#875

Fording River Operations

Summary Report

2000 Exploration Program

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Statements of Author's Academic and Professional Qualifications

The author of this report, K.A. Komenac, in 1973 received the degree of Bachelor of Science (Geology Major) from the University of British Columbia, and is registered as a Professional Engineer with the Association of Professional Engineers and Geoscientists of the Province of British Columbia. The author has been an employee of Fording Coal Limited at the Fording River Operation since November of 1973, as Assistance Pit Geologist, Exploration Geologist, Senior Exploration Geologist, and since 1989, Senior Geologist.

SCHEDULE C

PROVINCE OF BRITISH COLUMBIA	MINISTRY OF ENERGY AND MINES		TITLE PAGE OF ASSESSMENT REPORT
GENERAL NATURE OF WO	ORK		TOTAL COST
Exploration			\$220,000
Author of Landsman		Signature (s)	Jen Juna
K.A. Komenac (P. Eng.)			
Date report filed	. 12/2001	Year o	f work2000
Property Name Fordir	ng River Operations		
Coal type (if applicable)	Medium to High Vol	atile Bituminous	
Mining DivisionFort S	Steele Long	itude <u>114º 5</u>	2'
	Latitu	ide <u>50º 12</u>	,
Coal Licence Numbers; Coa	al Leases; Freehold	BC Coal Leas	e #1 and 9
Owens (s)			
(1) Fording Coal Limited			
PO Box 100, Elkford	, BC V0B 1H0		
Operator (s)			
(a)			
Same			
References to Previous Wo	rk		
Annual Assessment Repo	rts Since 1970		

Fording River Operations

Summary Report

2000 Exploration Program

I. Introduction

1. General Geography and History

The Fording River Coal property is located in the Fording River and Upper Elk Valleys, approximately 25 kilometres north of Elkford, BC. Access is by paved road north from Elkford along the Fording River Valley, or north along the Elk River Valley via the Forestry Service gravel road or the Kan-Elk Powerline road.

The Fording River minesite is situated within the front range of the southern Canadian Rocky Mountains. At least ten major coal seams, generally greater than four metres thick, are contained in the Mist Mountain Formation of the Kootenay Group.

The Elk River portion of the property was actively explored by the Canadian Pacific Railway Company in the period 1902 - 1908. Until 1947, the property was comprised of 10,276 hectares in 40 Crown Granted Lots. In that year, the holdings were reduced to 2,979 hectares in 15 Crown Granted Lots. In 1967 and 1968, Canadian Pacific Oil and Gas reacquired part of the coal lands which had been abandoned in 1947. At the present time, the Fording River Property consists of 20,304 hectares, held on seven Coal Leases, and 15 Crown Granted Lots.

Mining operations which commenced in 1971, have produced more than 137.0 million tonnes of clean metallurgical and thermal coal for markets in North and South America, Africa, Europe and Asia. Of this total, 9.0 million tonnes were produced in 2000.

Reference:

i) Illustration No. 1A: Index Map - Coal Properties

2. Geology

i) Stratigraphy

The general stratigraphic succession on the Fording River Property is summarized in the following table:

Period	Litho-Stratigraphic Units			Principal Rock Types
Recent			• •	Colluvium
Quatemary				Clay, silt, sand, gravel, cobbles
Lower Cretaceous			Blairmore Group	Massive bedded sandstones and conglomerates
			Elk Formation	Sandstone, siltstone, shale, mudstone, chert pebble
	к			conglomerate, minor coal
	0	M	ist Mountain Formation	Sandstone, siltstone, shale, mudstone, thick coal
Lower	0			seams
	Т		Moose Mountain Member	Medium to coarse grained quartz-chart sandstone
Cretaceous	E	MF		
	N	00		
to	A	RR		
	Y	RM		
Upper		I A		
	G	sт	Weary Ridge Member	Fine to coarse grained, slight ferruginous quartz-chart
Jurassic	R	S I		sandstone
	0	ΕO		
	υ	YN		
	Р			
Jurassic		F	ernie Formation	Shale, siltstone, fine-grained sandstone
Triassic	····	Spi	ay River Formation	Sandy shale, shale quartzite
· · •		Rock	y Mountain Formation	
Mississippian			Rundle Group	Limestone

The oldest rocks present on the Fording River property are the Rundle Group limestones, located on the west bank of the Fording River, near the southern property boundary. They are in faulted contact with the Kootenay Group to the west, and unconformable contact with Rocky Mountain Formation quartzites to the north. The latter are best exposed on the eastern slope of the Brownie Creek Valley. The Fernie Formation shales occur throughout the area, generally along the sides of the valleys on the lower flanks of the mountains. The shales are recessive and, therefore, poorly exposed. The Fernie Formation is in conformable contact with the Morrissey, through the "Passage Beds," which are a transitional zone from marine to non-marine sedimentation.

The Morrissey Formation, which is the "basal sandstone" of the Kootenay Group, is a prominent cliff-forming marker horizon in many locations. On the Fording River Property, the top of the Moose Mountain member (Morrissey Formation) is in sharp contact with #1 or A seam, the lowermost bed of the Mist Mountain Formation.

The Mist Mountain Formation contains all of the economic coal seams, and is the most widely occurring formation on Fording River Property. This economically important formation is an interbedded sequence of sandstones, siltstones, silty shales, mudstones, and medium to high volatile bituminous coal seams. The volatile content of the coal increases up section, with decreasing rank. Lenticular sandstones comprise about 1/3 of the Mist Mountain sediments at Fording River, but very few laterally extensive sandstone beds exist.

The sandstone above and below seam #4 (B) and above #9 (F), are the most persistent units, and are often cliff-forming marker horizons.

The Mist Mountain Formation is generally overlain conformably by strata of the Elk Formation. On the Fording property, this formation is commonly a succession of sandstones, siltstones, shales, mudstones, chert pebble conglomerates and sporadic, thin, high volatile bituminous coal seams. The coal seams are characterized by a high alginate content and referred to as "Needle" coal. The Elk Formation is observed near the tops of the mountains, mainly on the east side of the Elk Valley on the Greenhills Range, and northward to the Mount Tuxford areas.

The top of the Elk Formation marks the upper boundary of the Kootenay Group, which is unconformably overlain by the basal member of the Blairmore Group. This thick bedded, cliff-forming sandstone and conglomerate unit is observed on the upper slopes of Mount Tuxford.

ii) Structure

Subsequent to deposition, the sediments were involved in the mountain building movements of the late Cretaceous to early Tertiary Laramide orogeny. The major structural features of the Fording River property are the north-south trending synclines with near horizontal to steep westerly dipping thrust faults, and a few high angle normal faults. Some of the thrust faults probably were folded late in the tectonic cycle.

The formation of the major fold structures began early in the tectonic cycle. In the current mining area, two asymmetric synclines are evident; the Greenhills Syncline to the west, and the Alexander Creek Synclines to the east of the Fording River.

The thrust faulting (ie: the Ewin Pass and Brownie Ridge Thrusts), was probably contemporaneous with the later stages of folding. The intervening anticline was subsequently faulted (Ericson Fault), then eroded.

The Alexander Creek Syncline can be traced from the southern property boundary on Castle Mountain to the northern end of the property on Weary Ridge. The strata of the west limb, on the west face of Eagle Mountain, dips easterly at 20 to 25[°], decreasing gradually to zero as the axis is approached. The east limb, however, attains a 20[°] westerly dip within a much shorter (500m) distance of the axis. This asymmetry is possible due, at least in part, to the influence of the Ewin Pass Thrust which subcrops 600 to 800 metres east of the synclinal axis. Further to the east, on Brownie Ridge, the strata dips westerly at a mean dip of 42°. The Brownie Ridge Thrust, which subcrops near the crest of the ridge, probably contributes to this steepening.

Within the mining area, the axis of the Alexander Creek Syncline plunges to the north at an average of 4[°]. Turnbull Mountain exhibits a localized series of an echelon fold structures, plunging both to the north and south. These subsidiary folds may be related to thrust faulting. From the south end of Mount Tuxford, the synclinal axis continues north-northwest along the base of Mount Veits and into the Elk River Valley near Aldridge Creek.

On Mount Tuxford, the beds exposed are those of the Elk Formation and the overlying (non-coal bearing) Cadomin Formation. The area has not been extensively explored. The stratigraphic sequence of the east limb, in the more extensively explored Mist Mountain strata near Aldridge Creek (Elco property), closely resembles the east limb strata found on Henretta Ridge, ten kilometres to the south.

On the northwest corner of Eagle Mountain, the lower Kootenay-upper Fernie section is the locus for a zone of near horizontal thrust faulting. The effect is to cause a double repetition of the lower coal seams and basal sandstone on the west synclinal limb. This fault zone is synclinal in form, and continuous with the Ewin Pass Thrust zone found the east limb.

The Greenhills Syncline in the mining area, is essentially a "mirror-image" of the Alexander Creek structure. The east limb of the asymmetric syncline dips westerly at 15 to 25° , except in areas near the Ericson Fault, where 45 to 55° dips are common. The west limb exhibits much steeper dips; commonly in the 35 to 45° range. The Greenhills Syncline plunges northward (340 to 350°), at less than 5° , then apparently dies out to the north in the area of the Osborne Creek Depression.

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The Ericson Fault, which locally runs along the base of the Greenhills Range west of the Fording River, is one of the major regional faults. From south to north, this westerly dipping (40 to 70°) normal fault, brings Mist Mountain strata progressively into contact with Rundle, Rock Mountain, Spray River, Fernie and Morrissey strata. The downthrown block is to the west.

Near the south end of Lake Mountain, the Ericson Fault beings to "splay" into two zones. The main fault runs along the eastern margin of Lake Mountain, and the subsidiary fault runs to the west, and appears to "die out" northward. The steep northward dip exhibited in the Lake Mountain strata could be due to influence from these flanking "splays" of the fault. The flat lying region to the north of Lake Mountain (Osborne Creek Depression area) is completely void of outcrop, and the Ericson Fault has not been traced either through or to the north of this area.

Reference:

i) Illustration No. 1b: General Geology Map

3. Summary of Work Done in 2000

Seven reverse circulation drill holes were completed for a total of 2,845 metres. Geological field mapping was conducted by staff geologists on Turnbull Mountain.

Rotary drilling was done by SDS Drilling using an Ingersol Rand TH100.

All holes were geophysically logged through the rods using the gamma-neutron method. Holes that remained open after the rods were pulled were logged for hole deviation, and selected holes were logged for gamma-density. Logging was done by Century Geophysical Corporation.

Coal seams encountered by rotary drilling were samples in 0.5m intervals. Representative composite samples for each coal seam encountered in the hole were prepared at Fording's Process Plant Laboratory. Each seam composite was tested for proximate analysis, % Sulphur and Free Swelling Index. Samples from selected seam composites were sent to David E. Pearson and associates for petrographic analysis.

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Fording Coal Limited staff laid out the access road the drillsite locations. Pre-logging and stashing was done by Raymond Myles Contracting Limited. Road and drillsite construction was done by Elkford Industries Ltd. Staff surveyors provided the required survey control and drillhole pickups.

The following table shows the drillhole locations with respect to Coal Lease and Licence boundaries:

Lease / Licence	<u>Drillholes</u>
BC Coal Lease #1	RH # 2730, 2731, 2732, 2733
BC Coal Lease #9	RH # 2734, 2735, 2736

Reference:

i) Illustration No. 2: 2000 Exploration Program

II. Individual Area Programs

1. West Turnbull Area

ii) Objectives

The objective of the drilling program in West Turnbull was to obtain additional location, thickness and quality data, particularly for seams 7, 5 and 4 (220 block) in the area to the east of and deeper than the current highwall design.

ii) Summary of Work Done

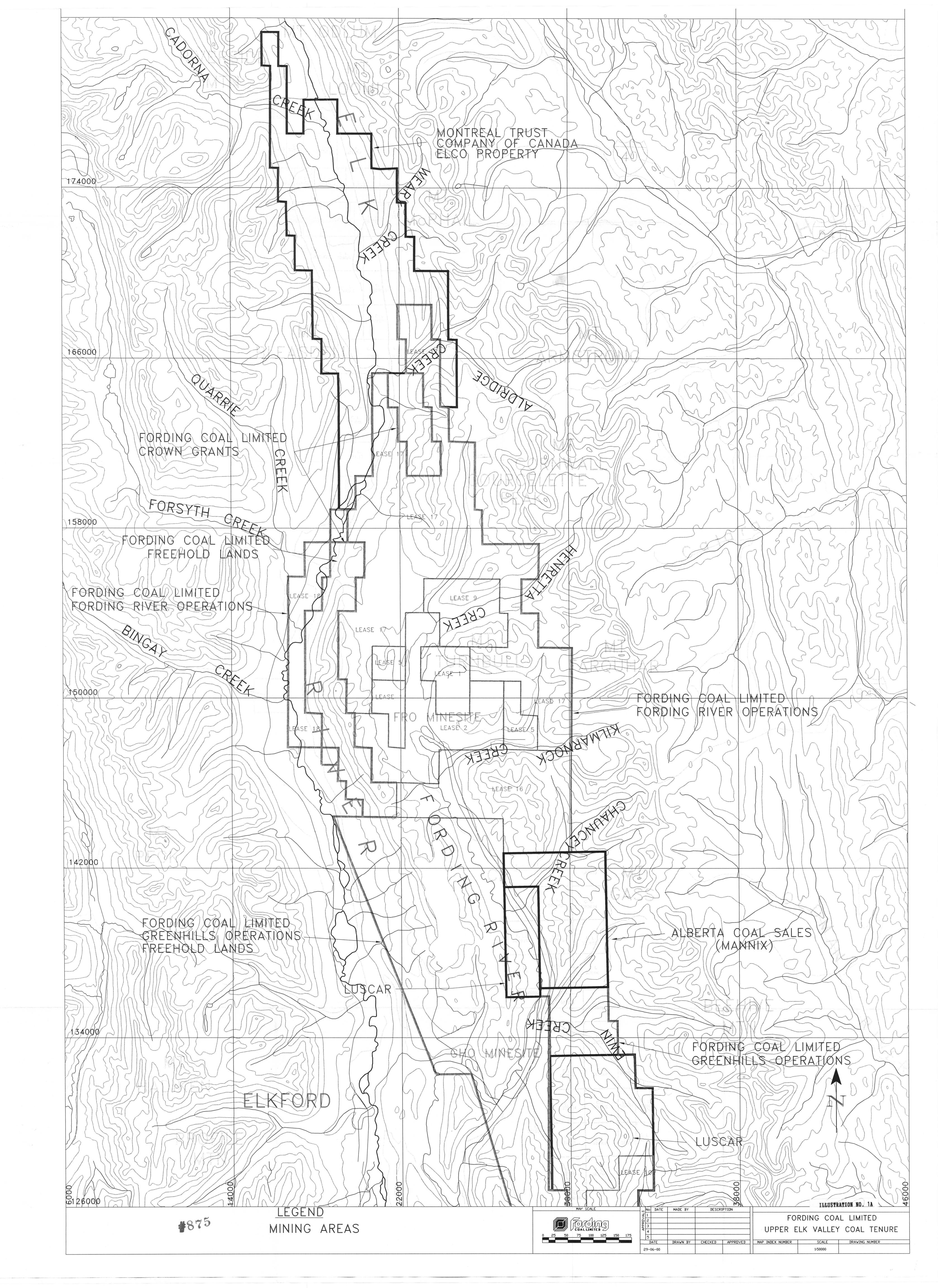
Seven holes were completed for a total of 2,845 metres. All holes were geophysically logged through the drill pipe using the gamma-neutron method. All but one hole (RH #2735) were also logged open hole using the gamma-density and deviation tools.

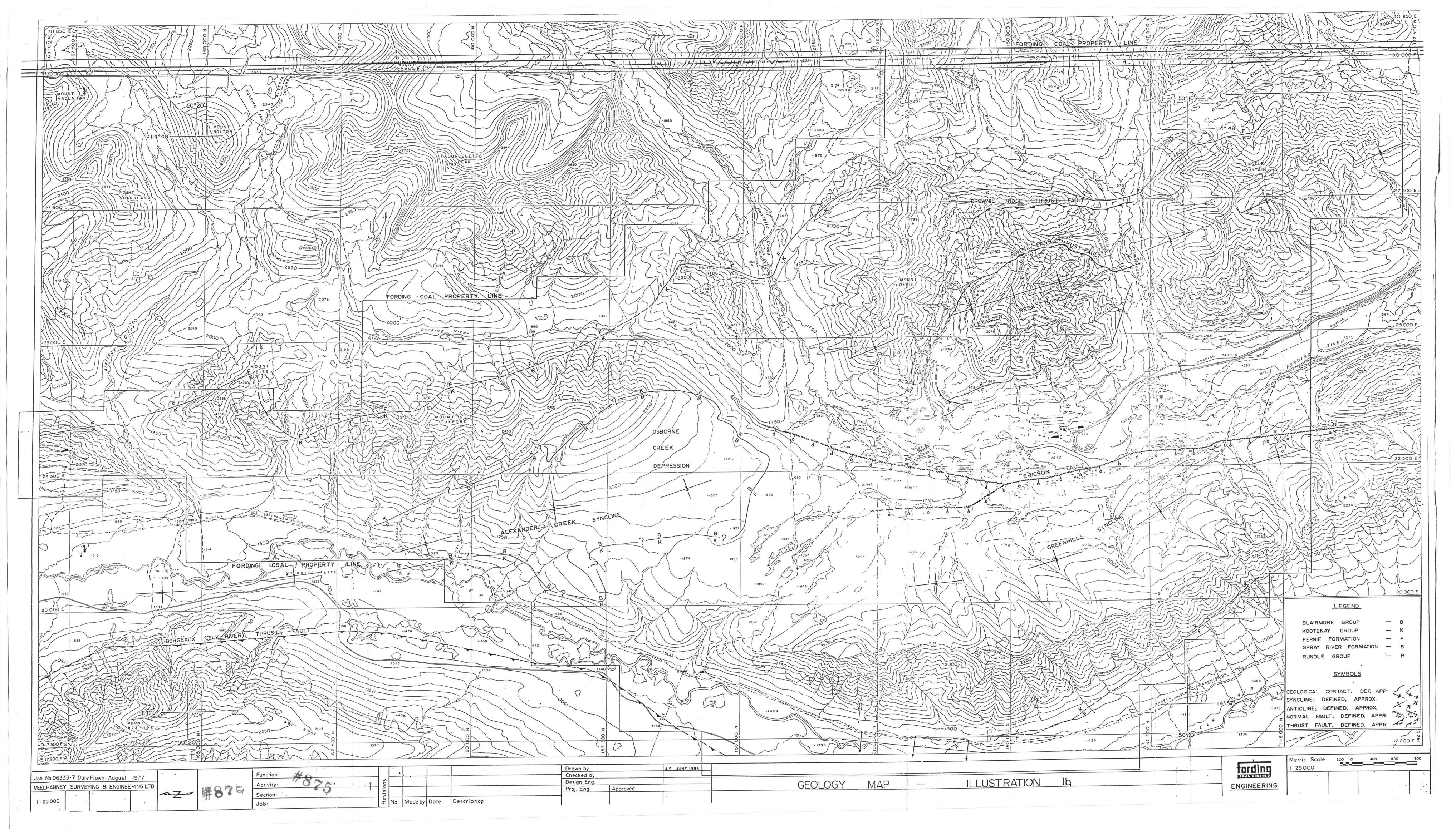
iii) Results and Conclusions

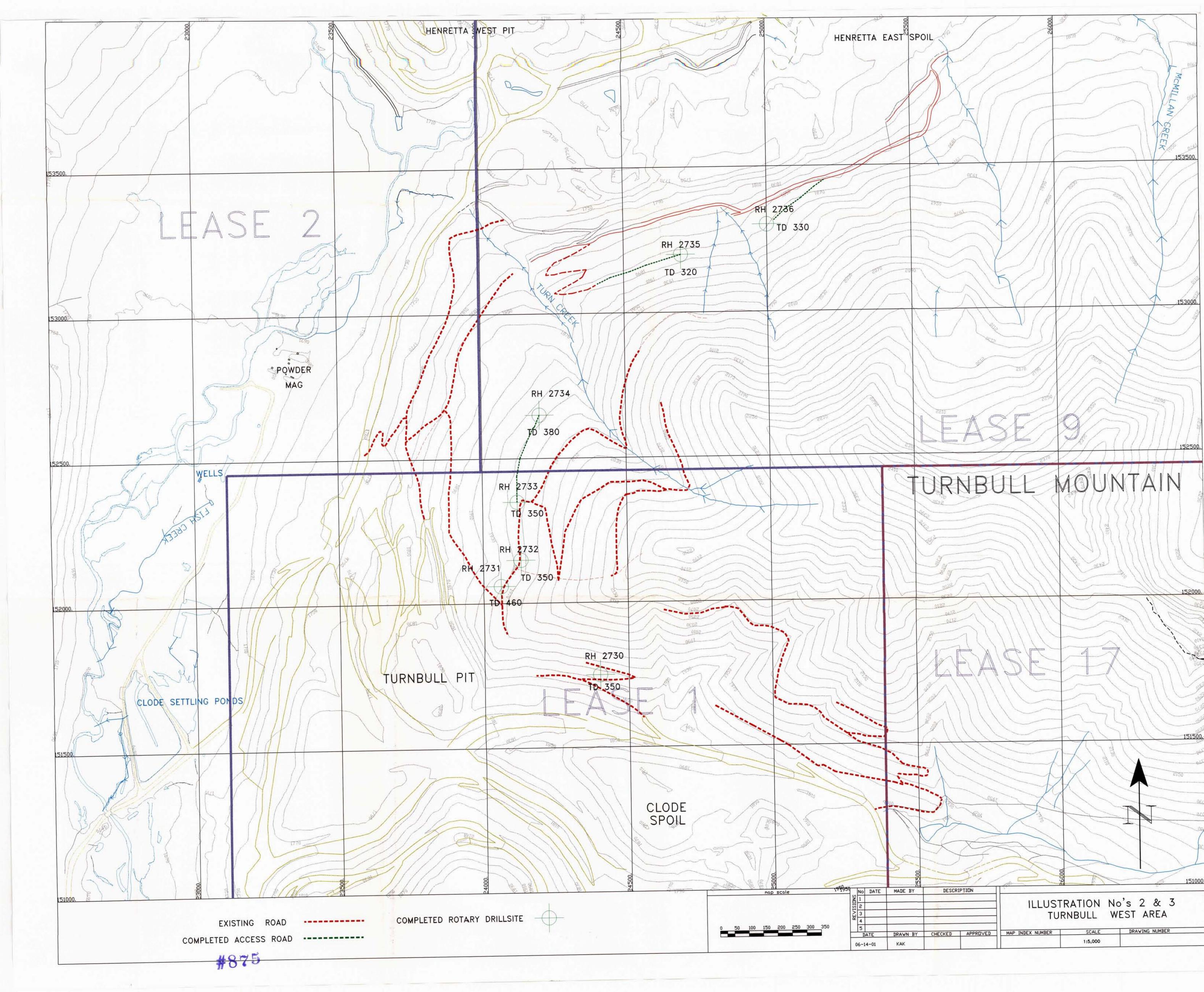
Of the seven reverse circulation rotary holes drilled in the area, two holes were stopped short of the required depth because of caving ground conditions. Of the five holes that reached their proposed depth, four holes intersected at least #7 seam. Additional drilling (2001) is required to finalize the ultimate pit limits for Turnbull West Pit.

References:

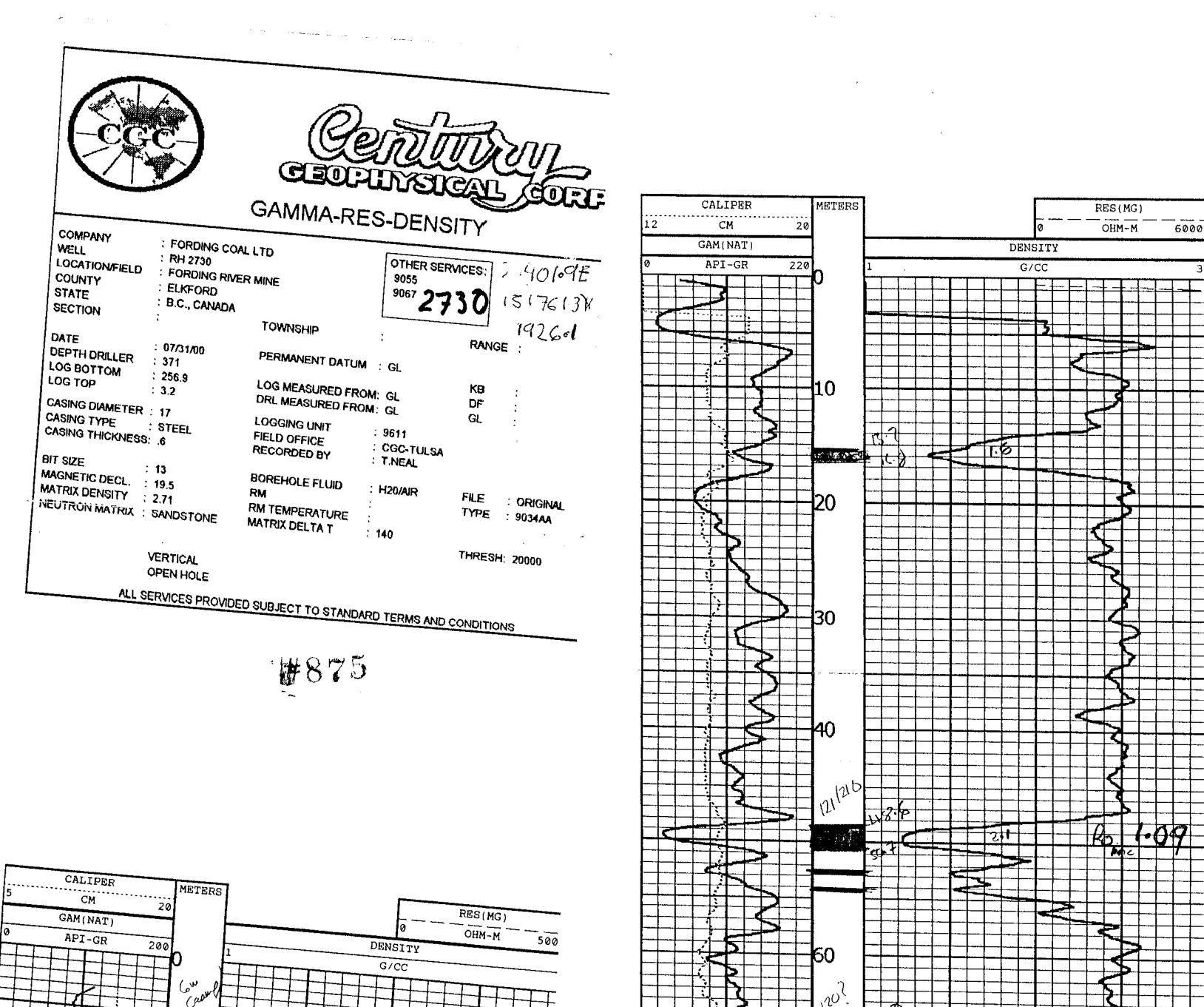
- i) Illustration No. 3: West Turnbull Area Program
- ii) Appendix 1: Drillhole Logs
- iii) Appendix 2: Sample Analyses

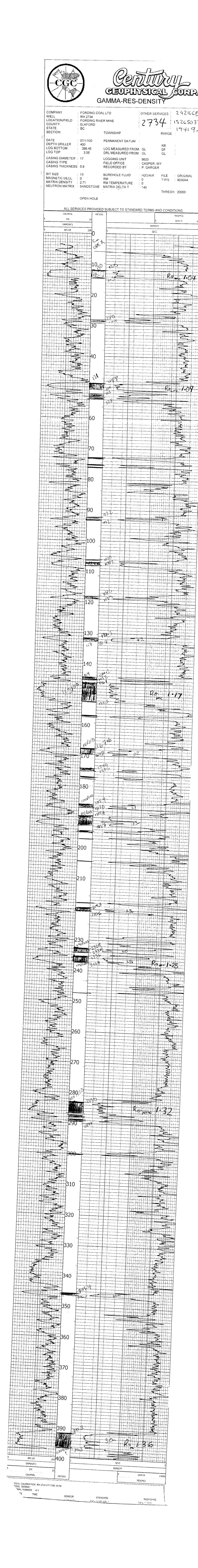






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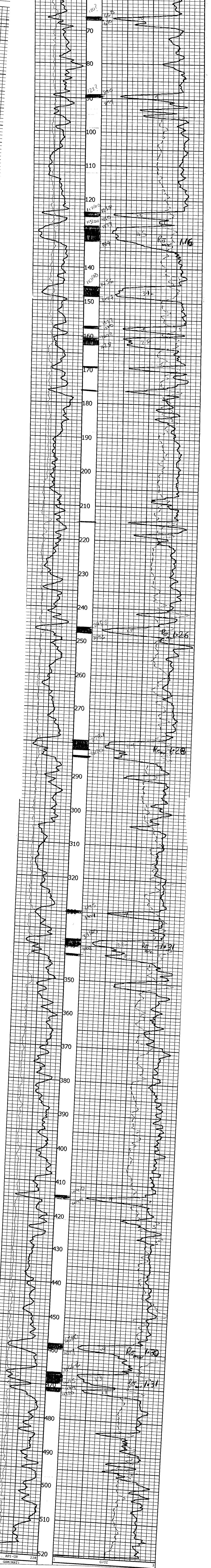




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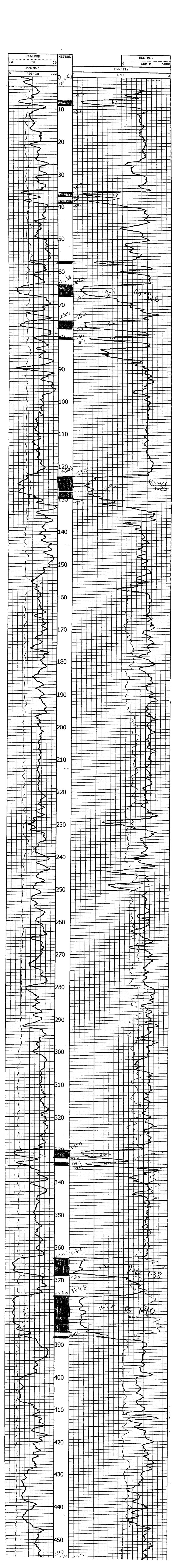


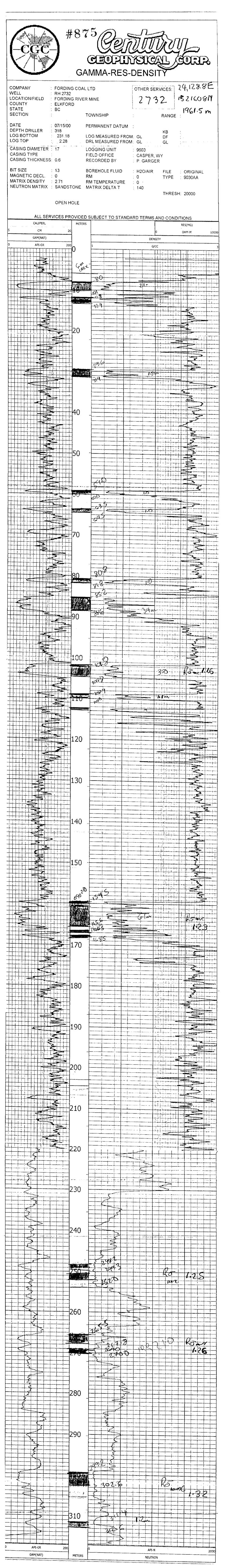
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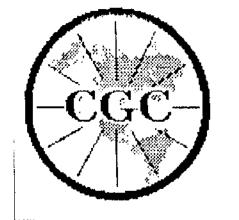
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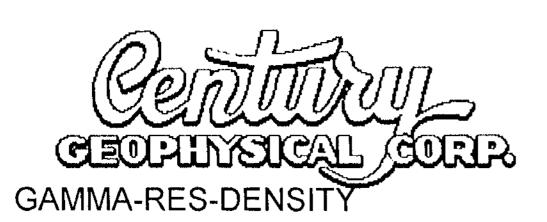
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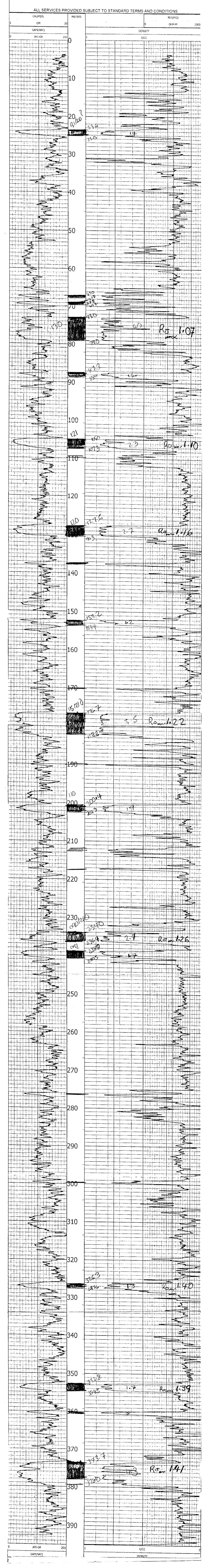
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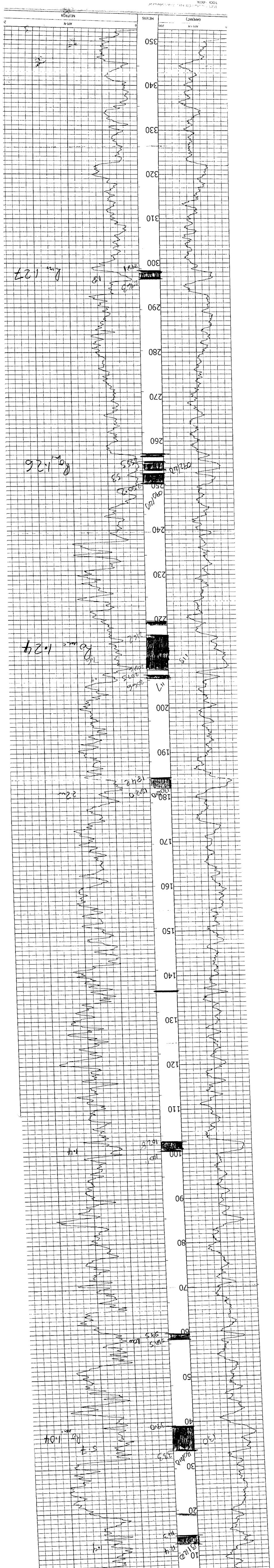




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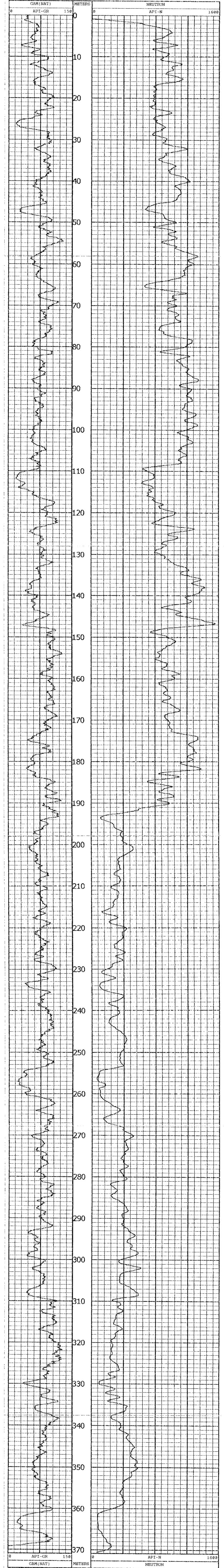


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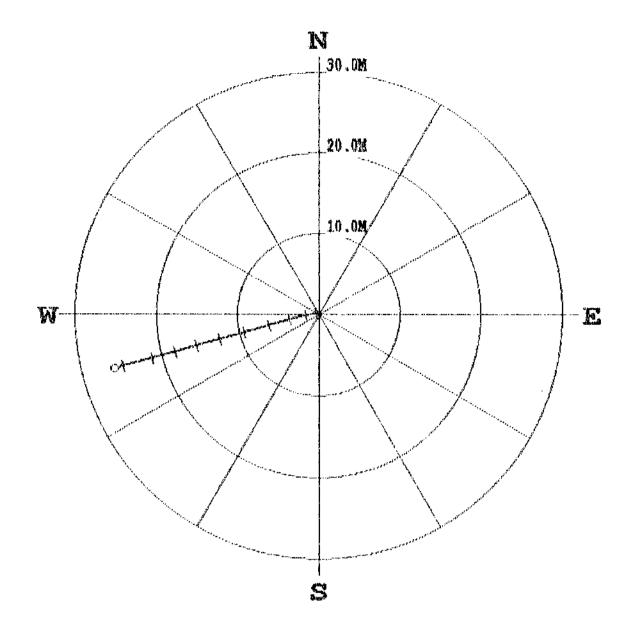
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PLAN VIEW COMPU-LOG DEVIATION

CLIENT: FORDING COAL LTD LOCATION: FORDING RIVER MINE HOLE ID: RH 2730 DATE OF LOG: 07/31/00 PROBE: 9055A 33



SCALE: 10 M/CM TRUE DEPTH: 255.16 M AZIMUTH: 255.1 DISTANCE: 26.0 M + = 25 M INCR • = BOTTON OF HOLE



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26.9	26.89	0.69 0.67 0.62 -0.03 -0.07	-0,49	0.5	279.1	2.5	
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131.9	1.51.30	-7 43	-0.05	10.3	256.1	1117 A 41	
136.9	136.34	-2.64	-10.55	30.9	955 6	7.0	
141.9	141.37	-2.MD	-9,95 -10,55 -33,15	10.9 11.5	255.9 255.9	7.1	
146,9	146.27	-2.96	-11.74	12.1	255.9	7.1	
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161.9	161.15		· · · · · ·		255.0	6.6	
166.9	166.12	-3.59	~ 14,09 - 14,09 ~14,65	14.5	255.7	6.2	261
371.9	171.08	-3.74	~14.65	14.5 15.1	255.7 255.7	6.6	2 42
176.9	176.05	~3,91	-15.19	15.7	2.55.6	6.1	2.50
DDL 9	101.02	-4.04	-15.70	16.2	255.6	6.4	2.50
186.9	105.99	~4.19	-16.20	16.7	255.5	6.3	2.50
191.9	190.97	ન્ય હુલ્ય	-16.72	17.3	255.5	6.3	247
196.9	195.93	-4.48	-17,25	17.9	255.4	6.9	260
801.9	200.90	~4,63	~17.83	18.4	255.4	7.0	2.56
206.9	205.96	-4.77	-19,39	19.0	255.4	6.6	250
211.9	210.93	-4.93	-18.94	19.6	255.4	6.6	\$ 50
216.9	23.5.80	~5,09	-19.46	20.1	255.4	6.2	2 60
221.9	250115	-5.22	-20.01	20.7	255.4	7.0	244
226.9	225.73	~5.38	-20.60	21.3	255.4	7.2	256

225.73

230.69

335.64

240.59

245.52

250.45

255.37

~5,39

-5.55

~5.73 -5.93

-6.14

~6,34

-6.61

-20.60

~21.23

-21,91

~22.61

-23,39

-24.20

~25.01

21.3

21.9

22.6

22.4

24.2

25.0

25.9

255.4

255.4

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255.2

226.9

231.9

236.9

243.9

246.9

251.9

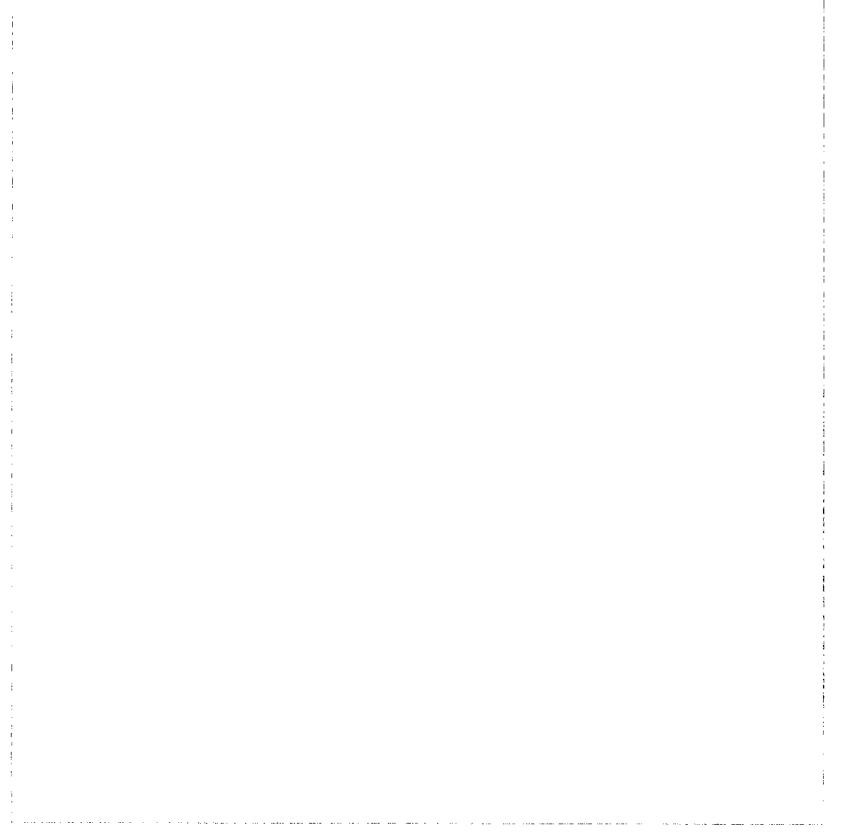
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* * * * * * * COMPU-LOG - VERTICAL DEVIATION * * * * * * * CLUSNE : FORDING COM LTD BOPR ID 101 5530 PIRED OFFICE : COC-THESE DATE OF LOSS : 07/31/00 DATE FROM : 90554 , **PROBE** 33 MAG. DECL. DEPTH UNITS : RETERS : 19,500 LOG: 882730_07-31-50_62-07_90558_,10_6,90_258,60_DBV1,109 CABLE DEPTH TRUE DEPTH NORTH DEV. EAST DEV. DISTANCE ASIAUTH SAME SANGE 257.7 256.16 ~6.67 -25.11 26.0 255.1 8.4 226.2



256.3

254.5

261.5

9.0 250.3

9.5 257.0

9.6 249.5

10.1 246.9

7.2

7.9

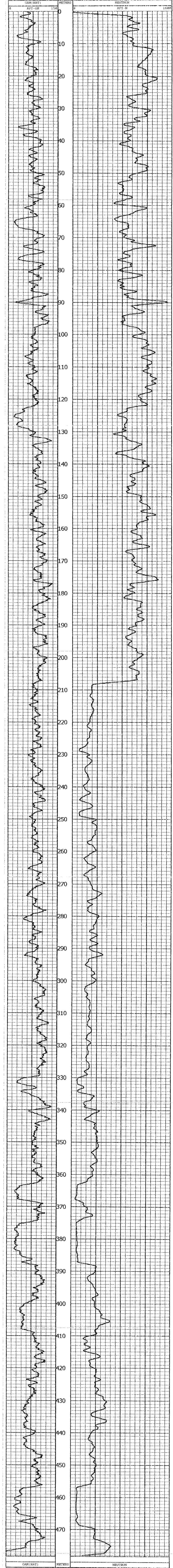
8.2

CCCC		Certi CERTI RH 27:		the second	72 Jaires
WELL :	FORDING COAL L' RH 2731 FORDING RIVER ELKFORD	TD	OTHER SERVIC 9034 9055	1997 - 19	#875
STATE : SECTION :	B.C., CANADA	TOWNSHIP		RANGE	
DEPTH DRILLER :	08/02/00 478 478.20 -1.00	PERMANENT DATUM LOG MEASURED FROM DRL MEASURED FROM	GL	KB DF GL	
CASING DIAMETER :	17 STEEL		: 9611 : CGC+TULSA		
BIT SIZE : MAGNETIC DECL. : MATRIX DENSITY : NEUTRON MATRIX :	2.71	RM RM TEMPERATURE	: 1-120/AIR : : : 140	FILE TYPE	: ORIGINAL : 9067A

THROUGH DRILL PIPE

ALL SERVICES PROVIDED SUBJECT TO STANDARD TERMS AND CONDITIONS

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PLAN VIEW COMPU-LOG DEVIATION

SCALE: 25 M/CM CLIENT: FORDING COAL LTD LOCATION: FORDING RIVER MINE TRUE DEPTH: 474.48 M HOLE ID: RH 2731 AZIMUTH: 262.9 DATE OF LOG: 08/03/00 DISTANCE: 35.2 M PROBE: 9055A 33 + = 100 M INCR MAG DECL: 19.5 \circ = bottom of hole N 175.0M 50.0M 25.0M/ E W Q S

* * * * * * * COMPU-LOG - VERTICAL DEVIATION * * * * * * *

CLIENT	: FORDING COAL LTD	HOLE ID.	: FH 2731
FIELD OFFICE	: CGC-TILSX	DATE OF LOG	: 09/03/00
DATA FROM	:	PROBE	: 9055X , 33
MAG. DBCL.	: 19,500	DEPTH UNITS	: NBTERS
LOG: RH2731_()8-03-00_11-18_9055 X	10_3.20_476.90_	DEVI, log

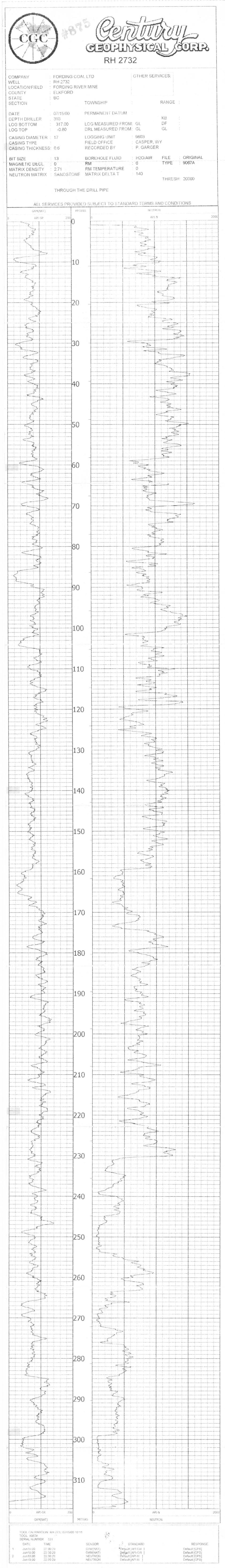
4.8 4.80 -0.00 -0.00 0.0 $192, 5$ 0.5 $245, 9$ $31, 2$ $13, 20$ -0.01 -0.02 0.0 $251, 2$ 0.5 $245, 9$ $13, 2$ $13, 20$ -0.01 -0.20 0.2 $273, 8$ 0.8 $277, 3$ $13, 2$ $13, 20$ -0.01 -0.20 0.2 $273, 8$ 0.8 $277, 3$ $23, 2$ $29, 20$ -0.01 -0.29 0.3 $267, 3$ 1.1 $282, 4$ $23, 2$ $29, 20$ -0.02 -0.41 0.4 $267, 1$ 1.4 $282, 4$ $33, 2$ $33, 19$ -0.03 -0.52 0.5 $269, 4$ 1.3 $239, 7$ $39, 2$ $39, 19$ -0.03 -0.75 0.8 $267, 5$ 1.2 $252, 1$ $49, 2$ $49, 19$ -0.03 -0.75 0.8 $267, 5$ 1.2 $252, 1$ $49, 2$ $49, 19$ -0.06 -1.01 1.0 $265, 6$ 1.3 $249, 4$ $59, 2$ $59, 1.9$ -0.14 -1.14 1.1 $262, 9$ 1.7 $239, 1$ $63, 2$ $63, 18$ $-0, 22$ -1.29 1.3 $269, 2$ $26, 29, 249, 249, 1$ $73, 2$ $73, 18$ -0.33 -1.44 1.5 $259, 0$ 1.6 $255, 4$ $73, 2$ $73, 18$ -0.33 -1.49 1.8 $259, 4$ 1.9 $256, 7$ $73, 2$ $93, 17$ -0.33 -1.89 1.9 $259, 1$ $2, 0$ $257, 7$ <th>CABLE DEPTH</th> <th>TRUB DBPTH</th> <th>NORTH DBV.</th> <th>BAST DEV.</th> <th>DISTANCE</th> <th>ASINUTH</th> <th>SNIG</th> <th>SANGB</th>	CABLE DEPTH	TRUB DBPTH	NORTH DBV.	BAST DEV.	DISTANCE	ASINUTH	SNIG	SANGB
13.213.20 -0.01 -0.12 0.1 264.7 1.2 287.3 10.210.210.30 0.01 -0.20 0.2 273.8 0.8 277.3 23.223.20 -0.02 -0.41 0.4 267.3 1.1 252.3 20.228.20 -0.02 -0.41 0.4 267.3 1.4 239.7 30.230.19 -0.03 -0.75 0.8 267.5 1.7 275.5 43.243.19 -0.03 -0.75 0.8 267.5 1.7 275.1 53.253.19 -0.00 -1.01 1.0 265.5 1.7 275.1 53.253.19 -0.00 -1.01 1.0 265.5 1.7 279.1 63.263.18 -0.22 -1.29 1.3 260.2 2.0 239.1 63.263.18 -0.22 -1.44 1.5 259.4 1.9 265.5 73.273.18 -6.40 -1.59 1.6 259.2 1.6 258.4 73.273.18 -6.40 -1.89 1.9 259.4 1.9 265.7 73.273.18 -6.47 -2.42 2.5 259.0 2.6 257.7 79.293.17 -0.36 -1.89 1.9 259.3 1.5 253.7 93.293.17 -0.32 -2.42 2.5 259.0 2.6 257.7 93.293.16 -0.47 -2.42 2.5 259.0 2.6 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>								
10.213,200,01-0,200,2233,300,8273,323,223,20-0,01-0,290,3267,31,1252,329,228,20-0,02-0,410,4267,11,4292,433,233,19-0,01-0,520,5269,41,3238,739,238,19-0,03-0,640,6267,21,7278,549,243,19-0,07-0,870,9265,51,7275,153,253,19-0,08-1,011,0205,61,3249,459,258,19-0,14-1,141,1262,91,7239,163,263,18-0,22-1,291,3260,22,0239,163,263,18-0,32-1,741,8259,21,6258,473,373,18-0,30-1,741,8259,31,5253,790,293,17-0,33-1,741,8259,31,5253,791,293,17-0,63-2,022,7238,82,6253,8109,2103,16-0,57-2,832,9258,72,6255,9103,2103,16-0,57-2,832,9258,72,6255,8109,2103,12-13,14-0,63-3,043,1258,01,9255,1113,2113,15-0,63-3,043,1258,01,9255,1123,2123,14-0,95								
23.223.20 -0.01 -0.29 0.3 267.3 1.1 252.3 29.223.20 -0.02 -0.41 0.4 267.1 1.4 292.4 33.233.19 -0.03 -0.64 0.6 267.2 1.7 276.5 43.2 43.19 -0.03 -0.75 0.8 267.5 1.2 252.1 49.2 43.19 -0.07 -0.75 0.8 267.5 1.7 275.5 43.2 43.19 -0.07 -0.75 0.8 267.5 1.7 275.7 53.2 53.19 -0.08 -1.01 1.0 265.6 1.3 249.4 59.2 58.19 -0.14 -1.14 1.1 262.9 1.7 239.1 63.2 69.18 -0.22 -1.29 1.3 260.2 0.2 239.1 69.2 69.18 -0.32 -1.44 1.5 259.0 1.6 258.4 79.2 73.18 -0.30 -1.89 1.9 259.2 1.6 258.4 79.2 73.18 -0.39 -2.23 2.3 259.1 2.0 255.7 79.2 99.17 -0.43 -2.23 2.3 259.2 2.6 257.9 99.2 99.16 -0.57 -2.63 2.7 258.8 2.6 257.8 109.2 109.15 -0.57 -2.63 2.7 258.8 2.6 257.9 103.2 123.14 -0.69 -3.63 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>								
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43.2 43.19 -0.03 -0.75 0.8 267.5 1.2 252.1 49.2 48.19 -0.07 -0.87 0.9 265.5 1.7 275.1 53.2 53.19 -0.08 -1.01 1.0 265.6 1.3 249.4 59.2 58.19 -0.14 -1.14 1.1 262.9 1.7 239.1 63.2 63.18 -0.22 -1.29 1.3 260.2 2.0 239.1 69.2 69.18 -0.23 -1.44 1.5 259.0 1.9 265.8 73.2 73.18 -0.33 -1.74 1.8 259.4 1.9 262.9 83.2 83.17 -0.36 -1.89 1.9 259.3 1.5 253.7 98.2 93.17 -0.43 -2.23 2.3 259.1 2.0 256.4 99.2 99.16 -0.47 -2.42 2.5 259.0 2.6 257.8 103.2 103.16 -0.57 -2.83 2.9 258.7 2.6 257.9 103.2 103.16 -0.57 -2.83 2.9 258.7 2.6 253.8 108.2 108.14 -0.69 -3.63 3.7 257.6 2.8 259.0 123.2 123.14 -0.69 -3.63 3.7 257.4 2.9 248.4 138.2 128.14 -0.80 -3.63 3.7 255.6 2.6 247.9 133.2 123.14 -0.95								
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53.2 53.19 -0.08 -1.01 1.0 265.6 1.3 249.4 59.2 58.19 -0.14 -1.14 1.1 262.9 1.7 239.1 63.2 63.18 -0.22 -1.29 1.3 260.2 2.0 239.1 68.2 68.18 -0.22 -1.44 1.5 259.2 1.6 258.4 73.2 73.18 -0.30 -1.59 1.6 259.4 1.9 262.9 73.2 73.17 -0.33 -1.74 1.8 259.4 1.9 262.9 83.2 83.17 -0.39 -2.05 2.1 259.2 2.1 260.1 99.2 99.17 -0.43 -2.23 2.3 259.2 2.1 260.1 99.2 99.16 -0.47 -2.23 2.3 259.1 2.0 256.4 99.2 99.16 -0.47 -2.33 2.3 259.1 2.0 257.9 103.2 103.16 -0.52 -2.62 2.7 258.8 2.6 253.8 109.2 109.15 -0.57 -2.83 2.9 258.7 2.6 257.9 113.2 113.15 -0.63 -3.04 3.1 258.0 1.9 259.0 123.2 123.14 -0.73 -3.43 3.5 257.9 2.7 253.8 109.2 129.14 -0.69 -3.23 3.2 257.6 2.8 259.9 123.2 129.14 -0.60								
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93.293.17 -0.43 -2.23 2.3 $2.59.1$ 2.0 256.4 99.299.16 -0.47 -2.42 2.5 259.0 2.6 257.9 103.2103.16 -0.52 -2.62 2.7 258.9 2.6 253.8 109.2109.15 -0.57 -2.83 2.9 259.7 2.6 254.7 113.2113.15 -0.63 -3.04 3.1 259.7 2.6 254.7 113.2113.14 -0.69 -3.23 3.3 259.0 1.9 259.0 123.2123.14 -0.73 -3.43 3.5 257.9 2.7 253.8 128.2128.14 -0.90 -3.63 3.7 257.6 2.8 259.9 133.2133.13 -0.86 -3.63 3.7 257.4 2.9 248.4 139.2 -0.95 -4.06 4.2 256.9 2.6 246.8 143.2143.12 -1.04 -4.30 4.4 256.4 2.8 249.4 149.2149.11 -1.12 -4.73 4.9 255.6 2.7 243.1 159.2159.10 -1.31 -4.96 5.1 255.2 2.5 249.5 161.2163.00 -1.32 -5.94 6.2 254.4 3.2 251.3 179.2179.07 -1.68 -5.94 6.2 254.2 3.2 252.6 193.1 193.07 -1.78 -6.19 6.4 254.0 2.9								
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113.2113.15 -0.63 -3.04 3.1 258.3 2.4 235.1 118.2118.14 -0.69 -3.23 3.3 258.0 1.9 259.0 123.2123.14 -0.73 -3.43 3.5 257.9 2.7 253.8 128.2128.14 -0.80 -3.63 3.7 257.6 2.8 259.9 133.2137.13 -0.86 -3.85 3.9 257.4 2.9 248.4 138.2138.12 -0.95 -4.08 4.2 256.9 2.6 246.8 143.2143.12 -1.04 -4.30 4.4 256.4 2.8 244.3 148.2149.11 -1.12 -4.73 4.6 256.6 2.6 247.8 153.2153.11 -1.21 -4.73 4.9 255.6 2.7 243.1 158.2158.10 -1.31 -4.96 5.1 255.2 2.5 249.5 163.2163.00 -1.39 -5.19 5.4 254.7 2.9 250.1 173.2173.08 -1.58 -5.67 5.9 254.4 3.2 251.3 178.2179.07 -1.68 -5.94 6.2 254.2 3.2 246.8 193.2193.05 -1.96 -6.72 7.0 253.7 3.0 252.7 193.2193.05 -1.96 -6.72 7.0 253.7 3.0 252.7 193.2199.04 -2.06 -6.72 7.0 253								
110.2 118.14 -0.69 -3.23 3.3 250.0 1.9 259.0 123.2 123.14 -0.73 -3.43 3.5 257.9 2.7 253.8 120.2 120.14 -0.90 -3.63 3.7 257.6 2.8 250.9 133.2 137.13 -0.86 -3.85 3.9 257.4 2.9 248.4 139.2 138.12 -0.95 -4.08 4.2 256.9 2.6 246.8 143.2 143.12 -1.04 -4.30 4.4 256.4 2.8 244.3 140.2 149.11 -1.12 -4.51 4.6 256.0 2.6 247.8 153.2 153.11 -1.21 -4.73 4.9 255.6 2.7 249.5 163.2 163.10 -1.31 -4.96 5.1 255.2 2.5 249.5 163.2 163.09 -1.49 -5.43 5.6 254.7 2.9 250.1 173.2 179.07 -1.68 -5.94 6.2 254.4 3.2 251.3 170.2 199.07 -1.78 -6.19 6.4 254.0 2.9 252.6 198.2 198.06 -1.87 -6.19 6.4 254.0 2.9 252.7 193.2 193.05 -1.96 -6.72 7.0 253.7 3.0 252.7 193.2 193.04 -2.06 -6.96 7.3 253.5 2.7 246.8 198.2 20								
123.2 123.14 -0.73 -3.43 3.5 257.9 2.7 253.8 120.2 120.14 -0.00 -3.63 3.7 257.6 2.8 259.9 133.2 133.13 -0.066 -3.855 3.9 257.4 2.9 248.4 130.2 130.12 -0.95 -4.00 4.2 256.9 2.6 246.8 143.2 143.12 -1.04 -4.30 4.4 256.4 2.8 244.3 148.2 149.11 -1.12 -4.51 4.6 256.0 2.6 247.6 153.2 157.11 -1.21 -4.73 4.9 255.6 2.7 243.1 159.2 159.10 -1.31 -4.96 5.1 255.2 2.5 249.5 163.2 163.10 -1.39 -5.19 5.4 255.0 3.0 252.4 169.2 169.09 -1.49 -5.43 5.6 254.7 2.9 250.1 173.2 179.08 -1.58 -5.67 5.9 254.4 3.2 246.8 193.2 193.07 -1.78 -6.19 6.4 254.0 2.9 252.7 193.2 193.07 -1.78 -6.19 6.4 253.8 3.0 252.7 193.2 193.05 -1.96 -6.72 7.0 253.7 3.0 249.8 199.2 199.04 -2.06 -6.96 7.3 253.5 2.9 247.8 203.2				-3.23				
$12\vartheta, 2$ $12\vartheta, 14$ $-0, \vartheta0$ $-3, 63$ $3, 7$ $257, 6$ $2, \vartheta$ $259, 9$ $133, 2$ $133, 13$ $-0, \vartheta6$ $-3, \vartheta5$ $3, 9$ $257, 4$ $2, 9$ $248, 4$ $13\vartheta, 2$ $13\vartheta, 12$ $-0, 95$ $-4, 0\theta$ $4, 2$ $256, 9$ $2, 6$ $246, \vartheta$ $143, 2$ $143, 12$ $-1, 04$ $-4, 30$ $4, 4$ $256, 4$ $2, \vartheta$ $244, 3$ $14\vartheta, 2$ $14\vartheta, 11$ $-1, 12$ $-4, 51$ $4, 6$ $256, 0$ $2, 6$ $247, \vartheta$ $153, 2$ $153, 11$ $-1, 21$ $-4, 73$ $4, 9$ $255, 6$ $2, 7$ $243, 1$ $15\vartheta, 2$ $15\vartheta, 10$ $-1, 31$ $-4, 96$ $5, 1$ $255, 2$ $2, 5$ $249, 5$ $163, 2$ $163, 10$ $-1, 39$ $-5, 19$ $5, 4$ $255, 0$ $3, 0$ $252, 4$ $16\vartheta, 2$ $16\vartheta, 09$ $-1, 49$ $-5, 43$ $5, 6$ $254, 7$ $2, 9$ $250, 1$ $173, 2$ $173, 00\theta$ $-1, 58$ $-5, 67$ $5, 9$ $254, 4$ $3, 2$ $251, 3$ $17\vartheta, 2$ $17\vartheta, 07$ $-1, 68$ $-5, 94$ $6, 2$ $254, 2$ $3, 2$ $246, \vartheta$ $133, 2$ $193, 07$ $-1, 78$ $-6, 19$ $6, 4$ $254, 0$ $2, 9$ $252, 6$ $19\vartheta, 2$ $19\vartheta, 06$ $-1, 87$ $-6, 19$ $6, 4$ $254, 0$ $2, 9$ $252, 7$ $193, 2$ $193, 05$ $-1, 96$ $-6, 72$ $7, 0$ $253, 7$ $3, 0$ $252, 7$ $19\vartheta, 2$ $19\vartheta, 04$ $-2, $								
133,2 $137,13$ -0.86 -3.85 3.9 257.4 2.9 248.4 $138,2$ $138,12$ -0.95 -4.08 4.2 256.9 2.6 246.8 $143,2$ 143.12 -1.04 -4.30 4.4 256.4 2.8 244.3 148.2 148.11 -1.12 -4.51 4.6 256.0 2.6 247.8 153.2 153.11 -1.31 -4.73 4.9 255.6 2.7 243.1 158.2 158.10 -1.31 -4.96 5.1 255.2 2.5 249.5 163.2 163.10 -1.39 -5.19 5.4 255.0 3.0 252.4 168.2 168.09 -1.49 -5.43 5.6 254.7 2.9 250.1 173.2 173.08 -1.58 -5.67 5.9 254.4 3.2 251.3 178.2 179.07 -1.68 -5.94 6.2 254.2 3.2 246.8 183.2 193.07 -1.78 -6.19 6.4 254.0 2.9 252.6 188.2 198.06 -1.87 -6.46 6.7 253.8 3.0 252.7 193.2 193.05 -1.96 -6.72 7.0 253.7 3.0 249.8 198.2 203.04 -2.13 -7.19 7.5 253.5 2.9 247.8 203.2 208.03 -2.13 -7.19 7.5 253.5 2.7 246.7 208.2 20								
138, 2 $138, 12$ -0.95 -4.08 4.2 256.9 2.6 246.8 $143, 2$ $143, 12$ -1.04 -4.30 4.4 256.4 2.9 244.3 $148, 2$ $148, 11$ -1.12 -4.51 4.6 256.0 2.6 247.8 $153, 2$ $153, 11$ -1.21 -4.73 4.9 255.6 2.7 243.1 $158, 2$ $153, 11$ -1.31 -4.96 5.1 255.2 2.5 249.5 $163, 2$ $163, 10$ -1.39 -5.19 5.4 255.0 3.0 252.4 $168, 2$ $168, 09$ -1.49 -5.43 5.6 254.7 2.9 250.1 $173, 2$ 173.08 -1.58 -5.67 5.9 254.4 3.2 251.3 $178, 2$ 178.07 -1.68 -5.94 6.2 254.2 3.2 246.8 $183, 2$ 193.07 -1.78 -6.19 6.4 254.0 2.9 252.6 $188, 2$ 198.06 -1.87 -6.46 6.7 253.8 3.0 252.7 $193, 2$ 193.05 -1.96 -6.72 7.0 253.7 3.0 249.8 $198, 2$ 198.04 -2.06 -6.96 7.3 253.5 2.9 247.8 203.2 203.04 -2.13 -7.19 7.5 253.5 2.7 246.7 $208, 2$ 208.03 -2.25 -7.67 8.0 253.7 2.7 260.4 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>								
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148.2148.11 $-1,12$ $-4,51$ $4,6$ $256,0$ $2,6$ $247,8$ 153.2153.11 $-1,21$ $-4,73$ $4,9$ $255,6$ $2,7$ $243,1$ 158.2158.10 $-1,31$ $-4,96$ $5,1$ $255,2$ $2,5$ $249,5$ 163.2163.10 $-1,39$ $-5,19$ $5,4$ $255,0$ $3,0$ $252,4$ 168.2168.09 $-1,49$ $-5,43$ $5,6$ $254,7$ $2,9$ $250,1$ 173.2173.08 $-1,58$ $-5,67$ $5,9$ $254,4$ $3,2$ $251,3$ 178.2178.07 $-1,68$ $-5,94$ $6,2$ $254,2$ $3,2$ $246,8$ 183.2183.07 $-1,78$ $-6,19$ $6,4$ $254,0$ $2,9$ $252,6$ 188.2198.06 $-1,87$ $-6,46$ $6,7$ $253,8$ $3,0$ $252,7$ 193.2193.05 $-1,96$ $-6,72$ $7,0$ $253,7$ $3,0$ $249,8$ 198.2198.04 $-2,06$ $-6,96$ $7,3$ $253,5$ $2,9$ $247,8$ 203.2203.04 $-2,13$ $-7,19$ $7,5$ $253,5$ $2,7$ $246,7$ 208.2208.03 $-2,25$ $-7,67$ $8,0$ $253,7$ $2,7$ $253,1$ 218.2218.02 $-2,34$ $-7,89$ $8,2$ $253,5$ $2,6$ $228,9$ $223,2$ $223,01$ $-2,43$ $-8,09$ $8,4$ $253,3$ $2,7$ $252,1$		143.12						
153,2 $153,11$ $-1,21$ $-4,73$ $4,9$ $255,6$ $2,7$ $243,1$ $159,2$ $158,10$ $-1,31$ $-4,96$ $5,1$ $255,2$ $2,5$ $249,5$ $163,2$ $163,10$ $-1,39$ $-5,19$ $5,4$ $255,0$ $3,0$ $252,4$ $160,2$ $168,09$ $-1,49$ $-5,43$ $5,6$ $254,7$ $2,9$ $250,1$ $173,2$ $173,00$ $-1,58$ $-5,67$ $5,9$ $254,4$ $3,2$ $251,3$ $179,2$ $179,07$ $-1,68$ $-5,94$ $6,2$ $254,2$ $3,2$ $246,0$ $103,2$ $103,07$ $-1,78$ $-6,19$ $6,4$ $254,0$ $2,9$ $252,6$ $103,2$ $103,06$ $-1,87$ $-6,46$ $6,7$ $253,8$ $3,0$ $252,7$ $193,2$ $193,05$ $-1,96$ $-6,72$ $7,0$ $253,7$ $3,0$ $249,8$ $199,2$ $198,04$ $-2,06$ $-6,96$ $7,3$ $253,5$ $2,9$ $247,8$ $203,2$ $203,04$ $-2,13$ $-7,19$ $7,5$ $253,5$ $2,7$ $246,7$ $208,2$ $208,03$ $-2,25$ $-7,67$ $8,0$ $253,7$ $2,7$ $260,4$ $213,2$ $213,02$ $-2,34$ $-7,89$ $8,2$ $253,5$ $2,6$ $228,9$ $223,2$ $223,01$ $-2,43$ $-7,89$ $8,4$ $253,3$ $2,7$ $252,1$		149,11	-1.12	-4.51			Z.6	
158,2 $158,10$ $-1,31$ $-4,96$ $5,1$ $255,2$ $2,5$ $249,5$ $163,2$ $163,10$ $-1,39$ $-5,19$ $5,4$ $255,0$ $3,0$ $252,4$ $168,2$ $168,09$ $-1,49$ $-5,43$ $5,6$ $254,7$ $2,9$ $250,1$ $173,2$ $173,08$ $-1,58$ $-5,67$ $5,9$ $254,4$ $3,2$ $251,3$ $179,2$ $179,07$ $-1,68$ $-5,94$ $6,2$ $254,2$ $3,2$ $246,8$ $183,2$ $183,07$ $-1,78$ $-6,19$ $6,4$ $254,0$ $2,9$ $252,6$ $189,2$ $193,05$ $-1,87$ $-6,46$ $6,7$ $253,8$ $3,0$ $252,7$ $193,2$ $193,05$ $-1,96$ $-6,72$ $7,0$ $253,7$ $3,0$ $249,8$ $198,2$ $198,04$ $-2,06$ $-6,96$ $7,3$ $253,5$ $2,9$ $247,8$ $203,2$ $203,04$ $-2,13$ $-7,19$ $7,5$ $253,5$ $2,7$ $246,7$ $208,2$ $208,03$ $-2,25$ $-7,67$ $8,0$ $253,7$ $2,7$ $260,4$ $213,2$ $213,02$ $-2,34$ $-7,89$ $8,2$ $253,5$ $2,6$ $228,9$ $223,2$ $223,01$ $-2,43$ $-8,09$ $8,4$ $253,3$ $2,7$ $252,1$		153.11	-1,21	-4,73	4.9	255.6	2.7	243.1
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	159.2	159.10	-1.31	-4.96	5.1	255.2	2.5	249.5
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	161.2	163.10	-1.39	-5.19	5.4	255.0	3.0	252.4
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	160.2	169.09	-1.49	-5.43	5.6	254.7	2.9	250.1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	173.2	173.00	-1.58	-5.67	\$.9	254.4	3.2	251.3
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	170.2	170.07	-1.69	-5.94	6.2	254.2	3.2	246.0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	193.2	193.07	-1,78	-6.19	6.4	254.0	2.9	252.6
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		100.06	-1.87	-6.46	6.7	253.8	3.0	252.7
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	193.2	193.05	-1.96	-6.72	7.0	253.7	3.0	249.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	199.2	199.04	-2.06	-6,96	7.3	253.5	2.9	247.9
213.2 213.02 ~2.25 ~7.67 9.0 253.7 2.7 253.1 215.2 218.02 ~2.34 ~7.89 9.2 253.5 2.6 228.9 223.2 223.01 ~2.43 ~8.09 9.4 253.3 2.7 252.1	203.2	203.04	-2.13	-7,19	7.5	253.5		246.7
219.2 219.02 -2.34 -7.09 8.2 253.5 2.6 229.9 223.2 223.01 -2.43 -8.09 8.4 253.3 2.7 252.1	209.2	208.03	~2.19	-7.43		253.6	2.7	260.4
223.2 223.01 -2.43 -8.09 8.4 253.3 2.7 252.1	213.2	213.02	-2.25	~7.67	9.0	253.7	2.7	253.1
279.7 779.01 –751 –933 B 7 753 7 7 8 7 7 8								
	228.2	229.01	-2.51	-9,31	8.7	253.2	2.4	2.50.8
233.2 233.00 -2.57 -0.51 0.9 253.2 2.2 260.0								
238.2 238.00 -2.60 -8.67 9.1 253.3 1.9 245.2								
243.2 243.00 ~2.56 ~8.85 9.2 253.9 2.7 287.5								
248.2 247.99 -2.51 -9.03 9.4 254.5 2.2 287.8								
253.2 252.99 -2.47 -9.21 9.5 255.0 2.2 278.7	253.Z	z 52 , 99	-2.47	~9.21	9.5	255.0	2.2	278.7

* * * * * * * COMPU-LOG - VERTICAL DEVINTION * * * * * * *

CLIENT	: FORDIN	G COML LTD	HOLE ID	. : PH	2731		
FIELD OFF	ICB : CGC-TU	LSN		106 : 09/			
DATA PROP	1		PRODE	; 905	5λ ,	33	
NNG. DBCL	. : 19.5	()()	ьветн Ц	NTTS : NET	BRS .		
LOG: RH27	31_08-03-00_	11-18_90\$5 k _	.10_3.20_47	6.90_08VI.	log		
				_			
CABLE DEPTH	TRUB DBPTH	NORTH DBV.	BAST DEV.	DISTANCE	ASIMUTH	SANG	SANGD
2.59.2	257.99	-2.43	~9,38	9.7	255.5	2.3	276.1
263.2	262.99	-2.39	-9.55	9.8	256.0	2.0	284.0
268.2	267.98	-2,36	-9,73	10.0	256.3	1.9	279.4
273.2	272.98	-2.34	-9.90	10.2	256.7	2.1	273.9
278.2	277.97	-2.32	-10.09	10.4	357.1		281.1
				• •		- • -	

490.4	411.91	-4.74	- 107.03	19.4	20171		301.I
293.2	282.97	-2.29	-10.29	10.5	257.4	2.6	266.0
209.2	287.97	-2.27	-10.50	10.7	257.0	2.4	270.0
293.2	292.96	-2.27	-10.72	11.0	259.1	2.3	274.5
299.2	297.96	-2.27	-10.95	11.3	259.3	2.8	267.4
303.2	302,95	-2.28	-11.19	11.4	250.5	2.8	269.6
309.2	307.94	-2.29	~11,43	11,7	258.7	3.9	267.4
313.2	312.94	-2.31	-11.69	11.9	259,9	2.9	266.6
319.2	317.93	-2.31	-11.97	12.2	259.1	3.4	265.1
323.2	322.92	-2.33	-12.28	12.5	2.59.3	3.8	266.9
329.2	327.91	-2.35	-12.63	12.0	259.5	4.7	266.2
333.2	332.89	-2.30	-13.01	13.2	259.6	4.3	264.0
339.2	337.87	~2.42	-13.44	13.7	259.0	5.2	265.3
343.2	342.85	-2.45	-13,91	14.1	260.0	6.0	265.0
349.2	347.82	-2.46	-14,42	14.6	260.3	6.1	266.5
353.2	352.80	-2.50	-14.94	15.1	269.5	5.3	268.3
3.59.2	357.77	-2.49	-15,49	15.7	369.9	6.2	270.0
363.2	362.73	~2.46	-16,07	16.3	261.3	7.4	273.8
368.2	367.69	-2,40	-16.69	16.9	261.5	6.9	258.6
373.2	372,65	-2.52	-17,30	17.5	261.7	$\mathfrak{B},\mathfrak{g}$	269.7
378.2	377,60	-2.56	-10.00	18.2	261.9	9.6	274.9
383.2	382.55	-2,61	-18.74	18.9	262.1	3,6	269.0
309.2	387,49	-2.69	-19,47	19.7	262.2	9.1	261.4
393.2	392.43	-2.79	-20.24	20.4	262.2	9.1	263.8
398.2	397.36	-2.85	-21,03	21.2	262.3	9,9	265.8
403.2	402.29	-2.97	-21.87	22.1	262.3	8,8	254.5
408.2	407.22	-3.07	-22.71	22.9	262.3	9,9	255.6
413.2	412.14	-3.15	-23.57	23.8	262.4	10.4	262.1
419.2	417.06	-3.26	-24.43	24.6	262.4	11.0	265.0
423.2	421.98	-3,41	-25,33	2.5.6	262.3	11.4	262.4
428.2	426,99	-3,60	~26.26	26.5	262.2	11.1	259.9
433.2	431.79	-3,93	-27.17	27.4	262.0	10.9	247.2
439.2	436.70	-4,00	-28.09	28.4	261.9	11.5	250.5
443.2	441.61	-4.14	-29.01	29.3	261.9	11.2	274.7
449.2	446.53	~4.27	-29.91	30.2	261.9	10.5	2.50,6
453.2	451.44	-4.31	-30,92	31.1	262.0	10.8	271.7
459.2	456.35	-4.31	-31,75	32.0	262.3	10.7	249.7
463.2	461.27	-4,32	-32.63	32.9	262.5	9.5	274.0
460.2	466.20	-4.35	-33,46	33.7	262.6	9.4	273.1
473.2	471.13	-4,37	-34,32	34.6	262.7	10.2	270.7
476.6	474.48	-4.37	-34,90	35.2	262.9	10.6	265.7



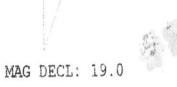


1. C.

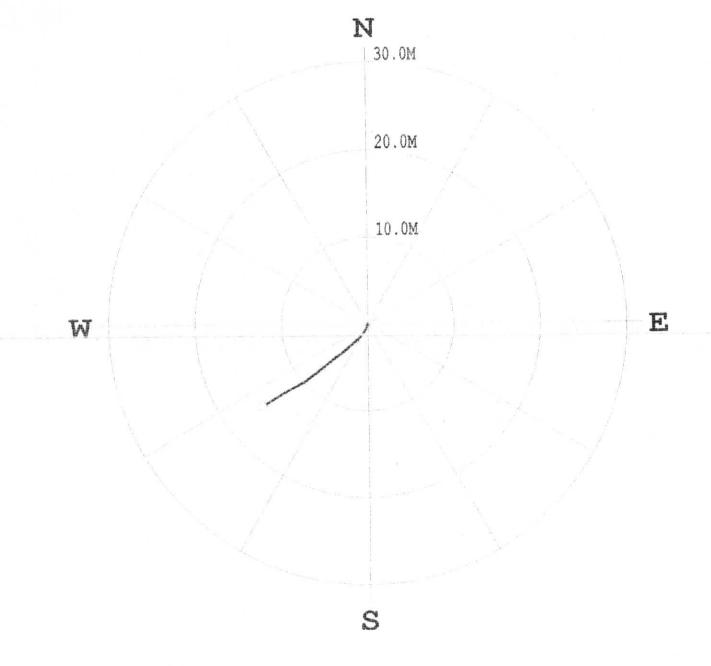
 $\langle p^{n} \rangle$

PLAN VIEW COMPU-LOG DEVIATION

CLIENT: FORDING COAL LTD LOCATION: FORDING RIVER MINE HOLE ID: RH 2732 DATE OF LOG: 07/15/00 PROBE: 9055A 238



SCALE: 10 M/CM TRUE DEPTH: 230.55 M AZIMUTH: 232.6 DISTANCE: 15.4 M + = 25 M INCR= BOTTOM OF HOLE



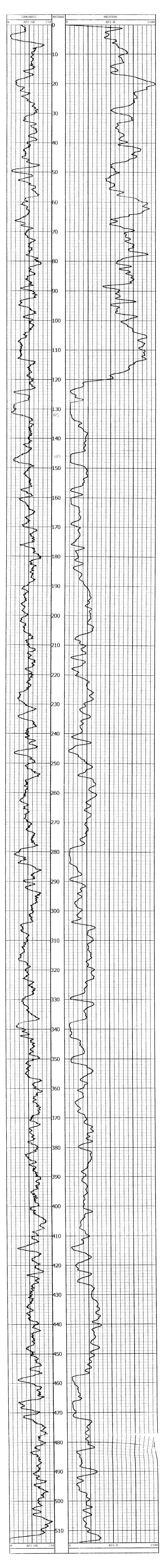
* * * * COMPU-LOG - CERTICAL ICATALL D * * *

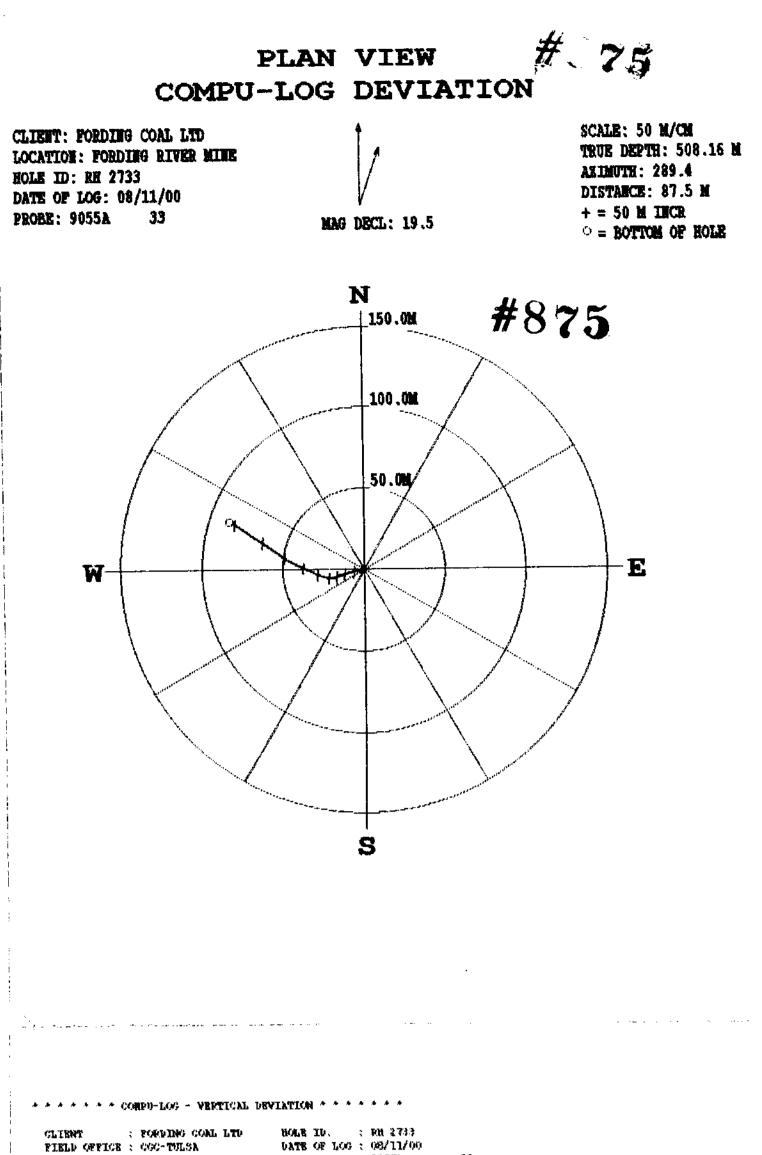
CTL LEDIT	: FORLING CAL DITE	14 1.H. 1 ³	ž	Ru d'aka	
EIEEP Or MINE	: CASTERN, WY	LATE GE LEE	:	1177 14 / G	
DATA FROM	4	(PROF41)		99955A ,	2.8
MAG. DECL.	1.9.COM	$\{[a_1, a_2], [a_1], [a_2], [a_3], [a_4], [a_5], [a_6], [$:	2416°1 1615.13	
109: RH1737_	00-1/+00_11-48_005*A .10	9.40 191.40	[4]	suit. Comp	

CAMLE DEFTH	TRUE DEPTH	NERTH DEV.	EAST OF .	$[1,1] \in [1,2] \in [1,2]$	AX IMPTH	STANG-	BANGS.
9.5	9 . Far	1. 1914	i), i)()		11.13	.) . ()	1.7% 6
14.4	19.40	-0.17	·········	• 2	1966.0	1.4	201.2
25.1	20.30	-0.41			1.0.2.	1.6	206.1
34.4	30.39	1) . () e	-().	A	2011.1	1.7	200.0
49.4	49.38	0 . 9 L	- 10 🖕 🕂	1.1	Sec.	1.94	没有我的。1
1.1.1	59.30	-1.17		1 m 1	21.7.	2.5	217.0
80.4	69.37	- 1 k. î	-(), 900	1.0	271.7		2.25,9
7.9 . 4	75.38	- <u>_</u>	-1.41		27.5.7	÷.,	2. 2. 2
o". 1	89.33	- 3.33	-1.45	2.0	C18.1	1.4	232.45
99.4	99.32	- 7 -	- 3. 31	8 . P	11 A. A.	3.4	225.3
109.1	100.30	-3.11	-2.15		21.	× . 5	221.0
119.4	719.27	-3.54	- 3, 33	4.8	2 3. 1	4.2	2.59.1
120.4	1.29.24		-3.21		2.4.5	4.3	233.9
130.4	139.22	-4.44	- 4 . En B	S	332.0	4.5	234.1
147.4	149.15	-4. Ob	and the second s	8 . .	. S	5.Q	208.2
159.4	1.5.0.14	-6.51	-5.191	· . 1	277.0	·	230.8
14.9.1	1000.10		- Er . Al Ka	5. K.	221.	5.G	_ 54 . 1
179-4	174.04	- 6. 6	- 1 . A S	10.0	200.0	6 . 1 <u>3</u>	242.
169.4	188.08	-7.17		11.1	State &	6 . 4	208.0
199.4	199.9	and the second second		1. · · ·	2.5 15	6.9	243.1
205.4	208.86	·····) • 1. Co.	-10.57	1.84.8	231.5	6.1	241.5
216.4	218.81	-0.61	-11.16	14.3	232.0	5.6	232.4
<u>0.1</u>	-220.76			- Shartson	222.5		-248.8-
231.	230.55	-9.313	-12.26] . vi	232.6	5.8	235.5

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, CANADA	ł	······		
	NSHIP :	Ę	RANGE	:
10/00 PER	MANENT DATUM :	GL		
			KB	2
4.10 LOG	MEASURED FROM:			N
.30 ORL	MEASURED FROM:	GL.	GL	:
LOG	GING UNIT :	9613		
	ORDED BY :	TINEAL		
BOR	EHOLE FLUID :	H20/AIR	FILE	: ORIGINAL
5 RM	:		TYPE	: 9067A
I RM	remperature :			
NDSTONE MAT	RIX DEUTA T	140		
			THRES	H: 20000
	ADING RIVER MINE FORD ,, CANADA TOW 10/00 PER 4.10 LOG .30 DRL 1.0G EEL FIEL REC BOR 5 RM 1 RM 1	2793 RDING RIVER MINE FORD , CANADA TOWNSHIP 10/00 PERMANENT DATUM 10/00 PERMANENT 10/00 PERM	2733 RUNG RIVER MINE FORD , CANADA TOWNSHIP TOWNSHI	2733 ADING RIVER MINE FORD , CANADA TOWNSHIP TOWNSHIP TOWNSHIP 1000 PERMANENT DATUM GL KB 4.10 LOG MEASURED FROM: GL KB 4.10 DRL MEASURED FROM: GL UOGGING UNIT EL LOGGING UNIT EL BOREHOLE FLUID TNEAL BOREHOLE FLUID TNEAL BOREHOLE FLUID TYPE MOSTONE MATRIX DELTA T 140





	FIELD OFF	ICB : 000-TU	LSA	UNTE OF	1,06 : 08/	11/00		
i.	DATA PROM			PROBE	: 905		33	
Į.	NAG, DBCL	. : 19.5	99		NITS : NBT			
1	LOG: RH27	33_08-11-90_	12-41_90558_	.10_4.20_52	0.20_DBVI.	1og		
i i	CABLE DEPTR		NGATH DEV.	BAST DEV.	DISTANCE	ASINUTH	SANG	SANGB
i.	SADLE PARTE	5.80	~0.00	0.00	0,0 0	90.7	0.2	90.7
1	ð.5 210	9.20	-0.02	-0.01	0.0	201.6		242.4
	14.2	14.20	-0.09	-0.13	0.2	236.7	2.2	250.4
1	19.2	19.20	-0.13	-0.27	0.3	243.4		239.3
i i	24.2	24.19	-0.23	-0.39	0.5	239.8		188.7
1	29.2	29.19	-0.28	-0.59	0.7	244.7		269.1
1	34.2	34.19	-0.33	-0.77	0.9	246.7		237.8
1	39.2	39.18	-0.41	-0.97	1.1	247.2		251.7
!	44.2	44.17	-0.46	~1.21	1.3	249.1	2.0	247.1
[49.2	49.16	-0.52	-1.51	1.6	250.8	3.8	263.0
	54.2	54.15	-0.59	-1,94	1.9	2.52.2	4.2	252.2
i i	59.2	59.14	-0.67	-2.20	2.3	253.2	4.7	254.9
ł	64.2	64.12	~0.76	-2,60	2.7	253.8	4.9	259.3
ļ.	69.2	69.10	-0,85	-3,04	3.2	254.4		265.7
1	74.3	74.00	-0.95	-3,52	3.7	254.9		261.4
1	79.2	79.05	-1.06	-4.02	4.2	255.2		257.7
	94、2	94.02	-1.19	-4.54	4.7	255.4		263.3
	89.2	39.99	-1.30	-5,47	5.2	255.6		250.0
ł	94.2	93,96	-1.43	-5,62	5.9	255.7		254.3
!	99.2	98,93	-1.56	-6.19	6.A	255.9		257.1
	104.2	103 . 89	-1,60	-6.72	6.9	255.9		252.3
į.	109.2	109,96	-1,79	-7.27	7.5	256.2		259.5
1	114.2	113.83	-1,91	-7.81	8.0	256.3		242.4
i	119.2	119.90	-2.05	-9.36	8,6	256.2		250.0
	124.2	123.77	-2.19	-9.92	9.2	256.2		258.8
÷	129.2	128,73	-2.35	-9.40	9,8	256.1		255.4
į.	134.2	133.70	-2.49	-10,03	10.3	2.56.0		255.3
	139.2	139.66	~2.64	-10.61	10.9	256.0		267.5
	144.2	143.63	-2.80	-11.17	11.5	255.9		254.0
	149.2	149.59	-2.97	-11.72	12.1	255.8		250.3
I	154.2	153.56	~3.12	-12.26	12.7	255.7	0.0	253.4
	159.2	158.53	-3.27	-12.90	13.2	255.7		256.1
i	164.2	163.59 169.47	-3,42 -3,60	-13.32	13.8	255.6		249.2
1	169.2			-13.81	14.3	255.4	0.3	260.3
ţ	174.2 179.2	173,44 178,41	-3,79 -3,98	-14.32	14.9	255.2		253.2
1	104.2	183.39	-4.20	-14,82 -15,30	15.3 15.9	255.0 254.7		245.3 244.9
1	189.2	198.36	-4.42	-13,30	16.4	254.4		250.7
	194.2	193.33	-4.59	-16.27	16.9			244.7
	199.2	199.31	-4.77	-16.71	17.4	254.1	5.6	248.9
Ì.	204.2	203.29	-4.91	-17.13	17.9	254.0	5.4	257.7
1	209.2	200.27	-5,06	-17.53	18.2	253.9	4.9	241.0
)	214.2	213.25	-5.21	-17.96	10.7	253.8	5.6	250.6
1	219.2	219.22	-5.35	-19.41	19.2	253.8	5.1	243.7
i	224.2	223.20	-5.40	-19.87	19.6	253.8	5.7	256.4
1	229.2	320.17	-5,55	-19.37	20.2	254.0	6.4	273.6
	234.2	233.14	-5.57	-19,91	20.7	254.4	6.4	271.2
1	239.2	239,11	-5.50	-20,46	21.2	254.7	6.3	275.6
1	244.2	243.09	-5.56	~21.03	21.7	255.2	6.7	274.4
	249.2	240.05	-5,49	-21.59	22.3	255.7	6.9	277.0
	254.2	253.01	-5.42	-22.18	22.0	256.3	7.2	279.4

* * * * * * COMPU-LOG - VERTICAL DEVIATION * * * * * *

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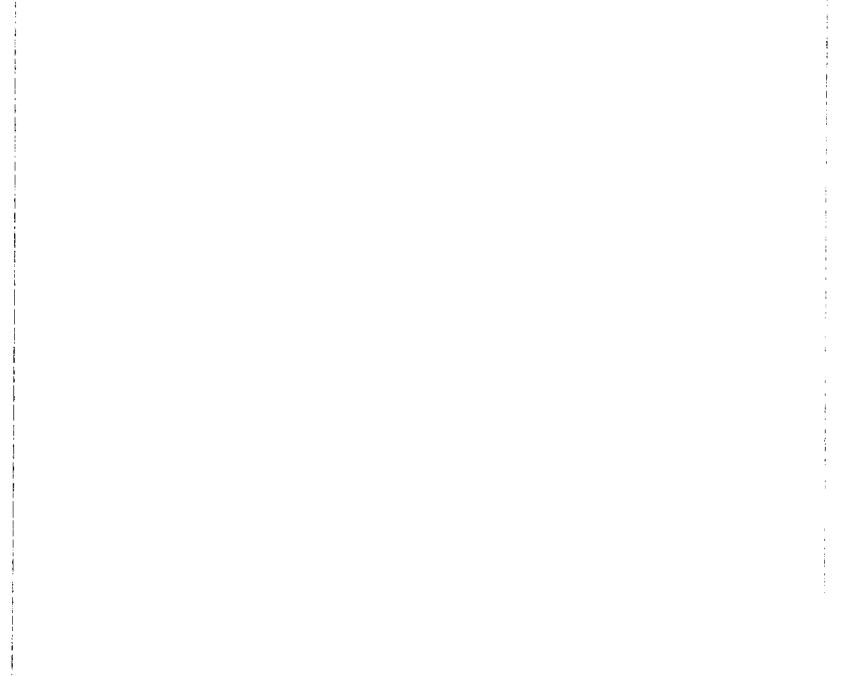
	108 : 090-11	NG CONL LTU FLSA		LOG : 08/	11/00		
DATA PRON	1		FRODE	: 905		33	
NAG. DECL	. : 19.5	5()4)	DBPTH U	NITS : KBY	CB P.S		
LOG: RH27	93_00-11-00_	12-41_9055N	.10_4.20_52	0.20 _0841 ,	199		
CABLE DEPTH	TRUB DBPTH 257.97	NORTH DEV. -5.30	BAST DEV.				
264.2	363 63	-5.14	-22.79	23.4	256.9	7.4	
269.2	267.87	~4.99	-23、45 -24、15	24、4			292
274.2	272.92	-4.76	-24,84	24.7 25.)	250.3		283.
279.2	277.76	-4.52	-25.54	47.3	259.2	0,0	291
284.2	282.71	-4.28	-26.20	25,9 26,6	260.0 260.7	2,9	293.
289.2	287.66	-4.04	-26.93	27.2	261.5	0.3	287
294.2	292.59	-3.79	-27.67	27.9	262.2	0.1	281
299.2	297.52	~3.53	~39,45	20.7	262.9	9.1	281
304.2	302.46	-3.22	-29.20	29.4	263.7	9.0	289
309.2	307.39	~2.81	-29.92	30.0	264.6	3.3	285
314.2	312.31	-2.42	-30,67	30.9	366 C	30.3	297
319.2	317.23	-1.99	-31,44	31.5	266.4	10.7	
324.2	322.15	-1.56	-32.23	32.3	267.2	17.7	
329.2	327.06	-1,20	-39,10	33.1	267.6	11.1	
334.2	331.96	-0.92	-33.99	34.0	267.9 269.6	11.3 11.1	
339.2	336.86	-0.39	-34.91	34.9	109.0		
344.2	341.75	0.04	-35.85	35.8	269.4 279.1	12.3	
349.2	346.63	0.400	-36.83	36.8	270.7	11.9	
354.2	351.50	0.94	-37,87			13.0	
359.2	356,36	1.45	-38,90		271.4	13.4	
364.2	361.23	1.95	-39,94	38.9	272.1	13.4	
369.2	366.09	2,46	-41.00	40.0	272.8	13.2	
374.2	370.94	3.03	-42.06	41.1 42.2	273.4	13.7	
379.2	375.79	3.59	-43.14	43.3	274.1	13.6	
384.2	380.63	4.17	-44.25	43.5	274.8	14.2	
389.2	385.46	4.75	-45.40		275.4	14.3	
394.2	390.27	5.37	-46.59	45.6	276.0	15.5	
399.2	395.08	6.04		46.9	276.6	15.8	
404.2	399.88	6.79	-47,78 -48,97	48.2	277.2	15.6	
409.2	404.66	7.56	-50,20	49.4	277.9	16.8	
414.2	409.43	8.47	-51.40	50.9 52 1	278.6	17.5	
419.2	414.19	9.45	-52.56	52.1	279.4	17.9	
424.2	410.95	10.42	-53.74	53.4	280.2	17.1	310.
429.2	423.72	11.33		54.7 56.1	281.0	17.6	
434.2	428.49	12.17	-54,91 -56,14	57.4	201.7	17.7	
439.2	433.25	13.01	-57.41	58.9	282.2	16.9	299.
444.2	437.98	13.90	-50.75		282.8	19.1	
449.2	442.70	14.82	-60.14	60.4 61.9	283.3 283.8	18.7	
454.2	447.39	15.74	-61.59			20.3	308.
459.2	452.05	16.72	-63.10	63.6 65 0	294.3		299.
464.2	456.70	17.72	-64.63	65.3	284.8		290.
469.2	461.35	19.69	- 64, 63 - 66, 19	67.0	285.3		305.
474.2	466.01	19,70	-67.70	68.8 70 5	285.8 286.2		307.
479.2	470.64	20.74	-69.25	70.5 72.3			303.
484.2	475.20	21.77	-70,80	74.1	296.7		305.
489.2	479,93	22.83	-72.32	74.1 75.8	287.1		303.
494.2	484.55	23.89	-73,90		287.5		308.
499.2	489.16	25.01		77.7	287.9		304.
504.2	493.75		-75,48	79.5	288.3		306.
509.2	499.35	26.15	-77.00	81.4	288.7	22.3	306.
17 T 1 1 1	-130.73	27.10	~78.80	83.3	289.0	23.4	301

CLIENT : POPULNG COAL LTD HOLE ID. ; PH 2733

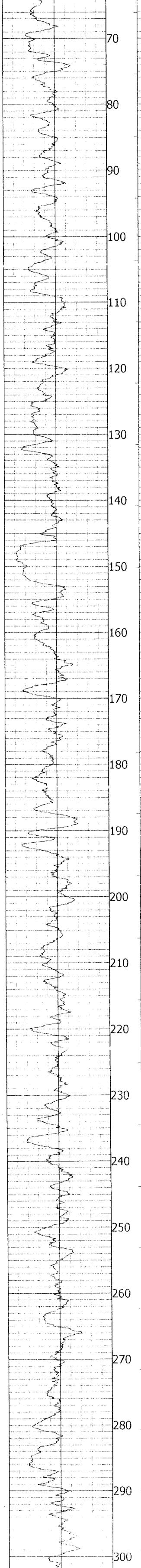
		TO A DECK	- 1 F			
PIBLE OPPICE :	CGC-TULSN	DATE OF LOG	: 0	8/11/00		
DATA PRON :		PRO BB	: 9	0558	33	
LOG: RH2733_09	-11-00_12~41_9055A_ 、1 0	4.20_520.20	UBV	I. log		
	1.117.000 11.0.0000 0.000					
	DATA PRON : MAG. DBCL. : LOG: RH2733_09		PIBLD OPPIGE : 060-TULSA DATE OP LOG DATA PROM : PRODE MAG, DECL, : 19,500 DEPTH UNITS LOG: RH2733_00-11-00_12-41_9055A_,10_4,20_520,20	PIBLD OPPIGE : 000-TULSA DATE OP LOG : 0 DATA PROM : PRODE : 9 MAG, DECL, : 19,500 DEPTH UNITS : N LOG: RH2733_000-11-00_12~41_9055A_10_4.20_520.20_DEV	DATA PRON PRODE 9055A MAG. DEGL. : 19.500 0EPTH UNITS : NETERS LOG: RH2733_09-11-00_12-41_9055A_10_4.20_520.20_DEVI.109	FIBLD OPPIGE : 000-TULSA DATE OP LOG : 00/11/00 DATA PROM : PROBE : 9055A MAG, DBCL, : 19,500 DEPTH UNITS : NETERS LOG: RH2733_000-11-00_12~41_9055A_10_4.20_520.20_DEVI.10g

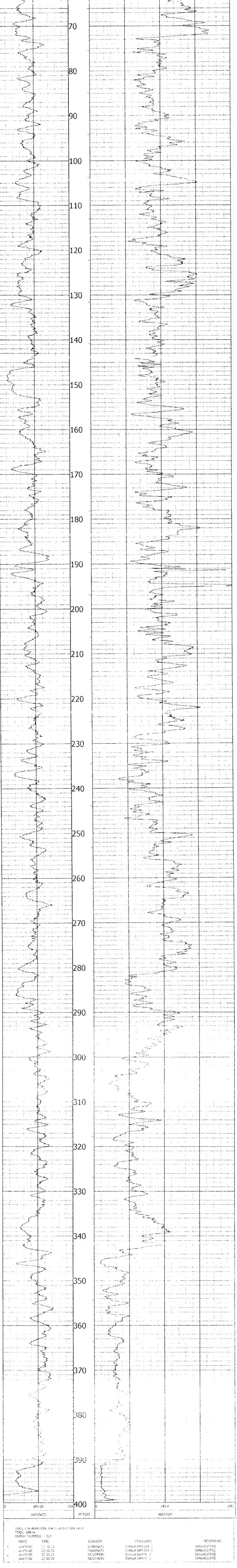
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GADLO DAPIN	THOR DEPIM	NORTH DRV.	KAST UKV.	WISTANCE	ASIMUTH	SNNG	SANGE
514.2	502.95	27.98	-80.53	85.3	289.2	22.9	305.1
519.2	507.53	28.96	-82.28	87.2	289.4	23.7	294.1
519.9	509.16	29.09	~82 \ 53	87.5	289.4	24.0	298.0



		Rob	ลึก	Trov	η		
-CGC		CEOPI RH 2					
WELL LOCATION/FIELD COUNTY	OCATION/FIELD FORDING RIVER MINE OUNTY ELKFORD			RVICES:			
SECTION	BC	TOWNSHIP		RANGE .			
DEPTH DRILLER LOG BOTTOM		PERMANENT DATU		KB : DF :			
LOG TOP CASING DIAMETER CASING TYPE		ORL MEASURED FR LOGGING UNIT FIELD OFFICE	: 9603 CASPER,	I ^I GL GL : CASPER, WY			
CASING THICKNESS BIT SIZE		RECORDED BY	P GARGE				
MAGNETIC DECL MATRIX DENSITY NEUTRON MATRIX	: 13 : 0 : 2 71 : SANDSTONE	BOREHOLE FLUID RM RM TEMPERATURE MATRIX DELTA T	: H2O/AIR 0 0 : 140		ORIGINAL 9067A		
			140	THRESH:	20000		
	THROUGH TH						
ALL SER GAM(NAT)	VICES PROVIDE	D SUBJECT TO STAN	DARD TERMS / NEUTR	a hinne fallen i sin ander ander sin der sin d	DNS		
API-GR	200	0	API-	hj	20		
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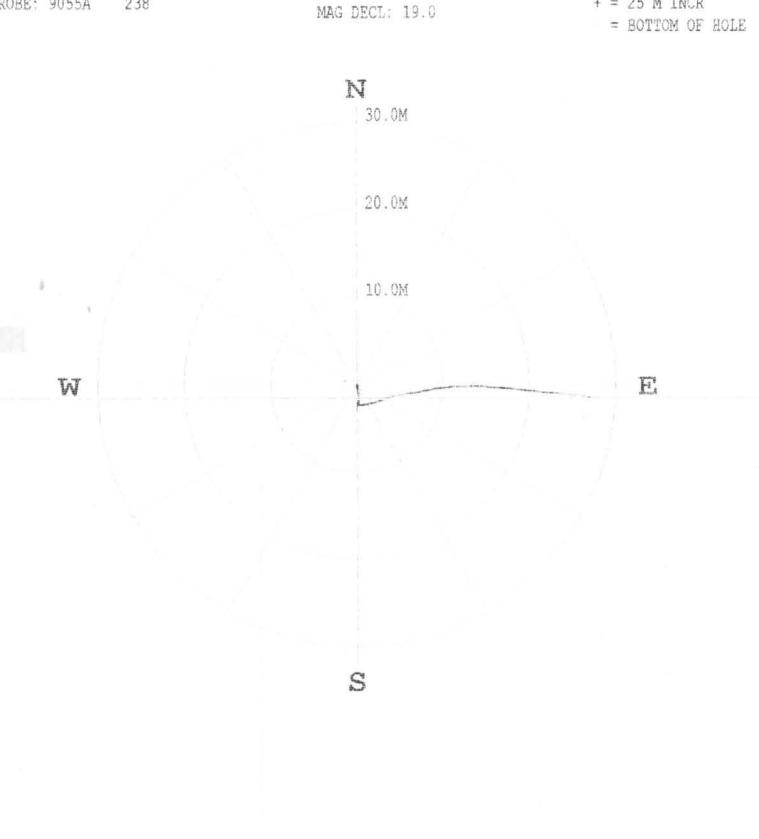


## PLAN VIEW COMPU-LOG DEVIATION

CLIENT: FORDING COAL LTD LOCATION: FORDING RIVER MINE HOLE ID: RH 2734 DATE OF LOG: 07/17/00 PROBE: 9055A 238



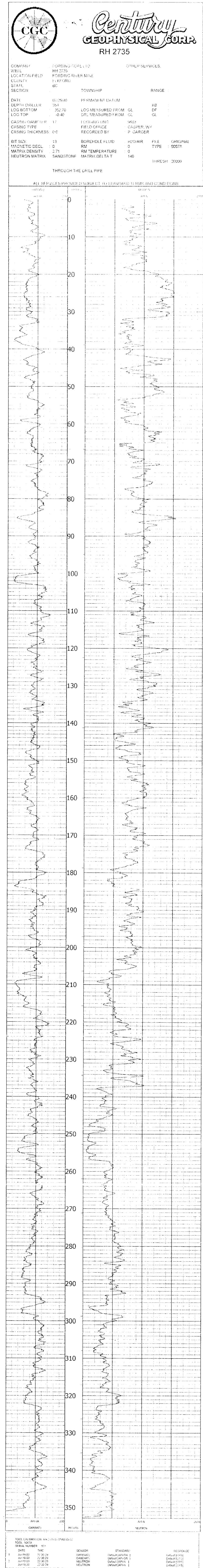
SCALE: 10 M/CM TRUE DEPTH: 396.81 M AZIMUTH: 93.2 DISTANCE: 27.6 M + = 25 M INCR = BOTTOM OF HOLE



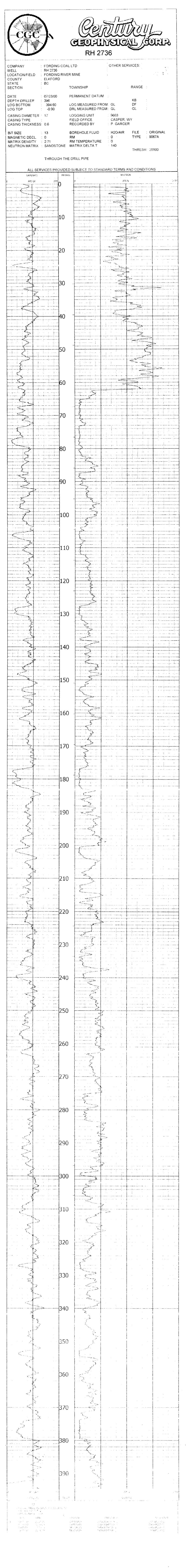
	医连发管子管	Q(1)(( ¹⁾ -),( ¹⁾ -	ventrola, o		Q LAR			
	CILLENN'	: Pakinna o	CAL COL	HOLE IC.	: (s ¹ )	213 f		
		: CASPER, N			us i wiy			
	LOTA DESCRIPTION			U.S. LOR	<ul> <li>(41)</li> </ul>	5.A	2 Acres	
		<ol> <li>E0.570</li> </ol>			Din i nev			
	1.078 88 7.01	07e17e07 38-	i statistik a	10.20,200,200	. 16, 16,14.			
1.213	5.4. DE 270 - 20	AND CREETE MC	an osv.	and the parts.	1	AP DORPH	SY 18 4	33.00 円。
	N. 1	9.4-1	11.110	21 g 10	0.941	0.00	Sec. 7	19.0
		1 (L. 12)	Sen. 30		. 7	100.0	2.2	182.9
	12.3	20. No	A 63	0.6	10 x 3	tan. E	75.0	1734.6
	8 mail:	34.20	- 1. St	0.10	1.20	3.03.0	Τ.	172.4
	11.3	4.5.45	-1.27	1.21	1.1	570.5	1.1	17.3.4
	States A	10.29	- Tadi P	1.2	1.0	1 here	1.2	1615.8
	7 a .		-1.71	u) . Son	1.7	. 1	0.8	118.1
	1.2	14.35	-Teub	6 a B	1.0	1 T. Cal	0.0	110.3
			<1.98	2.18		211.1	0.5	-0/4.7
	04. 9	nd., 27	-2.08	0.34	5. T	176.3	Sec. B.	366.5
		109.22	- 14	17.15		172.0	0.2	20.7. 2
		113.27	-2.27	D. 05	3. 8	138.0	0.01	2 cm b
		100.27	-0.23	0.06	÷.	1.550	0.4	4.1,4
		130.27	-/	0.70		171.8	0.4	10.4
		149.27	-2.25	14.00	1.1	194.99	0.0	10.0
		1.0		w. 11	1.1	4.2	1.6	a
		16.136	- 1.20	0.00	1.1	169.24	1.5	160.0
		179.26		eÇ ar	5.1	1.7	1.5	81.0
		1.899		1.10		1.01.2		19.0
		1.05.22	-1/19	1,1		147.4		71.1
			10	1,00	1.	131.1	. 14	
		44 A . 3 d	-2.03	213	1. V	1.4.2		
		104. 1	2000	1.51			( , f	24.9
the second se						11 .		
		230	-1.57 -1.46	1. 10		111.0	15	
		240.19					4.0	-9. L. T.
		25.0.10 26.5.10	-1. OX	1.		0.05 y 9 9.09 y 9	1.7	
			-1.1	14.61		18.1		86.2
		·	-0.00	8., 00 7.2725	1.1	n n y c	7.5	77.1
		1884.00	-0, 7					
	- 199. <b>.</b>	-98 <b>.</b> (1	H9.10			935.1 63	A.,	81.
		105.00	$= i \mathcal{F} = \mathcal{F} + \mathcal{F}$	1212		경험 기		nine i
		16.0	H0. N			생태	2.0	24.3
		4:0.4-	-0., 8%	1.34 35	1.	93.40	19.3	1.1
	813 i a 1	138.14	80.83	2.5 . 65	$11 \times 12$	4G • 2	9.0	95.5
		39.4.27		14.	1.0	10.0	30.9	90 - E
		1.9.01		10.1	1 si	21.4	10.8	96.7
		$\{g_{j}\}^{*}$ , $j \in I$	-11, 3 ² (1		21.1	251 <b>.</b> K	1.4.0	14.8
		51 ( <b>1</b> ( 1	- i galan	3.3	8 ge		1 - 5	91.6
		487 F • 330	-1. Y	1.1		10 x D	13.3	64 . A
		19.5	-1,250	17 - St		2.94	· · · ·	19.
	19.016	3/18-21	- 3 3 4	19. KI		2.1	11.2	$M_{F*}$

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N. Y.



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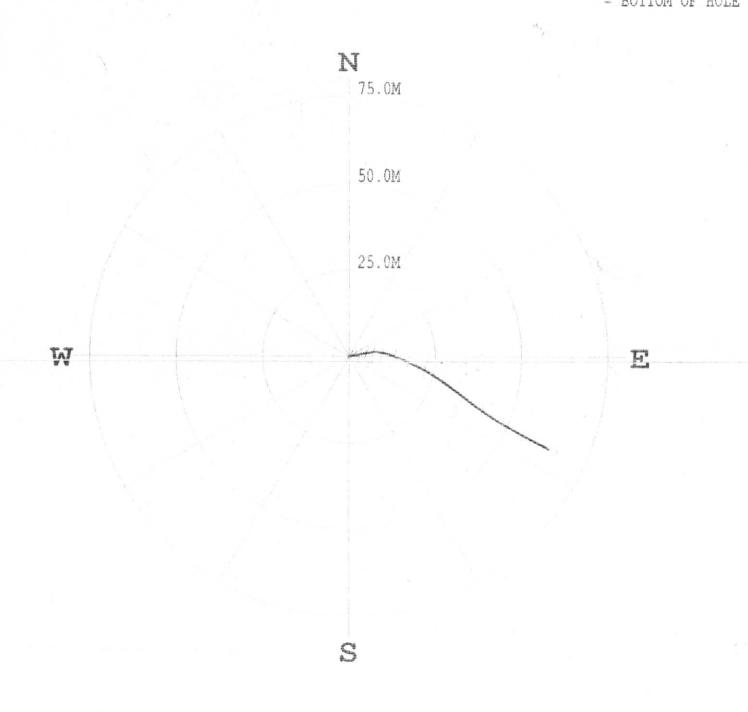


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## PLAN VIEW COMPU-LOG DEVIATION

MAG DECL: 19.0

CLIENT: FORDING COAL LTD LOCATION: FORDING RIVER MINE HOLE ID: RH 2736 DATE OF LOG: 07/23/00 PROBE: 9055A 238 SCALE: 25 M/CM TRUE DEPTH: 386.82 M AZIMUTH: 114.8 DISTANCE: 65.1 M + = 25 M INCR = BOTTOM OF HOLE



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