Summary Report on the Trefi Coal Property

2013-2014 Exploration Program

Northwest British Columbia: Centered at 6,148,000N and 572,000E (NAD 83)

Trefi Coal Ltd.

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Moose Mountain Technical Services

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ASSESSMENT REPORT TITLE PAGE AND SUMMARY

TITLE OF REPORT: Summary Report on the Trefi Coal Property, 2013-2014 Exploration Program

TOTAL COST: $ 9,907.50

AUTHOR(S): Robert J. Morris, M.Sc., P.Geo.
SIGNATURE(S):

NOTICE OF WORK PERMIT NUMBER(S)/DATE(S): CX-9-039

YEAR OF WORK: 2013-2014
PROPERTY NAME: Trefi Coal Project
CLAIM NAME(S) (on which work was done):

COMMODITIES SOUGHT: Coal

MINING DIVISION: Liard
NTS / BCGS:
LATITUDE: 55° 29' 43"
LONGITUDE: 121° 53' 34" (at centre of work)
UTM Zone: 9 **EASTING:** 572000 **NORTHING:** 6148000

OWNER(S): Trefi Coal Corp.

MAILING ADDRESS:, 33045-1583 Marine Drive, West Vancouver, BC V7V 2X7

OPERATOR(S) [who paid for the work]: Trefi Coal Corp.

MAILING ADDRESS:, 33045-1583 Marine Drive, West Vancouver, BC V7V 2X7

REPORT KEYWORDS: Walton Member, Commotion Formation, Coal

REFERENCES TO PREVIOUS ASSESSMENT WORK AND ASSESSMENT REPORT NUMBERS:

Portions of pages 6, 7, 25, 32, all of page 31, and Appendix A remain confidential under the terms of the Coal Act Regulation, and have been removed from the public version.

http://www.bclaws.ca/civix/document/id/complete/statreg/251_2004

Statement of Costs

Activity	Provider	2013	2014	Total 2013-2014
Technical Services	MMTS	$1,035.00	$2,260.00	$3,295.00
Archaeological Study	ECOFOR	$6,052.50		$6,052.50
Licences	Silenus	$560.00		$560.00
Grand Total		**$7,647.50**	**$2,260.00**	**$9,907.50**

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1 SUMMARY

This report summarizes exploration work completed on the Trefi coal property between 2008 and 2012. No physical work has been done on the property since 2012.

In June 2008, Moose Mountain Technical Services (MMTS) was retained by Anglo-Pacific Group Plc. (Anglo Pacific) to review the geology of the Trefi coal project area (Trefi), build a 3D computer model, generate a resource estimate, and recommend an infill drilling program. Since that time five drillholes, coal quality studies, and an updated resource estimate have been completed.

Anglo-Pacific is a natural resources royalties company with its head offices in London, England. The company, through its 100% owned subsidiary Trefi Coal Corp. (Trefi Coal), holds coal licences in the Pine River area, approximately 30km southwest of the town of Chetwynd, in northeast British Columbia.

The Trefi property comprises 18 coal licences covering 10,708ha. The property is approximately 30km southwest of Chetwynd, BC, centred at 6,148,000N and 572,000E (NAD 83).

This report deals with coal seams found in the Walton Member of the Commotion Formation. The Boulder Creek Formation of the Fort St. John Group hosts the coal-bearing strata on the property. Two coal seams have been modelled within a stratigraphic section up to 30m thick. The property is characterized by geology that is moderate, both with respect to stratigraphy and structure. The geology was originally defined by earlier work of geologists from Gulf Canada Resources Inc. (Gulf Canada) and Norwest Resource Consultants Ltd. Gulf Canada drilled 27 holes on the property, totalling 6,332.1m, and collected 31 coal samples, between 1980 and 1982. In 2009 five holes were completed totalling 1,006.4m and two coal core samples were collected. In 2010 and 2011, exploration options were reviewed along with coal quality data. In 2012, exploration options were again reviewed along with a site visit with Trefi management.

[redacted]

[redacted]

MMTS has modelled the deposit as geologically moderate using MineSight® software and resources have been estimated for the Trefi deposit. The project is considered a potential resource for underground mining.

A gridded-seam geological model has been developed which includes a review of the available data, formatting and treatment of data to support model development, a geological interpretation, and the construction of the gridded-seam model. Interpretation and modelling focused on the Caron Seam (Seam C).

Because Trefi is a potential underground project, physical parameters such as thickness of overburden and oxidized coal is not modelled. The bulk density of Seam C is 1.45g/cc (from Gulf Canada). Resource classification is based on distance to nearest composite. Measured mineral resources being within 450m of a neighbour, Indicated resources are in the zone between 451m-900m, while Inferred resources are 901m-2400m from a composite.

Assurance-of-existence categories are intended to reflect the level of certainty with which mineral resource quantities are known. Intuitively, one knows that the greater the distance over which seam thickness data are extrapolated, the greater the possible error; hence, several resource classification schemes have used distance from nearest data point or distance between data points as the primary criteria for assurance-of-existence categorization. In moderate geology type deposits, the assurance of existence is based on the distance from nearest data points for these deposits (GSC Paper 88-21).

Three mineral resource categories are used to define assurance-of-existence. In order of increasing uncertainty, these mineral resource categories are: Measured, Indicated, and Inferred. Measured resources have a high degree, Indicated a moderate degree, and Inferred resources a relatively low degree of geological assurance. Although the precise levels of uncertainty of these categories have not been calculated, geological experience with Canadian coal deposits suggests that Measured resource quantities are known within about 10%, Indicated within about 20%, and Inferred within about 50% (GSC Paper 88-21).

[1] *Moderate geology type refers to generally shallow dips and broad open folds*

MMTS is of the opinion that the Trefi property hosts significant coal resources and is a property of merit, worthy of further exploration. It is recommended that the next phase of exploration consist of a mapping program to verify the dip of the limbs of the syncline and to revise the geological model to fit the mapping. A follow-up drill program in several key areas along with additional coal quality testing is also recommended.

2 INTRODUCTION & SCOPE

In June 2008, Moose Mountain Technical Services (MMTS) was retained by Anglo-Pacific Group Plc (Anglo-Pacific) to create a geological model of the Trefi coal deposit, to estimate the coal resources for the deposit and to recommend a follow-up drill program. Since that time, five drillholes, coal quality studies, and an updated resource estimate have been completed.

This report deals with coal seams found in the Walton Member of the Commotion Formation. The geology of this property is defined by the previous work of geologists from Gulf Canada Resource Inc. (Gulf Canada) and Norwest Resource Consultants Ltd. This report includes a review of the previous geology and drillhole data to the end of December, 1982, as well as drillhole data from 2009.

The author, Robert J. Morris, inspected the property during 21-22 April 2009, 21-22 October 2009, and 26 October 2012. During the site visits, access to the property was observed, drilling was in progress, drill core was inspected, and coal sampling protocol was confirmed.

3 PROPERTY DESCRIPTION, ACCESSIBILITY, CLIMATE, HISTORY, INFRASTRUCTURE

The Trefi coal property is located south of the Pine River Valley, approximately 30km southwest of the town of Chetwynd in the Peace River District of northeast British Columbia, Figure 3-1. The coal licences are located south of Highway 97 and the B.C.R. railway line. The approximate centre of the property is 6,148,000N and 572,000E (UTM NAD 83).

The property consists of 18 tenures, as shown in Table 3-1 and Figures 3-1 and 3-2. The total area of the tenure is approximately 10,708 hectares. The coal licences are registered in the name of Trefi Coal Corp. (Trefi Coal), of Vancouver, B.C.; a wholly-owned subsidiary of Anglo Pacific. There are no underlying agreements or royalties on the property.

Table 3-1 Trefi Coal, Owned Tenures

Project	Claim Number	Mining Division	Issued	Expiry Date	Area (ha)
Trefi Coal Corp	411463	Liard	June 22, 2004	June 22, 2015	294
Trefi Coal Corp	411464	Liard	June 22, 2004	June 22, 2015	294
Trefi Coal Corp	411465	Liard	June 22, 2004	June 22, 2015	294
Trefi Coal Corp	411466	Liard	June 22, 2004	June 22, 2015	294
Trefi Coal Corp	411467	Liard	June 22, 2004	June 22, 2015	294
Trefi Coal Corp	411468	Liard	June 22, 2004	June 22, 2015	294
Trefi Coal Corp	411469	Liard	June 22, 2004	June 22, 2015	294
Trefi Coal Corp	417047	Liard	Sept 8, 2005	Sept 8, 2015	294
Trefi Coal Corp	417048	Liard	Sept 8, 2005	Sept 8, 2015	294
Trefi Coal Corp	417049	Liard	Sept 8, 2005	Sept 8, 2015	587
Trefi Coal Corp	417050	Liard	Sept 8, 2005	Sept 8, 2015	881
Trefi Coal Corp	417051	Liard	Sept 8, 2005	Sept 8, 2015	584
Trefi Coal Corp	417052	Liard	Sept 8, 2005	Sept 8, 2015	1,465
Trefi Coal Corp	417053	Liard	Sept 8, 2005	Sept 8, 2015	880
Trefi Coal Corp	417054	Liard	Sept 8, 2005	Sept 8, 2015	294
Trefi Coal Corp	418730	Peace River	Feb 26, 2015	Feb 26, 2016	1026
Trefi Coal Corp	418731	Peace River	Feb 26, 2015	Feb 26, 2016	1026
Trefi Coal Corp	418732	Peace River	Feb 26, 2015	Feb 26, 2016	1319
				Total	**10,708**

All of the exploration completed to date has been by permit from the BC Government. The project currently has an active Mines Act Permit, CX-9-039, which covers the completed drill program.

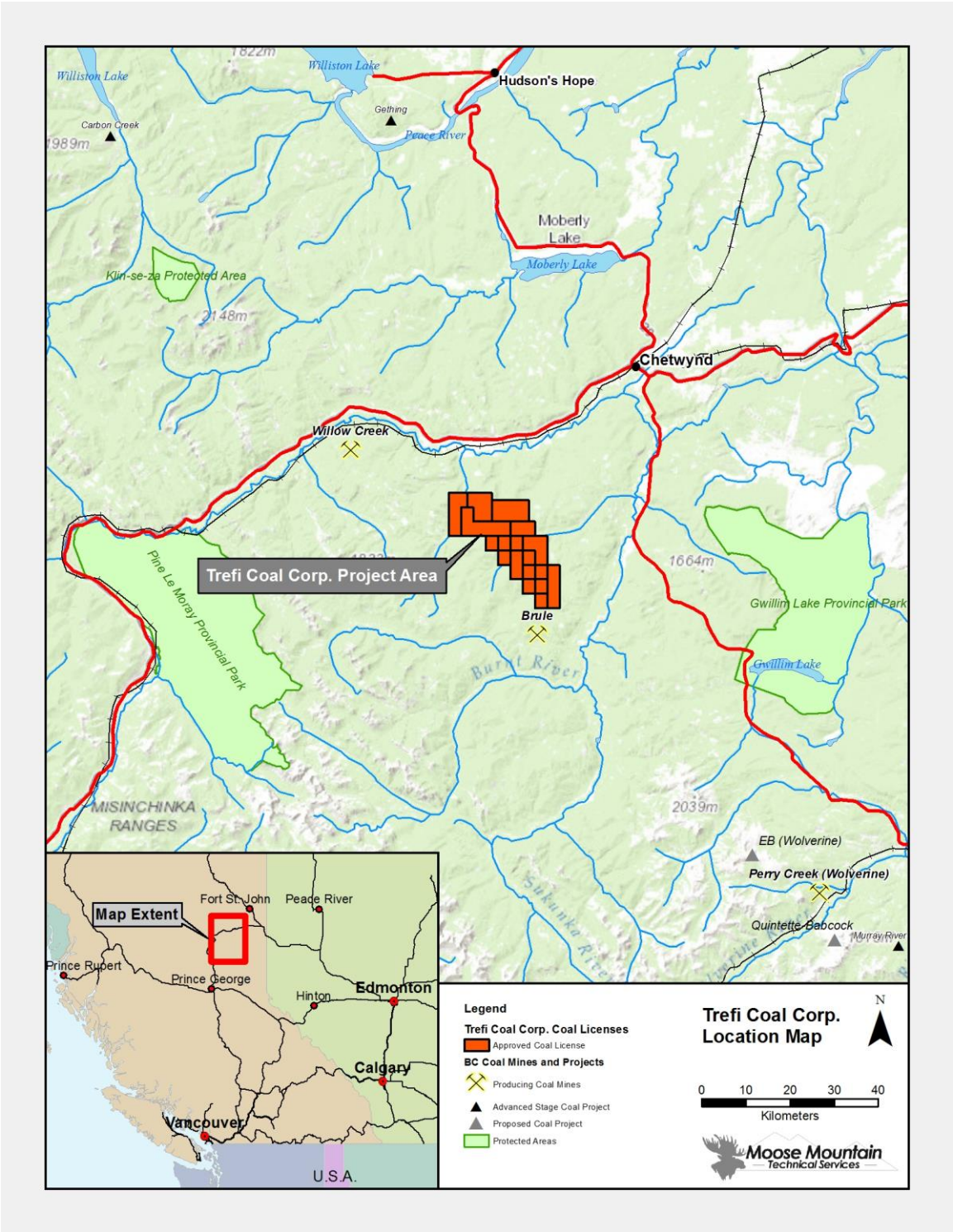

Figure 3-1 Trefi Coal Licences

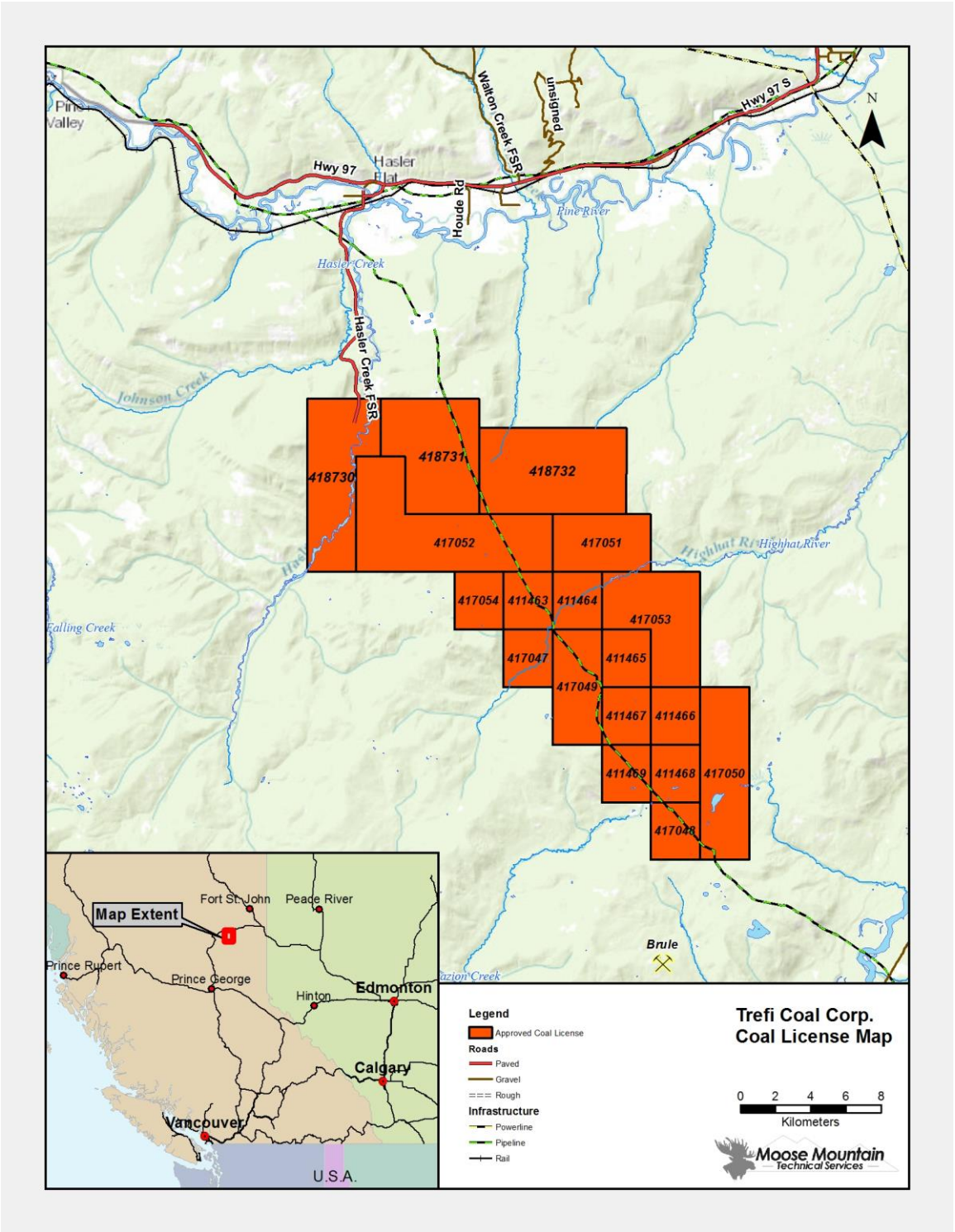

Figure 3-2 Trefi Coal Tenure

The Trefi property is located within the Pine Pass area in the Peace River District of northeast British Columbia. Primary road access to the general area is via the John Hart Highway, Highway 97, which is an all-weather paved highway which connects the Peace River District with the central interior city of Prince George, B.C. to the west and Chetwynd and Dawson Creek to the east. The southern portion of the property is accessible from Chetwynd via the Sukunka River road and an oil and gas and old coal exploration access road called the Highhat Road along Bluff Creek, a distance of about 50km. The northern portion of the property is accessible along the Hasler Creek road which leads off the main John Hart Highway about 26km west of Chetwynd and then along the Westcoast Transmission gas plant access road for a total distance from Chetwynd of about 40km. The Westcoast Transmission Grizzly Valley pipeline runs south from the main gas plant just south of the Pine River Valley through the western edge of the resource area. Some limited access is available along seismic cut lines during the winter season when the low swampy areas are sufficiently frozen.

Canadian National Railway (CN) operates a rail line through the Pine River Valley to service the Peace River District. The rail line is 8km north of the Trefi deposit and 21km from the south end of the property. The railway provides direct access to the port of Vancouver and to the Ridley Island Terminal at Prince Rupert.

The Peace River District is serviced by daily commercial airline flights to the cities of Prince George, Dawson Creek and Fort St. John. These services have respective road distances to the Trefi property of roughly 265km, 148km and 208km.

The property is situated in the Rocky Mountain Inner Foothills physiographical region and is characterized by relatively low, rounded, northwest-southeast trending ridges and valleys. Glaciation appears to have had a large influence in shaping the topography of the tenure area.

The highest elevation in the area is 1,425 metres at Highhat Mountain while the elevation in the Pine River Valley averages 600 metres. The average elevation of the area is approximately 1,240 metres.

The property is forested by jack pine and minor spruce. Poplar stands occur in low areas such as river valleys, and in wet areas adjacent to creeks and seepages. Most of the forested terrain may be classified as open forest, i.e., with little or no underbrush. The exceptions are the wet areas where willows and devil's club are common.

The climate of the region may be classified as northern temperate. Daily temperatures range from a mean maximum of 7ºC to a mean minimum of minus 6ºC, with a mean daily temperature of 1ºC. Extreme temperatures range from a maximum of 32ºC to a minimum of minus 48ºC. The average annual number of days with frost is 210.

The mean total precipitation in the region is approximately 425mm, which includes the rainfall equivalent of a mean snowfall of 165cm. The average annual number of days with measurable precipitation is ninety-five. The greatest recorded rainfall in twenty-four hours is 66.5mm.

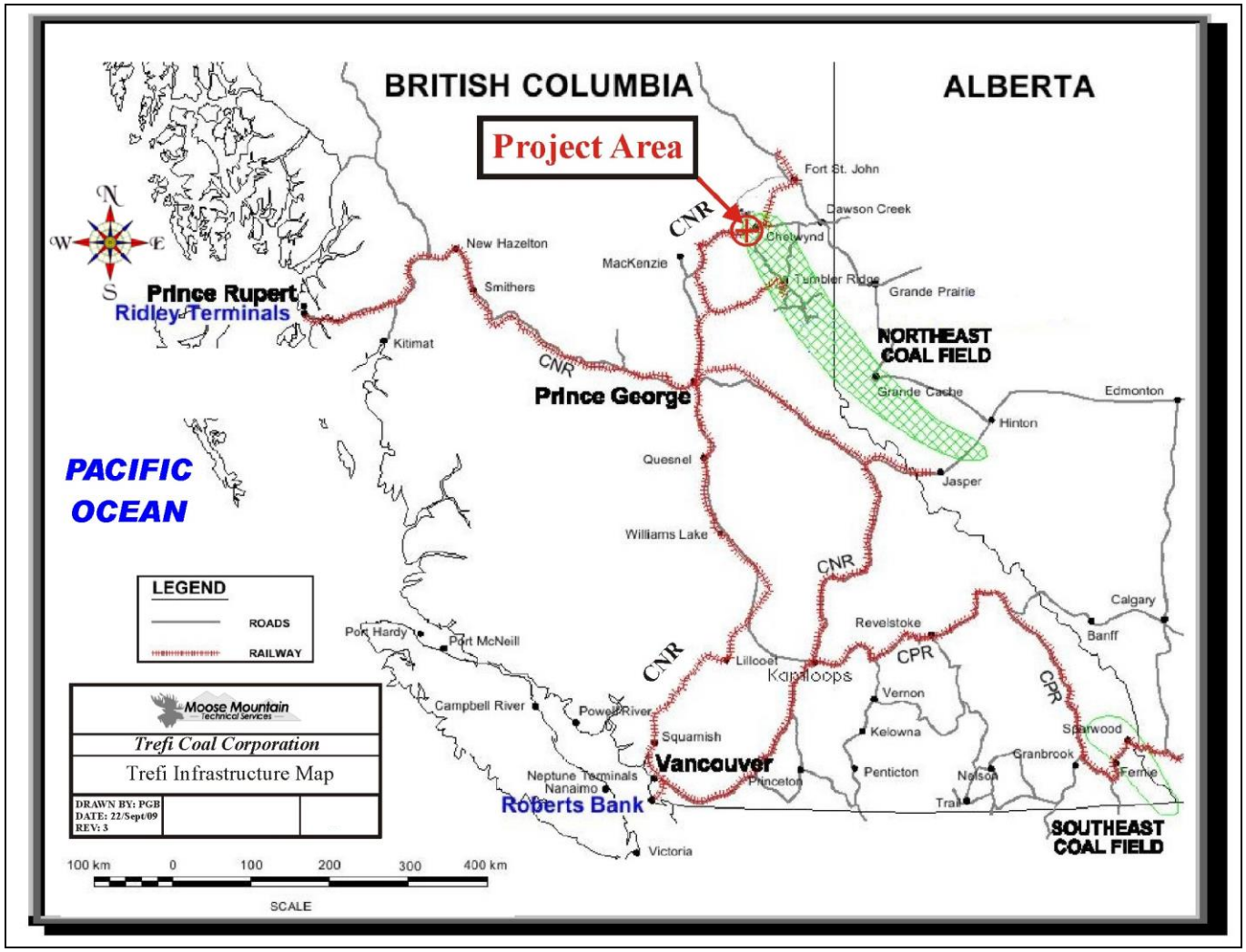

Figure 3-3 Trefi Coal, Infrastructure

4 GEOLOGY

4.1 History

Coal was discovered in the Peace River District of British Columbia during Alexander Mackenzie's overland journey to the Pacific about 200 years ago.

Exploration of the Trefi property began in April 1980, by Gulf Canada Resources Inc. The Trefi property at that time was three times the size that it is at present. Initial work involved 1:25,000 scale reconnaissance geological mapping and drilling. Rock and coal outcrop exposures on the tenures are limited due to a dense vegetative cover and overburden. The majority of geological field data was collected along drainage systems. Nine geological cross-sections were generated at approximately five kilometre centres on most of the property and at ten kilometre centres at the north end of the property.

Exploration in 1980 on the Trefi property consisted of twelve rotary drillholes and three diamond drillholes. The diamond drillholes were located south of the Pine River and have a total length of 641.4m. Core was sampled and sent for coal analysis. All holes were geophysically logged producing a suite of Gamma Ray, Neutron, Side Wall Density, Caliper and Focused Beam Resistivity Logs. The 1980 core was sent to Charlie Lake for storage. Of the rotary holes, six were drilled north of the Pine River and six south of the Pine River for a total length of 2,417.2m. Three of the 1980 holes south of the Pine River provided full seam core samples for analysis. After the 1980 field season, all the licences north of the Pine River were dropped. The size of the property shrank by approximately one half.

Exploration in 1981 on the Trefi property consisted of geological mapping at a 1:20,000 scale and the drilling of four diamond drillholes with a total length of 1,260.8m and six rotary drillholes with a total length of 1,662.3m. Four of these holes cored full seam samples of the Caron and Highhat Seams.

In 1982, exploration consisted of the drilling of two rotary drillholes with a total length of 350.4m. A full core section of the Caron seam was sampled in each hole. The drill program was designed to aid in a depositional analysis of the Trefi coal seams in order to better define the extent of the seams. Thirteen geological cross-sections were produced with the majority being spaced at two kilometre intervals though one at the south and two at the north were at four kilometre spacing.

Work completed on the Trefi property by Gulf Canada is filed with the BC Ministry of Energy and Mines as coal assessment reports 680, 681 and 682.

In the early 1980's, Gulf Canada estimated the inferred in-place resources for the Trefi region as 124.2 million tonnes for the thicker more extensive Caron seam (Seam C) and a possible 23.7 million tonnes for the thinner, less areal extensive Highhat seam (Seam H). These resources are considered historic in nature and do not comply with NI 43-101 standards.

The "inferred in-place" resource estimate from Gulf Canada would be equivalent to our total estimate of Measured, Indicated and Inferred resources combined. Gulf Canada's Caron seam resource estimate (124.2Mt) combines 11.6Mt of coal with true thickness between 0.5m and 1.5m, with an estimated 112.6Mt of coal with true thickness greater than 1.5m. The calculation methodology for the estimate is not stated. The difference between the Gulf Canada estimate and MMTS's would be that we have limited ours to the property boundary (some thick coal exists outside the coal licences) and we have not included coal that is greater than 600m below surface (some thick coal exists at greater depths of cover).

In 2009, Trefi Coal, a wholly-owned subsidiary of Anglo Pacific drilled five rotary drillholes on the Trefi property. Three of the holes were cored for coal. The total length of drilling was 1,006.39m.

The property is not in production nor has coal been produced from the property.

4.2 Geological Setting

The Cretaceous sediments of the northern Foothills were deposited along the western margin of the Western Canada Basin in a series of transgressive-regressive cycles during the Columbian Orogeny. Environments of deposition varied laterally and vertically from marine through prodeltaic and near shore, to delta plain and alluvial. Lithologies include mudstone, siltstone, sandstone, conglomerate and coal.

The Trefi property is underlain by the Lower Cretaceous Bullhead Group and Fort St. John Group sediments. Figure 4-1 compares the stratigraphic nomenclature used by Gulf Canada to that used by the Geological Survey of Canada (GSC). Because much of the present work is based on the former's work, the Gulf Canada nomenclature is used.

The oldest formation on the property is the Gething Formation which is part of the Bullhead Group. The Gething Formation is made up of fine to coarse grained sandstones, siltstones, mudstones, carbonaceous mudstones and coal. Many coal deposits in the Peace River district are in the Gething Formation. This formation may be present near the edge of the very southern licences but there are no known exposures of Gething Formation on the Trefi property.

Overlying the Gething Formation is the Moosebar Formation, which is marine and is the youngest unit of the Fort St. John Group. The Moosebar Formation is a recessive marine shale unit which consists of dark grey, rubbly weathering mudstones and siltstones.

Conformably overlying the Moosebar is the Commotion Formation, of which Gates Member is the youngest member. The Gates Member is comprised of sandstone, siltstone, mudstone, carbonaceous mudstone and some coal. Although the Gates, along with the Gething, is one of the main coal bearing units in the south part of the Peace River Coalfield, only thin seams, all less than 1.0 metre thick have been found in Gates drill core on the Trefi property.

The Hulcross Member is a recessive marine siltstone and mudstone sequence which conformably overlies the Gates Member. It, in turn, is conformably overlain by the Boulder Creek Member.

The Boulder Creek Member can be divided into 3 units: the lower, resistant, cliff forming sandstone and conglomerate unit, the middle interbedded sandstone, siltstone and minor mudstone unit and the upper, resistant, cliff forming sandstone/conglomerate unit. The majority of holes drilled on the Trefi property were terminated in this upper conglomeratic unit and it provided an excellent marker for the base of the coal-bearing Walton Member in the central part of the license area.

The Walton Member conformably overlies the Boulder Creek Member.

Overlying the Walton Member are the other formations of the Fort St. John Group, which, in this area, include in succeeding order, the Hasler and Goodrich Formations.

4.3 Walton Member

The coal-bearing Walton Member, between the underlying Boulder Creek Formation and the overlying Hasler Formation, is comprised of sandstone, siltstone, mudstone, carbonaceous mudstone, coal and occasional conglomeratic sandstone. Coal seam development occurs predominantly in the lower one-third of the Member. Interbedded mudstone, siltstone and channel sandstones comprise the upper two thirds of the Member.

South of the Pine River the thickness of the Walton Member varies from 60m to 88m, averaging 68m.

Prior to the 1980 drilling program, data on the coals of the Walton Member were derived from gas wells both on and off the property. Two seams, 2.1 and 1.37 metres thick, were intersected at a depth of 725.4m and 737.1m in Skelly Getty CS Commotion 93-P-12/a-23-D (Discovery Well) at the head waters of Goodrich Creek. Twenty-one kilometres south of this well, and outside the licences, two 0.9m seams at 1240m and 1243.5m and one 1.2m seam at 1261m, were intersected in Quasar et al Oetco: 93-P-5/c-28-I . Logs from Skelly Getty CS Commotion 93-P-12/c-29-C approximately 5.5km east of the "Discovery Well" indicated no coal of any significance and this well defines the easterly limit of coal development. The 1980 rotary and diamond drilling program demonstrated that the occurrence of these two seams is restricted to the South Pine Area. Thin coals and carbonaceous zones do occur north of the Pine River but appear discontinuous and difficult to correlate. Most of the coal seam development occurs within the basal one third of the member. Two significant coal seams are developed in the Walton Member. They are, in ascending stratigraphic, order the Highhat and the Caron Seams. A third, less significant but fairly continuous seam called the Linklater seam is found between the Highhat and Caron Seams.

The Highhat Seam occurs at the base of the member and either lies directly on the upper conglomeratic unit of the Boulder Creek Member or within one metre of the contact. The seam varies from a few centimetres to a maximum gross thickness of 2.68m containing 1.74m of coal.

The Linklater Seam is between the Highhat and Caron Seams at approximately 5 to 7m above the base of the Walton Member. It varies from 0.2m to 1.18m thick and averages 0.61m.

The Caron Seam occurs within eleven to nineteen metres of the base of the unit and varies in thickness from a few centimetres to a maximum thickness of 2.70m in the discovery well. The seam underlies most of the north-western portion of the South Pine area. The Caron Seam thins

to the east and north. In approximately half of the Caron Seam intersections, it is associated with a thin band of coal near its roof, called the Caron Rider Seam. The Caron Rider averages 0.43m thick and the rock band separating it from the Caron Seam averages 2.39m.

Detailed stratigraphic analysis undertaken as a part of the 1982 geologic program re-evaluated member contacts as well as the lateral continuity of stratigraphic units, particularly coal seams. Several datum horizons were identified including the tops of marine sandstones in the Boulder Creek Member, as well as coal seams, high natural gamma radiation beds and laterally persistent fluvial sandstone beds in the Walton Member.

This report deals with coal seams found in the Walton Member of the Commotion Formation. To date, two coal seams have been modelled on the Trefi property. They range in thickness from 0.2m to 4.85m. The seams are within a 20m portion of the lower Walton Member of the Commotion Formation.

For each seam the following criteria for inclusion in resource applies: minimum mineable seam thickness is 1.5m. A coal zone is considered mineable if it has a cumulative thickness of 1.5m or more.

Table 4-1 Distribution of Seam Thickness

Seam	Number of Intercepts	Thickness Range (m)	Number > 1m
CR	8	0.18 – 0.57	0
C	20	0.20 – 4.85	14
N	3	0.57 – 1.10	1
L	10	0.20 – 1.18	1
H	9	0.13 – 2.23	5

4.4 Structural Geology

The most intense structural feature affecting the Trefi property is the Pine River Anticline which lies immediately along the western margin of the property. Along the northeast limb of this feature resistant Boulder Creek Member sandstones and conglomerates outcrop and form northwest-trending ridges. The Walton Member is brought to surface as well, along this limb, but due to the recessive nature of the rocks and cover by surficial material, it is not normally exposed.

The northeast limb of the Pine River Anticline dips rather steeply to the northeast with attitudes ranging from 25° to 45°. At depth along this limb a flexure causes the dips to flatten and eventually dip in the opposite direction following a syncline. The syncline is called the Hulcross Syncline and this structure is generally broad with gentle dips, particularly along the northeast limb. The Hulcross Syncline narrows to the southeast and terminates just southeast of Highhat Mountain. To the northeast, the Hulcross Syncline is paired with the Commotion Anticline. Dips on the Commotion Anticline are relatively gentle. The Commotion Anticline terminates north of the Highhat Mountain where it converges with the Pine River Anticline. Axial plunge on all folds is towards the southeast.

A fault, named the Highhat Fault, is postulated just west of Highhat Mountain. Poor exposure makes it very difficult to detail this feature with any certainty.

Sub-surface investigation will be necessary to positively identify and locate this structure if present.

South of Highhat Mountain the structure becomes somewhat more complex with fold amplitudes increasing and some thrust faulting taking place. A series of thrust faults north-east of the north-east part of the property are considered to parallel the east edge of the Trefi coal property as far south as the Sukunka River. Displacement is considered to be in the order of 800metres, but there is a lack of detailed mapping in this area.

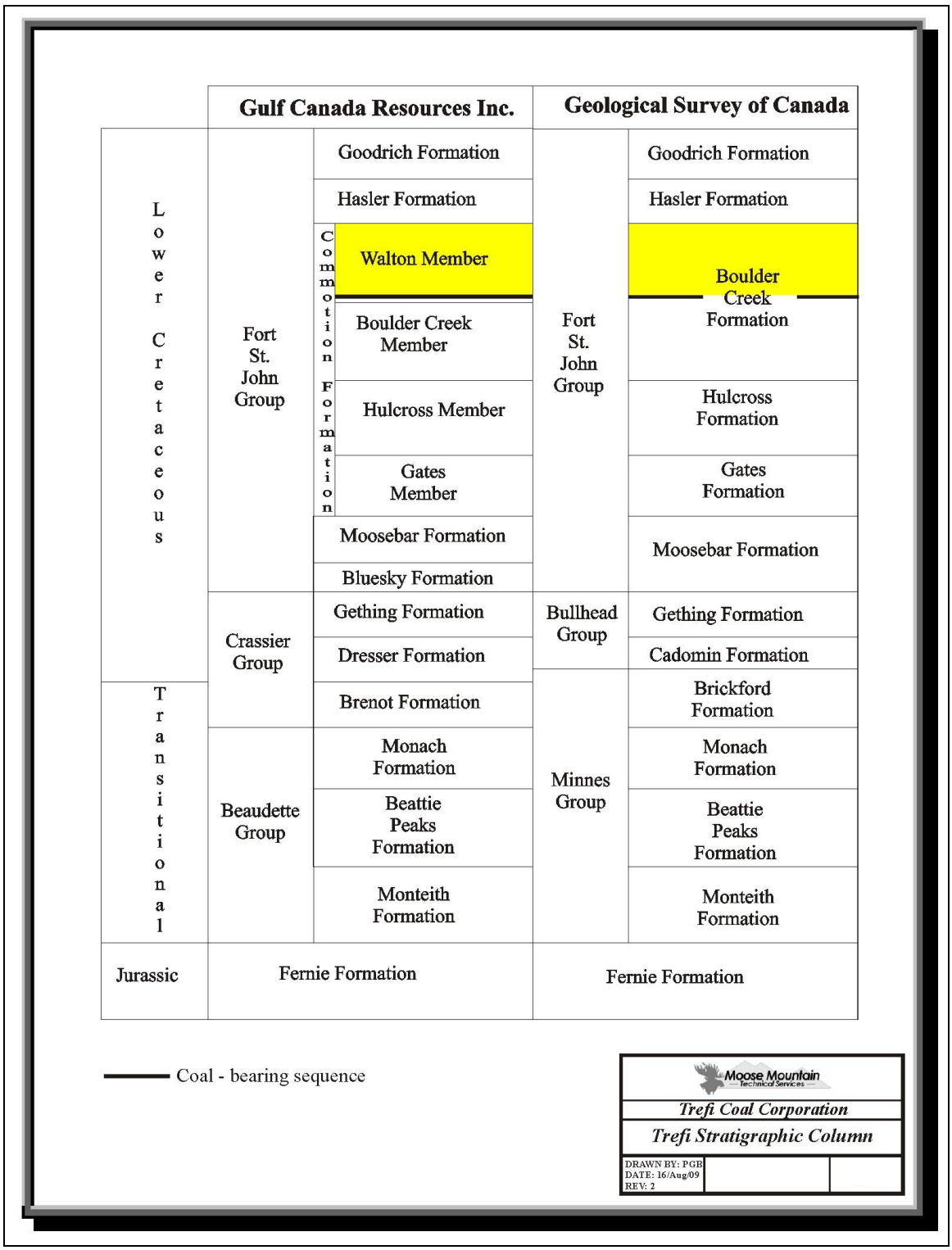

Figure 4-1 Stratigraphic Column; relates the older Gulf Canada nomenclature to the present day GSC nomenclature

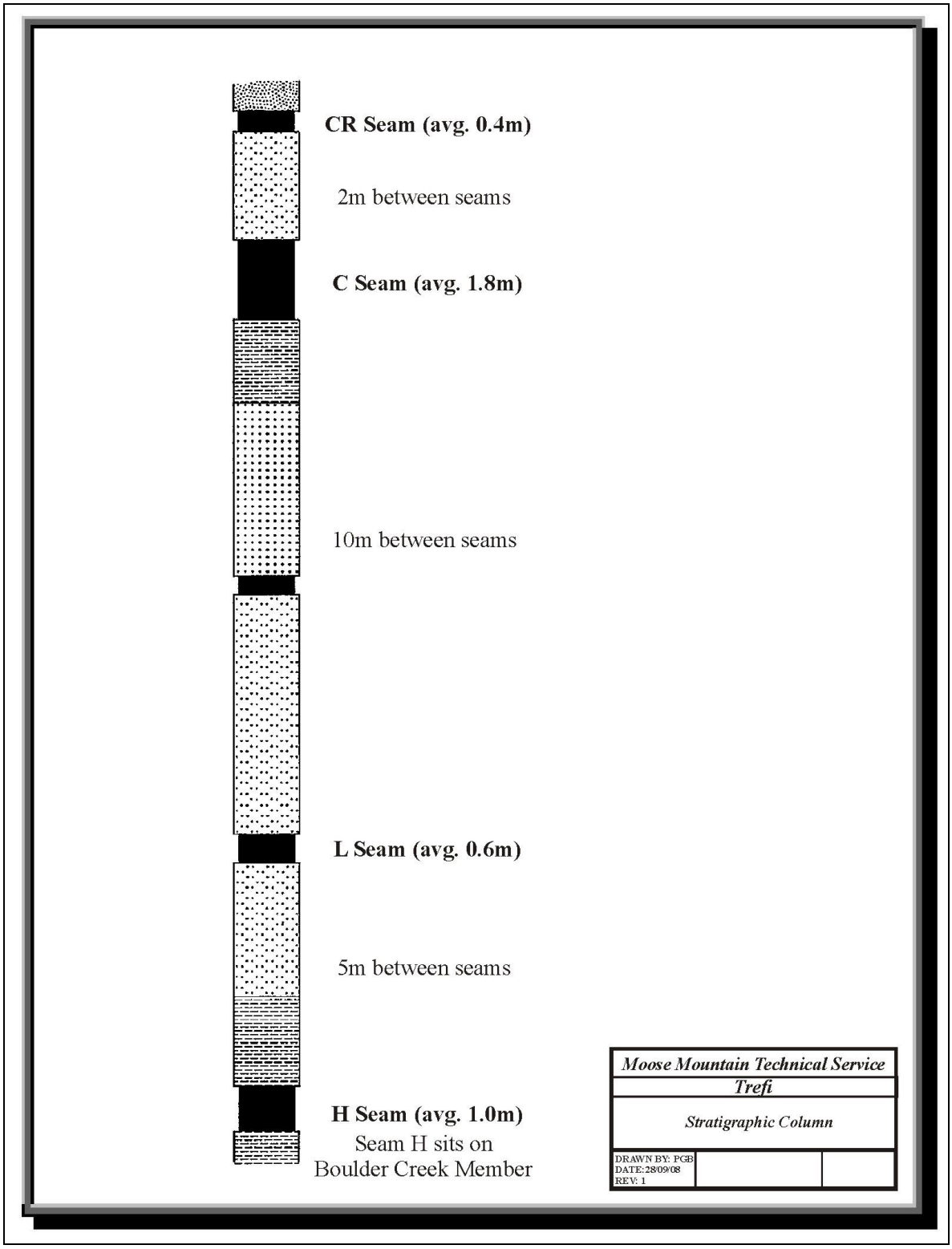

Figure 4-2 Detailed Stratigraphic Column

5 EXPLORATION PROGRAM

5.1 Historic Exploration

Coal was discovered in the Peace River District of British Columbia during Alexander Mackenzie's overland journey to the Pacific about 200 years ago.

Exploration of the Trefi property began in April 1980, by Gulf Canada Resources Inc. The Trefi property at that time was three times the size that it is at present. Initial work involved 1:25,000 scale reconnaissance geological mapping and drilling. Rock and coal outcrop exposures on the tenures are limited due to a dense vegetative cover and overburden. The majority of geological field data was collected along drainage systems. Nine geological cross-sections were generated at approximately five kilometre centres on most of the property and at ten kilometre centres at the north end of the property.

Exploration in 1980 on the Trefi property consisted of twelve rotary drillholes and three diamond drillholes. The diamond drillholes were located south of the Pine River and have a total length of 641.4m. Core was sampled and sent for coal analysis. All holes were geophysically logged producing a suite of Gamma Ray, Neutron, Side Wall Density, Caliper and Focused Beam Resistivity Logs. The 1980 core was sent to Charlie Lake for storage. Of the rotary holes, six were drilled north of the Pine River and six south of the Pine River for a total length of 2,417.2m. Three of the 1980 holes south of the Pine River provided full seam core samples for analysis. After the 1980 field season, all the licences north of the Pine River were dropped. The size of the property shrank by approximately one half.

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In 1982, exploration consisted of the drilling of two rotary drillholes with a total length of 350.4m. A full core section of the Caron seam was sampled in each hole. The drill program was designed to aid in a depositional analysis of the Trefi coal seams in order to better define the extent of the seams. Thirteen geological cross-sections were produced with the majority being spaced at two kilometre intervals though one at the south and two at the north were at four kilometre spacing.

Work completed on the Trefi property by Gulf Canada is filed with the BC Ministry of Energy and Mines as coal assessment reports 680, 681 and 682.

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The "inferred in-place" resource estimate from Gulf Canada would be equivalent to our total estimate of Measured, Indicated and Inferred resources combined. Gulf Canada's Caron seam

resource estimate (124.2Mt) combines 11.6Mt of coal with true thickness between 0.5m and 1.5m, with an estimated 112.6Mt of coal with true thickness greater than 1.5m. The calculation methodology for the estimate is not stated. The difference between the Gulf Canada estimate and MMTS's would be that we have limited ours to the property boundary (some thick coal exists outside the coal licences) and we have not included coal that is greater than 600m below surface (some thick coal exists at greater depths of cover).

The property is not in production nor has coal been produced from the property.

5.1.1 Drilling

Between 1980 and 1982, Gulf Canada completed seven diamond drillholes and sixteen rotary holes on the Trefi property. Holes were drilled into the Commotion Formation targeting the top of the Boulder Creek Member and ranged in depth from 90.0m to 617.2m.

Previous drilling located Seam C across a much larger area than that covered by the present day coal licences. It was found that to the north and northeast the seam became very thin and was deemed uneconomical.

In 2009, Trefi Coal drilled five rotary drillholes. Based on the 2008 model, holes were located in order to intersect and core the Walton Member coal seams. Four of the holes intersected the Walton Member seams, coal was cored and sampled in three of the holes and one hole was abandoned because of high water in-flow. Drillhole depths ranged from 161.84m to 288.95m.

Because the geology is simple and generally flat lying, vertical drillholes have been used to assess the resource potential of the area. The relationship between sample length and true thickness is very close to the same, but in detail it has been calculated using MineSight® which considers the 3D orientation of the drillhole and the coal seam.

In general, the Trefi coal deposit is an open syncline with a northwest/southeast strike orientation and dips on the limbs of less than 20°.

Table 5-1 Summary of Drilling, Trefi Property

Year	Diamond		Rotary		Total	
	Number	Length (m)	Number	Length (m)	Number	Length (m)
1980	3	641.4	8	1,967.7	11	2,609.1
1981	4	1,260.8	6	1,662.3	10	2,923.1
1982	0	0	2	350.4	2	350.4
2009	0	0	5	1,006.39	5	1,006.39
Totals	**7**	**1,902.2**	**21**	**4,986.8**	**28**	**6,889.0**

5.2 Geological Modelling 2009

Mineral resources have been estimated for the Trefi coal deposit. The property hosts a mineral resource that could be mined using underground methods.

The geological modelling portion of the project includes a review of the available data, formatting and treatment of data to support model development, a geological interpretation, and the construction of gridded-seam resource model. Interpretation and modelling has focused on the Caron Seam (Seam C) though the lower Highhat Seam (Seam H) may have some potential.

Model Extent
The block model is 17,500m long (in the northwest direction, the Y axis), 9,500m wide (in the northeast direction, the X axis), and 1,300m deep (elevation range from 300m to 1,600m, the Z axis). The model has been rotated 38° to the west (so that cross-sections view the deposit approximately at right angles to the strike).

Topography
Topography has been obtained from NTS maps at the scale of 1:50,000.

Overburden Surface
Overburden has not been considered in the model as it is a potential underground project.

Oxide Horizon
The degree of oxidation has not been considered in the model.

Geological Data
A geological interpretation of the footwall of Seam C was completed on cross-sections, and the footwalls from section were linked to develop a surface. The true thickness of the seam was determined mathematically by considering the orientation of the drillhole (from downhole survey) and the dip of the bedding as measured in drill core. A true thickness interpolation, using an inverse distance function (to the third power) and a 5,000m search distance, was then completed to determine seam thickness between drillholes.

Mineable thickness tagging
On the basis of the current knowledge, the Trefi deposit is classified as a moderate, potentially underground mineable deposit. Sample analysis shows the coal to be mid volatile bituminous rank, potentially marketable to the steel making industry as a weak coking coal (PCI) or as a thermal coal. Mineral resource assumptions for in situ bulk density, mineable true thicknesses, and depth below surface conform to the Paper 88-21 guidelines at 1.45g/cc, greater than 1.5 metres, and less than 600m respectively.

Mineral Resource Classification
During interpolation runs, MineSight® stores the distance from the model block to the nearest composite value in the zone that satisfies the search parameters. The distance values are then used to assign a resource classification code based on the sectional spacing prescription in GSC paper 88-21. A mineral resource code of one, Measured mineral resources indicates the influence of composite values within 450m of the model block. A value of two, Indicated resources indicates

the nearest composite in the zone is between 450 and 900 metres from the block. A value of three, Inferred resources indicates a composite value between 900 and 2400 metres away.

Assurance-of-existence categories are intended to reflect the level of certainty with which mineral resource quantities are known. Intuitively, one knows that the greater the distance over which seam thickness data are extrapolated, the greater the possible error; hence, several resource classification schemes have used distance from nearest data point or distance between data points as the primary criteria for assurance-of-existence categorization. In moderate geology type deposits, the assurance of existence is based on the distance from nearest data points for these deposits (GSC Paper 88-21).

Three mineral resource categories are used to define assurance-of-existence. In order of increasing uncertainty, these mineral resource categories are: Measured, Indicated, and Inferred. Measured resources have a high degree, Indicated a moderate degree, and Inferred resources a relatively low degree of geological assurance. Although the precise levels of uncertainty of these categories have not been calculated, geological experience with Canadian coal deposits suggests that Measured resource quantities are known within about 10%, Indicated within about 20%, and Inferred within about 50% (GSC Paper 88-21).

Robert J. Morris, M.Sc., P.Geo, managed and verified the resource estimate. Morris has no relationship to Anglo Pacific or the Trefi property. MMTS does not believe that there are permitting or environmental issues that affect the resource estimate.

[2] *Moderate geology type refers to generally shallow dips and broad, open folds*

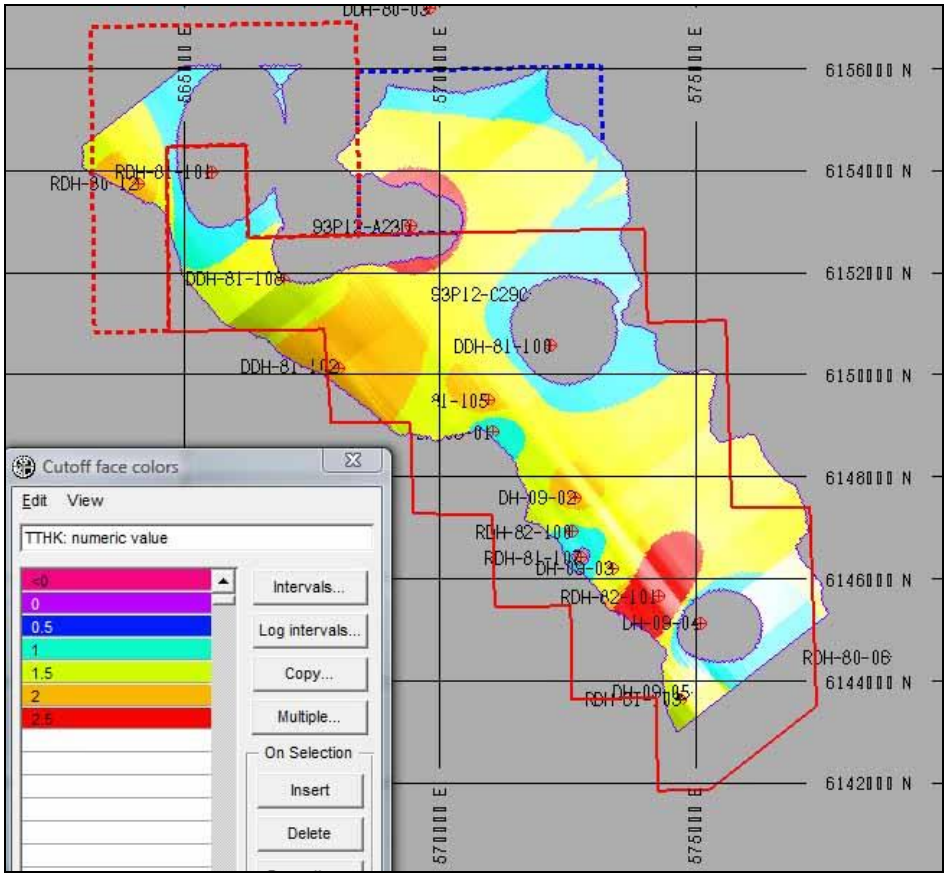

Figure 5-1 Distribution of Drillholes on Trefi Property

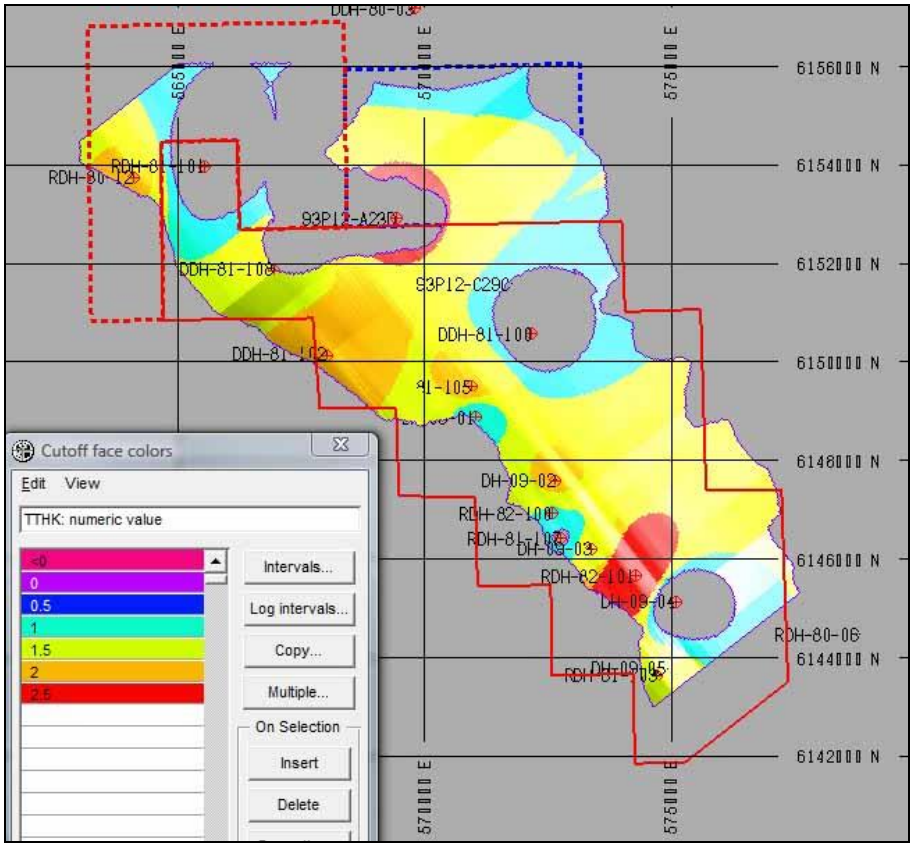

Figure 5-2 Plan showing the distribution of Seam C relative to the Trefi Property

(Red outlines the coal licences; while the red and blue dashed line outlines the coal licence application areas. The grid is 2km north/south and 5km east/west. The true thickness legend is shown in the lower left, with the yellow, orange and red colours representing coal >1.5m thick. The cut-out areas represent areas with >600m of cover.)

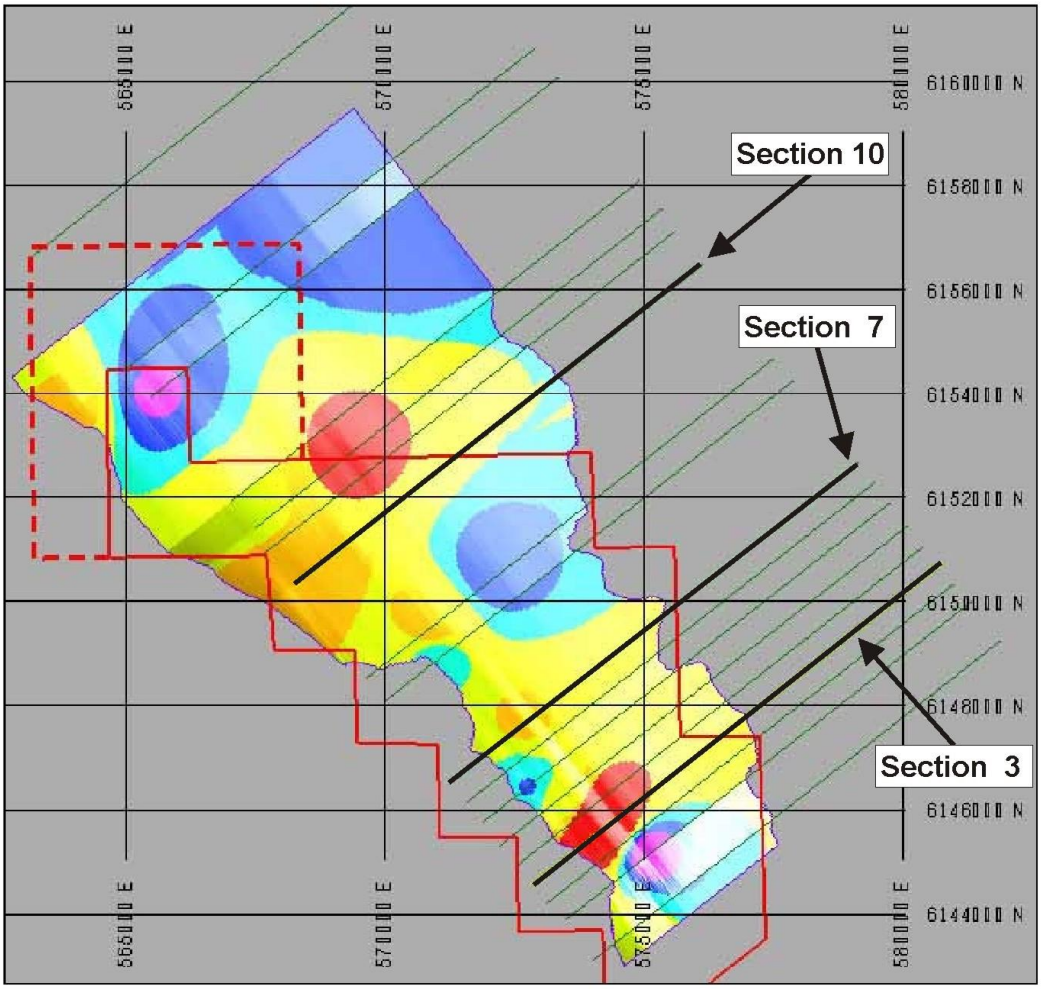

Figure 5-3 Plan showing Location of Cross-sections

(The solid red lines show the coal licences, while the dashed red line is one of the application areas (see Figure 5-2 for the additional application area)).

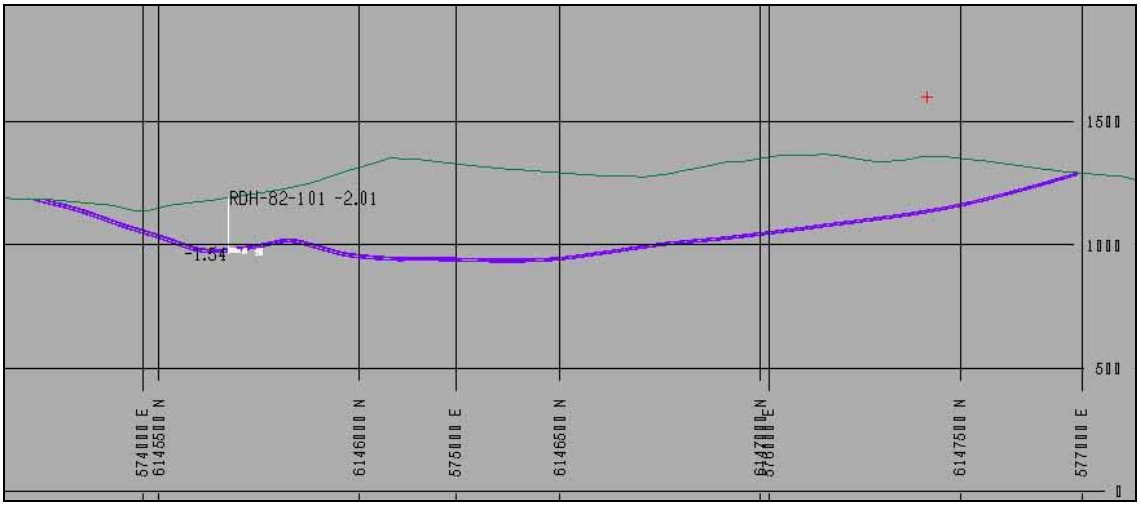

Figure 5-4 Cross-section 3; near the south end of the deposit, showing RDH82-101

(Seam C is shown in purple. The grid is 500m vertical.)

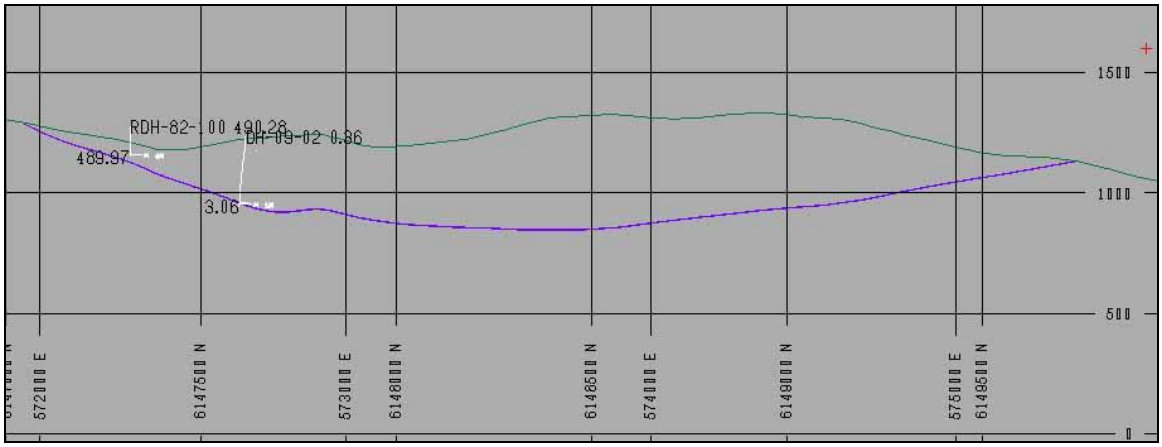

Figure 5-5 Cross-section 7; showing drillholes RDH82-100 and DH 09-02

(Seam C is in purple.)

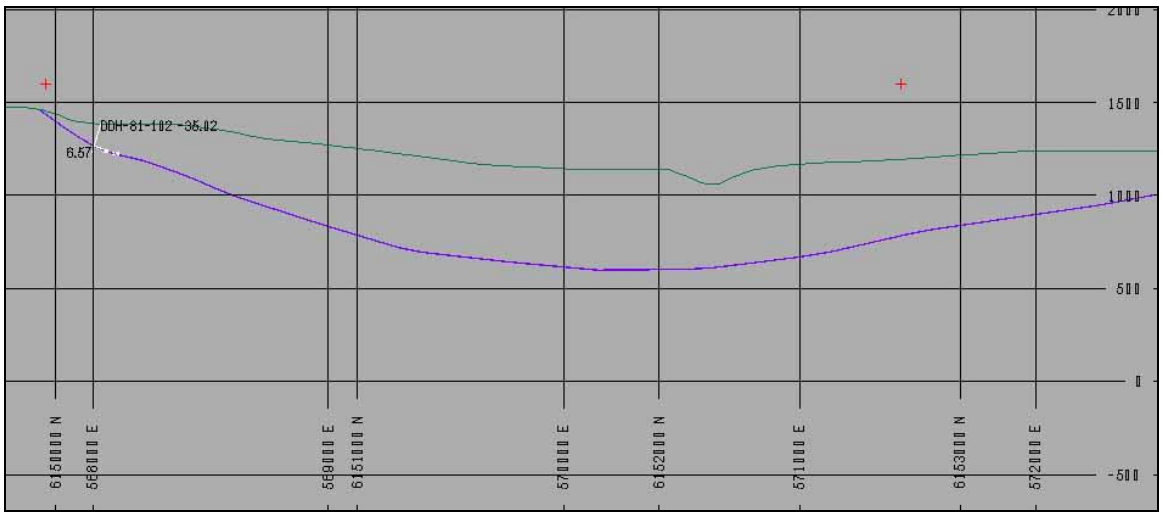

Figure 5-6 Cross-section 10; showing drillhole DDH81-102

(Seam C is in purple.)

6 SUMMARY AND CONCLUSIONS

The Trefi coal deposit is considered a property of merit, which warrants further exploration.

The Trefi coal property covers an area of 10,708ha approximately 30km southwest of Chetwynd, British Columbia. The property is within 10km of a railway, power, and a paved highway.

The property was explored in the early 1980's by Gulf Canada. In total, 28 drillholes have been completed for a total of 6,889.0m, including five holes completed in 2009 by Trefi Coal (a subsidiary of Anglo Pacific). All of the data from the 28 drillholes has been included in this study.

The coal seams are hosted by the Boulder Creek Formation of the Fort St. John Group. The Caron Seam (Seam C) has been studied in some detail and determined to cover an area at least 15km long in the northwest/southeast direction by 7km wide. Most of the drilling has been completed on the western side of the deposit leaving the eastern side with few drillholes. The area is geologically undeformed with shallow dips and open folds.

[redacted]

[redacted]

The Trefi property is considered a significant coal resource, which warrants further exploration. It is recommended that the next phase of exploration consist of a mapping program to verify the dip of the limbs of the syncline and to revise the geological model to fit the mapping. A preliminary economic assessment is suggested as well, with at least five drillholes to verify the resource potential. Additional coal quality testing is recommended in a Phase 1 program, and a further five holes in a Phase 2 program, if warranted.

7 REFERENCES

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Hughes, J.D., L. Klatzel-Mudry, and D.J. Nikols. A Standardized Coal Resource/Reserve Reporting System for Canada. Paper 88-21 Geological Survey of Canada. 1989.

MacFarlane, D. Geological Report, Trefi Coal Project- Peace River Coalfield, Northeastern British Columbia. 1981 Exploration Program. November, 1981.

CERTIFICATE AND SIGNATURE PAGES

CERTIFICATE OF QUALIFICATIONS: ROBERT J. MORRIS

I Robert J. Morris, Principal Geologist, Moose Mountain Technical Services hereby certify that:

1. This certificate applies to the assessment report titled ***Summary Report on the Trefi Coal Project – 2013-2014 Exploration Program*** dated 5 March 2015.
2. I am independent of the Trefi Coal Corp. and work as a consultant geologist.
3. That I graduated as a geologist from the University of British Columbia, Vancouver, with a degree of Bachelor of Science in 1973.
4. That I graduated as a geologist from Queen's University, Kingston, Ontario, with a degree of Master of Science in 1978.
5. That I am a member in good standing of the Association of Professional Engineers and Geoscientists of the Province of British Columbia (registration #18,301).
6. That I have been involved in the mining and exploration projects since my graduation in 1973.
7. That I am familiar with the subject area from site visits in 2009 and 2012, and that I personally supervised the preparation of this report.

Dated this 5th day of March 2015; in Fernie, British Columbia

"Signed and Sealed"

_____

R.J. Morris, M.Sc., P.Geo.

Appendix B Drillhole Data

LEGEND	
tw	top of Walton Member
ss	sandstone
r	rock
c	coal
bw	base of Walton Member
CR	Caron Rider Seam
C	Caron Seam
N	New Seam
L	Linklater Seam
H	Highhat Seam
th	top of Hulcross Member
tg	top of Gates Member
tm	top of Moosebar Formation

HOLE ID	UTM-E	UTM-N	Elev. (m)	TD (m)	From	To	Thick	Rock type	Seam
DDH-80-01	567031.22	6160881.20	710.00	198.70	0	124	124	tw	
DDH-80-01					124	128.5	4.5	ss	
DDH-80-01					128.5	132.3	3.8	r	
DDH-80-01					132.3	157.5	25.2	ss	
DDH-80-01					157.5	165.3	7.8	r	
DDH-80-01					165.3	165.5	0.2	c	C
DDH-80-01					165.5	170.28	4.78	r	
DDH-80-01					170.28	171.16	0.88	c	N
DDH-80-01					171.16	174.1	2.94	r	
DDH-80-01					174.1	174.3	0.2	c	L
DDH-80-01					174.3	180.5	6.2	r	
DDH-80-01					180.5	180.7	0.2	c	H
DDH-80-01					180.7	186.7	6	bw	
DDH-80-01					186.7	198.72	12.02	r	
DDH-80-02	556239.39	6160701.88	955.00	222.40	0	171.2	171.2	tw	
DDH-80-02					171.2	180	8.8	r	
DDH-80-02					180	189	9	ss	
DDH-80-02					189	208.5	19.5	r	
DDH-80-02					208.5	213.6	5.1	ss	
DDH-80-02					213.6	227.34	13.74	r	
DDH-80-03	569804.46	6157197.37	832.00	220.30	0	144.5	144.5	tw	
DDH-80-03					144.5	151	6.5	r	
DDH-80-03					151	158	7	ss	

HOLE ID	UTM-E	UTM-N	Elev. (m)	TD (m)	From	To	Thick	Rock type	Seam
DDH-80-03					158	173.3	15.3	r	
DDH-80-03					173.3	193.3	20	ss	
DDH-80-03					193.3	194.75	1.45	r	
DDH-80-03					194.75	195.27	0.52	c	C
DDH-80-03					195.27	201.1	5.83	r	
DDH-80-03					201.1	201.3	0.2	c	L
DDH-80-03					201.3	207.2	5.9	r	
DDH-80-03					207.2	207.65	0.45	c	H
DDH-80-03					207.65	212.8	5.15	bw	
DDH-80-03					212.8	220.3	7.5	r	
RDH-80-01	564531.63	6157670.08	775.00	317.00	0	228	228	tw	
RDH-80-01					228	283.1	55.1	r	
RDH-80-01					283.1	283.5	0.4	c	C
RDH-80-01					283.5	286.14	2.64	r	
RDH-80-01					286.14	286.94	0.8	c	L
RDH-80-01					286.94	294.65	7.71	r	
RDH-80-01					294.65	295.08	0.43	c	H
RDH-80-01					295.08	305.2	10.12	bw	
RDH-80-01					305.2	317	11.8	r	
RDH-80-02	560382.09	6163726.52	698.00	382.50	0	323.8	323.8	tw	
RDH-80-02					323.8	325	1.2	r	
RDH-80-02					325	335	10	ss	
RDH-80-02					335	358	23	r	
RDH-80-02					358	363	5	ss	
RDH-80-02					363	376.73	13.73	r	
RDH-80-02					376.73	377.6	0.87	c	
RDH-80-02					377.6	382	4.4	r	
RDH-80-03	548400.00	6168600.00	885.00	244.00	0	174	174	tw	
RDH-80-03					174	227.7	53.7	bw	
RDH-80-03					227.7	244	16.3	r	
RDH-80-04	567625.00	6167050.00	795.00	105.50	0	36.2	36.2	tw	
RDH-80-04					36.2	101.3	65.1	bw	
RDH-80-04					101.3	105.5	4.2	r	
RDH-80-05	569225.00	6163925.00	780.00	270.50	0	13.3	13.3	bw	
RDH-80-05					13.3	122.3	109	th	
RDH-80-05					122.3	216.5	94.2	tg	
RDH-80-05					216.5	381.3	164.8	tm	

HOLE ID	UTM-E	UTM-N	Elev. (m)	TD (m)	From	To	Thick	Rock type	Seam
RDH-80-05					381.3	399	17.7	r	
RDH-80-06	578811.77	6144477.39	1060.00	249.90	0	6.2	6.2	tw	
RDH-80-06					6.2	94	87.8	bw	
RDH-80-06					94	142.5	48.5	th	
RDH-80-06					142.5	247	104.5	r	
RDH-80-07	573475.09	6146149.91	1250.00	202.70	0	134.5	134.5	tw	
RDH-80-07					134.5	142.2	7.7	r	
RDH-80-07					142.2	148	5.8	ss	
RDH-80-07					148	154	6	r	
RDH-80-07					154	155.5	1.5	ss	
RDH-80-07					155.5	173.5	18	r	
RDH-80-07					173.5	174.5	1	ss	
RDH-80-07					174.5	179.5	5	r	
RDH-80-07					179.5	183.97	4.47	ss	
RDH-80-07					183.97	184.54	0.57	c	CR
RDH-80-07					184.54	186	1.46	ss	
RDH-80-07					186	188.53	2.53	r	
RDH-80-07					188.53	190.5	1.97	c	C
RDH-80-07					190.5	190.7	0.2	bw	
RDH-80-07					190.7	201.5	10.8	r	
RDH-80-08	575097.90	6145138.36	1153.00	172.50	0	82.5	82.5	tw	
RDH-80-08					82.5	85	2.5	r	
RDH-80-08					85	97	12	ss	
RDH-80-08					97	104.5	7.5	r	
RDH-80-08					104.5	108.5	4	ss	
RDH-80-08					108.5	132.7	24.2	r	
RDH-80-08					132.7	144	11.3	ss	
RDH-80-08					144	145.59	1.59	r	
RDH-80-08					145.59	148.3	2.71	c	C
RDH-80-08					148.3	148.5	0.2	bw	
RDH-80-08					148.5	172.5	24	r	
RDH-80-09	557125.00	6175400.00	940.00	90.00	0	36.2	36.2	tw	
RDH-80-09					36.2	79.63	43.43	r	
RDH-80-09					79.63	80.34	0.71	c	
RDH-80-09					80.34	85.25	4.91	r	
RDH-80-09					85.25	85.81	0.56	bw	
RDH-80-09					85.81	90	4.19	r	

HOLE ID	UTM-E	UTM-N	Elev. (m)	TD (m)	From	To	Thick	Rock type	Seam
RDH-80-10	543375.00	6192575.00	880.00	120.50	0	41	41	tw	
RDH-80-10					41	93	52	bw	
RDH-80-10					93	120.5	27.5	r	
RDH-80-11	564091.10	6153797.24	832.00	133.50	0	58.8	58.8	tw	
RDH-80-11					58.8	66.5	7.7	r	
RDH-80-11					66.5	76	9.5	ss	
RDH-80-11					76	99	23	r	
RDH-80-11					99	108.98	9.98	ss	
RDH-80-11					108.98	111.2	2.22	c	C
RDH-80-11					111.2	116.1	4.9	r	
RDH-80-11					116.1	116.82	0.72	c	L
RDH-80-11					116.82	122.55	5.73	r	
RDH-80-11					122.55	124.28	1.73	c	H
RDH-80-11					124.28	126.1	1.82	bw	
RDH-80-11					126.1	133.5	7.4	r	
RDH-80-12	564086.14	6153761.73	832.00	128.60	0	58.8	58.8	tw	
RDH-80-12					58.8	66.5	7.7	r	
RDH-80-12					66.5	76	9.5	ss	
RDH-80-12					76	99	23	r	
RDH-80-12					99	107.42	8.42	ss	
RDH-80-12					107.42	109.52	2.1	c	C
RDH-80-12					109.52	114.41	115.03	r	
RDH-80-12					114.41	115.03	0.62	c	L
RDH-80-12					115.03	120.85	5.82	r	
RDH-80-12					120.85	122.47	1.62	c	H
RDH-80-12					122.47	126.1	3.63	bw	
RDH-80-12					126.1	133.5	7.4	r	
93P12-A23D	569437.48	6152928.40	1264.00	4564.00	0	672	672	tw	
93P12-A23D					672	725.6	53.6	r	
93P12-A23D					725.6	728.3	2.7	c	C
93P12-A23D					728.3	733.5	5.2	r	
93P12-A23D					733.5	734.6	1.1	c	N?
93P12-A23D					734.6	737.16	2.56	r	
93P12-A23D					737.16	738.53	1.37	c	H
93P12-A23D					738.53	740	1.47	bw	
93P12-A23D					740	824	84	th	
93P12-A23D					824	938	114	tg	

HOLE ID	UTM-E	UTM-N	Elev. (m)	TD (m)	From	To	Thick	Rock type	Seam
93P12-A23D					938	1159	221	tm	
93P12-A23D					1159	4564	3405	r	
93P12-C29C	571750.00	6151600.00	1242.00	3594.00	0	550	550	tw	
93P12-C29C					550	625	75	bw	
93P12-C29C					625	748	123	th	
93P12-C29C					748	854	106	tg	
93P12-C29C					854	1083	229	tm	
93P12-C29C					1083	3594	2511	r	
DDH-81-100	572178.29	6150564.92	923.00	245.30	0	172.8	172.8	tw	
DDH-81-100					172.8	177.5	4.7	r	
DDH-81-100					177.5	182.5	5	ss	
DDH-81-100					182.5	205.6	23.1	r	
DDH-81-100					205.6	212.5	6.9	ss	
DDH-81-100					212.5	218.25	5.75	r	
DDH-81-100					218.25	218.43	0.18	c	CR
DDH-81-100					218.43	223.6	5.17	r	
DDH-81-100					223.6	224.21	0.61	c	C
DDH-81-100					224.21	228.84	4.63	r	
DDH-81-100					228.84	229.13	0.29	c	L
DDH-81-100					229.13	234	4.87	bw	
DDH-81-100					234	243.94	9.94		
RDH-81-101	565553.59	6153983.93	887.00	367.00	0	314	314	tw	
RDH-81-101					314	319.2	5.2	r	
RDH-81-101					319.2	330	10.8	ss	
RDH-81-101					330	343.5	13.5	r	
RDH-81-101					343.5	363.2	19.7	ss	
RDH-81-101					363.2	363.63	0.43	c	C
RDH-81-101					363.63	368.51	4.88	r	
RDH-81-101					368.51	369.2	0.69	c	L
RDH-81-101					369.2	377	7.8	r	
RDH-81-101					377	377.13	0.13	c	H
RDH-81-101					377.13	384.2	7.07	bw	
RDH-81-101					384.2	400	15.8	r	
DDH-81-102	568011.62	6150175.50	1380.00	160.00	0	46.5	46.5	tw	
DDH-81-102					46.5	57.8	11.3	r	
DDH-81-102					57.8	66.8	9	ss	
DDH-81-102					66.8	107	40.2	r	

HOLE ID	UTM-E	UTM-N	Elev. (m)	TD (m)	From	To	Thick	Rock type	Seam
DDH-81-102					107	118.77	11.77	ss	
DDH-81-102					118.77	119.33	0.56	c	CR
DDH-81-102					119.33	121.2	1.87	r	
DDH-81-102					121.2	123.63	2.43	c	C
DDH-81-102					123.63	128.43	4.8	r	
DDH-81-102					128.43	129	0.57	c	N
DDH-81-102					129	136.66	7.66	r	
DDH-81-102					136.66	137.84	1.18	c	L
DDH-81-102					137.84	151.3	13.46	bw	
DDH-81-102					151.3	159.09	7.79	r	
RDH-81-103	574739.14	6143658.88	1054.00	329.90	0	233.3	233.3	tw	
RDH-81-103					233.3	239	5.7	r	
RDH-81-103					239	246.5	7.5	ss	
RDH-81-103					246.5	253.5	7	r	
RDH-81-103					253.5	260	6.5	ss	
RDH-81-103					260	290.7	30.7	r	
RDH-81-103					290.7	301.7	11	ss	
RDH-81-103					301.7	303.14	1.44	r	
RDH-81-103					303.14	304.91	1.77	c	C
RDH-81-103					304.91	392.2	87.29	r	
RDH-81-104	572663.53	6147602.48	1233.00	281.90	0	208.5	0	tw	
RDH-81-104					208.5	211.5	3	r	
RDH-81-104					211.5	218.8	7.3	ss	
RDH-81-104					218.8	241	22.2	r	
RDH-81-104					241	259.2	18.2	ss	
RDH-81-104					259.2	260.82	1.62	r	
RDH-81-104					260.82	261.34	0.52	c	CR
RDH-81-104					261.34	263.28	1.94	r	
RDH-81-104					263.28	265.72	2.44	c	C
RDH-81-104					265.72	271.6	5.88	bw	
RDH-81-104					271.6	281.9	10.3	r	
DDH-81-105	570960.80	6149506.59	971.00	238.30	0	154.5	154.5	tw	
DDH-81-105					154.5	160	5.5	r	
DDH-81-105					160	166	6	ss	
DDH-81-105					166	187.3	21.3	r	
DDH-81-105					187.3	202	14.7	ss	
DDH-81-105					202	204.48	2.48	r	

HOLE ID	UTM-E	UTM-N	Elev. (m)	TD (m)	From	To	Thick	Rock type	Seam
DDH-81-105					204.48	206.85	2.37	c	C
DDH-81-105					206.85	213.78	6.93	r	
DDH-81-105					213.78	214.15	0.37	c	L
DDH-81-105					214.15	231.5	17.35	r	
DDH-81-105					231.5	232.5	1	bw	
DDH-81-105					232.5	238.3	5.8	r	
RDH-81-106C	575111.59	6145128.10	1153.00	148.90	0	82.5	82.5	tw	
RDH-81-106C					82.5	144.48	61.98	r	
RDH-81-106C					144.48	145.34	0.86	c	C
RDH-81-106C					145.34	149	3.66	r	
RDH-81-107	572773.64	6146442.84	1297.00	342.90	0	74.7	74.7	tw	
RDH-81-107					74.7	83.2	8.5	r	
RDH-81-107					83.2	86.8	3.6	ss	
RDH-81-107					86.8	89.5	2.7	r	
RDH-81-107					89.5	93.5	4	ss	
RDH-81-107					93.5	112	18.5	r	
RDH-81-107					112	116	4	ss	
RDH-81-107					116	120.65	4.65	r	
RDH-81-107					120.65	121.22	0.57	c	CR
RDH-81-107					121.22	122.3	1.08	r	
RDH-81-107					122.3	128	5.7	ss	
RDH-81-107					128	130.8	2.8	r	
RDH-81-107					130.8	131.76	0.96	c	C
RDH-81-107					131.76	136.5	4.74	r	
RDH-81-107					136.5	162	25.5	ss	
RDH-81-107					162	163	1	bw	
RDH-81-107					163	342.9	179.9		
DDH-81-108	566940.61	6151908.66	1204.00	617.20	0	542.4	542.4	tw	
DDH-81-108					542.4	548.8	6.4	r	
DDH-81-108					548.8	559.7	10.9	ss	
DDH-81-108					559.7	583.2	23.5	r	
DDH-81-108					583.2	590	6.8	ss	
DDH-81-108					590	592.8	2.8	r	
DDH-81-108					592.8	594.5	1.7	c	C
DDH-81-108					594.5	601.95	7.45	r	
DDH-81-108					601.95	602.83	0.88	c	L
DDH-81-108					602.83	608.42	5.59	r	

HOLE ID	UTM-E	UTM-N	Elev. (m)	TD (m)	From	To	Thick	Rock type	Seam
DDH-81-108					608.42	609.38	0.96	c	H
DDH-81-108					609.38	617.2	7.82	r	
RDH-81-109C	573475.09	6146179.48	1250.00	191.70	0	134.5	134.5	tw	
RDH-81-109C					134.5	184.54	50.04	r	
RDH-81-109C					184.54	184.96	0.42	c	CR
RDH-81-109C					184.96	187.94	2.98	r	
RDH-81-109C					187.94	190.24	2.3	c	C
RDH-81-109C					190.24	191.7	1.46	r	
RDH-82-100	572597.97	6146934.08	1274.00	122.40	0	50	50	tw	
RDH-82-100					50	61.8	11.8	r	
RDH-82-100					61.8	70	8.2	ss	
RDH-82-100					70	88.5	18.5	r	
RDH-82-100					88.5	100	11.5	ss	
RDH-82-100					100	105.7	5.7	r	
RDH-82-100					105.7	108.5	2.8	ss	
RDH-82-100					108.5	108.9	0.4	r	
RDH-82-100					108.9	109.1	0.2	c	CR
RDH-82-100					109.1	111.7	2.6	r	
RDH-82-100					111.7	113.2	1.5	c	C
RDH-82-100					113.2	122.4	9.2	r	
RDH-82-101	574273.90	6145675.33	1192.00	228.00	0	131.5	131.5	tw	
RDH-82-101					131.5	141	9.5	r	
RDH-82-101					141	155	14	ss	
RDH-82-101					155	173	18	r	
RDH-82-101					173	175.5	2.5	ss	
RDH-82-101					175.5	197	21.5	r	
RDH-82-101					197	203.57	6.57	ss	
RDH-82-101					203.57	204	0.43	c	CR
RDH-82-101					204	206	2	ss	
RDH-82-101					206	207.25	1.25	r	
RDH-82-101					207.25	212.1	4.85	c	C
RDH-82-101					212.1	217.42	5.32	r	
RDH-82-101					217.42	219.65	2.23	c	H
RDH-82-101					219.65	228	8.35	r	
DH-09-01	571044.89	6148897.43	977.28	184.09	0	52.1	52.1	r	
DH-09-01					52.1	52.4	0.3	c	CR
DH-09-01					52.4	56	3.6	r	

HOLE ID	UTM-E	UTM-N	Elev. (m)	TD (m)	From	To	Thick	Rock type	Seam
DH-09-01					56	56.1	0.1	c	
DH-09-01					56.1	58.8	2.7	r	
DH-09-01					58.8	60.1	1.3	c	C
DH-09-01					60.1	64.6	4.5	r	
DH-09-01					64.6	64.8	0.2	c	N
DH-09-01					64.8	76	11.2	r	
DH-09-01					76	77	1	bw	
DH-09-01					77	184.09	107.09	r	
DH-09-02	572672.67	6147614.16	1232.95	288.95	0	213	213	tw	
DH-09-02					213	270.8	57.8	r	
DH-09-02					270.8	271.25	0.45	c	CR
DH-09-02					271.25	273.9	2.65	r	
DH-09-02					273.9	274.2	0.3	c	C
DH-09-02					274.2	274.6	0.4	r	
DH-09-02					274.6	276.1	1.5	c	C
DH-09-02					276.1	288.95	12.85	r	
DH-09-03	573409.02	6146220.95	1258.79	197.51	0	134	134	tw	
DH-09-03					134	183.2	49.2	r	
DH-09-03					183.2	183.6	0.4	c	CR
DH-09-03					183.6	187.4	3.8	r	
DH-09-03					187.4	189.1	1.7	c	C
DH-09-03					189.1	197.51	8.41	r	
DH-09-04	575092.94	6145150.46	1141.30	161.84	0	84	84	tw	
DH-09-04					84	146.1	62.1	r	
DH-09-04					146.1	146.2	0.1	c	C
DH-09-04					146.2	161.84	15.64	r	
DH-09-05	574908.98	6143796.14	1046.11	175.00	0	0.1	0.1		