN REFL. (INDEX 0.00	F VITRINDIDS (STRENGTH IND	KD) 0.00 EX 0.00	PRED. COKE STAE	3. INDEX 0.	0¢
	HASHABILITY DATE RUN 00/00/90			i washability	DATE R	RUN 00/00/00		
	WASHABILITY DATE RUN 00/00/90 (WT.Z) S.G. DIRECT X FSI AND SIZE WT. ASH	91° (% +/1 YSH S.G.	I (WT.X) I AND SIZE	S,6,	DIRECT Z FSI WT. ASH	CUH, Z WT, AS	+/1 H 5.5.
Servers.	(0.0) FLT. 1.30	0.0 0	0.0	(100.0) -1/8'+ 0.	FLT: 1.30 1.40	0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0	0 0.0 0 0.0
<u> </u>	1,50 0.0 0.0 1,60 0.0 0.0 1,70 0.0 0.0	0.0 0 0.0 0 0.0 0	1.0 0.0 1.0 0.0		1,50 1,60 1,75	0.0 0.0 -0.0 0.0 -0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0	0.0
Name of the last	D SINK 1.70 0.0 0.0	6.0 0	· · · · · · · · · · · · · · · · · · ·	<u> </u>	SIRK 1.70	0.0 0.0	č.5 5.6	Š
	(0.0) FLT. 1.30 0.0 0.0 -28N+60N 1.40 0.0 0.0 0.0 1.50 0.0 0.0	0.0 0	.0 0.0	I FROTH I CELL TEST				
	-28N+40N 1.40 0.0 0.0 0.0 1.50 0.0 1.60 0.0 0.0 1.60 0.0 0.0	0.0 0	·0 0·0		FROTH	0.0 0.0	. 0.0 0.0	·) ·
	1,50 0.0 0.0 1,70 0.0 0.0 31NK 1,70 0.0 0.0	0.0 0.0	.0 .0	-28%+60% 	Tạilings	0.0 0.0 0.0 0.0	0.6 0.6	
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	1.60 0.0 0.0 1.70 0.0 0.0 SINK 1.70 0.0 0.0	0.0 0 0.0 0	.0 0.0	(G.O) -60% + G	FROTH TAILINGS	0.0 0.0	0.0 0.0	
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	NOTES:							

	ORILL HOLE: EVISO (CORE) SEAH 5.S VERTICAL THICKNESS 3.30 RIP ANGLE RECEIVED:	INTERCEI 30 LATITUÚ 00/CO/GO WEIGHT 4H DO YY COKFOSI	PT 39.60- 62 PE 3546734.970 M 0.00 K	,70 INYCPT T. DEPARTURE G HOISTURE RECOVERY	HICKRES3 3.30 659471.970 X 0.0 X 0.0 Z	TAME THICKNESS ELEVATION COMPLETE:	24 20 14 20,05/60 1223*400 H
)	PROXIMATE AMALYSIS (DRY BASIS) X OF 1/8' X O 100.00 20.40 ASH Z 12.40 22.50 F.C. Z 27.80 67.10 F.S.I. 1 7 X TOTAL SULF. 0.27 0.52 X P205 (PHCSPHAYE) 0.00 GROSS CAL. VALUE STU/LS 0.7836. V.M. X (BAF) 29.4 * (-1/8'70 COAL FLOATED AT 1.50 S.G.)	GIESELER PLAST START FUSION TEMP, HAX FLUID TEM FINAL FLUID TO SOLIDIFICATION MELTING RANGE HAYMEN FUTO	TCITY, DATE RUN OC 3 OC 3 OC 4 IEHP. OC 4 OR TEMP. CC 4	00/00/00 1 D 195.0 1 T 195.0 1 T 192.0 1 T 192.0 1	ILATATION (RUMA) I - SOFI. IEMP. II - MAX. COMTRACT III - MAX. DILATAT CONTRACTION DILATATION	OATE RUN 69. OCTION TEXP. CC LIE TEXP. CC	407.0 407.0 149.0 482.0 18.0 83.0
	GROSS CAL. VALUE STU/LB 0. 7836. V.M. X (BAF) 29.4 * (-1/8'+0 COAL FLOATED AT 1.50 S.G.)	PETROGRAPHIC B	PATA DATE CON REACTIVE COMPONE	FLETEB 00/00/	OC PELLET HANDE INERT COMPONENTS	R G	
2	SCREEN ANALYSIS (COAL CRUSHED TO 1/4')	1 TYPE 7. 1 9 0.7 1 10 2.1	TOTAL VITRINO REACTIVE SF. (EXIMOID 2 RES	(D 67.0 1/2) 7.7 (N 0.2	IMERT SF. (1/2) MICRINGIES FUSINGIES HIMPEN MATTER	2. 6.7 (2. 6.4 6. 6.7 (2. 6.4 6. 6.7 (2. 6.4	
	SIZE WT.Z ASHZ WT.Z ASHZ -174'+ 28H 89.7 70.3 87.7 70.5 -28H + 60H 6.3 27.8 76.2 67.7 -60H + 0 3.8 28.7 100.0 66.2	12 35.7 13 15.9 14 3.4 1 MAX. MEAN REF 1 BAL. INDEX	TOTAL REACTIVES L. OF VITRINDIDS 0.87 STRENGTR	77.1 (SC) 1.24 (NDEX 5.07	INERT COMPONENTS INERT SF. (1/2) MICRINGIDS FUSINGIDS MINERAL MATTER TOTAL INERTS FRED. COKE STAB.	20.9 INDEX 63.60	
	WASHABILITY DATE RUN 00/00/90 (WT,Z) S.G. DIRECT Z FSI	CUH. Z f/- WT. ASH S.	l WASHABIL) 1 1 (WT.Z) 0, l AND SIZE	CIY BATE R S.O.	UR 00/00/00 DIRECT Z FEI WT. ASH	CUH. Z NT., ASH	
	(87.9) FLT. 1.30 4.0 2.7 7-1/2 -1/4'728N 1.40 6.2 10.3 6-1/2 1.30 3.1 20.7 3 1.60 4.4 30.7 1-1/2 1.70 3.8 37.3 1 SINK 1.70 76.5 86.1 NC	4,0 2,7 43	3,4 (100.0) 3,1 -1/8/+ 0 0,4 1,7	51 T. 1.30	6.3 2.8 7-1/2 6.5 7.8 7 5.7 14.9 5 5.3 22.8 2 4.7 31.0 1 71.5 82.8 KC	44.3 2.3	44.7
Prince Prince	(6.3) FLT. 1.30 36.0 2.2 7-1/2 -28H460H 1.40 16.0 7.2 7 1.50 10.7 15.4 2 1.60 4.6 25.9 1 1.70 2.7 36.4 1 SINK 1.70 28.0 78.4 NC	54.0 3.7 37	7.0 FROTH 7.1 CELL TEST 1.2 0.1 (6.3) -29N+6CM	FROTH	0,0 .0.0 0,0 0,0	0.0 0.0	,
	(3.8) FLT. 1.30 0.0 0.0 -60H 0 1.40 0.0 0.0 1.50 0.0 1.60 1.60 0.0 0.0 1.70 0.0 0.0 51NK 1.70 0.0 0.0	0.0 0.0 0	0.0 FROIH FRET 1150 0.0 (8.5) 0.0 0 + KOb-		63.3 19.2 7 16.7 77.4 NC	63,3 17,2 100,0 28,7	
	NOTES:						

DRILL HOLE: EVISO (CORE) SEAK 5.3 VERTICAL THICKNESS 13.59 DIP ANGLE RECEIVED:	INTERCEPT 62.90- 76.47 INTOPT THICKNESS 13.57 TRUE THICKNESS 11.77 N 30 LATITUDE 5546736.970 N DEPARTURE 659471.970 N ELEVATION 1545.100 H 00/00/00 WEIGHT 0.00 NG HGISTURE 0.0 Z COMPLETE: 06/09/09 NH DD YY COMPOSITE: RECOVERY 65.0 Z NX DD YY
1329	GIESELER PLASTICITY, DATE RUN 00/09/00 DILATATION (RUHR) DATE RUN CO/OC/CO START
La V.A. X (1951) 23.1	I FEIRUGRAFHIC DATA DATE COMPLETED CO/00/00 PELLET RUMBER 1332
SCREEN ANALYSIS (COAL CRUSHED TO 1/4/1 CUMPLATIVE SIZE WI.Z ASHX WI.Z ASHX -1/4/† 28H 87.4 22.6 87.4 22.6 -28H † 60H 7.3 11.2 94.7 21.7 -60H † 0 5.3 15.2 100.0 21.4	V-TYPES REACTIVE COMPONENTS INERT COMPONENTS 1 TYPE Z TOTAL VITRINGID 54.3 INERT SF. (1/2) 15.3 11 2.7 REACTIVE SF. (1/2) 15.3 HIERINGIDS 3.5 12 20.6 EXINGID 2 RESIN 0.1 FUSINGIDS 7.0 13 26.1 HIRERAL HATTER 4.5 14 3.9 TOTAL REACTIVES 67.7 TOTAL INERTS 30.3 0 6.0 0 0.0
	HAX. HEAN REFL. OF VITRINGIDS (RO) 1.32 BAL. INDEX 1.58 STRENGTH INDEX 5.43 PRED. COKE STAB. INDEX 50.70 CUH. Z +/1 WASHABILITY DATE RUN 00/00/00 CUH. Z +/1 (WT.Z) S.G. DIRECT X FSI CUK. Z +/1 WT. ASH S.G. ARD SIZE WT. ASH WT. ASH S.G. 12.1 2.1 42.5 (106.0) FLT. 1.30 27.6 2.6 8 27.5 2.6 53.4 40.9 5.3 43.4 -1/8'+ 0 1.40 24.6 2.0 4 1/2 52.2 2.3 52.5 53.7 7.7 15.3 1.50 18.7 14.4 1 70.9 5.5 32.7 55.6 6.3 11.9 1.60 8.2 26.6 1 79.1 7.7 13.9 47.4 12.5 1.70 3.2 39.6 1 29.3 8.3
(67.4) FLT. 1.30 12.1 2.1 8-1/2 -1/4'+28H 1.40 28.8 6.6 7 1.50 13.0 15.3 1-1/2 1.60 1.7 27.7 1 1.70 9.8 36.6 1 81MK 1.70 3.7 63.7 MC	12.1 2.1 42.5 (100.0) FLT. 1.30 27.6 2.4 8 27.6 2.4 53.4 40.9 5.3 43.4 -1/8'+ 0 1.40 24.6 2.0 4 1/2 52.2 2.3 52.6 53.7 7.7 15.3 1.50 18.7 14.4 1 70.9 5.5 32.7 55.6 6.3 11.9 1.60 8.2 26.6 1 79.1 7.7 13.9 65.4 12.5 1.70 3.2 39.6 1 82.3 8.9 69.1 15.3 SIRK 1.70 17.7 59.4 NC 100.0 19.6
(7.3) FLT. 1.30 0.0 0.0 0.0 -28H±60X 1.40 0.0 0.0 1.50 0.0 0.0 1.20 0.0 0.0 1.20 0.0 0.0 1.70 0.0 0.0 5.0 SINK 1.70 0.0 0.0	0.0 0.0 0.0 FROTH 0.0 0.0 0.0 CELL TEST 0.0 0.0 0.0 CELL TEST 0.0 0.0 0.0 (7.3) FROTH 0.0 0.0 0.0 0.0 0.0 0.0 -28N+2CH TAILINGS 0.0 0.0 0.0 0.0
(5.3) FLT. 1.30 0.0 0.0 0.0 -6000 0 0.0 1.40 0.0 0.0 1.50 0.0 0.0 1.50 0.0 0.0 1.70 0.0 0.0 51NK 1.70 0.0 0.0	0.0 0.0 0.0 FROTH 0.0 0.0 0.0 CELL TEST 0.0 0.0 0.0 (5.3) FROTH 93.7 11.6 7 93.7 11.6 0.0 0.0 0.0 -60K + 0 TAILINGS 6.1 71.2 NC. 100.0 15.2 0.0 0.0
MATEG	

NOTES:

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	DRILL HOLE; VERTICAL 11	EVIS HICKN	0 E33	(CORE - 1.07) SEA DIF RECE	if Angle Tyen:	00/09/0 00/09/0 00 00 00	18 29 L4 10 WE (Y C)	MERCEPT METUBE MEHE MPOSITE	20 354 :	2, <u>16- 20</u> 6736,970 0,00	3.23 M DE KG HO RE	INTOPT PARTUR ISTURE COVERY	THICK E 6	ESE 9471, 0	1,07 970 H .0 X	TRUS ELEY! CGIPI	THICK THICK EYE:	MESS 1425 60/00 HM DE	0.74 1.840 1/90
)	PROXIMATE	AHAL	EISY	(BRY B	ASIS)	CLEAR	! GIE	ELER	PLASTIC	ΣΥΫ́	DATE RUN	00/00	/00 !	DILATA	TICH	(RUER)	CATE	RUN	99/90/8	.
	Z OF 1/8') ASH Z V.H. Z F.C. Z F.S.I. Z TOTAL SUL Z F205 (PHO GROSS CAL. V.H. Z (DAF	(0	•	· ·	0.00 0.00 0.00	0,00 0,00 0,00	FINE FINE FINE FINE SQL	RT ION T FLUI AL FL IDIFI	ESP. D TEHP. UID TEK CATION	o Tenr	00 00 00 00 00 00 00 00 00 00 00 00 00	0.0 0.0 0.0 0.0	, 800		SOFT MAX. MAX. CONTI	TEMP, CONTRAC DILATA RACTION	CIIOM TE	er He	00 00 00 X	0.0 0.0 0.0
	Z POS (PHO	.c., ISPOH	TE)	45. (15.)*80 }*86	0.00	HAX	TINE	range Fluidit	y ibo	9C - ZN (0 _* 0	. !		DIFV.	TATION	*.		Z .	0.0
E3	* (-1/3/10	COAL	FLGAT	TED AT	1.50	S.A.)	1 1							0/00	PELL	es núme	Ŗ _,	0 _	بر نر ر	
Second	SCREEN ANAL SIZE -1/4'+ 28%	.1020	, i Polit				TYP 1 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	; 0 0	. RE	CTI TOTAL EAC EXTN	VE COMPONI L VITRINO FIVE SF. (DIO & RES REACTIVES	EXTS ID (1/2) IN	0.0 0.0 0.0	IMER IN MI FU MI	T COM ERT SE CRINO! SINDI NERGI	ONENTS (1/2) (DS (S) HATTER	0.: 0.: 0.:			
	-1/4'+ 28% -28% + 60% -60% + 0	0	.0 (.0 ().0).0).0	0.0 0.0 0.0	0.0	O. I	O O O MEAN IND	.0 1 REFL.	OF 1	REACTIVES VITRINOIDS STRENGTH :	(02)	0.00)	-		^ ,	0,60		
The state of the s	WASHABILITY (WT.Z) AND SIZE		DATE S.G.	RUN O BIRE WT.	0/00/ 0/00/ CT % ASH)0 FSI	CU ST.	i. X ASH	+/- ,1 \$.8,	i !	WASHABILI (WT.Z) AND SIZE	CTY	DATE S.G.	RUN ON DIREC WI,	0/00/0 X T: HBA	G FBI	CU:	, % ASH	t/3	
	-1/4 ⁷ +26h		1,40 1,50 1,60 1,70	0.0 0.0 0.0 0.0	VtV	,	0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0	0.0 0.0 0.0	ļ	(100.0) -1/3/+ 0		1,40 1,50 1,50 1,70	G c O	0.0		0.0000000000000000000000000000000000000	4.0	0.0 0.0 0.0	
Contract Contract	(0.0) - F -28H÷60H		1.40 1.50 1.60 1.70	0.0	0.0		0,0 6,0 0,0 0,0	0.0 0.0 0.0	0.0		FROTH GELL TEST (0.0) -28%+60%	FRO TAII	[H _1NG3	0,0 0,6	0.0 0.0		0.0 0.0	0.0 0.0		-
	(0.0) =	ank .	1.30 1.40 1.50 1.60 1.70	0,0 0,0 0,0 0,0	0.0000000000000000000000000000000000000		0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0		FRC(H CELL TEST (0.0) -60m + 0	FROI TAIL	H Mos ·	0.0 0.0	9,0		0.0	0.0 6.0		•
-	Notes:			•					,					` .		·				·

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	BRILL HOL VERTICAL	E; EVI THICX	30 NESS	(CORE 6.22	) SE RIF REC	AM 4.8 AMGLE EIVED:	00/00/ HH BD	25 L 00 E YY C	NTERCEPT ATITUDE EIGHT OXPOSITE	20 55• :	11.49- 2 14736.970 0.00	57.71 M KG	INTEP DEPARTU VOISTURI RECOVER	THICK	XESS 59471 7	6,22 ,970 % ),0 %	TRUE ELEV COMP	•	09/ HH	5.64 76.510 99/00 90 YY	
8///	PROXIMAT	F MA	LÝSTS	CORY 3	42121									~~~~				E SUN	00/00	/00	- <del></del>
	Z OF 1/8 ASH Z V.H. Z F.G. Z F.S.I. Z TOTAL S Z.P205 (A	M O		10 2- 1, 55 2	0.00 4.50 6.10 7.40	73,60 7,70 17,20 73,10 5	1 57 1 70 1 84 1 71 1 80	ART SION X FLU MAL FI LIDIF	TEMP. ID TEMP. LUID TEM ICATION RANGE	o. Tenf	DATE RUI OC OC OC OC OC A M	419.0 450.0 459.0 469.0		TI TIII TIII	- Befi - Kaxi - Maxi Coni	. TERP. COHTRA DULATA RACTION	CTICH TION TO	m,	00 00 74	470.0° -14.0	
	Z. P205. (A GROSS CAL	ijošeki Vali	ATE) IF ATU	/t 8	0.00.	0.00 7918.	1. HA	KUHIX	FLUISIT	1 90	/X	1.6	i		Day.N	<u>11</u> 11.12% :		•		-16.0 	<i>=</i> -
	GROSS CAL V.H. Z (C * (-1/8'+	ήF)	,		1.50												<b>Ξ</b> R	0 <	-		-
Screen W	SCREEN AN	MLYSI	. / PGA		isn ti	Y 17873	V			- n - 1	VE COMPON L VITRING TIVE SF. GID & RES REACTIVES	777	. 31 4	71	ERT S CRINO ISINOI NERAL	F. (1/2) IBS	3. 6. 4.	2			
	=28M + 60 -60M + 0	. 10	).5 1	3.8 10	0.0	23.7	i ma				4 - 4 % (16H1) H		1 7.2	3			-				•-
1				·											: COK	e Stab.	INDEX	59.60	)	· · · · · · · · · · · · · · · · · · ·	-
	WASHABILI (WT.Z) AND SIZE	ſΥ	DATE S.G.	RUN O DIRE ST.	0/00/ CT % ASH	'00 FSI	CU Wi.	H, X ASH	∜- ;í 8,6,	1	WASHABIL (WY.X) AND SIZE	ITY .	BATE.	RUN Q DIRE WI.	0/00/4 CT X ASH	)) F3I	CM Mi	A. X ASH	1/- 3,	6.	
	WASHABILI (WI.Z) AND SIZE (77,7) -1/4'+28H	FLT	1.30 1.40 1.50 1.60 1.70	16.7 44,9 12,7 4,11 26,3	12.6 12.7 12.7 12.7 12.7 12.7 77.6	7-1/2 1-1/2 1 1 1 1 1 1 1 1	16.7 61.6 74.3 76.6 79.7 100.0	\$25.7.7.0 10.7.7.0 12.7.0.1 12.7.0.1	77.3 72.5 21.3 6.5		(100.0) -1/8/f 0	FL1 SIX	1.30 1.40 1.50 1.60 1.70	23,7 33,9 17,2 6,5 1,5 20,2	13.6 13.6 25.6 35.6 80.5	7-1/2 1 1 200	23,7 54.6 71.8 73.3 73.8 100.0	21.03.03.03.44.14.03.13.13.13.13	48 40 29 10	.7	-
	( 11,8) -28N+60M	SINK	1.30 1.40 1.50 1.60 1.70	25,0 25,5 25,7 25,7 2,3	1,5 5,3	7-1/2 6-1/2 1-1/2	200000 200000 2000000 2000000	11.00.00.00.00.00.00.00.00.00.00.00.00.0	60.7 62.1 36.7 10.0		FROTH CELL TEST ( 11.8) -28X+69H	FR	oth Ilingg		-	-		•			<b>.</b>
5 BWWW.	( 10,5) -60H 0	FLT.	1.30 1.40 1.50 1.70 1.70	0.0 0.0 0.0 0.0 0.0	0.00000		- 0*0 - 0*0 - 0*0	0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0	] { [   (	FROTH CELL TEST ( 10.5) -60% + 0	- FR(	oth Ilinge	75c3 4.7	13:1 71:5	ć 110	75.3 100.0	13.6			٠,
<u>g</u> -	vare								<del>-</del>					·							

-	DRILL HOLE: EVISO ( VERTICAL THICKNESS	CORE ) SEAM I.S 4.39 DIP ANGLE RECEIVED: CO	INTERCEPT 2 26 LATITUDE X /00/00 WEIGHT DO YY COMPOSITE:	277.77- 282.16 INTERT G46736.970 M DEPARTUR 0.00 K3 KSISTURE RECOVERY	THICKNESS +,37 E 657671,970 M 0,0 X 68.1 Z	TRUE THICKNESS 3.95 N ELEVATION 1350.730 H COMPLETE: 00/00/00 HH EE YY
	PROXINATE ANALYSIS	(DRY BASIS)       RAU	GTESELER PLASTICIT	7, DATE RUN 00/00/00	DILATATION (RUHR)	PATE RUN CO/CO/CO
	% OF 1/3' % C ASH % V.H. % F.C. %	100,00 64,60 i 32,60 6,60 l 15,20 18,10 l 52,20 73,10 l	START FUSION TEMP, HAX FLUID TEMP, FIMAL FLUID TEMP, BOUTOTETCATION TEM	OC 411.0   OC 411.0   OC 427.0   OC 466.0   OC 463.0   OC 493.0   OC 483.0   OC 473.0   OC 43.0   OC 43.0   OC 45.0   OC 45.0   OC 45.0   OC 45.0   OD/M 23.9	TI - SEFT. TEXT.  TII - SAX, CONTRACT  TIII - BAX, DILATAT	00 421.0 TION TESP, 00 404.0 TON TESP, 00 404.0
£.)§	Z TOTAL SULF. Z P205 (PHESPHATE)	0.39 0.51	KELTING RANGE HAXIHUM FLUIDTTY I	00 45.0 1 00/H 23.9 1	DILATATION	7 -12.0
Second of the second	GROSS CAL, VALUE BTU/ V.M. % (DAF) % (-1/8'+0 COAL FLCAT	LB 0, 7982. 1 22.6 ED AT 1.50 5.6.) 1	PETROGRAPHIC BATA	DATE COMPLETED 90/0	9/00 PELLET NÜNBE	R 4557
and the same	SCREEN ANALYSIS (COME	CRUSHED TO 1/4')	V-IVPES REACT TYPE % TO 12 066 RE/ 13 12.1 EX 14 26.5	DATE COMPLETED 00/0  [IVE COMPONENTS  [AL VITRINOID 35.2  ACTIVE SF. (1/2) 16.5  HOUD & RESIN 0.0  REACTIVES 71.7  VITRINOIDS (RO) 1.4	INERT LUBFORERIS INERT SF. (1/2) MICRIMOIDS FUSINGIDS HINERAL MATTER	16.5 4.3 2.7 5.0
(Co)	-1/4' + 288 84.6 32 -286 + 606 8.7 15 -606 + 6 6.7 15	1.5 84.6 32.5   1.5 93.3 30.9   1.4 100.0 29.9	15 16.0 101m 0 0.0 0 0.5 MAX. MEAN REFL. OF BAL. INDEX 2.06	VITRINOIDS (RO) 1.4 STRENGTH INDEX 6.6	PRED. COKE STAB.	INDEX 57.20
and particular						
	(WT.Z) S.G. AND SIZE	DIRECT X FSI "	CUH. % 1/- /1   WT, AEK S.G.	WASHABILITY DATE (WT.X) S.B. AND SIZE	DIRECT Z FSI WT. ASH	EUH. X +/1 BT. ASH S.G.
1227-44	(84.6) FLT, 1.30 -1/4'128N 1.40 1.30	10.2 3.4 7-1/2 33.1 9:3 1-1/2 14.5 13.1 1 6.5 29.5 1	10,2 3,4 63,7 43,3 7,9 70,2 157,8 10,5 31,0 14,7 14,7	(100,0) FLT. 1.30 -1/8'10' 1.50 1.50 1.70 SINK 1.70'	16.5 1.9 · 7-1/2 24.4 6.6 6 ·20.2 13.4 ·1 6.7 23.3 1	16.5 1.7 56.7 40.9 4.7 61.9 61.1 7.6 37.3 67.6 9.1 15.3
	31MK 1.70	3.5 36.4 1 32.2 72.2 NC	67,3 13,6 100,0 32,5 / 1	1.70 SINK 1.70	4.3 36.0 1 27.9 75.2 HC	72.1 10.7 100.0 28.7
	( 8.7) - FLT, 1.36 -26H+60H 1.40 1.59 1.60	27.5 1.5 7-1/2 35.6 3.5 5-1/2	27.5 1.6 71.8 6 62.1 3.8 40.6 1 80.8 5.9 20.9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	FROTH CELL TEST ( 8.7) FROTH	0.0 0.0	0.0 0.0
	1.70 SINK 1.70	2,0 37,7 1 12,1 71,1 MC	97,7 7,8 1 100,0 15,5 !	-20H+40% TATLINGS	0.01,0.0	
- CO	( 6.7) FLT. 1.30 -60Nf 0 1.40	0.0 0.0	0.0 0.0 0.0 l	FROTH CELL TEST		
	1,50 1,60 1,70	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	( 6.7) FROTH -60X + 0 TAXLINES	94.8 12.8 5 3.2 63.7 NC	94.8 (2.8 100.0 15.4
<b>.</b>	NOTES:					

	RILL HOLE: JERTICAL T	HICKNE	.83	ORE :	DIP RECE	II #3L ANOLE IVED:	00/00/0 HH DD	10 WE	ich! XPOSITE:	•	736.970   0.00	RECOVER	RE 65 E	7471.1 0 50	970 X ≥ .0 Z .5 Z	- CONFL	E!!! •	E93 2.4 1343.15 00/00/00 HSI 93 YY	
	% GF 1/8' ASH X V.H. % F.C. X F.S.I. % TOTAL SU % P205 (PH GROSS CAL. V.M. % (DA % (-1/8'+0 SCREEN AND SIZE -1/4'+ 28M	K G LF, COSPHAT VALUE F) COAL LYSIS	E) BTU/L FLOATE (CONL Z AS:	SOFT 100 144 175 2 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	.00 .10 .90 .37 .00 .38	CLERI 61.30 7.90 19.20 72.90 4-1/2 0.00 795. 20.6	. 1 V-	TYPES E % 1	REAM TOTAL	HIW	DATE RUN  OC  OC  OC  OC  OC  OC  OC  OC  I  DATE COMPONE  VITRINO  IVE SF.  ID & RES	00/00/00   1   412.0   1   412.0   1   453.0   1   455.0   1   50.0   1   50.1   1   1   1   1   1   1   1   1   1	INER IN FU FU TOTA	T CONF ERT OF CRINOI SINOI NERAL L INEF	CERENTS (1/2) IDS IS	13 3 4		0/46/90 23.0 472.0 478.0 2 5.0 2 10.0	
	-28% 1 60M -60M 1 0 WASHABILIT (WT.X) AND SIZE (77.3) -1/4/128H	13, 9,		NUN ON DIRECT UT.	0,00/ 0/00/ 0/ Z 0.00	00 FSI	I HAW I BAL BU WI.	HEAN INDI M. Z ASH	1 REFL. ( EX 1.3 +/1 3.8.	7 S	TRINGIDS TREMOTH ) (WT.Z) WD SIZE (100.0) 1/8'+ 0	(RO) 1; (HDEX 6. (TY DATE S.O) -FLT. 1.3(	RUN 0 DIREI 97.3	. COKE 0/00/( CT Z ASH 1:9	7-1/2	CU: %T. 27.3 53.5	1.7 1.7	1/1 5.5. 60.3 53.6	
	3	-	1.50 1.60 1.70	13.6 4.0 1.3	18.6 28.6 36.5 11.7	1	79,7 83,7	7,7 10,6 11,0	20,9 6,2	!		1.50 1.60	) 20,8 ) 6,7 ) 1,0	14,7 30,7	5-1/2 1 No	77.3 85.0 87.0 90.0	7,2 7,0 9,4	20,4 7,9	
Control Control	( 13.2) -26M±60H		1,40 1,50 1,60 1,70	46.73	1,61 7,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17,13 17	7-1/2 6-1/2 1-1/2 1 1 NC	16.9 79.2 90.3 92.6 100.0	3,8 5,5	84.4 46.3 14.3 3.7	1 (	ROTH ELL TEST 13.2) 28X+60X	FROTH TAILDIGS	0.0		, ,	0.0 0.0	0+0 0+0	· · · · · ·	··
	( 9.5) -60#+ 0	FLT.	1.60 1.70	0.0 0.0 0.0 0.0	0.0	·.	0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0	.: 0	ROTH 511 TEST 9.57 40% + 6	FROTH TAILINGS		8.3 10.8	5 NC	73,7 100,0	, co.co.		

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DRILL HOLE: EVISO (CORE ) SEAN VERTICAL THICKNESS 0.77 RIP ANGLE RECEIVED:	INTERCEPT 289.94- 290,73 INTERT THICKNESS 0,79 TRUE THICKNESS 0,70 27 LATITUDE 5046736.970 H DEPARTURE 659471.970 H ELEVATION 1333.060 000/00/00 WEIGHT 0.00 KB HDISTURE 0.0 % COMPLETE: 00/00/00 HX DD YY CCHPOSINE: RECOVERY 46.2 % HY DD YY
PROXIMATE MINLYSTS (DRY BASIS)	GIESELER PLASTICITY, DATE RUN 00/00/00   DILATATION (RUHR)   DATE RUN 00/00/00
ASH Z 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	GIESELER PLASTICITY, DATE RUN 00/00/00   DILATATION (RUHR) DATE RUN 00/00/00    START
X TOTAL SULF, 0.00 0.00 X P205 (PHOSPHATE) 0.00 0.00 ST GROSS CAL VALUE RIVING 0. 0.	SOLIDIFICATION TEMP. CC 0.0 I CONTRACTION % 0.0 I HELTING RANGE DC 0.0 I DILATATION % 0.0 I HAXIMUM FLUIDITY DO/N . I
V.H. X (BAF) 0.0	FETROGRAPHIC DATA DATE COMPLETED 00/00/00 PELLET NUMBER 0
SCREEN ANALYSIS (COAL CRUSHED TO 1/4')  CUMULATIVE  SIZE WT.Z ASHZ WT.Z ASHZ	FETROGRAPHIC DATA DATE COMPLETED 00/G0/00 PELLET NUMBER 0  U-TYPES REACTIVE COMPONENTS INERT COMPONENTS I TYPE X TOTAL VITRINGID 0.0 INERT SF. (1/2) 0.0 I 0 0.0 REACTIVE SF. (1/2) 0.0 MICRINGIDS 0.0 I 0 0.0 EXINGID & RESIN 0.0 FUSINGIDS 0.0 I 0 0.0 TOTAL REACTIVES 0.0 TOTAL INERTS 0.0 I 0 0.0 I 0 0.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.0 I 6.
=28m + 36m 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	O 0.0 O 0.0 I MAX. MEAN REFL. OF VITRINDIDS (RD) 0.00 I BAL. INCEX 0.00 STRENGTH INDEX 0.00 PRED. COKE STAB. INDEX 0.00
WASHABILITY DATE RUN 00/00/00 (WT.Z) S.G. DIRECT Z FSI AND SIZE WT. ASH	CUH, Z +/- i1 ! (W1.Z) S.S. BIRECT Z FSI CUH, Z 1/- i1 W1. ACH S.S. AND SIZE W1. ASH WI. ASH S.S.
1.40 0.0 0.0 0.0 0.0 0.0 0.0 1.40 0.0 0.0 0.0 1.50 0.0 0.0 0.0 1.60 0.0 0.0 0.0 1.70 0.0 0.0 0.0 SINK 1.70 0.0 0.0 0.0	0.6 0.0 0.0   (100.0) FLT. 1.30 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
( 0.0) Fit. 1,30 0.0 0.0	0.0 C.6 0.0   FROTH 0.0 0.0 0.0   CELL TEST 0.0 0.0 0.0   CO.0   FROTH 0.0 0.0 0.0 0.0 0.0 0.0   -28H&CM TAILINGS 0.0 0.0 0.0
( 0.0) FLT. 1.30	0.0 0.0 0.0   FROTH
MOTES:	

	DRILL HOLE VERTICAL 1	EV15	0 ( E85	(CDRE 0.55	DIP A RECEI	i WCLE (VED) (	2 20/00/0 #K DD Y	TRI 7 LA 10 MED Y COM	FERCEPT, FITUDE ISHT #POSITE	293 3546	.35- 29 736.970 0,00	93,90 H K6	INICPT DEPARTUR HOISTURE RECOVERY	THICKNE E 659	83 471,97 0,0	0.55 9 X X	TRUE 1 ELEVA COMPLE	HICKN TGN TE:	ESS 0 1334. 00/00/: Hn DD	650 K 00
	PROXINATE  Z OF 1/8' ASH Z V.M. Z F.C. Z	AMAL	YSIS (	IDRY BA RA 100 13 13 68	SIS). # #0 .00 6 .00 .60 1	LEAN 87+50 8.30 19.70	GIES GIA GIA GIA GIA GIA GIA GIA GIA GIA GIA	ELER I RT ION TE FLUTT YL FLU	YLASTIC TMP. D TEMP. NIS TEMP	177,	00 00 00 00 00 00 00 00	412. 434. 434. 469.	0 [:	DILATAT	ION (R SOFT, KAX, D NAX, D	CHR) TEKP DATRAC TLATAT	DATE TION TE TON TER			0
Carrier Carrier	V.M. X (DE * (-1/8'+0 SCREEN ANA	VALU F) CBAL LYSIS	FLOAT (COAL	ED AT :	L.50 S	733. (1,4) (.6.)	PETRI V-1 TYPI	JGRAPI TYPES Z	IIC BAIY	CYIVE OTAL EACT	DATE COMPON VITRING	OHPLE VENTS VID (1/2	TED 00/0	O/OO   INERT INE HICH EUS	PELLET COMPO RT SF. RINGID	NEMBE NEMTS (1/2) S	1354 11.3 1.8 4.3			
	F.S.I. Z TOTAL SI Z P205 (PI GROSS CAL. V.H. Z (PI * (-1/8'+0  SCREEN ANA SIZE -1/4'+ 28N -28M + 66N -50M + 0  WASHABILIT (UT.Z) AND SIZE	1 0 0 0	.X AS	HZ W	0.0 0.0 0.0 0.0	SHZ 0.0 0.0 0.0	13 14 15 16 16 182 184	10. 36. 17. 0. NEAN INSE	0 0	AL RE	ACTIVES TRINOIS RENGTH	is (Re Inde	77.9 3) 1.44 6.5	MINE COTAL PRED.	RAL M INERT	ATTER S STAB.	1.7 22.1 0952	61.60		
Andrea . Prophets	WASHABILIT (WT.Z) AND S(ZE	Y	DATE S.G.	RUN OG DIREC WT.	)/90/6 T Z ASH	FSI	CUI VII.	ASH	1/- ,1 8,6,	15	MSHADIL (WT,Z) MG SIZE	TIY.	DATE S.G.	RUN 00. DIRECT	/00/00   Z   ASH	FSI	CUH NT.	, % 46K	+/1 5.6. 66.5	· · · · · ·
	WASHABILIT (WT.Z) AND SIZE ( 0.6) -1/4'+28H	SINK	1.40 1.50 1.60 1.70	0.0 0.0 0.0	0.0	·	0.0 0.0 0.0	0.0	0.0		1/8/+ 0	SI	1.40 1.30 1.50 1.70 1.70	24.5 24.5 24.5 1.5 4.0 6	7.0 6.4 17.3 17.3	) 2 10	27,8 63,8 88,3 94,5 96,0	7.7	32:0 8:0	
Acres (Control	( 0.0) -28M+60N	FLT.	1.30	0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0	•	0.0	0.0 0.0 0.0 0.0	0.0 0.0 0.0		ROTH ELL TES 0.0) 28H+60H	T F	ROTH AILINGS	0.0		-		9.0		
	( 0.0) -60ñi 0	FLT: SINK	1.40 1.50 1.60 1.70	0.0 0.0 0.0	0.0		0.0	0.0 0.0 0.0	0.0 0.0 0.0	1 6	HTOR ELL TES (0,0 0 + KOE	F	ruth Ailines .	0.0	0.0 0.0	`	0.0	0.0 0.0		
تنت							,						•							

· NOTES:

	PRILL HOLE:	EV15 HICKN	) (I ESS	CORE :	) SEA) DIP : RECEJ	i ii MOLE (VED:	00/00/ NN DD	26 L 26 L 20 N	HTERCE ATITUD EIGHT CHPOSI	PT 29 E 35 TE:	77,04- 27 46738,970 0,00	7.80 (1) M DEP KG MDI REC	XICPT ARTURE STURE OVERY	AT THICKN	FSS 9471.5 0, 73.	0,78 70 H 0 K 0 Z	TAME ELEVA COMPLI	THICKNE TION ETE:	33 0.48 1330.940 90/96/00 HH DD YY	H.
	PROXIMATE  Z OF 1/8' ASH Z V.H. Z V.H. Z F.C. Z F.S.I. Z TOTAL SU Z P205 (PH	ANAL X O LF. OSPHA VALUE	(E) E BTU/I	ORY BAI 100 14 18 66 3-1 0	515) 4,00 40 1,40 1,40 1,40 1,48 1,48 1,48 1,48 1,48 1,48 1,48 1,48	CLEAN 55.30 7.60 21.70 70.70 0.53 0.00		ART SION X FLU NAL F LIDIF LIING XINUN	TEMP, ID TEM LUID TH ICATION RANGE FLUID	P. EMP. Y TEHI	OC OC OC OC	387.0 413.0 457.0 457.0 491.0 494.0 78.0 792.4	00 (04	VOO	SOFT. MAX. HAX. CONTR DILAT	TEMP. CONTRAC DILATA  ACTION ATION	TION TO	Rum VI	392.0 430.0 483.0 22.0 129.0	-
	SIZE -1/4 + 28H -28H + 60H -60H + 0	LYSIS WT O O	Z ASI 0 0 0 0	CRUSHI CRUSHI HZ UI 0 (0	ED TO UNULAT I.Z. A O.O O.O O.O	1/4') NIVE NSHX 0.0 0.0 0.0	A	7E 12 34 00 X	7 1.2 3.6 2.0 4.8 0.0 0.0 AN REFL	TOTAL.	AL VITRINO CTIVE SF, NUID & RES REACTIVES VITRINOID	ID (1/2) 1 IN	11.6 12.8 0.0 74.4	INI HIO FUI MIN TOTAL	ET SF RINGI SINGIO VERAL INER	(1/2) ES S WATTER TS	12.7 2.5 5.7 25.7	ZA 20		
	WASHABILIT (WT.Z) AND SIZE	Y	DATE :	RUN OC DIREC WT:	0/00/0 X T. Hea	)0 FSI	 	UH. Z . AS	+/ H S.(	1 1 3, 1	Washabil (WT.%) AND SIZE	ïiā	DAYE F	ON O DIREC ST.	0/00/0 T % ASH	FSI	 EUX	17 % ASH	:/1 5.6.	-
	( 0,0) -1/4' +28H	FLT. SINK	1.30 1.40 1.50 1.60 1.70	0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0		. 0; 0; 0;	0 0; 0 0; 0 0;	0 · 0; 0 · 0; 0 · 0; 0 · 0;	0	(100.0) -1/8/+ 0	FLT. SINK	1.30 1.40 1.50 1.60 1.70	25,8 35,8 20,5 8,0 3,7 6,2	1,2 6,2 14,5 27,0 37,6 65,1	7-1/2 7 2 1 1 NC	23.8 61.6. 92.1 73.3 100.0	4,1 4,1 6,7 8,5 9,7 13,2	65.7 69.0 39.4 12.5	-
1	( 0.0) -28##60H	FLT.	1,30	0.0 0.0	0.0		Q. 0.	0 0.0	0 0, 0 0,	1 0 1	FROTH CELL TEST ( 0.0) -28HF40H	ר ב דהפיד					•			- -
	( 0.0) -60H 0	FLT.	1,40 1,50 1,60	0*0 0*0 0*0.	000000000000000000000000000000000000000		0.	0 0.0	0 0, 0 0, 0 0,	0 1	FROTH CELL TEST ( 0.0) -60% + 0	r Frot	H INGS	0.0 0.0	0.0 0.0	. , , , , , , , , , , , , , , , , , , ,	0.0	0.0 0.0		
₹!}-											, ,					·				, ,

 NOTES:	1.70 0.0 0.0	0.0 0.0	) ]					
	1,40	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0	FROTH CELL TEST ( 0.0) -60% + 0	FROTH 0.0 TAILINGS 0.0	0.0	0.0 0.0 0.0 0.0	
	1.10 0,0 0,0 1.50 0.0 0,0 1.60 0,0 0,0 1.70 0.0 0.0	6.6 6.6	6 5.6 1	( 0.0)	FROTH 0.0 TAILINGS 0.0	0.0	0.0 0.0 0.0 0.0	
( 0.0) FLT, -1/4/†28H	1.30 0.0 0.0 1.40 0.0 0.0 1.50 0.0 0.0 1.50 0.0 0.0 1.70 0.0 0.0 1.70 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0 0.0 I	(100,0) ( -1/8'+ 0	FLT. 1.30 37.1 1.40 30.3 1.50 10.1 1.60 4.2 1.70 2.3 HMK 1.70 13.7	2.1 7 5.6 5 7 14.7 1 29.1 1 3 42.2 1 75.8 XC	37.0 2.1 69.3 3.6 77.3 5.1 84.0 6.3 96.3 7.2 100.0 16.6	99.3 47.3 17.0 7.5
WASHABILITY (WI,X) AND SIZE	DATE RUN 00/00/00 S.G. DIRECT % FS WT. ASH	i Cuk. Z Wi. As	;/-,i ;/-,i ; ;, 6,6	WASHABILITY (WT.Z) AND SIZE	DATE RUA S.S. DIRI HT	00/00/00 CT % FSI ASH	CUM, Z Wi. ASH	1/- 11 5.6.
71/4 + 28% 0, -28% + 60% 0, -60% + 0 0,	FLOATED AT 1.50 S.G.  FLOATED AT 1.50 S.G.  (COAL CRUSHED TO 1/4  CUMULATIVE Z ASHZ WT.Z ASHZ 0 0.0 0.0 0.0 0 0.0 0.0 0.0	13 14 0 1 MAX. ME 1 BAL. IN	1.7 TOTAL 0.6 0.0 AN REFL. OF DEX 0.83	NEACTIVES VITRINOIDS (STRENGTH IND	76.3 101 RO) 1.13 EX 4.39 PRE	AL INERTS U. COKE STAB. I	23.7 NDEX 60.30	
SCREEN ANALYSIS	COAL CRUSHED TO 1/4  CUMULATIVE Z ASHZ NT Z ASHZ	V-TYFE 1 10 2 1 11 3	REACT X 107 10,7 REA 14,1 EXI 5,7	IVE COMPONENT AL VITRINOID CTIVE SF, (1/) NOID 1 RESIN	S INE 63.2 I I I I I I I I I I I I I I I I I I I	KT COMPONENTS HERT SF. (1/2) TORONOIDS USINOIDS INFEAL HATTER	12.3 1.7 6.2 3.5	
 % P205 (PHOSPHAT GROSS CAL, VALUE V.N. % (GAF) * (-178'+0 CGAL	TE) 0.00 0.0 E BTU/LB 7750, 8054 28,2 FLGATED AT 1.50 S.6.	HAXIMUR PETROGRA	PHIC DATA	D/H, 9.8 DATE COMPL	ETED 00/00/00	FELLET NUMBER	1557	
X OF 1/8' X O ASH X V.N. X F.C. X F.S.I. X TOTAL SH'F.	YSIS (DRY BASIS)  RAW *CLEA 100.00 51.1 17.70 6.1 23.20 23.3 59.10 68.6 6-1/2 6-1/ 0.53 0.5 TE) 0.00 0.0 E BTU/LB 7750, 8056 7750, 8056 7160 85.6	)   START   FUSION   I - HAX FLL   I FINAL F   SOLIDIF	TEMP. UID TEMP. LUIB TEMP. FICATION TEM B SONGE	00 406 00 430 00 458 00 466 00 467 00 487	3.0   TI 3.0   TIT 3.0   TIT 3.0   TIT	- SOFT, TEMP, - HAX, CONTRACT - HAX, CILATAT CONTRACTION DITATATION	TICH TEHP. O	C 413.0 C 455.0 C 455.0 Z 12.0
PROXIMATE SHAL	YSIS (DRY BASIS) RAW *CLEA	ÇIEŞELEJ	R PLASTICIȚ	', DATE RUN CO	Noovoo'i bit'v	ATJOH (RUHR)	BATE RUH 0	0/00/00
ERILL HOLE: EVIS VERTICAL THICKN	1 (CORE ) SEAM B. ESS 4.35 DIF AND RECEIVED	27 00/00/00 HN 00 YY	intercept Latitude (2 Weight Confosite:	7,29-11,4 544674,130 H 0,00 KB	U INTOPT THICE OFFARTURE HOISTURE RECOVERY	GNESS 4.36 559152.135 H 0.6 % 42.7 X	TAVE THICKS ELEVATION CONFLETE:	ES3 3.65 H 1611.670 H 00/00/00 HX DD YY

		27 LATITUGE 5546676,130 H GEPARTURE 659152,130 H ELEVATION 1602,150 H 50/00/00 USIGHT 0.00 KG MOISTURE 0.0 % COMPLETE: CO/OG/OO HH OD YY COMPOSITE: RECOVERY 41.9 % HH DD YY
Ì	PROXINATE ANALYSIS (DRY SASIS)	1 GIESELER PLASTICITY: DATE RUN 00/00/00   DILATATION (RUHR)   DATE RUN 00/00/00
	Z OF 1/8' X O 100.00 35.00 ASH Z 50.60 8.50 V.H. X 16.10 25.70 E.C. Z 33.10 65.60 F.S.Y. 5-1/2 7 Z TOTAL SULF. 2.000 0.00 0.00	STAKT
zinie.	GROSS CAL. VALUE STU/LB 0. 7701. V.H. X (DAF) 32.7 * (-1/8/10 COAL FLOATED AT 1.50 S.G.)	PETROGRAPHIC DATA DATE COMPLETED 00/00/00 PELLET MUNGER 1540
Section 8	SCREEN ANALYSIS (COAL CRUSHED TO 1/4')  CUMULATIVE SIZE WINX ASHX WINX ASHX	- V-TYPES REACTIVE COMPONENTS INERT COMPONENTS I TYPE Z TOTAL VITRINOID 67.1 INERT SF, (1/2) 10.5 I 9 1.3 REACTIVE SF, (1/2) 10.7 MICRINOIDS 2.7 I 10 18.5 EXYNOID & REBIN 6.3 FUSINGIDS 3.8 I 11 39.3 I 12 6.0 TOTAL REACTIVES 78.1 TOTAL INERTS 21.7 I 13 2.0 I 0 6.0
	-1/4'+ 28M 0.0 0.0 0.0 0.0 0.0 -0 0.0 -28H + 60H 0.0 0.0 0.0 0.0 0.0 0.0 0.0	1 12 6.0 TOTAL REACTIVES 78.1 TOTAL INERTS 21.7 1 13 2.0 1 0 C.C 1 HAX. MEAH REFL. OF VITRINGIBS (RO) 1.13 1 BAL. INDEX 0.75 STRENGTH INDEX 4.37 PRED. COKE STAB. INDEX 59.80
Carried St.	UASHABILITY DATE RUN 00/00/00 (WT.Z) S.G. DIRECT Z FSI AND SIZE WT. ASH	CUH, Z +/- ,1   (WT.Z)
	( 0.0) FLT, 1.30	0.0 0.0 0.0   (100.0) FLT. 1.30 15.0 2.7 7-1/2 15.0 2.7 61.7 0.0 0.0 0.0   -1/8'+ 0 1.40 31.3 7.7 7 26.3 4.8 43.1 0.0 0.0 0.0   1.50 7.0 15.0 4-1/2 33.3 7.0 25.7 0.0 0.0 0.0   1.60 4.0 24.1 3 37.3 3.8 21.5 0.9 0.0 0.0   1.70 5.2 41.7 1 42.5 12.8 0.0 0.0 0.0   SINK 1.70 57.5 81.7 NC 100.0 52.5
	( 0.0) FLT. 1.30 0.0 0.0	
	( 0.0) FLT, 1.30 0.0 0.0 -60Hf 0 1.40 0.0 0.0 1.50 0.0 0.0 1.60 0.0 0.0 1.70 0.0 0.0 SINK 1.70 0.0 0.0	0.3 0.0 0.0   FROTH 0.0 0.0 0.0   CELL TEST G.0 0.0 0.0   0.0   0.0 0.0 0.0   0.0 FROTH 0.0 0.0 0.0 0.0 0.0 0.0 0.0   -40M   0 TAILINSS 0.0 0.0 0.0 0.0
-16	, NOTES:	

	DRILL HOLE: EVISI (CORE ) SEAM INTERCEPT 29,27- 30,18 INTERT THICKNESS 0,71 TRUE THICKNESS 0 VERTICAL THICKNESS 0,71 DIP ANGLE 27 LATITUDE 3348076,130 H DEPARTURE 639132,130 H ELEVATION 1387. RECEIVED: 00/00/00 WEIGHT 0,00 KB MGISTURE 0,00 X COMPLETE: 00/00/ NH DD YY COMPOSITE: RECOVERY 100.0 X NH DB	650 K 660 K 77
Ì	/	
	PROXIMATE ANALYSIS (ORY BASIS) RAW *CLEAN  X OF 1/8' X O 100.00 72.10   START OC 308.0   TI - SOFT. TEMP. OC 373  ASH X 21.80 7.60   FUSION TEMP. OC 416.0   TII - HAX. CONTRACTION TEMP. OC 434  V.N. X 21.20 25.10   HAX FULID TEMP. OC 452.0   TIII - HAX. DILATATION TEMP. OC 473  F.C. X 55.00 67.30   FINAL FULID TEMP. OC 482.0    F.S.I. 6 7-1/2   SOLIDIFICATION TEMP. OC 487.0   CONTRACTION X 24  X TOTAL SULF. 0.72 0.94   NELITAD RAMSE OC 66.0   DILATATION X 24  X P203 (PHOSPHATE) 0.00 0.00   NAXIHUM FUNIDITY BD/M 463.4    GROSS CAL, VALUE BIU/LB 0.8056.	0.0
44.55.22	V.H. Z (DGE) 2718 1 PETROBRAPHIC DATA RATE COMPLETED 00/00/00 PELLET HURSER 0	
	* (-1/8'+0 COAL FLOATED AT 1.50 S.G.)  V-TYPES REACTIVE COMPONENTS INERT COMPONENTS  SCREEN ANALYSIS (COAL CRUSHED TO 1/4')   TYPE	
1		
	WASHABILITY DATE RUN 00/00/00 I WASHABILITY DATE RUN 00/00/00  TO (WT.Z) S.G. DIRECT Z F31 CUM. Z 4/- 11 (WT.Z) S.G. DIRECT Z F31 CUM. Z 4/- 11 AND SIZE WT. ASH 91. ASH 5.9.	, -{: , :
	( 0.0) FLT, 1.30	
	( 0.0) FLT. 1.30	
	( 0.0) FLT. 1.30	
<b>23</b>	inter:	

	DRILL HOLE: EV VERTICAL THIC	isi (C XXESS	ORE ) SEAM 0.28 DTF ANGLE RECEIVED	27 L 99/09/00 - H HN BD YY C	NTERCEPT ATITUCE S EIGHT CHPOSITE:	35,24- 35 546876,130 H 0,00 K	.52 INTERT 1 DEPARTURE G MOISTURE RECOVERY	THICKNESS 637152. 0 0	0.28 II 130 H E .0 X CI	NE THICKS	ESS 0.23 H 1363.920 H 00/90/00 1H 00 YY
	EXEMPTER VET 410	*** ****** * ***	NV ELNIAL	2 STEATER		U 0475 0111	AA 443 454 1 1	TITL ITTI PTMIT	/EXITES 1		
	A OF 1/5 A S ASH X V.M. X F.C. X F.S.I. X TOTAL SULF. X F205 (PHGSP GROSS CAL. VA	HATE) LUE BTU/LI	RAM ≯CLEAN 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	HOISUR HOISUR HALIF HOILOS HOISUR HUNIXAN	TEMP. 10 TEMP. LUID TEMP. ICATION TEM RANGE FLUIDITY I	0C 0C 0C 0C 1P. 0C 0C	0.0	TI - BORT TITE - HAX. CONTI DILAT	COMTRACTIE BILATATICA RACTION TATION	M TEMP. I	0.0 0.0 0.0 2 0.0
	V.H. 7 (DAF) * (-1/8/10 CO	AL FLOATE	3 0, 0. 0.0 0 AT 1.50 S.G.) CRUSHED TO 1/4'	PETROGRA	PHIC DATA S PEACT	DATE CON SURGERAL SUTT	PLETED 00/00. Kts	700 FELLI TNERT COME	T HUHBER	0	
-	CT7E	OT W ADDRESS	CURULATIVE	1 0	G.O EXI	Hoto a Kest	H	FUSINOTI	90 3 VATTEO	ν.ν 6:0	
	-1/4'+ 28H -28H + 60H -60H + 0	0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0	0 ( 0 ( 1 0 (	0.0 TOTAL 3.0 3.0 AN REEL DE	REACTIVES VITRINGING	0.0	TOTAL INER	IS .	9.0	
500000			· · · · · · · · · · · · · · · · · · ·	FAL. IN	DEX 0.00	STRENGTH I	NDEX 0.00	PRED. COKE	STAB, IND	EX 0.00	
S. Constant	(UT,Z)	S.G.	DIRECT % FS Wf. ASH	I CUM. X WT. AS	+/-',1     \$.6.	(WT.X) AND SIZE	` S.G	PIRECT Z WT. ASH	FS1	CUH. X UT. ACH	*/1 \$.6.
	-1/4'+28H	1.40 1.40 1.50 1.60	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 1	(100.0) -1/8/+ 0	FLT. 1.30 1.40 1.50 1.60 1.70 SIMK 1.70	- 0.0 7.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	; ;	0.0 0.0 0.0 0.0 0.0 0.6 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0
	-28M+60M	1,30 1,40 1,50 1,50	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0	0.0	{ 0,0}	FROTH	0.0 0.0		).5 0.0°	
Section 1	31	1.70 % 1.70 .	0.0 0.0	0.0 0.0		-2811+60M	TAILINGS .	· 6.0 6.0		1.0 0.0	
	( 0.0) FLI -60Nf 0	7. 1.30 1.40 1.50	0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0	FROTH CELL TEST	eroti!	A A A A			
<b>.</b>	51?	1.40 1.50 1.60 1.70 K 1.70	0.0 0.0 0.0 0.0 0.0 0.0 ·	0.0 0.0 0.0 0.0	V.U	( 0.0) -40H f:0	FROTH TAILINGS	0.0 0.0		0.0 0.0 0.0	
	Novco+						\$ *				

. NOTES:

	DRILL HOLE; EVISI VERTICAL INICANE	CORE ) SEAN SS .0.70 DIP AND RECEIVE	LE 29 0: 00/00/60 HH DD YY	INTERCEPT LATITUCE UEIGHT COMPOSITE:	41,13- 44 5546976,130 N 0,00 N	.80 INTERT DEPARTURA G. KOISTURE RECOVERY	THICKNESS 0.70 E 657152,130 H 0.0 % 65,2 %	COMPLETE: COMPLETE: TRUE THICKN	E3S 0.61 H 1574.980 H 00/00/00 HH DO YY
) 	PROXIMATE SHALM	YSIS (DRY BASIS) RAN_ ≭CLE	GIESE	ier plastici -	TY> DATE RUN	1 00/00/00	BILATATION (RUHR)	DATE RUN C	10/00/10
	% OF 1/6' % O ASH % V.M. %	100,00 72, 20,40 8, 20,60 24,	00   STAF 70   FUSI 80   MAX	IT DN TEHP. FLUID TEHP.	6C 0C 6C	0.0 0.0	TI - SOFT, TEMP, TII - MAX, CORTRAC TIII - MAX, DILATAT	TIGN TEXP. C TON TEXP. C	IC 377.0 IC 431.0 IC 474.0
(America)	F.C. X F.S.I. X TOTAL SULF. X PROS (PHOSPHAT	SIS (DRY BASIS)  SAW *CLE 100.00 72. 20.40 8. 20.60 24. 59.00 67. 7 7-1 0.80 0. E) 0.00 6. BTU/LB 0. 786 FLOATED AT 1.50 S.6	00   FINA '2   SOLI 14   HELT 10   MAYT	L FLUID TEMP OIFICATION T ING RANGE MANA FILLERITY	00 EHP, 00 00 DE/H	0.0	TI - SOFT. TEMP. TII - MAX. CONTRACTION CONTRACTION DILATATION		7 22.0 Z 191.0
	. GROSS CAL, VALUE V.N. X (CAF)	BTU/LB 0, 786 25, SURATED AT 1.50 S.G	PETRO	GRAPHIC DATA	BATE COH	PLEYED 00/00	VOO PELLET NUHSE	R 0	
2	SCREEN ANALYSIS	COAL CRUSHED TO 1/ CUMULATIVE Z ASHZ UT.Z ASHZ C 0.0 C.0 O.	V-T Y)   TYPE	YPES REA	CTIVE COMPONEA OTAL VITRINGII EACTIVE SF. (1	VT3 S 72.9 L/2) 7.7	INERT COMPONENTS INERT SF, (1/2) HICRYMOIDS	7.7 2.3	
· ·	SIZE WT.	CUMULATIVI Z ASHZ UT.Z ASHZ C 0.0 0.0 0.1	10 11 11 12	2.1 E 16.0 : ror	XINGID & RESI A) REACTIVES	0.0	FUSINOIDS  ***********************************	5.0 10.4	
	603 + 6 0 0 ·-	0 0.0 0.0 0.0	. 13	ي د ي			PRED. COKE STAB.	_ '	
ina ke	WASHABILITY (WT.X) AND SIZE	DATE RUH 00/00/00 S.G. DIRECT % F HT. ASH	~~~~~~~~	~~~~~~~~~~					
		1.30 0.0 0.0 1.40 0.0 0.0 1.50 0.0 0.0 1.60 0.0 0.0 1.70 0.0 0.0	^ ^	40 00	1 /4 AA AA	F1 T 4 72	7/0 00 0	36.8 2.7	65.4 33.4 28.0
	) . SINK	1.30 0.0 0.0 1.70 0.0 0.0 1.70 0.0 6.0	0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0	1 -1/8/+ 0	1,40 1,70 SINK 1.70	14.2 17.2 4 9.2 28.4 2 5.5 39.7 1 16.4 61,0 NC	78.1 9.9 83.4 11.9 100.0 20.3	17.6
i i i i i i i i i i i i i i i i i i i	( 0.0)- FLT. :	1.30 0.0 0.0 1.40 0.0 0.0	0.0	0.0 0.0	I CELL TEST		•		
#1.6 #73		t.76 0.0 0.0	0.0 0.0	0.0 0.0	   ( 0.0)   -2894608	FROTH TAILINGS	0.0 0.0	0.0 0.0 0.0 0.0	
	. This	1.70 '0.0 0.0		0.0	<u> </u>	~~~~~~~~		<del></del>	
	( 0.0) FLT. 1	1.30 0.0 0.0 . 1.40 0.0 0.0 1.50 0.0 0.0	0.0	0.0 0.0 0.0 0.0 0.0 0.0	FROTH CELL TEST				
	1	1.60 0.0 0.0 1.70 6.0 0.0	0.0	0.0 0.0 0.0	(0.0 )   0 + HOA	FROTH TAILINGS	0.0 0.0	0.0 0.0 0.0 0.0	
	NOTES:	. :			·	·		-	

•	*			·		
			O YY COMPOSITE!	RECOVERY	639152.130 H 0:4 Z 25.0 %	COMPLETE: GG/99/09 HX DD YY
78000	PROXINATE ANALYSIS (	ERY BASIS)   GI	ESELER PLASTICITY,	DATE RUN 00/00/00	DILATATION (RUHR)	- DATE RUN 00/00/00
	X 07 1/8′ X 0 ASH X U.H. Y	NAW XULEAR   100.00 77.90   3 19.90 6.10   F	START USION TEHP. MAX STUTO TEMP.	00 0.0 1 00 0.0 1	II - SOFT, TEHP, III - KAX, CONTRAC	TION TEKP, OC 405.0 TION TEKP, OC 438.0 ION TEHP, OC 471.0
	Z OF 1/8' X O ASH Z V.H. X F.C. Z F.S.I. Z TOTAL SULF. Z POSS CAL UALUS BILL/	59.20 69.20   F .7-1/2 8     S 0.90 1.07   N	INAL FLUID TEMP, SOLIDIFICATION TEMP ELTING RANGE	0.0 0.0 0.0 0.0 0.0 0.0	CONTRACTION DILATATION	17.0 2 73.0
	Z P205 (PHOSPHATE)   GROSS CAL, VALUE BTU/!   V.H. Z (DAF)   k. (-1/8/+0 COAL FLOAT!	0.00 .0.00 1: 8 LR 6974, 811. [ 26.1   FE ED AT 1.50 S.G.)	TRUGRAPHIC DATA	DATE COMPLETED CO/CO.	700 PELLET WHEE	R 1561
	SCREEN ANALYSIS (COAL	CRUSHED TO 1/4')   T	V-TYPES REACTI YPE X TOTA 9 0.8 REAC 10 5.3 EXIN	VE COMPONENTS L VITRINGID 76.2 TIVE SF. (1/2) 8.1 OIO & RESIN 0.0	INERT COMPONENTS INERT SF. (1/2) MICRIMOIDS FUSINGIDS	8.0 1.4 2.7
	GROSS CAL. VALUE BIOM V.H. X (DAF) * (-1/8'+0 COAL FLOAT) SCREEN ANALYSIS (COAL SIZE WT.Z ASI -1/4'+ 2EN 0.0 0 -28M + 50M 0.0 0 -50M + 0 0.0 0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	12 34.3 TOTAL 0 0.0 0 0.0 AX, MEAN REFL. OF	REACTIVES 84.3 VITRINDIDS (RD) 1.18	TOTAL INERTS	15.7
		i . E	AL. INDEX 0.34	ŞIKERBIH INDEX, 4.48	PREB. COKE STAB. 1	INDEX 59.00
	WASHABILITY DATE F	RUH 00/00/00	CURE Z F/- 1	WASHABILITY DATE R	UH 00/00/00 DISECT V FST	in, z +/i
	( 0.0) FLT. 1.30 -1/4'+28H 1.40	0.0 0.0 0.0	0.0 0.0 0.0 1	(100.0) FLT. 1.30 -1/6'+ 0 1.40	51.0 2.1 8 14.7 8.4 8	51.0 2.1 76.7 65.7 3.5 30.9
	AND SIZE  ( 0.0) FUT. 1.30 -1/4'+28M 1.50 1.50 1.50 1.70 SINK 1.70	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	.0 0.0 0.0 I	1.20 1.60 1.70 SIMK 1.70	11.3 10.7 3-1/2 5.0 27.4 1 2.7 10.5 1 14.3 74.0 NC	77,5 5,4 20,2 63,0 7,0 7,5 85,7 8,0 100,0 17,5
Section 2	( 0.0) FLT. 1.30 -28H+60H 1.40	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	! 0.0 0.0 0. ! 0.0 0.0 0.	FROTH CELL TEST		
990	1,50 1,60 1,70 SIMK 1,70	0.0 0.0 0	0.0 0.0	( 0.0) FROTH -28H460N TAILINGS	6.0 0.0 6.0 0.0	0.0 0.0
	( 0.0) 5LT. 1.30 -50H+ 0 1.40	0'0 0'0		FROTH CELL TEST		
	-50H+ 0 1,40 1,50 1,50 1,70 1,70 SINK 1,70	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	.0 0.0 . 0.0 I	( 0.0) FROTH -40H + 0 TAILINGS	0.0 0.0	0.0 0.0
	Notest					

	DRILL HOLE: EVIS VERTICAL THICKN	1 (CORE ) SEAN ESS 0.52 DIP AN RECEIV	GLE 24 ED: 00/00/00 HH DD YY	INTERCEPT LATITURE SC UEIGHT CONFOSITE:	67,48- 70 546878,130 H 0,00 K	.00 INTEPT DEPARTURE G HOISYURE RECOVERY	THICKNESS 659152.1	0,57 TAUE 30 H ELEY 6 Z CORPL 0 X	THICKNESS 0.40 H TION 1547,489 H ETE; 00/00/00 NH DD YY
m		YSIS (DRY BASIS) RAW 3CL 0.00 C 0.00 C 0.00 0 0.00 0 0.00 0 TE) 0.00 G E BTU/LB 0. FLOATED AT 1.50 S.			<del></del>			~	
	SCREEN ANALYSIS  SIZE UT -1/4/2 28% 0 -28% + 6C% 0 -60% + 0 0	COAL ERUSHED TO 1 CUMULATI Z ASHZ UT.X ASI O 0.0 0.0 0 0 0.0 0.0 0 0 0.0 0.0 0	/4')   TYPE /4')   TYPE /6   0 /6   0 /6   0 /7   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8   0 /8	X TOT 0.0 REA 0.0 EXI 0.0 TOTAL 0.0 TOTAL 0.0 HEAR REFL: OF TNDEX 0.00	AL VITRINOI CTIVE SF, () NGID & RESIN REACTIVES VITRINOIPS SIRENOTH TO	0.0 L/2) 0.0 H 0.0 (8D) 0.00	INERT SF MICRIMOID FUSINOID HINERAL I TOTAL IMER	SERTION OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF T	
	UASHABILITY (WT.Z) AND SIZE	DATE RUN 00/00/00 S.G. DIRECT Z WI. ASH	FSI CUM.	X +/1   ASH S.G.	Washabilij (WT.Z) And Size	Y DATE R	UH 00/00/00 DIRECT % WT, ASH	FSI CUI	6 X 1/- 11 688 - 5.6.
	( 0.0) FLT. -1/4/+28K ) SINK	DATE RUN 00/00/00 S.G. DIRECT Z WT. ASH 1.30 0.0 0.0 1.40 0.0 0.0 1.50 0.0 0.0 1.50 0.0 0.0 1.70 0.0 0.0	0.0 0.0 0.0 0.0 0.0	0.0 0.0 1 0.0 0.0 1 0.0 0.0 1 0.0 0.0 1 0.0 1	(100.0) -1/8'+ 0	FLT. 1.30 1.40 1.50 1.60 1.70 SINK 1.70	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0
	( 0.0) FLT. -28H460H	1.33 0.0 0.0 1.40 0.0 0.0 1.50 0.0 0.0 1.60 0.0 0.0 1.70 0.0 0.0	0.0 · ( 0.0 · ( 0.0 · (	0.0 0.0   0.0 0.0   0.0 0.0	FROTH CELL TEST	•			0.0 3.0
	( 0.0) FLT. -60M1 0	1.30	0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 ! 0.0 0.0 ! 0.0 0.0 ! 0.0 0.0 !	FROTH CELL TEST ( 0.0) 60M t 0	FROTH TAILINGS	0.0 0.0	0.0 0.0	C ₁ O O ₁ O
## -						· · · · · · · · · · · · · · · · · · ·			

	/		CORE ) SEAN 7 3.23 DIP AND RECEIVE					E 659132	130 H 1.0 Z 1.6 Z	TRUE THICK ELEVATION CORPLETE:	1534.740 H 60/00/05 HH DO YY
	PROXIMATE	AMALYSIS	(DAY SMEIS) RAU #CLE	eies M	ELER PLASTIC	ETY, DATE RU	1 00/00/00 K	BILATATION	• •	•	***
	Z UF 1/3' ASH Z V.M. Z F.C. Z	X 6	RAW 20LE 100.00 74, 21.60 9, 21.00 22, 57.40 68, 6 362.00 0, 0.00 0,	yo i sta 30 i fus 20 i hax 30 i fin	RT ION TEMP. FLUID TEMP. AL FLUID TEM	0C 0C 6C P. 0E 1EHP. 0C Y BO/H	423.0   456.0   41.0	TI - SOFT TIII - YAX, TIII - NAX,	DIL ATATI	ION TENPA	OC - 100 K
11	/X TOTAL SU _X P205 (PE	LF, Daphate)	362.00 0. 0.00 0.	80   HEL 80   HAX	1914 ICATION TING RANGE IMUN FLUIDIT	P. DE TEHP: DC Y DD/H	492.0 58.0 175.4	COM DIL <u>A</u>	RACTION TATION		X 18.0 Z 28.0
	.GROSS CAL. .V.X. % (DA .* (-1/8/±0	VALUS BTU/ F) COAL FLOAT	/LB 7281. 745 26, 1ED AT 1.50 S.G	B PETR	uunernit, oni:	a mir o	JRPLEIE 00/0	0/00 FELL	ET HUNDES	1362	
· ·	SCREEN ANA	LYSIS (COAL	L CRUSHED TO 1/	4') ! TYP	Types Re E X 6,5 30,3	ACTIVE COMPON TOTAL VITRIM	eris Io 55.5.	INER) COM INERT 3 MICRING FUSINGI	FONENTS F. (1/2) IDS DS	13.5 4.5 7.0	
	SIZE -1/4' † 28H -26H † 60H -60H † 0	0.0 0.0 0.0 0.0 0.0	CUMULATIV GHZ UT.Z ASH 0.0 0.0 0.0 0.0 0.0 0.0	1 12 1 13 1 14 1 0	2.7 10 0.5 0.0	TAL REACTIVES	69.7	HINCRAL TOTAL INE	HATTER RTS	5.3 30.3	
,	garagan Tanggan			i Bar	. INDEX 1.	of Vitrinoid 3 Strength	140EX 4.5	4 PRED COK	E STAB. I	NDEX 59.50	
<u>.</u>	WASHABILIT (X.TW) AND SIZE	Y DATE S.G.	RUM 00/00/00 DIRECT X F HT. ASH 0.0 0.0	sı cun WT.	i, % +/1 ASH 8.6.	L WASHADIL ! (WT.Z) ! AHD SIZE	ATY BATE	RUH 00/00/ DIRECT Z WI. ASH	00 FSI	CUN. Z Wr. Agh	†/− .1 \$.6.
ESPECTED AND ADDRESS OF THE PERSON AND ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRESS OF THE PERSON ADDRE	( 0.0) -1/4/†28)	FLT. 1.30 1.40 1.50	0.0 0.0 0.0 0.0 0.0 0.0	0.0	0.0 0.0	1 -1/9/4 0	1.30	<ul> <li>27.1 9.1</li> </ul>	4	47.7 5.4	56,6 57,5 40,5
	)	1.60 1.70 SINK 1.70	0.0 0.0 0.0 0.0 0.0 0.0	0,0 0,0 0,0	0,0 0,0 0,0 0,0		1.60 1.70 SINK 1.70	8.7 27.5 2.5 38.8 15.7 82.2	i NS 1	81.8 10.6 84.3 11.4 80.0 22.5	13.3
	( 0.0) ⁻ -28H140H	1.40	0.0 0.0	9,0 0,0	0.0 0.0	I FROTH	·			• .	
	• ,	1.50 1.60 1.70 SINK 1.70	0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0	0.0 0.0	( 0.0)   -28H+6CH	FROTH TAILINGS	0.0 0.0		0.0 0.0	
	(0.0) -60%	FLT. 1.30 1.40	0.6 0.0 ·	0.0	0.0 0.0	! FROTH ! CELL TEST				·	
		1.50 1.60 1.70 SINK 1.70	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0,0 0,0 0,0,	0.0 0.0 0.0 0.0	( 0.0).	FROTH TAILINGS	0.0 0.0	• .	0.0 0.0	
<u>-</u>	 8376%		, , , , , , , , , , , , , , , , , , , ,								

	ORTLL HOLE: EVI51 (COR VERTICAL THICKNESS 0.	E ) GEAM 47 DIP ANGLE RECEIVED: 00/G MH D	INVERCEPT 8: 31 LAYITUGE SSAC 0/00 WEIGHT B YY COMPOSIYE:	1,72- 99,21 INTERT 1076,130 K BEFARTURE 0,00 KG HOISTURE RECOVERY	THICKNESS 0.49 657152.130 K 0.0 K 100.0 X	TRUE THICKNESS 0,42 M ELEVATION 130,440 M COMPLETE! 00/90/00 HM BD YY
	PROXIMATE AMALYSIS (DRY Z OF 1/8' X O ASH X. V.M. X F.C. Z	RASIS)   6 RAW *CLEAN   0.00 0.00   0.00 0.00   0.00 0.00   0.00 0.00	IESELER PLASTICITY, START FUSION TEMP, HAX FLUID TEMP, FINAL FLUID TEMP,	DATE RUN 00/00/00	BULATATION (RUHR)  TI - SOFT, TEHP,  TII - HAX, CONTRACT  TIII - HAX, DILATAT	DATE RUN 00/09/00  OC 0.0  TIGH TEMP: OC 0.0  IDN TEMP: OC 0.6
Trickers .	PROXIMATE ANALYSIS (DRY X OF 1/8' X O ASH X. V.H. X F.C. X F.S.I. X TOTAL SULF. X P205 (PHCSPHATE) BROSS CAL. VALUE BTU/LB V.H. X (DAF) X (-1/8'+0 COAL FLOATED	0.00 0.00   0.00 0.00   0. 0.   0.0 1.P AT 1.50 S.G.)	SULTUTE LCAT TON TEAM HELTING RANGE HAXIMUM FLUIDITY BD. ETROGRAPHIC DATA  V-TYPES REACTLY	OC 0.0 I  THE COMPLETED GO/OC  JE CONFONENTS	DILATATION  JOO PELLET HUMBES  INERT COMPONENTS	ž 0.0 R 0
	SCREEN ANALYSIS (COAL CR SIZE WT.X ASHX -174'+ 28H 0.0 0.0 -28H + 60H 0.0 0.0	USHED TO 1/4')   CUMULATIVE   UT.Z ASHZ   0.0 0.0 1	0 0.0 REACT 0 0.0 EXINI 0 0.0 TOTAL I	TYE SF. (1/2) 0.0 TYE SF. (1/2) 0.0 PID & RESIN 0.0	MICRINGIBS FUSINGIBS FUSINGIBS MINERAL HATTER TOTAL INERTS	0.0 9.0 0.0 0.0
			BAL. INDEX 0.00		PRED. COKE STAB.	CUH, Z +/1 UT, ACH S.6.
	( 0.0) FLT. 1.30 -1/4/†28f 1.40 1.50 1.60 1.70	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	1 0.0 0.0 0.0 1	(100.0) FLT. 1.30 -1/8'+ 0 1.40 1.50 1.60 1.70 SINK 1.70	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon	( 0.0) FLT. 1.30 -28H760H 1.40 1.50 1.60 1.70	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 I 0.0 0.0 0.0 i 0.0 0.0 0.0 I	FROTH CELL YEST ( 0.0) FROTH -23H+60M TAILINGS	0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0
		0.0 0.0	1 0.0 0.0 0.0 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0 1 0.0	FROTH CELL TEST ( 0.0) FROTH -60H + 0 TAILINGS	0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0
	NOTES:					

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	DRILL HOLE: EVIS: (CORE ) SEAM VERTICAL THICKNESS 1.25 DIP ANG RECEIVED	E 31 : 00/00/00 HM 00 YY	INTERCEPT LATITUDE SS WEIGHT COMPOSITE:	97.59- 98.84 INT 46876.130 H DEPAR 0.00 KG MOIST RECOV	PT THICKHESS 1.25 TURE 657152.136 H TRE 0.0 X TRY 100.0 X	TRUE THICKNESS 1,07 N ELEVATION 1521,570 N CONFLETE: 20/30/06 EM OD YY
200	### PROXIMATE ANOLYSIS (DRY EASIS)  ### ################################	O I STAR O I FUSI O I WAX	T SM TEMP. FLUID TEMP.	GC 0.0 0.0 0.0 0.0	I II - SOFT, TEMP. I III - MAX. CONTRAC I IIII - HAX. DILATA)	GC 0.0 TION TEMP. GC 0.0 TION TEMP. GC 0.0
	F.C. X 65.10 71.5 F.S.I. 2-1/2 3 X TOTAL SULF. 0.60 0.6 X P205 (PH3SPHATE) 0.00 0.6	O I FIMAL SOLI B I HELT O I HAXTE	. FLUID TEHP, DIFICATION YEN ING RANGE WUM FLUTTIY O	00 0.0 00 0.0 00 0.0	CONTRACTION DILATATION	X 0.0 ° Z 0.0
	GROSS CAL, VALUE BTU/LB 7160, 7228 V.H. Z (DAF) 22.0 X (-1/8/+0 CSAL FLOATED AT 1.50 S.S.	I PETRO	SCAPHIC DATA	DATE COMPLETED OF	V00/00 PELLET NUMBER	R 1563
	X P205 (PH3SPHATE) 0.00 0.0 0.0 GROSS CAL, VALUE BTU/LB 7160, 7228 V.H. X (DAF) 22.0 x (-1/6'+0 CSAL FLOATER AT 1.50 S.B. SCREEN ANALYSIS (CDAL CRUSHER TO 1/4 SIZE WT.X ASHX UT.X ASHX UT.X ASHX UT.X ASHX 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	')   TYPE   10   11   12	7 TOT: 3.4 REAL 12.2 EXII 16.0	L VITRINGID 42, TIVE SF, (1/2) 16, 1010 & RESIN 0,	2 INERT SF. (1/2) 5 HICRINOIDS 0 FUSINOIDS 14 HINERAL MATTER	18.4 4.3 11.7 4.9
	7-1/1/1 288 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	1 13 1 0 1 HAX. 1 BAL.	3.0 0.0 HEAN REFL. OF INDEX 2.04	VITRINOIDS (KD) 1 STRENOTH INDEX 4	,22 ,71 PRED, COKE STAB.	37.3 INDEX 50.50
	WASHABILITY DATE RUN 00/00/00 (WT.Z) S.G. DIRECT Z F AND SIZE WT. ASH					
	-1/4'+22H 1.30 0.0 0.0 1.30 1.30 0.0 0.0	0.0 0.0		(100+0) Fills 1s		22:6 2:4 63:3 577 5 A 10 C
	1.70 0.0 0.0 SINK 1.70 0.0 0.0	0.0 0.0 0.0	0,0	SIHK 1.	70 1 2.0 41.7 1 70 9.1 71.1 NC	90.9 10.6 100.0 16.1
Charles and	( 0.0). FLT. 1.30	0.0 0.0 0.0	0.0 0.0 l-	CELL TEST	0.0 Ó 0	. 0.0 0.0
	. 1170 010 010 SINK 1.70 0:0 0:0	0.0 0.0	0.0	-28HFAON - TAILIN	0.0 0.0 GS 0.0 0.0	0.0 0.0
200	( 0.0) FLT. 1.30 0.0 0.0 -60H 0 1.40 0.0 0.0 1.50 0.0 0.0	0,0 0,0	810 - 010 F	FROTH CELL TEST		
	-60H 0 1.40 6.0 0.0 1.50 0.0 0.0 1.60 0.0 0.0 1.70 0.0 0.0 SINK 1.70 0.0 0.0	0.0 0.0 0.0	0.0 0.0 1 0.0 0.0 1 9.0 1	( 0.0) FROTH -60H + 0 TOILIN	0.0 0.0	0.0 0.0 0.0 0.0
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	DRILL HOLE: EVIS VERTICAL THICKN	1 (CORE ) S ESS 0.71 DI RE	SEAM 6.8 IP ANGLE 25 ECETVED: CO/CO/OC HH DD YY	INTERCEPT 16 LATITUDE 554 WEIGHT COMPOSITE:	9.32- 170.7 6876.130 H 0.00 KG	I INTOFI THI OEPARTURE HOISTURE RECOVERY	CKNISS 0.91 637152.120 H 0.0 Z 80.0 Z	TRUE THICKS ELEPHICH COMPLETE:	233 0.32 H 1449.340 H 09/00/00 HS 0D YY
		YSIS (DRY BASIS	601 TAU 1	er plasticity.	DATE RUN 90	\00\00   BIL	.(7887), KOLȚATA.	DATE RUN (	0/20/00
	X OF 1/8' X C ASH Z V.M. X F.C. X F.S.I. X TOTAL SULF. X P205 (PE)3PHA GROSS (AL. VALU	RAW 100.00 41.30 17.10 75.80	*CLEAN   0 37.40   STAK 0 8.50   FUSI 0 21.70   HAX   0 69.80   FINAL	N TEMP. LUID TEMP. FLUID TEMP.	GC 417 GC 442 GC 459 GC 471	0   II   0   III   0   III	- SOFT. TEMP. - MAX. CONTRA I - MAX. DILATA	STICH TEXP. C	C 418.0 C 445.0 C 445.0
	F.S.I. W TOTAL SULF.	4 0,63 0.00	8-1/2   SOLI 3 0.81   HELTI 6 0.00   HAXT	NFICATION TEKP NG RANGE NA FLUIDITY DO	; 185 470		i. Bundani. Pidi	<b>!</b>	-2.0
	GROSS CAL. VALU V.M. % (DAF) * (-1/8'+9 COAL			RAPHIC DATA	DATE COMPL	ETED .00/00/00	PELLET YUN		
	SCREEN AWALYSIS	(COAL CRUSHED		PES REACTI X TOTA 1.0 REAC	VE COMPONENT: L VITRINGID TIVE SF, (1/:	3 50.7 2) 16.1	NERT COMPONENTS INERT SF. (1/2 HICKINOIDS	16.1 3.7 8.1	
	7-1/4/+ 28H 0			2.5 6.6 TOTAL 14.7	REACTIVES	67.0 T	HINCRAL MATTER OTAL INERTS	33.0	
	-60M + 0 0	6 0.0 0.0	0 0.0   12   MAY	MEAN REEL . RE-!	VITRIHOIDS (! STRENGTH INDI	1.16 EX 1.45 P	RED. COKE STAB.	INDEX 56.10	
	WASHABILITY (WT.X) AND SIZE		00/00 % FSI CUK ASH WT.	Z 77- 11 1	WASHABILITY (UT)Z) AND SYZE	" S.6. " P	00/00/00 IRECT % FSI WT. ASH	CUK, Z UT, ASK	ŧ/- ₊1 3.6.
	( 0.0) FLT. -1/4/+29H	1.50 0.0 0	0,0 0.0 0,0 0,0 0,0 0,0	0.0 0.0 l 0.0 0.0 l 0.0 0.0 l	(100.0)   -1/8'+ 0	FLT: 1:30 1 1:40 1 1:50 1:60	2.2 2.3 8-1/2 3.4 6.5 7 8.2 14.5 5 8.6 24.7 1 5.7 36.6 1	12,2 2,5 25,6 4,6 33,6 7,0 42,4 10,6	53.2 14.9 34.7 29.7
	D : : : sine	1.60 0.0 0 1.70 0.0 0 1.70 0.0 0	0.0	0.0	** ** **	1.70 SIRK 1.70 5	5.7 36.4 1 1.9 73.4 NC	48.1 13.7 106.0 44.8	
in the second	-( 0.0)- FLT. -28K#60H	1.40 0.0 0 1.50 0.0 0	0.0 0.0 0.0 0.0	0.0 0.0 1	FROTH CELL TEST				
	. SINK	1.60 0.0 0 1.70 0.0 0	0.0 0.0	0.0 0.0 I	( 0,0) -28H+60H -	FROTH TAILINGS	 0'0 0'0 '" 6'0 0'9	0.0 0.0 0.0 0.0	- · · · ·
	( 0.0) FLT.	1.40 0.0 0	0.0	0.0 0.0 1	FROTH CELL TEST			, .	
	Sina	1.30 0.0 0 1.60 0.0 0 1.70 0.0 0 1.70 0.0 0	0.0 0.0 0.0 0.0 0.0 0.0	6.6 A.8 E	( 0.0) -60H + 0	FROTH TAILINGS	0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0	
	. Notea:				1 441				

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	DRILL HOLE: EVI51 VERTICAL THICKHESS	(CORE ) SEAN 5.8 2.41 DIF ANOLE RECEIVED:	INTERCE 29 LATITU 00/00/00 UEIGHT 33 DD YY COMPOS	FT 214.55- 218 DE 5346876.130 H 0.00 K	.96 INTOPT THE DEPARTURE O HOISTURE RECOVERY	ICKNESS 2.41 657102.130 K 0.0 Z 0.0 X	TRUE THICKNED COMPLETE: 0	R 2.76 H 1402.610 H 9/09/00 H DD YY
	PROXIMATE ANALYSIS	(DRY BASTS)	. Į GIESELER PLAS	FICTTY, DATE RUN	00/00/00   BI	ATATION (RUMR)	DATE SUN GO!	00/00:
	PROXIMATE ANALYSIS  Z OF 1/8' X O ASH X V.N. X F.C. X F.S.I. Z TOTAL SULF. Z F205 (PHOSPHATE) GROSS CAL. VALUE BT V.H. X (DAF) * (-1/8'+0 COAL FLO SCREEN ANALYSIS (CC SIZE WT.X -1/4'+ 28H 0.0 -28H+ 60H 0.0 -60H+ 0 0.0	RAW *CLEAR 100.00 43.8: 41.40 8.20 41.40 20.20 44.20 71.60 1-1/2 7 0.44 0.54	START FUSION TEMP, HAX FLUIO TEI FINAL FLUID SOLIDIFICATI HELTING RANGI	0C 4 0C 4 1P 0C 4 1EHP 0C 4 3N TEHP 0C 6	113.0   II 137.0   II 163.0   II 181.0   194.0	- SOFT. TEMP. L - KAX. CONTRACTION CONTRACTION DILATATION	TION TEMP, OC TION TEMP, GC	415.0 445.0 445.0 7.0 -7.0
	Z P205 (PHOSPHATE) GROSS CAL. VALUE BT	0.00 0.00 U/LB 0. 7905.	HAXIAUM FLOO	MIY BU/A I	71/	A		
	.V.H. % (DAF) * (-1/8'+0 CDAL FLO	24.6 (.ated at 1.50 S.G.)	PETROGRAPHIC	DAIA WAIL LUF	HIFIFU OUVOOVO	THEOR COMPONENTS	in v	
	SCREEN ANALYSIS (CC	OAL CRUSHED TO 1/4' CUMULATIVE ASHZ NT.Z ASHZ	0-11FES 1 0 0.0 1 0 0.0 1 0 0.0	TOTAL VITRINOI REACTIVE SF. ( EXINOID & RESI	D 0.6 1/2) 0.0 N 0.0	INERT SF, (1/2) MICRIMOIDS FUSINOIDS HINERAL MATTER TOTAL INERTS	0.0 0.0 0.0	
	-28% + 60M 0.0 -60M + 0 0.0	0.0 0.0 0.0	0 0.0   0 0.0   MAX. MEAN REI   BAL: INDEX	L. OF VITRINOIDS 0.CO STRENGTH I	(RO) 0.00 (NDEX 0.00	PRED. COKE STAB.	INDEX 0.00	
Lä	WASHABILITY DAY (WT.Z) S.E AND SIZE	FE_RUN 00/00/00 FE_DIRECT % FS WT. ASH	I CUH, Y T/- WT. ASH S	.1 -I (WT.Z) .6. I AND SIZE	SiG.	DIRECT % FSI WT. ASH	CUN. X 1. MT. ASH	/- :1 5.6.
	( 0.0) FLT. 1. -1/4'+28M 1.4 1.2 1.2 51NK 1.7	30 14.4 3.2 7-1/10 19.2 8.9 2-1/10 7.9 20.1 1 50 4.8 32.6 1 70 6.0 44.3 1 70 47.7 71.4 NC	2 14.4 3.2 6 2 33.6 6.5 5 41.5 7.1 2 46.3 11.5 20 52.3 15.3 100.0 42.0	4.2   (100.0) 1.8   -1/8' ± 0 4.3   1.7	FLT. 1.30 1.40 1.50 1.60 1.70 SINK 1.70	17.5 2.2 8 14.3 6.6 5 10.7 14.3 1 5.5 22.4 1 3.5 33.8 1 18.5 70.4 NC	17,5 2,2 31,8 4,2 42,5 6,7 48,6 8,5 51,5 16,2 100,0 39,4	61,7 49,5 31,5 17,5
Processor St. Separate	( 0.0) FLT. 1.3 \$-28H+60H 1. 1.5 1.1 SINK 1.7	30 44.3 1.8 9	44.3 1.8 76	8.0   FROTH 8.0   CELL TEST 8.7   8.1   ( 0.0) -280160%			.·	
	( 0.0) FLT. 1. -60H 0 1.	10 0.0 0.0 30 0.0 0.0 60 0.0 0.0 70 0.0 0.0	0.0 0.0	0.0   FROTH 0.0   CELL TEST 0.0   ( 0.0) 1 -60H + 0	FROTH TAILINGS	0.0 0.0	0.0 0.0	
	NOTES:							

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	DRILL HOLE: EVISI (CORE ) SEAM VERTICAL THICKNESS 13.85 DIP AN RECEIV	5.8 DLE 20   ED: 00/00/00   HA DD YY (	INTERCEPT 21 LATITUDE 554 VEIGHT COMPOSITE:	8,71- 232,6 8674,130 H 0,00 KG	B1 INTCPT DEPARTURE MOISTURE RECOVERY	THICKYESS 13 657152.150 0.0 % 21.4 7	A ELEVATION CONFLETS:	1533 13,02 H 1400,200 H 00/00/00 HH DD YY
	FROXIMATE ANALYSIS (DRY EASIS)  RAW #CI  X OF 1/8' X 0 100.00 6:  ASH X 22.90 6  V.H. X 17.60 2:  F.C. X 59.50 70  F.S.I. 2-1/2 6  X TOTAL SULF. 0.27 0  X P203 (PHOSPHATE) 0.00 0  GROSS CAL. VALUE BTU/LB 0.75  U.H. X (DAF)	EAN   GIESELEI 1.00   START 1.30   FUSION 1.50   MAX FLI 1.20   FINAL F 1.35   HELTING 1.60   MAXIMUM 25.   PETROGRA	R FLASTICITY, TEMP, UIB TEMP, FLUID TEMP, FICATION TEMP B RANGE A FLUIDITY DO APHIC DATA	DATE RUN OF 421 DC 441 DC 441 DC 441 DC 491 DC 471 MM 73	0/00/00	DILATATION (RUH TI - SOFT, TE TII - MAX, CON TIXI - MAX, TIXI CONTRACT DILATATI  /00 PELLET 3	IR) DATE RUN ( THP. CONTROL TEMP. CONTROL TON TON THEER O	00/00/00 6C 418.0 6E 453.0 6C 453.0 7Z 11.0 7Z -11.0
	FROXIMATE ANALYSIS (DRY BASIS)  RAW *CI  X OF 1/8' X 0 100.00 5  ASH X 22,90 E  V.H. X 17.60 21  F.C. X 59.50 70  F.S.I. 2-1/2 6  X TOTAL SULF. 0.27 (  X P203 (PHOSPHATE) 0.00 (  GROSS CAL. VALUE BTU/LB 0. 75  V.H. X (DAF)  * (-1/8'+0 COAL FLOATED AT 1.50 S  3CREEN ANALYSIS (COAL CRUSHED TO 1  SIZE WT.X ASHX WT.X ASHX  -1/4'+ 28H 87.1 22.0 87.1 25  -28M + 60M 8.1 12.2 95.2 21  -60H + 0 4.6 14.4 100.0 20	G;)   V-TYPE   11   12   12   13   2   15   14   15   16   16   17   18   18   18   18   18   18   18	ES REACTI	VE COMPONENT L VITRIHOID TIVE SF, (1/ OID & RESIN REACTIVES VITRINOIDS ( STRENGTH INI	(S \$2.5 /2) 15.9 0.0 68.4 (RO) 1.35 0EX 5.84	INERT COMPONE INERT SF. ( MICRINOIDS FUSCHOIDS HIMERAL HOT TOTAL INERTS	MIS 1/2) 15.9 4.3 6.7 TER 4.7 31.6	
Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of the Comments of th	WASHABILITY DAYE RUN 00/00/00 (WT.Z) S.B. DIRECT Z AND SIZE WT. ASH	FSI CUH. Z	% +/- ,1   Sh S.6,	WASHABILITY (WT.X) AHB SIZE	PATE :	RUN 00/00/00 DIRECT Z F WT. ASH	SI CUH, X NT, ASH	‡/- ,1 5,6,
	(87.1) FLT. 1:30 14:3 3:9 7 -1/4'+28N 1:40 41:9 9:7 1 1:50 13:5 17:1 1 1:60 6:8 26:9 1 1:70 4:7 33:0 1 SINK 1:70 18:8 60:5 N	14.7 7	.9 69,2   .2 68,2   .3 25,0   .8 14,2	(100.01)	FLT. 1.30	22.0 2.2 ? 25.6 6.7 3-	. 22.0 2.2 1/2 47.6 4.6 1/2 45.4 7.6	62.2 55.7 35.2 24.5
	( S.i)- FLT. 1.30 41.4 2.0 7 -28M+60M 1.40 30.7 6.7 6 1.50 13.4 15.7 1 1.50 4.0 28.2 1 1.70 1.3 36.1 1 SIMK 1.70 9.0 61.4 M	72.1 4. -1/2 83.5 5.	.1 48.5   .9 19.1	FROTH CELL TEST ( 8.1) -28H18SH	FROTH TAILINGS	0.0 0.0	0.0 0.0 0.0 0.0	· · · · ·
<i>(1111112</i> )	( 4.8) FLT. 1.30 0.0 0.0 0.0 -60M± 0 1.40 0.0 0.0 1.50 0.6 0.0 1.60 0.0 0.0 1.70 0.0 0.0 3INK 1.70 0.0 0.0	0.0 0. 0.0 0. 0.0 0. 0.0 0. 0.0 0.	1 0.0 0. 1 0.0 0. 1 0.0 0.	FROTH CELL TEST ( 4.8) -60M + 0	FROTH TAILINGS	92,3 10,7 6- 7,7 58,3 HC	1/2	
	NOTES:	98 4						

	DRILL HOLE: EVISI (CORE ) SEAM VERT (CAL THICKNESS 0.64 DIP ANOL RECEIVED	INTERCEPT 24 LATITUDE 00/00/00 WEIGHT NH DD YY COMPOSITE:	324,72- 327.54 INTO 5346076.130 M DEPAK 0.00 KG MOISTA RECOV	OPT THICKNESC 0.64 PURE 639132.130 H URE 0.0 Z ERY 100.0 Z	TRUE THECKNESS G.58 K ELEVATION 1292.240 H COMPLETE: 00/00/00 WH DD YY
	JERROVINATE ANALYPIO JERNY DARTON	. A OTEOPLE'S PLACETOR	TV. DATE DUN AAJAAJAA	し かちしんかんててのい くのりじかき	nate bill acidalar :
	RAW   KCLEA    X OF 1/8' X O   100,00   44.0     ASH	FUSION TEMP,   MAX FLUID TEMP,   FINAL FLUID TEMP   SOLIDIFICATION     MELTIMO RANGE   MAXIMUM FLUTETTY	0.0 0.0 0.0 0.0 0.0 0.0 EHP. 0C 0.0 0.0 0.0	I III - MAX. CONTRACTION DILATATION	TION TEMP. OC 455.0 TON TEMP. CC 456.0 Z 14.0 Z -14.0
	V.N. 7 (DAF) 22.9	I PETROGRAPHIC DATA	DATE COMPLETED OF	0/00/00 · PELLET NUMBE	R 0
	* (-1/8'+0 COAL FLOATED AT 1.50 S.G.  SCREEN ANALYSIS (CGAL CRUSHED TO 1/4  SIZE WI.Z ASHX WI.Z ASHX -1/4'+ 23H 0.0 0.0 0.0 0.0  -28H + 60M 0.0 0.0 0.0 0.0 0.0  -60M + 0 0.0 0.0 0.0 0.0 0.0	V-TYPES REGION OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY	CTIVE COMPONERIS OTAL VITRINGID AP ENCTIVE SF. (1/2) 17 XINGIO & RESIR 0 AL REACTIVES 66	INERT COMPUNENTS INERT SF. (1/2) KICRINOIDS FUSINOIDS HINERAL HATTER TOTAL INERTS	17.4 3.7 8.4 3.7 33.2
	-28# + 60# 0.0 0.0 0.0 0.0 0.0 -60# + 0 0.0 0.0 0.0 0.0	0 0.0 1 0 0.0 1 HAX. HEAN REFL. 1 2 BAL. INDEX 2.4	OF VITRINOIDS (RO) 1 6 STRENOTH INDEX 6	.43 .55 PRED. COKE STAB.	INDEX 57.00
	WASHABILITY DATE RUN 00/C0/00 (UT.Z) S.G. DIRECT Z FO	1 7 - 1 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	MASHABILITY DA   (WT.Z) S.   AND SIZE	TE RUM 00/00/00 G. BIREST Z FSI WT. ASH	CUK, Z +/1 9T, ASH 5.6,
	( 0.0) FLT. 1.30	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	1 (100.0) FLT. 1. ! -1/8'	30 12.8 1.7 8-1/2 40 19.7 5.8 2 30 10.3 13.6 1 60 4.5 27.0 1 70 4.5 37.9 1 70 48.0 78.3 MC	12.8 1.7 62.5 32.5 4.2 58.1 43.0 6.5 28.8 47.5 6.4 17.3 52.0 11.0 100.0 43.3
		0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	I FROTH I CELL TEST	0.0 0.0	0.0 0.0
	( 0.0) FLT. 1.30 0.0 0.0 -50H 0 1.40 0.0 0.0 1.30 0.0 0.0 1.60 0.0 0.0 1.70 0.0 0.0 SINX 1.70 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	FROTH   CELL TEST   ( 0.0) FROTH   -60N + 0 TAILIN	0.0 0.0 0.0 0.0	0.0 0.0
- - -	MOTES:		1		

6.00	( 						
	DRILL HOLE: EVI51 (CORE VERTICAL THICKNESS 5.19	) SEAM 4:8 DIP ANGLE 24 RECEIVED: 00/00/00 MM DD YY	INTERCEPT 328 LATITUDE 5546 SEIGHT COMPUSITE:	,26- 333,45 II 876,130 H DEP 0,00 KG MDI REC	KTOPT THICKMESS ARTURE 659152. STURE 0 OVERY 79	5,19 TRUE THICH 130 N ELEVATION 0 Z COMPLETE: ,4 Z	ANESS 4.74 N 1270.760 N 00/00/00 N/ DD YY
	PROXIMATE AMALYSIS (BAY B	ASIS)   GIESEL	ER PLASTICITY,	DAYE RUN 00/00/	KOLTATAJIO   OÖ	(ruhr) 📋 date run	00/00/00
	X OF 1/8' X 0 10 ASH X 15 V.N. X 1	0.60 76.60   START 9.10 7.40   FUSIO 6.40 19.30   MAX F	H TEKP. LUID TEMP.	00 414.0 00 410.0 00 467.0	I II - SOFT I TII - MAX. I TIII - MAX.	TEMP. CONTRACTION TEMP. DILATATION TEMP. RACTION (ATION	90 417.0 90 437.0 90 437.0
	F.C. Z F.S.I. Z TOTAL SULF.	4.50 73.10   FINAL 3-1/2   SOLIO 0.39 0.43   MELTI 0.00 0.00   MAYIM	FLUID.TENP. TFICATION TEMP. NO RANGE NO FLUTDITY DD/	00 480.0 00 493.0 00 40.0 80 7.7	l CONT	RACTION PATION	業 17.0 第 −17.0
	PROXIMATE AMALYSIS (BRY B. R. X OF 1/S' X O 10 ASH X 11 Y.N. X 12 Y.N. X 14 F.C. X 5. X TOTAL SULF. X P205 (PHOSPHATE) GROSS CAL, VALUE BTU/LB 35 Y.N. X (DAF) X (-1/S'+0 COAL FLOATED AT	374. 8009. 1	RAPHIC DAYA	DATE COMPLETED	00/00/00 PELL	ET HUHBER 0	
	SCREEN ANALYSIS (COAL CRUS)		PES REACTIVE 7 - TOTAL 0,5 REACT 2,0 EXIND 6,8	E COMPONENTS VITRINGID IVE SF. (1/2) ID & RESIN	INERT COM 19:4 INERT S 19:0 HICRINO 0:0 FUSINOI HINERAL 58.4 TOTAL THE	**************************************	
	SCREEN ANALYSIS (COAL CRUS)  SIZE WT.Z ASHZ 1  -1/4/7 28% 0.0 0.0  -29% 1 60% 8.2 9.6  -60% 1 0 6.4 10.3	8.2 7.6   14 14.6 10.1   15   HAX.     FAL.	19.8 8.7 HEAR REFL. OF V. INDEX 2.06 S	ITRINDIDS (RD) TRENOTH INDEX	1,40 6.15 PREB. CGK	STAB. INDEX 59.	50
	WASHABILITY DATE RUN ( UT.Z) S.G. DIRE AND SIZE WI	00/00/00 ECT % FSI CUH; • ASH WT.	3 t/1 1 ASH S.G. 1	MASHABILITY (WI.X) AND SIXE	DATE RUN 00/00/ S.G. DIRECT X WT. ASH	)O FSI CUH. X WI. ASH	₩- ,1 1 8.8.
	( 0.0) FLT. 1.30 12. -1/4'+28H 1.40 51.5 1.50 12.1 1.60 5.2 1.70 2.3 SIMK 1.70 16.0	5 2.8 7-1/2 12.5 5 9 8.2 2-1/2 64.4 7 1 18.7 1 76.5 5 2 29.8 1 81.7 10 3 36.3 1 84.0 11 0 76.1 NC 100.0 21	2.8 76.7   7.2 76.2   - 9.0 20.6   0.3 8.9   1.0	(100.0) FLT. -1/8/+ 0 SINK	1.30 25.1 1.6 1.40 26.6 4.4 1.50 20.9 11.0 1.60 8.2 21.3 1.70 3.8 31.4 1.70 15.4 70.8	9 25,1 1.6 4 51,7 3.0 1 72,6 3.2 1 80,8 7.0 1 84,4 8.1 NC 100,0 17,7	5 61.1 55.1 51.4 14.2
	, -28n+60h 1.40 24.6 1.50 13.4 1.60 4.6 1.70 2.5		3.2. 39.9 ! [	FROTH CELL TEST ( 8,2) FROT -28N46GN TAIL	H 0.0 0.0 INGS 0.0 0.0	0.0 0.0 0.0 0.0	
	( 6.4) FLT. 1.30 0.0 -60H 0 1.40 0.0 1.50 0.0 1.60 0.0 1.70 0.0 SINK 1.70 0.0	0 0.0 0.0 0.0 0 0 0.0 0.0 0 0 0.0 0 0.0 0	0.0 0.0 1 ( 0.0 0.0 1 ( 0.0 0.0 1 (	FROTH CELL TEST ( 6.4) FROT -60M + 0 TAIL	H 61.0 7.4 INGS 39.0 16.0	7 61.0 7.4 5-1/2 100.0 10.5	
	NOTES:						
3	* · · · · · · · · · · · · · · · · · · ·			* * *			

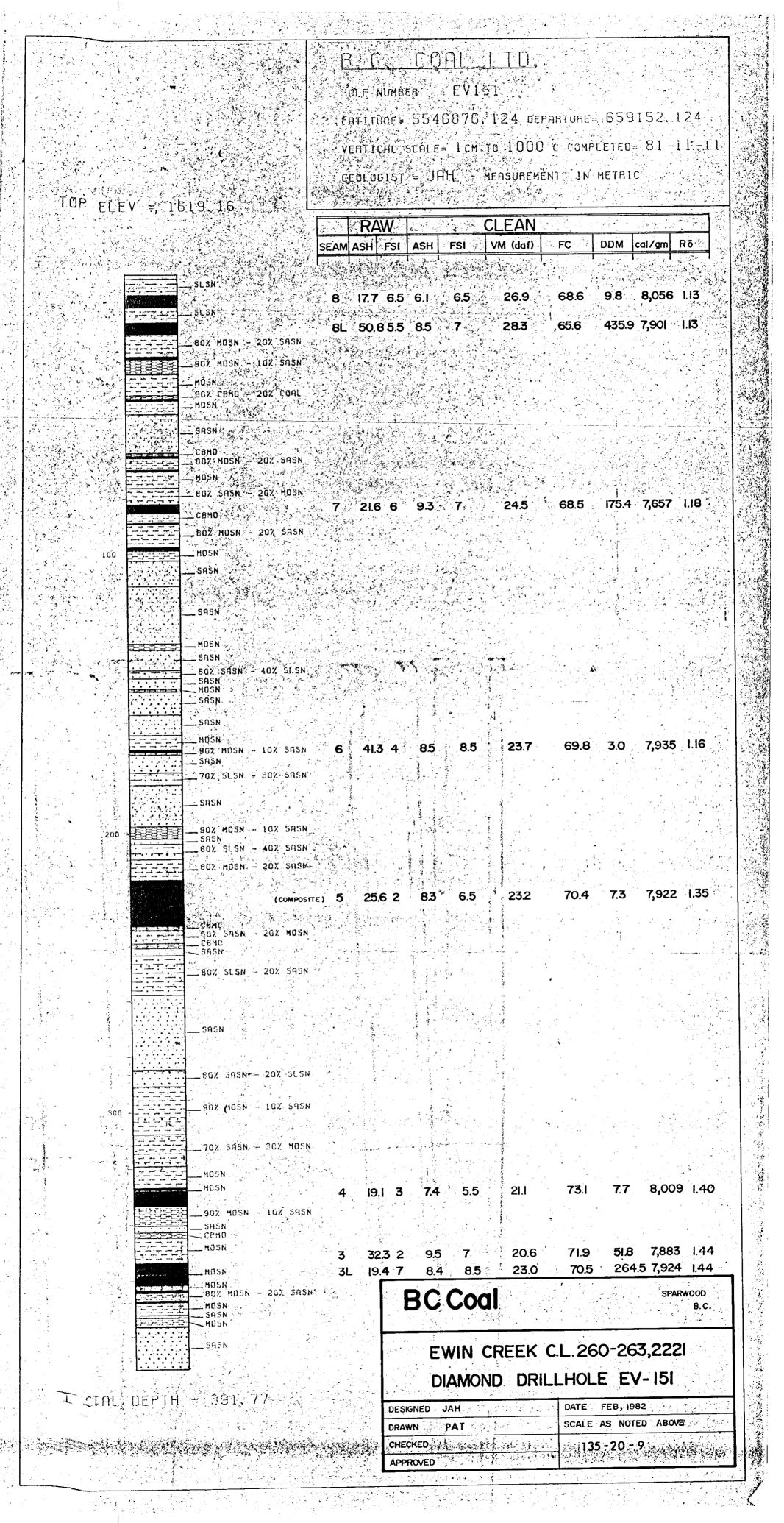
	DRILL HOLE: EVISI VERTICAL THICKNES	(CORE ) SE SS 3.90 DIF	AM 3.3 ANGLE EIVED: 00/00/00	INTERCEPT LATITUPE VEIGHT COMPOSITE:	353.72- 357. 3546876.130 H 0.00 KG	62 INTOPT DEPARTURE - KOISTURE SECOVERY	7810KWESS 637152	3.70 130 H 1.0 %	TAME THICK ELEMATION COMPLETE:	1265,440 H
	1350	·				3 /3 5 / 3 A 1	NT: LTLTTOIL	reman.	maker milita	22/00/00
m	PROXIMATE ANALYS  Z OF 1/8' X O ASH Z V.N. Z F.C. Z F.S.I. Z TOTAL SULF. Z P205 (PHOSPHATE	100.00 32.30 11.30	60.80   STAR 9.50   FUSI 18.60   MAX	T ON TEHP, FLUID TEHP,	0C 41 0C 43 0C 46 nr 49	6.0 1 6.0 1	TI - SOFI IXI - MAXA TEXI - MAXA	CONTRACT CONTRACT COLATAT	ILDN TENP. ION TENP.	9D 417.0 CC 462.0 GC 477.0
	F.S.I. Z TOTAL SULF. Z P205 (PHOSPHATE	2 0,31 0.00	7   SOLT 0.42   HELT 0.60   HAXI	DIFICATION TO ING RANGE WHAT FLUIDITY	EMP, OC 50 BD/H 51	0.0 2.0	CGNT DILA	RACTION TATION		Z 15.0 Z 5.0
	V.M. % (CAF)	Didito ()	21.4 i PETRO	GRAPHIC, DATA	. DATE COMP	LETEB 00/00.	700 PELI	er whee	G .	
	\$ (-1/8'+0 COAL F SCREEN ANALYSIS ( SIZE WT.Z -1/4'+ 2SH 83.1 -28H + 60H 9.1 -60H + 0 7.8	COAL CRUSHED CUHUL ASHZ HT.Z 33.8 83.1 17.9 92.2 17.0 100.0	0 1/4')   TYPE ATIVE   12 ASHZ   13 33.8   14 32.2   15 31.2   0	YFES REAC 2 TO 0.5 RE 1.1 ET 6.8 32.0 TOTA 12.1 0.0 HEAN REFL. (	CTIVE COMPONEN OTAL VITRINOID EACTIVE OF, (1 XINDIO & RESIN AL REACTIVES OF VITRINOIDS	75 72,5 72) 15,7 0.0 63,2 (80) 1,44	INERT CON INERT E MICRING FUSINGS KINERAL TOYAL INS	PONENTS F. (1/2) IDS .RS .MATTER .RTS	15.6 2.7 5.2 5.3 31.8	
	• "									
	WASHABILITY I	NATE RUN 00/00 1.6. BIRECT X . VT. AS	1/00 FSI CUH H WT.	, % +/1 ASH S.G.	.i .washnailit I (UT.Z) I AND SIZE	Y PATE I S.G.	RUN 00/00/ DIRECT X WT. ASH	00 FSI I	CUH. Z Yr. ASI	1/1 S.9.
	( 93.1) FLT. 1 -1/4'+28% i 1 1 1 2 SINK 1	.30 11.7 3. .40 30.9 9. .50 15.8 19.	A 7_1/2 11 7	7 # 17 7	(100.0)   -1/8'+ 0     	ELT. 1.70	0.0 0.0	i ,	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0
	. 1	.40 24.2 7. .50 12.7 13. .60 8.2 22.	8 6-1/2 61.4 9 1-1/2 74.1 1 1 82.3 7 1 65.5	4.5 43.2 6.1 24.4 7.7 13.3 8.5	FROTH CELL TEST ( 9,1) ( 9,1) ( -28)11-603	FROTH TAILINGS	0.0 0.0		0.0 0.0 0.0 0.0	
E	( 7.5) FLT. 1 -60H; 0 1 i	.40 0.0 0. .50 0.0 0. .60 0.0 0. .70 0.0 0.	0 0.0 0 0.0 0 0.0 0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	FROTH CELL TEST ( 7.3)	FROTH TAILINGS	51 (1 12)5 43,9 25,7	ć. 4	51.1 12.5 100.0 19.0	
	SINK 1 NOTES:	.70 0.0 0.	0.0	6.0	I					

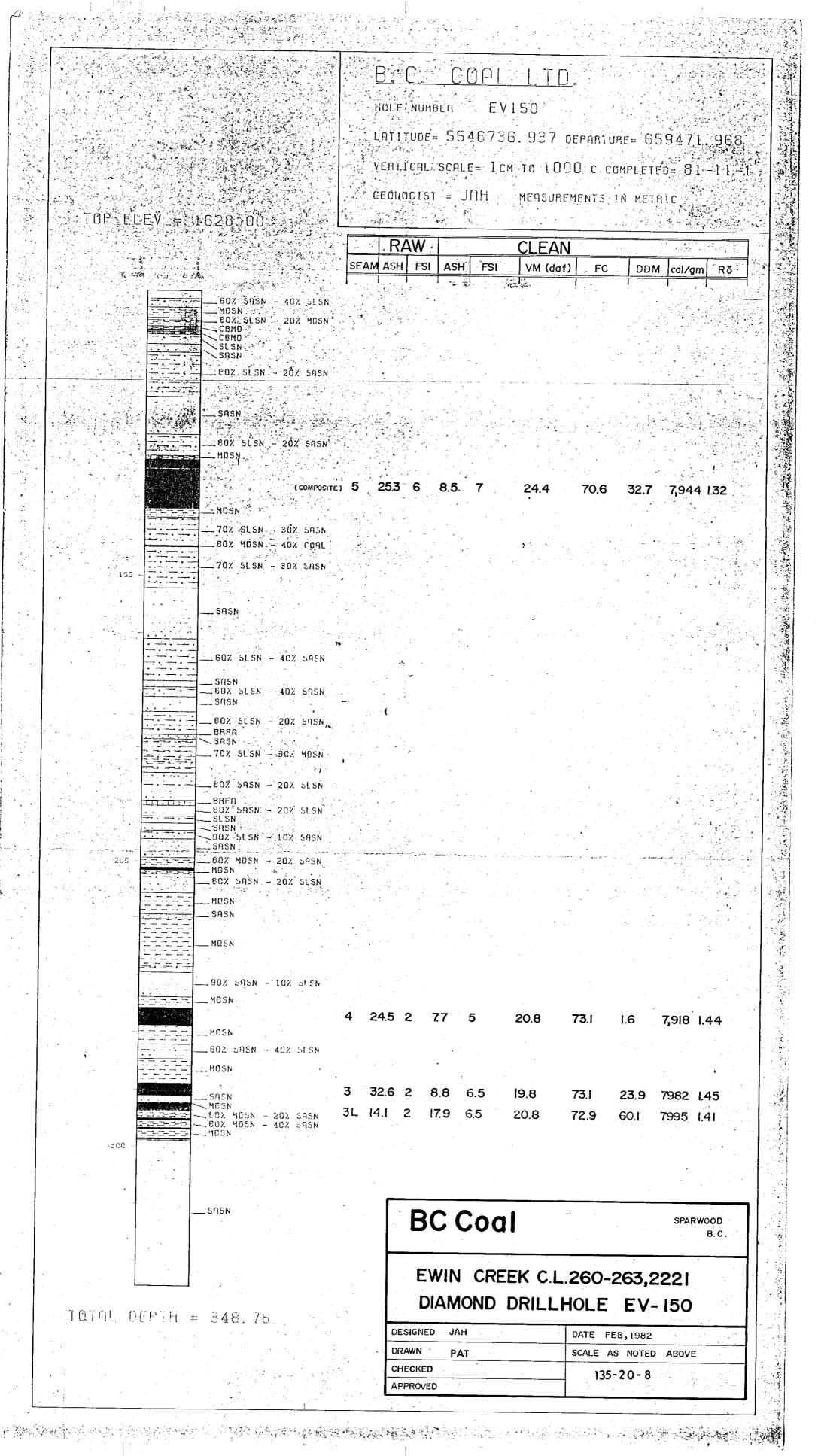
	DRILL HOLE: VERTICAL TH	EV151 IICKNESS	· R	ECEIVED: (	00/00/00	INTERCEAL LATITUDE WEIGHT COMPOSI	٠.	8.24- 35 6976.130 0.00	1.45 INT W VEPAS KO KOIST - RECOU	CPT TH YTURE YURE YERY	Ç	3,42 130 H 10 T	CURPLEN	E: 4	3,12 H 1260,900 H 10/00/00 H DD YY
	PROXIMATE		DAU	やごり ごんぴ	GIESE	LER PLAST	CITY	BATE RUN	00/00/00	}   : 01  .			DAYE R	UN 00 <i>1</i>	
Ľ3	% OF 1/8' X -ASH %	(0)	100.0	0 0,00 0 8,40 0 21,10	I STAR I FUSI	T CM TEXE:		. 00 00 00	397:0 430:0 441:0		- 50F] I - XXX II - XXX	CONTRAC DINATAN	TION TENS		413.0 451.0 -467.0
	Z OF 1/8' X ASH Z V.N. Z F.C. Z F.S.I. Z TOTAL SUL Z P205 CHO	F. SPHATE)	22.1 7 0.3 0.0	0 70.50 8-1/2 7 0.53 0 0.00	FINAL SOLI MELT MAXI	FLUID TE GIFICATION ING RANGE HUM FLUID	MP. I YEMP CTY DD	0C 0C 0C 0C 0C 0C	197.0 193.0 57.0 264.5		CONT BILM	RACTION TATION		,	13.0 3.1
	GROSS CAL, V.N. % (DAF * (-1/8'+0	AHMAT DII	11/60 - 6107	, 7924, 23,0 50 S.G.)	i raidu į	GUSSLITE DE	HH.	THE CO.	aritiza A	יט לעט לעו	o peli	ET NUKE	ir o		
	SCREEN ANAL	YSIS (CO	AL CRUSHED	TO 1/4')	V-T ! TYFE ! 12	IPES R	EACTI TOTA REAC	VE COMPONI L VITRINO TIVE SF, (	EXTS IB 67 (1/2) 10	).7	NERT CON IKERT S MICRINO	ING .	2.7 2.5		
	5-17474 98K	85.6 8.5 5.9	21,2 83, 0,0 94, (1,9 100,	6 21,2 1 19,3 0 18,8	1 15	. 0.0		REACTIVES VITRINGIDS STRENGTH			TOTAL INE FRED. COK	•	20.0	.05	
Toward .	 Washability						. ,					~~~~			<del></del>
ينب	Tr (UT.Z). : AND SIZE	S.6	DIRECT	Z FSI ASH	CUH:	7 1/- ASH 5.6		Washabili (WT.X) AND SIZE		•G• I	DIRECT I WI. ASH	-51	CUH. Hr. A	Z ł	/1 3.6.
	( 85.6) -1/4/+28H	FLT. 1.3 1.4 1.5	0 17.0 37.7 10 17.2 2	2,9 7-1/2 0,2 6 0,7 4-1/2 2,2 2	17.0 56.7 73.7	8.0 49.	7 1	(100.0) -1/8'+ 0	1	.40	0.0 0.0 0.0 0.0 0.0 0.0		0.0 0.0	).0 ).0	0.0 0.0 0.0
		1.66 1.76 SINX 1.70	3.2 3	7.8 NC .	79.3 1 32.5 100.0 2	13.5 11.2			sink i	.70 .70	0.0 0.0 0.0 0.0 0.0			).0 ).0	 
Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial Commercial	( 8,5) -28H+60H	1.40 1.50	0.0 (		0.0	0.0 0.	0   0   -					<u>.</u> .		_	
Param.		1.80 1.70 SINK 1.70	0.0 (	),0 ),0 ),0	0.0	0.0		( 8,5) <del>-</del> 288 <del>1</del> 603	FROTH TAILI	H03	0.0 0.0 0.0 0.0		111 1	.0	•
e e	( 5.9) 60%+ 0	FLT. 1.30	0.0 (	)₊0	0.0	0.0 0. 0.0 0. 0.0 0.	0 1	FROTH CELL TEST			, . ,			-	: :
		1.50 1.60 1.70 SINK 1.70	) 0.0 (	),0 ),0 ),0	0.0	0.0 0.0 0.0 0.0	Ŏ	( 5.9) -60% + 0	FROTH TAILU	) 1963 3	6.5. 8.4 3.5 18.8	7-1/2 6	65.5 8 100.0 11	.1	
	NOTES	<b>‡</b>								-					

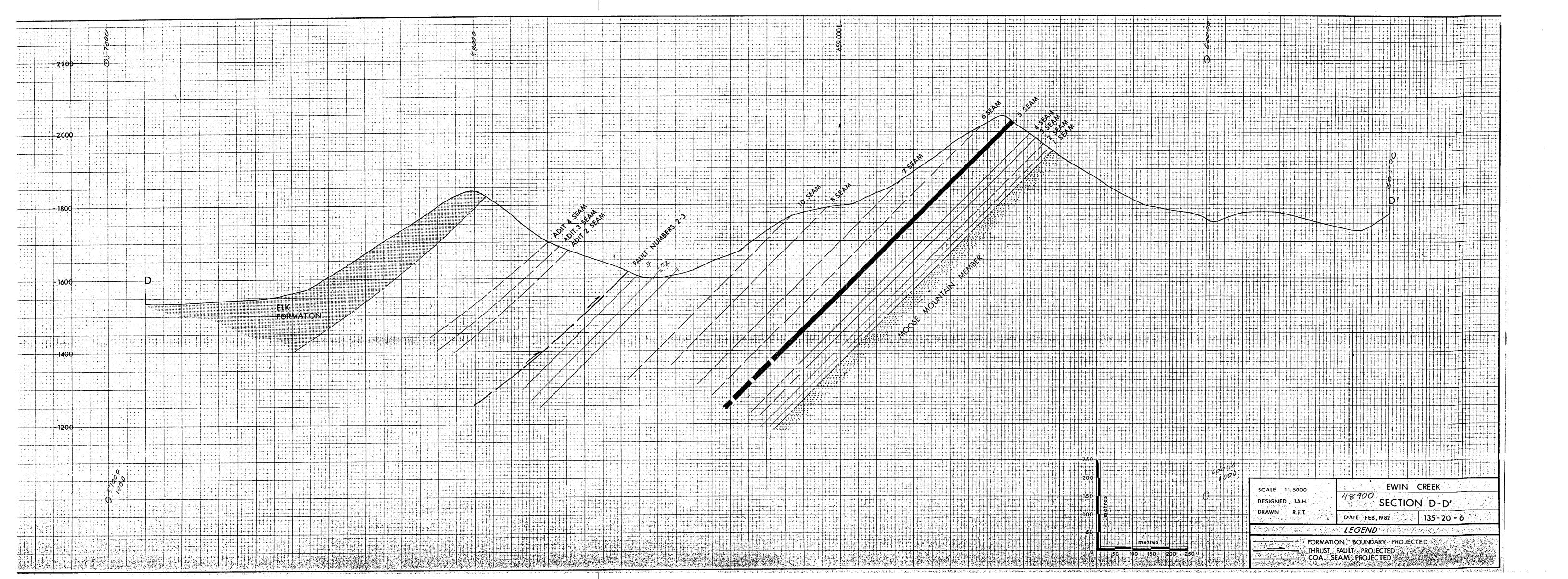
WEGETAED!	INTERCEPT 363.50- 364.39 INTERT THICKNESS 0.79 TRUE THICKNESS 0.72 24 LATITUDE 3346876.130 % DEPARTURE 659152.130 % ELEVATION 1255.560  00/00/00 WEIGHT 0.00 KG MOISTURE 0.0 % COMPLETE: 00/CO/00 MH DO YY COMPOSITE: SECOVERY 100.0 % WHID YY	# #
PROXIMATE ANALYSIS (DRY PASIS)   RAW *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEAR -   *CLEA	START OC 0.0 TIL - MAX. CONTRACTION TEMP. OC 407.0 FUSION TEMP. OC 0.0 TIL - MAX. CONTRACTION TEMP. OC 449.0 HAX FLUID TEMP. OC 0.0 TILL - HAX. BILATATION TEMP. OC 488.0 FINAL FLUID TEMP. OC 0.0 SGLIDIFICATION TEMP. OC 0.0 NELTING RANGE OC 0.0 NELTING RANGE OC 0.0 NELTING RANGE OC 0.0	
GROSS CAL, VALUE BTU/LB 7913, 8123, 19.4 (-1/8'+0 COAL FLOATED AT 1.50 S.B.)	1 PETROGRAPHIC DATA DATE COMPLETED 00/00/00 PELLET HUMBER 0  V-TYPES REACTIVE COMPONENTS INTEST COMPONENTS 1 TYPE Z TOTAL VITRINGID 54.3 INTEST SF. (1/2) 17.1	•
SIZE WT.Z ASHZ WT.Z ASHZ -1/4'+ 28M 0.0 0.0 0.0 0.0 0.0 -28M + 60M 0.0 0.0 0.0 0.0 -60M + 0 0.6 0.0 0.0 0.0	PETROGRAPHIC DATA DATE COMPLETED 00/00/00 PELLET NUMBER 0  V-TYPES REACTIVE COMPONENTS INERT COMPONENTS TYPE Z TOTAL VITRINGID 54.3 INERT SF. (1/2) 17.1  12 0.5 REACTIVE SF. (1/2) 17.2 MICRINGIDS 3.4  13 8.7 EXINGIB 2 RESIN 0.0 FUSINGIDS 4.1  14 41.8 MINERAL MATIER 3.9  15 3.3 TOTAL REACTIVES 71.5 TOTAL THERTS 28.5  0 0.0  0 0.0  MAX. MEAN REFL. OF VITRINGIDS (RO) 1.44  BAL. INDEX 1.79 STRENGTH INDEX 0.00 PRED. COXE STAB. INDEX 62.00	
WASHABILITY DATE RUN 00/00/00 (WF.X) S.G. DIRECT X FSI AND SIZE WT. ASH	CUN. Z +/- ,1   WASHABILXIY DATE RUM 00/00/00  CUN. Z +/- ,1   (WT.Z)	- ::::
( 0.0) FLT. 1.30 0.0 0.0 -1/4/+28N 1.40 0.0 0.0 0.0 1.50 0.0 0.0 1.50 0.0 0.0 1.70 0.0 0.0 SINK 1.70 0.0 0.0	G.O 0.0 0.0   (100.0) FLT, 1.30 0.0 G.O 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	• •
( 0.0) FLT. 1.30 0.0 0.0 -28M+60M 1.40 0.0 0.0		
( 0.0) FLT. 1.30 0.0 9.0 1.49 0.0 0.0 1.50 0.0 0.0 1.60 0.0 0.0 1.70 0.0 0.0 31NK 1.70 0.0 0.0	0.0 0.0 0.0   FROTH 0.0 0.0 0.0   CELL TEST 0.0 0.0 0.0   ( 0.0) FROTH 0.0 0.0 0.0 0.0 0.0 0.0   ( 0.0) FROTH 0.0 0.0 0.0 0.0 0.0 0.0   -60H + 0 TAILINGS 0.0 0.0	· · ·
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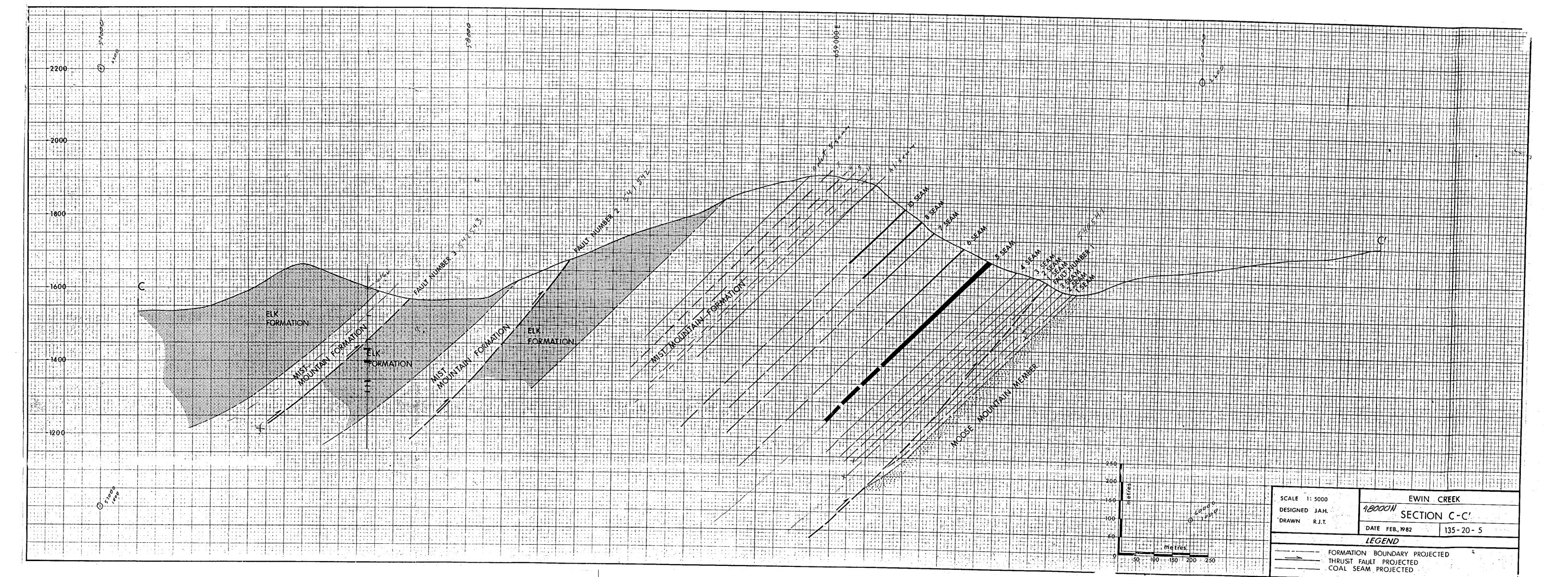
PRILL HOLE: EVISI (CORE ) SEAH VERTICAL THICKNESS 0.55 DIF ANGLE RECEIVED:	INTERCEPT 367.29- 367.84 INTERT THICKNESS 0.55 TRUE THICKNESS 0.50 N 24 LATITUDE 3546976.130 M DEPARTURE 657152.130 N ELEVATION 1251.870 H 00/00/00 WEIGHT 0.00 KB HEISTURE 0.0 Z COMPLETE: 60/00/06 WH DD YY COMPOSITE: RECOVERY 72.2 Z MX DD YY
	START OC 0.0 TI - SGFT, TEMP. CC 0.0  FUSION TEMP. OC 0.0 TII - HAX, CONTRACTION TEMP. GC 0.0  HAX FLUID TEMP. OC 0.0 TIII - HAX, DILATATION TEMP. GC 0.0  FINAL FLUID TEMP. OC 0.0  FINAL FLUID TEMP. OC 0.0  GOLIDIFICATION TEMP. OC 0.0  NEITING RAMGE OC 6.0  MAXINUM FLUIDITY OD/M  FETROGRAPHIC CATA DATE COMPLETED 00/00/00 PELLET HUNDER C
SCREEN ANALYSIS (COAL CRUSHED TO 1/4'  SIZE NT.X ASHX NT.X ASHX  -1/4'+ 28H 0.0 0.0 0.0 0.0 0.0  -28H + 60K 0.0 0.0 0.0 0.0 0.0  -60H + 0 0.0 0.0 0.0 0.0	TYPE X
WASHABILITY DATE RUN 00/00/00 (NT.X) S.O. DIRECT X FS.	WASHABILITY DATE RUN 00/00/00   CUN, Z +/1   (NT, Z)   S.C. BIRECT Z FSI CUN, Z +/1   NT, ASH S.G.   AND SIZE NT, ASH ST. GSH S.G.
-1/4'+28H 1.40 0.0 0.0 1.50 0.0 1.50 0.0 0.0 1.50 0.0 0.0 1.70 0.0 0.0 0.0 1.70 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0   -1/8'+0   1.40 0.0 0.0   0.0 0.0 0.0 0.0 0.0 0.0 0.0
( 0.0) FLT. 1.30 0.0 0.0 0.0 1.50 0.0 0.0 1.50 0.0 0.0 1.50 0.0 0.0 1.70 0.0 0.0 1.70 0.0 0.0 0.0 1.70 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 ( 0.0) FROTH 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.
( 0.0) FLT. 1.30 0.0 0.0 0.0 1.40 0.0 0.0 1.50 0.0 0.0 1.60 0.0 0.0 1.70 0.0 0.0 1.70 0.0 0.0 0.0 1.70 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0   FROTH 0.0 0.0 0.0   CELL TEST 0.0 0.0 0.0   ( 0.0) FROTH 0.0 0.0 0.0 0.0 0.0 0.0   -60H + 0 JAILINGS 0.0 0.0 0.0 0.0 0.0 0.0   -60H + 0 JAILINGS 0.0 0.0

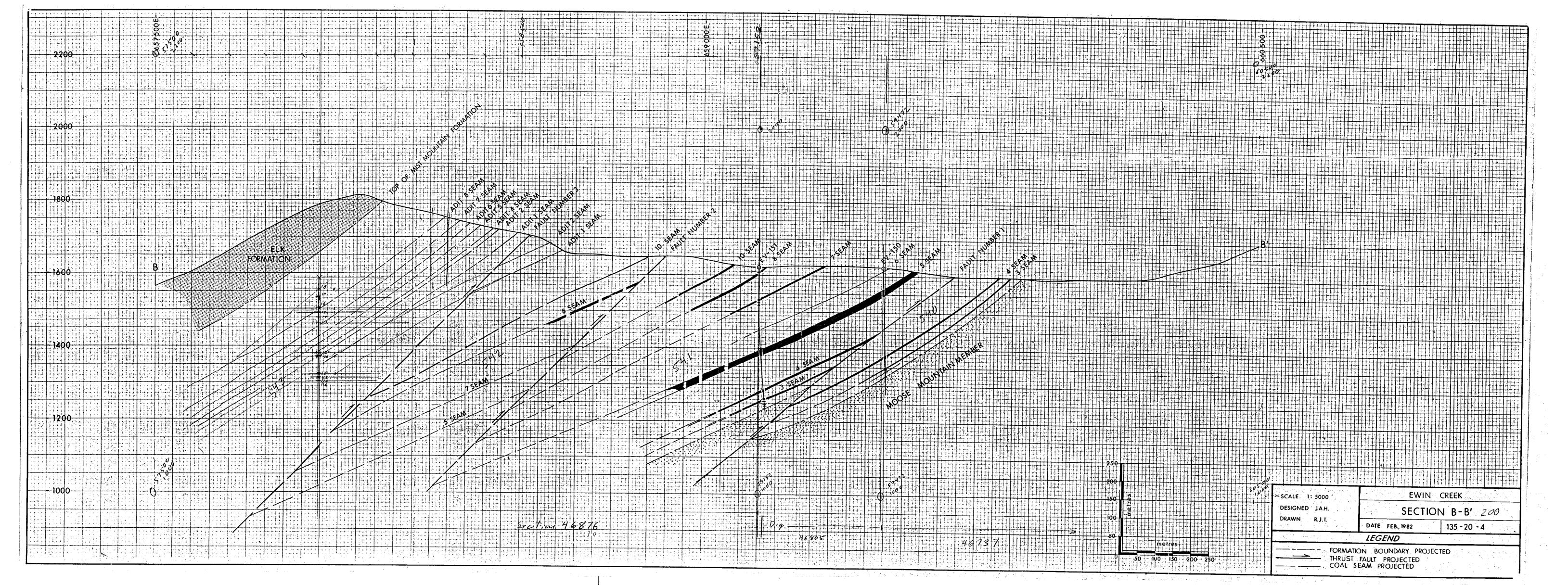
DRILL HOLE; EVI51 (CORE ) SEAN A PERTICAL THICKNESS 6.31 DIP ANGLE RECEIVED;	- INTERCEPT 376.43- 376.74 INTOPT THICKNESS 0.21 TRUE THICKNESS 0.28 K 24 LATTICUTE 5546876.130 N DEPORTURE 637152.130 M ELEVATION - 1242.730 M 00/00/00 WEIGHT 0.00 KG MOISTURE 0.0 % COMPLETE: CO/00/00 MM DD YY COMPGEITE: RECOVERY 0.0 % IN DB YY
PROXIMATE AMALYSIS (DRY BASIS)	BIEGELER PLASTICITY, DATE RUN 00/00/00   BILATATION (RUHR) / DATE RUN CC/90/00
### ##################################	BIEGELER PLASTICITY, DATE RUN 00/00/00   BILATATION (RUHR) / DATE RUN CC/00/00  START
U.M. I (DAF)	PETROGRAPHIC DATA DATE COMPLETED 00/00/00 PELLET NUMBER 0
SIZE WT.Z ASHZ WT.Z ASHZ -1/4'+ 25% 0.0 0.0 0.0 0.0 0.0  -28h + 60h 0.0 0.0 0.0 0.0 0.0  -60h + 0 0.0 0.0 0.0 0.0 0.0	V-TYPES REACTIVE COMPONENTS INERT COMPONENTS    TYPE X
DASHABILITY DATE RUN 00/00/60 (WT.Z) S.G. DIRECT Z FSI AND SIZE WT. ASH	CUM, Z +/- 1 1 (97.Z) S.C. DIRECT Z FSI CUM, X +/- 1 WT. ASH S.C. I AND SIZE ST. ASH ST. ASH S.C.
( 0.0) FLT. 1.30	0.0 0.0 0.0   (100.0) FLT. 1.3C 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.
( 0.0). FLT. 1.30 0.0 0.0 0.0 1.40 0.0 0.0 1.50 0.0 0.0 1.60 0.0 0.0 1.70 0.0 0.0 1.70 0.0 0.0 0.0 1.70 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	
( 0.0) FLT. 1.30 0.0 0.0 -60%+ 0 1.40 0.0 6.0 1.50 0.0 0.0 1.60 0.0 0.0 1.70 0.6 0.0	0.0 0.0 0.0   FR0(H 0.0 0.0 0.0   CELL TEST 0.0 0.0 0.0   ( 0.0) FR0TH 0.0 0.0 0.0 0.0 0.0 0.0   -40H + 0 TAILINGS 0.0 0.0 0.0 0.0
SINK 1.70 G.0 0.0 NOTES:	

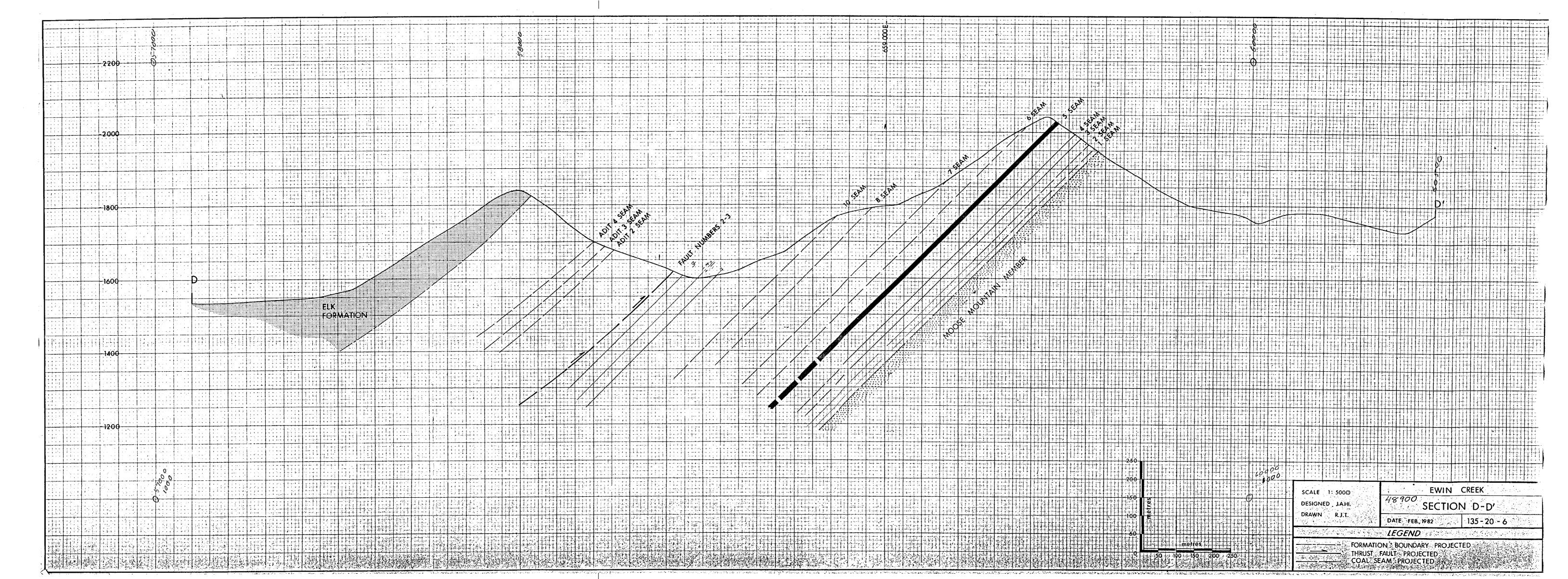


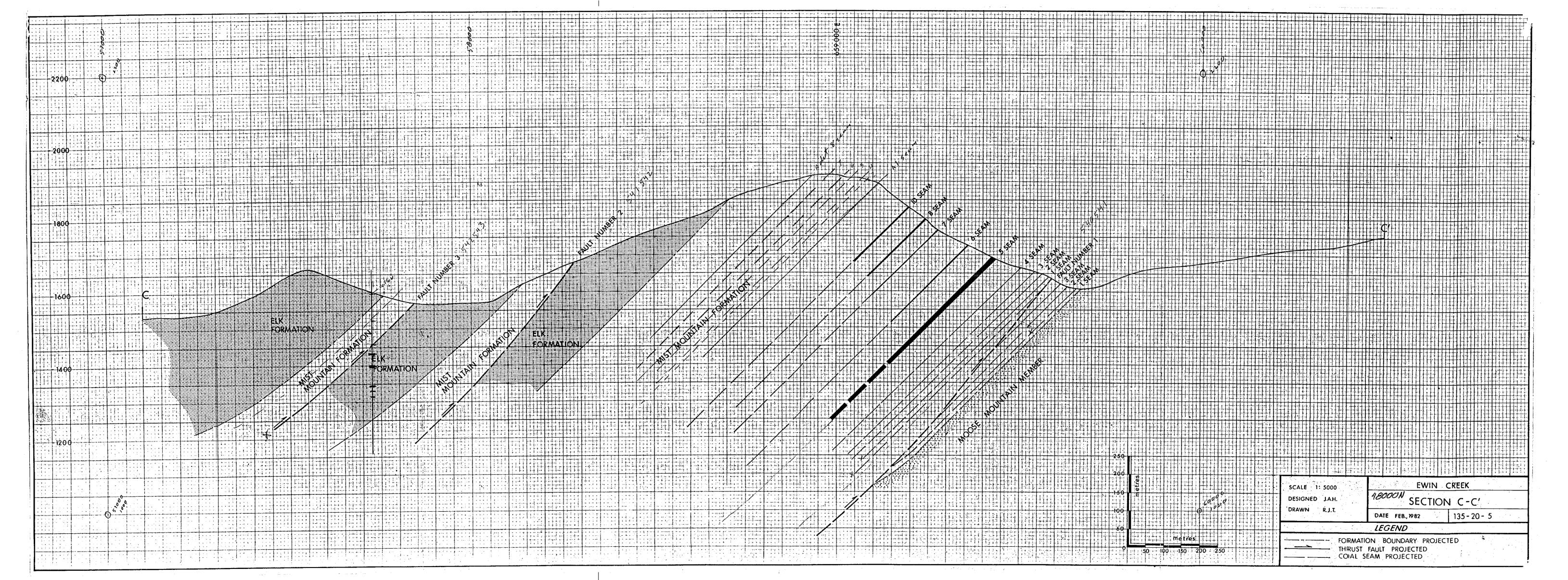


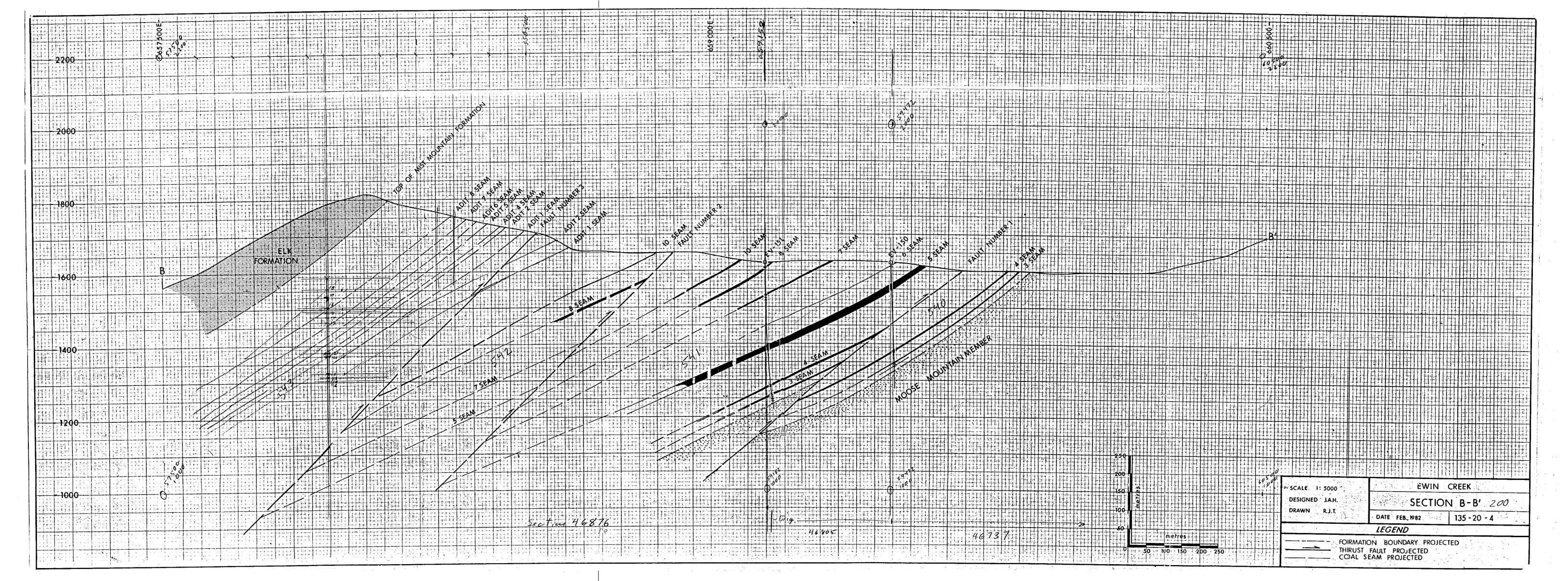


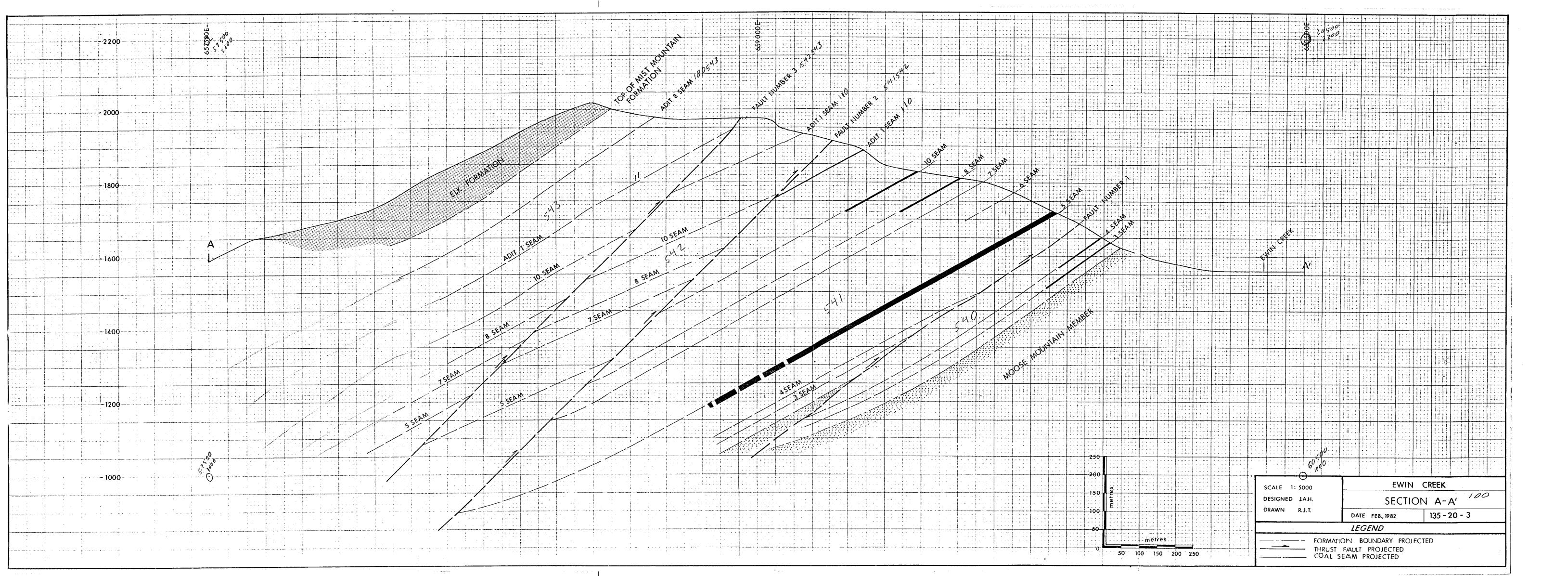


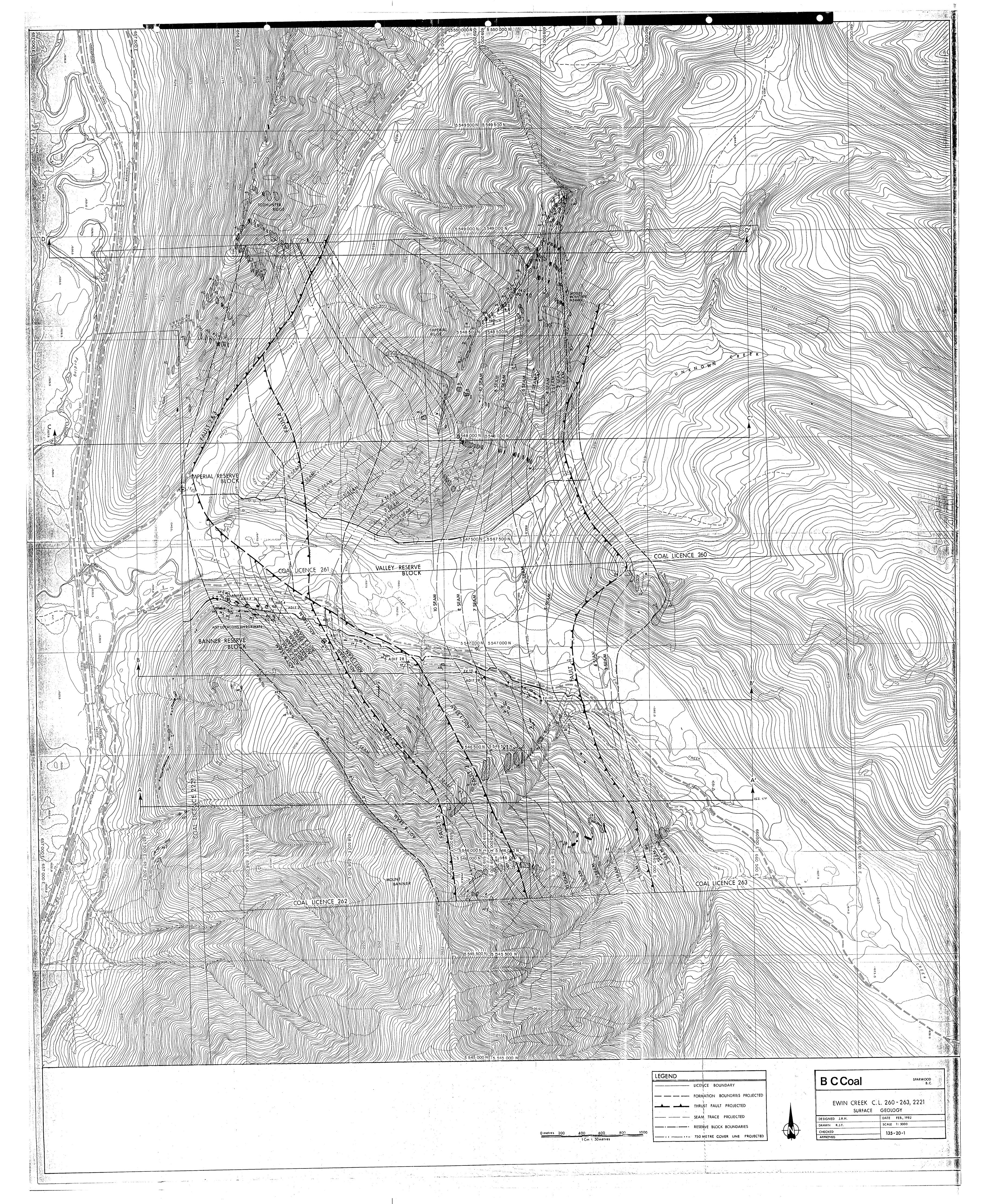


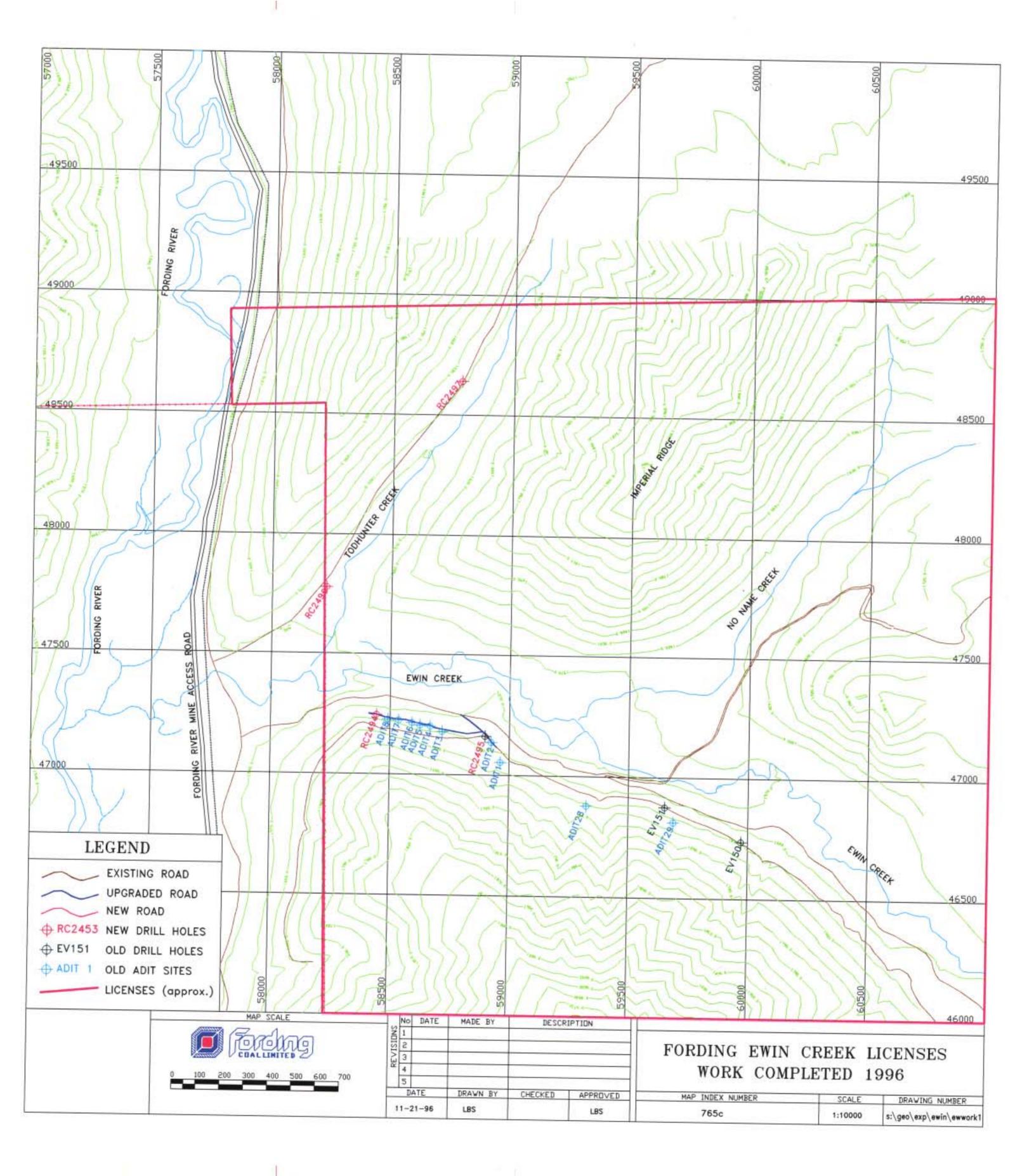


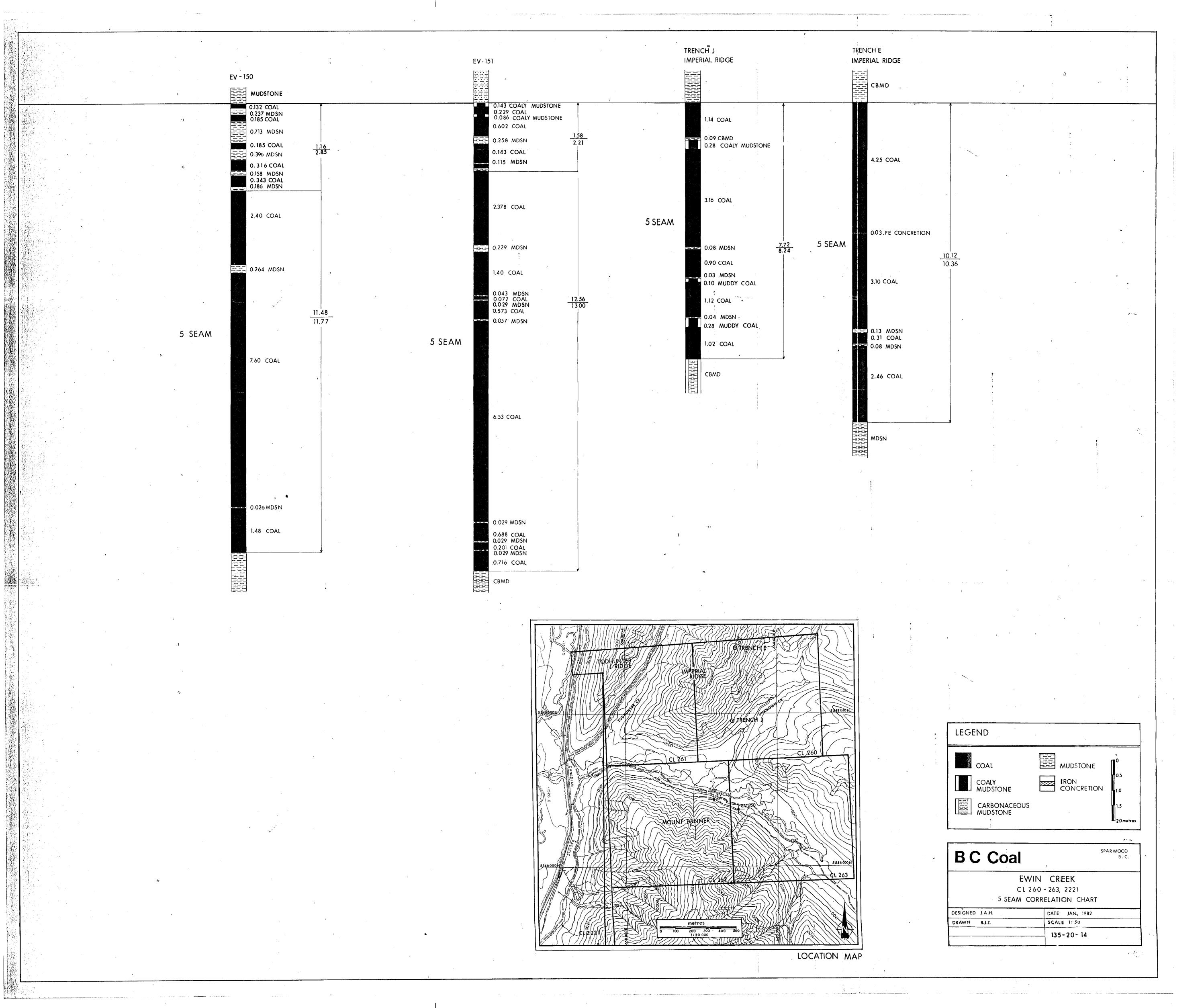


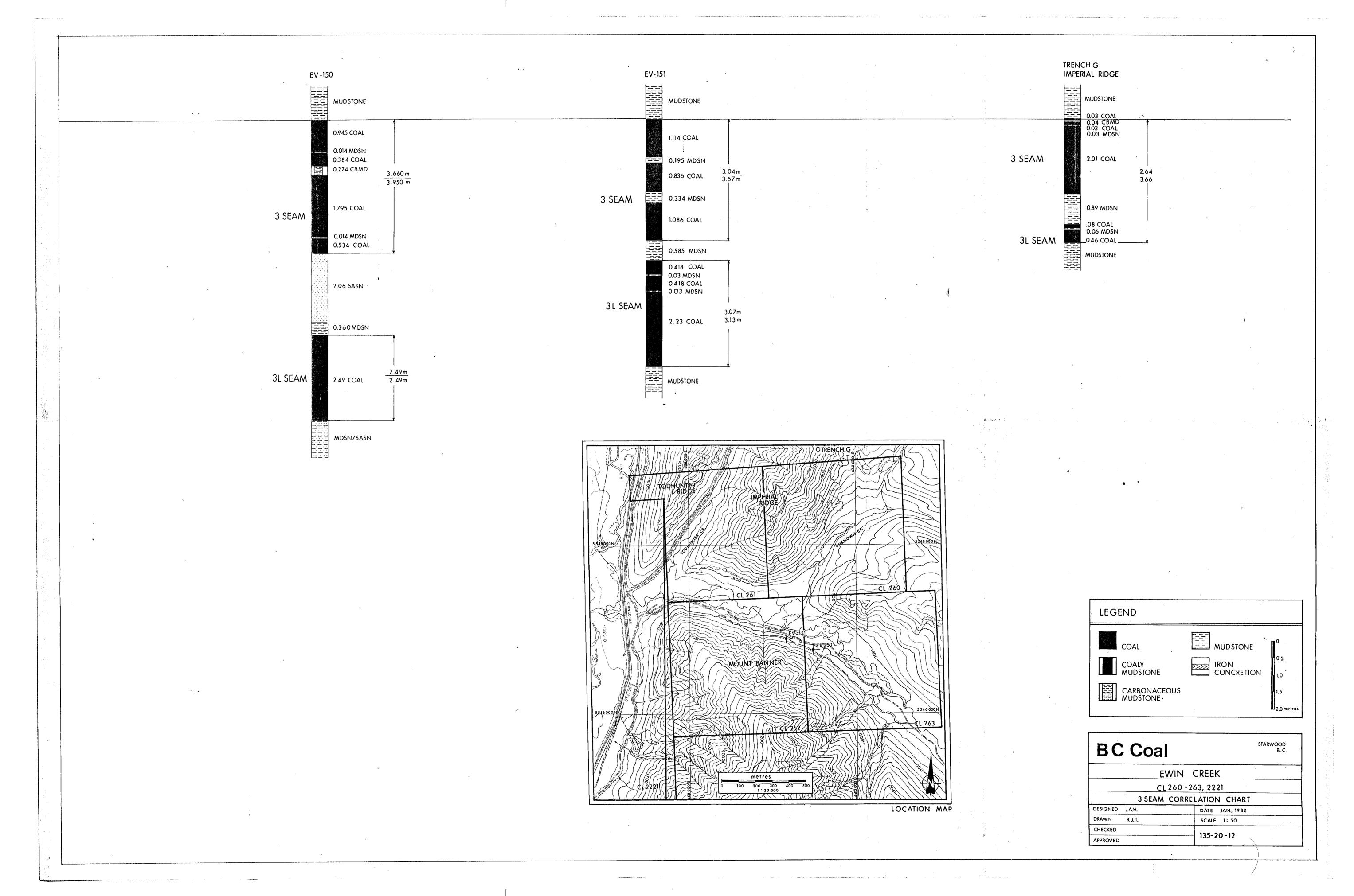


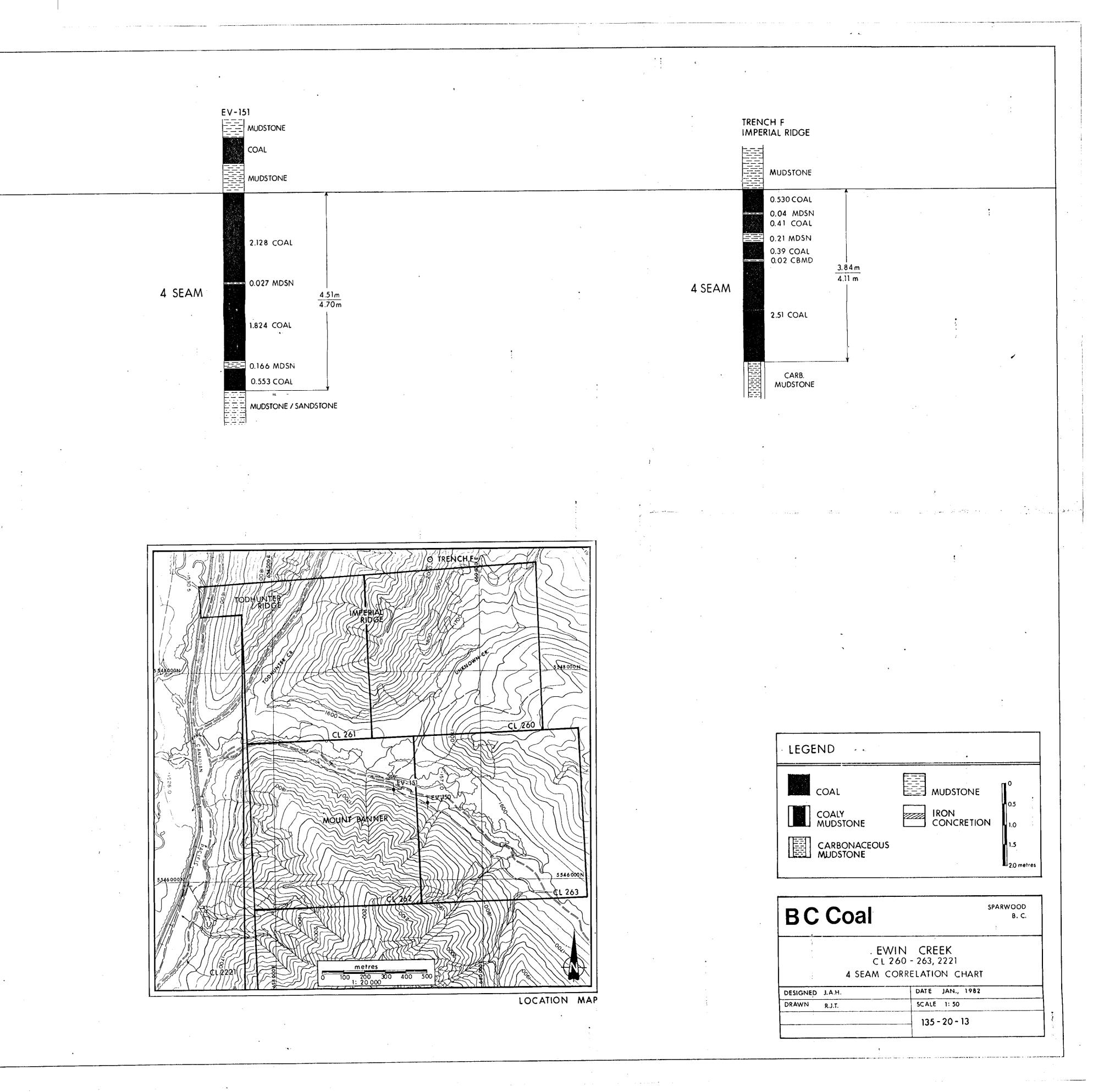












EV - 150

4 SEAM

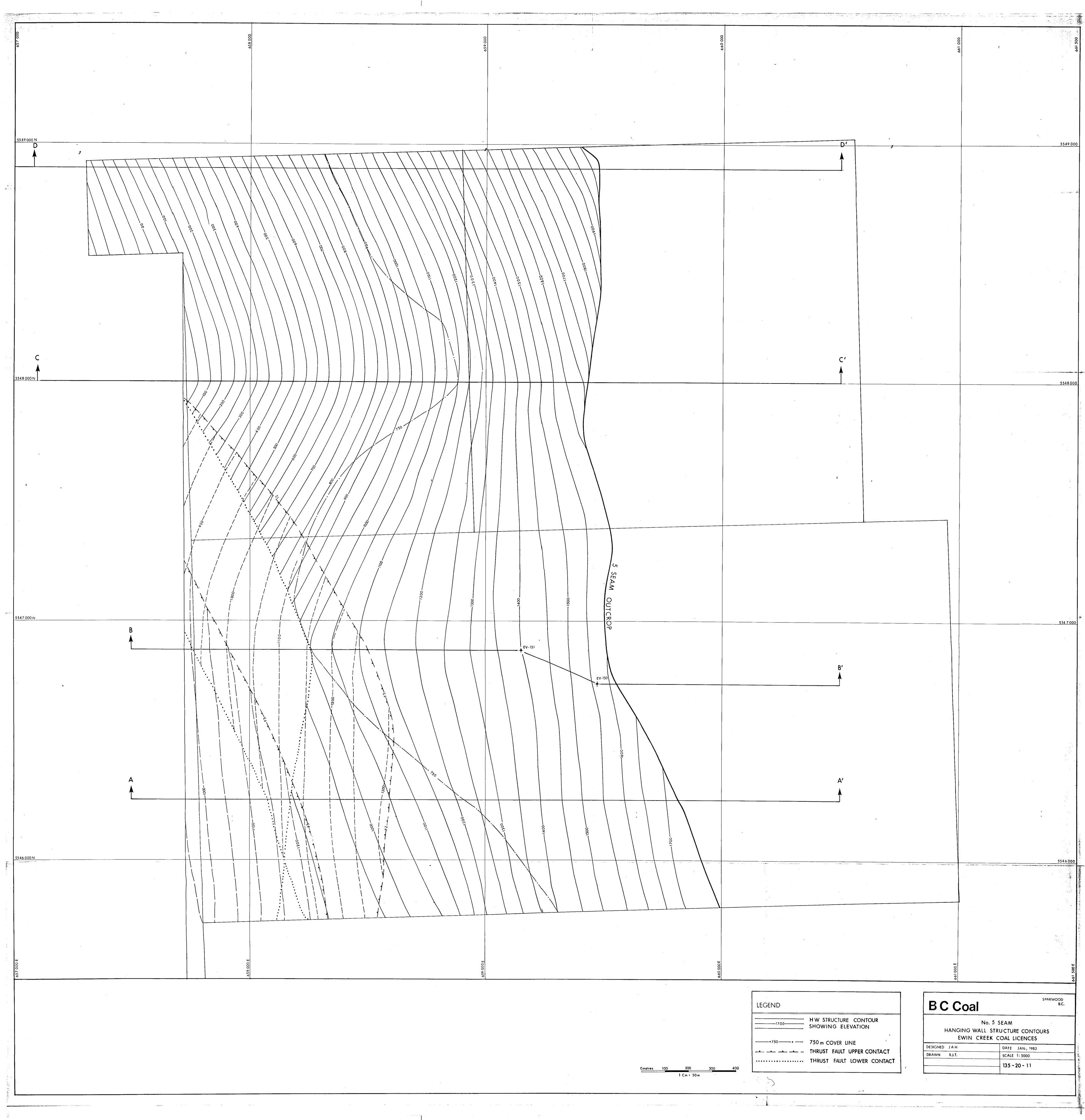
MUDSTONE

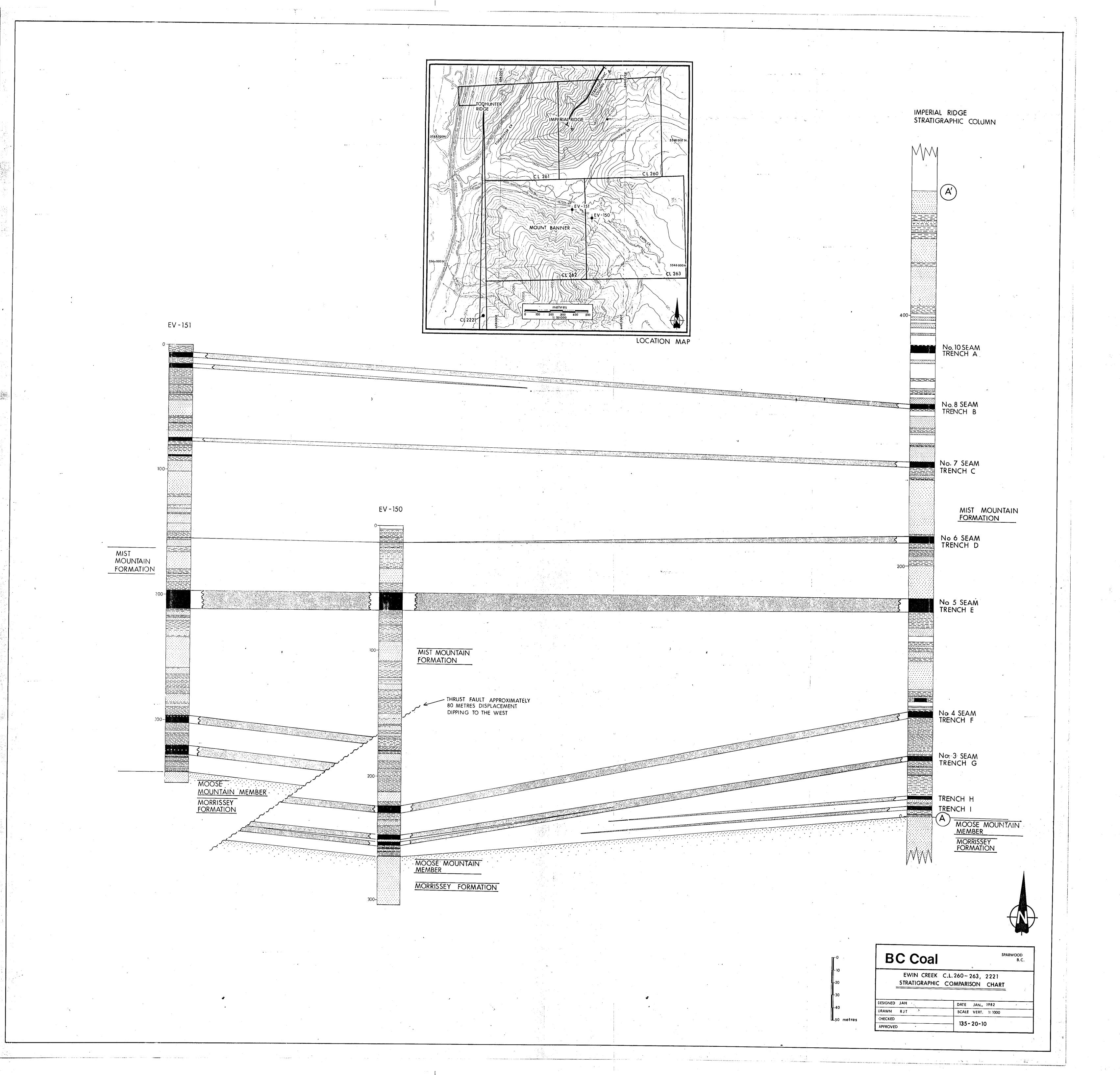
4.062 COAL

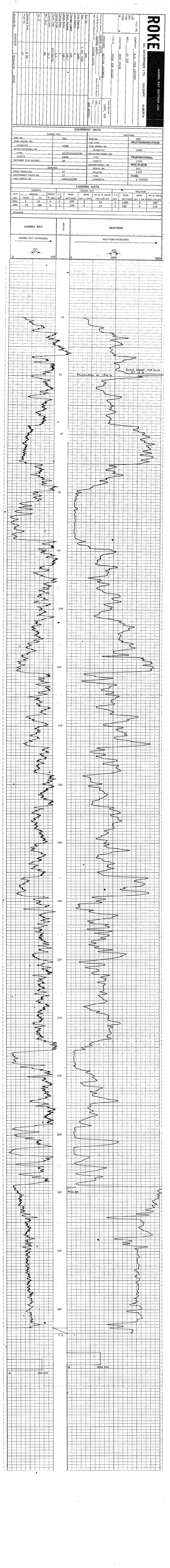
0.589 MDSN

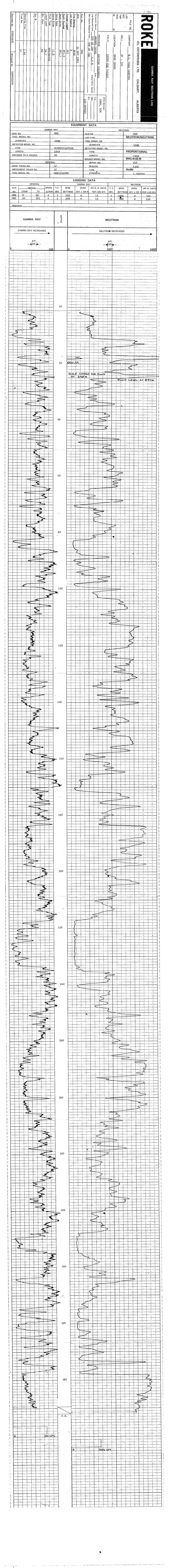
0.636 COAL 0.055 MDSN 0.304 COAL

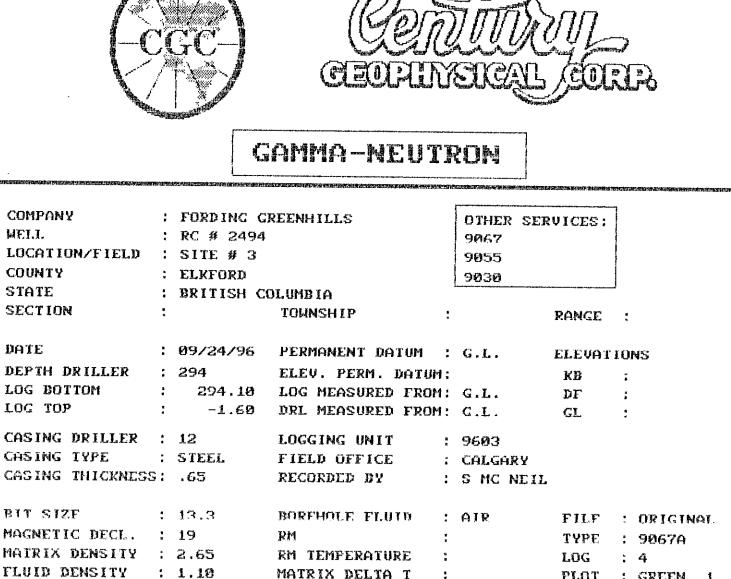
MUDSTONE









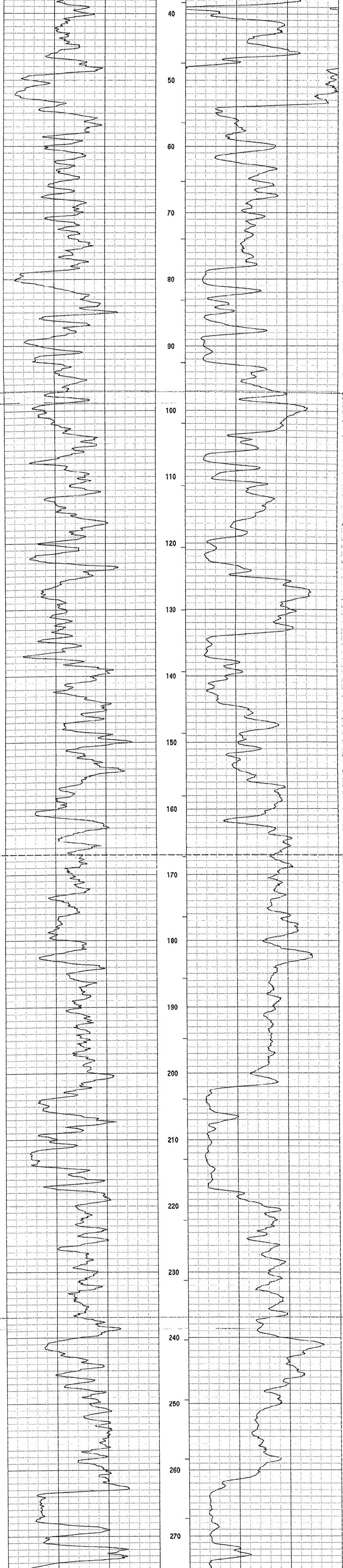


MELI.

STATE

DATE

CASING THICKNESS: .65 BIT SIZE MAGNETIC DECL. : 19 MATRIX DENSITY : 2.65 FLUID DENSITY : 1.10 MATRIX DELTA T : PLOT : GREEN 1 NEUTRON MATRIX : SANDSTONE FLUID DELTA T : THRESH: REMARKS HULE ANGLE 60 DEGREES 9067 , 0012 RUN THROUGH THE RODS , 9055 , 9030 RUN OPEN HOLE ALL SERVICES PROVIDED SUBJECT TO STANDARD TERMS AND CONDITIONS GAM(NAT) API-GR NEUTRON API-N 0 10 20 30 40 50 60 70 80 90 100 110



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PC

API-GR Gam(nat)

API-N NEUTRON



: FORDING CREENHILLS

COMPANY

## GAMA-NEUTRON

OTHER SERVICES: : PC # 2495 9067 LUCATION/FIELD : SITE # 4 9055 COUNTY : ELXFORD 9030 STATE : DRITISH COLUMDIA SECTION TOWNSHIP PANCE : DATE : 09/26/96 PERMANENT DATUM : G.L. **ELEVATIONS** DEPTH DRILLER : 313 ELEU. PERM. DATUM: KB LOG BOTTOM : 312.20 LOG MEASURED FROM: G.L. MF. LOG TOP : -1.60 DRL MEASURED FROM: G.L.  $\mathbf{GL}$ CASING DRILLER : 45 LOGGING UNIT : 9603 CASING TYPE : STEEL FIELD OFFICE : CALGARY CASING THICKNESS: .65 RECORDED BY : S MC NEIL BIT SIZE BOREHOLE FLUID : AIR : 13.3 FILE : ORIGINAL MAGNETIC DECL. : 19 RM TYPE : 9067A MATRIX DENSITY : 2.65 RM TEMPERATURE LOG : 8 FLUID DENSITY : 1.10 MATRIX DELTA T : PLOT : GREEN 1 THRESH: PEMARKS HOLE ANGLE 60 DEGREES 9067 , 0012 RUN THROUGH THE RODS , 9055 , 9030 RUN OPEN HOLE ALL SERVICES PROVIDED SUBJECT TO STANDARD TERMS AND CONDITIONS

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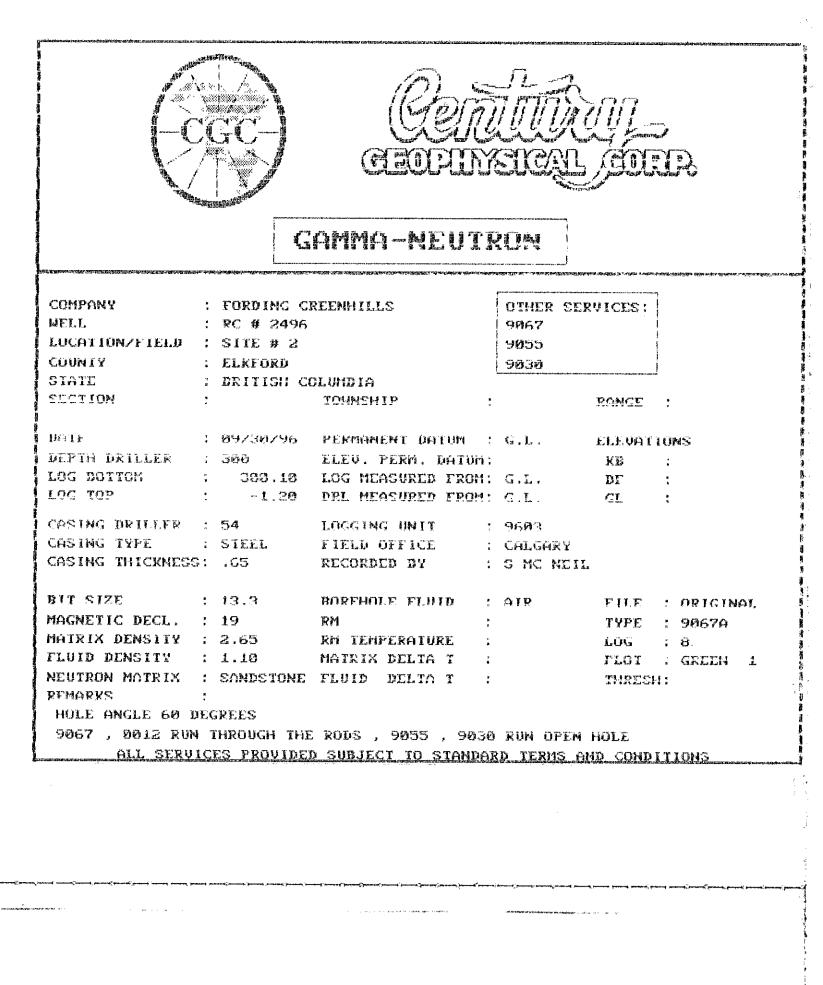
API-UK GAM(NAT)

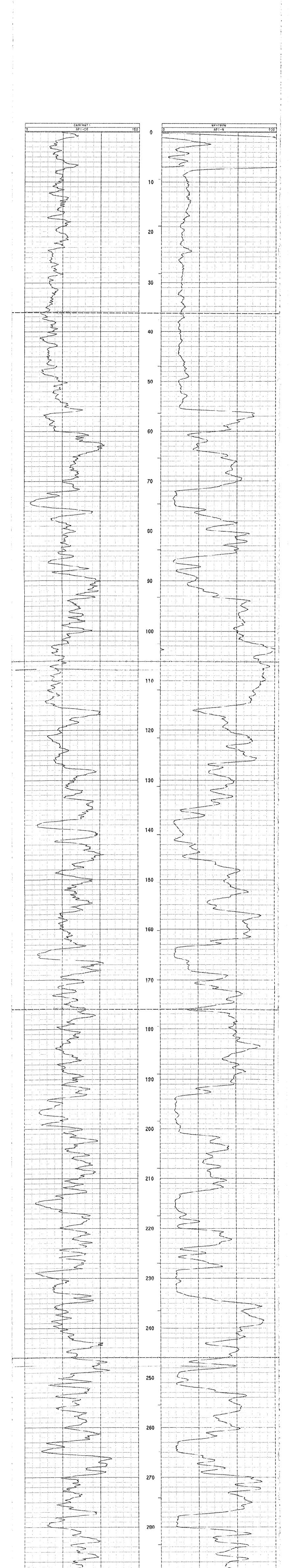
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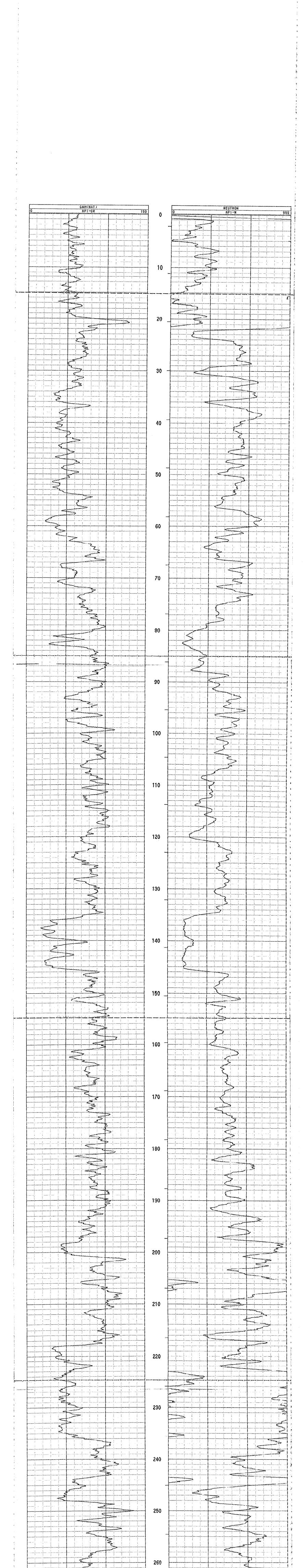


COMPANY



## : FORDING CREENHILLS OTHER SERVICES:

MELT. : RC # 2497 9067 LOCATION/FIELD : SITE # 1 9055 COUNTY : ELXFORD 9030 STATE : BRITISH COLUMBIA SECTION TOWNSHIP RANGE : : 10/03/96 PERMANENT DATUM : G.L. ELEVATIONS DATE DEPTH DRILLER : 282 ELEV. PERM. DATUM: KB : LOG BOTTOM : 202.00 LOG MEASURED FROM: G.L. Dr LOC TOP : -1.20 DRL MEASURED FROM: C.L. GL CASING DRILLER : 24 LOGGING UNIT : 9603 CHSING TYPE : STEEL FIELD OFFICE : CALGARY CASING THICKNESS: .65 RECORDED DY : S MC MEIL BORFHOLE FLUID : AIR FUF : ORIGINAL BIT SIZE : 13.3 MAGNETIC DECL. : 19 RM TYPE : 9067A MATRIX DENSITY : 2.65 RM TEMPERATURE : roe : 5 FLUID DENSITY : 1.10 MATRIX DELTA T ; PLOT : GREEN 1 NEUTRON MATRIX : SANDSTONE FLUID DELTA T : THRESH: REMARKS 9067 , 0012 RUN THROUGH THE RODS , 9055 , 9030 RUN OPEN HOLE ALL SERVICES PROVIDED SUBJECT TO STANDARD TERMS AND CONDITIONS



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10/03/96

API-GR GAM(NAT)

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API-N NEUTRON