# BC Geological Survey Coal Assessment Report 1048



#### COAL ASSESSMENT REPORT TITLE PAGE AND SUMMARY

TITLE OF REPORT: Coal Assessment Report for the Willow Creek coal lease -- Volume 5: Willow Creek Mine, 2018 infill drilling

TOTAL COST: \$1,617,533.79

AUTHOR(S): C.G. Cathyl-Huhn P.Geo, 17.March, 2019

SIGNATURE(S):

NOTICE OF WORK PERMIT NUMBER(S)/DATE(S):

YEAR OF WORK: 2018-2019 lease term

PROPERTY NAME: Willow Creek

COAL LICENSE(S) AND/OR LEASES ON WHICH PHYSICAL WORK WAS DONE:

Coal Lease 389294

MINERAL INVENTORY MINFILE NUMBER(S), IF KNOWN: 930.008

MINING DIVISION: Liard

NTS / BCGS: NTS 93O/9 / BCGS 93O.059, 93O.060, 93O.069, and 93O.070

LATITUDE: 55° 36' 00" North; LONGITUDE: 122° 12' 50" West (at centre of work)

UTM Zone: **10N** EASTING: **549540** NORTHING: **6161855** 

OWNER(S): Conuma Coal Resources Limited

MAILING ADDRESS: 200-235 Front St. (P.O. Box 2140). Tumbler Ridge, BC, V0C 2W0

OPERATOR(S) [who paid for the work]: Conuma Coal Resources Limited

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REPORT KEYWORDS (lithology, age, stratigraphy, structure, alteration, mineralisation, size and attitude). coal, Minnes Group, Bickford Formation, Bullhead Group, Cadomin Formation, Gething Formation, Gaylard Member, Bluesky Formation, Moosebar Formation, Bullmoose Member, Chamberlain Member, Cowmoose Member, anticlines, synclines, thrust faults

REFERENCES TO PREVIOUS ASSESSMENT WORK AND ASSESSMENT REPORT NUMBERS: Coal Assessment Reports 984, 986, 988, and 1001 (primary references); also 490, 526, 667, 861, 936, 937, 952, 966, and 972; Petroleum Reports 582, 746, 863, and 1161.

SUMMARY OF TYPES OF WORK IN THIS REPORT	EXTENT OF WORK (in metric units)	ON WHICH TENURES
GEOLOGICAL (scale, area)		
Ground, mapping	nil	n/a
Photo interpretation	nil	n/a
GEOPHYSICAL (line-kilometres)		
Ground (Specify types)	nil	n/a
Airborne	nil	n/a
(Specify types)		
Borehole geophysical logs in all 37 holes		
Gamma-density (logged within drill rods)	3310.09 m in 25 holes	389294
Compensated gamma-density-caliper-resistivity	4699.35 m in 37 holes	389294
Deviation	4659 m in 37 holes	389294
Gamma-neutron (logged within drill rods)	3647.20 m in 27 holes	389294
Gamma-neutron	4322.19 m in 37 holes	389294
Dipmeter	1715.17 m in 14 holes	389294
Sonic	449.51 m in 4 holes	389294
Spectral gamma-ray (KUT-log)	nil	389294
Others	nil	n/a
Core drilling	3676.59 m in 27 holes	389294
Non-core (rotary) drilling	1022.94 m in 10 holes	389294
SAMPLING AND ANALYSES		
Total number of samples	499 samples	389294
Proximate (with sulphur)	499 analyses	389294
Ultimate	nil	n/a
Apparent specific gravity	499 analyses	389294
Ash chemistry (reported as oxides)	nil	n/a
Ash fusibility	nil	n/a
Petrographic	nil	n/a
Vitrinite reflectance	nil	n/a
Light transmission (oxidation test)	414 analyses	389294
Caking (Free Swelling Index determination)	414 analyses	389294
Coking	nil	n/a
Wash tests	nil	n/a
PROSPECTING (scale/area)	nil	n/a
PREPARATORY/PHYSICAL		
Line/grid (km)	nil	n/a
Trench (number, metres)	nil	n/a
Bulk sample(s):	nil	n/a

Section 7 remains confidential under the terms of the Coal Act Regulation, and has been removed from the public version.

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# 2 Introduction

The Willow Creek coal lease, although held as one tenure, has been in recent years been explored and developed as three geographically (and to some extent tectonically) distinct blocks, although these blocks do not have independent identities as mineral tenures in their own right:

- Willow Creek Mine block, the subject of the present study, previously-reported in Coal Assessment Reports (CARs) 988 and 1001;
- Willow West block, situated along the southwestern bank of Willow Creek, and thus lying to the west of Willow Creek Mine, previously reported in CAR-984;
- <u>Willow South block</u>, situated along the northeastern bank of Willow Creek, and thus lying to the southeast of Willow West, previously reported in Coal Assessment Report 986; and

The present volume is the fifth in a series of coal assessment reports concerning portions of the Willow Creek coal lease, covered by Crown tenure 389294. Previous volumes have focussed on the Willow South and Willow West exploration activities, previous work at Willow Creek Mine itself, and archival presentation of borehole data from exploration conducted at the mine in 1997. The present report discusses results of year-2018 infill drilling, conducted to investigate coal-quality trends and geological structure (both of tectonic and sedimentological origin) within the 4N2 area of Willow Creek Mine.

### 2.1 Arrangement of this report

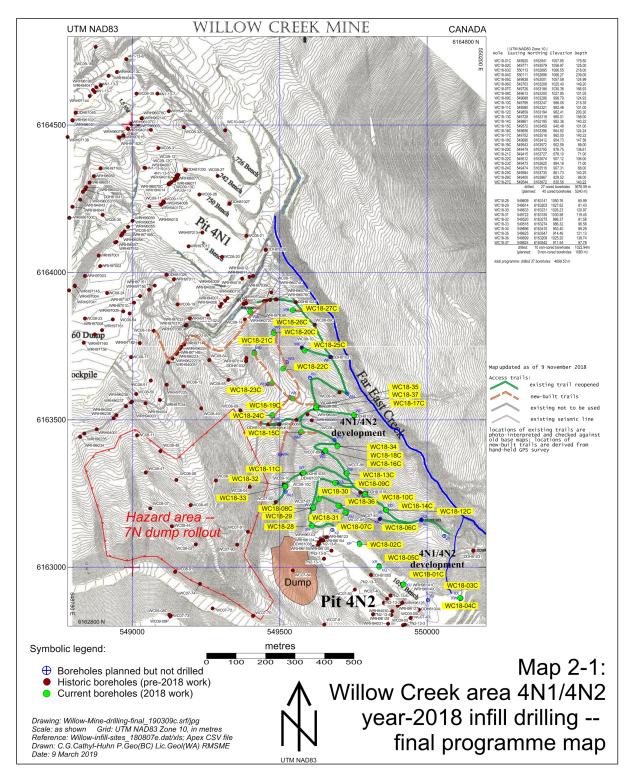
To reiterate, this report concerns the Willow Creek Mine block. The text and **Appendix A** discuss year-2018 infill diamond core-drilling, non-coring rotary-drilling, and associated downhole geophysical surveys. **Appendix B** presents initial (raw-coal) results of coal-quality sampling and consequent proximate analyses of diamond-drill cores. All of this work was done within the mine's permitted disturbance boundary, specifically within the 4N1/4N2 development area of the mine (as shown in detail within **Map 2-1**). Results of this infill work are being incorporated into a geological model and an updated mine plan, being prepared by the mine's engineering and geological staff.

#### 2.2 Distinction of historic and current work

<u>Historic work</u> comprises drilling of 726 boreholes (a majority of which were non-coring rotaryholes) and ancillary downhole geophysical surveys, as previously reported in Coal Assessment Reports 984 (Cathyl-Huhn *et al.*, 2015a), 986 (Cathyl-Huhn *et al.*, 2015b), 988 (Cathyl-Huhn *et al.*, 2015c), and 1001 (Cathyl-Huhn, 2015). Historic work was conducted between 1980 through 2013.

<u>Current work</u> (**Table 3-1**) comprises drilling of 37 boreholes (the majority of which were cored diamond-drill holes) and an ancillary programme of downhole geophysical surveys (as documented in **Appendix A** of this report). Current work was done in 2018 (during which year all of the disturbant work was done) and 2019 (with year-2019 work being analytical in scope).

The total number of boreholes now known to have been drilled at Willow Creek Mine is 763. Borehole records, which are presented in **Appendix A**, are filed in the geological archives of Willow Creek Mine. Diamond-drill core samples are stored at the mine's coreshack and laydown yard, situated within the 7N area of the mine.



**Map 2-1**: Willow Creek area 4N1/4N2 year-2018 infill drilling -- final programme map

### 2.3 Regulatory basis of report

This report has been compiled and submitted by Conuma Coal Resources Limited (Conuma), in keeping with the provisions of the *Coal Act* and the *Coal Act Regulation*, with respect of exploratory activities on Crown coal tenures within British Columbia.

This report documents infill drilling and associated geophysical and analytical work, focussed on the 4N1/4N2 development area (**Map 2-1**) of Willow Creek Mine, situated within Conuma's Willow Creek coal lease (**Maps 2-2** and **2-3**), sited in the northeastern part of British Columbia, Canada (**Map 2-4**).

## 2.4 Situation and current drilling objectives

The objective of current work was to increase Conuma's level of understanding of coal quality and geological structure within the 4N1/4N2 area of Willow Creek Mine, and furthermore to test for the potential mineability of coal zones not previously brought into the mine's resource base and reserves.

Current work has consisted of maintenance and extension of access trails and drillsite pads within the 4N1/4N2 area of Willow Creek Mine, diamond- and rotary-drilling, acquisition of borehole geophysical data, and the measurement of physical and chemical properties of coal samples through laboratory analysis, including proximate analysis, determination of total sulphur, caking (FSI) tests, and tests for oxidation by optical means.

### 2.4.1 Tenure description

The Willow Creek Mine block occupies the northeastern portion of the Willow Creek coal lease (Tenure 389294), within the Liard Mining District of northeastern British Columbia, situated within the eastern half of map-area 93O/9 of Canada's National Topographic System.

	Table 2-1. Tenare details of the Willow Oreck coal lease								
Tenure Number	Мар	Block	Units	Date Acquired	Area (hectares)	Former coal lease number			
	93O/9E	В	61, 62, 63, 64, 71, 72, 73, 74, 81, 82, 83, 84, 85, 86, 87, 88 91, 92, 93, 94, 95, 96, 97, 98						
389294 (84 units)	93O/9W	F	1, 2, 11, 12, 21, 22, 31, 32 41, 42, 51, 52, 61, 62, 63, 64 71, 72, 73, 74, 83, 84, 93, 94	March 31, 1998	6151	Coal Lease 15			
	93O/9E	G	3, 4, 5, 6, 7, 8, 9, 10, 13, 14, 15, 16, 17, 18, 19, 20, 25, 26, 27, 28, 29, 30, 35, 36, 37, 38, 39, 40, 47, 48, 49, 50, 57, 58, 59, 60						
Totals:	1 tenure		84 units		6,151 hectares				

**Table 2-1:** Tenure details of the Willow Creek coal lease

Note: Map sheets listed are within the National Topographic System. Blocks and Units refer to the British Columbia Coal Tenures Grid System, whose unit cells are based upon NAD 27 surveys, and translated into NAD 83 coordinates for purposes of mapping.

The aggregate area of the Willow Creek coal lease is 6151 hectares. Tenure 389294 was granted by the Crown on March 31, 1998 (as listed in **Table 2-1**). Annual reporting and rental-payment anniversary dates are therefore March 31. The Willow Creek Mine block is an informal operational subdivision of the coal lease, with no formal stand-alone identity within

the Crown mineral-tenure system of British Columbia. The outline of the Willow Creek Mine block is depicted upon **Map 2-2** and **Map 2-3** of the present report.

### 2.4 Coal production history

Willow Creek Mine's coals have been extensively worked by open-pit operations, commencing in year-2001 and proceeding with some interruptions to the present day.

### 2.4.1 Mine operation under Conuma ownership

In 2016, Conuma acquired the then-dormant mine in 2016. Mining operations recommenced in July 2018, and has continued to the present date. The mine is working within its 4N1/4N2 mining areas, which had previously been worked by Walter Energy. Workshops and other requisite support facilities (including administrative, environmental, and technical offices) exist at Willow Creek Mine, and are in active use. A coal-washery and railcar-loader with railway-sidings are also present.

#### 2.4.2 Production statistics

During the overall period of operation, Willow Creek Mine has produced slightly more than 6.05 million run-of-mine (ROM) tonnes of coal, at a strip ratio of 9.35 cubic metres/ROM tonne. Breakdown by year and material type is presented as **Table 2-2**.

Table 2-2: Production statistics by year and material type								
	Ва	nk cubic metre	s	Tonnes				
Year	Total mined	Waste	Coal	Total mined	Waste	Coal		
2001	186,690	160,000	26,690	452,031	416,000	36,031		
2002	215,811	180,000	35,811	516,345	468,000	48,345		
2003	0	0	0	0	0	0		
2004	1,594,963	1,412,000	182,963	3,918,200	3,671,200	247,000		
2005	5,748,955	5,219,615	529,339	14,285,608	13,571,000	714,608		
2006	4,779,093	4,328,231	450,861	11,862,062	11,253,400	608,662		
2007	0	0	0	0	0	0		
2008	1,249,000	1,212,000	37,000	3,201,150	3,151,200	49,950		
2009	0	0	0	0	0	0		
2010	6,415,816	6,078,157	337,659	16,259,048	15,803,208	455,840		
2011	6,285,249	5,594,582	690,667	15,478,314	14,545,913	932,401		
2012	16,228,129	15,245,144	982,985	40,964,404	39,637,374	1,327,030		
2013	7,942,988	7,433,970	509,018	20,015,496	19,328,322	687,174		
2014	1,727,828	1,581,502	146,326	4,309,445	4,111,905	197,540		
2015	0	0	0	0	0	0		
2016	0	0	0	0	0	0		
2017	0	0	0	0	0	0		
2018 (Jul- Dec)	n/a	5,907,000	n/a	n/a	n/a	549,000		
2019 (Jan-Feb)	n/a	2,186,000	n/a	n/a	n/a	197,000		
Totals		56,538,201				6,050,081		

Notes: data to end of 2014 compiled by Allen Baron, P.Eng. Figures for years prior to 2010 were taken from annual reports. Year-2018 and 2019 data provided by Sal Bafaro and by Lukas Klemke P.E.

### 2.5 Geological setting of Willow Creek Mine

Near-surface sedimentary rocks within and adjacent to the Willow Creek Mine block are of Lower Cretaceous age, comprising (from youngest to oldest) the basal formations of the Fort St. John Group, and the entirety of the Bullhead Group. The older and stratigraphically-lower Minnes Group is inferred to underlie the Willow Creek Mine block, but it is not mapped at outcrop at any point, and it likely has not yet been reached by coal-exploration drilling within the block, although oil and gas wells have drilled through these rocks.

The regionally-extensive coal-measures of the Gates and Boulder Creek formations have not been drilled at Willow Creek. Coal has, however been extensively drilled within the Gaylard Member (Gibson,1992a) of the Gething Formation of the Bullhead Group (**Map 2-3**).

### 2.5.1 Stratigraphic summary

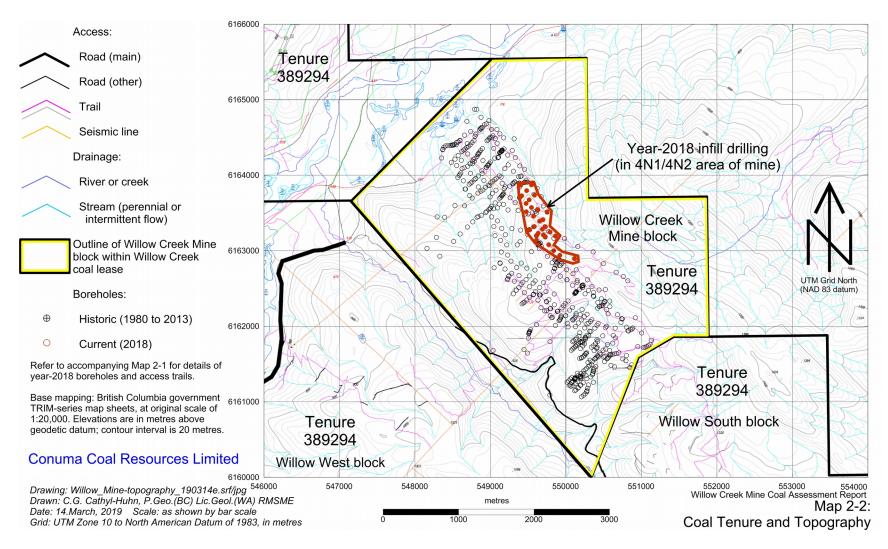
Other than the coals which have been the focus of exploratory activities within the Willow Creek Mine block, associated sedimentary rocks comprise conglomerates, sandstones, siltstones, mudstones, carbonaceous mudstones, concretionary or banded ironstone, and thin but distinctive bands of igneous tuff (Kilby, 1984a; 1985). Marine mudstones and siltstones occur within the Fort St. John Group (Wickenden and Shaw, 1943; Hughes, 1963), most notably within the Moosebar and Hulcross formations. Furthermore, the local occurrence of bioturbated mudstones and siltstones in the basal half of the Gething Formation's Gaylard Member hints at the presence of marine conditions, there too, during deposition. The facies of the remainder of the Gaylard Member, of the overlying Gates and Boulder Creek coalmeasures, and also of the underlying Cadomin and Bickford formations, are otherwise alluvial, fluvial, or deltaic.

# 2.5.2 Structural summary

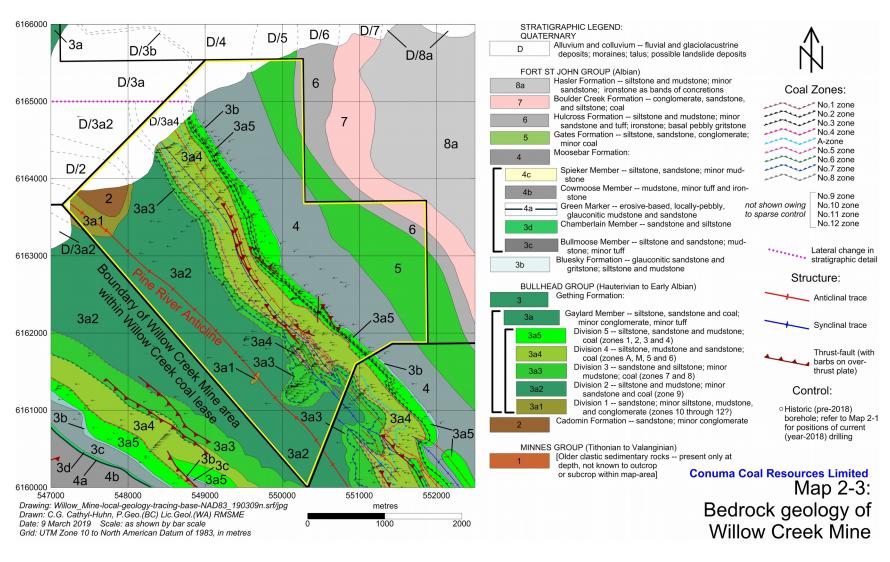
Bedrock within the Willow Creek Mine block is moderately- to complexly-deformed, possibly more-so than is the case in the adjoining Willow West and Willow South blocks (James, 1998; Jordan and Acott, 2005; Cathyl-Huhn *et al.*, 2015a; 2015b). Southwest-verging thrust-faults, some of which may be folded, and associated northwest-striking, southwest-verging folds predominate at Willow Creek Mine, consistent with a structural setting within a passive-roof duplex system. Folding of the near-surface thrust-faults, and refolding of some of the folds, are very likely the result of tectonic ramping of younger, underlying, northeast-verging thrust-faults, as suggested by oilfield seismic surveys. The opposing vergences of the shallow and deep structures is consistent with the triangle-zone structure which is well-established to be present within the Pine Pass area (McMechan, 1985; Lingrey, 1996).

### 2.5.3 Nomenclature and context of coal zones

Within the Gaylard coal-measures, numerous coal zones have been found by historic and current drilling at Willow Creek Mine. Coal zones are numbered in downward succession from the No.1 (near the top of the coal-measures) through No.12, following a long-established schema (McKechnie, 1955). As well, a coal zone at the immediate top of the coal-measures has been given the local name of Bird Seam, although this coal is by no means correlative with the Bird Seam as previously-recognised (Wallis and Jordan, 1974) in other coal properties of northeastern British Columbia.



Map 2-2: Coal Tenure and Topography



Map 2-3: Bedrock geology of Willow Creek Mine block

Most of the coal zones contain one or more major coal beds, often associated with laterally-branching splits, stringers and stringer plies (as summarised in **Table 5-1**). Individual coal beds and sub-beds range in thickness from a few decimetres to several metres.

At Willow Creek Mine, the Gaylard coal-measures may be conveniently subdivided into five informal divisions, numbered in upward succession from Division 1 at the base of the Gaylard, to Division 5 at the top of the Gaylard. Drilling has established that the thickest, and possibly more laterally-extensive, coals occur within Divisions 3, 4, and 5 of the Gaylard Member, at Willow Creek Mine.

### 2.5.4 Proposed regional coal correlations

Regional correlations of Gaylard coals are suggested as follows:

- The 'Bird' zone at Willow Creek Mine may be correlative with the Lower Gething A
  zone at Sukunka Colliery. It is definitely <u>not</u> correlative with the type Bird Seam at
  Sukunka, East Bullmoose, and Perry Creek.
- No.4 zone at Willow Creek Mine may be correlative with the Brenda in the Hudette area, F zone at Mink Creek, Conuma A coal zone (formerly known as Seam C60) at Brule Mine, and the B zone at Sukunka;
- No.6 zone at Willow Creek Mine may be correlative with the Conuma B coal zone (formerly known as the Upper Seam) at Brule Mine; and
- No.7 zone at Willow Creek Mine may be correlative with the Conuma C coal zone (formerly known as the Lower Seam) at Brule Mine.

#### 2.6 Location and access

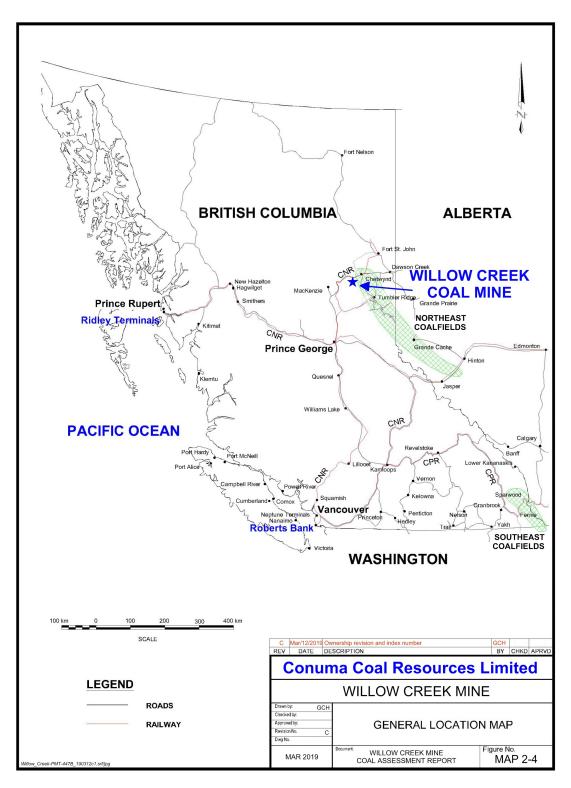
Chetwynd town, located on Highway 97 and situated approximately 50 kilometres northeast of Willow Creek Mine, is the closest incorporated settlement to Willow Creek Mine (**Map 2-4**). Chetwynd's population was reported as 2,633 persons in the year-2006 census. In the context of more-distant communities within British Columbia, the Willow Creek Mine coal property is located 130 kilometres south of Fort St John, 95 kilometres west of Dawson Creek, and 315 kilometres northeast of Prince George. Vancouver is situated 730 kilometres to the south-southwest of the property. Commercially-scheduled aircraft flights connect Vancouver to Fort St. John and Dawson Creek. A municipal airstrip is maintained at Chetwynd for non-scheduled use, chiefly by chartered helicopters.

### 2.6.1 Coal-loading facility and railway connections

A coal-loading facility is situated on the southern bank of the Pine River, 2 kilometres to the northwest of Willow Creek Mine. This loadout site, which fills railway cars with coal produced from Brule Mine and from the Willow Creek coal washery, allows rail access to ports along the Pacific Coast of Canada, and elsewhere within the North American railway network. CN Rail are the operator of the former BC Rail line to which the loadout site is connected.

#### 2.7 Climate

The nearest climate station to Willow Creek Mine is at Chetwynd, with 'cool continental' climate of frigid winters and warm summers. Average annual rainfall and snowfall at Chetwynd are 306



Map 2-4: General location map

millimetres and 169 centimetres respectively. The average frost free period ranges between 84 to 91 days, and about 30 foggy days are expected per year. The mean daily temperature at Chetwynd is 15.4 C in July and -10.7 C in January. Winter temperatures below -40C are not uncommon, with the coldest weather occurring in January and February of most years.

#### 2.8 Landforms and forest cover

The Willow Creek Mine block lies within the Inner Foothills of the Rocky Mountains. Topography comprises deeply-dissected, steep-sided, rounded hills and mountains, with elevations ranging from 635 to 1345 metres above sea level. Topographic contours at 20-metre intervals, based upon provincial government mapping (TRIM map-sheets 93O.059 and 93O.069), are shown in **Map 2-2**.

The Willow Creek Mine block is heavily forested, chiefly with lodgepole pine, trembling aspen, balsam poplar, white and black spruce, and tamarack. The property lies within Tree Farm Licence 48, part of the Dawson Creek Timber Supply Area. Some cut-blocks have been operated for timber harvesting within the Willow Creek Mine block. As well, areas of forest cover (including a substantial portion of the mine's 4N1/4N2 development area) have been cleared in preparation for mine development. As a result, forest cover exhibits a range of ages and states of maturity.

### 2.8.1 Biogeoclimatic ecosystem classification

Willow Creek Mine lies within the Sub-Boreal Interior ecoprovince, within which are three biogeoclimatic ecosystem classification variants:

- Boreal White and Black Spruce moist warm Peace variant (BWBSmw1),
- Sub-boreal Spruce wet cool Finlay-Peace variant (SBSwk2), and
- Englemann Spruce Subalpine Fir moist very cold Bullmoose variant (ESSFmv2).

### 2.9 Acknowledgements and statement of professional responsibility

Thanks are due to many past and present workers:

- Allen Baron, P.Eng., senior mining engineer at Willow Creek Mine;
- Jerry Holmes, P.Geo., Apex Geoscience's drilling project manager;
- Dr. Peter Jones, at International Tectonic Consultants, who has continued to offer thoughtprovoking insights into the structural geology of the Mink-Brazion coalfield, including the Pine River Anticlinorium and the associated triangle-zone structure;
- Vesko Karadzic, P.Geo., mine geologist at Willow Creek Mine, who is reconstructing the structural and quality models of the mine, as well as maintaining the mine's geological archives; and
- John Stokmans, Laura LeMay, and Katherine Evans, former mine geologists at Walter Energy, for stimulating discussions of the geological structure and mining conditions at Willow Creek.

The author accepts professional responsibility for data and conclusions presented within this report.

# 3 Exploration

Both historic (pre-2018) and current (year-2018) coal exploration has been done by various parties within the Willow Creek Mine segment of the Willow Creek coal lease. The majority of the work is of historic vintage. In all, 763 historic and current boreholes (**Table 3-1**) are known to have been drilled between the years 1980 and 2018. Earlier (1946 to 1951) diamond-drilling is known to have occurred (as reported by McKechnie, 1955), but has not yet been accurately-located within the Willow Creek Mine block.

### 3.1 History of coalfield development

The following discussion is adapted in part from an unpublished report (Ryan, 2010) on behalf of Unicorn International Mines Group Inc.

Coal was first discovered in the Peace River District in 1793, by Alexander MacKenzie's exploring expedition (MacKenzie, 1801). Prior to 1980, less than 100,000 tonnes of coal were mined at all locations within northeastern British Columbia (Ryan, 2002).

At a location on Hasler Creek, situated about 17 kilometres southeast of Willow Creek Mine, the Hasler Creek Coal Company commenced small-scale underground coal-mining in 1943, continuing through 1944 and 1945. At this time, considerable geological mapping and some prospecting were undertaken within the Pine River Anticlinorium, including the Willow Creek Mine area (Wickenden and Shaw, 1943, Spivak, 1944; reviewed by Stott, 1973).

From 1946 onward to 1951, British Columbia's former Department of Mines conducted a diamond-drilling and trenching programme of the then-known coal deposits near the Pine River valley (McKechnie, 1955). This programme entailed extensive drilling within the Willow Creek Mine block, but logs of these boreholes have not yet been located, although they might eventually be found within the working files of the British Columbia Geological Survey Branch, or within the British Columbia Archives.

From the late 1950s onward, several oil companies undertook structural and stratigraphic mapping within and adjacent to Willow Creek Mine, and within the Mink-Brazion coalfield generally.

- In the summer and autumn of 1956, Photographic Survey Corporation Limited compiled a aerial-photographic interpretation of the geological structure of the area (Pekar and Scott, 1956), on behalf of West Canadian Petroleums and Trans Empire Oils Ltd.
- In the summer of 1957, Trans Empire Oils Ltd. conducted a follow-up fieldwork programme, as reported by Bossort (1957).
- Two reports prepared on behalf of Triad Oil by Dr. Peter Jones (1960; 1963) are the most useful of those reports which are publicly-available, as they incorporate detailed structural and stratigraphic mapping.

Governmental and academic surveys were carried on concurrently. In 1963, Dr. John Hughes compiled a dissertation for McGill University, concerning structural geology and tectonics of the Pine River valley, including the Willow Creek Mine area (Hughes, 1963). Dr. Hughes' work was sponsored by the then-extent British Columbia Department of Mines, leading to the publication of two provincial Geological Survey Bulletins (Hughes, 1964; 1967).

The expansion of steel production in mid-1960s stimulated exploration for metallurgical coking coal. By the mid-1970s within northeastern British Columbia, most of the land with coal potential had been acquired by mining companies, or by oil and gas companies seeking to enter the coal industry as a means of diversification. Initial development interest was along the existing railway (then known as the British Columbia Railway) which passed through Pine Pass and thus connected Chetwynd and Dawson Creek with then-existing ports along British Columbia's western coast.

Interest in coal development increased with rapid increase in crude oil prices, and concomitant increase in coal prices. These price increases were followed in short order by the signing of a joint government-industry agreement between Japan and Canada, to develop new coal mines, highways, railways, other infrastructure, and a workers' townsite at Tumbler Ridge. Shipments of northeastern British Columbia coal through a new port at Ridley Island (near Prince Rupert, British Columbia) commenced in 1984, and have continued to the present day, albeit at currently-reduced levels owing to the present depression in global coal prices.

The Geological Survey of Canada published a regional-scale structural synthesis (McMechan, 1984), consisting of a map and cross-section at a scale of 1:250,000, followed by a journal article concerning the geometry of thrust-faults (McMechan, 1985).

# 3.2 Historic (years-1980 through 2013) exploration

The bulk of historic exploratory work at Willow Creek Mine has been by means of drilling, although considerable trenching and test-pitting was also done, especially within coal outcrops exposed during the construction of access trails and drill pads. A continuous miner (an underground coal-cutting and loading machine) was transported to the property from the Sukunka Mines in the early 1980s, but it remains unclear whether it was ever put into use to drive adits into the property although such work was planned (A.S. Marton, personal communication, 1981).

Historic work has been documented within coal-assessment reports and unpublished technical reports prepared by third parties (Marton, 1981; Marton and Jones, 1981; Anonymous, 1997; James; 1998; Jordan and Acott, 2005) and by Walter Energy (Cathyl-Huhn, 2015b; Cathyl-Huhn *et al.*, 2015c). By the late 1990s, the structure and general characteristics of the Willow Creek coals were sufficiently well-understood, to appreciate that the coal-measures were complexly-folded and faulted, and that principal structures had a southwestern vergence (in contrast to the usual northeastern structural vergence of the Peace River coalfields).

Locations of historic boreholes are generally well-established by means of surveying, initially established in terms of local (minesite) coordinate systems (*vide* Section 3.2.2, and Table 3-2, below), but subsequently translated into Universal Transverse Mercator (UTM) coordinates referred to the older NAD27 (North American Datum of 1927) or the modern NAD83 (North American Datum of 1983) metrologies.

A conspicuous exception concerns the positions of numerous year-1997 boreholes from which cores were aggregated to form drilled bulk-samples for coking tests (Anonymous, 1997); these boreholes' positions are only known in general terms, from graphic symbols presented on a drilling plan. The reason for the lack of surveyed coordinate data for these holes is unknown.

The substantial majority (**Table 3-1**, below) of historic boreholes were drilled by means of non-coring rotary methods. Rotary-holes were generally shallower than diamond-cored

boreholes. Drilling of the property in 1980-81 was entirely by means of coring, in keeping with the need to establish stratigraphy and structural style through the examination of cores (A.S. Marton, personal communication, 1980).

The numerous boreholes drilled in years-1980 through 1996 are documented in maps and data tables within coal-assessment reports (Marton, 1981; Marton and Jones, 1981; James, 1998). More recent historic work, by Western Coal and by Walter Energy, has also been documented within more recent coal-assessment reports (*vide* Cathyl-Huhn, 2015b; Cathyl-Huhn *et al.*, 2015c).

Table 3-1: Statistical summary of historic and current drilling

Year in	Core	drilling	Rotary	drilling	All bor	All boreholes	
which drilled	Total holes	Total metres	Total holes	Total metres	Total holes	Total metres	
historic drilli	ng						
1980	3	854.70	0	nil	3	854.70	
1981	43	11,240.30	0	nil	43	11,240.30	
1994	3	107.91	54	2,694.29	57	2,802.20	
1996	55	2,041.76	145	4,781.04	200	6,822.80	
1997	73	2,052.30	67	3,119.88	140	5,172.18	
1999	16	299.95	24	627.83	40	927.78	
2001	5	708.80	15	576.20	20	1,285.00	
2005	0	nil	28	1,975.40	28	1,975.40	
2007	3	201.16	74	8,079.65	77	8,280.81	
2008	3	475.30	50	5,887.68	53	6,362.98	
2009	13	380.00	25	1,983.15	38	2,363.15	
2010	5	493.05	1	13.00	6	506.05	
2011	0		7	1,024.35	6	1,024.35	
2013	14	1,083.83	0		14	1,083.83	
totals	236 core	19,939.06	490 rotary	30,762.47	726 overall	50,701.53	
current drilli	ng						
2018	27	3,676.59	10	1,022.94	37	4,699.53	
totals	27 core	3,676.59	10 rotary	1,022.94	37 overall	4,699.53	
all years	263 core	23,616.65	500 rotary	31,785.41	763 overall	55,401.06	

### 3.2.1 Cross-reference to historic borehole positions and depths

Positions and depths of historic (pre-2018) boreholes are presented in Tables 3-2 and 3-3 of the year-2015 coal assessment report for Willow Creek Mine (Cathyl-Huhn *et al.*, 2015c).

### 3.2.2 Coordinate transformation from minesite grid to UTM (NAD83 Zone 10)

Prior to 2008, most exploration activities were surveyed in terms of a local mine grid, for convenience in locating boreholes along cross-section lines. Although the mine grid is no longer in active use, mathematical transformations are required to bring earlier work into present-day terms of the UTM grid system used in governmental base-mapping. The following notes summarise the transformation algorithm.

# Table 3.2: Coordinate transformation notes

Minesite grid

**UTM** grid

Transformed east 534954.317 Transformed north 6146860.561

Rotation -46° 55' 52.918088"

Scale factor 0.99946605 Elevation adjustment -2.623 metres



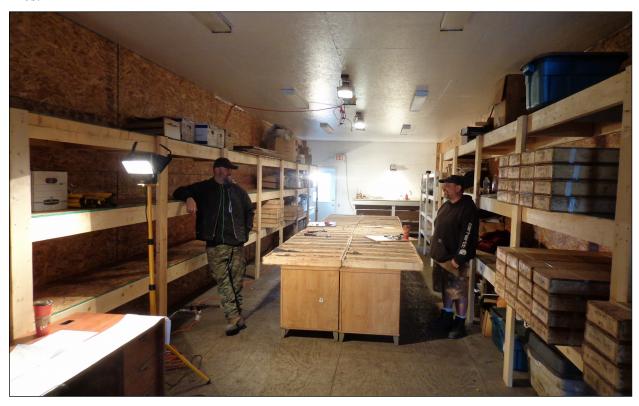
**Plate 1:** Geotech Drilling Services diamond-drill at site on then-inactive floor of 4N2 open-pit. Orange bladder contains water supply for drilling. Metal structure at extreme right is skid-mounted mud-tank. Southeastern highwall of 4N2 pit is in distance. [*RC4927/18.jpg*]

# 3.3 Current (year-2018) in-mine drilling

Conuma conducted drilling programmes within the Willow Creek Mine block in the summer and autumn of 2018. Drilling contractors were Geotech Drilling Services (two skid-mounted A5 diamond-drill rigs) and RC Drilling Ltd. (one track-mounted air-rotary drilling rig).

In all, 37 boreholes were drilled, with overall depth of 4,699.35 metres. Of these boreholes, 27 were cored and 10 were rotary-drilled.

**Table 3-3** (below) and **Table A-1** (within **Appendix A**) presents the positional details and depths of the year-2018 boreholes. Lithological interpretation, including correlated intersections of coal and associated rock partings, are presented as **Table A-2**, within **Appendix A**. This table is followed (in the printed form of this report) by core descriptions pertaining to the 27 cored boreholes drilled in 2018. The core logs are also presented in digital form, as PDF-format scan-files.



**Plate 2**: Interior view of core shack at 7S laydown area of Willow Creek Mine. Building was previously used as a mine dry and subsequently as a storage facility. Core boxes are Northeast Coal standard length of 2.5 feet (ca. 75 cm), holding HQ diamond-drill core. Lighting was provided by a rented generator situated outside the building. [RC4948/18.jpg]

The purpose of the current drilling was to refine and extend the understanding of the structure and extent of surface-mineable coal in Willow Creek Mine's 4N1/4N2 area, and to better define the quality variations of major coal beds. Initial coal-quality results are presented as **Table B-1** in **Appendix B**. Current drilling mainly examined the coals of zones No. 1 through No.4 and A, within the upper and middle portions of the Gaylard Member. Less attention was paid to the No.5 coal zone. The majority of the boreholes, as noted above, were advanced by means of diamond-drills, allowing the recovery of coal and rock cores. A modest amount of follow-up rotary-drilling was undertaken; cores were not taken in these holes.

Access to drill sites was via a combination of existing and new trails, including reactivated logging trails where they were conveniently located with regard to the desired drilling locations. Efforts were made to maximise re-use of existing trails, in the interests of minimising construction of new trails. Some drill-pads were built directly open the existing (but then-inactive) floor of the 4N2 pit of Willow Creek Mine.



**Plate 3**: Geophysical logging engineer prepares to run gamma-density tool down borehole WC18-03C. Talus in background is derived from weathered highwall of 4N2 pit, excavated in silty mudstone of the Bullmoose Member of the Moosebar Formation [*RC4951/18.jpg*].

### 3.3.1 Borehole geophysics

Downhole geophysical logging of all of the current boreholes was done by Century Wireline Services (based out of Red Deer, Alberta, but operating from a hotel in Chetwynd), using a truck-mounted logging unit with draw-works and generator-derived power supply. A standard coal-industry suite of logs was run:

- Gamma/caliper/resistivity/compensated density (9239C tool);
- Gamma/density through drill rods (9068 tool, run in anticipation of hole instability);
- Gamma/neutron (9067 and 9058A tools);
- Deviation/verticality (9058A tool); and in certain boreholes,
- Dipmeter (9411A tool); and
- Sonic (9325A tool).

General-scale logs were plotted at 1:100 vertical scale, with selected detail logs at 1:50 vertical scale. Digital copies of downhole geophysical logs are presented in **Appendix A**, with an inventory of logs given as **Table A-1**. The digital logs are presented in LAS (Log ASCII Standard, as promulgated by the Canadian Well Logging Society) format, in TIF (Tagged Image File) format, and as PDF (Portable Document Format) files. LAS files can readily be imported into, and manipulated by, geophysical-processing software such as *LAS Viewer* or *WellCAD*, whereas TIF files may be opened by the native *Microsoft Windows* image-viewer, or by image-processing programmes such as *Photoshop*. PDF files are suitable for printing via plotter, or as sectionalised images via a capable printer.

## 3.4 Comments on validity of exploratory work

Historic and current drilling at Willow Creek Mine, comprising 55,401.06 metres' total length (**Table 3-1**) is regarded as having validly tested the coal potential of the coal-measures of the Gaylard Member of the Gething Formation, such that a revised structural and quality models can be compiled, and that tonnage estimates of the coal resource (of coal-in-place) can be undertaken with reasonable confidence. Coal-resource and coal-reserve estimation are discussed in greater detail within **Section 7** of the present report.

Stratigraphic variations in coal quality (notably, in the characteristic caking propensities of the various coal beds) between coal zones are reasonably-well established by existing drilling and analytical work. However, understanding of spatial variations of coal quality within individual coal beds, or closely-associated coal beds within a given coal zone, is hampered by the missing positional data of numerous historic boreholes, which would otherwise be useful in refining the spatial variations of coal quality. In contrast, positional data is available for all 37 of the current (year-2018) boreholes.

**Table 3-3**: Details of current boreholes

Borehole	Surve	ed borehole posit			th (metres)	Borehole		
('C' indicates	(metres:	UTM NAD83 Zor	ne 10)	-		ation (degrees)		
cored hole)	Easting	Northing	Elevation	Cored (HQ size)	Non-cored (114.3 mm)	Azimuth	Dip	
WC18-01C	549919.717	6162941.125	1057.853	179.50		46.51	69.1	
WC18-02C	549770.728	6163078.855	1056.971	125.00		230.43	69.8	
WC18-03C	550113.152	6162894.828	1066.552	218.00		243.94	70.0	
WC18-04C	550111.305	6162896.186	1066.265	239.00		53.88	69.8	
WC18-05C	549837.504	6163001.175	1057.579	124.99		228.91	69.9	
WC18-06C	549703.347	6163208.038	1025.403	149.20		249.27	69.2	
WC18-07C	549726.288	6163185.982	1030.381	166.93		238.40	67.3	
WC18-08C	549613.477	6163200.911	1027.849	101.05		227.96	69.7	
WC18-09C	549687.550	6163285.864	998.789	124.93		242.24	69.8	
WC18-10C	549789.164	6163247.370	986.076	215.35		226.56	71.3	
WC18-11C	549580.191	6163320.688	992.477	101.00		228.83	70.3	
WC18-12C	549859.289	6163193.974	982.413	200.30		47.31	69.5	
WC18-13C	549727.625	6163318.047	980.012	158.00		47.77	70.2	
WC18-14C	549861.101	6163194.631	982.358	140.22		231.90	69.0	
WC18-15C	549571.514	6163458.394	940.478	101.00		225.37	68.9	
WC18-16C	549655.649	6163395.747	964.918	124.24		230.42	68.4	
WC18-17C	549752.080	6163516.076	891.998	140.22		236.95	68.6	
WC18-18C	549696.047	6163411.618	954.725	147.58		49.76	72.3	
WC18-19C	549543.156	6163572.340	902.591	89.00		222.17	71.5	
WC18-20C	549478.986	6163795.215	876.747	136.61		233.10	68.5	
WC18-21C	549414.521	6163726.503	876.097	71.00		223.80	69.3	
WC18-22C	549512.394	6163673.934	907.123	106.00		233.07	69.5	
WC18-23C	549472.881	6163624.654	894.18	71.00		221.07	72.6	
WC18-24C	549474.112	6163516.344	907.308	68.00		229.47	69.1	
WC18-25C	549584.109	6163735.278	861.732	140.25		228.77	68.5	
WC18-26C	549400.485	6163867.209	829.519	98.00		226.54	70.9	
WC18-27C	549544.060	6163871.966	830.558	140.22		227.48	69.2	
WC18-28	549608.840	6163141.020	1050.764		65.99	156.46	86.3	
WC18-29	549613.570	6163203.004	1027.623		81.43	206.04	87.4	
WC18-30	549632.612	6163231.418	1026.229		120.97	217.24	59.7	
WC18-31	549722.241	6163184.832	1030.577		119.45	216.97	60.8	
WC18-32	549519.825	6163274.772	986.371		81.58	230.21	87.9	
WC18-33	549518.468	6163274.156	986.323		96.58	229.82	58.5	
WC18-34	549696.213	6163410.049	953.399		99.29	220.11	59.4	
WC18-35	549624.894	6163546.955	914.489		121.13	217.99	87.2	
WC18-36	549699.301	6163208.768	1025.2		138.74	200.80	58.6	
WC18-37	549623.775	6163541.670	911.541		97.78	214.96	68.7	
37 holes 4699.53 m				27 holes 3676.59 m	10 holes 1022.94 m			

Note: borehole orientation from geophysical deviation survey; azimuth is over entire surveyed extent of hole, relative to astronomic north (at assumed declination of 17.5 degrees east). Dip is complement of uppermost slope-angle reading, and is here assumed to approximate the dip of borehole casing.

# 4 Review of coalfield geology

This chapter of the report is adapted from the discussion presented in Coal Assessment Report No. 988 (Cathyl-Huhn *et al.*, 2015c), in light of recent drilling results. Discussion proceeds from regional setting to local scale.

The coalfields of northeastern British Columbia are hosted by marine and non-marine clastic sediments of Jurassic, Cretaceous and earliest Tertiary age. These rocks form a series of thick sequences of molasse and flysch, all of which was deposited into the Rocky Mountain Foreland Basin of Western Canada. The basin is bounded by the mobile crustal terranes of the Cordilleran Orogen to the west, and the cratonic rocks and Palaeozoic cover sequences of the Canadian Shield to the east.

### 4.1 Regional structural setting

Most of the Jura-Cretaceous sediments were derived from orogenically-uplifted landmasses lying to the southwest of the basin, although patterns of sedimentation were to some extent influenced by occasional vertical movements of underlying structures within the cratonic basement rocks, chief amongst which was the Peace River Arch (Stott, 1968).

During Late Mesozoic and Early Cenozoic time, the Cordilleran Orogen underwent two main phases of deformation: the Late Jurassic to earliest Late Cretaceous Columbian Orogeny, and the Late Cretaceous to Oligocene Laramide Orogeny (Douglas *et al*, 1970). Both of these orogenies were driven by transpressional crustal movements along the outboard (western) edge of the North American continent. In each case, orogenic activity was driven by the collision of northward-moving exotic crustal terranes, which in turn caused compressive strains within the previously-accreted western margin of the continent. Northeast-directed overthrusting of Palaeozoic rocks caused episodic uplift of the Cordilleran Orogen, in turn providing a ready source of sediment into the Foreland Basin (Cant and Stockmal, 1989; Cant, 1996; Cant and Abrahamson, 1996).

The present-day Rocky Mountains are the most visible manifestation of Columbian and Laramide overthrusting, which gradually proceeded northeastward, with successively-younger thrusts tending to break through the Foreland's rocks at successively-deeper stratigraphic levels. As successively-younger thrusts developed, they generated passive folding within overlying, previously-deformed rocks. Overlying, older thrusts were therefore passively folded along with their adjoining strata. Recognition of folded thrusts is essential to understanding the structural geology of the Foothills coal deposits of northeastern British Columbia.

From southwest to northeast, the Cordilleran fold-thrust belt gradually changes structural styles (Thompson, 1979) from a thrust-dominant regime(within the mostly-Palaeozoic carbonate-clastic rocks of the Rocky Mountain Main Ranges and Front Ranges) to a mixed fold-thrust regime (within the Inner Foothills, including the Willow Creek Mine property) to a gently-folded frontal regime (within the Outer Foothills, five to ten kilometres to the northeast of Willow Creek Mine).

### 4.2 Regional stratigraphic setting

Stratigraphic nomenclature within the coalfields of northeastern British Columbia has undergone considerable revision during the past fifty years. Principal workers, whose reports were used as

primary references for the present report, are J.E. Hughes (1964, 1967), D. Stott (1968, 1973, 1981, 1998), P.McL.D. Duff and R.D. Gilchrist (1981), and D.W. Gibson (1992).

The stratigraphic sequence within the northwestern part of the Mink-Brazion coalfield (including Willow Creek Mine) comprises Lower Cretaceous rocks of the Fort St. John and Bullhead groups, and older Jurassic to Lower Cretaceous rocks of the Minnes Group (**Table 4-1**). Fort St. John Group rocks are present only along the northeastern fringe of the Willow Creek Mine block, owing to substantial erosion. Minnes Group rocks are present only in the subsurface at Willow Creek Mine, inasmuch as the Bullhead Group rocks are nowhere completely strippedaway by erosion (**Map 2-3**). Almost all of the block is covered with coal-measures of the Gaylard Member of the Gething Formation, which forms the upper part of the Bullhead Group, or by the marine rocks of the overlying Bluesky and Moosebar formations, which form the basal part of the Fort St. John Group.

### 4.2.1 The Gething-Bluesky controversy and its resolution

Considerable stratigraphic controversy (as expressed in works of Hughes and Stott, studied further by Oppelt (1988), and to some extent resolved by Gibson's 1992a report) has revolved around the stratonymy and chronological topology of rocks underlying and overlying the coal-measures of the Gething Formation. In this report, the Gething Formation, as well as immediate sub-Gething rocks, are assigned to the Bullhead Group, following Stott's extensive regional work. Hughes' previous stratonymy, comprising the Crassier and Beaudette groups, is now formally deprecated, although it is still being used by some industrial geologists.

At the latitude of the Willow Creek Mine block, and within the Pine Pass area in general, only the Gaylard Member of the Gething Formation is known to contain coal of potentially-mineable thickness, although within the nearby Burnt River property (McClymont, 1981; Cathyl-Huhn and Avery, 2014b), the Chamberlain Member (there the uppermost subdivision of the Gething Formation) also appears to be coal-bearing (although not thus far examined beyond initial prospecting during the property's early years of exploration).

Owing to the general southwestward back-stepping of the Gething paleodelta complex, at Willow Creek Mine the Bluesky is in the present report recognised as a formation in its own right (homotaxial with the more-extensive Bluesky sediments within the Deep Basin of the Alberta Syncline), and the Bullmoose and Chamberlain members (elsewhere assigned to the Gething Formation) are both considered to be members of the Moosebar Formation, as neither the Bullmoose rocks nor the Chamberlain rocks manifest any non-marine indicators. Supra-Gething rocks (from the Bluesky Formation upwards) are assigned to the Fort St. John Group, following Stott's work.

### 4.3 Local structural geology

Structural geology of the Willow Creek Mine area would be difficult to decipher on the sole basis of bedding attitudes within exposed bedrock, owing to the isolated nature of the outcrops, other than those formed by temporary or longer-lived open-pit walls. Much of our understanding of local structural geology comes from borehole intersections of faulted coal-measures, supplemented by isolated exposures of bedrock alongside roads and trails. An additional source of structural information, albeit indirect, is from the interpretation of landforms as visible in aerial photographs and on detailed topographic maps, although this indirect observation is locally hampered by Drift cover.

Map 2-3 depicts, in general terms, our understanding of bedrock structure at property scale. Willow Creek Mine comprises a series of moderately-tight southwest-verging folds, overlain and bounded to the northeast by a northeast-dipping monoclinal panel of coal-measures and cover rocks, dislocated by southwest-verging thrust-faults. The Willow Creek Mine block occupies the leading (northeastern) limb and central duplex zone of the Pine River Anticlinorium, which in turn lies within a regional-scale triangle zone (McMechan, 1984; 1985; Lingrey, 1996). Willow Creek Mine's coal-measures appear to occupy a shallower structural position within the triangle-zone than those of the Willow South or Willow West blocks.

Within the 4N1/4N2 development area (the site of year-2018 drilling), the upper portion of the Gaylard coal-measures appears to form a consistent northeast-dipping homoclinal panel of strata, broken by metre- to dekametre-scale southwest-verging thrust-faults. Faulting is visible as contorted and shattered zones within cores, as well as borehole-wall breakouts visible on geophysical caliper logs. Faults, as interpreted from downhole duplication of geophysical-log response patterns, have been subdivided into three levels-of-assurance:

- <u>Fault</u>, <u>established</u> -- where there is a demonstrable repeat of log-response interpreted to be associated with a consistently-developed coal bed
- <u>Fault, probable</u> -- where there appears to be a repeat of a minor coal, or of a characteristic sequence of non-coal strata
- <u>Fault, possible</u> -- where there appears to be a local thickening or duplication of stratal pattern, generally-associated with borehole breakout(s), but the interpretation is not robust-enough to justify classification as 'probable'.

This tripartite structural classification follows practice developed by geologists of BP Coal, working in the late 1970s and early 1980s on their then-operated Sukunka coal property.

Furthermore, bedding-plane shearing is pervasive within incompetent strata such as dirty coals or coaly mudstones, and some of this shearing might be associated with bedding-plane faulting. However, this possibility might be difficult to validate prior to downward and lateral extension of the 4N2 open-pit workings into the 4N1/4N2 area.

### 4.3.1 Tectonostratigraphic coherence

Normal stratigraphic sequences are generally preserved at Willow Creek Mine, despite the thrust-faulting of the rocks and concomitant folding and tectonic stacking. Overturned strata appear to be rare, although this determination is clouded by the angled geometry of most exploratory boreholes.

## 4.4 Local stratigraphy

Based largely upon the interpretation of downhole geophysical logs of coal-exploration boreholes and natural-gas wells, the local stratigraphic sequence (as shown in **Table 4-1**) has been identified within and adjacent to the Willow Creek Mine block.

Relationships between the various rock-units that occur within and adjacent to the Willow Creek Mine block are shown on the geological map (Map 2-3) accompanying this report. Map 2-3 incorporates results of current drilling, together with historic drilling and geological mapping

done by others, as cross-referenced in **Section 10** of this report. Geological contacts shown on the map are approximate to inferred, owing to the generally-discontinuous nature of bedrock exposures, and paucity of documented stratigraphic and structural fieldwork.

Table 4-1: Table of formations and subdivisions

Group/Formation/Member			_	ар-	Lithology and thickness				
Quaternary Drift				)	Alluvium; lodgement till; moraines; talus; glaciolacus 150 m thick within Pine Valley.			•	
John Group	Hasler Fm.		8a		concretions; at least 180 m to	Siltstone and mudstone; minor sandstone; ironstone as bands of concretions; at least 180 m thick			
hn G	Boulder Creek Fm.			7	Sandstone and siltstone; cor glomerate; coal; 75 to 95 m		within Willow	oal not yet proven Creek Mine block	
); Jc Jc	Hul	cross Fm.	(	6	Siltstone and mudstone; min gritstone; erosional base; 12	0 to 13	0 m thick		
Fort St.	Gá	ates Fm.	5		Siltstone, sandstone and con-		oal not yet proven Creek Mine block		
		Spieker Mb.		4c	Siltstone, sandstone; minor mudstone; 60 to 90 m thick				
	Moosebar Fm. 165 to 280 m thick	Cowmoose Mb.		4b	Mudstone; minor tuff and ironstone; erosive-based bas glauconitic grit; 80 to 100 m		thickened due induced telesc	ally structurally- e to internal thrust- coping, or repeated	
		Green Marker	4	4a	Locally-glauconitic siltstone a sandstone; nil to ca. 3 m thic			nrusting. Possible zones at base of	
		Chamberlain Mb.		3d	Sandstone and siltstone; 3 to thick	o 6 m		se Member and ose Member.	
		Bullmoose Mb.		3с	Siltstone and sandstone; muds minor tuff; 100 to 120 m thick				
	Blu	esky Fm.	3	b	Glauconitic sandstone and gritstone; siltstone and mudstone				
Bullhead Group					Numerous fining-upward and coal		Siltstone, sand and coal (zone through 4); mir		
head		Gaylard Mb.			siltstone, mudstone and coal (zones 'Bird' and 1		Siltstone and mudstone; coal (zones A, 5 and 6)		
Ball	Gething Fm.		3	a	through 12); minor tuff; local concentration of	3a3		inor siltstone and al (zones 7 and 8)	
					sandstone beds; 260 to 3a2 360? metres thick			nudstone; minor	
						3a1	Basal sandy us siltstone; mino 12 correlatio	nit: sandstone and r coal (zones 10 to ns tentative)	
	Cadomin Fm.	Gritty to pebbly, siliceous sandstone and sandy conglomerate distinctive 'blocky' gamma-log response; minor siltstone and c to 14? m thick; erosional base							
Gp.	Bickford Fm.				Siltstone, sandstone, conglomerate, and mudstone; minor coal; 285 to 300 m thick				
nnes	Monach Fm.		1		Sandstone and conglomerate; siltstone; 210 to 260 m thick			present only at	
Į≌	Monach Fm. Beattie Peaks Fm.				Siltstone, sandstone and mudstone; minor coal; 285 to 350 m thick			depth beneath the property	
	Monteith Fm.				Quartzite and sandstone; minor siltstone; 340 to 425 m thick				

Rock-units are discussed in detail below, in order from youngest (generally nearest the ground surface) to oldest. Localised inversions of stratigraphic position have been induced by

stratal shuffling consequent upon thrust-faulting, but the overall stratigraphic relations remain readily-recognisable, owing to distinctive geophysical and lithological characteristics of the various rock-units.

### 4.5 Drift (map-unit D)

Unconsolidated sediments, inferred to be of Quaternary age, form a patchy blanket at the ground surface throughout the Willow Creek Mine block. For reasons of clarity, Drift is not mapped as a separate entity within **Map 2-3**, except along the floor of the Pine River valley.

The most pervasive Drift cover consists of glacial till, usually less than 10 metres thick within the upland areas of the property. Patches of sandy, gravelly and bouldery alluvium are present within stream channels. McKechnie (1955) noted the presence of possibly-glaciolacustrine silt deposits within the southeastern portion of the Willow South area; although an extension of such deposits into Willow Creek Mine area is considered likely, the extent of such deposits has yet to be assessed in detail, owing to lack of lithological records in Drift-penetrating boreholes.

The Pine River valley is inferred to be floored and possibly flanked by valley-filling alluvial, glacial, and glaciolacustrine sediments. By inference with results of sparse drilling in other valleys within the Foothills of northeastern British Columbia, such deposits are inferred to be locally more than 150 metres thick.

### 4.6 Fort St. John Group (map-units 5, 4, and upper part of map-unit 3)

The uppermost of the Early Cretaceous rocks of the Fort St. John Group have been completely removed by erosion at Willow Creek Mine. Most of this erosion is likely to have occurred during a prolonged episode of regional uplift during the Tertiary era (Cant and Stockmal, 1989), followed by further glacial scouring during the Quaternary era, and continuing through fluvial down-cutting to the present time.

Within the Group, the remainder of its constituent formations remain at least locally-present within the Willow Creek Mine map-area. From top down, these are the basal half of the Hasler Formation, and the entirety of the Boulder Creek, Hulcross, Gates, Moosebar and Bluesky formations.

### 4.6.1 Hasler Formation (map-unit 8a)

The Hasler Formation, of late Middle Albian to Late Albian age (Gibson, 1992b) forms subdued slopes within the upland area northeast of the Willow Creek Mine block. The Hasler Formation is not interpreted to form bedrock within the boundaries of the block, but its basal portion (at least 180 metres thick) is mapped as forming bedrock within the northeastern corner of the mapped area of **Map 2-3**, completely outside the property's extent.

The Hasler Formation comprises marine siltstone, overlain by dark grey to black marine mudstone with occasional bands of sideritic concretions. The complete, undeformed thickness of the formation is approximately 335 to 365 metres (Wickenden and Shaw, 1943). A few centimetres to decimetres of erosive-based cherty gritstone commonly mark the Hasler Formation's abrupt basal contact with the underlying Boulder Creek Formation (Wickenden and Shaw, *op.cit.*, page 6).

### 4.6.2 Boulder Creek Formation (map-unit7)

The Boulder Creek Formation, of late Middle Albian age (Gibson, 1992b) forms prominent cliffs in the upland area, along and immediately to the northeast of the Willow Creek Mine block's northeastern boundary. The Boulder Creek Formation is the uppermost of the three formations (Boulder Creek, Hulcross, and Gates) formerly covered by the now-superseded Commotion Formation of Wickenden and Shaw (1943).

Regionally, conglomerate and sandstone are the predominant lithologies of the Boulder Creek Formation, but the Walton Creek Member of the formation also contains fine-grained rocks including siltstone, root-penetrated, variably-carbonaceous mudstone, and coal, some of which attains thicknesses of interest for underground mining.

Conglomerate and sandstone are concentrated in the basal Cadotte Member of the formation, while fine-grained rocks are concentrated in the overlying Walton Creek Member (Gibson, 1992b). The uppermost regionally-mapped division of the Boulder Creek Formation, comprising the conglomerate of the Paddy Member, is not recognised within the Willow Creek Mine area.

The overall thickness of the Boulder Creek Formation is tentatively inferred to be 75 to 95 metres at Willow Creek Mine, of which the basal 30 to 45 metres comprises the Cadotte Member and the overlying 45 to 50 metres comprises the Walton Creek Member. The basal contact of the Boulder Creek Formation with the underlying Hulcross Formation is abrupt to erosional at local scale, and likely to be interfingering at regional scale.

#### 4.6.2.1 Walton Creek Member

The Walton Creek Member of the Boulder Creek Formation comprises 45 to 50 metres of generally-recessive siltstone, variably-carbonaceous, locally root-penetrated mudstone and variably-thick coal beds, of which two or three appear to be laterally-continuous within Trefi Coal Corp.'s Trefi coal property, which lies to the southeast of the Willow Creek Mine block (Morris, 2015).

The swale-forming fine-grained rocks of the Walton Creek Member are punctuated by cliff-forming lenses of sandstone, gritstone and pebble-conglomerate, inferred to be channel-fills. Gibson (1992b) considered the Walton Creek Member to be of probable Late Albian age, based on angiosperm flora. The basal contact of the Walton Creek Member with the underlying Cadotte Member is generally abrupt, and regarded by Gibson (*op. cit.*) as being conformable.

### 4.6.2.2 Cadotte Member

The Cadotte Member of the Boulder Creek Formation comprises 30 to 45 metres of cliff-forming sandstone and pebble-conglomerate with rare thin interbeds of siltstone. The Cadotte generally coarsens upward, with its sandstones being at its base and its conglomerates being in its middle and at its top. Other than isolated coalified logs, the Cadotte Member is devoid of coal. The basal contact of the Cadotte Member with the underlying Hulcross Formation is generally abrupt and therefore considered to be conformable at local scale (Gibson, 1992b), although it may intertongue at regional scale.

### 4.6.3 Hulcross Formation (map-unit 6)

The Hulcross Formation, of middle Albian age within the Early Cretaceous (Stelck and Leckie, 1988) comprises thinly-interbedded, locally-concretionary grey siltstone, fine-grained sandstone and dark grey mudstone with occasional very thin but extremely-persistent interbeds of soft, light grey to white tuff (Kilby, 1985; Gibson, 1992b) and rare thin stringers of coal. Sideritic concretions are commonly found in isolated, laterally-persistent bands.

Within the area covered by **Map 2-3**, the Hulcross Formation forms a recessive band along the northeastern margin of the Willow Creek Mine block. The thickness of the Hulcross Formation at Willow Creek Mine is estimated to be 120 to 130 metres, based on borehole data and measured outcrop sections from nearby properties, as reported by Gibson (1992b). The formation's immediate base is characteristically marked by a thin (generally less than a metre thick) erosive-based bed of pebbly sandstone or gritstone, lying erosionally upon the underlying strata of the Notikewin Member of Gates Formation.

### 4.6.4 Gates Formation (map-unit 5)

The Gates Formation, of late Early Albian age within the Early Cretaceous, comprises thin to thick interbeds of sandstone, siltstone, conglomerate, and shale, locally accompanied by coal beds.

Coals of the Gates Formation, and their enclosing sedimentary rocks, were deposited on the shoreline of the Clearwater Sea (part of the Western Interior Seaway) between 108.7 and 111.0 million years ago, as part of an extensive complex of coastal plains, deltas and estuaries collectively known as the Gates Delta.

At Willow Creek Mine, the Gates coal-measures are present along the northeastern margin of the property. No boreholes have yet penetrated the Gates Formation at or near Willow Creek Mine, and hence its coal potential is unknown in detail, although expected to be low on account of the well-established northward diminishment of coal content within the formation.

Regionally, the Gates Formation may be readily subdivided into three members: the uppermost, dominantly fine-grained Notikewin coal-measures (90 to 120 metres thick?), the medial, dominantly coarse-grained conglomeratic Falher coal-measures (50 to 90 metres thick?), and the basal Torrens sandstone (30 to 40 metres thick?). The Notikewin, Falher and Torrens members can be reasonably-distinguished in the logs of oil and gas wells drilled to within the Highhat gasfield, situated to the southeast of Willow South, but these units cannot be easily mapped separately without the aid of detailed aerial imagery, so no attempt has been made to depict them separately on **Map 2-3**.

The Gates Formation is inferred to be 190 to 230 metres at Willow Creek. The nature of its contact with the underlying Moosebar Formation appears to be abrupt at local scale, but likely to be interfingering at the regional scale.

### 4.6.5 Moosebar Formation (map-units 4c, 4b, 3d, and 3c)

The Moosebar Formation, of early Albian age (Stott, 1968) forms the basal part of the Fort St John Group. At and near Willow Creek Mine, the Moosebar Formation has a typical stratigraphic thickness of at least 165 metres (Wickenden and Shaw, 1943, page 4) and

perhaps 240 to 280 metres, although the latter figure likely indicates substantial structural thickening due to thrust-induced telescoping of the Moosebar rocks.

The Moosebar Formation comprises an overall coarsening-upward sequence, comprised of several lesser coarsening-upward cycles, of mudstone passing upward to sandy siltstone. A basal pebbly, locally-glauconitic gritstone occurs within the middle of the formation in some sections. Very thin (a few millimetres to a few decimetres) bands of tuff form conspicuous marker bands, generally concentrated within the basal 30 metres of the formation (Kilby, 1984a; 1985).

At Willow Creek Mine, the Moosebar Formation is inferred to form bedrock along the block's northeastern side, flanking the Gething coal-measures exposed within the northeastern limb of the Pine River Anticlinorium (**Map 2-3**).

Regionally, deep exploratory drilling for natural gas targets allows the recognition of five lithological subdivisions (from top down, the Spieker and Cowmoose members, the Green Marker, and the Chamberlain and Bullmoose members) within the Moosebar Formation of the Willow Creek Mine area. All but the uppermost of these subdivisions are present and recognisable in pit-slope exposures at Willow Creek Mine, although one (the Green Marker, map-unit 4a) is consistently too thin to be mappable as anything other than a single line at the scale of **Map 2-3**.

Owing to the sparse extent of drilling within the Moosebar Formation, and the lack of detailed borehole records, no attempt has been made to map the subdivisions of the formation within the Willow Creek Mine block *per se*, although such mapping has been accomplished within the adjoining Willow West block.

### 4.6.5.1 Spieker Member (map-unit 4c)

The Spieker Member of the Moosebar Formation (Duff and Gilchrist, 1981), of early Albian age (Stott, 1968), comprises thinly-interbedded, coarsening-upward units of siltstone and very fine sandstone, within an overall coarsening-upward sequence. Bioturbation is pervasive and intense within the Spieker Member, which is interpreted to have formed as shallow-water turbidites within a proximal shelf setting in advance of the northward-prograding Gates paleodelta. The undeformed thickness of the Spieker Member at Willow Creek Mine is estimated to be 60 to 90 metres, possibly being locally thickened through thrust-induced structural telescoping.

The Spieker Member's existence at the latitude of the Willow Creek coal lease is established by drilling within the western part of the Willow West area (Cathyl-Huhn, 2015c), outside the extent of **Map 2-3**. The Spieker Member is also likely to be present within the northeastern part of the Willow Creek Mine block, but beyond the area which has been tested by drilling.

The basal contact of the Spieker Member with the underlying Cowmoose Member is abrupt, generally drawn at the base of an upward decrease in natural gamma radiation, which appears to coincide with an upward increase in the silt content of the rocks, and a concomitant passage from dark greyish-black to medium grey rock colour. The immediate base of the Spieker Member is in some sections marked by one or two metres of distinctly-sandy siltstone.

### 4.6.5.2 Cowmoose Member (map-unit 4b)

At and near Willow Creek Mine, the Cowmoose Member of the Moosebar Formation comprises 80 to 100 metres of rubbly-weathering, massive-appearing, dark greyish-black to black mudstone, punctuated by occasional bands crowded with ironstone concretions, and several very thin (a few millimetres to a few decimetres) but laterally-persistent and visually-prominent bands of light olive drab to white tuff. The tuff bands are useful as local structural markers (Duff and Gilchrist, 1981; Kilby, 1984a; Jordan and Dawson, 1988). The Cowmoose mudstones are sparsely-bioturbated, and locally contain sparse to abundant burrow-fillings, irregular blebs and euhedral crystals of pyrite, indicative of overall anoxic depositional conditions. Pyrite is particularly abundant near the base of the Cowmoose Member.

The name 'Cowmoose' was introduced by Cathyl-Huhn and Singh (2014) as an informal and pragmatic stratigraphic name, for the purposes of Walter Canadian Coal Partnership's coal-assessment studies; these rocks were previously referred to as the 'basal mudstone member' of the Moosebar Formation or simply as the 'mudstone member' (Duff and Gilchrist, 1981). The recommended type-section of the Cowmoose Member (Cathyl-Huhn and Singh, 2014) is on the northeastern face of Cowmoose Mountain, situated between Sukunka River and the western fork of Bullmoose Creek. Within the Willow Creek Mine block, the Cowmoose Member is locally exposed in road-cuttings and shalepits along access roads within the northeastern fringe of the block.

Without recourse to cored sections or gamma-neutron logs, isolated exposures of the Cowmoose Member would be quite similar in weathering-habit to, and therefore difficult to distinguish from, the basal part of the older Bullmoose Member. The Cowmoose Member is locally thickened to over 200 metres by thrust-induced structural telescoping (Cathyl-Huhn, 2015a; 2015b; Cathyl-Huhn *et al.*, 2015).

The age of the Cowmoose Member is Early Albian (as noted for the mudstones of the Moosebar Formation by Stott, 1968). The basal contact of the Cowmoose mudstones over the underlying Green Marker is gradational to abrupt, and generally easily-recognised on geophysical logs.

The basal contact of the Cowmoose Member with the underlying Green Marker (an informal lithostratigraphic unit previously designated as the 'Bluesky-S unit' by Kilby, 1984b) is abrupt, being readily recognised as a downward decrease of gamma-log counts, and the downward appearance of distinctively-greenish glauconitic sediments.

### 4.6.5.3 Green Marker (map-unit 4a)

The Green Marker (Cathyl-Huhn and Avery, 2014c) is a thin but regionally-persistent zone of erosive-based, pebbly, intensely-bioturbated, commonly-glauconitic sandstone, siltstone and mudstone. The Green Marker comprises zero to perhaps 3 metres of variably-glauconitic siltstone or chert-rich lithic arenite, locally containing stringers or lenses of gritstone or pebble-conglomerate. Owing to its minimal thickness, the Green Marker is depicted as a single line upon **Map 2-3**.

The Green Marker is locally altogether absent; hence its minimum thickness of 'nil' as given in **Table 4-1**. Glauconite development within this unit is patchy, in contrast with its more obvious presence in other areas.

Earlier reports (Wallis and Jordan, 1975; Jordan and Dawson, 1978) denoted this zone as the Bluesky Formation, on the grounds of its lithologic similarity to the typical Bluesky rocks of the Alberta Syncline and Deep Basin, but that correlation is now understood to be incorrect (Cathyl-Huhn and Singh, 2014). Although the lithology of the Green Marker is superficially similar to that of the older Bluesky Formation, these two glauconite-bearing zones are stratigraphically distinct, both in space and in time (Kilby, 1984b; Legun, 1990).

Kilby's (op. cit.) 'Bluesky-S unit' corresponds to the beds currently mapped as the Green Marker, whereas his older and stratigraphically-lower 'Bluesky-N' unit corresponds to beds here mapped as the Bluesky Formation.

The basal contact of the Green Marker with the underlying Chamberlain Member, or with the Bullmoose Member where the Chamberlain is absent, is characteristically abrupt and may at least locally be erosional.

### 4.6.5.4 Chamberlain Member (map-unit 3d)

At Willow Creek Mine, the Chamberlain Member of the Moosebar Formation is a geophysically-distinctive (moderately-low gamma-log responses) unit within the Moosebar, comprising a few (3 to perhaps 6) metres of rocks with a geophysical-log signature consistent with the regionally-known Chamberlain lithologies of interbedded sandstone and siltstone.

In contrast with the Chamberlain sections drilled in the Sukunka area (to the southeast of Willow Creek Mine), no coal has been found within the Chamberlain Member at Willow Creek Mine. Regionally, the Chamberlain Member is well-established as thinning to the east and northeast; it is locally altogether absent within oil and gas wells drilled at Highhat Mountain (a few tens of kilometres east of Willow Creek Mine), and in those wells the Cowmoose mudstones appear to directly overlie the Bullmoose siltstones.

Although in its type area at Sukunka Colliery and Bullmoose Mountain, the Chamberlain Member was defined by Gibson (1992a) as the uppermost member of the Gething Formation, in the Willow Creek area the Chamberlain's much-reduced thickness and apparent non-coalbearing nature support its being more properly assigned to the Moosebar Formation.

The Chamberlain Member is not known to contain diagnostic fossils; it has therefore been assigned an Early Albian age by Gibson (1992) on the basis of fossils found within the overlying Cowmoose Member of the Moosebar Formation. The basal contact of the Chamberlain Member with the underlying Bullmoose Member is gradational by interbedding, being drawn at the base of the Chamberlain's lowest thick sandstone. The Chamberlain-Bullmoose contact possibly rises stratigraphically, to the north and east (Cathyl-Huhn *et al.*, 2015), but available drilling does not suffice to confirm nor contradict this supposition.

### 4.6.5.5 Bullmoose Member (map-unit 3c)

The Bullmoose Member of the Willow Creek Mine block comprises 100 to 120 metres of thinly-interbedded, recessive-weathering mudstone, siltstone and minor sandstone of turbiditic aspect, forming several fining-upward sequences within an overall coarsening-upward sequence.



**Plate 4**: Southeastern highwall of 4N2 pit, as seen prior to resumption of mining in autumn of 2018. Forested slopes are underlain by siltstones with minor bands of ironstone and tuff, of the basal two-thirds of the Bullmoose Member of the Moosebar Formation. Cleared hillside to right is underlain by interbedded siltstone, sandstone, coal and variably-carbonaceous mudstone of the Gaylard Member of the Gething Formation. Closely-associated 400, 401, and 410 coals come to the ridgeline at the extreme right of the photograph. Bedding forms a northeastward homoclinal panel of strata, at dips of 30 to 32 degrees. [*RC4849/18.jpg*]

The geophysical log response of the Bullmoose Member is very distinct, as compared with the overlying Chamberlain Member and the underlying Bluesky Formation. Bullmoose rocks have characteristically-higher natural-gamma log responses than their bounding rock-units. On the other hand, the Bullmoose Member is difficult to distinguish from the younger Cowmoose Member.

The Bullmoose Member is well-exposed in the southeastern highwall of the 4N2 open-pit workings (as shown in **Plate 4**). The Bullmoose is inferred to form extensive areas of bedrock along the northeastern margin of the Willow Creek Mine block, extending into the adjoining Willow South block (**Map 2-3**).

The Bullmoose lacks coal, other than isolated coalified logs and coarse, poorly-preserved 'plant trash', likely of drifted origin. The Bullmoose does, however, contain abundant molluscan fossils, including *Pecten (Entolium)* cf. *irenense* McLearn (Gibson, 1992a) and *Yoldia kissoumi* (Duff and Gilchrist, 1981), which, although not age-diagnostic, are locally-characteristic of the unit. The Bullmoose Member likely corresponds with the 'Lower Silty Member' of the Moosebar Formation, as originally suggested and locally-recognised by Duff and Gilchrist (1981), within those areas (for example, the deep subsurface under Highhat Mountain, southeast of the Willow Creek Mine block) where the overlying Chamberlain Member is absent. Geophysical logs of the Bullmoose Member show a characteristic high-gamma response at two horizons situated a few tens of metres above the Bullmoose/Bluesky contact. These gamma 'spikes' are interpreted to be thin bands of tuff, each of them one to two decimetres thick, with the lower of the two bands being more persistent. These bands provide a regionally-extensive geophysical marker throughout the Falling Creek region (Kilby, 1984a).

The basal contact of the Bullmoose, with the underlying Bluesky Formation, is drawn at the top of the underlying glauconitic sandy mudstone. In geophysical logs, the Bullmoose/Bluesky contact is readily recognised as a rapid downward change in log response to higher resistivity response, lower natural-gamma counts, and higher API neutron counts. This downward change is interpreted to correspond with a rapid downward passage from fine-grained mudstone of the basal Bullmoose, to the sandy mudstone and sandstone of the uppermost Bluesky.

The Bullmoose Member is of late Early Albian age (Gibson, 1992a). The original stratigraphic thickness of the Bullmoose is approximately 100 to 120 metres at Willow Creek Mine, although thicker sections (likely structurally-thickened by thrust-induced telescoping of the strata) are suspected to exist. Similar anomalous thickening was previous noted from the Highhat Mountain area, where the Bullmoose Member was found to be 189 and 237 metres thick, respectively, in natural-gas wells b-91-L and a-23-D (Cathyl-Huhn, 2015b).

### 4.6.6 Bluesky Formation (map-unit 3b)

The Bluesky Formation is a transitional unit between marine and non-marine facies. Accordingly, there has been considerable debate within the geological literature -- starting with Stott (1968), and further discussed by Kilby (1984b) and Legun (1990) -- as to the Bluesky's stratigraphic affinities. In the present report, the Bluesky is considered to constitute a formation in its own right, bounded above by the Moosebar Formation, and beneath by the Gething Formation, following earlier workers (*cf.* Legun, 1990 and James, 1998). Further to the south within the Mink-Brazion coalfield, the Bluesky is considered to be a member within the Gething Formation (Cathyl-Huhn, 2015a; Cathyl-Huhn and Avery, 2014a; 2014b)



**Plate 5**: Geologist's hand marks erosional contact of Bluesky pebbly gritstone over Gaylard sandy siltstone. Rusty weathering habit of Bluesky rock suggests potential for acid rock drainage. View is to northeast, along eastern edge of 7S open-pit workings [*RC4945/18.jpg*]

The Bluesky Formation generally consists of coarsening-upward cycles of interbedded mudstone, siltstone, and sandstone. The top of the Bluesky is characteristically marked by a glauconitic horizon, a few decimetres thick (observed to be 40 to 57 centimetres thick at the nearby Mink Creek coal property by Sultan and Cathyl-Huhn, 2014), comprising abundant fine-grained, green glauconite within sandy mudstone and argillaceous, locally-pebbly, sandstone. The base of the Bluesky (shown in **Plate 5**) is marked by a distinctive erosive-based chert- and quartz-pebble conglomerate up to a metre thick, grading to argillaceous sandstone with few randomly-distributed chert and quartz pebbles. The conglomerate horizon's presence has been noted on numerous historic borehole records at Willow Creek Mine.

Bluesky sediments likely represent the initial transgressive deposits of an early tongue of the Clearwater Sea, which shortly after deposition of the Bluesky had transgressed to a southerly limit several hundred kilometres southeast of the Willow Creek area (Gibson, 1992a). The Bluesky Formation, as-drilled at and near Willow Creek Mine, is 1 to 8 metres thick. The age of the Bluesky is not directly known, but inferred to be late Early Albian on the basis of the ages of its bounding strata. The basal contact of the Bluesky Formation within the underlying Gething Formation is almost always erosional, locally with substantial downward scour into the older Gething rocks.

### 4.7 Bullhead Group (map-units 3a and 2)

Both formations of the Bullhead Group -- the Gething and the older Cadomin -- are present at Willow Creek Mine, with the Gething containing all known potentially-mineable coal beds.

#### 4.7.1 Gething Formation (map-unit 3a)

The Gething Formation, of Hauterivian to late Early Albian age (Gibson, 1992a), comprises thin to thick interbeds of siltstone, sandstone, mudstone and coal, with lesser amounts of gritstone, pebble-conglomerate, ironstone and tuff.

The Gething Formation originated as a complex of non-marine to shallow-marine sedimentary deposits, laid down by meandering and braided streams and rivers within a widely-extensive belt of coastal deltas and an intervening marine-influenced bay, of which the basal delta (the coal-bearing Gaylard paleodelta) extended throughout the Mink-Brazion coalfield, including the Willow Creek Mine block. At the latitude of Willow Creek Mine, the overlying (and therefore younger) Chamberlain paleodelta is presumed to have been only represented by a thin, non-coal-bearing, fringe of sandy/silty delta-front to prodeltaic deposits (Gibson, 1992a).

The Gething Formation forms the top of the Bullhead Group (Stott, 1968, as used in the present report), and of the Crassier Group (*sensu* Hughes, 1964, as previously observed in the Mink Creek coal property by Sultan and Cathyl-Huhn, 2014).

During historic (pre-2007) as well as current (years-2007 through 2013) drilling within the Willow Creek Mine block, nearly every coal-exploration borehole has intersected some section of the Gething Formation, but the thickness of the formation can only be indirectly estimated from this work, owing to lack of drilling into the underlying Cadomin Formation, as well as the block's pervasive structural complexity.

The basal contact of the Gething Formation with the underlying Cadomin Formation

is inferred to be abrupt to possibly erosional at the local scale (Cant, 1996) and interfingering at the regional scale (Stott, 1968; Gibson, 1992a), drawn at the top of a bed of coarse-grained, often gritty and occasionally pebbly sandstone which may laterally grade into more typical pebble-conglomerate or multi-storey sandstone characteristic of the underlying sub-Gething beds.

#### 4.7.1.1 Gaylard Member

Only one member (the Gaylard Member) is recognised within the Gething Formation at Willow Creek Mine, the overlying Bullmoose and Chamberlain rocks being here assigned to the Moosebar Formation, instead of to the Gething Formation as has been the case in property studies of areas lying further to the southeast.

#### 4.7.1.2 Subdivisions of the Gaylard Member (map-units 3a1 through 3a5)

The Gaylard Member may be conveniently divided into five informal subdivisions, on the basis of characteristic lithologies (chiefly changes in sand-shale ratio, with alternations of sandier and shalier sub-units), anchored by the presence of thick and laterally-extensive coal zones which likely formed atop regionally-extensive interfluves.

The divisions of the Gaylard are numbered in upward succession from Division 1 at the base of the Gaylard, to Division 5 at the top of the Gaylard. Drilling has established that the thickest, and possibly more laterally-extensive, coals occur within the Divisions 3, 4 and 5 of the Gaylard Member, within the Willow Creek Mine block.

**Table 4-1** (given above) summarises the subdivisions of the Gaylard Member. Major coal zones and other lithologies used as division markers are:

- No.4 coal zone, marking the base of Division 5;
- No.6 coal zone, marking the base of Division 4;
- No.8 coal zone, marking the base of Division 3;
- Heterolithic, mainly silty, strata forming Division 2; and
- Dominantly-sandy strata, comprising Division 1.

#### 4.7.1.3 Sedimentological and cyclothemic details

The Gaylard Member is interpreted to consist predominantly of non-marine sedimentary rocks within the Willow Creek Mine block, although the presence of at least one coal zone with slightly-elevated sulphur content (within the adjoining Willow South block) suggests that some marine influence may have occurred. The coal zone in question, No.8, lies within the basal half of the Gaylard Member.

The Gaylard Member consists principally of many vertically-stacked, locally erosive-based, fining-upward bedsets, such as are typical of fluvial and deltaic depositional settings.

A typical cyclic succession of Gaylard sediments commences with basal sandstone (rarely basal gritstone or pebble-conglomerate), passing upward through coarse- to fine-grained sandstone, siltstone, variably-carbonaceous mudstone, rooty

seatearth mudstone and coal. Most, but not all, Gaylard cycles are capped by coal beds, or by laterally-correlative carbonaceous to coaly mudstones. Coals vary in thickness: some are too thin (less than 40 to 50 cm) or too dirty, to be considered potentially-mineable, whereas other coals locally coalesce to form thick conjoint zones up to 4 metres thick. The individual component coal beds of these conjoint zones are readily-traceable on gamma-density logs, and they thus are interpreted to maintain their identity as sedimentation-units despite their bounding coal-on-coal contacts.

Coals frequently contain partings of siltstone or variably-carbonaceous mudstone, sometimes of tuff (the 'tonstein' bands of Kilby, 1984a and 1985), and rarely of nodular or banded ironstone. Splitting and lateral coalescence of coals is interpreted to represent the near-isochronous interaction peat accumulation in wetlands, avulsive processes within nearby river distributaries, and concomitant crevasse-splay sedimentation atop the coeval coal-forming wetlands (Banerjee and others, 1996).

Gamma-log response of the Gaylard sandstones (within and between these cycles) are 'ragged' in detail, occasionally capped by an upward-increasing 'bell-shaped' log response. In contrast, the siliceous sandstones and conglomerates within the underlying Cadomin Formation display distinctly 'blockier' responses than those of the Gaylard sandstones.

#### 4.7.1.4 Discussion concerning the thickness of the Gaylard Member

The thickness of the Gaylard Member is not directly known at Willow Creek Mine, owing to the lack of completely-drilled sections, and the pervasive presence of incompetent structures comprising folds and both small- and large-scale thrust-faults within the Gaylard's coal-measures. From incomplete, but apparently minimally-disturbed, sections the Gaylard is established to be at least 260 metres thick at Willow Creek Mine, and possibly up to 360 metres thick. Yet-greater thickness has not yet been ruled-out.

In contrast, within the nearby Highhat gasfield (15 kilometres to the southeast of Willow Creek Mine), complete sections of the Gething Formation are 475 to 720 metres thick (Cathyl-Huhn, 2015a), although some of that thickness is made up by marginal-marine deposits which are considered to be homotaxial with the basal part of the Moosebar Formation as found at Willow Creek Mine.

## 4.7.2 Cadomin Formation (map-unit 2)

The Cadomin Formation immediately underlies the Gething Formation, forming the basal part of the Bullhead Group (Stott, 1968). As such, the Cadomin Formation includes strata which may alternatively be assigned to the now-deprecated Dresser Formation of the Crassier Group *sensu* Hughes (1964) and Sultan (2015).

<u>Regionally</u>, the Cadomin Formation comprises one or more thick beds of coarse-grained, gritty to pebbly sandstone and pebble-conglomerate (McLean, 1977) with occasional lenses of siltstone and pebbly gritstone, and rare thin lenses of coal, several tens of metres thick overall.

The Cadomin Formation may be distinguished from the sandier parts of the Gaylard Member, upon the bases of the Cadomin Formation's greater lateral continuity, the

Cadomin's distinctly-'blocky' gamma-log response, and the frequent (but not universal, cf. Cant and Abrahamson, 1996) presence of an intervening zone of fine-grained coalmeasures strata.

Again regionally, the base of the Cadomin marks a northeastward-deepening angular unconformity, cutting down into successively-older rocks of the Minnes Group (Stott, 1973).

<u>Locally</u>, it remains uncertain whether the Cadomin Formation has been reached by any of the historic or current boreholes at Willow Creek Mine. By comparison with nearby properties, the Cadomin's basal contact with the underlying Bickford Formation of the Minnes Group is presumed to be erosional, with considerable local scour into the older sediments. The thickness of the Cadomin Formation at Willow Creek Mine is unknown, on account of lack of deep drilling. The estimated thickness of 2.5 to ca. 14 metres, as given in **Table 4-1** above, is derived from studies of the Gething and Cadomin formations within the adjoining Willow South coal property.

## 4.8 Minnes Group (map-unit 1)

The Minnes Group comprises 1000 to 1200 metres of clastic sedimentary rocks of latest Jurassic and earliest Cretaceous age, forming a poorly-exposed deltaic/shelfal/basinal complex which is overlain by the Bullhead Group. Four formations are locally recognised within the Minnes Group. From top down, they are the Bickford (equivalent to most of the now-deprecated Brenot Formation of Hughes, 1964), the Monach, the Beattie Peaks, and the Monteith formations (Stott, 1981; 1998). Coal is known to at least locally occur in all four of the Minnes Group's formations (Chowdry, 1980), but only the Bickford Formation is inferred to occur at reasonable depths within the Willow Creek Mine block, and therefore to be a credible (albeit thus-far apparently-untested) target for coal exploration.

## 5 Coal

As discussed above in **Section 4**, the Gaylard Member contains numerous coal beds, some of which are sufficiently thick and apparently laterally-continuous to constitute reasonable exploratory and mining targets, within the Willow Creek Mine block.

#### 5.1 Regional correlations of major Gaylard coals

Regional correlations of Gaylard coals are here proposed, although not examined in detail:

- The variably-sulphurous 'Bird' zone at Willow Creek Mine (shown in **Plate 6**) may be correlative with the Lower Gething A zone at Sukunka Colliery. It is definitely <u>not</u> correlative with the type Bird Seam at Sukunka, which instead lies near the top of the Chamberlain Member of the Gething Formation.
- No.4 zone at Willow Creek Mine may be correlative with the Brenda Seam at Hasler Creek, F zone at Mink Creek, Seam C60 at Burnt River, and the Lower Gething B zone at Sukunka Colliery;
- No.6 zone at Willow Creek Mine may be correlative with the Upper Seam at Burnt River; and
- No.7 zone at Willow Creek Mine may be correlative with the Lower Seam at Burnt River.

Coals of the Gaylard Member at Willow Creek Mine, and their enclosing sedimentary rocks, were deposited during Hauterivian to late Early Albian time, between 112 and 133 million years ago, on the basis of plant-fossil and foraminiferal zonations, as presented by Gibson (1992a).



**Plate 6**: Bird coal seam, approximately a metre thick, as exposed in the southeastern highwall of the 4N2 openpit workings. Coal seam comprises alternating blocky and sheared mushy bands. Note the bright yellow sulphate bloom on the weathered surface of the coal. Above is about 3 metres of silty sandstone and pebbly sandstone of the uppermost Gaylard Member, in turn erosionally-overlain by dark-weathering Bluesky gritstone. Top of exposed section is Bullmoose siltstone with centimetre- to decimetre-thick bands of conspicuously lightweathering tuff. [*RC4841/18.jpg*]

#### 5.2 Local naming scheme for Gaylard coals

**Table 5-1** depicts the conceptual stratigraphic hierarchy of coal zones, coal beds, and lesser subdivisions of coal beds, at Willow Creek Mine. Coal zones are numbered downwards from the Bird at the immediate top of the Gaylard Member, and then proceeding downward from the No.1 zone to the No.4 zone, then the A zone, followed by the No.5 through No.12 zones. The No.12 zone is postulated to lie close to the base of the Gaylard Member (or even, conceivably, within the older Bickford Formation although that supposition is not yet established). Each coal zone contains at least one major coal bed, and numerous subordinate and associated 'splits', 'stringers' and 'stringer plies'. Designations of the various major and minor coal beds have evolved with time from McKechnie's (1955) original concept of a series of numbered coal beds, into a more complex scheme of subordinate relationships. A system of split numbering was established by James (1998), who assigned odd terminal digits to subordinate coals lying above a major coal bed, and even terminal digits to those lying below a major coal bed.



**Plate 7**: Overturned chevron-fold, about 5 metres wide across axial plane, in the A1/A3/A5 group of coals within the A coal zone, as exposed in the highwall of a subsidiary pit situated to the southwest of 4N1 open-pit workings. View is upward and to the southwest, into the northwestern edge of the 4N1/4N2 development area. [*RC4922/18.jpg*]

#### 5.2.1 Caveat concerning coal bed designations

The system of coal-bed designation presented within **Table 5-1** is not intended to imply that major ('00' terminal-digit) coal beds become completely split into subordinate beds. Furthermore, not all stringers necessarily originate as laterally-continuous extensions of major coal beds. Considerable work likely remains to fully-establish splitting and coalescent relationships of the Gaylard Member coals at Willow Creek Mine, and within the Willow Creek coal lease in general.

Table 5-1: Stratigraphic hierarchy of coals and carbonaceous zones at Willow Creek Mine

		T 5		Ullaceous			
Formation	Member	Division	Coal Zone	Bed	Split	Stringer	Stringer Ply
Formation Gething	3.2	Division 9 Division	Bird	Bird			
듩	Gaylard	. <u></u>		190 (rare)			
99		Ĭ. Š		170			
				150			
			No.1				
				130			
					/ 111		
				110	110		
					/ 101		
				100	100		
				100	/ 201		
			N- O	000	7 201		
			No.2	200			
					\ 202		
				203 (rare)			
				330 (rare)			
				310			
				310	/ 201		
			l	200	/ 301		
			No.3	300	300		
				320			
				340			
				360 (rare)			
				430			
				430		/ / / / 0	
						/ 410	
					/ 401	401	
				400	400	400	
			No.4			\420	420
						0	\ 422 (rare}
				440	110	440	\ 422 (lale)
				440	440	440	
						\ 442	
				460			
				463			
				480	480	İ	
				100	\ 483		
		4					
		Division 4			/ A71	-	
		Sio		A7	A7		
		<u>`</u> <u>≥</u>			\A72		
							/ A55 (rare)
						/ A53 (rare)	A53 (rare)
					/ A51 (rara)		7.00 (laic)
				A.5	/ A51 (rare)	A51 (rare)	
				A5			
					/ A3		
				A1	A1		
						/ A03 (?)	
					/ ^ 01		
				10	/ A01	A01 (?)	
				A0	A0		
					\A02		
				A2 (?)			
	!			<u> </u>	Į	<u> </u>	<u> </u>

**Table 5-1**: Stratigraphic hierarchy of coals and carbonaceous zones at Willow Creek Mine (continued)

Formation	Member	Division	Coal Zone	Bed	Split	Stringer	Stringer Ply
Tomation	WEITIDEI	DIVISION	Coar Zoric	550	Орис	Ottringer	Ottlinger i ly
		Division 4		530			
Gething	Gething Gaylard			330	/ 511		
(continued)	(continued)	(continued)		510	510		
			No.5	510			
			No.5	500 (0)	/ 501		
				500 (?)	\ 500		
					\ 502		
				520			
				540			
				560			
				580			
				670			
		Division 3		650			
		sio			/ 631		
		ï∑		630	630		
				610			
			N. 0		/ 601		
			No.6	600	600		
					\ 602 (?)		
				620			
				640			
				770			
				750			
					731		
				730			
					/ 703 (?)		
							/ 712 (?)
						/ 710	710
					/ 701	701	
				700	700		
			No.7		\ 702		
					/ 721		
				720	720		
					\ 722		
				740			
				760			
				830			
			No.8	810	1	1	
				800	800		
					\ 802		
				820			
		_					
		) jor		900	900		
		Division 2	No.9		\ 920 (?)		
				980			

<b>Table 5-1</b> : Stratigraphic hierarchy of	f coals and
carbonaceous zones at Willow Creek Mine (	(concluded)

Formation	Member	Division	Coal Zone	Coal Bed	Split	Stringer	Stringer Ply
				1090			
				1070			
					/ 1003		
Gething	Gaylard	on				/ 1010 (?)	
		<u>is</u> +	No.10		/ 1001	1001	
(continued)	(continued)	Division 1		1000	1000		
				1020			
				1060			
				1080			
					/ 1101		
				1100	1100		
					\ 1102	1102	
							/ 1121 (?)
			No.11			\ 1120 (?)	1120
							\ 1122 (?)
					\ 1104		
				1140			
				1160			
				1180			
					/ 1210 (?)		
			No.12	1200	1200		
					\ 1220 (?)		

Note: table compiled by C.G. Cathyl-Huhn from Willow Creek Mine year-2001 through year-2018 drilling. Drilling of coal zones No.9 through No.12 is sparse; existence of No.12 zone in any of the year-2001 or more recent boreholes is not adequately established. Assignment of coal zone 12 to the Gething Formation is speculative, and merits further critical consideration. (?) indicates uncertainty of correlation. Symbols \ and / denote postulated splitting relationships.

## 5.3 Coals intersected by current boreholes at Willow Creek Mine

Correlatable coal intersections within the more recently-drilled of the historic boreholes (those drilled in years-2001 and 2005) and the current boreholes (those drilled in years-2007 through 2013) are collated as **Table A-2** within **Appendix A** of this report. Most of the coal intersections listed in **Table A-2** have been given identifying codes, such as '400', '442', or 'A3'. These codes have been assigned in aid of generating digital deposit models, subject to explicit hierarchical rules (presented graphically as **Table 5-1**) denoting their postulated 'parent-child' relationships as the various coal zones and coal beds are interpreted to split and possibly rejoin laterally.

Uncorrelated coal intersections are simply marked as 'coal'; additionally, thicknesses of Drift, presence of marker-horizons such as the Moosebar and Bluesky formations, along with the positions of inferred fault zones, are given within this table. It should not be presumed that all faults have yet been found, as it is likely to be more difficult to identify bedding-parallel faults (where the usual cues of missing or repeated sections of strata may be absent). Faults have been classified into their level-of-assurance as 'established', 'probable', and 'possible'.

# 6 Coal quality

Coal-quality data on samples of raw coal and associated rocks (from year-2018 borehole cores) are presented as **Table B-1** within **Appendix B** of this report.

#### 6.1 Scope of current coal-quality data

Amongst the 37 year-2018 boreholes, 27 were fully-cored at HQ size. Samples were taken of potentially-mineable coal beds as well as zones of rock (mostly carbonaceous or coaly rock) which might report as dilution within a mined product. Although it was planned and initially budgeted to conduct single-point washing at a separating density of 1.60 s.g., followed by compositional. petrographic, and reflectometric analyses, this work was not commenced during the period covered by this report, owing to backlogs in processing of the raw-coal samples.

A sample inventory and summary of raw coal quality results is presented as **Table B-1** within **Appendix B**. This table is followed by copies of analytical certificates provided by Birtley Coal & Minerals Testing, who conducted the laboratory tests of raw coal quality.

## 6.1.1 Cross-reference to historic coal-quality data

A considerable volume of historic (pre-2018) coal quality data is available; these data are presented within a prior coal assessment report (CAR-988: Cathyl-Huhn *et al.*, 2015c).

## 8 Reclamation

Drilling at Willow Creek Mine in year-2018 required the construction or reoccupation of 27 drill sites (see **Map 2-1**), some of which were pre-existing. Drill pads were mostly situated along pre-existing exploration trails, or atop the pit floor of the then-inactive 4N2 pit of the mine. Some drill pads were situated along newly-constructed trails. All work was done within the mine's existing disturbance boundary, and care was taken to avoid riparian setback areas.

As per usual practice, the drill sites were cleared of equipment, supplies and trash prior to demobilisation of the drilling rigs. Steep banks were pulled down at two locations, water bars were emplaced along the trails, deadfall was bucked and delimbed, and trees cut along new trails were bucked and delimbed. Wood was scattered along the trails, to create coarse woody substrates along the trails. Appropriate seeding will be undertaken as necessary, once the winter's snow has melted away.

## 9 Statement of costs

'Current work' at Willow Creek Mine, for purposes of the present report, comprises exploratory work done during the 2018-2019 tenure term, incorporating invoiced costs received to compilation date (March 17, 2019). No additional invoices are expected to be received during the remainder of March, 2019.

Work consisted mainly of drilling, by means of diamond-drilling (coring) and rotary (non-coring) methods (as referenced in **Table 3-3**, within **Section 3** of this report). All of the boreholes were logged by means of downhole geophysical surveys (as discussed in **Appendix A** of this report). Analytical work (see **Appendix B**) was done on core samples recovered from the diamond-drill holes.

Costs given below in **Table 9-1** (given on the following page) are based on invoices, net of Goods and Services Tax (GST). Drilling depths have been compiled from a collection of individual records, aggregated as hole-by-hole running totals.

In aid of planning future work, unit costs per metre have been determined via division of invoiced cost by relevant total metreages of drilling.

Overall cost of current work is estimated to have been \$1,617,533.79.

Cost breakdown by activity for the 2018-2019 reporting period: **Table 9-1** 

				<u> </u>					9   6				
Year / activity	mobe/de casing an	lling (including emobe of rig, d bit charges, nsumables))	subsistence, casing and bit charges, consum- ables, and catwork in support of rig moves)		Geophysical logging (including mobe/demobe of logging unit, subsistence, and crew rotation costs		Lab analysis (as reported in <b>Appendix B</b> of this report)		Roadwork (in support of rotary-drilling, and for trail deactivation)		Consultants (geological supervision and core-logging), including subsistence, crew rotations, and consumables)		Cost totals
	rotary metres	cost	cored metres	cost	drilled metres	cost	cored metres	cost	rotary metres	cost	drilled metres	cost	
2018/2019	1022.94	\$74,792.50	3676.59	\$943,543.1 3	4699.53	\$203,580.00	3676.59	\$100,397.55	1022.94	\$62,976.91	4699.53	\$232,243.70	\$1,617,533.79
Totals	1022.94	\$74,792.50	3676.59	\$943,543.1 3	4699.53	\$203,580.00	3676.59	\$100,397.55	1022.94	\$62,976.91	4699.53	\$232,243.70	\$1,617,533.79
Unit cost	\$73.1	2 / metre	\$256.64 / metre		\$43.3	\$43.32 / metre		31 / metre	\$61.5	6 / metre	\$49.4	2 / metre	\$344.19 / metre

Notes: unit costs are on per-metre drilled length basis, by division of the net invoiced costs by the length of relevant (cored vs. non-cored vs. all) drilling. Roadwork cost is only available for the rotary-drilling programme, inasmuch as the diamond-drilling programme carried costs of catwork for its drill-pads and access trails. Row and column totals contain slight rounding errors. Overall unit cost is based on all net costs divided by all metres drilled.

Personnel estimate: 405 total person-days of direct employment upon the work programme.

## 9.1 Contractor list

The following contractors provided goods or services in support of the 2018 drilling programme:

- Apex Geoscience -- consulting geology and project management, led by Jerry Holmes P.Geo.;
- Can-West Exploration -- catwork, in support of RC Drilling, and for trail deactivation;
- Century Wireline Services -- geophysical logging of all 37 boreholes;
- Duz Cho Construction -- catwork, billed through Geotech Drilling;
- Geotech Drilling Services -- diamond core drilling of 27 boreholes, with two drilling-rigs;
- RC Drilling -- air-rotary drilling of 10 boreholes, with one drilling-rig; and
- Robertson Manufacturing -- custom-made core boxes, billed through Geotech Drilling.

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## 11 Conclusions

Coal occurrences, known to include coals of workable thickness and variable raw (unwashed) ash content and caking propensity, occur within the Willow Creek Mine block of the Willow Creek coal property. These coals are contained within the Gaylard Member of the Lower Cretaceous (Hauterivian to Early Albian) Gething Formation. The Gaylard coal-measures have a stratigraphic thickness of at least 260 metres, possibly 360 metres or more. Numerous coal zones, each containing one or more major coal beds, are present within the Gaylard Member. Coal beds split and coalesce laterally, complicating their correlation and tracing throughout the Willow Creek Mine block.

Rocks at Willow Creek Mine have been dislocated by several southwest-verging thrust faults, likely accompanied by incompetent mesoscale folds, within an overall passive-roof duplex (triangle-zone) structural style consisted with lying within the northeastern leading edge of the Pine River Anticlinorium.

In all, 726 historic boreholes, totalling 50,701.53 metres' length, have been drilled during years-1980 through 2013 within the Willow Creek Mine block of the Willow Creek coal lease. No drilling is known by the author to have been done in years-2014 through 2017. An additional 37 current boreholes (here-reported for the first time), with overall length of 4,699.53 metres, were drilled on the property in year-2018. Overall drilling totals to date are 763 boreholes and 55,401.06 metres. This total does not include earlier drilling (at locations not yet confirmed by site surveys, and for which logs are as-yet unavailable) of boreholes by the British Columbia Department of Mines (reported by McKechnie, 1955) in years-1946 through 1951.

Drilling at Willow Creek Mine is regarded as sufficient to support the determination of coal-resources to current Canadian geometric standards (Hughes *et al.*, 1989), provided that an updated structural model is assembled, and an updated coal-quality model is constructed, in order to support the distinction of coking-coal, PCI coal, and thermal-coal within the deposit. This modelling work is now being undertaken by the mine's engineering and geological staff

Estimated current exploratory and analytical costs to date (from April 1, 2019 through to March 17, 2019, and anticipating no further invoices received prior to the tenure's anniversary date of March 31, 2019), are \$1.617.533.79.

The Willow Creek Mine block is regarded as being a property of merit.

# 12 Statement of qualifications

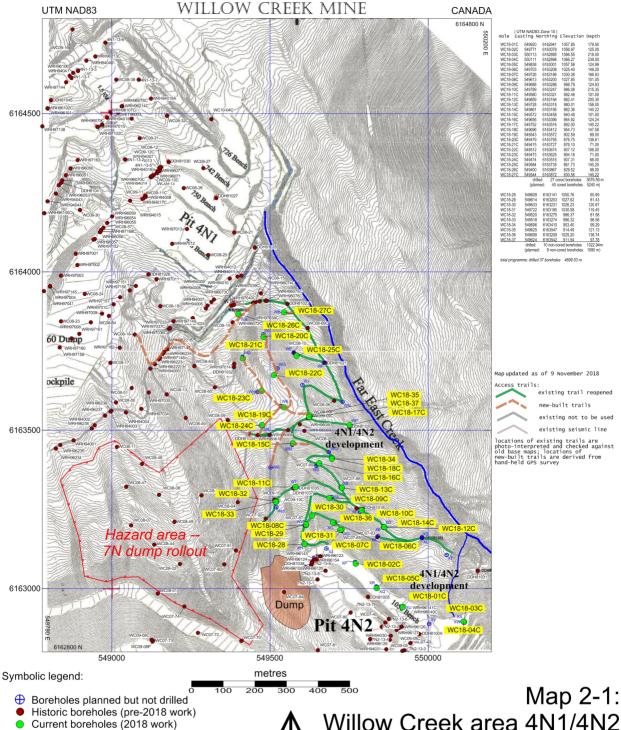
## I, C.G. Cathyl-Huhn P.Geo.(BC) Lic.Geol.(WA) RMSME, do hereby certify that:

- a) I am currently employed on a full-time basis as Chief Geologist by Conuma Coal Resources Limited, in their Canadian regional office in 200-235 Front Street (PO Box 2140), Tumbler Ridge, British Columbia, V0C 2W0 Canada, with permanent domicile at P.O. Box 40, Cumberland, British Columbia V0R 1S0 Canada.
- b) This certificate applies to the current report, titled *Coal Assessment Report for the Willow Creek coal lease -- Volume 5: Willow Creek Mine, 2018 infill drilling*, dated March 17, 2019.
- c) I am a member (Professional Geoscientist, Licence No.20550) of the Association of Professional Engineers and Geoscientists of British Columbia, licensed as a geologist (Licence No.2089) in Washington State, a founding Registered Member of the Society for Mining, Metallurgy and Exploration (SME, Member No.518350), and a Life Member of the Canadian Institute of Mining, Metallurgy, and Petroleum (CIM). I hold British Columbia certification as a Mine Supervisor (No.835247, valid until May 31, 2023). I have worked as a colliery geologist in several countries for 40 years since my graduation from university.
- d) I certify that by reason of my education, affiliation with professional associations, and past relevant work experience, having written numerous published and private reports and technical papers concerning coalfield geology, coal-mining geology and coal-resource estimation, that I am qualified as a Qualified Person as defined by Canadian *National Instrument 43-101* and a Competent Person as defined by the Australian *JORC Code*.
- e) My most recent visits to the Willow Creek Mine block of the Willow Creek coal property were in the summer and autumn of 2018, to oversee and direct the drilling and geophysical logging programme in my capacity as Chief Geologist.
- f) I am the author of this report, titled *Coal Assessment Report for the Willow Creek coal lease Volume 5: Willow Creek Mine, 2018 infill drilling*, dated March 17, 2019, concerning the Willow Creek Mine block of the Willow Creek coal property.
- g) As of the date of the writing of this report, I am not independent of Conuma Coal Resources Limited, pursuant to the tests in Section 1.4 of *National Instrument 43-101*.

"original signed and sealed by"

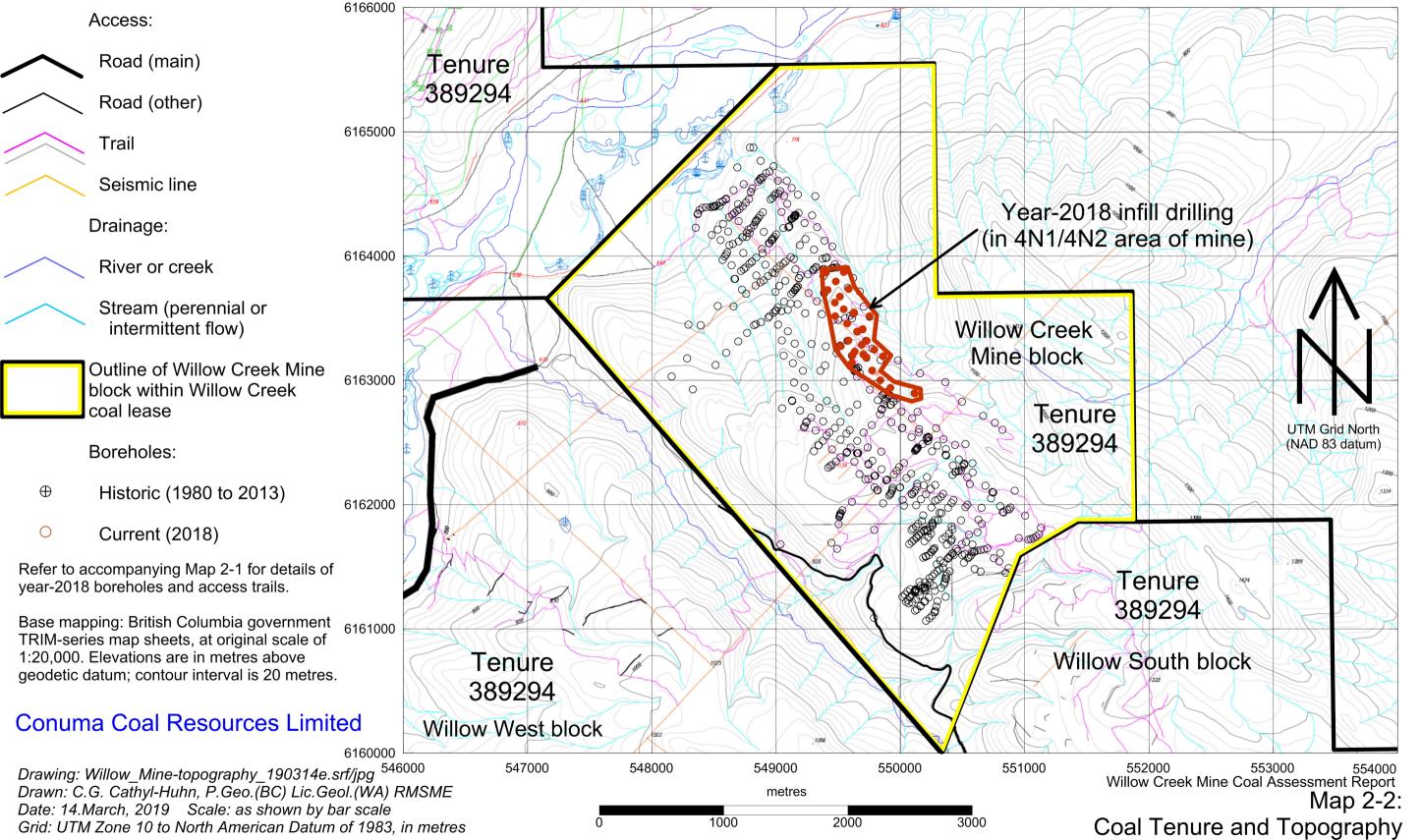
Dated this 17th day of March, 2019.

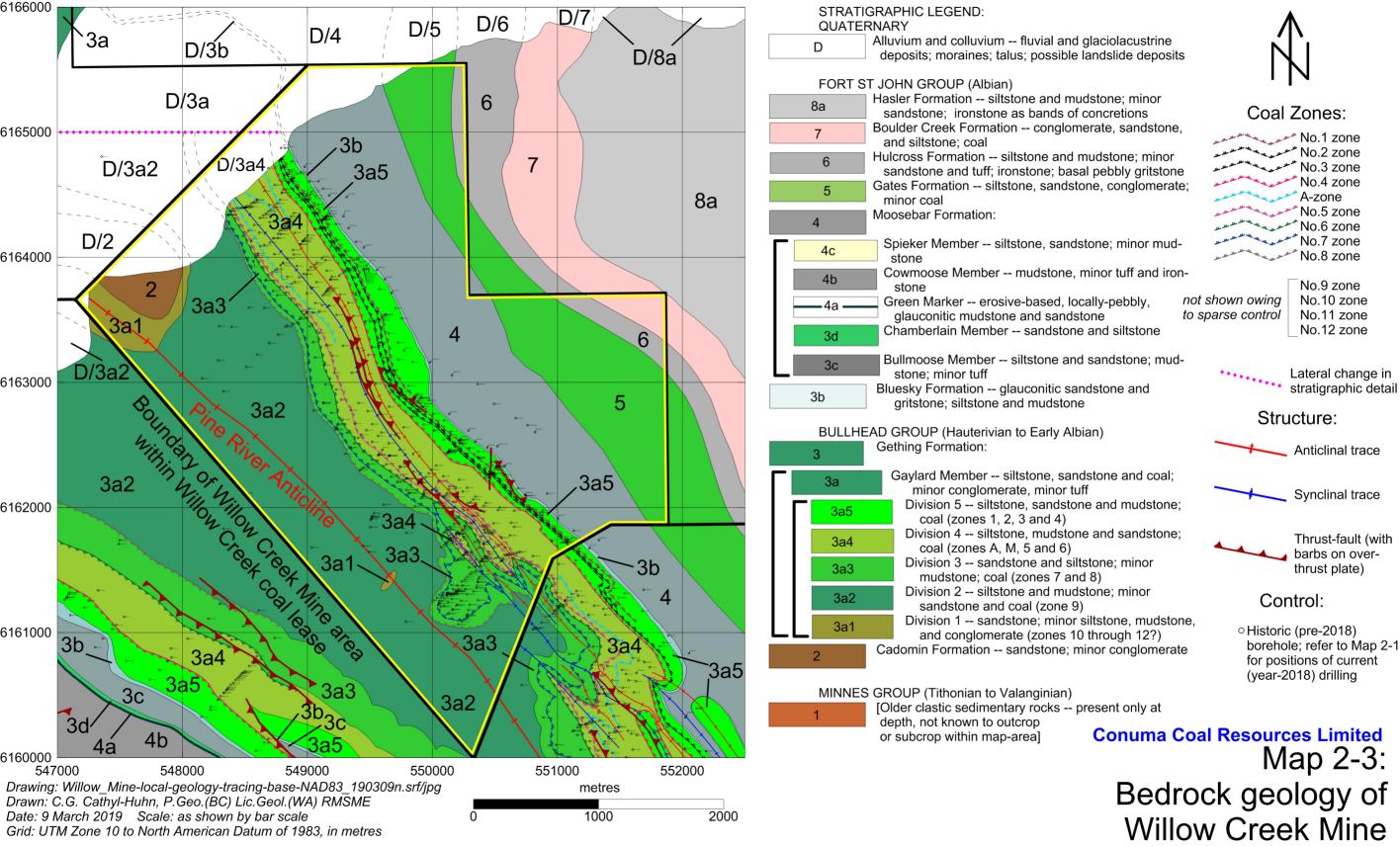
C.G. Cathyl-Huhn P.Geo. (BC) Lic.Geol. (WA) RMSME British Columbia Mine Supervisor No.835247



Drawing: Willow-Mine-drilling-final\_190309c.srf/jpg Scale: as shown Grid: UTM NAD83 Zone 10, in metres Reference: Willow-infill-sites\_180807e.dat/xls; Apex CSV file Drawn: C.G.Cathyl-Huhn P.Geo(BC) Lic.Geol(WA) RMSME Date: 9 March 2019  $\bigwedge$ 

Willow Creek area 4N1/4N2 year-2018 infill drilling -final programme map







# Geophysical logs and borehole statistics: Appendix A

Geophysical logging and the pertinent statistics of the current (year-2018) boreholes at Willow Creek Mine are summarised in **Table A-1** (commencing on the following page). Copies of the geophysical logs are submitted as digital files on a flash drive accompanying this report, in LAS, TIF, and/or PDF formats.

LAS and TIF are the primary digital formats within which geophysical logs are customarily (in modern practice) provided by borehole-logging service companies. PDF is a secondary format.

Geophysical logs are obtained by lowering a self-contained cylindrical sonde to the bottom of a borehole (or as close to the bottom as is safely practicable, given borehole wall stability conditions), and then drawing the sonde upward by means of a cable which contains power and data-transfer conductors. Depth reference on each log is based upon readings of a depth transponder connected to the geophysical logging system's drawworks. A very small amount of cable stretch may occur, depending upon the weight and diameter of each sonde; this accounts for slight variations in reported depths of log measurements as compared from one log suite to another.

Ordinarily, geophysical logs are run within boreholes once the drilling rods have been withdrawn. This practice allows for measurement of borehole diameter with a caliper instrument, and further allows for the effective collection of properly-calibrated log measurements. In some occasions, logs have been run within the drill rods, owing to concerns regarding borehole stability; these logs may or may not be subsequently be re-run with the rods withdrawn, again depending upon borehole conditions.

Positional and elevation data for boreholes are given in metres. Depths given on all geophysical logs are also given in metres, below the datum points mentioned in the headers of each log. Downhole depths reached by individual logging suites will vary, according to the length of each sonde, and also according to the source/detector geometry (and hence the measurement reference point) of each sonde. Geophysical log depth is therefore generally slightly less than driller's reported depth of each hole.

**Table A-2** presents interpretations of principal correlatable coal beds within current (year-2018) boreholes at Willow Creek Mine. All depths presented within this table are given in terms of downhole depth (along the boreholes' trajectories) in metres.

**Table A-3** presents cross-references between PDF scan-files and borehole core descriptions for boreholes WC18-01C through WC18-27C. In the printed copies of this report, xerographic copies of core descriptions follow **Table A-4**.

**Table A-4** describes methods of core description, and identifies the contract geological staff (from Apex Geoscience) who logged the cores under the author's direction and supervision.

											y of bor				llogs	Table A	<b>\-1</b> - shee	et 1 of 1
	1	ails (suffix 'C' de									ophysical logs							
Borehole		ed borehole posi		Drilled dep	th (metres)		ensity through		ited gamma-	Deviation		utron through	Gamm	a-neutron	Dip	meter	S	onic
		UTM NAD83 Zoi					l rods		stivity-caliper	<u> </u>		roads				• • • • • • • • • • • • • • • • • • • •		
	Easting	Northing	Elevation	Cored	Non-cored	Century	9068 tool	Century 9	9239C tool	Century	Century	9067 tool	Century	9058A tool	Century	9411A tool	Century	9325A tool
				(HQ size)	(114.3	TD	1	TD	1	9058A	TD I	1	TD	1	TD	1	TD	<del></del>
					mm)	TD logger	Last rdg	TD logger	Last rdg	Last rdg	TD logger	Last rdg	TD logger	Last rdg	TD logger	Last rdg	TD logger	Last rdg
WC18-01C	549919.717	6162941.125	1057.853	179.50		179.26	179.06	179.26	179.02	179	n/a	179.10	179.26	179.08				
WC18-02C	549770.728	6163078.855	1056.971	125.00		125.00	124.92	125.00	124.74	124	125.00	124.86	125.00	124.86	101000			
WC18-03C	550113.152	6162894.828	1066.552	218.00		200 00	200 =0	218.00	217.76	217	218.00	217.92	218.00	217.80	218.00	217.40		
WC18-04C	550111.305	6162896.186	1066.265	239.00		239.00	238.76	239.00	238.76	238	239.00	238.80	239.00	238.84				
WC18-05C	549837.504	6163001.175	1057.579	124.99		124.99	124.74	124.99	124.72	124	124.99	124.64	124.99	124.56	140.00	440.00		
WC18-06C	549703.347	6163208.038	1025.403	149.20		400.00	100.70	149.00	148.76	148	100.00	100.00	149.00	148.68	149.00	148.90		
WC18-07C	549726.288	6163185.982	1030.381	166.93		166.93	166.78	166.93	166.66	165	166.93	166.62	166.93	166.74	166.93	165.97		
WC18-08C	549613.477	6163200.911	1027.849	101.05		101.05	100.84	101.05	100.74	100	101.05	100.84	101.05	100.88				
WC18-09C	549687.550	6163285.864	998.789	124.93		124.93	124.64	124.93	124.68	124	124.93	124.88	124.93	124.54				
WC18-10C	549789.164	6163247.370	986.076	215.35		215.35	215.02	215.35	215.10	215	215.35	215.04	215.35	215.22				
WC18-11C	549580.191	6163320.688	992.477	101.00		101.00	100.74	101.00	100.74	100	101.00	100.86	101.00	100.88				
WC18-12C	549859.289	6163193.974	982.413	200.30		200.30	200.04	200.30	200.02	200	200.30	200.04	200.30	200.04	150.00	157.70		
WC18-13C	549727.625	6163318.047 6163194.631	980.012	158.00		158.00	157.76	158.00	157.76	157 139	158.00	157.90	140.00	120.04	158.00	157.72	_	
WC18-14C WC18-15C	549861.101	6163458.394	982.358 940.478	140.22 101.00		140.22 101.00	140.00 101.20	140.22 101.00	139.98 100.74	100	140.22 101.00	139.90 101.12	140.22 101.00	139.94				
WC18-15C	549571.514 549655.649	6163395.747	964.918	124.24		124.24	124.74	124.24	124.00	124	124.24	124.78	124.24	124.00				
WC18-16C	549055.049	6163516.076	891.998	140.22		140.22	139.76	140.22	139.98	139	140.22	139.90	140.22	139.94				
WC18-17C	549696.047	6163411.618	954.725	147.58		147.82	145.72	140.22	147.58	147	n/a	146.00	140.22	148.80			+	+
WC18-19C	549543.156	6163572.340	902.591	89.00		89.00	79.98	89.00	88.74	79	89.00	79.92	89.00	88.62		+		
WC18-19C	549478.986	6163795.215	876.747	136.61		136.61	135.84	136.61	136.36	136	136.61	135.92	136.61	136.52				
WC18-20C	549414.521	6163726.503	876.097	71.00		71.00	70.76	71.00	70.76	70	71.00	70.90	71.00	70.90				
WC18-21C	549512.394	6163673.934	907.123	106.00		106.00	95.08	106.00	105.76	105	106.00	95.12	106.00	105.72				
WC18-23C	549472.881	6163624.654	894.18	71.00		71.00	70.76	71.00	70.76	70	71.00	70.80	71.00	70.90		1	71.00	70.54
WC18-24C	549474.112	6163516.344	907.308	68.00		68.00	67.76	68.00	67.30	67	68.00	67.90	68.00	67.90			71.00	70.54
WC18-25C	549584.109	6163735.278	861.732	140.25		140.25	140.00	140.25	140.02	140	140.25	140.16	140.25	140.16			140.25	139.30
WC18-26C	549400.485	6163867.209	829.519	98.00		98.00	97.74	98.00	97.74	97	98.00	97.90	98.00	97.88			140.20	100.00
WC18-27C	549544.060	6163871.966		<del></del>		140.22	139.76	140.22	139.98	140	140.22	139.90	140.22	140.12			140.22	139.06
WC18-28	549608.840	6163141.020	1050.764	140.22	65.99	140.22	100.70	65.99	65.74	65	140.22	100.00	65.99	65.72	65.99	65.34	140.22	100.00
WC18-29	549613.570	6163203.004	1027.623		81.43			81.43	81.16	81			81.43	81.12	81.43	81.19		+
WC18-30	549632.612	6163231.418			120.97			120.97	120.70	120			120.97	120.70	120.97	120.79		
WC18-31	549722.241	6163184.832	1030.577		119.45			119.45	119.26	119			119.49	119.24	119.49	119.31		+
WC18-32	549519.825	6163274.772	986.371		81.58			81.58	81.30	81			81.58	81.16	81.58	81.14		
WC18-33	549518.468	6163274.156	986.323		96.58			96.58	96.32	96			96.58	96.32	96.58	82.63		
WC18-34	549696.213	6163410.049	953.399		99.29			99.29	99.02	99			12.00	1	99.29	99.14		+
WC18-35	549624.894	6163546.955	914.489		121.13			121.13	120.86	119	121.13	116.38			121.13	120.97		+
WC18-36	549699.301	6163208.768	1025.2		138.74			138.74	138.48	138	1=11.0		138.74	138.28	138.74	138.20		
WC18-37	549623.775	6163541.670	911.541		97.78			98.04	97.78	97			98.04	97.86	98.04	97.86	98.04	97.84
37 holes				27 holes	10 holes	25	holes	+	holes	37 holes	27 1	holes		holes		holes		holes
4699.53 m				3676.59 m	1022.94 m		0.09 m		9.35 m	4659 m		7.20 m		2.19 m		5.17 m		9.51 m

**Abbreviations:** TD -- total depth (in metres); rdg - reading (on log, in metres); all log depths are taken from log headers, with exception of deviation, taken as deepest reported depths *Willow-2018-Table-A-1\_190310b.doc* 

# Lithology codes for CAR-1048 **Table A-2**:

ASH = volcanic ash (high-gamma zone)

C = coal

CBSH = carbonaceous rock

CR = coaly rock

DC = dirty coal

DNR = did not reach (the horizon in question)

ND = no data

NP = not present

NR = not recognised

R= rock

From	To	Drilled	of geophysical logs Interpreted lithology	Name
		thickness		
Log inter	pretation of V	WC18-01C (me	tres)	
0	4.1	4.1	DRIFT	DRIFT
4.1	5.75	1.65	R	
5.75	6.1	0.35	DC	111
6.1	6.45	0.35	CBSH	111
6.45	6.75	0.3	DC	111
6.75	8.9	2.15	R	
8.9	9.8	0.9	С	110
9.8	18.65	8.85	R	
18.65	18.95	0.3	DC	101
18.95	20.55	1.6	С	101
20.55	23.8	3.25	С	100
23.8	24.1	0.3	CBSH	
24.1	26.8	2.7	R	
26.8	27	0.2	CBSH	
27	27.9	0.9	R	
27.9	38.35	10.45	CBSH	
38.35	38.55	0.2	CR	
38.55	40.05	1.5	С	201
40.05	40.3	0.25	CR	
40.3	40.45	0.15	CBSH	
40.45	42.2	1.75	R	
42.2	42.45	0.25	DC	202
42.45	42.65	0.2	ASH	202
42.65	42.8	0.15	CR	202
42.8	43.02	0.22	DC	202
43.02	43.35	0.33	С	202
43.35	54.35	11	R	
54.35	55.2	0.85	CBSH	
55.2	55.6	0.4	С	310
55.6	55.75	0.15	CBSH	
55.75	61.6	5.85	R	
61.6	61.9	0.3	С	300
61.9	62.05	0.15	DC	300
62.05	62.6	0.55	С	300
62.6	62.8	0.2	CBSH	
62.8	68.8	6	R	
68.8	69.2	0.4	CBSH	
69.2	69.5	0.3	DC	320
69.5	69.8	0.3	С	320
69.8	70.3	0.5	CBSH	

From	То	Drilled	Interpreted lithology	Name
Lasintan	mustation of W	thickness	tuna) nautiumad	
	73.9		tres) continued R	
70.3		3.6 0.8	CBSH	340
73.9	74.7			340
74.7	74.95	0.25	CR	
74.95	75.15	0.2	DC	340
75.15	75.6	0.45	CR	340
75.6	75.9	0.3	DC	340
75.9	76.25	0.35	CBSH	340
76.25	76.4	0.15	R	340
76.4	76.8	0.4	CBSH	340
76.8	77.2	0.4	CR	340
77.2	77.65	0.45	CBSH	340
77.65	78.35	0.7	CR	340
78.35	78.55	0.2	CBSH	340
78.55	111.65	33.1	R	1100
111.65	112.2	0.55	CBSH	410?
112.2	112.4	0.2	CR	
112.4	113.6	1.2	С	401
113.6	115.6	2	С	400
115.6	115.8	0.2	С	420
115.8	116.05	0.25	CBSH	
116.05	118.65	2.6	R	
118.65	118.9	0.25	CBSH	
118.9	119.65	0.75	С	440
119.65	122.65	3	R	
122.65	122.9	0.25	IRST	IRONSTONE
122.9	128.6	5.7	R	
128.6	129.05	0.45	CBSH	
129.05	129.3	0.25	R	
129.3	130.4	1.1	CBSH	463
130.4	137.1	6.7	R	
137.1	137.3	0.2	CR	460
137.3	137.5	0.2	CBSH	460
137.5	139.55	2.05	R	
139.55	139.9	0.35	CBSH	483?
139.9	140.1	0.2	FAULT	POSSIBLE
140.1	144.4	4.3	R	
144.4	144.6	0.2	CR	460
144.6	144.8	0.2	CBSH	460
144.8	156.4	11.6	R	

Table A-2:	Lithological i	nterpretation	of geophysical logs	
From	То	Drilled	Interpreted lithology	Name
		thickness		
Log interpre	etation of WC	C18-01C (met	res) continued	
156.4	156.65	0.25	CR	
156.65	157.05	0.4	С	480
157.05	157.25	0.2	DC	480
157.25	157.65	0.4	С	480
157.65	157.9	0.25	CR	
157.9	163.5	5.6	R	
163.5	163.7	0.2	CR	
163.7	172.65	8.95	R	
172.65	172.85	0.2	CBSH	
172.85	173.8	0.95	С	A7
173.8	174.1	0.3	CR	
174.1	174.4	0.3	CBSH	
174.4	179.5	5.1	R	
Log interpre	etation of WC	18-02C (met	res)	
From	То	Drilled	Interpreted lithology	Name
		thickness		
0	4.5	4.5	DRIFT	DRIFT
4.5	6.05	1.55	R	
6.05	6.3	0.25	CBSH	170?
6.3	9.8	3.5	R	
9.8	10.1	0.3	С	150
10.1	10.4	0.3	DC	150
10.4	10.6	0.2	CR	
10.6	11.2	0.6	CBSH	
11.2	16.65	5.45	R	
16.65	17.05	0.4	CBSH	130
17.05	20.55	3.5	R	
20.55	20.9	0.35	DC	111
20.9	21.05	0.15	CBSH	
21.05	22	0.95	R	
22	22.43	0.43	DC	110
22.43	22.6	0.17	С	110
22.6	26	3.4	R	
26	26.55	0.55	С	101
26.55	27.8	1.25	С	100
27.8	28.4	0.6	R	
28.4	28.8	0.4	CBSH	

From	То	Drilled	of geophysical logs Interpreted lithology	Name
		thickness		
Log inter	pretation of V	VC18-02C (me	tres) continued	
28.8	32	3.2	R	
32	32.5	0.5	CBSH	
32.5	32.59	0.09	DC	201
32.59	33.3	0.71	С	201
33.3	33.5	0.2	CBSH	
33.5	35.5	2	R	
35.5	35.7	0.2	С	202
35.7	35.83	0.13	DC	202
35.83	36.03	0.2	С	202
36.03	36.05	0.02	DC	202
36.05	36.16	0.11	ASH	202
36.16	36.25	0.09	DC	202
36.25	36.55	0.3	С	202
36.55	43.8	7.25	R	
43.8	44.3	0.5	CBSH	
44.3	44.75	0.45	R	
44.75	45.1	0.35	CBSH	310
45.1	46.3	1.2	R	
46.3	46.6	0.3	IRST	IRONSTONE
46.6	49.75	3.15	R	
49.75	49.88	0.13	DC	300
49.88	50.4	0.52	С	300
50.4	54.2	3.8	R	
54.2	54.35	0.15	С	320
54.35	54.39	0.04	R	320
54.39	54.46	0.07	С	320
54.46	56.15	1.69	R	
56.15	57.55	1.4	CBSH	340
57.55	79.35	21.8	R	
79.35	79.5	0.15	С	410
79.5	80.05	0.55	R	
80.05	80.6	0.55	С	401
80.6	81.4	0.8	С	400
81.4	83.55	2.15	R	
83.55	83.79	0.24	DC	420
83.79	84.05	0.26	С	420
84.05	84.6	0.55	DC	420
84.6	85	0.4	R	
85	85.4	0.4	DC	422?

From	То	Drilled	of geophysical logs Interpreted lithology	Name
1 10111	10	thickness	interpreted nunorogy	Turne
Log interr	oretation of W		tres) continued	
85.4	89.25	3.85	R	
89.25	89.6	0.35	С	440
89.6	89.77	0.17	R	
89.77	89.9	0.13	DC	442
89.9	90	0.1	CR	
90	105.1	15.1	R	
105.1	105.33	0.23	DC	460
105.33	105.39	0.06	С	460
105.39	105.5	0.11	DC	460
105.5	115.2	9.7	R	
115.2	115.44	0.24	DC	480
115.44	115.55	0.11	R	480
115.55	116.1	0.55	С	480
116.1	117.5	1.4	R	
117.5	117.9	0.4	CBSH	
117.9	120.2	2.3	R	
120.2	120.5	0.3	CBSH	
120.5	125	4.5	R	
Log interp	oretation of W	/C18-03C (me	tres)	
From	То	Drilled	Interpreted lithology	Name
		thickness		
0	11.78	11.78	DRIFT	DRIFT
11.78	14.65	2.87	R	BULLMOOSE
14.65	15	0.35	IRST	BULLMOOSE
15	17.35	2.35	R	BULLMOOSE
17.35	17.75	0.4	IRST	BULLMOOSE
17.75	20.7	2.95	R	BULLMOOSE
20.7	21.1	0.4	IRST	BULLMOOSE
21.1	30.6	9.5	R	BULLMOOSE
30.6	34.5	3.9	R	BLUESKY
34.5	34.6	0.1	R	
34.6	35.6	1	DC	BIRD
35.6	36.4	0.8	R	
36.4	36.75	0.35	CBSH	
36.75	36.95	0.2	R	
36.95	37.3	0.35	CBSH	
37.3	41.7	4.4	R	

From	То	Drilled	Interpreted lithology	Name
		thickness		
			tres) continued	1
41.7	41.95	0.25	CBSH	190
41.95	55.35	13.4	R	
55.35	55.9	0.55	DC	150
55.9	60.25	4.35	R	
60.25	60.7	0.45	CBSH	130
60.7	64.2	3.5	R	
64.2	64.5	0.3	DC	111
64.5	65.55	1.05	R	
65.55	65.9	0.35	C	110
65.9	69.05	3.15	R	
69.05	69.6	0.55	С	101
69.6	71.8	2.2	С	100
71.8	72	0.2	DC	100
72	85.25	13.25	R	
85.25	85.6	0.35	CBSH	
85.6	86.42	0.82	С	201
86.42	86.55	0.13	DC	201
86.55	87.2	0.65	R	
87.2	87.65	0.45	С	202
87.65	88.02	0.37	ASH	202
88.02	88.4	0.38	С	202
88.4	94.25	5.85	R	
94.25	94.55	0.3	CBSH	330
94.55	95.85	1.3	R	
95.85	96	0.15	CR	
96	96.15	0.15	DC	310
96.15	96.7	0.55	CR	
96.7	97	0.3	CBSH	
97	97.1	0.1	CR	
97.1	97.3	0.2	DC	300
97.3	97.4	0.1	CR	300
97.4	97.55	0.15	CBSH	300
97.55	97.7	0.15	DC	300
97.7	98.4	0.7	С	300
98.4	101.3	2.9	R	
101.3	101.75	0.45	CBSH	320?
101.75	102.2	0.45	CR	320?
102.2	105.4	3.2	R	
105.4	105.65	0.25	CBSH	340

From	То	Drilled	Interpreted lithology	Name
		thickness		
			tres) continued	
105.65	121.35	15.7	R	
121.35	121.55	0.2	CBSH	410
121.55	122.4	0.85	C	401
122.4	123.7	1.3	C	400
123.7	123.95	0.25	DC	400
123.95	125	1.05	R	
125	125.35	0.35	CBSH	420
125.35	129.65	4.3	R	
129.65	129.9	0.25	CBSH	
129.9	130.9	1	R	
130.9	131.05	0.15	CR	
131.05	131.2	0.15	R	
131.2	131.5	0.3	DC	440
131.5	133.8	2.3	R	
133.8	134.05	0.25	CBSH	442?
134.05	135.95	1.9	R	
135.95	136.65	0.7	CBSH	463
136.65	140.5	3.85	R	
140.5	140.8	0.3	CBSH	460?
140.8	143.75	2.95	R	
143.75	143.9	0.15	CBSH	483?
143.9	148.45	4.55	R	
148.45	149.05	0.6	С	480
149.05	149.35	0.3	DC	480
149.35	153.45	4.1	R	
153.45	153.75	0.3	CBSH	
153.75	159	5.25	R	
159	159.3	0.3	CBSH	
159.3	159.7	0.4	С	A7
159.7	159.9	0.2	DC	A7
159.9	167	7.1	R	
167	167.55	0.55	CBSH	
167.55	168.6	1.05	R	
168.6	168.9	0.3	CBSH	
168.9	169.95	1.05	R	
169.95	170.3	0.35	CBSH	
170.3	180.9	10.6	R	
180.9	181	0.1	CR	
181	181.4	0.4	C	A5

Table A-2:	Lithologica	1 interpretation	of geophysical logs	
From	То	Drilled thickness	Interpreted lithology	Name
Log interp	retation of W	/C18-03C (me	tres) continued	
181.4	189.8	8.4	R	
189.8	190	0.2	CR	
190	190.2	0.2	DC	A3
190.2	190.45	0.25	С	A3
190.45	192.5	2.05	R	
192.5	192.9	0.4	CBSH	
192.9	193.2	0.3	CR	A1
193.2	194.05	0.85	R	
194.05	194.45	0.4	CR	A0
194.45	215.9	21.45	R	
215.9	216.2	0.3	CBSH	
216.2	216.65	0.45	DC	511
216.65	217.2	0.55	R	
217.2	217.5	0.3	CR	510
217.5	218	0.5	R	
Log interp	retation of W	/C18-04C (me	tres)	
From	То	Drilled	Interpreted lithology	Name
		thickness		
0	14.5	14.5	DRIFT	DRIFT
14.5	25.5	11	R	BULLMOOSE
25.5	26	0.5	IRST	BULLMOOSE
26	30.1	4.1	R	BULLMOOSE
30.1	30.6	0.5	IRST	BULLMOOSE
30.6	46.45	15.85	R	BULLMOOSE
46.45	52.9	6.45	R	BLUESKY
52.9	53.16	0.26	R	
53.16	53.26	0.1	CBSH	
53.26	53.74	0.48	DC	BIRD
53.74	53.85	0.11	CR	BIRD
53.85	53.97	0.12	DC	BIRD
53.97	54.29	0.32	CR	BIRD
54.29	54.42	0.13	DC	BIRD
54.42	54.62	0.2	CR	
54.62	54.83	0.21	CBSH	
54.83	62.4	7.57	R	
62.4	62.7	0.3	CR	190
62.7	77.7	15	R	+

From	То	Drilled	Interpreted lithology	Name
		thickness		
Log inter	pretation of W	/C18-04C (me	tres) continued	
77.7	78	0.3	CBSH	170
78	82.74	4.74	R	
82.74	82.98	0.24	CR	
82.98	83.14	0.16	C	150
83.14	83.27	0.13	CR	150
83.27	83.33	0.06	DC	150
83.33	83.41	0.08	С	150
83.41	83.63	0.22	DC	150
83.63	83.82	0.19	CR	
83.82	84.36	0.54	CBSH	
84.36	89.7	5.34	R	
89.7	90	0.3	CR	130
90	95.44	5.44	R	
95.44	95.5	0.06	CBSH	
95.5	95.78	0.28	CR	111
95.78	95.9	0.12	DC	111
95.9	96.06	0.16	CR	111
96.06	96.26	0.2	CBSH	
96.26	97.5	1.24	R	
97.5	97.7	0.2	CBSH	
97.7	97.95	0.25	DC	110
97.95	98.04	0.09	С	110
98.04	98.21	0.17	DC	110
98.21	98.36	0.15	CBSH	
98.36	101.65	3.29	R	
101.65	101.83	0.18	CBSH	
101.83	101.93	0.1	CR	
101.93	103.01	1.08	С	101
103.01	105.85	2.84	С	100
105.85	105.94	0.09	DC	100
105.94	106.09	0.15	CBSH	
106.09	125.19	19.1	R	
125.19	125.31	0.12	CBSH	
125.31	125.5	0.19	R	
125.5	125.71	0.21	CBSH	
125.71	125.82	0.11	DC	201
125.82	126.78	0.96	С	201
126.78	127.03	0.25	DC	201
127.03	127.17	0.14	CR	

			of geophysical logs	
From	То	Drilled	Interpreted lithology	Name
		thickness		
Log interp	retation of W	C18-04C (me	tres) continued	
127.17	127.89	0.72	R	
127.89	128	0.11	CR	
128	128.09	0.09	DC	202
128.09	128.6	0.51	С	202
128.6	128.77	0.17	ASH	202
128.77	129.02	0.25	CR	202
129.02	129.48	0.46	С	202
129.48	129.7	0.22	CBSH	
129.7	140.2	10.5	R	
140.2	140.6	0.4	CBSH	310
140.6	141.76	1.16	R	
141.76	141.85	0.09	CBSH	
141.85	141.94	0.09	CR	
141.94	141.98	0.04	DC	300
141.98	142.64	0.66	С	300
142.64	142.85	0.21	FAULT	POSSIBLE
142.85	144.12	1.27	С	300
144.12	144.33	0.21	CBSH	
144.33	144.6	0.27	R	
144.6	144.66	0.06	CBSH	
144.66	144.74	0.08	CR	
144.74	145.02	0.28	DC	320
145.02	145.82	0.8	С	320
145.82	146.1	0.28	CBSH	
146.1	149.5	3.4	R	
149.5	150.25	0.75	CR	340
150.25	150.4	0.15	CBSH	340
150.4	150.55	0.15	CR	340
150.55	151.15	0.6	CBSH	340
151.15	155.45	4.3	R	
155.45	155.62	0.17	CBSH	360
155.62	180.3	24.68	R	
180.3	180.48	0.18	CBSH	410
180.48	180.9	0.42	R	
180.9	181	0.1	CBSH	
181	181.08	0.08	CR	
181.08	181.2	0.12	DC	401
181.2	182.63	1.43	С	401
182.63	183.02	0.39	С	400

From	То	Drilled thickness	Interpreted lithology	Name
Lagintam	matation of W		tuan) aantinuad	
183.02	183.1	0.08	tres) continued FAULT	POSSIBLE
183.1	187.56	4.46	C	400
183.1			DC	400
	187.65	0.09		
187.65	187.8	0.15	C	400
187.8	187.91	0.11	DC	400
187.91	188.01	0.1	CR	
188.01	188.1	0.09	CBSH	
188.1	191	2.9	R	120
191	191.4	0.4	CR	420
191.4	191.5	0.1	CBSH	
191.5	191.8	0.3	R	
191.8	192.2	0.4	CBSH	
192.2	198.14	5.94	R	
198.14	198.74	0.6	CBSH	
198.74	198.84	0.1	CR	
198.84	198.9	0.06	DC	440
198.9	199.12	0.22	С	440
199.12	199.16	0.04	DC	440
199.16	199.33	0.17	С	440
199.33	199.36	0.03	DC	440
199.36	199.46	0.1	C	440
199.46	199.55	0.09	DC	440
199.55	199.64	0.09	CR	
199.64	200.02	0.38	CBSH	
200.02	205.25	5.23	R	
205.25	205.7	0.45	CBSH	
205.7	205.9	0.2	CR	
205.9	206.3	0.4	CBSH	
206.3	206.75	0.45	R	
206.75	207	0.25	CBSH	
207	207.4	0.4	CR	463
207.4	207.5	0.1	CBSH	
207.5	213.7	6.2	R	
213.7	214.1	0.4	CBSH	460?
214.1	218.39	4.29	R	
218.39	219.25	0.86	CBSH	483?
219.25	220	0.75	R	
220	221	1	CBSH	
221	224.95	3.95	R	

Table A-2:	Lithologica	l interpretation	of geophysical logs	
From	То	Drilled thickness	Interpreted lithology	Name
Log interpo	retation of W	C18-04C (me	tres) continued	
224.95	225.12	0.17	CBSH	
225.12	225.19	0.07	DC	480
225.19	226.25	1.06	С	480
226.25	226.4	0.15	DC	480
226.4	226.71	0.31	CBSH	
226.71	232.7	5.99	R	
232.7	233.02	0.32	DC	
233.02	239	5.98	R	
Log interpo	retation of V	VC18-05C (me	etres)	
From	То	Drilled	Interpreted lithology	Name
		thickness		
0	7.15	7.15	DRIFT	DRIFT
7.15	10.5	3.35	R	
10.5	10.85	0.35	CBSH	130
10.85	13.83	2.98	R	
13.83	14.04	0.21	CBSH	
14.04	14.18	0.14	DC	111
14.18	14.42	0.24	CR	
14.42	14.52	0.1	CBSH	
14.52	15.46	0.94	R	
15.46	15.6	0.14	CBSH	
15.6	15.94	0.34	С	110
15.94	16.14	0.2	CBSH	
16.14	17.8	1.66	R	
17.8	17.93	0.13	CBSH	
17.93	18.95	1.02	С	101
18.95	20.87	1.92	С	100
20.87	20.95	0.08	DC	
20.95	21.2	0.25	CBSH	
21.2	28.44	7.24	R	
28.44	28.56	0.12	CR	
28.56	29.21	0.65	С	201
29.21	29.31	0.1	DC	201
29.31	29.5	0.19	CBSH	
29.5	30.09	0.59	R	
30.09	30.3	0.21	CBSH	
30.3	30.51	0.21	С	202

Table A-2			of geophysical logs	
From	To	Drilled	Interpreted lithology	Name
		thickness		
	retation of V	VC18-05C (me	tres) continued	
30.51	30.6	0.09	CR	
30.6	30.72	0.12	CBSH	
30.72	35.3	4.58	R	
35.3	35.7	0.4	CBSH	310
35.7	36	0.3	R	310
36	36.4	0.4	CBSH	310
36.4	40.9	4.5	R	
40.9	41.16	0.26	CBSH	
41.16	41.28	0.12	C	300
41.28	41.35	0.07	ASH?	300
41.35	41.53	0.18	С	300
41.53	41.7	0.17	CR	
41.7	41.8	0.1	CBSH	
41.8	45.39	3.59	R	
45.39	45.62	0.23	CBSH	
45.62	45.8	0.18	С	320
45.8	46.04	0.24	CBSH	
46.04	47.05	1.01	R	
47.05	47.2	0.15	IRST	IRONSTONE
47.2	48.02	0.82	R	
48.02	48.23	0.21	CBSH	340
48.23	48.36	0.13	CR	340
48.36	48.53	0.17	CBSH	340
48.53	48.74	0.21	R	340
48.74	49.42	0.68	CBSH	340
49.42	52.3	2.88	R	
52.3	52.6	0.3	CBSH	360
52.6	70.52	17.92	R	
70.52	70.7	0.18	CBSH	
70.7	70.88	0.18	DC	410
70.88	71.03	0.15	CBSH	
71.03	71.28	0.25	R	
71.28	71.48	0.2	CBSH	
71.48	72.3	0.82	С	401
72.3	73.24	0.94	С	400
73.24	73.35	0.11	DC	400
73.35	73.51	0.16	CR	
73.51	73.7	0.19	CBSH	
73.7	74.6	0.9	С	420

From	То	Drilled	Interpreted lithology	Name
		thickness		
Log interp	oretation of W	/C18-05C (me	tres) continued	
74.6	74.68	0.08	DC	420
74.68	74.8	0.12	CR	
74.8	75.21	0.41	CBSH	
75.21	77.16	1.95	R	
77.16	77.32	0.16	CBSH	
77.32	77.42	0.1	DC	440
77.42	77.53	0.11	С	440
77.53	77.63	0.1	DC	440
77.63	77.75	0.12	С	440
77.75	77.94	0.19	DC	440
77.94	78.12	0.18	CBSH	
78.12	80.45	2.33	R	
80.45	80.7	0.25	CBSH	442
80.7	88.2	7.5	R	
88.2	88.6	0.4	CBSH	
88.6	89.05	0.45	R	
89.05	89.6	0.55	CBSH	463
89.6	93.4	3.8	R	
93.4	93.55	0.15	CBSH	
93.55	93.85	0.3	CR	460
93.85	102.3	8.45	R	
102.3	102.54	0.24	CBSH	
102.54	103.13	0.59	С	480
103.13	103.35	0.22	DC	480
103.35	103.54	0.19	CBSH	
103.54	104.73	1.19	R	
104.73	105.2	0.47	CBSH	
105.2	107.76	2.56	R	
107.76	108.14	0.38	CBSH	
108.14	113.65	5.51	R	
113.65	113.81	0.16	CBSH	
113.81	113.94	0.13	CR	
113.94	114.78	0.84	С	A7
114.78	115.03	0.25	CBSH	
115.03	122.35	7.32	R	
122.35	123	0.65	CBSH	A5?
123	124.99	1.99	R	

Table A-2	Lithologica	al interpretation	of geophysical logs	
From	То	Drilled thickness	Interpreted lithology	Name
Log interp	retation of V	WC18-06C (me	tres)	
0	2.4	2.4	DRIFT	DRIFT
2.4	4.65	2.25	R	
4.65	4.9	0.25	DC	130
4.9	5.1	0.2	CR	130
5.1	5.4	0.3	С	130
5.4	5.6	0.2	CBSH	
5.6	8.76	3.16	R	
8.76	8.94	0.18	CBSH	
8.94	9.25	0.31	С	111
9.25	9.4	0.15	CBSH	
9.4	10.32	0.92	R	
10.32	10.43	0.11	CR	
10.43	10.84	0.41	С	110
10.84	11.03	0.19	CR	
11.03	14.8	3.77	R	
14.8	15.05	0.25	CBSH	
15.05	17.16	2.11	R	
17.16	17.34	0.18	CBSH	
17.34	17.85	0.51	С	101
17.85	19.37	1.52	С	100
19.37	19.47	0.1	DC	100
19.47	19.58	0.11	CR	
19.58	22.9	3.32	R	
22.9	23.24	0.34	CBSH	
23.24	23.42	0.18	CR	
23.42	24	0.58	С	201
24	24.07	0.07	DC	201
24.07	24.22	0.15	CR	
24.22	24.62	0.4	CBSH	
24.62	27.23	2.61	R	
27.23	27.35	0.12	CBSH	
27.35	27.44	0.09	CR	
27.44	27.66	0.22	С	202
27.66	27.7	0.04	DC	202
27.7	27.88	0.18	CR	202
27.88	28.04	0.16	ASH	202
28.04	28.18	0.14	С	202
28.18	28.3	0.12	CR	
28.3	28.37	0.07	CBSH	

From	To	Drilled	Interpreted lithology	Name
		thickness		
			tres) continued	
28.37	32.8	4.43	R	
32.8	33.1	0.3	CBSH	
33.1	35	1.9	R	
35	35.65	0.65	CBSH	
35.65	36.9	1.25	R	
36.9	37.3	0.4	CBSH	
37.3	40.24	2.94	R	
40.24	40.42	0.18	CR	
40.42	40.64	0.22	DC	300
40.64	40.77	0.13	CR	300
40.77	40.97	0.2	DC	300
40.97	41.13	0.16	CBSH	
41.13	45.25	4.12	R	
45.25	45.6	0.35	CR	320
45.6	45.9	0.3	CBSH	320
45.9	48.3	2.4	R	
48.3	48.6	0.3	CR	340
48.6	49	0.4	R	340
49	49.7	0.7	CBSH	340
49.7	70.5	20.8	R	
70.5	70.62	0.12	CBSH	
70.62	70.83	0.21	CR	410
70.83	70.95	0.12	CBSH	
70.95	71.84	0.89	R	
71.84	71.96	0.12	CBSH	
71.96	72.63	0.67	С	401
72.63	74.84	2.21	С	400
74.84	75.2	0.36	DC	400
75.2	75.34	0.14	CBSH	
75.34	75.85	0.51	R	
75.85	76.22	0.37	CBSH	420
76.22	78.74	2.52	R	1.20
78.74	78.84	0.1	CBSH	
78.84	78.95	0.11	DC	440
78.95	79.14	0.19	C	440
79.14	79.22	0.08	DC	440
79.22	79.39	0.17	CBSH	110
79.39	80.74	1.35	R	
80.74	80.74	0.2	CBSH	442

Table A-2:	Lithological	interpretation	of geophysical logs	
From	То	Drilled	Interpreted lithology	Name
		thickness		
Log interpr	retation of Wo	C18-06C (me	tres) continued	
80.94	87.1	6.16	R	
87.1	87.35	0.25	CBSH	463
87.35	91.4	4.05	R	
91.4	91.8	0.4	CBSH	460
91.8	102.43	10.63	R	
102.43	102.77	0.34	CBSH	
102.77	103.19	0.42	R	
103.19	103.33	0.14	CBSH	
103.33	103.43	0.1	CR	
103.43	104.12	0.69	С	480
104.12	104.28	0.16	DC	480
104.28	104.48	0.2	CR	
104.48	104.59	0.11	CBSH	
104.59	107.6	3.01	R	
107.6	107.8	0.2	CBSH	
107.8	114.7	6.9	R	
114.7	115.05	0.35	CBSH	A71?
115.05	118.28	3.23	R	
118.28	118.37	0.09	CBSH	
118.37	118.44	0.07	CR	
118.44	118.53	0.09	DC	A7?
118.53	118.68	0.15	С	A7?
118.68	118.78	0.1	CR	
118.78	118.85	0.07	CBSH	
118.85	121.44	2.59	R	
121.44	121.93	0.49	CBSH	
121.93	122.23	0.3	R	
122.23	122.37	0.14	CBSH	
122.37	122.53	0.16	CR	
122.53	122.77	0.24	DC	A5
122.77	123.1	0.33	CR	A5
123.1	123.32	0.22	DC	A5
123.32	124.2	0.88	C	A5
124.2	124.3	0.1	DC	A5
124.3	124.76	0.46	CR	
124.76	124.95	0.19	CBSH	
124.95	141.4	16.45	R	
141.4	141.7	0.3	CBSH	
141.7	141.9	0.2	R	

Table A-2:	Lithologica	1 interpretation	of geophysical logs	
From	То	Drilled thickness	Interpreted lithology	Name
Log interpr	retation of W	/C18-06C (me	tres) continued	
141.9	142.2	0.3	CBSH	A3
142.2	147.05	4.85	R	
147.05	147.35	0.3	CBSH	A1?
147.35	147.85	0.5	R	
147.85	148.5	0.65	CBSH	A0?
148.5	149.2	0.7	R	
Log interpr	retation of W	/C18-07C (me	tres)	
From	То	Drilled	Interpreted lithology	Name
		thickness		
0	3.9	3.9	DRIFT	DRIFT
3.9	5.9	2	R	
5.9	6.1	0.2	CBSH	
6.1	6.3	0.2	DC	150
6.3	6.4	0.1	CBSH	150
6.4	6.6	0.2	CR	150
6.6	6.8	0.2	DC	150
6.8	7.15	0.35	CBSH	
7.15	11.2	4.05	R	
11.2	11.6	0.4	CBSH	130
11.6	14.8	3.2	R	
14.8	15	0.2	CBSH	
15	15.3	0.3	C	111
15.3	15.45	0.15	CBSH	
15.45	16.4	0.95	R	
16.4	16.6	0.2	CBSH	110
16.6	17.15	0.55	C	
17.15	17.4	0.25	CBSH	
17.4	24.2	6.8	R	
24.2	24.45	0.25	CBSH	
24.45	25.08	0.63	С	101
25.08	26.42	1.34	С	100
26.42	26.7	0.28	CR	
26.7	27	0.3	CBSH	
27	29.9	2.9	R	
29.9	30.15	0.25	CBSH	
30.15	30.7	0.55	С	201
30.7	31	0.3	DC	201

From	То	al interpretation Drilled	Interpreted lithology	Name
		thickness		
			tres) continued	
31	34.4	3.4	R	
34.4	34.75	0.35	С	202
34.75	34.9	0.15	CR	202
34.9	35	0.1	DC	202
35	35.12	0.12	CR	202
35.12	35.42	0.3	С	202
35.42	42.05	6.63	R	
42.05	42.3	0.25	CBSH	
42.3	43.2	0.9	R	
43.2	43.6	0.4	CBSH	
43.6	46.4	2.8	R	
46.4	46.55	0.15	CR	
46.55	46.65	0.1	DC	300
46.65	47.2	0.55	C	300
47.2	51.2	4	R	
51.2	51.5	0.3	CBSH	320
51.5	51.65	0.15	CR	320
51.65	52.1	0.45	CBSH	320
52.1	53.65	1.55	R	
53.65	54.08	0.43	CBSH	340
54.08	54.4	0.32	CR	340
54.4	55.35	0.95	CBSH	340
55.35	76.05	20.7	R	
76.05	76.5	0.45	CR	410
76.5	77.25	0.75	R	
77.25	77.42	0.17	CBSH	
77.42	77.72	0.3	С	401
77.72	78.74	1.02	С	400
78.74	79	0.26	DC	400
79	80.8	1.8	R	
80.8	81.25	0.45	DC	420
81.25	86.08	4.83	R	
86.08	86.3	0.22	CBSH	
86.3	86.55	0.25	CR	440
86.55	86.7	0.15	CBSH	
86.7	87.15	0.45	R	
87.15	87.52	0.37	CBSH	442
87.52	91.65	4.13	R	
91.65	92.02	0.37	CR	463?

From	То	Drilled	Interpreted lithology	Name
		thickness		
			tres) continued	
92.02	94.05	2.03	R	
94.05	94.6	0.55	CBSH	
94.6	97.05	2.45	R	
97.05	97.45	0.4	CBSH	
97.45	97.6	0.15	CR	460
97.6	97.8	0.2	CBSH	
97.8	99.9	2.1	R	
99.9	100	0.1	FAULT	POSSIBLE
100	108.9	8.9	R	
108.9	109	0.1	CBSH	460
109	121.4	12.4	R	
121.4	121.65	0.25	CBSH	
121.65	122.05	0.4	CR	480
122.05	122.2	0.15	CBSH	480
122.2	122.45	0.25	CR	480
122.45	122.9	0.45	DC	480
122.9	123.1	0.2	CBSH	
123.1	128.4	5.3	R	
128.4	128.7	0.3	CR	
128.7	133.1	4.4	R	
133.1	133.45	0.35	CBSH	A71?
133.45	135.1	1.65	R	
135.1	135.6	0.5	CBSH	
135.6	135.8	0.2	R	
135.8	136	0.2	CBSH	
136	136.5	0.5	С	A7
136.5	136.65	0.15	DC	A7
136.65	136.9	0.25	CBSH	
136.9	144.6	7.7	R	
144.6	145.4	0.8	CBSH	
145.4	150.35	4.95	R	
150.35	150.65	0.3	CR	
150.65	151.25	0.6	R	
151.25	151.65	0.4	CBSH	
151.65	153.85	2.2	R	
153.85	154.1	0.25	CBSH	
154.1	154.7	0.6	С	A5
154.7	154.95	0.25	DC	A5
154.95	155.2	0.25	CBSH	

Table A-2:	Lithological	interpretation	of geophysical logs	
From	То	Drilled	Interpreted lithology	Name
		thickness		
Log interpre	etation of WC	C18-07C (met	tres) continued	
155.2	160.4	5.2	R	
160.4	160.8	0.4	CBSH	
160.8	161	0.2	R	
161	161.28	0.28	CBSH	
161.28	161.48	0.2	C	A3
161.48	161.75	0.27	DC	A3
161.75	162.2	0.45	CBSH	
162.2	162.45	0.25	R	
162.45	162.65	0.2	CR	
162.65	162.9	0.25	С	A1
162.9	163.1	0.2	CR	
163.1	163.9	0.8	CBSH	
163.9	164.2	0.3	CR	
164.2	164.3	0.1	DC	A0
164.3	164.5	0.2	CBSH	
164.5	166.93	2.43	R	
Log interpre	etation of WC	C18-08C (met	tres)	
From	То	Drilled	Interpreted lithology	Name
<u> </u>		thickness		
0	2.55	2.55	DRIFT	DRIFT
2.55	2.9	0.35	R	
2.9	3.55	0.65	CBSH	310?
3.55	12.4	12.95	R	
12.4	12.5	0.1	IRST	IRONSTONE
12.5	12.65	0.15	R	
12.65	12.75	0.1	IRST	IRONSTONE
12.75	16.5	3.75	R	
16.5	17.1	0.6	CBSH	
17.1	17.6	0.5	R	
17.6	17.65	0.05	CBSH	
17.65	18.05	0.4	DC	300
18.05	18.1	0.05	CBSH	
18.1	21.05	2.95	R	
21.05	21.45	0.4	CBSH	320
21.45	24.1	2.65	R	
∠1. <del>4</del> J	4 <b>7.</b> 1	4.05		
24.1	24.6	0.5	CBSH	340

From	To	Drilled	Interpreted lithology	Name
		thickness		
			tres) continued	
24.7	24.95	0.25	CBSH	340
24.95	25.4	0.45	R	340
25.4	26.1	0.7	CBSH	340
26.1	30.4	4.3	R	
30.4	30.85	0.45	CBSH	360
30.85	46.7	15.85	R	
46.7	47.1	0.4	CR	410
47.1	48.3	1.2	R	
48.3	48.5	0.2	CBSH	
48.5	49.1	0.6	С	401
49.1	49.2	0.1	FAULT	ESTABLISHED
49.2	49.3	0.1	R	
49.3	49.55	0.25	CBSH	
49.55	49.6	0.05	DC	401
49.6	50.75	1.15	С	401
50.75	50.85	0.1	FAULT	ESTABLISHED
50.85	50.9	0.05	DC	401
50.9	52.2	1.3	С	401
52.2	52.7	0.5	DC	400
52.7	54.8	2.1	С	400
54.8	55.1	0.3	FAULT	PROBABLE
55.1	55.25	0.15	CBSH	
55.25	55.4	0.15	R	
55.4	55.65	0.25	CBSH	
55.65	56.1	0.45	С	420
56.1	58.6	2.5	R	
58.6	58.85	0.25	CBSH	
58.85	59.5	0.65	С	440
59.5	59.7	0.2	CBSH	
59.7	60.9	1.2	R	
60.9	61.3	0.4	CBSH	442
61.3	71.25	9.95	R	
71.25	71.45	0.2	CBSH	463
71.45	75.95	4.5	R	
75.95	76.1	0.15	CBSH	
76.1	76.5	0.4	DC	460
76.5	76.6	0.1	CBSH	
76.6	78.1	1.5	R	
78.1	78.5	0.4	CBSH	

			of geophysical logs	
From	То	Drilled	Interpreted lithology	Name
		thickness		
			tres) continued	
78.5	79.6	1.1	R	
79.6	80	0.4	CBSH	
80	83.4	3.4	R	
83.4	83.8	0.4	CBSH	
83.8	85.95	2.15	R	
85.95	86.2	0.25	CBSH	
86.2	86.5	0.3	DC	480
86.5	86.9	0.4	С	480
86.9	87.1	0.2	DC	480
87.1	87.4	0.3	CBSH	
87.4	89.4	2	R	
89.4	89.75	0.35	CBSH	
89.75	91.4	1.65	R	
91.4	91.7	0.3	CBSH	
91.7	92.87	1.17	R	
92.87	93.3	0.43	DC	A71
93.3	94.55	1.25	R	
94.55	95.18	0.63	С	A7
95.18	95.4	0.22	CR	
95.4	101.05	5.65	R	
Log interr	oretation of W	/C18-09C (me	tres)	
From	То	Drilled	Interpreted lithology	Name
		thickness		
0	0.5	0.5	DRIFT	DRIFT
0.5	2	1.5	R	
2	2.35	0.35	DC	111
2.35	2.55	0.2	CR	
2.55	2.75	0.2	CBSH	
2.75	2.85	0.1	R	
2.85	2.95	0.1	CBSH	
2.95	3.5	0.55	R	
3.5	3.7	0.2	CR	
3.7	4	0.3	C	110
4	4.25	0.25	CBSH	
4.25	9.8	5.55	R	
9.8	10	0.2	CR	
10	10.55	0.55	C	101

Table A-2	Lithologica	al interpretation	of geophysical logs	
From	То	Drilled thickness	Interpreted lithology	Name
Log interp	retation of V		tres) continued	
10.55	11.95	1.4	C	100
11.95	12.05	0.1	DC	100
12.05	13.05	1	CBSH	
13.05	15	1.95	R	
15	15.3	0.3	CBSH	
15.3	15.4	0.1	CR	
15.4	15.5	0.1	CBSH	
15.5	15.6	0.1	DC	201
15.6	15.7	0.1	CR	201
15.7	15.98	0.28	DC	201
15.98	16.95	0.97	С	201
16.95	17.15	0.2	CBSH	
17.15	20.6	3.45	R	
20.6	20.9	0.3	CBSH	
20.9	21.1	0.2	С	202
21.1	21.3	0.2	CR	202
21.3	21.4	0.1	DC	202
21.4	21.55	0.15	CR	202
21.55	21.7	0.15	С	202
21.7	21.95	0.25	CBSH	
21.95	28	6.05	R	
28	28.4	0.4	CBSH	
28.4	30.8	2.4	R	
30.8	31.2	0.4	CBSH	310
31.2	31.3	0.1	ASH	310
31.3	31.4	0.1	CBSH	310
31.4	37.1	5.7	R	
37.1	37.3	0.2	CBSH	
37.3	37.6	0.3	С	300
37.6	37.9	0.3	CBSH	
37.9	40.8	2.9	R	
40.8	41	0.2	CR	320
41	41.3	0.3	CBSH	320
41.3	43.75	2.45	R	
43.75	44.5	0.75	CBSH	340
44.5	45.2	0.7	R	340
45.2	45.65	0.45	CBSH	340
45.65	50.15	4.5	R	
50.15	50.5	0.35	CBSH	360

From	То	Drilled	of geophysical logs Interpreted lithology	Name
		thickness		
Log interp	pretation of W	/C18-09C (me	tres) continued	
50.5	65.55	15.05	R	
65.55	66	0.45	CBSH	430
66	67.4	1.4	R	
67.4	67.6	0.2	CR	
67.6	68.15	0.55	С	410
68.15	68.65	0.5	CBSH	
68.65	68.8	0.15	DC	401
68.8	69.97	1.17	С	401
69.97	70.02	0.05	DC	400
70.02	71.3	1.28	С	400
71.3	71.5	0.2	DC	400
71.5	72.1	0.6	R	
72.1	72.3	0.2	CBSH	
72.3	72.6	0.3	DC	420
72.6	72.8	0.2	CR	
72.8	75.8	3	R	
75.8	75.95	0.15	CR	
75.95	76.1	0.15	DC	440
76.1	76.28	0.18	С	440
76.28	76.4	0.12	DC	440
76.4	76.5	0.1	С	440
76.5	76.65	0.15	DC	440
76.65	76.8	0.15	С	440
76.8	77	0.2	CBSH	
77	78.3	1.3	R	
78.3	78.7	0.4	CBSH	442
78.7	82.8	4.1	R	
82.8	83	0.2	CBSH	
83	83.3	0.3	R	
83.3	83.7	0.4	CBSH	463
83.7	87.95	4.25	R	
87.95	88.4	0.45	CBSH	460
88.4	99.75	11.35	R	
99.75	100	0.25	CBSH	
100	100.65	0.65	С	480
100.65	100.9	0.25	DC	480
100.9	101.1	0.2	CBSH	
101.1	106.3	5.2	R	
106.3	106.7	0.4	CBSH	

Table A-2:	Lithological	interpretation	of geophysical logs	
From	То	Drilled	Interpreted lithology	Name
		thickness		
	etation of Wo	C18-09C (me	tres) continued	
106.7	107.85	1.15	R	
107.85	107.95	0.1	CBSH	
107.95	108.15	0.2	DC	A71
108.15	108.4	0.25	CBSH	
108.4	108.9	0.5	R	
108.9	109.12	0.22	CBSH	
109.12	109.75	0.63	С	A7
109.75	110.2	0.45	DC	A7
110.2	116.4	6.2	R	
116.4	116.85	0.45	CBSH	
116.85	117.1	0.25	CR	
117.1	117.3	0.2	CBSH	
117.3	121.9	4.6	R	
121.9	122.1	0.2	CBSH	
122.1	122.3	0.2	CR	
122.3	122.4	0.1	CBSH	
122.4	122.9	0.5	R	
122.9	123.3	0.4	CBSH	
123.3	124.93	1.63	R	
Log interpre	etation of Wo	C18-10C (me	tres)	
From	То	Drilled	Interpreted lithology	Name
		thickness		
0	4.6	4.6	DRIFT	DRIFT
4.6	6.8	2.2	R	
6.8	7.1	0.3	CBSH	
7.1	7.2	0.1	С	150
7.2	7.3	0.1	CR	150
7.3	7.45	0.15	С	150
7.45	7.65	0.2	CR	150
7.65	7.8	0.15	DC	150
7.8	8.95	1.15	CBSH	
8.95	12.5	3.55	R	
12.5	12.9	0.4	CBSH	130
12.9	15.75	2.85	R	
15.75	15.95	0.2	CBSH	111
15.95	16.1	0.15	R	111
16.1	16.6	0.5	CBSH	111

			n of geophysical logs	
From	То	Drilled thickness	Interpreted lithology	Name
Lasintan	matation of V		tuna) antinuad	
	17.15		tres) continued	
16.6 17.15	17.15	0.55	R	
			CBSH	110
17.35	17.7	0.35	C	110
17.7	17.9	0.2	CBSH	
17.9	20	2.1	R	
20	20.3	0.3	CBSH	101
20.3	21.09	0.79	C	101
21.09	21.14	0.05	DC	100
21.14	23.1	1.96	С	100
23.1	26.95	3.85	R	
26.95	27.5	0.55	CBSH	
27.5	28.1	0.6	С	201
28.1	28.25	0.15	DC	201
28.25	28.4	0.15	CBSH	
28.4	30.65	2.25	R	
30.65	30.95	0.3	CBSH	
30.95	31.1	0.15	C	202
31.1	31.4	0.3	DC	202
31.4	31.5	0.1	CR	202
31.5	31.6	0.1	DC	202
31.6	31.85	0.25	CBSH	
31.85	39.4	7.55	R	
39.4	39.95	0.55	CBSH	
39.95	40.1	0.15	R	
40.1	40.7	0.6	CBSH	
40.7	42.8	2.1	R	
42.8	43.05	0.25	CBSH	
43.05	43.6	0.55	С	300
43.6	43.85	0.25	CBSH	
43.85	47.7	3.85	R	
47.7	47.95	0.25	CBSH	
47.95	48.4	0.45	DC	320
48.4	48.65	0.25	CBSH	-
48.65	51.05	2.4	R	
51.05	51.8	0.75	CBSH	340
51.8	52.5	0.7	R	340
52.5	53.2	0.7	CBSH	340
53.2	68.65	15.45	R	
68.65	68.75	0.1	FAULT	POSSIBLE

From	To	Drilled	of geophysical logs Interpreted lithology	Name
		thickness	T I I I I I I I I I I I I I I I I I I I	
Log interp	pretation of W	/C18-10C (me	tres) continued	
68.75	73.6	4.85	R	
73.6	73.75	0.15	CBSH	430
73.75	76.18	2.43	R	
76.18	76.23	0.05	CBSH	410
76.23	76.4	0.17	R	
76.4	76.68	0.28	CR	
76.68	78.48	1.8	С	401
78.48	78.53	0.05	DC	400
78.53	81.08	2.55	С	400
81.08	81.28	0.2	CBSH	
81.28	83.8	2.52	R	
83.8	84.25	0.45	CR	420
84.25	86.2	1.95	R	
86.2	86.4	0.2	CBSH	
86.4	86.75	0.35	С	440
86.75	86.9	0.15	DC	440
86.9	87.05	0.15	С	440
87.05	87.25	0.2	DC	440
87.25	87.4	0.15	CBSH	
87.4	88.7	1.3	R	
88.7	89.2	0.5	CBSH	442
89.2	92.4	3.2	R	
92.4	92.85	0.45	CBSH	
92.85	93.15	0.3	R	
93.15	93.55	0.4	CBSH	463
93.55	97.5	3.95	R	
97.5	98	0.5	CBSH	460
98	108.9	10.9	R	
108.9	109.15	0.25	CBSH	
109.15	109.95	0.8	C	480
109.95	110.1	0.15	DC	480
110.1	110.35	0.25	CBSH	
110.35	115.4	5.05	R	
115.4	115.8	0.4	CBSH	
115.8	116.65	0.85	R	
116.65	116.85	0.2	CBSH	
116.85	117	0.15	С	A71
117	117.2	0.2	CBSH	
117.2	117.6	0.4	R	

From	То	Drilled	of geophysical logs Interpreted lithology	Name
		thickness		
Log interp	pretation of W	/C18-10C (me	tres) continued	
117.6	117.85	0.25	CBSH	
117.85	118.4	0.55	С	A7
118.4	118.6	0.2	DC	A7
118.6	118.9	0.3	CBSH	
118.9	125.55	6.65	R	
125.55	126.35	0.8	CBSH	
126.35	131.4	5.05	R	
131.4	131.6	0.2	CBSH	
131.6	131.85	0.25	CR	
131.85	132.55	0.7	R	
132.55	132.9	0.35	CBSH	
132.9	137.1	4.2	R	
137.1	137.4	0.3	CBSH	
137.4	138.15	0.75	С	A5
138.15	138.4	0.25	CBSH	
138.4	141.7	3.3	R	
141.7	142.2	0.5	CBSH	
142.2	142.6	0.4	R	
142.6	142.8	0.2	CBSH	
142.8	143.05	0.25	CR	
143.05	143.2	0.15	С	A3
143.2	143.3	0.1	DC	A3
143.3	143.4	0.1	С	A3
143.4	143.6	0.2	CR	
143.6	144.2	0.6	CBSH	
144.2	144.4	0.2	C	A1
144.4	144.9	0.5	CBSH	
144.9	145.2	0.3	R	
145.2	145.45	0.25	CBSH	
145.45	145.9	0.45	CR	A0
145.9	155.6	9.7	R	
155.6	155.75	0.15	CBSH	
155.75	165.4	9.65	R	
165.4	165.6	0.2	DC	530
165.6	165.8	0.2	С	530
165.8	166.1	0.3	CBSH	
166.1	166.8	0.7	R	
166.8	167.2	0.4	CBSH	510
167.2	168.7	1.5	R	

Table A-2:	Lithological	linterpretation	of geophysical logs	
From	То	Drilled	Interpreted lithology	Name
		thickness		
	etation of W	C18-10C (me	tres) continued	
168.7	168.95	0.25	CBSH	
168.95	169.8	0.85	C	501
169.8	170	0.2	CBSH	
170	170.4	0.4	R	
170.4	170.6	0.2	CBSH	
170.6	171.05	0.45	C	502
171.05	171.3	0.25	CBSH	
171.3	174.4	3.1	R	
174.4	174.8	0.4	CBSH	520
174.8	176.15	1.35	R	
176.15	176.4	0.25	CR	
176.4	176.6	0.2	CBSH	
176.6	176.95	0.35	R	
176.95	177.15	0.2	CR	
177.15	177.4	0.25	С	540
177.4	177.6	0.2	CBSH	
177.6	179.3	1.7	R	
179.3	179.7	0.4	CBSH	
179.7	189.45	9.75	R	
189.45	189.7	0.25	CBSH	
189.7	189.9	0.2	С	630
189.9	190.2	0.3	CR	
190.2	190.85	0.65	R	
190.85	191.05	0.2	CBSH	
191.05	191.2	0.15	CR	
191.2	191.4	0.2	DC	610
191.4	191.5	0.1	CBSH	
191.5	191.6	0.1	CR	
191.6	191.9	0.3	CBSH	
191.9	192.3	0.4	R	
192.3	192.5	0.2	CBSH	
192.5	193.4	0.9	С	601
193.4	193.6	0.2	DC	601
193.6	193.8	0.2	CBSH	
193.8	194	0.2	CR	
194	194.65	0.65	С	600
194.65	194.9	0.25	CBSH	
194.9	197.4	2.5	R	
197.4	197.85	0.45	CBSH	

From	To	Drilled	of geophysical logs Interpreted lithology	Name
1 10111	10	thickness	interpreted ittiology	Ivame
Log interr	oretation of W		tres) continued	
197.85	199.3	1.45	R	
199.3	199.75	0.45	CBSH	
199.75	204.1	4.35	R	
204.1	204.6	0.5	CBSH	770
204.6	207.4	2.8	R	
207.4	207.6	0.2	CBSH	
207.6	207.8	0.2	CR	750
207.8	208.65	0.85	R	
208.65	209.1	0.45	CBSH	
209.1	211.55	2.45	R	
211.55	211.8	0.25	CR	
211.8	212	0.2	C	730
212	212.15	0.15	CBSH	
212.15	213.9	1.75	R	
213.9	214.05	0.15	CBSH	
214.05	214.25	0.2	CR	710
214.25	214.4	0.15	CBSH	
214.4	215.35	0.95	R	
Log interp	oretation of W	VC18-11C (me	tres)	
From	То	Drilled	Interpreted lithology	Name
		thickness	DDIE	DDVE
0	3	3	DRIFT	DRIFT
3	10.4	7.4	R	
10.4	11.3	0.9	CBSH	
11.3	14.7	3.4	R	
14.7	15.2	0.5	CBSH	
15.2	15.4	0.2	CR	200
15.4	15.6	0.2	C	300
15.6	15.8	0.2	CR	
15.8	19	3.2	R	220
19	19.7	0.7	CBSH	320
19.7	22.15	2.45	R	240
22.15	23.05	0.9	CBSH	340
23.05	23.85	0.8	R	340
23.85	24.65	0.8	CBSH	340
24.65	28.5	3.85	R	
28.5	28.55	0.05	CBSH	

From	То	Drilled	Interpreted lithology	Name
		thickness		
			tres) continued	
28.55	28.65	0.1	FAULT	POSSIBLE
28.65	28.7	0.05	CBSH	
28.7	42.95	14.25	R	
42.95	43.25	0.3	CBSH	
43.25	43.7	0.45	R	
43.7	43.95	0.25	CR	430
43.95	44.2	0.25	CBSH	
44.2	44.35	0.15	R	
44.35	44.4	0.05	FAULT	POSSIBLE
44.4	46.3	1.9	R	
46.3	46.5	0.2	CBSH	
46.5	47.2	0.7	C	410
47.2	47.45	0.25	CBSH	
47.45	47.9	0.45	R	
47.9	48.15	0.25	CBSH	
48.15	48.4	0.25	CR	
48.4	49.65	1.25	С	401
49.65	49.7	0.05	DC	401
49.7	49.9	0.2	С	401
49.9	49.95	0.05	DC	400
49.95	52.13	2.18	С	400
52.13	52.28	0.15	DC	400
52.28	52.4	0.12	С	400
52.4	52.5	0.1	CR	
52.5	52.62	0.12	DC	420
52.62	52.8	0.18	CR	420
52.8	52.95	0.15	DC	420
52.95	53.05	0.1	CR	
53.05	53.3	0.25	CBSH	
53.3	55.15	1.85	R	
55.15	55.42	0.27	CBSH	
55.42	55.6	0.18	С	440
55.6	55.85	0.25	DC	440
55.85	56	0.15	С	440
56	56.1	0.1	DC	440
56.1	56.3	0.2	С	440
56.3	56.5	0.2	CBSH	
56.5	58.15	1.65	R	
58.15	58.65	0.5	CBSH	442

From	То	l interpretation Drilled	Interpreted lithology	Name
		thickness		
Log inter	pretation of W	VC18-11C (me	tres) continued	
58.65	66.25	7.6	R	
66.25	66.85	0.6	CBSH	463
66.85	70.6	3.75	R	
70.6	70.75	0.15	CBSH	
70.75	70.9	0.15	CR	460
70.9	71.02	0.12	DC	460
71.02	71.3	0.28	CBSH	
71.3	74.65	3.35	R	
74.65	75.02	0.37	CBSH	
75.02	75.8	0.78	R	
75.8	75.95	0.15	CBSH	
75.95	78.95	3	R	483
78.95	79.32	0.37	CBSH	
79.32	81.9	2.58	R	
81.9	82.15	0.25	CBSH	
82.15	82.8	0.65	С	480
82.8	83	0.2	DC	480
83	83.2	0.2	CBSH	
83.2	83.85	0.65	R	
83.85	84.05	0.2	CBSH	
84.05	85.05	1	R	
85.05	85.5	0.45	CBSH	
85.5	87.5	2	R	
87.5	87.85	0.35	CBSH	
87.85	88.3	0.45	R	
88.3	88.6	0.3	DC	A71
88.6	88.8	0.2	CBSH	
88.8	89.7	0.9	R	
89.7	89.98	0.28	CR	
89.98	90.65	0.67	С	A7
90.65	90.9	0.25	DC	A7
90.9	91.1	0.2	CBSH	
91.1	98	6.9	R	
98	98.8	0.8	CBSH	
98.8	99.1	0.3	CR	A5
99.1	99.2	0.1	DC	A5
99.2	99.45	0.25	CBSH	
99.45	100.2	0.75	R	
100.2	100.55	0.35	CBSH	

From	То	Drilled	of geophysical logs Interpreted lithology	Name
110111		thickness	interpreted numerogy	T (diffe
Log inter	pretation of V		tres) continued	
100.55	101	0.45	R	
Log inter	pretation of V	VC18-12C (me	tres)	
From	То	Drilled	Interpreted lithology	Name
		thickness		
0	4.3	4.3	DRIFT	DRIFT
4.3	15.25	10.95	R	
15.25	15.5	0.25	IRST	IRONSTONE
15.5	15.8	0.3	CBSH	
15.8	16.45	0.65	R	
16.45	16.8	0.35	CBSH	170
16.8	21.6	4.8	R	
21.6	21.7	0.1	CR	
21.7	21.9	0.2	DC	150
21.9	22.1	0.2	C	150
22.1	22.22	0.12	DC	150
22.22	22.6	0.38	C	150
22.6	22.8	0.2	DC	150
22.8	23.15	0.35	CBSH	
23.15	24.05	0.9	R	
24.05	24.75	0.7	CBSH	
24.75	28.85	4.1	R	
28.85	29.08	0.23	CBSH	
29.08	29.2	0.12	DC	130
29.2	29.45	0.25	CR	130
29.45	35.02	5.57	R	
35.02	35.3	0.28	DC	111
35.3	35.5	0.2	CR	111
35.5	35.92	0.42	DC	111
35.92	37.25	1.33	R	
37.25	37.5	0.25	DC	110
37.5	37.75	0.25	С	110
37.75	37.9	0.15	DC	110
37.9	39.8	1.9	R	
39.8	40.18	0.38	DC	101
40.18	41.1	0.92	С	101
41.1	44.8	3.7	С	100
44.8	45.05	0.25	CR	

From	То	Drilled	of geophysical logs Interpreted lithology	Name
		thickness		
Log inter	pretation of V	VC18-12C (me	tres) continued	
45.05	50.85	5.8	R	
50.85	51.05	0.2	IRST	IRONSTONE
51.05	52.6	1.55	R	
52.6	53	0.4	CBSH	
53	53.2	0.2	DC	201
53.2	54.3	1.1	C	201
54.3	54.6	0.3	DC	201
54.6	54.7	0.1	CBSH	
54.7	55.55	0.85	R	
55.55	55.8	0.25	IRST	IRONSTONE
55.8	56.4	0.6	R	
56.4	56.6	0.2	DC	202
56.6	57.1	0.5	С	202
57.1	57.35	0.25	R	202
57.35	57.55	0.2	CR	202
57.55	57.9	0.35	С	202
57.9	58.1	0.2	CBSH	
58.1	62.7	4.6	R	
62.7	62.9	0.2	CBSH	330
62.9	63	0.1	FAULT	POSSIBLE
63	68.5	5.5	R	
68.5	68.75	0.25	CBSH	330
68.75	70.15	1.4	R	
70.15	70.6	0.45	CBSH	
70.6	71.15	0.55	R	
71.15	71.5	0.35	DC	310
71.5	71.65	0.15	CR	310
71.65	72.75	1.1	R	
72.75	73.05	0.3	CBSH	
73.05	73.6	0.55	R	
73.6	73.9	0.3	CBSH	
73.9	74.15	0.25	DC	300
74.15	74.53	0.38	С	300
74.53	74.68	0.15	R	300
74.68	75.12	0.44	С	300
75.12	75.45	0.33	CBSH	
75.45	79.2	3.75	R	
79.2	79.8	0.6	CBSH	
79.8	80.28	0.48	С	320

			of geophysical logs	NT.
From	То	Drilled thickness	Interpreted lithology	Name
Lagintarr	ratation of W		traa) aantinuad	
	80.5		tres) continued	
80.28		0.22	CBSH	
80.5	85.1	4.6	R	240
85.1	85.8	0.7	CBSH	340
85.8	85.9	0.1	CR	340
85.9	86.15	0.25	CBSH	340
86.15	86.3	0.15	CR	340
86.3	86.55	0.25	CBSH	340
86.55	87.45	0.9	R	340
87.45	88	0.55	CBSH	340
88	88.15	0.15	R	340
88.15	88.35	0.2	CBSH	340
88.35	110.55	22.2	R	
110.55	110.65	0.1	IRST	IRONSTONE
110.65	118.85	8.2	R	
118.85	119.2	0.35	DC	410
119.2	120	0.8	R	
120	120.2	0.2	CR	
120.2	121.85	1.65	С	401
121.85	123.7	1.85	С	400
123.7	124	0.3	CR	
124	125.3	1.3	R	
125.3	125.5	0.2	CBSH	
125.5	125.75	0.25	С	420
125.75	126.05	0.3	CBSH	
126.05	126.55	0.5	R	
126.55	126.8	0.25	CR	
126.8	127.22	0.42	CBSH	
127.22	127.34	0.12	DC	440
127.34	127.8	0.46	C	440
127.8	127.9	0.1	DC	440
127.9	128.2	0.3	C	440
128.2	128.38	0.18	CR	440
128.38	128.7	0.10	C	440
128.7	128.9	0.32	CBSH	
128.9	131.3	2.4	R	1
131.3	131.56	0.26	CBSH	+
131.56	131.75	0.20	CR	442
131.75	131.75	0.19	CBSH	<del>11</del> 2
	_		+	
131.85	132.8	0.95	R	

From	То	Drilled	Interpreted lithology	Name
		thickness		
			tres) continued	
132.8	133.2	0.4	CR	
133.2	133.4	0.2	CBSH	
133.4	134.05	0.65	R	
134.05	134.65	0.6	CBSH	
134.65	135	0.35	R	
135	135.4	0.4	CBSH	
135.4	135.6	0.2	R	
135.6	136.2	0.6	CBSH	
136.2	136.6	0.4	R	
136.6	137	0.4	CBSH	463
137	143.4	6.4	R	
143.4	143.7	0.3	DC	460
143.7	150.32	6.62	R	
150.32	150.5	0.18	CBSH	483
150.5	159.2	8.7	R	
159.2	159.35	0.15	CR	
159.35	159.6	0.25	С	480
159.6	159.75	0.15	CBSH	480
159.75	159.95	0.2	DC	480
159.95	160.7	0.75	С	480
160.7	160.85	0.15	CR	
160.85	163.75	2.9	R	
163.75	163.9	0.15	CBSH	
163.9	172.25	8.35	R	
172.25	172.45	0.2	CR	
172.45	172.65	0.2	CBSH	
172.65	175.2	2.55	R	
175.2	175.45	0.25	CBSH	
175.45	175.8	0.35	DC	A71
175.8	177	1.2	R	
177	177.25	0.25	CBSH	
177.25	178.3	1.05	С	A7
178.3	178.5	0.2	DC	A7
178.5	178.72	0.22	CBSH	
178.72	186.7	7.98	R	
186.7	187.6	0.9	CBSH	A5
187.6	187.9	0.3	CR	A5
187.9	188.1	0.2	CBSH	A5
188.1	191.45	3.35	R	

Table A-2:	Lithologica	1 interpretation	of geophysical logs	
From	То	Drilled thickness	Interpreted lithology	Name
Log interp	retation of W	/C18-12C (me	tres) continued	
191.45	191.8	0.35	CBSH	
191.8	193.95	2.15	R	
193.95	194.3	0.35	DC	A3
194.3	194.5	0.2	CBSH	
194.5	195.3	0.8	R	
195.3	195.7	0.4	CBSH	A1
195.7	200.3	4.6	R	
Log interp	 retation of W	/C18-13C (me	tres)	
From	То	Drilled thickness	Interpreted lithology	Name
0	3	3	DRIFT	DRIFT
3	3.15	0.15	DC	150
3.15	3.65	0.5	С	150
3.65	3.8	0.15	CR	150
3.8	3.95	0.15	С	150
3.95	4.1	0.15	DC	150
4.1	4.3	0.2	С	150
4.3	4.6	0.3	DC	150
4.6	4.85	0.25	CR	
4.85	5.3	0.45	CBSH	
5.3	5.7	0.4	R	
5.7	5.85	0.15	CBSH	
5.85	6.2	0.35	CR	
6.2	6.35	0.15	CBSH	
6.35	6.8	0.45	CR	
6.8	7.1	0.3	DC	
7.1	7.45	0.35	CBSH	
7.45	11	3.55	R	
11	11.32	0.32	CBSH	
11.32	11.8	0.48	CR	130
11.8	16.65	4.85	R	
16.65	16.7	0.05	CR	
16.7	16.85	0.15	DC	111
16.85	17	0.15	С	111
17	17.2	0.2	DC	111
17.2	17.6	0.4	С	111
17.6	17.85	0.25	CBSH	

From	То	Drilled	of geophysical logs Interpreted lithology	Name
		thickness		
Log inter	pretation of V	VC18-13C (me	tres) continued	
17.85	19.2	1.35	R	
19.2	19.45	0.25	CR	
19.45	20.2	0.75	С	110
20.2	20.4	0.2	CBSH	
20.4	20.75	0.35	R	
20.75	21	0.25	CBSH	
21	28.3	7.3	R	
28.3	28.45	0.15	CR	
28.45	28.6	0.15	DC	101
28.6	29.95	1.35	С	101
29.95	32.65	2.7	С	100
32.65	32.9	0.25	DC	100
32.9	33.2	0.3	CBSH	
33.2	33.45	0.25	CR	
33.45	36.2	2.75	R	
36.2	36.55	0.35	CBSH	
36.55	38.95	2.4	R	
38.95	39.4	0.45	CBSH	
39.4	39.7	0.3	R	
39.7	39.95	0.25	CR	
39.95	40.9	0.95	С	201
40.9	41.2	0.3	CR	
41.2	46.75	5.55	R	
46.75	46.9	0.15	CBSH	
46.9	47	0.1	DC	202
47	47.4	0.4	С	202
47.4	47.6	0.2	CBSH	202
47.6	47.8	0.2	CR	202
47.8	48.3	0.5	С	202
48.45	54.55	6.1	R	
54.55	55.1	0.55	CBSH	330
55.1	58	2.9	R	
58	58.55	0.55	CBSH	310
58.55	63.95	5.4	R	
63.95	64.55	0.6	CBSH	
64.55	68.25	3.7	R	
68.25	68.4	0.15	CR	
68.4	68.62	0.22	С	300
68.62	68.85	0.23	DC	300

From	То	Drilled	of geophysical logs Interpreted lithology	Name
		thickness		
			tres) continued	
68.85	69.15	0.3	R	300
69.15	69.35	0.2	CBSH	300
69.35	69.65	0.3	C	300
69.65	69.85	0.2	CBSH	
69.85	73.55	3.7	R	
73.55	74	0.45	CBSH	
74	74.35	0.35	R	
74.35	74.62	0.27	CBSH	
74.62	75.18	0.56	C	320
75.18	75.9	0.72	CBSH	
75.9	81.2	5.3	R	
81.2	81.9	0.7	CBSH	340
81.9	82.05	0.15	CR	340
82.05	82.15	0.1	CBSH	340
82.15	82.32	0.17	CR	340
82.32	82.8	0.48	CBSH	340
82.8	83.85	1.05	R	340
83.85	85.3	1.45	CBSH	340
85.3	89.7	4.4	R	
89.7	89.9	0.2	CBSH	
89.9	90.55	0.65	R	
90.55	90.95	0.4	CBSH	360
90.95	99.8	8.85	R	
99.8	99.9	0.1	FAULT	POSSIBLE
99.9	105.05	5.15	R	
105.05	105.3	0.25	CBSH	
105.3	112.75	7.45	R	
112.75	112.85	0.1	CR	430
112.85	113.15	0.3	C	430
113.15	113.4	0.25	CBSH	
113.4	115.6	2.2	R	
115.6	115.85	0.25	DC	410
115.85	117.05	1.2	С	410
117.05	117.4	0.35	CBSH	
117.4	117.55	0.15	CR	
117.55	119.6	2.05	С	401
119.6	122.8	3.2	С	400
122.8	125.45	2.65	R	
125.45	125.6	0.15	CBSH	

Table A-2:	Lithological i	nterpretation	of geophysical logs	
From	То	Drilled thickness	Interpreted lithology	Name
Log interpre	etation of WC	<u> </u>	res) continued	
125.6	125.75	0.15	DC	420
125.75	126	0.25	С	420
126	126.2	0.2	DC	420
126.2	126.45	0.25	CBSH	
126.45	130.1	3.65	R	
130.1	130.18	0.08	CR	
130.18	130.28	0.1	DC	440
130.28	130.63	0.35	С	440
130.63	130.75	0.12	DC	440
130.75	130.9	0.15	С	440
130.9	131.05	0.15	DC	440
131.05	131.2	0.15	R	440
131.2	131.35	0.15	С	440
131.35	131.45	0.1	DC	440
131.45	131.6	0.15	С	440
131.6	131.8	0.2	CBSH	
131.8	133.55	1.75	R	
133.55	133.72	0.17	CBSH	
133.72	133.9	0.18	DC	442
133.9	134.1	0.2	CBSH	
134.1	139.85	5.75	R	
139.85	140.3	0.45	CBSH	463
140.3	145.25	4.95	R	
145.25	145.4	0.15	CR	
145.4	145.5	0.1	CBSH	
145.5	145.65	0.15	DC	460
145.65	157	11.35	R	
157	157.5	0.5	CBSH	483
157.5	158	0.5	R	
	etation of WC			
From	То	Drilled thickness	Interpreted lithology	Name
0	3.9	3.9	DRIFT	DRIFT
3.9	14.95	11.05	R	
14.95	15.1	0.15	CR	
15.1	15.7	0.6	С	150
15.7	15.95	0.25	DC	150

То	Drilled thickness	Interpreted lithology	Name
oretation of V		tres) continued	-
16.1	0.15	CBSH	
16.3	0.2	R	
16.65	0.35	CBSH	
20.3	3.65	R	
20.5	0.2	CBSH	
20.7	0.2	CR	130
21	0.3	CBSH	
23.75	2.75	R	
24	0.25	CBSH	
24.2	0.2	С	111
24.5	0.3	CBSH	
25.1	0.6	R	
25.3	0.2	CBSH	
25.6	0.3	С	110
26.75	1.15	R	
27	0.25	CBSH	
28.12	1.12	С	101
30	1.88	С	100
30.18	0.18	DC	100
30.4	0.22	CR	
31.4	1	CBSH	
34.5	3.1	R	
34.82	0.32	CBSH	
35.05	0.23	CR	
35.8	0.75	С	201
36	0.2	CR	
37	1	R	
37.15	0.15	CBSH	
37.22	0.07	DC	202
37.5	0.28	С	202
37.87	0.37	DC	202
38.1	0.23	С	202
38.3	0.2	CBSH	
45.6	7.3	R	
45.95	0.35	CBSH	
46.2	0.25	R	
46.35	0.15	CBSH	
46.6	0.25	CR	
46.8	0.2	CBSH	
	To    To     16.1     16.3     16.65     20.3     20.5     20.7     21     23.75     24     24.2     24.5     25.1     25.3     25.6     26.75     27     28.12     30     30.18     30.4     31.4     34.5     34.82     35.05     35.8     36     37     37.15     37.22     37.5     37.87     38.1     38.3     45.6     45.95     46.2     46.35     46.6	To Drilled thickness or etation of WC18-14C (metation of WC18-14C (metation of WC18-14C) (m	thickness retation of WC18-14C (metres) continued    16.1

From	То	al interpretation Drilled	Interpreted lithology	Name
		thickness		
Log inter	rpretation of V	VC18-14C (me	tres) continued	
46.8	48.45	1.65	R	
48.45	48.8	0.35	С	300
48.8	49	0.2	DC	300
49	49.15	0.15	С	300
49.15	49.4	0.25	CR	
49.4	51.5	2.1	R	
51.5	51.75	0.25	CBSH	
51.75	52.12	0.37	C	320
52.12	52.2	0.08	CBSH	
52.2	54.8	2.6	R	
54.8	55.35	0.55	CBSH	340
55.35	55.45	0.1	CR	340
55.45	55.5	0.05	CBSH	340
55.5	55.9	0.4	R	340
55.9	56.55	0.65	CBSH	340
56.55	77.6	21.05	R	
77.6	78	0.4	CR	410
78	78.3	0.3	R	
78.3	78.6	0.3	CBSH	
78.6	79.05	0.45	C	401
79.05	79.4	0.35	DC	400
79.4	80	0.6	C	400
80	80.1	0.1	FAULT	ESTABLISHED
80.1	81.2	1.1	C	401
81.2	81.75	0.55	DC	400
81.75	81.8	0.05	C	400
81.8	81.85	0.05	FAULT	POSSIBLE
81.85	85.05	3.2	C	400
85.05	85.4	0.35	DC	400
85.4	85.5	0.1	FAULT	ESTABLISHED
85.5	86.9	1.4	C	400
86.9	87.38	0.48	DC	400
87.38	88.45	1.07	R	
88.45	88.7	0.25	CR	
88.7	88.95	0.25	С	420
88.95	89.2	0.25	CBSH	
89.2	89.35	0.15	R	
89.35	89.8	0.45	CBSH	
89.8	90.1	0.3	R	

From	То	Drilled	of geophysical logs Interpreted lithology	Name
		thickness		
Log interp	pretation of W	VC18-14C (me	tres) continued	
90.1	90.45	0.35	IRST	IRONSTONE
90.45	90.85	0.4	R	
90.85	91.5	0.65	CBSH	
91.5	92	0.5	R	
92	92.25	0.25	CBSH	
92.25	92.32	0.07	DC	440
92.32	92.7	0.38	C	440
92.7	92.9	0.2	DC	440
92.9	93.05	0.15	C	440
93.05	93.3	0.25	DC	440
93.3	95.5	2.2	R	
95.5	96	0.5	CBSH	442
96	96.3	0.3	R	
96.3	96.65	0.35	CBSH	
96.65	97	0.35	R	
97	97.35	0.35	CBSH	
97.35	98.95	1.6	R	
98.95	99.3	0.35	CBSH	
99.3	101.2	1.9	R	
101.2	101.65	0.45	CBSH	
101.65	102.1	0.45	R	
102.1	102.6	0.5	CBSH	463
102.6	106.9	4.3	R	
106.9	107.05	0.15	CBSH	460
107.05	107.3	0.25	CR	460
107.3	114.2	6.9	R	
114.2	114.7	0.5	CBSH	483
114.7	118.1	3.4	R	
118.1	118.45	0.35	CBSH	
118.45	118.6	0.15	R	
118.6	118.8	0.2	CBSH	
118.8	119.15	0.35	С	480
119.15	119.3	0.15	DC	480
119.3	119.55	0.25	CBSH	
119.55	124.8	5.25	R	
124.8	125.2	0.4	CBSH	
125.2	127	1.8	R	
127	127.2	0.2	CBSH	
127.2	127.45	0.25	DC	A71

From	To	Drilled	of geophysical logs Interpreted lithology	Name
110111		thickness	interpreted nunorogy	Tuille
Log interr	oretation of W		tres) continued	
127.45	127.95	0.5	R	
127.95	128.4	0.45	DC	A7
128.4	128.95	0.55	C	A7
128.95	129.1	0.15	DC	A7
129.1	129.35	0.25	CBSH	
129.35	135.7	6.35	R	
135.7	136.4	0.7	CBSH	A5
136.4	138.45	2.05	R	
138.45	138.8	0.35	CBSH	
138.8	140.22	1.42	R	
Log interp	oretation of W	/C18-15C (me	tres)	
From	То	Drilled	Interpreted lithology	Name
		thickness		
0	4	4	DRIFT	DRIFT
4	5.2	1.2	R	
5.2	5.42	0.22	CBSH	310
5.42	5.6	0.18	DC	310
5.6	5.82	0.22	CR	310
5.82	11.75	5.93	R	
11.75	11.95	0.2	CBSH	
11.95	12.1	0.15	DC	300
12.1	12.6	0.5	С	300
12.6	12.8	0.2	CBSH	
12.8	15.6	2.8	R	
15.6	16.5	0.9	CBSH	320
16.5	19.4	2.9	R	
19.4	20.7	1.3	CBSH	340
20.7	22.35	1.65	R	340
22.35	23.2	0.85	CBSH	340
23.2	32.72	9.52	R	
32.72	32.9	0.18	CBSH	360
32.9	41.7	8.8	R	
41.7	42.05	0.35	DC	430
42.05	42.2	0.15	CBSH	
42.2	45.12	2.92	R	
45.12	45.35	0.23	DC	410
45.35	46.18	0.83	С	410

			of geophysical logs	1
From	То	Drilled thickness	Interpreted lithology	Name
Log interp	retation of V	VC18-15C (me	tres) continued	
46.18	47.2	1.02	R	
47.2	47.38	0.18	CBSH	
47.38	47.58	0.2	CR	
47.58	48.55	0.97	С	401
48.55	48.65	0.1	DC	400
48.65	50.3	1.65	С	400
50.3	50.65	0.35	DC	400
50.65	50.85	0.2	CR	
50.85	51.05	0.2	R	
51.05	51.3	0.25	DC	420
51.3	51.5	0.2	CBSH	
51.5	53.82	2.32	R	
53.82	54.27	0.45	С	440
54.27	54.37	0.1	DC	440
54.37	54.45	0.08	С	440
54.45	54.52	0.07	DC	440
54.52	54.85	0.33	С	440
54.85	55.05	0.2	CBSH	
55.05	56.7	1.65	R	
56.7	57.1	0.4	CR	442
57.1	62.85	5.75	R	
62.85	63.2	0.35	CBSH	
63.2	63.9	0.7	R	
63.9	64.5	0.6	CBSH	463
64.5	68.48	3.98	R	
68.48	68.6	0.12	CBSH	
68.6	68.8	0.2	DC	460
68.8	68.9	0.1	CBSH	
68.9	70.9	2	R	
70.9	71.3	0.4	IRST	IRONSTONE
71.3	71.55	0.25	CBSH	
71.55	72.08	0.53	R	
72.08	72.4	0.32	CBSH	
72.4	73.3	0.9	R	
73.3	73.65	0.35	IRST	IRONSTONE
73.65	75.95	2.3	R	
75.95	76.2	0.25	CBSH	
76.2	78.85	2.65	R	
78.85	79.05	0.2	CBSH	

Table A-2:	Lithological	interpretation	of geophysical logs	
From	То	Drilled thickness	Interpreted lithology	Name
Log interpr	etation of WC	C18-15C (met	res) continued	
79.05	79.2	0.15	C	480
79.2	79.35	0.15	DC	480
79.35	79.8	0.45	С	480
79.8	80	0.2	DC	480
80	81.05	1.05	R	
81.05	81.5	0.45	CBSH	
81.5	82.9	1.4	R	
82.9	83.3	0.4	CBSH	
83.3	84.9	1.6	R	
84.9	85.25	0.35	CBSH	
85.25	85.5	0.25	R	
85.5	85.7	0.2	CBSH	
85.7	86.12	0.42	С	A71
86.12	86.35	0.23	CBSH	
86.35	87.1	0.75	R	
87.1	87.5	0.4	С	A7
87.5	87.6	0.1	DC	A7
87.6	87.68	0.08	CBSH	
87.68	88	0.32	R	
88	88.13	0.13	CBSH	
88.13	88.3	0.17	DC	A72
88.3	88.5	0.2	CBSH	
88.5	95.2	6.7	R	
95.2	95.72	0.52	CBSH	
95.72	96	0.28	CR	A5
96	96.2	0.2	CBSH	
96.2	99.3	3.1	R	
99.3	99.6	0.3	CBSH	
99.6	101	1.4	R	
Logintarn	etation of WC	18 16C (mat	ras)	
From	To	Drilled	Interpreted lithology	Name
1 10111	10	thickness	interpreted nulology	TAUTIC
0	1.6	1.6	DRIFT	DRIFT
1.6	2.5	0.9	R	
2.5	2.9	0.4	DC	110
2.9	3.1	0.2	CBSH	
3.1	8.6	5.5	R	

From	То	Drilled	Interpreted lithology	Name
		thickness		
Log inter		VC18-16C (me	tres) continued	
8.6	8.8	0.2	CBSH	
8.8	9.25	0.45	C	101
9.25	10.65	1.4	C	100
10.65	10.93	0.28	CR	
10.93	11.65	0.72	CBSH	
11.65	14.8	3.15	R	
14.8	15.4	0.6	CBSH	
15.4	16	0.6	C	201
16	16.15	0.15	DC	201
16.15	16.4	0.25	CBSH	
16.4	17.7	1.3	R	
17.7	17.85	0.15	IRST	IRONSTONE
17.85	18.55	0.7	R	
18.55	18.7	0.15	CR	
18.7	18.85	0.15	С	202
18.85	19.2	0.35	DC	202
19.2	19.48	0.28	CBSH	
19.48	37.55	18.07	R	
37.55	37.75	0.2	CBSH	
37.75	38.12	0.37	С	300
38.12	38.22	0.1	CBSH	
38.22	41.2	2.98	R	
41.2	41.45	0.25	CBSH	320
41.45	41.6	0.15	CR	320
41.6	41.85	0.25	CBSH	320
41.85	44.85	3	R	
44.85	45.45	0.6	CBSH	340
45.45	45.6	0.15	CR	340
45.6	45.85	0.25	CBSH	340
45.85	46.63	0.78	R	340
46.63	47.5	0.87	CBSH	340
47.5	51.65	4.15	R	
51.65	52	0.35	CBSH	360
52	66	14	R	
66	66.12	0.12	CBSH	
66.12	66.4	0.28	DC	430
66.4	68.45	2.05	R	
68.45	68.55	0.1	CBSH	
68.55	68.95	0.4	С	410

From	То	Drilled	of geophysical logs Interpreted lithology	Name
		thickness		
			tres) continued	
68.95	69.05	0.1	FAULT	POSSIBLE
69.05	69.3	0.25	C	410
69.3	70	0.7	R	
70	70.28	0.28	CBSH	
70.28	71	0.72	C	401
71	71.38	0.38	DC	400
71.38	72.6	1.22	C	400
72.6	73.08	0.48	DC	400
73.08	73.3	0.22	CBSH	
73.3	73.6	0.3	R	
73.6	73.8	0.2	CBSH	
73.8	73.95	0.15	DC	420
73.95	74.2	0.25	CR	
74.2	74.4	0.2	CBSH	
74.4	77.45	3.05	R	
77.45	77.7	0.25	CBSH	
77.7	77.92	0.22	C	440
77.92	78.28	0.36	DC	440
78.28	78.5	0.22	C	440
78.5	79.9	1.4	R	
79.9	80.3	0.4	CBSH	442
80.3	84.75	4.45	R	
84.75	85.15	0.4	CBSH	463
85.15	89.22	4.07	R	
89.22	89.55	0.33	CR	460
89.55	98.8	9.25	R	
98.8	99.25	0.45	CBSH	
99.25	101.1	1.85	R	
101.1	101.3	0.2	CBSH	
101.3	101.53	0.23	DC	480
101.53	102.1	0.57	С	480
102.1	102.3	0.2	DC	480
102.3	102.48	0.18	CBSH	
102.48	103.25	0.77	R	
103.25	103.9	0.65	CBSH	
103.9	105.05	1.15	R	
105.05	105.45	0.4	CBSH	
105.45	107.4	1.95	R	
107.4	107.7	0.3	CBSH	

Table A-2	: Lithologica	l interpretation	of geophysical logs	
From	То	Drilled	Interpreted lithology	Name
		thickness		
Log interp	retation of W	C18-16C (met	tres) continued	
107.7	107.85	0.15	R	
107.85	108	0.15	CBSH	
108	108.35	0.35	C	A71
108.35	108.55	0.2	CBSH	
108.55	109.05	0.5	R	
109.05	109.3	0.25	CBSH	
109.3	110.15	0.85	С	A7
110.15	110.3	0.15	DC	A7
110.3	116.5	6.2	R	
116.5	117	0.5	CBSH	
117	117.15	0.15	CR	A5
117.15	117.4	0.25	CBSH	
117.4	120.5	3.1	R	
120.5	120.9	0.4	CBSH	
120.9	122.45	1.55	R	
122.45	122.75	0.3	DC	A3
122.75	123.4	0.65	R	
123.4	123.6	0.2	CBSH	A1
123.6	123.75	0.15	CR	A1
123.75	124.24	0.49	R	
Log interp	retation of W	VC18-17C (met	tres)	
From	То	Drilled	Interpreted lithology	Name
		thickness		
0	7.45	7.45	DRIFT	DRIFT
7.45	10.9	3.45	R	
10.9	11.05	0.15	CBSH	
11.05	11.2	0.15	R	
11.2	11.3	0.1	CBSH	
11.3	11.7	0.4	R	
11.7	12.2	0.5	CBSH	
12.2	13.1	0.9	R	
13.1	13.4	0.3	CBSH	
13.4	13.9	0.5	R	
13.9	14.4	0.5	CBSH	
14.4	16.8	2.4	R	
				150
			+	
16.8 17	17 17.6	0.2 0.6	C DC	150 150

			n of geophysical logs	
From	То	Drilled	Interpreted lithology	Name
<del>-</del> • ·		thickness		
			tres) continued	
17.6	17.85	0.25	CBSH	
17.85	18	0.15	R	
18	18.4	0.4	CBSH	
18.4	21.35	2.95	R	
21.35	21.8	0.45	CR	130
21.8	23.6	1.8	R	
23.6	24.05	0.45	CBSH	
24.05	26.85	2.8	R	
26.85	27.05	0.2	CBSH	
27.05	27.35	0.3	С	111
27.35	27.6	0.25	CBSH	
27.6	28.3	0.7	R	
28.3	28.65	0.35	С	110
28.65	28.8	0.15	CR	
28.8	29.18	0.38	R	
29.18	29.4	0.22	CBSH	
29.4	30.35	0.95	С	101
30.35	32.05	1.7	С	100
32.05	39.6	7.55	R	
39.6	40.12	0.52	С	201
40.12	40.2	0.08	DC	201
40.2	40.32	0.12	CBSH	
40.32	43.4	3.08	R	
43.4	43.75	0.35	C	202
43.75	43.85	0.1	CR	202
43.85	43.98	0.13	DC	202
43.98	44.08	0.1	CR	202
44.08	44.2	0.12	DC	202
44.2	44.3	0.1	CR	
44.3	44.38	0.08	CBSH	
44.38	52.8	8.42	R	
52.8	53.2	0.4	CBSH	310
53.2	62.85	9.65	R	
62.85	63.3	0.45	CBSH	
63.3	63.9	0.6	R	
63.9	64.1	0.2	CBSH	
64.1	64.32	0.22	CR	
64.32	64.45	0.13	CBSH	
64.45	64.83	0.38	С	300

From	То	Drilled	Interpreted lithology	Name
<del>-</del> • .	CAN CAN	thickness		
	· ,		tres) continued	
64.83	68	3.17	R	220
68	68.2	0.2	CR	320
68.2	68.4	0.2	DC	320
68.4	68.62	0.22	CBSH	
68.62	74.25	5.63	R	
74.25	74.6	0.35	CBSH	340
74.6	74.92	0.32	R	340
74.92	75.39	0.47	CBSH	340
75.39	75.8	0.41	R	340
75.8	76.2	0.4	CBSH	340
76.2	79.2	3	R	340
79.2	79.8	0.6	CBSH	340
79.8	84.6	4.8	R	
84.6	84.8	0.2	CBSH	
84.8	93.9	9.1	R	
93.9	94.2	0.3	DC	430
94.2	94.4	0.2	CBSH	
94.4	97.48	3.08	R	
97.48	98.3	0.82	С	410
98.3	98.8	0.5	R	
98.8	99.03	0.23	CR	
99.03	99.8	0.77	С	401
99.8	100	0.2	DC	400
100	101.2	1.2	С	400
101.2	101.5	0.3	DC	400
101.5	101.75	0.25	CBSH	
101.75	104.05	2.3	R	
104.05	104.25	0.2	CBSH	
104.25	104.4	0.15	DC	420
104.4	104.6	0.2	CR	420
104.6	106.85	2.25	R	
106.85	107	0.15	CBSH	
107	107.2	0.2	С	440
107.2	107.3	0.1	DC	440
107.3	107.42	0.12	C	440
107.42	107.58	0.16	DC	440
107.58	107.85	0.27	C	440
107.85	108.85	1	R	
108.85	109.05	0.2	CBSH	

Table A-2:	Table A-2: Lithological interpretation of geophysical logs					
From	То	Drilled	Interpreted lithology	Name		
		thickness				
Log interpre	etation of WC	C18-17C (met	res) continued			
109.05	109.2	0.15	DC	442		
109.2	109.4	0.2	CBSH			
109.4	113.3	3.9	R			
113.3	113.8	0.5	CBSH	463		
113.8	117.6	3.8	R			
117.6	117.8	0.2	CBSH	460		
117.8	118	0.2	CR	460		
118	118.12	0.12	CBSH	460		
118.12	126.05	7.93	R			
126.05	126.26	0.21	CBSH			
126.26	127.1	0.84	С	480		
127.1	127.2	0.1	DC	480		
127.2	127.4	0.2	CBSH			
127.4	128.6	1.2	R			
128.6	129.2	0.6	CBSH			
129.2	132.53	3.33	R			
132.53	132.9	0.37	CBSH			
132.9	133.35	0.45	R			
133.35	133.75	0.4	DC	A71		
133.75	134.2	0.45	R			
134.2	134.45	0.25	CBSH			
134.45	134.65	0.2	С	A7		
134.65	135.05	0.4	DC	A7		
135.05	135.15	0.1	CR	A7		
135.15	135.35	0.2	DC	A7		
135.35	140.22	4.87	R			
Log interpre	etation of WC	C18-18C (met	res)			
From	То	Drilled	Interpreted lithology	Name		
		thickness				
0	2.44	2.44	DRIFT	DRIFT		
2.44	11.15	8.71	R			
11.15	11.43	0.28	CR			
11.43	11.6	0.17	С	150		
11.6	11.8	0.2	R	150		
11.8	12.05	0.25	DC	150		
12.05	12.15	0.1	С	150		
12.15	12.45	0.3	DC	150		

			of geophysical logs	N
From	То	Drilled thickness	Interpreted lithology	Name
Log inter	nretation of V		tres) continued	
12.45	12.7	0.25	CBSH	
12.7	13.3	0.6	R	
13.3	13.52	0.22	CBSH	
13.52	18.85	5.33	R	
18.85	19.2	0.35	CR	130
19.2	19.4	0.2	CBSH	130
19.4	23.05	3.65	R	
23.05	23.38	0.33	DC	111
23.38	23.48	0.1	CR	111
23.48	23.8	0.32	DC	111
23.8	24	0.32	CBSH	111
24	25.3	1.3	R	
25.3	25.75	0.45	C	110
25.75	26.1	0.45	CBSH	110
26.1	27.4	1.3	R	
27.4	27.4	0.25	CBSH	
27.65	29.3	1.65	C	101
29.3	31.5	2.2	C	100
31.5	31.75	0.25	DC	100
31.75	32.05	0.23	CR	100
32.05	33.25	1.2	CBSH	
33.25	40.3	7.05	R	
40.3	41.35	1.05	C	201
41.35	44.25	2.9	R	201
44.25	44.25	0.4	CBSH	
44.65	45.7	1.05		
	_		R	202
45.7	45.9	0.2	DC	202
45.9	46.4	0.5	CDCH	202
46.4	46.6	0.2	CBSH	202
46.6	46.82	0.22	CR	202
46.82	47.05	0.23	C	202
47.05	47.23	0.18	DC	202
47.23	58.7	11.47	R	2100
58.7	59.75	1.05	CBSH	310?
59.75	62.85	3.1	R	IDONGTONE
62.85	63.2	0.35	IRST	IRONSTONE
63.2	67.3	4.1	R	
67.3	67.8	0.5	CBSH	
67.8	71.55	3.75	R	

From	То	Drilled	Interpreted lithology	Name
		thickness		
			tres) continued	
71.55	72.2	0.65	IRST	IRONSTONE
72.2	76.05	3.85	R	
76.05	76.3	0.25	CR	
76.3	76.55	0.25	DC	300
76.55	76.75	0.2	С	300
76.75	77	0.25	R	300
77	77.08	0.08	DC	300
77.08	77.6	0.52	С	300
77.6	77.8	0.2	CBSH	
77.8	81.6	3.8	R	
81.6	81.8	0.2	CBSH	
81.8	82	0.2	CR	320
82	82.22	0.22	C	320
82.22	82.85	0.63	CBSH	
82.85	90.05	7.2	R	
90.05	90.2	0.15	CBSH	
90.2	90.8	0.6	R	
90.8	92.6	1.8	CBSH	340
92.6	94.3	1.7	R	340
94.3	95.45	1.15	CBSH	340
95.45	95.65	0.2	R	340
95.65	95.95	0.3	CBSH	340
95.95	100.8	4.85	R	
100.8	101.1	0.3	CBSH	
101.1	101.6	0.5	R	
101.6	101.8	0.2	CBSH	360
101.8	121.15	19.35	R	
121.15	121.25	0.1	CR	430
121.25	121.4	0.15	DC	430
121.4	121.65	0.25	CR	430
121.65	121.85	0.2	CBSH	
121.85	125	3.15	R	
125	125.1	0.1	IRST	IRONSTONE
125.1	125.7	0.6	R	
125.7	125.97	0.27	CR	
125.97	126.5	0.53	С	410
126.5	126.63	0.13	FAULT	PROBABLE
126.63	126.95	0.32	С	410
126.95	127.4	0.45	R	

Table A-2:	Lithological i	nterpretation	of geophysical logs	
From	То	Drilled thickness	Interpreted lithology	Name
Log interpre	etation of WC	18-18C (met	res) continued	
127.4	128.4	1	С	401
128.4	128.6	0.2	DC	400
128.6	130.15	1.55	С	400
130.15	130.4	0.25	DC	400
130.4	133.3	2.9	R	
133.3	133.5	0.2	CBSH	
133.5	133.7	0.2	DC	420
133.7	133.9	0.2	CR	
133.9	134.15	0.25	CBSH	
134.15	137.75	3.6	R	
137.75	138.1	0.35	IRST	IRONSTONE
138.1	138.85	0.75	R	
138.85	139	0.15	CR	
139	139.1	0.1	DC	440
139.1	139.4	0.3	С	440
139.4	139.52	0.12	DC	440
139.52	139.75	0.23	CR	440
139.75	140.15	0.4	DC	440
140.15	140.6	0.45	CR	440
140.6	142.65	2.05	R	
142.65	143.05	0.4	С	
143.05	143.25	0.2	CBSH	
143.25	147.58	4.33	R	
Log interpre	etation of WC	18-19C (met	res)	
From	То	Drilled	Interpreted lithology	Name
		thickness		
0	5.8	5.8	DRIFT	DRIFT
5.8	8.15	2.35	R	
8.15	8.55	0.4	CBSH	310?
8.55	15.55	7	R	
15.55	15.85	0.3	IRST	IRONSTONE
15.85	16	0.15	CBSH	
16	16.52	0.52	С	300
16.52	17.45	0.93	R	
17.45	17.9	0.45	CBSH	
17.9	19.8	1.9	R	
19.8	20.6	0.8	CBSH	320

From	То	Drilled	of geophysical logs Interpreted lithology	Name
		thickness		
Log inter	pretation of V	VC18-19C (me	tres) continued	
20.6	25.4	4.8	R	
25.4	25.5	0.1	CBSH	340
25.5	30.2	4.7	R	340
30.2	30.8	0.6	CBSH	340
30.8	36.25	5.45	R	
36.25	36.75	0.5	CBSH	360
36.75	46.55	9.8	R	
46.55	46.8	0.25	CBSH	
46.8	47.05	0.25	DC	430
47.05	49.6	2.55	R	
49.6	49.95	0.35	IRST	IRONSTONE
49.95	50.25	0.3	R	
50.25	50.45	0.2	CBSH	
50.45	50.6	0.15	DC	410
50.6	51.4	0.8	С	410
51.4	51.7	0.3	CBSH	
51.7	52.7	1	R	
52.7	52.95	0.25	CBSH	
52.95	53.9	0.95	С	401
53.9	54.1	0.2	DC	400
54.1	55.4	1.3	С	400
55.4	55.85	0.45	DC	400
55.85	56	0.15	С	420
56	56.1	0.1	DC	420
56.1	56.3	0.2	CR	
56.3	56.55	0.25	CBSH	
56.55	56.95	0.4	R	
56.95	57.4	0.45	IRST	IRONSTONE
57.4	57.6	0.2	CBSH	
57.6	57.9	0.3	С	440
57.9	58	0.1	DC	440
58	58.1	0.1	С	440
58.1	58.2	0.1	DC	440
58.2	58.3	0.1	С	440
58.3	58.5	0.2	DC	440
58.5	58.75	0.25	CBSH	
58.75	60.2	1.45	R	
60.2	60.3	0.1	CBSH	
60.3	60.6	0.3	DC	442

From         To         Drilled thickness         Interpreted lithology         Name           Log interpretation of WC18-19C (metres) continued         60.6         68         7.4         R           68         68.8         0.8         CBSH         463           68.8         72.52         3.72         R           72.52         72.9         0.38         DC         460           72.9         75.7         2.8         R           75.7         76         0.3         CBSH         483           76         80         4         R         80         80.4         0.4         CBSH           80.4         81.6         1.2         R         81.6         81.95         0.35         CBSH           81.95         82.3         0.35         CBSH         82.3         82.5         0.2         CBSH           82.3         82.5         0.2         CBSH         88.2         480           83.18         85.05         1.87         R         85.9         86.2         0.3         CBSH           85.9         86.2         0.3         CBSH         86.2         87.5         87.85         0.35         CBSH	iadic A-4. I	Limologicai i	nterpretation	of geophysical logs	
Log interpretation of WC18-19C (metres) continued   60.6			Drilled		Name
60.6         68         7.4         R           68         68.8         0.8         CBSH         463           68.8         72.52         3.72         R           72.52         72.9         0.38         DC         460           72.9         75.7         2.8         R           75.7         76         0.3         CBSH         483           76         80         4         R         80         481.6         R           80.4         81.6         1.2         R         81.6         R         81.95         0.35         CBSH           81.95         82.3         0.35         R         82.3         82.5         0.2         CBSH           82.3         82.5         0.2         CBSH         480           82.5         83.18         0.68         C         480           83.18         85.05         1.87         R           85.05         85.4         0.35         CBSH           85.9         86.2         0.3         CBSH           86.2         87.5         1.3         R           87.5         87.85         0.35         CBSH			thickness		
68         68.8         0.8         CBSH         463           68.8         72.52         3.72         R           72.52         72.9         0.38         DC         460           72.9         75.7         2.8         R           75.7         76         0.3         CBSH         483           76         80         4         R         80         80.4         0.4         CBSH           80.4         81.6         1.2         R         81.6         81.95         0.35         CBSH           81.95         82.3         0.35         R         82.3         82.5         0.2         CBSH           82.3         82.5         0.2         CBSH         82.5         83.18         0.68         C         480           83.18         85.05         1.87         R         85.9         85.4         85.9         R           85.9         86.2         0.3         CBSH         86.2         87.5         1.3         R           87.5         87.85         0.35         CBSH         88.2         88.2         0.35         R           88.2         88.5         0.3         CBSH <t< td=""><td>Log interpre</td><td>etation of WC</td><td>218-19C (met</td><td>res) continued</td><td></td></t<>	Log interpre	etation of WC	218-19C (met	res) continued	
68.8         72.52         3.72         R           72.52         72.9         0.38         DC         460           72.9         75.7         2.8         R           75.7         76         0.3         CBSH         483           76         80         4         R         80         80.4         0.4         CBSH           80.4         81.6         1.2         R         81.6         81.95         0.35         CBSH           81.95         82.3         0.35         R         82.3         82.5         0.2         CBSH           82.3         82.5         0.2         CBSH         82.5         83.18         0.68         C         480           83.18         85.05         1.87         R         85.05         R         85.4         85.9         0.5         R         85.9         86.2         0.3         CBSH         85.9         86.2         87.5         1.3         R         87.5         87.85         0.35         CBSH         87.85         88.2         0.35         CBSH         88.2         88.5         0.3         CBSH         88.2         88.5         0.3         CBSH         88.2         88.5	0.6	68	7.4	R	
72.52         72.9         0.38         DC         460           72.9         75.7         2.8         R           75.7         76         0.3         CBSH         483           76         80         4         R         80         80.4         0.4         CBSH           80.4         81.6         1.2         R         81.6         81.95         0.35         CBSH           81.95         82.3         0.35         R         82.3         82.5         0.2         CBSH           82.3         82.5         0.2         CBSH         480         83.18         85.05         1.87         R           85.05         85.4         0.35         CBSH         85.9         86.2         0.3         CBSH           85.9         86.2         0.3         CBSH         86.2         87.5         1.3         R           87.5         87.85         0.35         CBSH         88.2         0.35         R           88.2         88.5         0.3         CBSH         88.2         88.5         0.3         CBSH	8	68.8	0.8	CBSH	463
72.9         75.7         2.8         R           75.7         76         0.3         CBSH         483           76         80         4         R         80         80.4         0.4         CBSH           80.4         81.6         1.2         R         81.6         81.95         0.35         CBSH           81.95         82.3         0.35         R         82.3         82.5         0.2         CBSH           82.3         82.5         0.2         CBSH         480         83.18         85.05         1.87         R           83.18         85.05         1.87         R         85.05         85.4         0.35         CBSH           85.4         85.9         0.5         R         85.9         86.2         0.3         CBSH           86.2         87.5         1.3         R         87.5         87.85         0.35         CBSH           87.85         88.2         0.35         R         88.2         88.5         0.3         CBSH	8.8	72.52	3.72	R	
75.7         76         0.3         CBSH         483           76         80         4         R           80         80.4         0.4         CBSH           80.4         81.6         1.2         R           81.6         81.95         0.35         CBSH           81.95         82.3         0.35         R           82.3         82.5         0.2         CBSH           82.5         83.18         0.68         C         480           83.18         85.05         1.87         R           85.05         85.4         0.35         CBSH           85.4         85.9         0.5         R           85.9         86.2         0.3         CBSH           86.2         87.5         1.3         R           87.5         87.85         0.35         CBSH           87.85         88.2         0.35         R           88.2         88.5         0.3         CBSH	2.52	72.9	0.38	DC	460
76         80         4         R           80         80.4         0.4         CBSH           80.4         81.6         1.2         R           81.6         81.95         0.35         CBSH           81.95         82.3         0.35         R           82.3         82.5         0.2         CBSH           82.5         83.18         0.68         C         480           83.18         85.05         1.87         R           85.05         85.4         0.35         CBSH           85.4         85.9         0.5         R           85.9         86.2         0.3         CBSH           86.2         87.5         1.3         R           87.5         87.85         0.35         CBSH           87.85         88.2         0.35         R           88.2         88.5         0.3         CBSH	2.9	75.7	2.8	R	
80         80.4         0.4         CBSH           80.4         81.6         1.2         R           81.6         81.95         0.35         CBSH           81.95         82.3         0.35         R           82.3         82.5         0.2         CBSH           82.5         83.18         0.68         C         480           83.18         85.05         1.87         R           85.05         85.4         0.35         CBSH           85.4         85.9         0.5         R           85.9         86.2         0.3         CBSH           86.2         87.5         1.3         R           87.5         87.85         0.35         CBSH           87.85         88.2         0.35         R           88.2         88.5         0.3         CBSH	5.7	76	0.3	CBSH	483
80.4       81.6       1.2       R         81.6       81.95       0.35       CBSH         81.95       82.3       0.35       R         82.3       82.5       0.2       CBSH         82.5       83.18       0.68       C       480         83.18       85.05       1.87       R         85.05       85.4       0.35       CBSH         85.4       85.9       0.5       R         85.9       86.2       0.3       CBSH         86.2       87.5       1.3       R         87.5       87.85       0.35       CBSH         87.85       88.2       0.35       R         88.2       88.5       0.3       CBSH	'6	80	4	R	
81.6         81.95         0.35         CBSH           81.95         82.3         0.35         R           82.3         82.5         0.2         CBSH           82.5         83.18         0.68         C         480           83.18         85.05         1.87         R           85.05         85.4         0.35         CBSH           85.4         85.9         0.5         R           85.9         86.2         0.3         CBSH           86.2         87.5         1.3         R           87.5         87.85         0.35         CBSH           87.85         88.2         0.35         R           88.2         88.5         0.3         CBSH	30	80.4	0.4	CBSH	
81.95         82.3         0.35         R           82.3         82.5         0.2         CBSH           82.5         83.18         0.68         C         480           83.18         85.05         1.87         R           85.05         85.4         0.35         CBSH           85.4         85.9         0.5         R           85.9         86.2         0.3         CBSH           86.2         87.5         1.3         R           87.5         87.85         0.35         CBSH           87.85         88.2         0.35         R           88.2         88.5         0.3         CBSH	30.4	81.6	1.2	R	
82.3         82.5         0.2         CBSH           82.5         83.18         0.68         C         480           83.18         85.05         1.87         R           85.05         85.4         0.35         CBSH           85.4         85.9         0.5         R           85.9         86.2         0.3         CBSH           86.2         87.5         1.3         R           87.5         87.85         0.35         CBSH           87.85         88.2         0.35         R           88.2         88.5         0.3         CBSH	31.6	81.95	0.35	CBSH	
82.5     83.18     0.68     C     480       83.18     85.05     1.87     R       85.05     85.4     0.35     CBSH       85.4     85.9     0.5     R       85.9     86.2     0.3     CBSH       86.2     87.5     1.3     R       87.5     87.85     0.35     CBSH       87.85     88.2     0.35     R       88.2     88.5     0.3     CBSH	31.95	82.3	0.35	R	
83.18     85.05     1.87     R       85.05     85.4     0.35     CBSH       85.4     85.9     0.5     R       85.9     86.2     0.3     CBSH       86.2     87.5     1.3     R       87.5     87.85     0.35     CBSH       87.85     88.2     0.35     R       88.2     88.5     0.3     CBSH	32.3	82.5	0.2	CBSH	
85.05         85.4         0.35         CBSH           85.4         85.9         0.5         R           85.9         86.2         0.3         CBSH           86.2         87.5         1.3         R           87.5         87.85         0.35         CBSH           87.85         88.2         0.35         R           88.2         88.5         0.3         CBSH	32.5	83.18	0.68	С	480
85.4     85.9     0.5     R       85.9     86.2     0.3     CBSH       86.2     87.5     1.3     R       87.5     87.85     0.35     CBSH       87.85     88.2     0.35     R       88.2     88.5     0.3     CBSH	33.18	85.05	1.87	R	
85.9     86.2     0.3     CBSH       86.2     87.5     1.3     R       87.5     87.85     0.35     CBSH       87.85     88.2     0.35     R       88.2     88.5     0.3     CBSH	35.05	85.4	0.35	CBSH	
86.2     87.5     1.3     R       87.5     87.85     0.35     CBSH       87.85     88.2     0.35     R       88.2     88.5     0.3     CBSH	35.4	85.9	0.5	R	
87.5     87.85     0.35     CBSH       87.85     88.2     0.35     R       88.2     88.5     0.3     CBSH	35.9	86.2	0.3	CBSH	
87.85     88.2     0.35     R       88.2     88.5     0.3     CBSH	36.2	87.5	1.3	R	
88.2 88.5 0.3 CBSH	37.5	87.85	0.35	CBSH	
	37.85	88.2	0.35	R	
	88.2	88.5	0.3	CBSH	
88.5 89 0.5 R	88.5	89	0.5	R	
Log interpretation of WC18-20C (metres)	og interpre	etation of WC	18-20C (met	res)	
From To Drilled Interpreted lithology Name			· · · · · · · · · · · · · · · · · · ·		Name
thickness			thickness		
0 2.5 2.5 DRIFT DRIFT	)	2.5	2.5	DRIFT	DRIFT
2.5 9.55 7.05 R	2.5	9.55	7.05	R	
9.55 9.7 0.15 CBSH	0.55	9.7	+	CBSH	
9.7 9.9 0.2 C 150			+		150
9.9 10 0.1 DC 150	+		<del> </del>	<del> </del>	
10 10.15 0.15 C 150					
10.15 10.5 0.35 DC 150					
10.5 10.75 0.25 CBSH					
10.75 11.1 0.35 R				<u> </u>	
11.1 11.3 0.2 CBSH			+		
11.3 16.3 5 R			ļ	<del> </del>	
16.3 16.7 0.4 CBSH 130			<del>                                     </del>	<u> </u>	130

Table A-2:	Lithologica	l interpretation	of geophysical logs	
From	То	Drilled thickness	Interpreted lithology	Name
Log interpr	etation of W		tres) continued	
16.7	19.35	2.65	R	
19.35	19.55	0.2	CBSH	
19.55	20.45	0.2	СВЗП	111
20.45	20.43	0.9	CBSH	111
20.45	20.63	0.2	R	
21.4	21.4	0.73	CR	
21.4	22.05	0.23	C	110
22.05	22.03	0.4	DC	101
	+			
22.4	22.65	0.25	C	101
22.65	24.25	1.6	C	100
24.25	24.5	0.25	DC	100
24.5	26.45	1.95	R	
26.45	26.8	0.35	CBSH	
26.8	28.25	1.45	R	
28.25	28.8	0.55	C	201
28.8	29	0.2	CR	
29	29.45	0.45	CBSH	
29.45	30.4	0.95	R	
30.4	30.55	0.15	CBSH	
30.55	30.75	0.2	С	202
30.75	30.85	0.1	CR	202
30.85	30.98	0.13	DC	202
30.98	31.07	0.09	CR	202
31.07	31.32	0.25	DC	202
31.32	31.5	0.18	CBSH	
31.5	37	5.5	R	
37	37.2	0.2	CBSH	310?
37.2	41.55	4.35	R	
41.55	41.7	0.15	CBSH	
41.7	42.35	0.65	C	300
42.35	42.45	0.1	DC	300
42.45	42.6	0.15	CBSH	
42.6	44.25	1.65	R	
44.25	44.4	0.15	IRST	IRONSTONE
44.4	44.65	0.25	R	
44.65	44.85	0.2	CBSH	320
44.85	70.65	25.8	R	
70.65	71.1	0.45	DC	430
71.1	72	0.9	R	

Table A-2	: Lithologica		of geophysical logs	,
From	То	Drilled	Interpreted lithology	Name
		thickness		
			tres) continued	
72	72.35	0.35	CBSH	
72.35	73.8	1.45	R	
73.8	74	0.2	CBSH	
74	74.2	0.2	CR	
74.2	74.8	0.6	C	410
74.8	75.8	1	R	
75.8	76	0.2	CBSH	
76	76.75	0.75	C	401
76.75	77	0.25	CBSH	
77	82.42	5.42	R	
82.42	83	0.58	С	400
83	83.42	0.42	DC	400
83.42	83.55	0.13	CR	
83.55	83.7	0.15	C	420
83.7	83.8	0.1	DC	420
83.8	83.9	0.1	C	420
83.9	84.15	0.25	CR	
84.15	84.95	0.8	R	
84.95	85.3	0.35	С	440
85.3	85.4	0.1	DC	440
85.4	85.65	0.25	С	440
85.65	85.85	0.2	DC	440
85.85	85.95	0.1	CBSH	
85.95	86.25	0.3	R	
86.25	86.5	0.25	CR	
86.5	86.75	0.25	DC	442
86.75	97.5	10.75	R	
97.5	97.75	0.25	CBSH	463
97.75	103.35	5.6	R	
103.35	103.5	0.15	CBSH	460
103.5	103.7	0.2	CR	460
103.7	103.85	0.15	CBSH	460
103.85	106.4	2.55	R	
106.4	106.75	0.35	CBSH	483
106.75	108.95	2.2	R	
108.95	109.15	0.2	CBSH	
109.15	109.45	0.3	C	480
109.45	109.6	0.15	DC	480
109.6	110.2	0.6	C	480

Table A-2:	Lithological i	nterpretation	of geophysical logs	
From	То	Drilled	Interpreted lithology	Name
		thickness		
Log interpre	etation of WC	C18-20C (met	res) continued	
110.2	112.7	2.5	R	
112.7	113.05	0.35	CBSH	
113.05	113.5	0.45	R	
113.5	113.85	0.35	CBSH	
113.85	114.4	0.55	R	
114.4	114.6	0.2	CBSH	
114.6	114.8	0.2	DC	A71
114.8	114.9	0.1	CR	A71
114.9	115	0.1	DC	A71
115	115.1	0.1	CR	
115.1	115.2	0.1	CBSH	
115.2	117.45	2.25	R	
117.45	117.7	0.25	CBSH	
117.7	117.95	0.25	С	A7
117.95	118.2	0.25	CBSH	
118.2	119.05	0.85	R	
119.05	119.2	0.15	CBSH	
119.2	119.45	0.25	CR	A72
119.45	119.8	0.35	CBSH	
119.8	125.3	5.5	R	
125.3	125.8	0.5	CBSH	A5
125.8	125.9	0.1	CR	A5
125.9	126.15	0.25	CBSH	A5
126.15	132.75	6.6	R	
132.75	133.15	0.4	DC	A3
133.15	133.5	0.35	R	
133.5	133.8	0.3	CBSH	
133.8	135.3	1.5	R	
135.3	135.5	0.2	CBSH	
135.5	136.15	0.65	С	A1
136.15	136.61	0.46	R	
Log interpre	etation of WC	218-21C (met	res)	
From	То	Drilled thickness	Interpreted lithology	Name
0	5.3	5.3	DRIFT	DRIFT
5.3	24.7	19.4	R	
24.7	24.85	0.15	CBSH	

			n of geophysical logs	
From	То	Drilled thickness	Interpreted lithology	Name
Log interp	retation of V		tres) continued	
24.85	25.15	0.3	DC	430
25.15	28.25	3.1	R	
28.25	28.4	0.15	CBSH	
28.4	28.55	0.15	CR	
28.55	29.35	0.8	С	410
29.35	29.55	0.2	CBSH	
29.55	30.85	1.3	R	
30.85	31.8	0.95	С	401
31.8	32	0.2	CR	
32	34.2	2.2	R	
34.2	35.75	1.55	С	400
35.75	35.9	0.15	DC	400
35.9	36.05	0.15	С	420
36.05	36.3	0.25	CR	
36.3	37.1	0.8	R	
37.1	37.4	0.3	С	440
37.4	37.7	0.3	DC	440
37.7	38	0.3	С	440
38	38.5	0.5	R	
38.5	38.8	0.3	CBSH	
38.8	39.1	0.3	С	442
39.1	39.2	0.1	CBSH	
39.2	55.05	15.85	R	
55.05	55.25	0.2	CBSH	460
55.25	55.4	0.15	CR	460
55.4	55.5	0.1	CBSH	460
55.5	57.9	2.4	R	
57.9	60	0.1	CBSH	483
60	60.55	0.55	R	
60.55	60.7	0.15	CBSH	
60.7	61.55	0.85	C	480
61.55	63	1.45	R	
63	63.35	0.35	CBSH	
63.35	64.8	1.45	R	
64.8	65.1	0.3	CBSH	A71
65.1	65.3	0.2	CR	A71
65.3	67.7	2.4	R	
67.7	68.2	0.5	C	A7
68.2	69.1	0.9	R	

Table A-2	: Lithologica	al interpretation	of geophysical logs	
From	То	Drilled	Interpreted lithology	Name
		thickness		
Log interp		VC18-21C (me	tres) continued	
69.1	69.5	0.4	DC	A72
69.5	71	1.5	R	
Log interp	retation of V	VC18-22C (me		
From	То	Drilled	Interpreted lithology	Name
		thickness		
0	2.45	2.45	DRIFT	DRIFT
2.45	9.05	6.6	R	
9.05	9.3	0.25	CBSH	
9.3	9.45	0.15	С	150
9.45	9.8	0.35	DC	150
9.8	9.95	0.15	CR	150
9.95	10.05	0.1	DC	150
10.05	10.1	0.05	CR	
10.1	10.9	0.8	CBSH	
10.9	12.45	1.55	R	
12.45	12.8	0.35	CBSH	
12.8	14.95	2.15	R	
14.95	15.5	0.55	CBSH	130
15.5	18.2	2.7	R	
18.2	19.15	0.95	C	111
19.15	19.3	0.15	CBSH	
19.3	20.85	1.55	R	
20.85	21.3	0.45	C	110
21.3	21.6	0.3	DC	110
21.6	22.05	0.45	C	101
22.05	23.7	1.65	C	100
23.7	24.12	0.42	DC	100
24.12	24.6	0.48	CBSH	
24.6	26.55	1.95	R	
26.55	26.9	0.35	CBSH	
26.9	27.35	0.45	R	
27.35	27.55	0.2	CBSH	
27.55	28.1	0.55	С	201
28.1	28.3	0.2	CR	
28.3	28.8	0.5	CBSH	
28.8	29.8	1	R	
29.8	30.2	0.4	C	202

From	To	Drilled	of geophysical logs Interpreted lithology	Name
		thickness		
Log inter	pretation of V		tres) continued	
30.2	30.3	0.1	CR	202
30.3	30.4	0.1	DC	202
30.4	30.5	0.1	CR	202
30.5	30.72	0.22	DC	202
30.72	30.85	0.13	CBSH	
30.85	35.6	4.75	R	
35.6	35.8	0.2	CBSH	
35.8	36.65	0.85	R	
36.65	37.05	0.4	CBSH	
37.05	37.75	0.7	R	
37.75	38.15	0.4	IRST	IRONSTONE
38.15	40.95	2.8	R	
40.95	41.4	0.45	CBSH	
41.4	42.35	0.95	R	
42.35	42.6	0.25	CBSH	
42.6	43.1	0.5	С	300
43.1	43.35	0.25	CR	
43.35	44.25	0.9	R	
44.25	44.65	0.4	CBSH	
44.65	46.5	1.85	R	
46.5	46.7	0.2	CBSH	320
46.7	46.9	0.2	CR	320
46.9	47.2	0.3	CBSH	320
47.2	60.05	12.85	R	
60.05	61.05	1	CBSH	340
61.05	64.6	3.55	R	340
64.6	65	0.4	CBSH	340
65	65.85	0.85	R	340
65.85	66.4	0.55	CBSH	340
66.4	75.1	8.7	R	340
75.1	75.25	0.15	CR	
75.25	75.6	0.35	С	430
75.6	79	3.4	R	
79	79.2	0.2	CBSH	
79.2	79.4	0.2	CR	
79.4	80.1	0.7	С	410
80.1	80.25	0.15	CBSH	
80.25	81.5	1.25	R	
81.5	81.65	0.15	CBSH	

From         To         Drilled thickness         Interpreted lithology thickness         Name           81.65         81.85         0.2         DC         401           81.85         82.45         0.6         C         401           82.45         82.6         0.15         CR           82.45         82.6         0.15         CR           82.6         82.95         0.35         CBSH           82.95         84.6         1.65         C         400           84.6         85.15         0.55         C         420           85.15         85.4         0.25         CR         85.1         85.4         0.25         CR           85.4         85.6         0.2         CBSH         86.8         86.1         0.5         R         86.3         86.5         0.25         CBSH         86.35         0.25         CBSH         86.35         86.5         0.15         C         440 <th>Table A-2:</th> <th>: Lithologica</th> <th>l interpretation</th> <th>of geophysical logs</th> <th></th>	Table A-2:	: Lithologica	l interpretation	of geophysical logs	
81.65         81.85         0.2         DC         401           81.85         82.45         0.6         C         401           82.45         82.6         0.15         CR           82.6         82.95         0.35         CBSH           82.95         84.6         1.65         C         400           84.6         85.15         0.55         C         420           85.15         85.4         0.25         CR         2           85.15         85.4         0.25         CR         420           85.6         86.1         0.5         R         86.1         86.5         86.1         0.5         R           86.1         86.5         0.2         CBSH         86.3         86.5         86.6         0.1         DC         440           86.5         86.6         0.1         DC         440         40         40         86.85         87.15         0.3         C         440         40         40         86.85         87.15         0.3         C         440         40         40         86.85         87.15         0.3         C         442         440         86.85         87.15			thickness		Name
81.85         82.45         0.6         C         401           82.45         82.6         0.15         CR           82.6         82.95         0.35         CBSH           82.95         84.6         1.65         C         400           84.6         85.15         0.55         C         420           85.15         85.4         0.25         CR         CBSH           85.4         85.6         0.2         CBSH         S6.6           85.6         86.1         0.2         CBSH         S6.5           86.1         86.35         0.25         CBSH         S6.5           86.5         0.15         C         440           86.5         86.6         0.1         DC         440           86.7         86.85         0.15         DC         440           86.85         87.15         0.3         C         440           86.85         87.15         0.3         C         440           88.80         99.5         10.9         R           99.5         99.7         0.2         CBSH         463           103.75         4.05         R	Log interp	retation of W	/C18-22C (me	tres) continued	
82.45         82.6         0.15         CR           82.6         82.95         0.35         CBSH           82.95         84.6         1.65         C         400           84.6         85.15         0.55         C         420           85.15         85.4         0.25         CR         85.4         85.6         0.2         CBSH           85.6         86.1         0.5         R         86.1         86.5         86.1         86.5         86.5         86.5         86.6         0.1         DC         440         86.85         87.15         88.3         1.15         R         440         88.6         87.15         88.3         1.15         R         442         88.6         99.5         10.9         R         463         99.5         10.9         R         463         99.7         103.7	81.65	81.85	0.2	DC	401
82.6         82.95         0.35         CBSH           82.95         84.6         1.65         C         400           84.6         85.15         0.55         C         420           85.15         85.4         0.25         CR         85.1         85.6         0.2         CBSH           85.6         86.1         0.5         R         86.1         86.35         0.25         CBSH           86.35         86.5         0.15         C         440           86.5         86.6         0.1         DC         440           86.6         86.7         0.1         C         440           86.85         0.15         DC         440           86.85         87.15         0.3         C         440           87.15         88.3         1.15         R         88.3         88.6         0.3         C         442           88.3         88.6         0.3         C         442         463         99.5         10.9         R         99.5         10.9         R         99.7         0.2         CBSH         463         99.7         0.2         CBSH         460         463         99.7	81.85	82.45	0.6	C	401
82.95         84.6         1.65         C         400           84.6         85.15         0.55         C         420           85.15         85.4         0.25         CR         CR           85.4         85.6         0.2         CBSH         CBSH           85.6         86.1         0.5         R         R           86.1         86.35         0.25         CBSH         CBSH           86.5         86.6         0.1         DC         440           86.6         86.7         0.1         C         440           86.7         86.85         0.15         DC         440           86.7         86.85         0.15         DC         440           86.85         87.15         0.3         C         440           86.85         87.15         0.3         C         442           88.8         3         1.15         R           88.6         0.3         C         442           88.6         99.5         10.9         R           99.7         103.75         4.05         R           104.15         0.4         CR         460	82.45	82.6	0.15	CR	
84.6         85.15         0.55         C         420           85.15         85.4         0.25         CR           85.6         85.6         0.2         CBSH           85.6         86.1         0.5         R           86.1         86.35         0.25         CBSH           86.35         86.5         0.15         C         440           86.5         86.6         0.1         DC         440           86.7         86.85         0.15         DC         440           86.7         86.85         0.15         DC         440           86.7         86.85         0.15         DC         440           86.85         87.15         0.3         C         440           87.15         88.3         1.15         R           88.3         88.6         0.3         C         442           88.6         99.5         10.9         R           99.7         0.2         CBSH         463           99.7         10.2         CBSH         460           104.15         10.4         CR         460           104.15         10.4         CR	82.6	82.95	0.35	CBSH	
85.15         85.4         0.25         CR           85.6         85.6         0.2         CBSH           85.6         86.1         0.5         R           86.1         86.35         0.25         CBSH           86.35         86.5         0.15         C         440           86.5         86.6         0.1         DC         440           86.7         86.85         0.15         DC         440           86.85         87.15         0.3         C         440           87.15         88.3         1.15         R           88.3         88.6         0.3         C         442           88.6         99.5         10.9         R           99.7         0.2         CBSH         463           99.7         103.75         4.05         R           103.75         104.15         0.4         CR         460           104.15         106         1.85         R         Interpreted lithology         Name           From         To         Drilled thickness         Interpreted lithology         Name           10         10.15         0.15         CBSH         340	82.95	84.6	1.65	С	400
85.4         85.6         86.1         0.5         R           86.1         86.35         0.25         CBSH           86.35         86.5         0.15         C         440           86.6         86.6         0.1         DC         440           86.6         86.7         0.1         C         440           86.7         86.85         0.15         DC         440           86.85         87.15         0.3         C         440           87.15         88.3         1.15         R           88.3         88.6         0.3         C         442           88.6         99.5         10.9         R           99.7         103.75         4.05         R           103.75         104.15         0.4         CR         460           104.15         106         1.85         R           Log interpretation of WC18-23C (metres)         Name           From         To         Drilled thickness         Interpreted lithology         Name           10         10.15         0.15         CBSH         340           10.3         10.6         0.3         CBSH         340	84.6	85.15	0.55	С	420
85.6         86.1         0.5         R           86.1         86.35         0.25         CBSH           86.35         86.5         0.15         C         440           86.5         86.6         0.1         DC         440           86.7         86.85         0.15         DC         440           86.85         87.15         0.3         C         440           87.15         88.3         1.15         R           88.3         88.6         0.3         C         442           88.6         99.5         10.9         R           99.5         99.7         0.2         CBSH         463           99.7         103.75         4.05         R         460           104.15         10.4         CR         460           104.15         10.6         1.85         R           Log interpretation of WC18-23C (metres)         Name           From         To         Drilled thickness         Name           0         5.45         5.45         DRIFT         DRIFT           5.45         10         4.55         R         340           10.15         0.15         <	85.15	85.4	0.25	CR	
86.1         86.35         0.25         CBSH           86.35         86.5         0.15         C         440           86.5         86.6         0.1         DC         440           86.6         86.7         0.1         C         440           86.7         86.85         0.15         DC         440           86.85         87.15         0.3         C         440           87.15         88.3         1.15         R           88.3         88.6         0.3         C         442           88.6         99.5         10.9         R           99.5         99.7         0.2         CBSH         463           99.7         103.75         4.05         R           104.15         106         1.85         R	85.4	85.6	0.2	CBSH	
86.35         86.6         0.1         DC         440           86.6         86.7         0.1         C         440           86.7         86.85         0.15         DC         440           86.7         86.85         0.15         DC         440           86.85         87.15         0.3         C         440           87.15         88.3         1.15         R           88.3         88.6         0.3         C         442           88.6         99.5         10.9         R         99.5         99.7         0.2         CBSH         463           99.7         103.75         4.05         R         460<	85.6	86.1	0.5	R	
86.5         86.6         0.1         DC         440           86.6         86.7         0.1         C         440           86.7         86.85         0.15         DC         440           86.85         87.15         0.3         C         440           87.15         88.3         1.15         R           88.3         88.6         0.3         C         442           88.6         99.5         10.9         R           99.5         99.7         0.2         CBSH         463           99.7         103.75         4.05         R           103.75         104.15         0.4         CR         460           104.15         106         1.85         R                 From         To         Drilled thickness         Name           0         5.45         5.45         DRIFT         DRIFT           5.45         10         4.55         R           10         10.15         0.15         CBSH         340           10.3         10.6         0.3         CBSH         340           10.6 <td>86.1</td> <td>86.35</td> <td>0.25</td> <td>CBSH</td> <td></td>	86.1	86.35	0.25	CBSH	
86.6         86.7         0.1         C         440           86.7         86.85         0.15         DC         440           86.85         87.15         0.3         C         440           87.15         88.3         1.15         R           88.3         88.6         0.3         C         442           88.6         99.5         10.9         R           99.5         99.7         0.2         CBSH         463           99.7         103.75         4.05         R           103.75         104.15         0.4         CR         460           104.15         106         1.85         R	86.35	86.5	0.15	С	440
86.6         86.7         0.1         C         440           86.7         86.85         0.15         DC         440           86.85         87.15         0.3         C         440           87.15         88.3         1.15         R           88.3         88.6         0.3         C         442           88.6         99.5         10.9         R           99.5         99.7         0.2         CBSH         463           99.7         103.75         4.05         R           103.75         104.15         0.4         CR         460           104.15         106         1.85         R	86.5	86.6	0.1	DC	440
86.7         86.85         0.15         DC         440           86.85         87.15         0.3         C         440           87.15         88.3         1.15         R           88.3         88.6         0.3         C         442           88.6         99.5         10.9         R         99.7         0.2         CBSH         463           99.7         103.75         4.05         R         460         460           103.75         104.15         0.4         CR         460           104.15         106         1.85         R           Log interpretation of WC18-23C (metres)         From         To         Drilled thickness           From         To         Drilled thickness         Name           0         5.45         5.45         DRIFT         DRIFT           5.45         10         4.55         R           10         10.15         0.15         CBSH         340           10.3         10.6         0.3         CBSH         340           10.6         11.5         0.9         R         340           11.5         11.65         0.15         CBSH         3		_	0.1		440
86.85         87.15         0.3         C         440           87.15         88.3         1.15         R           88.3         88.6         0.3         C         442           88.6         99.5         10.9         R           99.5         99.7         0.2         CBSH         463           99.7         103.75         4.05         R           103.75         104.15         0.4         CR         460           104.15         106         1.85         R                 Log interpretation of WC18-23C (metres)         Name           From         To         Drilled thickness         Interpreted lithology         Name           0         5.45         5.45         DRIFT         DRIFT           5.45         10         4.55         R         10           10.15         0.15         CBSH         340           10.15         10.3         0.15         R         340           10.6         11.5         0.9         R         340           11.5         11.65         0.15         CBSH         340				+	
87.15         88.3         1.15         R           88.3         88.6         0.3         C         442           88.6         99.5         10.9         R           99.5         99.7         0.2         CBSH         463           99.7         103.75         4.05         R           103.75         104.15         0.4         CR         460           104.15         106         1.85         R                 Log interpretation of WC18-23C (metres)         Name           From         To         Drilled thickness         Name           0         5.45         5.45         DRIFT         DRIFT           5.45         10         4.55         R         10           10.15         0.15         CBSH         340           10.15         10.3         0.15         R         340           10.6         11.5         0.9         R         340           11.5         11.65         0.15         CBSH         340           11.65         14.6         2.95         R         340           14.6         15.1					440
88.3       88.6       0.3       C       442         88.6       99.5       10.9       R         99.5       99.7       0.2       CBSH       463         99.7       103.75       4.05       R       460         103.75       104.15       0.4       CR       460         104.15       106       1.85       R          Log interpretation of WC18-23C (metres)         From       To       Drilled thickness       Interpreted lithology       Name         0       5.45       5.45       DRIFT       DRIFT         5.45       10       4.55       R         10       10.15       0.15       CBSH       340         10.15       10.3       0.15       R       340         10.6       11.5       0.9       R       340         11.5       11.65       0.15       CBSH       340         11.65       14.6       2.95       R       340         15.1       15.85       0.75       R       340         15.85       16.1       0.25       CBSH       340		_			
88.6         99.5         10.9         R           99.5         99.7         0.2         CBSH         463           99.7         103.75         4.05         R           103.75         104.15         0.4         CR         460           104.15         106         1.85         R                 From         To         Drilled thickness         Interpreted lithology         Name           0         5.45         5.45         DRIFT         DRIFT           5.45         10         4.55         R           10         10.15         0.15         CBSH         340           10.15         10.3         0.15         R         340           10.6         11.5         0.9         R         340           11.5         11.65         0.15         CBSH         340           11.65         14.6         2.95         R         340           14.6         15.1         0.5         CBSH         340           15.1         15.85         0.75         R         340           15.85         16.1         0.25         CB					442
99.5         99.7         0.2         CBSH         463           99.7         103.75         4.05         R         460           103.75         104.15         0.4         CR         460           104.15         106         1.85         R           Log interpretation of WC18-23C (metres)           From         To         Drilled thickness           0         5.45         5.45         DRIFT         DRIFT           5.45         10         4.55         R         10         10.15         0.15         CBSH         340           10.15         10.3         0.15         R         340         340         340           10.6         11.5         0.9         R         340	88.6	99.5	10.9	R	
99.7         103.75         4.05         R           103.75         104.15         0.4         CR         460           104.15         106         1.85         R           Log interpretation of WC18-23C (metres)           From         To         Drilled thickness         Interpreted lithology         Name           0         5.45         5.45         DRIFT         DRIFT           5.45         10         4.55         R         Name           10         10.15         0.15         CBSH         340           10.15         10.3         0.15         R         340           10.3         10.6         0.3         CBSH         340           11.5         11.65         0.15         CBSH         340           11.65         14.6         2.95         R         340           14.6         15.1         0.5         CBSH         340           15.1         15.85         0.75         R         340           15.85         16.1         0.25         CBSH         340			_	CBSH	463
103.75         104.15         0.4         CR         460           104.15         106         1.85         R                 Log interpretation of WC18-23C (metres)          Name           From         To         Drilled thickness         Interpreted lithology         Name           0         5.45         5.45         DRIFT         DRIFT           5.45         10         4.55         R           10         10.15         0.15         CBSH         340           10.15         10.3         0.15         R         340           10.3         10.6         0.3         CBSH         340           10.6         11.5         0.9         R         340           11.5         11.65         0.15         CBSH         340           11.65         14.6         2.95         R         340           14.6         15.1         0.5         CBSH         340           15.1         15.85         0.75         R         340           15.85         16.1         0.25         CBSH         340					
104.15       106       1.85       R         Log interpretation of WC18-23C (metres)         From       To       Drilled thickness       Interpreted lithology       Name         0       5.45       5.45       DRIFT       DRIFT         5.45       10       4.55       R         10       10.15       0.15       CBSH       340         10.15       10.3       0.15       R       340         10.3       10.6       0.3       CBSH       340         10.6       11.5       0.9       R       340         11.5       11.65       0.15       CBSH       340         11.65       14.6       2.95       R       340         14.6       15.1       0.5       CBSH       340         15.1       15.85       0.75       R       340         15.85       16.1       0.25       CBSH       340			_		460
Log interpretation of WC18-23C (metres)					
From         To         Drilled thickness         Interpreted lithology         Name           0         5.45         5.45         DRIFT         DRIFT           5.45         10         4.55         R           10         10.15         0.15         CBSH         340           10.15         10.3         0.15         R         340           10.3         10.6         0.3         CBSH         340           10.6         11.5         0.9         R         340           11.5         11.65         0.15         CBSH         340           11.65         14.6         2.95         R         340           14.6         15.1         0.5         CBSH         340           15.1         15.85         0.75         R         340           15.85         16.1         0.25         CBSH         340					
From         To         Drilled thickness         Interpreted lithology         Name           0         5.45         5.45         DRIFT         DRIFT           5.45         10         4.55         R           10         10.15         0.15         CBSH         340           10.15         10.3         0.15         R         340           10.3         10.6         0.3         CBSH         340           10.6         11.5         0.9         R         340           11.5         11.65         0.15         CBSH         340           11.65         14.6         2.95         R         340           14.6         15.1         0.5         CBSH         340           15.1         15.85         0.75         R         340           15.85         16.1         0.25         CBSH         340	Log intern	retation of W	/C18-23C (me	tres)	
0         5.45         5.45         DRIFT         DRIFT           5.45         10         4.55         R           10         10.15         0.15         CBSH         340           10.15         10.3         0.15         R         340           10.3         10.6         0.3         CBSH         340           10.6         11.5         0.9         R         340           11.5         11.65         0.15         CBSH         340           11.65         14.6         2.95         R         340           14.6         15.1         0.5         CBSH         340           15.1         15.85         0.75         R         340           15.85         16.1         0.25         CBSH         340			Drilled		Name
5.45         10         4.55         R           10         10.15         0.15         CBSH         340           10.15         10.3         0.15         R         340           10.3         10.6         0.3         CBSH         340           10.6         11.5         0.9         R         340           11.5         11.65         0.15         CBSH         340           11.65         14.6         2.95         R         340           14.6         15.1         0.5         CBSH         340           15.1         15.85         0.75         R         340           15.85         16.1         0.25         CBSH         340	0	5.45		DRIFT	DRIFT
10         10.15         0.15         CBSH         340           10.15         10.3         0.15         R         340           10.3         10.6         0.3         CBSH         340           10.6         11.5         0.9         R         340           11.5         11.65         0.15         CBSH         340           11.65         14.6         2.95         R         340           14.6         15.1         0.5         CBSH         340           15.1         15.85         0.75         R         340           15.85         16.1         0.25         CBSH         340		_	_	+	
10.15       10.3       0.15       R       340         10.3       10.6       0.3       CBSH       340         10.6       11.5       0.9       R       340         11.5       11.65       0.15       CBSH       340         11.65       14.6       2.95       R       340         14.6       15.1       0.5       CBSH       340         15.1       15.85       0.75       R       340         15.85       16.1       0.25       CBSH       340			<del>-  </del>		340
10.3       10.6       0.3       CBSH       340         10.6       11.5       0.9       R       340         11.5       11.65       0.15       CBSH       340         11.65       14.6       2.95       R       340         14.6       15.1       0.5       CBSH       340         15.1       15.85       0.75       R       340         15.85       16.1       0.25       CBSH       340			<del></del>	+	
10.6     11.5     0.9     R     340       11.5     11.65     0.15     CBSH     340       11.65     14.6     2.95     R     340       14.6     15.1     0.5     CBSH     340       15.1     15.85     0.75     R     340       15.85     16.1     0.25     CBSH     340		+		+	
11.5       11.65       0.15       CBSH       340         11.65       14.6       2.95       R       340         14.6       15.1       0.5       CBSH       340         15.1       15.85       0.75       R       340         15.85       16.1       0.25       CBSH       340				+	
11.65     14.6     2.95     R     340       14.6     15.1     0.5     CBSH     340       15.1     15.85     0.75     R     340       15.85     16.1     0.25     CBSH     340					
14.6     15.1     0.5     CBSH     340       15.1     15.85     0.75     R     340       15.85     16.1     0.25     CBSH     340				<del></del>	
15.1     15.85     0.75     R     340       15.85     16.1     0.25     CBSH     340					
15.85 16.1 0.25 CBSH 340		+	_	+	
			_	+	
16.1   30.6   14.5   R				+	3.10

Table A-2:	Lithological i	interpretation	of geophysical logs	
From	То	Drilled thickness	Interpreted lithology	Name
Log interpre	etation of WC		res) continued	
30.6	30.8	0.2	CR	
30.8	31.15	0.35	С	430
31.15	34.7	3.55	R	
34.7	34.9	0.2	CBSH	
34.9	35.05	0.15	CR	
35.05	35.8	0.75	С	410
35.8	35.95	0.15	CR	
35.95	37.15	1.2	R	
37.15	37.4	0.25	CR	
37.4	38.05	0.65	С	401
38.05	38.3	0.25	DC	401
38.3	38.45	0.15	CR	
38.45	39.8	1.35	C	400
39.8	39.9	0.1	DC	400
39.9	40.32	0.42	С	420
40.32	40.75	0.43	R	
40.75	40.9	0.15	CBSH	440
40.9	41.6	0.7	R	
41.6	41.85	0.25	CBSH	442
41.85	42.05	0.2	CR	442
42.05	52.85	10.8	R	
52.85	53.35	0.5	CBSH	463
53.35	57.7	4.35	R	
57.7	58.03	0.33	CR	460
58.03	61.7	3.67	R	
61.7	62.1	0.4	CBSH	483
62.1	65.35	3.25	R	
65.35	65.7	0.35	С	480
65.7	65.85	0.15	DC	480
65.85	65.9	0.05	С	480
65.9	66	0.1	DC	480
66	66.2	0.2	С	480
66.2	66.4	0.2	CR	
66.4	69.2	2.8	R	
69.2	70.45	1.25	CBSH	
70.45	71	0.55	R	

			of geophysical logs	
		VC18-24C (me		
From	То	Drilled thickness	Interpreted lithology	Name
0	1.4	1.4	DRIFT	DRIFT
1.4	3.95	2.55	R	
3.95	4.2	0.25	DC	410
4.2	5.05	0.85	С	410
5.05	5.35	0.3	CR	
5.35	6.5	1.15	R	
6.5	6.8	0.3	CBSH	
6.8	8.15	1.35	R	
8.15	8.5	0.35	CR	
8.5	10	1.5	С	401
10	12.15	2.15	С	400
12.15	12.35	0.2	DC	400
12.35	12.7	0.35	С	420
12.7	12.8	0.1	DC	420
12.8	12.95	0.15	С	420
12.95	13.2	0.25	CR	
13.2	14.4	1.2	R	
14.4	14.6	0.2	CR	
14.6	14.8	0.2	С	440
14.8	14.9	0.1	DC	440
14.9	15.45	0.55	С	440
15.45	15.6	0.15	CBSH	
15.6	17.5	1.9	R	
17.5	17.9	0.4	DC	442
17.9	26.6	8.7	R	
26.6	27	0.4	CBSH	463
27	31.35	4.35	R	
31.35	31.7	0.35	DC	460
31.7	35.1	3.4	R	
35.1	35.35	0.25	CBSH	483
35.35	41.3	5.95	R	
41.3	41.5	0.2	CBSH	
41.5	42.5	1	С	480
42.5	42.65	0.15	CBSH	
42.65	44.15	1.5	R	
44.15	44.55	0.4	CBSH	
44.55	45.6	1.05	R	
45.6	46	0.4	CBSH	
46	46.4	0.4	R	

Table A-2:	Lithological	interpretation	of geophysical logs	
Log interpr	retation of W	C18-24C (me	tres) continued	
From	То	Drilled thickness	Interpreted lithology	Name
46.4	46.65	0.25	CBSH	
46.65	46.9	0.25	CR	A71
46.9	47.25	0.35	С	A71
47.25	48.7	1.45	R	
48.7	48.85	0.15	CBSH	
48.85	49.2	0.35	С	A7
49.2	49.3	0.1	CR	A7
49.3	49.8	0.5	R	
49.8	50	0.2	CBSH	A72
50	50.15	0.15	CR	A72
50.15	50.35	0.2	CBSH	A72
50.35	57.5	7.15	R	
57.5	58.05	0.55	CBSH	
58.05	58.25	0.2	CR	A5
58.25	58.4	0.15	CBSH	
58.4	64.1	5.7	R	
64.1	64.5	0.4	DC	A3
64.5	64.85	0.35	R	
64.85	65.15	0.3	CBSH	
65.15	65.7	0.55	R	
65.7	65.8	0.1	CBSH	
65.8	68	2.2	R	
<del>-</del>	2777			
		C18-25C (met	1 '	T
From	То	Drilled thickness	Interpreted lithology	Name
0	1.85	1.85	DRIFT	DRIFT
1.85	2.5	0.65	R	
2.5	2.65	0.15	IRST	IRONSTONE
2.65	6.55	3.9	R	
6.55	6.9	0.35	CBSH	170
6.9	14.8	7.9	R	
14.8	14.95	0.15	CBSH	
14.95	15.1	0.15	С	150
15.1	15.2	0.1	DC	150
15.2	15.6	0.4	С	150
15.6	15.9	0.3	CR	
15.9	16.5	0.6	CBSH	

Table A-2:	Lithological	l interpretation	of geophysical logs	
			etres) continued	
From	То	Drilled thickness	Interpreted lithology	Name
16.5	20.6	4.1	R	
20.6	20.8	0.2	CBSH	
20.8	21.05	0.25	CR	130
21.05	23.2	2.15	R	
23.2	23.6	0.4	CBSH	
23.6	24.3	0.7	С	111
24.3	24.5	0.2	CBSH	
24.5	25.2	0.7	R	
25.2	25.45	0.25	CR	
25.45	26.12	0.67	С	110
26.12	26.6	0.48	С	101
26.6	28.5	1.9	С	100
28.5	29.1	0.6	CR	
29.1	29.6	0.5	CBSH	
29.6	30.05	0.45	R	
30.05	30.5	0.45	IRST	IRONSTONE
30.5	30.9	0.4	R	
30.9	31.3	0.4	CBSH	
31.3	31.85	0.55	R	
31.85	32.1	0.25	CBSH	
32.1	32.25	0.15	DC	201
32.25	32.8	0.55	C	201
32.8	33.1	0.3	CR	
33.1	34.6	1.5	R	
34.6	34.8	0.2	DC	202
34.8	35.03	0.23	C	202
35.03	35.23	0.2	DC	202
35.23	35.4	0.17	R	202
35.4	35.65	0.25	C	202
35.65	50.8	15.15	R	
50.8	51	0.2	CR	300
51	51.2	0.2	CBSH	
51.2	53.05	1.85	R	
53.05	53.6	0.55	CBSH	320
53.6	80.8	27.2	R	
80.8	81	0.2	CBSH	
81	81.18	0.18	С	430
81.18	81.45	0.27	DC	430
81.45	84.95	3.5	R	

Log interp	oretation of V	VC18-25C (me	etres) continued	
From	То	Drilled thickness	Interpreted lithology	Name
84.95	85.15	0.2	CBSH	
85.15	85.35	0.2	CR	
85.35	86.18	0.83	С	410
86.18	87.2	1.02	R	
87.2	87.38	0.18	CBSH	
87.38	88.4	1.02	С	401
88.4	90.75	2.35	R	
90.75	92.1	1.35	С	400
92.1	92.6	0.5	DC	400
92.6	92.8	0.2	С	420
92.8	93	0.2	DC	420
93	93.1	0.1	CBSH	
93.1	93.85	0.75	R	
93.85	94.05	0.2	CBSH	
94.05	94.35	0.3	CR	
94.35	94.7	0.35	DC	440
94.7	95.1	0.4	С	440
95.1	96	0.9	R	
96	96.45	0.45	С	442
96.45	105.7	9.25	R	
105.7	105.95	0.25	CBSH	463
105.95	111.2	5.25	R	
111.2	111.4	0.2	CBSH	460
111.4	111.55	0.15	CR	460
111.55	111.75	0.2	CBSH	460
111.75	114.9	3.15	R	
114.9	115.3	0.4	CBSH	483
115.3	118.45	3.15	R	
118.45	118.55	0.1	CBSH	
118.55	118.65	0.1	CR	
118.65	118.98	0.33	DC	480
118.98	119.5	0.52	С	480
119.5	119.7	0.2	CBSH	
119.7	121.9	2.2	R	
121.9	122.28	0.38	CBSH	
122.28	122.95	0.67	R	
122.95	123.35	0.4	CBSH	
123.35	124	0.65	R	
124	124.48	0.48	С	A71

Log inter	pretation of V	VC18-25C (me	etres) continued	
From	То	Drilled thickness	Interpreted lithology	Name
124.48	126.5	2.02	R	
126.5	126.75	0.25	CBSH	
126.75	127.07	0.32	DC	A7
127.07	127.25	0.18	CBSH	
127.25	128.4	1.15	R	
128.4	128.8	0.4	CR	A72
128.8	129.15	0.35	CBSH	
129.15	134.9	5.75	R	
134.9	135.4	0.5	CBSH	
135.4	135.6	0.2	CR	A5
135.6	135.75	0.15	CBSH	
135.75	139.5	3.75	R	
139.5	139.75	0.25	CBSH	
139.75	140.25	0.5	R	
Log inter	oretation of W	/C18-26C (me	tres)	-
From	То	Appt	Lith	Name
0	1.3	1.3	DRIFT	DRIFT
1.3	2.7	1.4	R	
2.7	3	0.3	CBSH	320
3	18.7	15.7	R	
18.7	18.8	0.1	CBSH	340
18.8	18.95	0.15	CR	340
18.95	19.1	0.15	CBSH	340
19.1	22.6	3.5	R	340
22.6	22.8	0.2	CBSH	340
22.8	29.4	6.6	R	
29.4	29.85	0.45	CBSH	430
29.85	33.85	4	R	
33.85	34	0.15	CBSH	
34	34.25	0.25	CR	
34.25	34.9	0.65	С	410
34.9	36.1	1.2	R	
36.1	36.3	0.2	CBSH	
36.3	37.15	0.85	C	401
37.15	42.1	4.95	R	
42.1	42.3	0.2	CBSH	
42.3	43.4	1.1	С	400

			of geophysical logs etres) continued	
From	To	Drilled	Interpreted lithology	Name
1 10111	10	thickness	interpreted nullology	Name
43.4	43.65	0.25	С	420
43.65	43.75	0.1	DC	420
43.75	43.9	0.15	C	420
43.9	44.2	0.3	CR	1.20
44.2	44.8	0.6	R	
44.8	45	0.2	CBSH	
45	45.75	0.75	C	440
45.75	46.1	0.35	R	
46.1	46.3	0.2	CBSH	
46.3	46.65	0.35	С	442
46.65	62.7	16.05	R	
62.7	63.05	0.35	CBSH	460
63.05	65.25	2.2	R	
65.25	65.85	0.6	CBSH	483
65.85	68.3	2.45	R	
68.3	68.5	0.2	CBSH	
68.5	69.4	0.9	С	480
69.4	69.5	0.1	DC	480
69.5	69.65	0.15	CBSH	
69.65	71.05	1.4	R	
71.05	71.35	0.3	CBSH	
71.35	72.15	0.8	R	
72.15	72.5	0.35	CBSH	
72.5	74.3	1.8	R	
74.3	74.6	0.3	CR	A71
74.6	78.25	3.65	R	
78.25	78.45	0.2	CBSH	
78.45	78.65	0.2	DC	A7
78.65	78.75	0.1	C	A7
78.75	79.05	0.3	CBSH	
79.05	79.9	0.85	R	
79.9	80.3	0.4	CR	A72
80.3	80.5	0.2	CBSH	
80.5	86.35	5.85	R	
86.35	87.2	0.85	CBSH	A5
87.2	94.05	6.85	R	
94.05	94.2	0.15	CBSH	
94.2	94.45	0.25	DC	A3
94.45	94.65	0.2	R	

Table A-	2: Lithologica	al interpretation	of geophysical logs	
			etres) continued	
From	То	Drilled	Interpreted lithology	Name
		thickness		
94.65	94.95	0.3	CBSH	
94.95	96.15	1.2	R	
96.15	96.35	0.2	CBSH	
96.35	96.95	0.6	С	A1
96.95	97.15	0.2	CBSH	
97.15	98	0.85	R	
Log inter	pretation of V	VC18-27C (me	tres)	
From	То	Drilled	Interpreted lithology	Name
		thickness		
0	3.8	3.8	DRIFT	DRIFT
3.8	4.6	0.8	R	
4.6	4.75	0.15	IRST	IRONSTONE
4.75	4.9	0.15	R	
4.9	5	0.1	IRST	IRONSTONE
5	9.1	4.1	R	
9.1	9.4	0.3	CBSH	
9.4	10.4	1	R	
10.4	10.8	0.4	CBSH	
10.8	11.45	0.65	R	
11.45	11.65	0.2	CBSH	170
11.65	11.75	0.1	CR	170
11.75	12	0.25	CBSH	170
12	13.05	1.05	R	
13.05	13.4	0.35	CBSH	
13.4	14.3	0.9	R	
14.3	14.75	0.45	CBSH	
14.75	18.6	3.85	R	
18.6	18.75	0.15	CBSH	
18.75	19.6	0.85	С	150
19.6	19.8	0.2	CR	
19.8	20.3	0.5	CBSH	
20.3	24.1	3.8	R	
24.1	24.6	0.5	CBSH	130
24.6	27.05	2.45	R	
27.05	28	0.95	C	111
28	28.5	0.5	R	
28.5	28.7	0.2	CBSH	

	•		etres) continued	
From	То	Drilled thickness	Interpreted lithology	Name
28.7	29	0.3	С	110
29	29.1	0.1	DC	110
29.1	29.35	0.25	С	110
29.35	29.5	0.15	DC	101
29.5	29.65	0.15	С	101
29.65	29.8	0.15	DC	101
29.8	29.95	0.15	С	101
29.95	31.5	1.55	С	100
31.5	31.55	0.05	DC	100
31.55	31.75	0.2	CR	
31.75	32.3	0.55	CBSH	
32.3	33.55	1.25	R	
33.55	33.9	0.35	CBSH	
33.9	34.7	0.8	R	
34.7	34.9	0.2	CR	
34.9	35.3	0.4	С	201
35.3	35.45	0.15	DC	201
35.45	35.6	0.15	CR	
35.6	36.7	1.1	R	
36.7	36.95	0.25	CBSH	
36.95	37.15	0.2	DC	202
37.15	37.3	0.15	С	202
37.3	37.85	0.55	DC	202
37.85	45.05	7.2	R	
45.05	45.3	0.25	IRST	IRONSTONE
45.3	52.75	7.45	R	
52.75	53.2	0.45	CBSH	
53.2	53.35	0.15	CR	300
53.35	53.5	0.15	CBSH	
53.5	56.75	3.25	R	
56.75	56.97	0.22	CBSH	320
56.97	57.12	0.15	CR	320
57.12	57.35	0.23	CBSH	320
57.35	71.1	13.75	R	
71.1	71.5	0.4	CBSH	340
71.5	74.1	2.6	R	340
74.1	74.35	0.25	IRST	340
74.35	75.1	0.75	R	340
75.1	75.5	0.4	CBSH	340

			of geophysical logs	
Log interp	oretation of V	VC18-27C (me	etres) continued	
From	То	Drilled thickness	Interpreted lithology	Name
75.5	82.05	6.55	R	
82.05	82.45	0.4	С	430
82.45	86.85	4.4	R	
86.85	87.4	0.55	С	410
87.4	87.7	0.3	CR	
87.7	88.35	0.65	R	
88.35	88.55	0.2	CBSH	
88.55	89.45	0.9	С	401
89.45	95.15	5.7	R	
95.15	95.35	0.2	CBSH	
95.35	96.08	0.73	С	400
96.08	96.3	0.22	С	420
96.3	96.45	0.15	DC	420
96.45	96.85	0.4	CBSH	
96.85	97.3	0.45	R	
97.3	97.8	0.5	CBSH	
97.8	98.15	0.35	DC	440
98.15	99	0.85	С	440
99	99.15	0.15	CBSH	
99.15	99.5	0.35	R	
99.5	99.75	0.25	С	442
99.75	116.95	17.2	R	
116.95	117.3	0.35	CBSH	460
117.3	120.55	3.25	R	
120.55	121	0.45	CBSH	483
121	123.95	2.95	R	
123.95	124.2	0.25	CR	
124.2	124.35	0.15	С	480
124.35	124.5	0.15	DC	480
124.5	125	0.5	C	480
125	126.85	1.85	R	
126.85	127.2	0.35	CBSH	
127.2	127.65	0.45	R	
127.65	128.02	0.37	CBSH	
128.02	128.6	0.58	R	
128.6	129	0.4	CBSH	
129	129.2	0.2	CR	A71
129.2	129.4	0.2	DC	A71
129.4	129.5	0.1	CBSH	

Table A-2	2: Lithologica	1 interpretation	of geophysical logs	
			etres) continued	
From	То	Drilled thickness	Interpreted lithology	Name
129.5	132.8	3.3	R	
132.8	133.05	0.25	CBSH	
133.05	133.3	0.25	DC	A7
133.3	133.45	0.15	CR	A7
133.45	133.55	0.1	CBSH	
133.55	134.5	0.95	R	
134.5	134.88	0.38	CR	A72
134.88	140.22	5.34	R	
Log interr	pretation of W	/C18-28 (metro	20)	
From	To	Drilled	Interpreted lithology	Name
1 10111		thickness	interpreted nulology	Truffic
0	2.77	2.77	DRIFT	DRIFT
2.77	17.2	14.43	R	Didi i
17.2	17.45	0.25	CBSH	
17.45	17.55	0.1	CR	
17.55	17.85	0.3	C	300
17.85	18.05	0.2	CBSH	
18.05	22	3.95	R	
22	22.35	0.35	CBSH	
22.35	24.3	1.95	R	
24.3	24.45	0.15	FAULT	POSSIBLE
24.45	25.2	0.75	R	2.3.3
25.2	25.4	0.2	CR	320?
25.4	25.8	0.4	R	
25.8	25.95	0.15	IRST	IRONSTONE
25.95	26.2	0.25	R	
26.2	27.3	1.1	CBSH	
27.3	32.05	4.75	R	
32.05	32.7	0.65	CBSH	340
32.7	36.85	4.15	R	
36.85	37	0.15	CBSH	360
37	52.55	15.55	R	
52.55	52.95	0.4	CBSH	430
52.95	55.6	2.65	R	
55.6	55.9	0.3	CBSH	410
55.9	57.2	1.3	R	
57.2	57.45	0.25	CBSH	

			of geophysical logs	
			res) continued	
From	То	Drilled thickness	Interpreted lithology	Name
57.45	58.35	0.9	C	401
58.35	58.75	0.4	DC	400
58.75	59.45	0.7	С	400
59.45	59.7	0.25	CBSH	
59.7	61.8	2.1	R	
61.8	62.05	0.25	CBSH	
62.05	62.3	0.25	С	420
62.3	62.5	0.2	DC	420
62.5	64.85	2.35	R	
64.85	65	0.15	CBSH	
65	65.3	0.3	С	440
65.3	65.6	0.3	DC	440
65.6	65.99	0.39	R	
Log inter	pretation of V	VC18-29 (metro	es)	·
From	То	Drilled thickness	Interpreted lithology	Name
0	2.8	2.8	DRIFT	DRIFT
2.8	3.95	1.15	R	
3.95	4.05	0.1	CBSH	310?
4.05	13.95	9.9	R	
13.95	14.05	0.1	IRST	IRONSTONE
14.05	18.2	4.15	R	
18.2	18.55	0.35	CBSH	
18.55	19.05	0.5	R	
19.05	19.45	0.4	DC	300
19.45	22.9	3.45	R	
22.9	23.2	0.3	CBSH	320
23.2	23.55	0.35	R	320
23.55	23.7	0.15	CBSH	320
23.7	24.2	0.5	R	320
24.2	24.4	0.2	CBSH	320
24.4	26	1.6	R	
26	26.5	0.5	CBSH	340
26.5	27.05	0.55	CR	340
27.05	27.3	0.25	R	340
27.3	27.9	0.6	CBSH	340
27.9	49.2	21.3	R	1

	pretation of '			
From	То	Drilled thickness	Interpreted lithology	Name
49.2	49.35	0.15	CBSH	410
49.35	49.55	0.2	CR	410
49.55	49.65	0.1	CBSH	410
49.65	50.8	1.15	R	
50.8	51	0.2	CR	
51	51.55	0.55	С	401
51.55	51.75	0.2	CR	
51.75	51.95	0.2	CBSH	
51.95	52.1	0.15	DC	400
52.1	52.75	0.65	С	400
52.75	52.8	0.05	FAULT	ESTABLISHED
52.8	54.15	1.35	С	401
54.15	57.4	3.25	С	400
57.4	57.55	0.15	DC	400
57.55	57.9	0.35	R	
57.9	58.1	0.2	CBSH	
58.1	58.3	0.2	DC	420
58.3	58.5	0.2	CR	
58.5	61.15	2.65	R	
61.15	61.2	0.05	FAULT	ESTABLISHED
61.2	61.65	0.45	R	
61.65	61.95	0.3	DC	420
61.95	62.2	0.25	CBSH	
62.2	63.15	0.95	R	
63.15	63.4	0.25	DC	440
63.4	63.9	0.5	С	440
63.9	63.95	0.05	FAULT	ESTABLISHED
63.95	64.05	0.1	CR	
64.05	64.3	0.25	DC	440
64.3	64.7	0.4	С	440
64.7	64.9	0.2	CBSH	
64.9	65.6	0.7	R	
65.6	65.7	0.1	CBSH	
65.7	65.75	0.05	FAULT	PROBABLE
65.75	66	0.25	DC	440?
66	66.18	0.18	CR	440?
66.18	66.3	0.12	DC	440?
66.3	68.1	1.8	R	
68.1	68.45	0.35	CBSH	442

Table A-2	2: Lithologica	al interpretation	of geophysical logs	
			res) continued	
From	То	Drilled	Interpreted lithology	Name
		thickness		
68.45	76.35	7.9	R	
76.35	76.75	0.4	CBSH	463
76.75	80.85	4.1	R	
80.85	80.95	0.1	CBSH	
80.95	81.16	0.21	R	
81.16	81.43	0.27	ND	
Log inter	pretation of V	VC18-30 (metro	es)	
From	То	Drilled	Interpreted lithology	Name
		thickness		
0	2.2	2.2	DRIFT	DRIFT
2.2	2.4	0.2	R	
2.4	2.5	0.1	С	101
2.5	2.65	0.15	DC	101
2.65	2.85	0.2	С	101
2.85	3	0.15	CR	
3	3.9	0.9	С	100
3.9	4.15	0.25	DC	100
4.15	6.5	2.35	CBSH	
6.5	7.4	0.9	R	
7.4	7.9	0.5	CBSH	
7.9	8.55	0.65	С	201
8.55	8.65	0.1	DC	201
8.65	8.8	0.15	CBSH	
8.8	11.6	2.8	R	
11.6	11.8	0.2	CR	
11.8	12	0.2	С	202
12	12.7	0.7	DC	202
12.7	16.35	3.65	R	
16.35	16.8	0.45	CBSH	310
16.8	29	12.2	R	
29	29.45	0.45	CBSH	
29.45	29.6	0.15	CR	
29.6	29.7	0.1	DC	300
29.7	29.85	0.15	С	300
29.85	30.05	0.2	CBSH	
30.05	33.3	3.25	R	
33.3	33.7	0.4	CBSH	320

Table A-2:	Lithological	interpretation	of geophysical logs	
Log interpr	retation of W	VC18-30 (metr	res) continued	
From	То	Drilled thickness	Interpreted lithology	Name
33.7	33.9	0.2	R	320
33.9	34.3	0.4	CBSH	320
34.3	36.4	2.1	R	
36.4	36.6	0.2	CBSH	340
36.6	36.9	0.3	CR	340
36.9	37.05	0.15	CBSH	340
37.05	37.35	0.3	R	340
37.35	38.25	0.9	CBSH	340
38.25	58.7	20.45	R	
58.7	58.8	0.1	CBSH	
58.8	59.1	0.3	CR	430
59.1	60.4	1.3	R	
60.4	60.6	0.2	CBSH	
60.6	60.75	0.15	DC	410
60.75	61	0.25	С	410
61	61.15	0.15	CR	
61.15	61.4	0.25	DC	401
61.4	63	1.6	С	401
63	64.45	1.45	С	400
64.45	64.5	0.05	FAULT	PROBABLE
64.5	65.9	1.4	С	401
65.9	68.7	2.8	С	400
68.7	68.85	0.15	DC	420
68.85	69.4	0.55	С	420
69.4	69.65	0.25	CBSH	
69.65	70.05	0.4	R	
70.05	70.4	0.35	CBSH	
70.4	70.6	0.2	R	
70.6	70.7	0.1	FAULT	PROBABLE
70.7	70.95	0.25	CBSH	
70.95	71.15	0.2	DC	420
71.15	71.3	0.15	С	420
71.3	71.5	0.2	CBSH	
71.5	72	0.5	R	
72	72.15	0.15	DC	
72.15	72.4	0.25	CR	
72.4	75.9	3.5	R	
75.9	76.1	0.2	CBSH	
76.1	76.7	0.6	DC	440

Log mien	pretation of v	VC18-30 (meti	res) continued	
From	То	Drilled thickness	Interpreted lithology	Name
76.7	76.95	0.25	С	440
76.95	78.7	1.75	R	
78.7	79.1	0.4	CBSH	442
79.1	85.4	6.3	R	1
85.4	85.85	0.45	CBSH	463
85.85	91.1	5.25	R	
91.1	91.3	0.2	CBSH	
91.3	91.55	0.25	С	460
91.55	91.75	0.2	CBSH	
91.75	93.2	1.45	R	
93.2	93.6	0.4	CBSH	483?
93.6	100.7	7.1	R	
100.7	101.05	0.35	CBSH	
101.05	101.35	0.3	R	
101.35	101.8	0.45	С	480
101.8	102	0.2	DC	480
102	102.2	0.2	CBSH	
102.2	108.1	5.9	R	
108.1	108.25	0.15	CBSH	
108.25	108.5	0.25	DC	A71
108.5	108.7	0.2	CBSH	
108.7	109.8	1.1	R	
109.8	110	0.2	CBSH	
110	110.3	0.3	DC	A7
110.3	110.9	0.6	С	A7
110.9	111	0.1	DC	A7
111	111.2	0.2	CBSH	
111.2	118	6.8	R	
118	118.3	0.3	CBSH	
118.3	118.45	0.15	R	
118.45	118.8	0.35	CR	A55
118.8	120.7	1.9	R	
120.7	120.97	0.27	ND	

			of geophysical logs	
		WC18-31 (metr		
From	То	Drilled thickness	Interpreted lithology	Name
0	2.65	2.65	DRIFT	DRIFT
2.65	5.5	2.85	R	
5.5	5.75	0.25	CR	
5.75	5.9	0.15	С	150
5.9	6.45	0.55	DC	150
6.45	6.7	0.25	CBSH	
6.7	7.1	0.4	R	
7.1	7.45	0.35	CBSH	
7.45	10.55	3.1	R	
10.55	10.85	0.3	CR	130
10.85	14.2	3.35	R	
14.2	14.35	0.15	CR	
14.35	14.5	0.15	DC	111
14.5	14.6	0.1	CBSH	
14.6	14.75	0.15	CR	
14.75	15	0.25	CBSH	
15	16	1	R	
16	16.2	0.2	CBSH	
16.2	16.65	0.45	С	110
16.65	16.85	0.2	CR	
16.85	23.1	6.25	R	
23.1	23.3	0.2	CBSH	
23.3	23.85	0.55	С	101
23.85	25.4	1.55	С	100
25.4	25.65	0.25	CR	
25.65	26.05	0.4	R	
26.05	26.2	0.15	CBSH	
26.2	28.8	2.6	R	
28.8	29	0.2	CBSH	
29	29.1	0.1	CR	
29.1	29.3	0.2	DC	201
29.3	29.9	0.6	С	201
29.9	30.05	0.15	DC	201
30.05	30.3	0.25	CBSH	
30.3	33.7	3.4	R	
33.7	33.9	0.2	CBSH	
33.9	34.2	0.3	С	202
34.2	34.3	0.1	CR	202
34.3	34.4	0.1	DC	202

			of geophysical logs es) continued	
From	To	Drilled	Interpreted lithology	Name
		thickness	I I I I I I I I I I I I I I I I I I I	
34.4	34.55	0.15	CR	202
34.55	34.7	0.15	С	202
34.7	34.9	0.2	CBSH	
34.9	40.3	5.4	R	
40.3	40.6	0.3	IRST	IRONSTONE?
40.6	45.85	5.25	R	
45.85	46	0.15	CBSH	
46	46.25	0.25	CR	
46.25	46.7	0.45	С	300
46.7	46.9	0.2	CR	
46.9	50.7	3.8	R	
50.7	50.9	0.2	CBSH	320
50.9	51.05	0.15	CR	320
51.05	51.75	0.7	CBSH	320
51.75	53.7	1.95	R	
53.7	54.15	0.45	CBSH	340
54.15	54.55	0.4	R	340
54.55	55	0.45	CR	340
55	59.05	4.05	R	
59.05	59.5	0.45	CBSH	360?
59.5	74.7	15.2	R	
74.7	74.95	0.25	DC	410
74.95	75.1	0.15	CBSH	
75.1	75.9	0.8	R	
75.9	76.1	0.2	CBSH	
76.1	76.5	0.4	С	401
76.5	76.9	0.4	С	400
76.9	77.05	0.15	CBSH	
77.05	77.45	0.4	R	
77.45	77.8	0.35	CBSH	420
77.8	83.05	5.25	R	
83.05	83.4	0.35	CBSH	440
83.4	88.45	5.05	R	
88.45	88.65	0.2	CBSH	463?
88.65	91.35	2.7	R	
91.35	91.4	0.05	FAULT	PROBABLE
91.4	100.4	9	R	
100.4	100.6	0.2	CBSH	463
100.6	101.95	1.35	R	

Table A-2	2: Lithologica	1 interpretation	of geophysical logs	
Log interp	oretation of W	/C18-31 (metro	es) continued	
From	То	Drilled thickness	Interpreted lithology	Name
101.95	102.35	0.4	CBSH	460
102.35	109.65	7.3	R	
109.65	110	0.35	CBSH	483
110	110.1	0.1	R	483
110.1	110.4	0.3	CBSH	483
110.4	119.26	8.86	R	
119.26	119.45	0.19	ND	
Log interp	oretation of W	/C18-32 (metro	es)	
From	То	Drilled thickness	Interpreted lithology	Name
0	2.82	2.82	DRIFT	DRIFT
2.82	9.7	6.88	R	
9.7	10	0.3	CR	410
10	10.2	0.2	CBSH	
10.2	12.3	2.1	R	
12.3	12.7	0.4	CBSH	
12.7	12.95	0.25	DC	401
12.95	13.65	0.7	С	401
13.65	14.25	0.6	R	
14.25	14.4	0.15	DC	400
14.4	14.5	0.1	FAULT	PROBABLE
14.5	15.3	0.8	С	401
15.3	15.55	0.25	DC	400
15.55	17.05	1.5	С	400
17.05	17.2	0.15	DC	420
17.2	17.35	0.15	С	420
17.35	17.65	0.3	CBSH	
17.65	18.2	0.55	R	
18.2	18.45	0.25	IRST	IRONSTONE
18.45	18.7	0.25	R	
18.7	19	0.3	CBSH	
19	19.6	0.6	DC	440
19.6	19.85	0.25	С	440
19.85	21.55	1.7	R	
21.55	21.9	0.35	CBSH	442
21.9	28.85	6.95	R	
28.85	29.05	0.2	CBSH	

Table A-2	2: Lithologica	al interpretation	of geophysical logs	
Log interp	pretation of V	VC18-32 (metro	es) continued	
From	То	Drilled thickness	Interpreted lithology	Name
29.05	29.25	0.2	CR	
29.25	29.8	0.55	R	
29.8	30.15	0.35	CBSH	
30.15	31.5	1.35	R	
31.5	31.7	0.2	CBSH	
31.7	32.3	0.6	R	
32.3	32.85	0.55	CBSH	463
32.85	33.9	1.05	R	
33.9	34	0.1	CBSH	
34	34.4	0.4	R	
34.4	34.6	0.2	CBSH	
34.6	36.6	2	R	
36.6	36.7	0.1	CBSH	
36.7	39.8	3.1	R	
39.8	40.05	0.25	CBSH	
40.05	40.3	0.25	DC	460
40.3	40.6	0.3	CBSH	
40.6	45.95	5.35	R	
45.95	46.3	0.35	CBSH	483
46.3	49.95	3.65	R	
49.95	50.4	0.45	CBSH	
50.4	52.15	1.75	R	
52.15	52.4	0.25	CBSH	
52.4	52.65	0.25	CR	
52.65	53.1	0.45	C	480
53.1	53.35	0.25	DC	480
53.35	56.2	2.85	R	
56.2	56.45	0.25	CBSH	
56.45	59.4	2.95	R	
59.4	59.8	0.4	DC	A71
59.8	60.6	0.8	R	
60.6	60.85	0.25	CR	
60.85	61.4	0.55	С	A7
61.4	61.65	0.25	DC	A7
61.65	61.9	0.25	CBSH	
61.9	68.2	6.3	R	
68.2	69.05	0.85	CBSH	A55
69.05	74.1	5.05	R	
74.1	74.4	0.3	CR	A53

Table A-2	2: Lithologica	al interpretation	of geophysical logs	
			es) continued	
From	То	Drilled thickness	Interpreted lithology	Name
74.4	74.9	0.5	R	
74.9	75.2	0.3	CBSH	A51
75.2	76.6	1.4	R	
76.6	77.3	0.7	С	A5
77.3	77.5	0.2	CBSH	
77.5	81.3	3.8	R	
81.3	81.58	0.28	ND	
Log inter	pretation of V	VC18-33 (metro	es)	
From	То	Drilled thickness	Interpreted lithology	Name
0	2.7	2.7	DRIFT	DRIFT
2.7	5.6	2.9	R	
5.6	5.9	0.3	CR	430?
5.9	8.75	2.85	R	
8.75	8.9	0.15	CR	
8.9	9.15	0.25	DC	410
9.15	9.5	0.35	CBSH	
9.5	9.7	0.2	R	
9.7	10.35	0.65	CBSH	
10.35	10.5	0.15	R	
10.5	10.7	0.2	CBSH	
10.7	11.6	0.9	R	
11.6	11.9	0.3	CR	
11.9	12.15	0.25	DC	401
12.15	12.75	0.6	C	401
12.75	13.8	1.05	C	400
13.8	14	0.2	DC	420
14	14.25	0.25	CBSH	
14.25	14.9	0.65	R	
14.9	15.05	0.15	CBSH	
15.05	15.6	0.55	DC	440
15.6	15.75	0.15	С	440
15.75	16	0.25	CBSH	
16	17.4	1.4	R	
17.4	17.8	0.4	CBSH	442
17.8	23.85	6.05	R	
23.85	24	0.15	CBSH	463

			of geophysical logs	
From	To	Drilled	es) continued	Name
FIOIII	10	thickness	Interpreted lithology	Ivame
24	29.45	5.45	R	
29.45	29.6	0.15	CBSH	
29.6	29.8	0.2	DC	460
29.8	30	0.2	CBSH	
30	34.55	4.55	R	
34.55	34.9	0.35	CBSH	483
34.9	40.35	5.45	R	
40.35	40.6	0.25	CBSH	
40.6	40.7	0.1	CR	
40.7	40.8	0.1	CBSH	
40.8	41	0.2	CR	
41	41.25	0.25	DC	480
41.25	41.5	0.25	С	480
41.5	41.7	0.2	DC	480
41.7	41.9	0.2	CBSH	
41.9	44.3	2.4	R	
44.3	44.65	0.35	CBSH	
44.65	48	3.35	R	
48	48.2	0.2	CBSH	
48.2	48.5	0.3	DC	A71
48.5	49.95	1.45	R	
49.95	50.55	0.6	С	A7
50.55	50.8	0.25	DC	A7
50.8	51	0.2	CBSH	
51	57.8	6.8	R	
57.8	58.7	0.9	CBSH	A55
58.7	64.85	6.15	R	
64.85	65.2	0.35	CBSH	A53
65.2	65.75	0.55	R	
65.75	66.05	0.3	CBSH	A51
66.05	67.55	1.5	R	
67.55	67.7	0.15	CBSH	
67.7	68.85	1.15	С	A5
68.85	69.05	0.2	CBSH	
69.05	80.25	11.2	R	
80.25	80.65	0.4	CBSH	
80.65	81.05	0.4	R	
81.05	81.25	0.2	CR	
81.25	81.4	0.15	CBSH	

			of geophysical logs	
		<del></del>	es) continued	
From	То	Drilled thickness	Interpreted lithology	Name
81.4	81.6	0.2	DC	A3
81.6	81.8	0.2	С	A3
81.8	81.9	0.1	DC	A3
81.9	82.1	0.2	CR	
82.1	82.25	0.15	DC	A1
82.25	82.5	0.25	CR	
82.5	82.65	0.15	CBSH	
82.65	82.8	0.15	CR	
82.8	83	0.2	DC	A0
83	95.2	12.2	R	
95.2	96.1	0.9	CBSH	
96.1	96.32	0.22	R	
96.32	96.58	0.26	ND	
Log interp	pretation of V	VC18-34 (metro	es)	
From	То	Drilled thickness	Interpreted lithology	Name
0	1.15	1.15	DRIFT	DRIFT
1.15	6.3	5.15	R	
6.3	6.55	0.25	CR	150
6.55	6.65	0.1	С	150
6.65	6.8	0.15	CR	150
6.8	6.95	0.15	С	150
6.95	7.1	0.15	CR	150
7.1	7.2	0.1	DC	150
7.2	7.4	0.2	CR	150
7.4	7.55	0.15	DC	150
7.55	7.8	0.25	CR	150
7.8	8.05	0.25	CBSH	
8.05	9.75	1.7	R	
9.75	9.9	0.15	FAULT	ESTABLISHED
9.9	10	0.1	С	150
10	10.3	0.3	CR	150
10.3	10.5	0.2	CBSH	
10.5	11	0.5	R	
11	11.3	0.3	CBSH	
11.3	11.45	0.15	R	
11.45	11.65	0.2	CR	

			of geophysical logs	
	To	Drilled	es) continued	Name
From	10	thickness	Interpreted lithology	Name
11.65	11.85	0.2	CBSH	
11.85	12.5	0.65	R	
12.5	12.75	0.25	FAULT	PROBABLE
12.75	13	0.25	R	
13	13.2	0.2	C	130
13.2	13.5	0.3	CBSH	
13.5	14.3	0.8	R	
14.3	14.5	0.2	CBSH	
14.5	14.7	0.2	DC	111
14.7	14.9	0.2	CBSH	
14.9	15.55	0.65	R	
15.55	15.8	0.25	CBSH	
15.8	15.95	0.15	С	110
15.95	16.1	0.15	CR	110
16.1	16.2	0.1	DC	110
16.2	16.4	0.2	CR	
16.4	17.4	1	R	
17.4	17.7	0.3	CBSH	
17.7	18.5	0.8	С	101
18.5	18.7	0.2	DC	100
18.7	20.3	1.6	С	100
20.3	20.55	0.25	CR	
20.55	21.2	0.65	CBSH	
21.2	25.2	4	R	
25.2	25.4	0.2	CR	
25.4	25.85	0.45	С	201
25.85	26.05	0.2	CBSH	
26.05	28.45	2.4	R	
28.45	28.7	0.25	CBSH	
28.7	28.9	0.2	С	202
28.9	29	0.1	CR	202
29	29.15	0.15	DC	202
29.15	29.25	0.1	CR	202
29.25	29.4	0.15	DC	202
29.4	29.55	0.15	CBSH	
29.55	47.2	17.65	R	
47.2	47.3	0.1	CBSH	
47.3	47.75	0.45	DC	300
47.75	48	0.25	C	300

			of geophysical logs es) continued	
From	To	Drilled	Interpreted lithology	Name
110111		thickness	interpreted ittilology	Tunie
48	48.15	0.15	CR	
48.15	50.35	2.2	R	
50.35	50.5	0.15	CBSH	320
50.5	50.7	0.2	DC	320
50.7	50.9	0.2	CBSH	320
50.9	54.2	3.3	R	
54.2	54.6	0.4	CBSH	340
54.6	54.85	0.25	R	340
54.85	55.35	0.5	CBSH	340
55.35	56.4	1.05	R	340
56.4	56.9	0.5	CBSH	340
56.9	73.9	17	R	
73.9	74.3	0.4	CBSH	430
74.3	75.45	1.15	R	
75.45	75.8	0.35	IRST	IRONSTONE
75.8	76.2	0.4	R	
76.2	77	0.8	С	410
77	77.55	0.55	R	
77.55	77.8	0.25	CR	
77.8	78.4	0.6	С	401
78.4	78.5	0.1	DC	400
78.5	79.85	1.35	С	400
79.85	80.1	0.25	DC	420
80.1	80.3	0.2	С	420
80.3	80.5	0.2	CR	
80.5	80.9	0.4	R	
80.9	81.1	0.2	CBSH	
81.1	81.2	0.1	FAULT	PROBABLE
81.2	81.4	0.2	CR	
81.4	84.9	3.5	R	
84.9	85	0.1	FAULT	POSSIBLE
85	85.15	0.15	CR	
85.15	85.7	0.55	DC	440
85.7	85.9	0.2	CBSH	
85.9	87.15	1.25	R	
87.15	87.4	0.25	CBSH	442
87.4	88	0.6	R	
88	88.3	0.3	CBSH	463
88.3	89.6	1.3	R	

			of geophysical logs es) continued	
From	To	Drilled	Interpreted lithology	Name
110111	10	thickness	interpreted ithology	Tranic
89.6	89.7	0.1	CBSH	
89.7	89.8	0.1	CR	460
89.8	90.05	0.25	DC	460
90.05	90.5	0.45	CBSH	
90.5	91.2	0.7	R	
91.2	91.5	0.3	CBSH	483
91.5	95.3	3.8	R	
95.3	95.7	0.4	CBSH	480
95.7	99.02	3.32	R	
99.02	99.29	0.27	ND	
T ' '		VC10.25 (		
		VC18-35 (metro	1	NI
From	То	Drilled thickness	Interpreted lithology	Name
0	5.4	5.4	DRIFT	DRIFT
5.4	6	0.6	R	
6	6.4	0.4	CBSH	130
6.4	9.4	3	R	
9.4	9.6	0.2	CBSH	
9.6	9.9	0.3	R	
9.9	10.1	0.2	CBSH	
10.1	10.4	0.3	C	111
10.4	10.9	0.5	CBSH	
10.9	11.15	0.25	R	
11.15	11.3	0.15	CBSH	
11.3	11.5	0.2	CR	
11.5	11.65	0.15	DC	110
11.65	11.95	0.3	CR	
11.95	13.2	1.25	R	
13.2	13.5	0.3	CR	
13.5	14.5	1	C	101
14.5	16.4	1.9	C	100
16.4	16.65	0.25	DC	100
16.65	16.9	0.25	CR	
16.9	17.7	0.8	CBSH	
17.7	20.3	2.6	R	
20.3	20.45	0.15	CBSH	
20.45	21	0.55	R	+

			es) continued	1
From	То	Drilled thickness	Interpreted lithology	Name
21	21.2	0.2	CBSH	
21.2	23.3	2.1	R	
23.3	23.6	0.3	CBSH	203
23.6	23.75	0.15	CR	203
23.75	25.2	1.45	R	
25.2	25.5	0.3	CBSH	
25.5	25.85	0.35	CR	
25.85	26.5	0.65	С	201
26.5	26.8	0.3	CBSH	
26.8	29.15	2.35	R	
29.15	29.4	0.25	CBSH	
29.4	29.6	0.2	CR	
29.6	29.7	0.1	DC	202
29.7	29.9	0.2	С	202
29.9	30.1	0.2	DC	202
30.1	30.25	0.15	CR	202
30.25	30.4	0.15	DC	202
30.4	30.65	0.25	CBSH	
30.65	32.15	1.5	R	
32.15	32.25	0.1	FAULT	POSSIBLE
32.25	32.35	0.1	CBSH	
32.35	43.65	11.3	R	
43.65	43.8	0.15	CBSH	310
43.8	44	0.2	FAULT	PROBABLE
44	44.2	0.2	CBSH	310
44.2	50.6	6.4	R	
50.6	51.15	0.55	CR	
51.15	51.4	0.25	C	300
51.4	51.65	0.25	CR	
51.65	54.4	2.75	R	
54.4	54.6	0.2	CBSH	320
54.6	54.85	0.25	DC	320
54.85	55	0.15	CBSH	320
55	60	5	R	
60	60.3	0.3	CBSH	340
60.3	61.8	1.5	R	340
61.8	61.9	0.1	CBSH	340
61.9	65.6	3.7	R	
65.6	66	0.4	CBSH	360

To  84.1 84.3 84.5 84.6 87.4 87.6 88.3 88.5 89.5 90.5 91.2	Drilled thickness 18.1 0.2 0.2 0.1 2.8 0.2 0.7 0.2	R CBSH DC CBSH R CR CR CR	Name  430 430 430
84.1 84.3 84.5 84.6 87.4 87.6 88.3 88.5 90.5	thickness 18.1 0.2 0.2 0.1 2.8 0.2 0.7 0.2	R CBSH DC CBSH R CR	430 430
84.3 84.5 84.6 87.4 87.6 88.3 88.5 90.5	18.1 0.2 0.2 0.1 2.8 0.2 0.7 0.2	CBSH DC CBSH R CR	430
84.3 84.5 84.6 87.4 87.6 88.3 88.5 90.5	0.2 0.2 0.1 2.8 0.2 0.7 0.2	CBSH DC CBSH R CR	430
84.5 84.6 87.4 87.6 88.3 88.5 89.5 90.5	0.2 0.1 2.8 0.2 0.7 0.2	DC CBSH R CR	430
84.6 87.4 87.6 88.3 88.5 89.5 90.5	0.1 2.8 0.2 0.7 0.2	R CR	
87.4 87.6 88.3 88.5 89.5 90.5	2.8 0.2 0.7 0.2	R CR	
88.3 88.5 89.5 90.5	0.7 0.2		<del> </del>
88.5 89.5 90.5	0.2		
89.5 90.5			410
90.5	1	CR	
90.5	1	R	
91.2	1	С	401
	0.7	С	400
91.4	0.2	CR	
91.75	0.35	CBSH	
92	0.25	С	420
92.2	0.2	CR	
94.1	1.9	R	
94.3	0.2	CBSH	
94.45	0.15	DC	440
94.6	0.15	C	440
95.15	0.55	DC	440
96.5	1.35	R	
97	0.5	CR	442
102.5	5.5	R	
102.6	0.1	CBSH	463
107	4.4	R	
107.2	0.2	CBSH	460
107.3	0.1	CR	460
107.5	0.2	CBSH	460
117.1	9.6	R	
117.7	0.6	CBSH	
118.1	0.4	С	480
118.4	0.3	DC	480
118.5	0.1	CBSH	
120.86	2.36	R	
	0.27	ND	
121.13		ļ - · <del>-</del>	
	94.1 94.3 94.45 94.6 95.15 96.5 97 102.5 107.2 107.2 107.3 107.5 117.1 117.7 118.1 118.4 118.5 120.86	94.1     1.9       94.3     0.2       94.45     0.15       94.6     0.15       95.15     0.55       96.5     1.35       97     0.5       102.5     5.5       102.6     0.1       107     4.4       107.2     0.2       107.3     0.1       107.5     0.2       117.1     9.6       117.7     0.6       118.1     0.4       118.4     0.3       118.5     0.1       120.86     2.36	94.1       1.9       R         94.3       0.2       CBSH         94.45       0.15       DC         94.6       0.15       C         95.15       0.55       DC         96.5       1.35       R         97       0.5       CR         102.5       5.5       R         102.6       0.1       CBSH         107       4.4       R         107.2       0.2       CBSH         107.3       0.1       CR         107.5       0.2       CBSH         117.1       9.6       R         117.7       0.6       CBSH         118.1       0.4       C         118.4       0.3       DC         118.5       0.1       CBSH         120.86       2.36       R

	pretation of V			
From	То	Drilled thickness	Interpreted lithology	Name
0	2	2	DRIFT	DRIFT
2	3.2	1.2	R	
3.2	3.4	0.2	CR	
3.4	4.65	1.25	R	
4.65	4.8	0.15	CBSH	130
4.8	5	0.2	CR	130
5	5.15	0.15	CBSH	130
5.15	8.2	3.05	R	
8.2	8.4	0.2	CBSH	
8.4	8.65	0.25	С	111
8.65	8.8	0.15	CBSH	
8.8	9.7	0.9	R	
9.7	9.9	0.2	CBSH	
9.9	10.4	0.5	С	110
10.4	10.5	0.1	CBSH	
10.5	17	6.5	R	
17	17.2	0.2	CBSH	
17.2	17.3	0.1	DC	101
17.3	17.5	0.2	С	101
17.5	17.6	0.1	DC	101
17.6	17.9	0.3	С	101
17.9	19.4	1.5	С	100
19.4	19.5	0.1	DC	100
19.5	19.7	0.2	CBSH	
19.7	20.15	0.45	R	
20.15	20.6	0.45	CBSH	
20.6	23	2.4	R	
23	23.2	0.2	CBSH	
23.2	23.35	0.15	CR	
23.35	23.5	0.15	DC	201
23.5	23.9	0.4	C	201
23.9	24.2	0.3	CR	
24.2	28.4	4.2	R	
28.4	28.65	0.25	CR	
28.65	28.8	0.15	C	202
28.8	28.9	0.1	CR	202
28.9	29.05	0.15	DC	202
29.05	29.15	0.1	ASH	202
29.15	29.3	0.15	C	202

			of geophysical logs es) continued	
From	То	Drilled thickness	Interpreted lithology	Name
29.3	29.5	0.2	CBSH	
29.5	42.1	12.6	R	
42.1	42.4	0.3	DC	300
42.4	42.5	0.1	C	300
42.5	42.6	0.1	CR	300
42.6	43	0.4	C	300
43	43.15	0.15	CBSH	
43.15	45.5	2.35	R	
45.5	45.8	0.3	CBSH	320
45.8	45.9	0.1	DC	320
45.9	46.15	0.25	CBSH	320
46.15	48.65	2.5	R	
48.65	48.9	0.25	CBSH	340
48.9	49.3	0.4	CR	340
49.3	49.4	0.1	CBSH	340
49.4	49.8	0.4	R	340
49.8	50.5	0.7	CBSH	340
50.5	71.3	20.8	R	
71.3	71.5	0.2	CBSH	410
71.5	71.6	0.1	CR	410
71.6	71.8	0.2	CBSH	410
71.8	72.8	1	R	
72.8	73	0.2	CR	
73	73.55	0.55	C	401
73.55	75.25	1.7	С	400
75.25	75.55	0.3	С	420
75.55	75.8	0.25	CBSH	
75.8	76.4	0.6	R	
76.4	76.7	0.3	CBSH	
76.7	77.05	0.35	DC	440
77.05	77.25	0.2	CR	
77.25	78.3	1.05	R	
78.3	78.5	0.2	CBSH	442
78.5	84.25	5.75	R	
84.25	84.35	0.1	CBSH	463
84.35	87.85	3.5	R	
87.85	88	0.15	CBSH	460?
88	103.7	15.7	R	
103.7	103.95	0.25	CR	

Table A-2:	Lithological i	interpretation	of geophysical logs							
			es) continued							
From	То	Drilled thickness	Interpreted lithology	Name						
103.95	105.6	1.65	С	480						
105.6	105.7	0.1	FAULT	POSSIBLE						
105.7	106.7	1	DC	480?						
106.7	106.9	0.2	С	480?						
106.9	107	0.1	DC	480?						
107	107.25	0.25	С	480?						
107.25	107.55	0.3	DC	480?						
107.55	108.2	0.65	CR							
108.2	120.95	12.75	R							
120.95	121.5	0.55	CBSH							
121.5	121.9	0.4	С	A7						
121.9	122.1	0.2	DC	A7						
122.1	128.2	6.1	R							
128.2	128.35	0.15	CBSH							
128.35	128.5	0.15	DC	A51						
128.5	128.7	0.2	CBSH							
128.7	129.2	0.5	R							
129.2	129.4	0.2	CBSH							
129.4	129.9	0.5	С	A5						
129.9	130.15	0.25	DC	A5						
130.15	130.4	0.25	CBSH							
130.4	137.35	6.95	R							
137.35	138.05	0.7	CBSH	A3?						
138.05	138.48	0.43	R							
138.48	138.74	0.26	ND							
Log interpre	etation of WC	218-37 (metre	es)							
From	То	Drilled thickness	Interpreted lithology	Name						
0	2.9	2.9	DRIFT	DRIFT						
2.9	3.2	0.3	CR	130						
3.2	6.05	2.85	R							
6.05	6.3	0.25	CBSH							
6.3	6.55	0.25	С	111						
6.55	6.8	0.25	CR							
6.8	7.5	0.7	R							
7.5	7.8	0.3	DC	110						
7.8	9.25	1.45	R							

Table A-2:	Lithologica	ıl interpretation	of geophysical logs	
Log interpr	retation of V	VC18-37 (metro	es) continued	
From	То	Drilled thickness	Interpreted lithology	Name
9.25	9.45	0.2	CBSH	
9.45	10.45	1	С	101
10.45	12	1.55	С	100
12	12.35	0.35	DC	100
12.35	12.6	0.25	CR	
12.6	12.7	0.1	CBSH	
12.7	12.8	0.1	CR	
12.8	12.9	0.1	DC	
12.9	13.1	0.2	CR	
13.1	13.45	0.35	CBSH	
13.45	17.7	4.25	R	
17.7	17.8	0.1	CBSH	203
17.8	19.95	2.15	R	
19.95	20.3	0.35	CR	
20.3	20.6	0.3	С	201
20.6	20.7	0.1	DC	201
20.7	20.8	0.1	С	201
20.8	21.05	0.25	CR	
21.05	21.4	0.35	R	
21.4	21.7	0.3	CBSH	
21.7	21.8	0.1	CR	
21.8	22.15	0.35	CBSH	
22.15	23.65	1.5	R	
23.65	23.8	0.15	CR	
23.8	24.05	0.25	С	202
24.05	24.3	0.25	DC	202
24.3	24.4	0.1	CR	202
24.4	24.55	0.15	DC	202
24.55	24.75	0.2	CBSH	
24.75	28.2	3.45	R	
28.2	28.4	0.2	CBSH	
28.4	31.05	2.65	R	
31.05	31.4	0.35	CBSH	
31.4	42.9	11.5	R	
42.9	43.1	0.2	CBSH	
43.1	43.35	0.25	С	300
43.35	43.6	0.25	CBSH	
43.6	46.25	2.65	R	
46.25	46.4	0.15	CBSH	320

Table A-2:	: Lithologica	al interpretation	of geophysical logs	
			es) continued	
From	То	Drilled thickness	Interpreted lithology	Name
46.4	46.7	0.3	CR	320
46.7	46.95	0.25	CBSH	320
46.95	51.95	5	R	
51.95	52.3	0.35	CBSH	340
52.3	55.55	3.25	R	
55.55	55.9	0.35	CBSH	360
55.9	72.5	16.6	R	
72.5	72.65	0.15	CBSH	430
72.65	72.8	0.15	DC	430
72.8	73	0.2	CBSH	430
73	75.6	2.6	R	
75.6	75.8	0.2	CR	
75.8	76.4	0.6	С	410
76.4	76.6	0.2	CR	
76.6	77.45	0.85	R	
77.45	77.7	0.25	CR	
77.7	78.5	0.8	C	401
78.5	80.25	1.75	C	400
80.25	80.75	0.5	R	
80.75	81.05	0.3	C	420
81.05	81.25	0.2	CR	-
81.25	82.95	1.7	R	
82.95	83.2	0.25	CR	
83.2	83.35	0.15	С	440
83.35	83.5	0.15	CR	440
83.5	83.6	0.1	DC	440
83.6	83.7	0.1	CR	440
83.7	83.9	0.2	C	440
83.9	84.05	0.15	CBSH	
84.05	85.25	1.2	R	
85.25	85.4	0.15	CBSH	
85.4	85.7	0.3	DC	442
85.7	91.45	5.75	R	
91.45	91.75	0.3	CBSH	463
91.75	95.9	4.15	R	
95.9	96.3	0.4	CR	460
96.3	97.78	1.48	R	
97.78	98.04	0.26	ND	

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**Table A-3**: Cross-reference of PDF scan-files to borehole core descriptions

Table A-3. Ci	oss-reference o	I PDF Scal	11-11165	נט טט	renoie	e core descriptions
Borehole	Scanfile	File p	arts			Number of hard
						copy log pages
18-01C	0733	001	011	022		23
18-02C	0734	001	012			17
18-03C	0735	001	010	030		28
18-04C	0736	001	011	020	030	34
18-05C	0737	001	011			20
18-06C	0738	001	010	021		25
18-07C	0740	001	007	016	026	27
18-08C	0741	001	007	013		14
18-09C	0742	001	011			19
18-10C	0743	001	012	023		31
18-11C	0744	001	011			19
18-12C	0745	001	011	022	033	37
18-13C	0746	001	011	022		27
18-14C	0747	001	012	024		25
18-15C	0748	001	012			18
18-16C	0749	001	012			20
18-17C	0750	001	011	021		27
18-18C	0751	001	012			21
18-19C	0752	001	013			13
18-20C	0753	001	011	021		24
18-21C	0754	001	011			12
18-22C	0755	001	011			18
18-23C	0756	001				11
18-24C	0757	001	012			12
18-25C	0758	001	011	022		23
18-26C	0759	001	010			15
18-27C	0760	001	010	021		24

Example: core description of WC18-27C is presented as three files: 0760\_001.pdf, 0760\_010.pdf, and 0760\_021.pdf

#### **Table A-4**: Authorship of core descriptions

Consulting geologists, working for Apex Geoscience, logged and sampled the year-2018 diamond-drill cores under the author's guidance and direction. Standard forms, including directions on descriptive format, were designed and provided by the author, allowing for large-format handwritten data entry, and for reproduction and scanning on commonly-available office equipment. The logging forms were printed at tabloid (11 x 17 inch) format, initially on waterproof paper, but subsequently on untreated paper (as the waterproof paper was found to rapidly attract dirt, and become readily smeared).

Hardcopy geophysical logs were made available for consultation during logging; this was found to be a helpful means of identifying subtle metre- to dekametre-scale changes in apparent clay content of the drilled and logged strata.

Core logs focus on describing the rock type and physical state of the cores, including documentation of recovered thicknesses of core with respect to lithological boundaries, core box ends, and drillers' depth blocks.

The following personnel worked on the cores:

Initial	Name	Title
AA	Andres Acevado	Geologist
EP JH	Ernie Popyk, Jerry Holmes	Geologist Project Geologist
KT	Karys Leonard-Fortune,	Geologist
TH	Tyler Hnatiuk	Geological Technician

Original manuscript core description forms are stored in the minesite archives at Willow Creek Mine. Xerographic copies are presented following this table, within the printed version of this report; scanned copies (as PDF files) are presented on the flash-drive copies of this report, and also archived within Conuma's technical network.

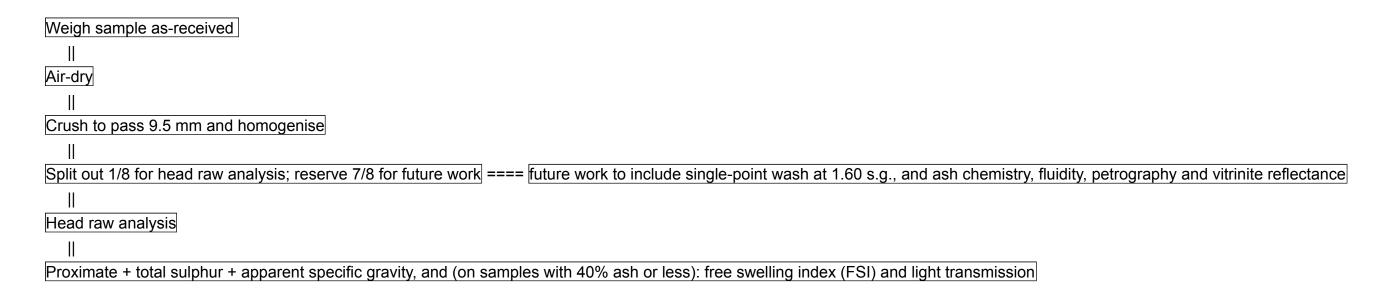
Raw-coal quality data: Appendix B

On this page is presented the flowsheet used for head raw analyses of coal and rock core samples taken from the year-2018 boreholes. Analytical work in this programme was undertaken by Birtley Coal & Minerals Testing in Calgary, Alberta. Provision was made for splitting-out samples to be retained for further work, which has not commenced at the time of this report's compilation (March 17, 2019).

**Table B-1** presents a sample inventory, a cross-reference between sample tag numbers (as assigned by Apex Geoscience) and lab numbers (assigned by Birtley Coal & Minerals Testing). Also presented in this table are results of head raw analyses.

Following the table are copies of analytical certificates from Birtley Coal & Minerals Testing.

#### Flowsheet used for head raw analyses:



	Cross-reference to composites	Head (raw	) samples	Geoph	ysical lo	g interpret	ation				Sample		eterisation								s otherwis	e stated)		
Borehole		<u> </u>	<u> </u>	· ·		De	pth		Dep	th	Thick	ness		Core		Proxi	mate an	alvsis			Addition	al analysi	 S	Comments
Doronoid	Birtley lab Composite no. no.	Birtley lab no.	Sample no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
		+		DC		5.75	6.1		(111)	(111)	CIIL			)										
WC18-01C		-		CBSH	111	6.1	6.45	111	5.75	6.75	1.00	1 00	Not recovered	0.0%										-
WC10-01C		1		DC	┨ '''	6.45	6.75	111	5.75	0.75	1.00	1.00	INOUTECOVERED	0.0 /						 				
WC18-01C		186371	4501	C	110	8.90	9.80	110	8.90	9.80	0.90	0 44	Coal	8.9%	4.04	0.67	37.97	30.58	30.78	0.59	1.5	94.8	1.81	
***************************************		100071	1001	DC		18.65	18.95	110	0.00	0.00	0.00	0.11	Cour	0.070	1.01	0.07	01.01	00.00	00.10	0.00	1.0	0 1.0	1.01	
WC18-01C		186372	4502	C	101	18.95	20.55	101/100	18.65	23.80	5.15	2.18	Coal	39.2%	1.77	0.72	4.09	21.35	73.84	0.54	3.0	97.4	1.32	
				C	100	20.55	23.8																	
WC18-01C				CR	none	38.35	38.55		38.35	38.55	0.20	0.20	Carb mudstone	0.0%										
WC18-01C		186373	4503	С	201	38.55	40.05	201	38.55	40.05	1.50	0.70	Coal	6.7%	2.10	0.66	11.25	19.05	69.04	0.52	2.0	98.0	1.40	
WC18-01C		188197	4951	CR	none	40.05	40.30		40.05	40.30	0.25	0.12	Coaly mudstone	36.0%	0.78	0.61	54.91	14.67	29.81	0.25			1.92	
				DC		42.2	42.45																	
				ASH	]	42.45	42.65						Lost coal seam?,											
WC18-01C		186374	4504	CR	202	42.65	42.8	202	42.20	43.35	1.15	0.54	15 cm siltstone, 10cm	8.7%	1.37	0.86	69.74	9.90	19.50	0.24	n/a	n/a	2.07	
				DC	]	42.8	43.02						coal											
				С		43.02	43.35																	
WC18-01C				С	310	55.2	55.6	310	55.20	55.60	0.40	0.18	Coaly mudstone	70.0%										
				С	]	61.6	61.9						Coal and broken chunks											
WC18-01C		186375	4505	DC	300	61.9	62.05	300	61.60	62.60	1.00	0.44	of carbonaceous	5.0%	1.64	0.83	50.15	13.94	35.08	0.43	n/a	n/a	1.82	
				С		62.05	62.6						mudstone											
WC18-01C		186376	4506	DC	320	69.2	69.5	320	69.20	69 80	0.60	0.26	Stony coal, coal,	65.0%	2.35	0.76	12.41	18.23	68.60	0.72	2.0	96.5	1.38	
		1.000.0		С		69.5	69.8	020				UU	sheared coal	00.070		00				V <u>-</u>				
		-		CBSH	]	73.9	74.7																	
				CR	]	74.7	74.95																	
WC18-01C		188198	4952	DC	]	74.95	75.15		74 70	75 90	1 20	0.53	Coaly mudstone	64.2%	3.51	0.84	58.65	12.41	28.10	0.53			1.89	
		100100	1002	CR	]	75.15	75.6		0	10.00	1.20	0.00	Soury madetone	011.270	0.01	0.01	00.00		=00	0.00			1.00	
				DC	]	75.6	75.9																	
				CBSH	340	75.9	76.25	340																
				R		76.25	76.4	-																
				CBSH	]	76.4	76.8																	
WC18-01C				CR	.	76.8	77.2																	
				CBSH		77.2	77.65																	
				CR		77.65	78.35																	
				CBSH		78.35	78.55																<u> </u>	

		ference to	Head (raw)	samples	Geoph	ysical lo	g interpre	tation				Sample	e charac	cterisation			Head r	aw anal	lysis (air c	ried bas	sis unles	ss otherwi	se stated)		
Borehole		Composite	Dirtloy Joh	Comple			De	pth		Dep	oth	Thic	kness		Core		Proxi	mate ar	nalysis			Addition	nal analysi	s	Comments
	no.	no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
					CBSH	410?	111.65	112.2	410?	111.65	111.90	0.25	0.12	Stony coal	0.0%										110.50-113.50m there was no
W040 040			400077	4507	CR	none	112.2	112.4							0.0%	2.00	0.70	40.54	00.40	F0.00	0.40	0.5	000	1 40	core recovery, noted by the
WC18-01C			186377	4507	С	401	112.4	113.6	401	111.90	113.60	1.70	0.82	Coal	44.1%	3.99	0.76	19.51	20.10	59.63	0.42	6.5	98.3	1.42	drillers
					С	400	113.6	115.6	400	113.60	115.60	2.00	0.97	Coal	1.0%										
WC18-01C					С	420	115.6	115.8	420	115.60	115.80	0.20	0.10	Not recovered	0.0%										
WC18-01C			186378	4508	С	440	118.90	119.65	440	118.90	119.65	0.75	0.52	Coal	26.7%	6.40	0.74	17.77	18.56	62.93	0.69	4.0	98.3	1.42	
					CBSH	463	129.30	130.40																	
WC18-01C					CR	460	137.1	137.3	460	137.10	137 50	0.40	0.19	Coal	5.0%										
WC10-01C					CBSH		137.3	137.5	+00	137.10	107.00	0.40	0.13	Coal	3.070										
					CBSH	483?	139.55	139.9																	
					Fault	Poss.	139.9	140.1														ļ	ļ		
WC18-01C					CR	460	144.40	144.60	460	144.40	144.60	0.20	0.10	Coal	35.0%							1			
***************************************					CBSH	100	144.6	144.8	460	ļ												<u> </u>			
WC18-01C			188199	4953	CR	none	156.40	156.65		156.40	156.65	0.25	0.12	Coaly rock, coaly mudstone	152.0%	1.76	0.36	22.65	30.35	46.64	0.75	2.0	97.7	1.60	More coaly mudstone in box than in geophysical log
					С		156.65	157.05																	
WC18-01C			186379	4509	DC	480	157.05	157.25	480	156.65	157.90	1.25	0.61	Coal	46.4%	1.63	0.66	14.92	24.89	59.53	0.90	7.0	94.8	1.44	
					С		157.25	157.65														1			
WC18-01C			186380	4510	С	A7	172.85	173.80	A7	172.85	173.80	0.95	0.60	Coal	28.4%	1.73	0.64	13.67	17.82	67.87	0.87	3.0	98.6	1.39	
					CBSH	170?	6.05	6.3														-			
WC18-02C			188200	4954	C	150	9.8	10.1	150	9.80	10.40	0.60	0.34	Coal	50.0%	3.10	0.66	20.95	21.72	56.67	0.84	8.0	97.4	1.46	
					DC		10.1	10.4		10.10	40.00				400.00/			-			-	-	-	-	
WC18-02C					CR	none	10.40	10.60	120	10.40	10.60			Carb mudstone	100.0%							+		-	
WC18-02C WC18-02C	-		188233	4987	CBSH DC	130 111	16.65 20.55	17.05 20.90	130 111	16.65 20.55	17.05 20.90		0.30	Carb mudstone	25.0% 48.6%	1.81	0.47	17.08	26.30	56.15	0.92	4.5	96.8	1.45	
VVC 10-02C			100233	4907	DC	111	20.55	22.43	111	20.55	20.90	0.33	0.32	Coal	40.0%	1.01	0.47	17.00	20.30	30.13	0.92	4.5	90.0	1.45	
WC18-02C			186381	4511	C	110	22.43	22.43	110	22.00	22.60	0.60	0.55	Coal	5.0%	2.71	1.57	12.64	17.94	67.85	0.70	2.5	98.3	1.39	
WC18-02C			186382	4512	C	101	26.00	26.55	101	26.00	26.55	0.55	0.49	Coal	98.2%	2.27	0.74	4.08	21.84	73.34	0.45	4.0	97.7	1.33	
WC18-02C			186383	4513	C	100	26.55	27.80	100	26.55					42.4%	2.90	0.74	10.22	23.94				96.2	1.35	
					DC		32.5	32.59					1	1											
WC18-02C			186384	4514	С	201	32.59	33.3	201	32.50	33.30	0.80	0.73	Stony coal, coal	61.3%	2.03	0.86	13.38	20.15	65.61	0.57	4.0	94.2	1.38	
					С		35.5	35.7																	
WC18-02C			186385	4515	DC	202	35.7	35.83	202	35.50	36.06	0.56	0.55	Coal	75.0%	1.89	0.68	8.05	19 85	71.42	0.64	3.0	98.3	1.35	0.16m added from picked 0.35m
			'00000		C		35.83	36.03			30.00	0.00	0.00		. 5.5 , 6	1.00	0.00	0.00		2	0.01	0.0	55.5		parting
					DC		36.03	36.05																	

	Cross-refere		Head (raw)	samples	Geoph	ysical lo	g interpre	ation				Sample	e charac	cterisation			Head r	aw anal	ysis (air d	ried bas	sis unles	s otherwis	se stated)		
Borehole	Birtley lab Co	omnocito	Dirtloy lab	Sample			De	pth		Dep	oth	Thick	ness		Core		Proxi	mate an	alysis			Addition	nal analysi	S	Comments
	no.	no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent )	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-02C			186386	4516	ASH	202 (con-	36.05	36.16	202 (con-	36.06	36.17	0.11	0.11	Sandstone (very fine- grained, pale grey, massive)	100.0%	0.86	0.62	81.24	13.67	4.47	0.07	n/a	n/a	2.37	Dirty coal top (0.16m applied to sample 4515) and bottom (0.08m applied to sample 4517) with sandstone parting of 0.11m
WC18-02C			186387	4517	DC C	tinued)	36.16 36.25	36.25 36.55	tinued)	36.17	36.55	0.38	0.38	Stony coal, Coal	102.6%	1.59	0.60	6.74	22.41	70.25	0.75	8.5	97.1	1.31	0.08m added from picked 0.35m parting
WC18-02C					CBSH	310	44.75	45.10	310	44.75	45.10	0.35	0.33	Mudstone with coal spars	68.6%										
WC18-02C			188234	4988	DC	300	49.75	49.88	300	49.75	49.88	0.13		Stony coal	100.0%	1.83	0.61	64.23	12.95	22.21				1.97	
WC18-02C			186388	4518	С	300	49.88	50.40	300	49.88	50.40	0.52	0.52	Coal	75.0%	6.19	0.87	22.98	21.49	54.66	0.60	1.5	95.4	1.50	
					С		54.20	54.35																	
WC18-02C					R	320	54.35	54.39	320	54.20	54.46	0.26	0.21	Coal/mudstone/coal	100.0%										
					С	1	54.39	54.46																	
WC18-02C					CBSH	340	56.15	57.55	340	56.15	57.55	1.40	1 13	Not recovered?	67.9%							<u> </u>			
WC18-02C			188240	4994	С	410	79.35	79.50	410	79.35		0.15			100.0%	0.52	0.38	10.63	19.35	69.64	0.71	3.5	98.3	1.36	
W040 000			400000	4540	С	401	80.05	80.6	404/400					İ	05.00/			44.55		70.00	0.44	4.0	00.0	4.00	
WC18-02C			186389	4519	С	400	80.6	81.4	401/400	80.05	81.40	1.35	1.13	Coai	25.2%	3.08	1.09	11.55	17.04	70.32	0.44	1.0	98.3	1.36	
WC18-02C			186390	4520	DC		83.55	83.79	420	83.55	83.79	0.24	0.20	Coal	108.3%	1.62	0.60	22.19	26.81	50.40		1.5	98.6	1.61	
WC18-02C			188238	4992	С	420	83.79	84.05	420	83.79	84.05	0.26		Sheared carb. mudstone	65.4%	3.12	0.51	56.50	14.93	28.06				1.93	
WC18-02C			186391	4521	DC		84.05	84.60	420	84.05	84.60			Coal	50.9%	1.91	0.70	6.17	20.80	72.33		1.5	98.0	1.34	
WC18-02C			188239	4993	DC	422	85.00	85.40	422	85.00	85.40			Coal	37.5%	6.78	0.46	60.43	11.73	27.38				1.91	
WC18-02C			188235	4989	С	440	89.25	89.6	440	89.25				Coal, dirty coal	22.9%	2.18	0.47	33.51	17.72	48.30		1.5	98.6	1.59	Corrected log page 13.5
WC18-02C			188236	4990	R	none	89.6	89.77	440	89.60	89.77	0.17		Ash band	58.8%	0.97	0.36	57.71	16.11	25.82				1.96	May have been two ash layers
WC18-02C			186392	4522	DC	442	89.77	89.90	440	89.77	89.90	0.13	0.13	Coal	100.0%	1.38	0.70	19.53	18.81	60.96	0.65	3.0	98.6	1.44	
WC18-02C			188237	4991	CR	none	89.9	90		89.90	90.00	0.10	0.10	Coaly rock	80.0%	0.67	0.46	44.98	12.46	42.10	0.44			1.68	Not in log - upon resampling seam, noticed the coaly rock
		T			DC	]	105.1	105.33																	
WC18-02C			186393	4523	С	460	105.33	105.39	460	105.10	105.50	0.40	0.37	Coal	42.5%	0.88	0.48	16.33	18.48	64.71	0.80	2.5	99.1	1.46	
					DC		105.39	105.5														ļ			
					DC			115.44																	
WC18-02C			186394	4524	R	480	115.44		480	115.20	116.10	0.90	0.85	Coal	73.3%	1.20	0.49	15.76	20.27	63.48	0.89	7.0	99.1	1.46	
W040 000			400005	4505	l C	D: a	115.55	116.1	D: u	24.00	25.00	4.00	0.05	Onel made with the	07.00/	4.00	0.75	20.00	04.50	40.70	0.00	<u> </u>	000	4.00	
WC18-03C			186395	4525	DC	Bird	34.6	35.6	Bird	34.60	35.60	1.00	0.95	Coal, coaly mdst, coal	87.0%	1.68	0./5	36.96	21.59	40.70	2.69	5.0	96.2	1.63	
	+				CBSH	190	41.7	41.95						Cool siltatona cool	$\vdash$		-				-	-	-	-	
WC18-03C			186396	4526	DC	150	55.35	55.90	150					Coal, siltstone, coal, siltstone, coal	98.2%	1.65	0.73	28.83	20.30	50.14	0.82	7.5	99.4	1.52	
WC18-03C					CBSH	130	60.25	60.70	130					Not recovered	0.0%						ļ				
WC18-03C					DC	111	64.20	64.50	111	64.20	64.50	0.30	0.28	Coal	43.3%										

	Cross-reference composite		Head (raw)	samples	Geophy	ysical lo	g interpret	ation				Sample		eterisation							•	s otherwis	•		Sheet 4 of 40
Borehole	Birtley lab Com		Rirtlev lah	Sample			De	pth		Dep	oth	Thick	ness		Core		Proxi	mate an	alysis			Addition	al analysi	s	Comments
	1 -	no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	(percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-03C			186397	4527	С	110	65.55	65.90	110	65.55	65.90	0.35	0.35	Dirty coal / coal	74.3%	1.54	0.57	4.20	23.77	71.46	0.93	8.0	98.0	1.31	
WC18-03C			186398	4528	С	101	69.05	69.60	101	69.05	69.60	0.55	0.53	Coal	94.5%	1.66	0.81	4.39	20.40	74.40	0.59	2.0	99.1	1.32	
WC18-03C			186399	4529	C DC	100	69.9 71.8	71.8 72	100	69.60	72.00	2.40	2.32	Coal	58.7%	2.78	0.97	2.48	22.73	73.82	0.53	4.5	98.8	1.29	
WC18-03C			186400	4530	C DC	201	85.6 86.42	86.42 86.55	201	85.60	86.55	0.95	0.90	Dirty coal, coal, mudstone parting, coal	70.5%	1.80	0.65	8.19	22.43	68.73	0.71	7.0	98.8	1.32	
WC18-03C			186401	4531	С		87.20	87.65	202	87.20	87.65	0.45	0.42	Coal	77.8%	1.79	0.79	7.13	20.61	71.47	0.58	2.5	98.3	1.33	
WC18-03C			186402	4532	ASH	202	87.65	88.02	202	87.65	88.02	0.37	0.36	Mudstone/siltstone	40.5%	0.78	0.60	82.96	12.62	3.82	0.05	n/a	n/a	2.41	
WC18-03C			186403	4533	С		88.02	88.40	202	88.02	88.40	0.38	0.36	Coal	13.2%	1.86	0.55	17.55	18.55	63.25	0.63	3.0	98.8	1.42	
WC18-03C					CBSH	330	94.25	94.55	330	94.25	94.55	0.30	0.28	Mudstone with coal spars?	100.0%										
					CR		95.85	96.00																	
WC18-03C					DC	310	96	96.15	310	95.85	96.70	0.85	0.78	Not recovered	0.0%										
					CR		96.15	96.7															ļ	ļ	
					CR	none	97	97.1																	
WC18-03C			186404	4534	DC		97.1	97.3	300	97.00	97.40	0.40	0.37	Ground coal, dirty coal	92.5%	3.53	0.66	38.16	16.04	45.14	0.39	2.5	98.6	1.61	
		$\rightarrow$			CR		97.3	97.4															ļ	-	
					CBSH	300	97.4	97.55																-	
WC18-03C			186405	4535	DC		97.55 97.7	97.7 98.4	300	97.55	98.40	0.85	0.80	Coal	20.0%	1.59	0.61	6.60	19.93	72.86	0.59	2.5	98.6	1.33	
		-+			CBSH		101.3	101.75			-				-									-	
WC18-03C	<del> </del>	$\rightarrow$			CR	320?	101.75	101.75	320?	101.75	102.20	0.45	0.41	Not sampled	100.0%								-	<u> </u>	
WC18-03C		-+			CBSH	340	105.40	105.65	340					Mudstone	100.0%										
WC18-03C					CBSH	410	121.35	121.55	410	121.35				Carb mudstone	145.0%									1	
			100/55		C	401	121.55	122.4							1							1	<b>.</b>	1	16cm of ground core represents
WC18-03C			186406	4536	C		122.4	123.7	401/400	121.55	123.70	2.15	2.14	Coal	7.4%	22.12	0.86	33.90	15.24	50.00	0.40	1.0	94.5	1.56	the 401 and 400
WC18-03C					DC	400	123.7	123.95	400	123.70	123.95	0.25	0.25	Not recovered	0.0%										
WC18-03C					CBSH	420	125.00	125.35	420					Carb mudstone	100.0%										
WC18-03C			186407	4537	DC	440	131.20	131.50	440	131.20					100.0%	1.04	0.52	33.44	17.72	48.32	0.60	2.5	95.4	1.58	
		1			CBSH	442	133.80	134.05																	
WC18-03C			188241	4995	CBSH	463	135.95	136.65	463	135.95	136.65	0.70	0.69	Coal - pyrite	8.6%	1.36	0.34	39.44	27.63	32.59	2.55	2.5	96.2	1.80	
					CBSH	460	140.50	140.80																	
					CBSH	483	143.75	143.90																	
WC18-03C			186408	4538	C DC	480	148.45 149.05	149.05 149.35	480	148.45	149.35	0.90	0.90	Coal	61.1%	1.21	0.48	16.64	26.41	56.47	1.08	7.0	98.6	1.46	
WC18-03C			186409	4539	C DC	A7	159.3 159.7	159.7 159.9	A7	159.30	159.90	0.60	0.60	Coal	38.3%	1.45	0.73	10.63	19.78	68.86	0.94	3.0	98.8	1.36	

## Head raw analyses and cross-reference to composite samples Table B-1 - sheet 5 of 40

	1	eference to posites	Head (raw)	samples	Geoph	ysical lo	g interpre	ation				Sample	e charac	eterisation			Head r	aw anal	ysis (air d	dried ba	sis unles	ss otherwi	se stated)		
Borehole	Dirtley Joh	Composito	Dietlavilah	Cample			De	pth		Dep	oth	Thick	kness		Core		Proxi	mate an	alysis			Addition	nal analys	is	Comments
	no.	Composite no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-03C					CR	none	180.9	181		180.90	181.00	0.10	0.10	Not recovered	0.0%					ľ	ľ				
WC18-03C			186410	4540	С	A5	181.00	181.40	A5	181.00		0.40		Coal	72.5%	7.23	0.64	17.89	18.35	63.12	0.99	9.0	97.4	1.41	
WC18-03C					CR	none	189.80	190.00		189.80	190.00	0.20	0.19	Not recovered	0.0%										
WC18-03C			186411	4541	DC	A3	190 190.2	190.2 190.45	A3	190.00	190.45	0.45	0.42	Coal	93.3%	2.47	0.83	25.60	18.28	55.29	0.78	8.0	98.6	1.47	
WC18-03C					CR	A1	190.2	190.45	A1	192.90	102.20	0.20	0.20	Carb mudstone	100.0%		-					-		-	
VVC 10-03C					CR	A0	194.05	193.20	A1	192.90	193.20	0.30	0.30	Carb muusione	100.0%										
WC18-03C					DC	511	216.20	216.65	511	216.20	216 65	0.45	0.45	Mudstone with coal beds	4.4%								<u> </u>	<u> </u>	
WC18-03C			186412	4542	CR	510	217.20	217.50	510	217.20					33.3%	2.67	0.83	46.43	14.13	38 61	0.59	n/a	n/a	1.72	
WC18-04C			186413	4543	DC	0.10	53.26	53.74	010					Coal rock	12.5%	2.23	0.94		21.92			5.5	94.5	1.58	Very little dirty coal recovery at top of Bird; coaly rock only after top 6 cm.
					CR	Bird	53.74	53.85	D: 1																
					DC	] [	53.85	53.97	Bird					Coaly mudstone and											
WC18-04C					CR	] [	53.97	54.29		53.74	54.62	0.88	0.68	carbonaceous mudstone	98.9%										
					DC		54.29	54.42						da bonacodo madolono											
					CR	none	54.42	54.62																	
					CR	190	62.4	62.7			-														
14/040 040					CBSH	170	77.7	78		00.74	00.00	0.04	0.44	N. ( 10	0.00/									-	
WC18-04C					CR	none	82.74	82.98		82.74	82.98	0.24	0.14	Not recovered?	0.0%										
					C CR		82.98 83.14	83.14 83.27																	
WC18-04C			186414	4544	DC	150	83.27	83.33	150	82.98	83 63	0.65	0.37	Coal, coaly rock (carbonaceous	90.8%	1.93	0.87	61.51	17.22	20.40	0.31	n/a	n/a	1.96	No apparent coaly rock above DD 83m, nor coaly rock below ground
VVC 10-04C			100414	4544	C	130	83.33	86.14	130	02.90	05.05	0.03	0.57	mudstone?), coal	90.07	1.95	0.07	01.51	17.22	20.40	0.51	II/a	11/a	1.90	7 cm of coal at base
					DC	1 1	83.41	83.63						, , , , , , , , , , , , , , , , , , ,											Tom or ocal at bacc
WC18-04C					CR	none	83.63	83.82		83.63	83.82	0.19	0.15	Carb mudstone	100.0%										
WC18-04C					CR	130	89.7	90	130	89.70	90.00			Carb mudstone	100.0%										
					CR		95.5	95.78																	
WC18-04C			186415	4545	DC	111	95.78	95.9	111	95.50	96.06	0.56	0.34	Coal	92.9%	1.46	0.74	8.85	23.99	66.42	0.57	7.0	98.0	1.36	
					CR	1 1	95.9	96.06																	
					DC		97.7	97.95																	
WC18-04C				]	С	110	97.95	98.04	110	97.70	98.21	0.51	0.29	Coal	49.0%										
					DC		98.04	98.21																	
					CR	none	101.83	101.93																	
WC18-04C			186416	4546	С	101	101.93	103.01	101/100	101.83	105 94	4 11	2 96	Coal	60.6%	2.07	0.81	2.95	21.08	75 16	0.51	3.0	98.3	1.29	No visible separation, so one
71010-040			100710	1070	С	100	103.01	105.85	10 1/ 100	101.00	100.04	7.11	2.50		00.070	2.01	0.01	2.55	21.00	70.10	0.01	0.0	33.3	1.25	sample
					DC		105.85	105.94																	

	Cross-re	ference to						. [												•			•		S I Sheet o of 40
		osites	Head (raw)	samples	Geoph	ysical lo	g interpre	tation				Sample	e charac	cterisation			Head r	aw anal	lysis (air d	ried bas	is unles	ss otherwis	se stated)		
Borehole	Diation lab	0	Diatles dela	01-			De	pth		Dep	oth	Thicl	kness		Core		Proxi	mate an	nalysis			Addition	al analysi	S	Comments
	no.	Composite no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
					DC		125.71	125.82		, ,	, ,				'							1			
WC18-04C			186417	4547	С	201	125.82	126.78	201	125.71	127.03	1.32	0.98	Coal	45.5%	3.03	0.78	13.67	21.22	64.33	0.56	7.0	98.0	1.36	
					DC		126.78	127.03																	
WC18-04C	ļ				CR	none	127.03	127.17		127.03	127.17	0.14	0.10	Not recovered	100.0%								ļ		
					CR	none	127.89	128																	
WC18-04C			186418	4548	DC		128	128.09	202	127.89	128.60	0.71	0.50	Coal	95.8%	1.77	0.71	11.24	20.73	67.32	0.58	0.40	97.1	1.35	
14/0/10 0/10	-		100110	45.40	C	202	128.09	128.6		400.00	400 ==	0.47	0.40		100.00/	4.40	0.00	74.00	44.47	40.70	0.40	ļ ,	,	0.45	
WC18-04C	-		186419	4549	ASH		128.6	128.77		128.60	128.77	0.17	0.12	Ash	100.0%	1.10	0.68	74.09	14.47	10.76	0.12	n/a	n/a	2.15	
WC18-04C			186420	4550	CR C	202	128.77 129.02	129.02 129.48	202	128.77	129.48	0.71	0.50	Dirty coal, coal	83.1%	1.77	0.65	7.13	25.57	66.65	0.77	8.5	96.0	1.32	
WC18-04C					CBSH	310	140.2	140.6	310	140.20	140.60	0.40	0.22	Carb mudstone	50.0%										
WC18-04C					CR	none	141.85	141.94		141.85				Not recovered	0.0%										
WC18-04C					DC		141.94	141.98	200					Not recovered	0.0%										
WC18-04C					С	300	141.98	142.64	300	141.98	142.64	0.66	0.49	Not recovered	0.0%										
					Fault	Poss.	142.64	142.85																	
WC18-04C			186421	4551	С	300	142.85	144.12	300	142.85	144.12	1.27	0.94	Coal	11.8%	2.05	0.60	24.58	29.63	45.19	0.49	2.5	97.7	1.60	No recovery of 310 above, or only recovery for both?
WC18-04C					CR	none	144.66	144.74		144.66	144.74	0.08	0.06	Carb mudstone	100.0%										
WC18-04C			186422	4552	DC C	320	144.74 145.02	145.02 145.82	320	144.74	145.82	1.08	0.80	Coal	66.7%	3.56	0.76	9.62	23.97	65.65	0.58	4.5	97.1	1.37	
					CR		149.5	150.25																	
WC18-04C					CBSH	340	150.25	150.4	340	149 50	  151 15	1 65	1 17	Coaly mudstone	34.5%								ļ		
W010 040					CR	0,10	150.4	150.55	040	143.00	101.10	1.00	'''	Codiy madotone	04.070										_
11/0/10 0/10	ļ				CBSH		150.55	151.15			1 00	2.4-	0.10		100.00/								ļ		
WC18-04C					CBSH	360	155.45	155.62	360					Carb mudstone	100.0%										
WC18-04C WC18-04C					CBSH CR	410	180.30 181.00	180.48 181.08	410	180.30				Coaly mudstone	227.8% 50.0%									-	
VVC10-04C	<del> </del>				DC	none	181.08	181.2		101.00	101.00	0.00	0.00	ASII!	30.0%								-	-	
					C	401	181.2	182.63																	
					C	400	182.63	183.02																	
WC18-04C			186423	4553	Fault	Poss.	183.02	183.1	401/400/	181.08	  187.80	6.72	4.58	Coal	28.7%	5.23	0.75	2.85	19.94	76.46	0.47	2.0	95.7	1.29	
					С		183.1	187.56	Fault/			•=													
					DC	400	187.56	187.65	400																
					С	400	187.65	187.8																	
WC18-04C					DC		187.8	187.91		187.80	100 01	0.21	0.14	Not recovered?	0.0%										
					CR	none	187.91	188.01																	
WC18-04C					CR	420	191.00	191.40	420	191.00	191.40	0.40	0.29	Coal, coaly mudstone	42.5%										

	Cross-ref	ference to osites	Head (raw)	) samples	Geoph	ysical lo	g interpre	tation				Sample	e charac	eterisation			Head r	aw anal	ysis (air d	ried bas	is unles	s otherwis	se stated)		
Borehole	Rirtley lah	Composite	Rirtley lah	Sample			De	pth		Dep	th	Thicl	kness		Core		Proxi	mate an	alysis			Addition	nal analysi	is	Comments
	no.	no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	(percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-04C					CR	none	198.74	198.84		198.74	198.84	0.10	0.07	Not recovered	0.0%										
					DC		198.84	198.9																	
					С	]	198.9	199.12																	
					DC	_	199.12	199.16						Coal, dirty coal with ash?,											
WC18-04C			186424	4554	С	440	199.16	199.33	440	198.84	199.55	0.71	0.48	Icoal	84.5%	0.95	0.55	16.90	19.80	62.75	0.78	4.0	95.4	1.42	
					DC	]	199.33	199.36						Joodi											
					С	1	199.36	199.46																	
					DC		199.46	199.55																	
WC18-04C					CR	none	199.55	199.64		199.55	199.64			Carb mudstone	100.0%								ļ	<u> </u>	
WC18-04C					CR	none	205.70	205.90						Carb mudstone	35.0%										
WC18-04C					CR	463	207.00	207.40	463	207.00	207.40	0.40	0.27	Not recovered?	0.0%					ļ				ļ	
					CBSH	460?	213.70	214.10																ļ	
					CBSH	483?	218.39	219.25									ļ						<u> </u>	-	1
					DC			225.19	400																
WC18-04C			186425	4555	C	480	225.19	226.25	480	225.12	226.40	1.28	0.98	Coal	16.4%	1.59	0.61	8.41	20.46	70.52	1.01	7.0	97.1	1.34	
14/040 040					DC	-	226.25	226.40		000.70	000.00	0.00	0.04		50.00/								-	<del> </del>	
WC18-04C					DC	none	232.7	233.02	400	232.70				<u> </u>	50.0%								-	-	
WC18-05C				-	CBSH	130	10.5	10.85	130	10.50	10.85	0.35	0.32	Carb mudstone	48.6%									<del>                                     </del>	
WC18-05C				-	DC CR	111	14.04 14.18	14.18 14.42	111	14.04	14.42	0.38	0.34	not recovered	0.0%								+	-	-
WC18-05C			188201	4955	C	none 110		15.94	110	15.60	15.04	0.24	0.22	DC/coaly mudstone	23.5%	0.74	0.37	49.11	43.54	6.98	0.24		-	2.37	
VVC 10-03C			100201	4900	C	101	15.6 17.93	18.95	110	15.60	15.94	0.34	0.32	DC/coaly mudstone	23.5%	0.74	0.37	49.11	43.54	0.90	0.24			2.31	
WC18-05C			186426	4556	C	101	18.95	20.87	101/100	17.93	20.05	3 02	2.80	Coal	22.5%	2.30	0.79	2.77	21.03	75.41	0.49	3/5	96.8	1.31	
VVC 10-03C			100420	4550	DC	100	20.87	20.95	10 1/ 100	17.33	20.33	3.02	2.00	Coal	22.570	2.50	0.73	2.11	21.00	75.41	0.43	3/3	30.0	1.51	
WC18-05C					CR	none	28.44	28.56		28.44	28 56	0.12	0.11	Carb mudstone	58.3%								+	-	
VVO 10-030					C	Hone	28.56	29.21		20.44	20.50	0.12	0.11	Carb mudstone	30.370								+	<del>                                     </del>	Bad recovery- chips of
WC18-05C			188231	4985	DC	201	29.21	29.31	201	28.56	29.31	0.75	0.72	Coal/Coaly mudstone	9.3%	1.49	0.38	52.38	14.65	32.59	0.27			1.83	carbonaceous mudstone were hard to sort out from dirty coal.
WO40 050					С	202	30.3	30.51	000	20.00	20.00	0.00	0.00	Divid blood	40.70/								1	1	,
WC18-05C				1	CR	none	30.51	30.6	202	30.30	30.60	0.30	0.28	Black blocky mud	16.7%								1	1	1
					CBSH		35.3	35.7					İ	01 1.1 1									1	1	0.1
WC18-05C					R CBSH	310	35.7 36	36 36.4	310	35.30	36.40	1.10	1.03	Coaly mudstone / carb mudstone	72.7%										Carbonaceous mudstone and 3cm of coaly mudstone
WC18-05C			186427	4557	C ASH?	300	41.16 41.28	41.28 41.35	300	41.16	41.53	0.37	0.36	Coal / two competent pieces of dirty coal, coal	97.3%	2.21	0.67	19.60	25.08	54.65	0.68	5.0	98.0	1.47	
\MC10.05C				-	C	none	41.35	41.53		11 52	11 70	0 17	0 17	Carb mudatons	100.00/		-			-			<del>                                     </del>	<del>                                     </del>	
WC18-05C					CR	none	41.53	41.7		41.53	41./0	0.17	J U.17	Carb mudstone	100.0%										

## Head raw analyses and cross-reference to composite samples Table B-1 - sheet 8 of 40

		eference to posites	Head (raw)	samples	Geoph	ysical lo	g interpre	tation				Sample	e chara	cterisation			Head r	aw anal	ysis (air d	ried bas	is unles	s otherwis	se stated)		
Borehole	Dirtley Joh	Composite	Dirtloy Joh	Cample			De	pth		Dep	oth	Thicl	kness		Core		Proxi	mate an	alysis			Addition	al analysi	s	Comments
	no.	no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-05C			186428	4558	С	320	45.62	45.8	320	45.62	45.80	0.18	0.17	DC/C	177.8%	1.99	0.79	24.74	17.32	57.15	0.75	2.5	98.6	1.49	Sampled as per log: 0.15m of dirty coal and 0.17m of coal
					CBSH		48.02	48.23																	
					CR		48.23	48.36						Coaly rock and										ļ	Recovery is all grinding and
WC18-05C					CBSH	340	48.36	48.53	340	48.02	49.42	1.40	1.39	carbonaceous mudstone	55.0%									ļ	gouge according to log
					R	1	48.53	48.74																	- geage according to log
	ļ				CBSH		48.74	49.42				2.22			2.22/									1	
WC18-05C	-				CBSH	360	52.3	52.6	360	52.30	52.60			Not recovered	0.0%										
WC18-05C					DC	410	70.7	70.88	410	70.70	70.88	0.18	0.17	Dirty coal	38.9%										14000/
					С	401	71.48	72.3																	100% recovery? Depths for seams 401-400 and 440 work
WC18-05C			186429	4559	C DC	400	72.3 73.24	73.24 73.35	401/400	71 48	73.51	2.03	1 95	DC/C	100.0%	3.14	0.81	7.58	18.79	72.84	0.51	1.0	98.3	1.35	right, what happened to 0.35m of
W 0 10 000			100120	1000	CR	none	73.35	73.51	10 17 100	71.10	70.01	2.00	1.00		100.070	0.11	0.01	7.00	10.70	72.01	0.01	1.0	00.0	1.00	rock? 420 was found downhole of the 4 seam.
					С		73.7	74.6									1								Very bad recovery - coal is ground
WC18-05C			188232	4986	DC	420	74.6	74.68	420		74.68			Coal	7.1%	5.01	0.54	47.23	17.18	35.05	0.65			1.73	into mud and carbon-aceous mudstone chips are hard to sort out. Original log identified it as a broken area with shearing.
WC18-05C					CR	none	74.68	74.8		74.68	74.80	0.12	0.11	Not recovered?	0.0%										
					DC		77.32	77.42	]																
					С	]	77.42	77.53	ļ					Coal, ash band?, coal,											
WC18-05C			186430	4560	DC	440	77.53	77.63	440	77.32	77.94	0.62	0.58	dirty coal	66.1%	1.68	0.71	25.05	18.04	56.20	0.55	2.0	98.8	1.48	
					С		77.63	77.75																	
	-				DC	110	77.75	77.94																-	
	-		-		CBSH	442	80.45	80.7					-				-							-	
WC18-05C	-		-		CBSH CR	463 460	98.05 93.55	89.6 93.85	460	93.55	03 05	0.30	0.20	Coal rock	60.0%	1.60	0.61	18.44	26.58	54 27	0.05	7.0	98.0	1.49	
WC 10-03C	-		-		C	400	102.54	103.13	400	33.55	33.03	0.30	0.29	Dirty coal, coal, coalified	00.0%	1.00	0.01	10.44	20.50	154.57	0.00	1.0	90.0	1.49	
WC18-05C			186431	4561	DC	480	103.13	103.13	480	102.54	103.35	0.81	0.79	wood parting, coal, dirty	84.0%										
WC18-05C					CR	none	113.81	113.94		113.81	113.94	0.13	0.12	Carb mudstone	100.0%	1.84	0.83	6.80	19.56	72.81	0.96	6.5	98.0	1.32	
WC18-05C			186432	4562	С	A7	113.94	114.78	A7	113.94					61.9%										
					CBSH	A5?	122.35	123																	
WC18-06C					DC		4.65	4.9	130	4.65	4.90	0.25	0.25		0.0%										
WC18-06C			186433	4563	CR C	130	4.9 5.1	5.1 5.4	130	4.90	5.40	0.50	0.50	Coaly rock/coal	62.0%	4.21	0.97	81.70	13.44	3.89	0.24	n/a	n/a	2.19	Sampled as parting, mixed with coal? Ground blocky core
WC18-06C					C	111	8.94	9.25	111	8.94	9.25	0.31	0.30	Dirty coal/coal	100.0%		1								
WC18-06C					CR	none	10.32	10.43			10.43	0.11	0.11	Not recovered?	0.0%		1								

		eference to	Head (raw)	samples	Geoph	nysical lo	g interpre	tation				Sample	e chara	cterisation			Head r	aw analy	ysis (air d	ried bas	is unles	s otherwis	se stated)		
Borehole	Dirtlay lab	Composite	Dirtloy lob	Cample			De	pth		Dep	oth	Thick	ness		Core		Proxi	mate an	alysis			Addition	al analysi	S	Comments
	no.	no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent )	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-06C			186434	4564	С	110	10.43	10.84	110	10.43	10.84		0.40		100.0%	2.42	0.70	15.38	22.96	60.96	0.74	3.0	97.4	1.41	
WC18-06C					CR	none	10.84	11.03		10.84	11.03	0.19	0.18	Carb mudstone	100.0%										
					С	101	17.34	17.85																	
WC18-06C			186435	4565	С	100	17.85	19.37	101/100	17.34	19.47	2.13	2.06	Dirty coal/coal	15.5%	11.42	1.06	41.49	16.92	40.53	0.31	1.0	92.8	1.63	
WC18-06C				4565?	DC CR	none	19.37 19.47	19.47 19.58		19.47	19.58	0.11	0.11	Chunky mud	100.0%										May have been sampled in 4565
														-										-	as recovery is a chunky mud
WC18-06C					CR C	none	23.24 23.42	23.42 24		23.24	23.42	0.18	0.18	Carb mudstone	100.0%					-		-			Complete a logged and
WC18-06C			186436	4566	DC	201	23.42	24.07	201	23.42	24.07	0.65	0.64	Dirty coal / coal	115.4%	2.96	0.82	10.85	22.47	65.86	0.64	7.0	95.4	1.32	Sampled as logged, coal recovered 0.75m
WC18-06C					CR	none	24.07	24.07		24.07	24 22	0.15	0.15	Carb mudstone	53.3%									<del> </del>	recovered 0.75m
WC18-06C					CR	none	27.35	27.44			27.44			Ash band?	22.2%									<u> </u>	
11010000					C	110110	27.44	27.66		21.00		0.00	0.00	, torr barra.	22.270									1	_
WC18-06C			186437	4567	DC	1 1	27.66	27.7		27.44	27.88	0.44	0.43	Dirty coal / coal	100.0%	1.81	0.80	8.10	20.26	70.84	0.65	3.5	97.1	1.35	Sampled with interpreted coaly
					CR	202	27.7	27.88	202					,											rock, no coaly rock recovered
WC18-06C			186438	4568	ASH	1 1	27.88	28.04		27.88	28.04	0.16	0.16	Ash band?	100.0%	1.47	0.75	74.04	13.37	11.84	0.10	n/a	n/a	2.15	
WC18-06C			188202	4956	С		28.04	28.18		28.04	28.18	0.14	0.14	Coal	100.0%	1.44	0.49	20.89	20.90	57.72	0.60	7.5	93.4	1.42	
					CR	none	28.18	28.3																	
WC18-06C					CR	none	40.24	40.42		40.24	40.40	0.16	0.16	Ash band and coaly rock	75.0%										Ash parting was recovered, however all coal was ground out.
WC18-06C			188203	4957	DC		40.42	40.64		40.40	40.70	0.30	0 29	Ash parting / coal	96.7%	3.51	0.81	19.74	18.36	61.09	0.49	1.0	92.8	1.44	
WC18-06C			188204	4958	CR DC	300	40.64	40.77 40.97	300	40.70	40.97		0.26	Coalified wood? Parting,	59.3%	2.63	0.41	26.10	30.61	42.88	0.40	1.5	97.7	1.67	
			100204	4330										coal		2.00	0.41	20.10	30.01	42.00	0.40	1.5	31.1	1.07	
WC18-06C					CR	320	45.25	45.6	320	45.25	45.60	0.35	0.34	Coal? Ground to mud	17.1%									-	
					CBSH		45.6	45.9						0			-							-	
WC18-06C					CR	340	48.3	48.6	340	48.30	48.60	0.30	0.30	Coal / coal rock / Car- bonaceous mudstone	70.0%										
					R	1	48.6	49																-	
W040 000					CBSH	440	49	49.7	440	70.00	70.00	0.04	0.04	Melet with a sel enem	400.00/		-							-	
WC18-06C					CR	410	70.62	70.83	410	70.62	70.83	0.21	0.21	Mdst with coal spars	100.0%										
WC18-06C			186439	4569	C	401	71.96 72.63	72.63 74.84	401/400	71.06	75 20	2 24	2 17	Coal / dirty coal	16.7%	11.64	0.75	7.96	18.99	72 20	0.39	1.5	96.8	1.35	
WC10-00C			100439	4309	DC	400	74.84	75.2	401/400	71.90	75.20	3.24	3.17	Coal / ulity coal	10.7 %	11.04	0.75	7.90	10.99	12.30	0.39	1.5	90.0	1.33	
					CBSH	420	75.85	76.22			-				<del>                                     </del>		+	$\vdash$		-	<del>                                     </del>	<del>                                     </del>		+	<del>                                     </del>
					DC	740	78.84	78.95																<u> </u>	+
WC18-06C			186440	4570	C	440	78.95	79.14	440	78.84	79.22	0.38	0.37	Coal / dirty coal	52.6%	3.39	0.69	8.03	20.70	70.58	0.70	3.5	94.2	1.36	
					DC		79.14	79.22						1											

	Cross-referen		Head (raw)	samples	Geoph	ysical lo	g interpret	tation				Sample	e charac	eterisation			Head r	aw anal	ysis (air d	ried bas	is unles	s otherwis	se stated)		
Borehole	Birtley lab Con	mpocito	Dirtlov lah	Cample			De	pth		Dep	oth	Thick	ness		Core		Proxi	mate an	alysis			Addition	al analysi	S	Comments
	1 -	no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
					CBSH	442	80.74	80.94																	
					CBSH	463	87.1	87.35																	
					CBSH	460	91.4	91.8																	
WC18-06C					CR	none	103.33	103.43		103.30	103.43	0.13	0.13	Hornfels? Ironstone?	100.0%										
WC18-06C			186441	4571	С	480	103.43	104.12	480	103 43	104 28	0.85	0.79	Coal / dirty coal	45.9%	3.31	0.70	8.08	23.94	67.28	1.07	8.0	94.2	1.32	
			100111	1071	DC		104.12	104.28	100					-		0.01	0.70	0.00	20.01	01.20	1.07	0.0	01.2	1.02	
WC18-06C					CR	none	104.28	104.48		104.28	104.48	0.20	0.19	Carb mudstone	25.0%									ļ	
					CBSH	A71?	114.70	115.05	A71?															-	
					CR	none	118.37	118.44																	
WC18-06C					DC	A7?	118.44	118.53	A7?	118.37	118.78	0.41	0.19		95.1%										
					C		118.53	118.68																	
14/040 000					CR	none	118.68	118.78		400.07	400.50	0.40	0.04		400.00/										
WC18-06C					CR	none	122.37	122.53		122.37	122.53	0.16	0.01	Carb mudstone	100.0%		-							-	
WC18-06C			188205	4959	DC		122.53	122.77		122.53	123.10	0.57	0.26	Coaly mudstone	17.5%	1.52	0.58	61.79	13.16	24.47	0.35			1.96	
					CR DC	A5	122.77 123.1	123.1 123.32	A5								-							}	
WC18-06C			186442	4572	С	Ab	123.1	123.32	AS	122 10	124 20	1 20	0.52	Dirty coal / coal	40.0%	2.32	0.68	9.27	22.05	68.00	0.83	6.0	95.4	1.35	
VVC 10-00C			100442	4372	DC		123.32	124.2		123.10	124.50	1.20	0.55	Dirty Coal / Coal	40.0%	2.32	0.00	9.21	22.03	00.00	0.03	0.0	95.4	1.33	
WC18-06C					CR	none	124.2	124.76		12// 30	124 76	0.46	N 10	Carb mudstone	21.7%										
VVO 10-000		+			CBSH	A3	141.9	142.2	A3	124.50	124.70	0.40	0.13	Carb madatorie	21.770									<del> </del>	
	<del>                                     </del>	+			CBSH	A1?	147.05	147.35	A1?															1	
	<del>                                     </del>				CBSH	A0?	147.85	148.5	A0?																
					CBSH	none	5.9	6.1	710.																
WC18-07C			186857	4573	DC	110110	6.1	6.3		5.90	6.30	0.40	0.38	Coaly mudstone	37.5%	5.64	1.12	20.15	23.75	54.98	0.98	1.5	58.1	1.47	
			4000-0		CBSH		6.3	6.4	150						10.00/			22 = 1				<b>.</b>	<b>.</b>		
WC18-07C			186858	4574	CR	150	6.4	6.6		6.30	6.55	0.25	0.24	Mudstone pieces	48.0%	4.49	1.32	83.71	7.70	7.27	0.14	n/a	n/a	2.35	
WC18-07C			186859	4575	DC		6.6	6.8		6.55	6.90	0.35	0.33	Ground coal	88.6%	9.59	0.76	27.01	22.05	50.18	0.82	6.5	91.1	1.50	
					CBSH	130	11.2	11.6	130																
WC18-07C			186860	4576	С	111	15	15.3	111	14.95	15.25	0.30	0.28	Coal, dirty coal, ground coal, dirty muddy coal.	113.3%	1.78	0.63	10.97	26.35	62.05	0.87	7.5	88.0	1.39	
WC18-07C			186861	4577	С	110	16.60	17.15	110	16.60	17.15	0.55	0.52	Dirty coal	96.4%	1.70	0.57	15.16	25.53	58.74	0.74	6.0	94.2	1.44	
WC18-07C			186862	4578	С	101	24.45	25.08	101	24.45	25.08	0.63	0.61	Coal	77.8%	2.10	0.62					5.0	95.7	1.31	
					С	100	25.08	26.42	100	25.08	26.42	1.34	1.30	Coal	99.3%								i		
WC18-07C			186863	4579	CR	none	26.42	26.70						Coaly mudstone	10.7%	2.67	0.00	5.74	24.59	09.07	0.50	5.5	93.7	1.32	
WC18-07C			186864	4580	С	201	30.15	30.70	201	30.15					80.0%	2.50			21.92			6.5	97.1	1.38	
WC18-07C			186865	4581	DC	201	30.70	31.00	201	30.70	31.00	0.30	0.30	Coaly mudstone	23.3%	2.11	0.73	46.91	16.98	35.38	0.39	n/a	n/a	1.77	

	Cross-refe		Head (raw)	samples	Geoph	ysical lo	g interpret	ation				Sample	e charac	terisation			Head r	aw anal	ysis (air d	ried bas	is unles	s otherwis	se stated)		
Borehole	Birtley lab (	Composito	Dirtloy lob	Cample			De	pth		Dep	oth	Thick	kness		Core		Proxi	mate an	alysis			Addition	nal analysi	S	Comments
	no.	no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
					С		34.4	34.75																	
WC18-07C			186866	4582	CR	]	34.75	34.9		34.40	35.00	0.60	0.60	Dirty (stony?) coal, coal	76.7%	2.11	0.74	5.61	20.44	73.21	0.73	3.5	98.6	1.33	
					DC	202	34.9	35	202																
WC18-07C			188206	4960	CR	]	35	35.12		35.00	35.12				91.7%	1.38	0.62	79.24	11.86		0.08			2.36	
WC18-07C			186867	4583	С		35.12	35.42		35.12	35.42	0.30	0.30	Dirty coal	26.7%	1.24	0.66	11.00	21.70	66.64	0.72	3.5	97.7	1.36	
WC18-07C			188207	4961	CR	none	46.40	46.55		46.40	46.55	0.15	0.15	Ash band (minor coal inside it)	73.3%	0.66	0.51	66.72	14.43	18.34	0.17			2.16	Coal uphole of ash has not been recovered
WC18-07C			186868	4584	DC C	300	46.55 46.65	46.65 47.2	300	46.55	47.20	0.65	0.65	Dirty coal	30.8%	2.07	0.56	5.49	22.15	71.80	0.67	4	97.4	1.33	
					CBSH		51.2	51.5																	
WC18-07C					CR	320	51.50	51.65	320	51.50	51.65	0.15	0.15	Coaly mudstone	160.0%										
					CBSH		51.65	52.10															ļ		
	]				CBSH	]	53.65	54.08															ļ		
WC18-07C	1 1				CR	340	54.08	54.40	340	54.08	54.40	0.32	0.31	Carb mudstone	100.0%										
14/04/0.07/0			100000	4505	CBSH	140	54.40	55.35	440	70.05	70.50	0.45	0.45		07.00/	4.04	0.04	40.50	40.04	00.00	0.70	0.5	00.0	1.00	
WC18-07C			186869	4585	CR	410	76.05	76.50	410	76.05	76.50	0.45	0.45	Coal / carb mudstone	37.8%	1.84	0.61	13.53	19.24	66.62	0.73	2.5	98.3	1.39	1
WC18-07C			186870	4586	C	401	77.42 77.72	77.72 78.74	401/400	77.42	79.00	1.58	1.54	Coal	22.2%	3.19	0.64	15.48	18.04	65.84	0.41	1.5	99.1	1.39	401/400 were mixed together and were sampled together
WC18-07C			186871	4587	DC DC	420	78.74 80.80	79 81.25	420	80.80	01.05	0.45	0.44	Coal / dirty coal	77.8%	2.46	0.79	48.43	14.17	36.61	0.50	n/o	n/o	1.76	
WC18-07C			100071	4307	CR	440	86.30	86.55	440	86.30				Carb mudstone	72.0%	2.40	0.79	40.43	14.17	30.01	0.50	n/a	n/a	1.70	
VVC10-07C					CBSH	442	87.15	87.00	442	00.50	00.00	0.23	0.24	Carb muustone	12.070								1	-	
WC18-07C			186872	4588	CR	463	91.65	92.02	463?	91.65	92.02	0.37	0.35	Dirty coal / coaly mudstone	24.3%	1.09	0.60	23.31	23.99	52.10	0.83	6.5	98.6	1.50	
WC18-07C					CR	460	97.45	97.60		97.45	97.60	0.15	0.14	maastorio	100.0%										
					Fault	Poss.	99.90	100.00	460				****		1								1		
					CR	460	108.90	109.00																	
					CR		121.65	122.05																	
WC18-07C			186873	4589	CBSH	480	122.05	122.2	480	121 70	122.00	1 20	0.42	Dirty coal	19.2%	5.10	0.72	44.45	16.05	37.88	1.35	n/o	n/o	1.70	
VVC10-07C			100073	4309	CR	] 400	122.2	122.45	400	121.70	122.90	1.20	0.43	Diffy Coal	19.270	5.10	0.72	44.45	10.93	31.00	1.33	n/a	n/a	1.70	
					DC		122.45	122.9																	
WC18-07C					CR	none	128.40	128.70		128.40	128.70	0.30	0.22	Mudstone with coal spars	100.0%										
					CBSH	A71?	133.10	133.45	A71?						ļ								ļ		
WC18-07C			186874	4590	C	A7	136	136.5	A7	136.00	136.65	0.65	0.64	Coal	6.2%	1.43	0.50	27.82	16.48	55.20	0.57	1.0	96.0	0.59	
	<del>                                     </del>				DC		136.5	136.65	- "											<b>-</b>	ļ <b>.</b>	ļ			
WC18-07C					CR	none	150.35	150.65		150.35	150.65	0.30	0.28	Carb mudstone	106.7%								-	-	-
WC18-07C			186875	4591	DC	A5	154.1 154.7	154.7 154.95	A5	154.10	154.95	0.85	0.78	Coal	23.5%	2.64	0.57	2.67	24.23	72.53	0.96	9.0	96.5	1.28	

	1	eference to	Head (raw)	samples	Geoph	ysical lo	g interpret	tation				Sample	e charac	cterisation			Head r	aw anal	ysis (air d	ried bas	is unles	s otherwis	se stated)		
Borehole		Composite	Rirtley Jah	Sample			De	pth		Dep	th	Thick	ness		Core recovery		Proxi	mate an	alysis			Addition	nal analysi	S	Comments
	no.	no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	(percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-07C			186876	4592	C DC	A3	161.28 161.48	161.48 161.75	A3	161.30	161.75	0.45	0.41	Coal	22.2%	1.48	0.66	23.43	17.67	58.24	0.69	4.0	98.3	1.49	
					CR		162.45	162.65																	
WC18-07C			186877	4593	С	A1	162.65	162.9	A1	162.50	163.10	0.60	0.54	Coal	33.3%	1.39	0.63	13.96	17.82	67.59	0.74	2.5	98.3	1.39	
					CR		162.9	163.1																	
MO40 070			400070	4504	CR	none	163.9	164.2	40	402.00	101 20	0.40	0.00	0	00.00/	4.05	0.54	44.05	10.10	CE 45	0.05	7.5	07.4	1 10	
WC18-07C			186878	4594	DC	A0	164.2	164.3	A0	163.90	164.30	0.40	0.36	Coal	20.0%	1.25	0.54	14.85	19.16	65.45	0.85	7.5	97.1	1.40	
					CBSH	310?	2.9	3.55	310?																
WC18-08C			186879	4595	DC	300	17.65	18.05	300	17.65	18.05	0.40	0.39	Coal	55.0%	1.60	0.50	8.46	23.75	67.29	0.80	7.0	92.5	1.35	
					CBSH	320	21.05	21.45	320																
WC18-08C					CBSH		24.1	24.6		24.10	24.70	0.60	0.57	Coaly mudstone	30.0%										
VVC 10-00C					CR		24.6	24.7		24.10	24.70	0.00	0.57	Coary muustone	30.0%										
					CBSH	340	24.7	24.95	340																
					R		24.95	25.4																	
					CBSH		25.4	26.1																	
WC18-08C			188208	4962	CR	410	46.70	47.10	410					Coaly mudstone	37.5%	1.09	0.51	15.49		64.43		3.0	98.8	1.42	
WC18-08C	-		186880	4596	С	401	48.50	49.10	401	48.50		0.60			16.7%	3.29	0.67	26.73	16.16	56.44	0.45	0.0	96.5	1.53	
WC18-08C	-				Fault	Estab.	49.10	49.20	Fault	49.10	49.20	0.10	0.10	Not recovered	0.0%					ļ					
WC18-08C			188209	4963	CBSH	none	49.30	49.55		49.30	49.55	0.25	0.25	Coaly mudstone	28.0%	2.08	0.67	37.81	13.77	47.75	0.66	0.5	99.7	1.69	Carbonaceous shale to coaly mudstone above the coal of 401
					DC	401	49.55	49.6																	
			,,,,,,		C		49.6	50.75							20.404						<b> </b>				
WC18-08C			186881	4597	Fault	Estab.	50.75	50.85	401	49.55	52.20	2.65	2.60	Coal	80.4%	6.77	0.69	6.81	19.10	73.40	0.44	1.0	96.0	1.35	
					DC	401	50.85	50.9																	
	-				DC		50.9	52.2												-					Consoled as leaved as al
WC18-08C			186882	4598		400	52.2 52.70	52.7 54.80	400	52.20	54.80	2.60	2.55	Coal	102.7%	4.13	0.42	13.23	19.42	66.93	0.38	4.0	96.8	1.37	Sampled as logged, coal recovered 2.67m
	<del>                                     </del>				Fault	Prob.	54.80	55.10	Fault											-		<del>                                     </del>	<del>                                     </del>	<del>                                     </del>	100070100 2.07111
WC18-08C	<del>                                     </del>		186883	4599	C	420		56.10	420	55.65	56.10	0.45	0.45	Coal	51.1%	4.36	0.37	14.31	19.67	65.65	0.45	6.0	95.7	1.40	
WC18-08C	<u> </u>		186884	4600	C	440	58.85	59.50	440	58.85					78.5%	3.73		9.05					96.2	1.36	
					CBSH	442	60.90	61.30	442											<u> </u>	<u> </u>	1	1	1	
WC18-08C					DC	460	76.10	76.50	460	76.10	76.50	0.40	0.37	Not recovered	0.0%										
					DC		86.20	86.50																	
WC18-08C			186885	4601	С	480	86.50	86.90	480	86.20	87.10	0.90	0.89	Dirty coal	45.6%	1.40	0.30	21.28	27.66	50.76	0.73	5.5	96.0	1.55	
					DC		86.90	87.10																	
WC18-08C			188210	4964	DC	A71	92.87	93.30	A71	92.87					65.1%	1.66		26.68					99.7	1.50	
WC18-08C			186886	4602	С	A7	94.55	95.18	A7	94.55	95.18	0.63	0.63	Coal	61.9%	3.25	0.44	14.14	18.50	66.92	0.81	3.5	94.0	1.41	

	Cross-refe		Head (raw)	samples	Geoph	ysical lo	g interpre	tation				Sample	e charac	eterisation			Head r	aw anal	ysis (air d	ried bas	is unles	s otherwis	se stated)		
Borehole	Dirtley Joh	Composito	Dietlovilob	Comple			De	pth		Dep	oth	Thick	kness		Core		Proxi	mate an	alysis			Addition	nal analysi	s	Comments
	no.	no.	Birtley lab no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-08C					CR	none	95.18	95.40		95.18	95.40	0.22	0.22	Mudstone with coal spars	72.7%										
WC18-09C					DC	111	2.00	2.35	111	2.00	2.55	0.55		Not recovered	0.0%										Inside casing - not recovered
WC18-09C			188211	4965	C	110	3.70	4.00	110	3.50	4.00	0.50			8.0%	1.89	0.71	9.78	21.58	67.93	0.79	2.0	66.4	1.39	
					CR	none	9.80	10.00																	
WC19 00C			100007	4600	С	101	10.00	10.55	101/100	0.00	10.05	0.05	2 22	Cool	F0.60/	2.45	0.40	C OF	00.76	60.04	0.54	F 0	00.0	4 22	Does not look like any coaly rock
WC18-09C			186887	4603	С	100	10.55	11.95	101/100	9.80	12.05	2.25	2.23	Coai	59.6%	3.15	0.48	6.95	22.76	69.81	0.54	5.0	92.3	1.33	was taken with the sample
					DC	100	11.95	12.05																	
WC18-09C					CR	none	15.30	15.40		15.30	15.40	0.10	0.10	Coal	30.0%										
					DC		15.50	15.60																	
WC18-09C			186888	4604	CR	201	15.60	15.70	201	15.50	16.95	1.45	1.36	Coal	4.8%	2.02	0.77	46.14	15.04	38.05	0.35	n/a	n/a	1.80	Very poor recovery, just a few
WC10-03C			100000	4004	DC	] 201	15.70	15.98	201	15.50	10.55	1.43	1.50	Coai	7.070	2.02	0.77	40.14	13.04	30.03	0.00	11/4	11/4	1.00	chunks of coal.
					С		15.98	16.95																	
					С	]	20.90	21.10																	
WC18-09C			186889	4605	CR		21.10	21.30		20.90	21.40	0.50	0.49	Coal	96.0%	2.43	0.61	5.63	20.50	73.26	0.71	3.5	97.1	1.33	All coal no rock
					DC	202	21.30	21.40	202																
WC18-09C			186890	4606	CR	202	21.40	21.55	202	21.40	21.55	0.15	0.15	Siltstone (sandstone in log)	100.0%	1.53	0.58	84.82	12.94	1.66	0.03	n/a	n/a	2.51	
WC18-09C			186891	4607	С		21.55	21.70		21.55	21.70	0.15	0.15	Coal	160.0%	2.56	0.49	9.62	23.13	66.76	0.75	8.0	94.8	1.34	Thickness measured in core box was 24cm
					CBSH	] [	30.80	31.20																	
					ASH	310	31.20	31.30	310																
					CBSH		31.30	31.40																	
WC18-09C					С	300	37.30	37.60	300	37.30	37.60	0.30	0.29	Coal	33.3%										
					CR	320	40.80	41.00	320																
					CBSH		41.00	41.30							-								<u> </u>		
					CBSH	- ,,,	43.75	44.50	0.40																
					R CBSH	340	44.50	45.20 45.65	340																
					CBSH	360	45.20 50.15		360						1								1		
					CBSH	430	65.55	50.50 66.00	430																
WC18-09C			186892	4608	С	410	67.60	68.15	410	67.40	69 15	0.75	0.74	Cool	89.3%	2.01	0.63	7.04	18.39	72 04	0.56	0.5	99.4	1.35	
VVC 10-09C			100032	4000	DC		68.65	68.80	410	07.40	00.13	0.73	0.74	Coai	09.570		0.03	7.04	10.59			0.5	33.4	1.33	
WC18-09C			186893	4609	C	401	68.80	69.97	401	68.65	69.97	1.32	1.31	Dirty coal / coal	56.8%	2.02	0.56	4.61	19.97	74.86	0.41	2.0	98.3	1.32	
					DC		69.97	70.02																	
WC18-09C			186894	4610	С	400	70.02	71.30	400	69.97	71.50	1.53	1.52	Dirty coal / coal	45.1%	6.77	0.59	9.64	20.62	69.15	0.39	4.0	98.8	1.37	
					DC	1	71.30	71.50																	
WC18-09C			188212	4966	DC	420	72.30	72.60	420	72.30					10.0%	1.74			18.65				98.8	1.41	
WC18-09C			188213	4967	CR	none	72.60	72.80	420	72.60	72.80	0.20	0.20	Ash parting / coal	90.0%	1.57	0.50	32.37	19.98	47.15	0.37	8.0	99.4	1.56	

WC18-10C   187341   4618   C   101   20.30   21.09   101   20.30   21.09   0.79   0.78   Coal   75.9%   2.10   0.84   9.32   20.18   69.66   0.45   1.5   98.3   1.35	
MC18-09C   MC18-09C	ents
WC18-09C   187334   4611   2	
MC18-0PC   MC18-0PC	
$ \begin{tabular}{ c c c c c c c c c c c c c c c c c c c$	
WC18-19C   WC18-19C	
Note	
C	
CBSH   442   78.30   78.70   442   461   460	
CBSH   463   83.20   83.70   463   460   79.5   88.40   460   46.40	
MC18-09C   187335   4612   C	
WC18-09C   187335   4612   C   DC   DC   DC   DC   DC   DC   DC	
WC18-09C   B7335   4612   DC   480   100.65   100.90   100.05   100.00   100.90   0.90   0.80   0.	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	
WC18-10C   187337   4614   C   7.10   7.20   7.30   7.45   1.020   7.30   7.45   1.020   7.45   7.65   7.80   7.80   7.80   7.85   7.80   7.	
WC18-10C         187337         4614         C         7.10         7.20         7.09         7.20         0.11         Coal         100.0%         3.46         1.23         5.64         23.31         69.82         1.21         1.5         65.6         1.33           WC18-10C         187338         4615         CR         150         7.30         7.45         7.20         7.30         7.45         7.20         7.30         7.45         7.20         7.30         7.45         7.50         7.45         7.80         0.35         0.34         Not recovered         0.0%         1.17         0.75         69.62         15.62         14.01         0.22         n/a         n/a         2.09           WC18-10C         CR         CR         7.45         7.65         7.80         0.35         0.34         Not recovered         0.0%         0.0%         35.12         18.92         45.00         0.69         1.5         74.7         1.57           WC18-10C         CBSH         110         15.95         16.10         111         15.95         18.10         111         15.95         18.10         111         15.95         18.10         111         17.35         17.70         110	
WC18-10C         187338         4615         CR         7.20         7.30         7.20         7.30         0.10         0.10         Coaly mudstone         40.0%         1.17         0.75         69.62         15.62         14.01         0.22         n/a         n/a         2.09           WC18-10C         187339         4616         C         7.45         7.65         7.65         7.80         7.45         7.80         7.45         7.80         7.45         7.80         0.35         0.34         Not recovered         0.0%         0.0%         0.06         35.12         18.92         45.00         0.69         1.5         74.7         1.57         1.57         1.57         1.57         1.57         1.57         1.57         1.57         1.57         1.57         1.57         1.57         1.57         1.59         1.11         1.595         16.10         1.11         1.595         16.10         1.11         1.595	
WC18-10C         187339         4616         C CR DC         150 T.45 T.65 T.65 T.80         T.45 T.80 T.80 T.80         T.45 T.80 T.80 T.80 T.80 T.80 T.80 T.80 T.80	
Not recovered   Not recovere	
Mathematical Column   Mathematical Column	,
CBSH   The control of the control	
R   111   15.95   16.10   111   16.00   16.60	
WC18-10C         187340         4618         C         101         20.30         21.09         101         20.30         21.09         21.14         20.30         21.14         23.10         100         21.14         23.10         20.30         21.09         23.14         20.5         20.31         Coal         71.2%         1.60         0.84         3.45         22.90         72.81         0.44         7.0         98.6         1.29	
WC18-10C         187340         4617         C         110         17.35         17.70         110         17.35         17.70         0.35         0.35         Coal         105.7%         2.39         0.69         7.52         21.74         70.05         0.75         4.5         96.5         1.33           WC18-10C         187341         4618         C         101         20.30         21.09         101         20.30         21.09         0.79         0.78         Coal         75.9%         2.10         0.84         9.32         20.18         69.66         0.45         1.5         98.3         1.35         It was discoal con           WC18-10C         187342         4619         DC         100         21.09         21.14         2.05         2.03         Coal         71.2%         1.60         0.84         3.45         22.90         72.81         0.44         7.0         98.6         1.29	
WC18-10C	
WC18-10C	difficult to find 5cm dirty
WC18-10C 187342 4619 C 100 21.14 23.10 100 21.09 23.14 2.05 2.03 Coal 71.2% 1.60 0.84 3.45 22.90 72.81 0.44 7.0 98.6 1.29	
C 21.14   23.10	
WC18-10C   187343   4620   C   201   27.50   28.10   28.25   201   27.50   28.26   0.76   0.75   Coal   100.0%   1.65   0.54   11.57   22.38   65.51   0.70   7.5   98.0   1.36	
WC18-10C 1873/4 /621 C 30.95 31.10 30.95 31.40 0.45 0.43 Coal 80.0% 1.64 0.69 7.18 20.56 71.57 0.66 3.0 98.6 1.35	
DC 202 31.10 31.40 202	
WC18-10C         187345         4622         CR         202         31.40         31.50         202         31.40         31.50         31.50         31.50         31.50         31.50         31.50         31.50         31.50         31.50         31.50         31.50         31.50         31.50         31.50         31.50         31.60         0.15         Coal         100.0%         1.75         0.78         17.83         22.13         59.26         0.64         7.5         98.3         1.47	
WC18-10C	
WC18-10C DC 320 47.95 48.40 320 47.95 48.40 0.45 Carb. mudstone 100.0% 1.80 0.08 28.19 18.05 53.08 0.48 1.5 98.8 1.50	

	Cross-reference composites	Head (rav	v) samples	Geoph	ysical lo	g interpret	tation				Sample	e charac	cterisation			Head r	aw anal	ysis (air d	ried bas	sis unles	s otherwi	se stated)		
Borehole	i i	ita Diatlas Ial	0			De	pth		Dep	oth	Thick	ness		Core		Proxi	mate an	alysis			Addition	nal analysi	s	Comments
	Birtley lab Compo no. no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
				CBSH		51.05	51.80		, ,	<u> </u>														
WC18-10C				R	340	51.80	52.50	340																
				CBSH	1 1	52.50	53.20																	
WC18-10C				CBSH	430	73.60	73.75	430																
WC18-10C				CBSH	410	76.18	76.23	410																
				CR	none	76.40	76.68																	Coal is broken into chunks down
				С	401	76.68	78.48																	to powder, impossible to discern
WC18-10C		187348	4625	DC		78.48	78.53	401/400	76.40	81.08	4.68	4.59	Coal	15.0%	6.39	0.91	10.99	19.28	68.82	0.37	2.0	97.4	1.38	401 from 400, therefore one
				С	400	78.53	81.08																	sample. Does not look like any coaly rock was taken.
WC18-10C		188214	4968	CR	420	83.80	84.25	420	83.80	84.25	0.45	0.41	Coal	26.7%	6.47	0.60	54.18	14.56	30.66	0.28			1.84	
				С	]	86.40	86.75																	
WC18-10C		187349	4626	DC	440	86.75	86.90	440	86.34	87.31	0.97	0.89	Stony coal, mudstone,	100.0%	2.65	0.84	15.77	18.65	64.74	0.55	3.0	98.3	1.41	
WO10 100		107043	1020	С	]	86.90	87.05	110	00.04	07.01	0.57	0.00	coal, ash band, coal	100.070	2.00	0.04	10.77	10.00	04.74	0.00	0.0	30.0	1	
				DC		87.05	87.25																	
				CBSH	442	88.70	89.20	442												ļ				
				CBSH	463	93.15	93.55	463																
				CBSH	460	97.50	98.00	460																
WC18-10C		187350	4627	DC DC	480	109.15 109.95	109.95 110.10	480	109.15	110.10	0.95	0.88	Coal	33.7%	1.34	0.73	31.79	22.275	44.73	0.90	4.5	98.8	1.61	
WC18-10C				С	A71	116.85	117.00	A71	116.85	117.00	0.15	0.14	Coal	80.0%										
WC18-10C		187351	4628	С	A7	117.85	118.40	A7		118.60				92.0%	2.54	0.85	11.00	19.25	68.90	0.84	7.0	99.1	1.35	
WC 10-10C		107331	4020	DC	] A/	118.40	118.60	A	117.00	1110.00	0.75	0.70	Coal, dirty coal, coal	92.0%	2.54	0.00	11.00	19.25	00.90	0.04	7.0	99.1	1.35	
WC18-10C		187352	4629	С	A5	137.40	138.15	A5	137.40	138.15	0.75	0.70	Coal	42.7%	0.93	0.46	14.29	17.01	68.24	0.73	1.5	99.1	1.41	
WC18-10C				CR	none	142.80	143.05		142.80	143.05	0.25	0.25	Carb mudstone	88.0%										
				С		143.05	143.20																	No analysis and into the
WC18-10C		187535	4630	DC	A3	143.20	143.30	A3	143.05	143 60	0.55	0.54	Cool	54.5%	1.84	0.55	17.47	17.15	64.83	0.69	2.0	99.4	1.42	No coaly rock was put into the bag - depths should be shortened
WC 10-10C		107333	4030	С		143.30	143.40	AS	143.03	143.00	0.55	0.54	Coai	34.5%	1.04	0.55	17.47	17.15	04.03	0.09	2.0	99.4	1.42	to reflect this.
				CR	none	143.40	143.60																	to renect this.
WC18-10C				С	A1	144.20	144.40	A1	144.20	144.40	0.20	0.20		90.0%										
WC18-10C		187354	4631	CR	A0	145.45	145.90	A0	145.45	145.90	0.45	0.44	Coal, dirty coal with ash?, coal	40.0%	1.42	0.49	35.71	15.19	48.61	0.79	2.5	99.4	1.59	
WO40 400		407055	4000	DC	500	165.40	165.60	500	405.40	405.00	0.40	0.00		20.50/	4.00	0.44	0.05	04.44	00.00	4.04		000	4.00	
WC18-10C		187355	4632	С	530	165.60	165.80	530	165.40	165.80	0.40	0.39	Coal	32.5%	1.20	0.44	9.35	21.41	68.80	1.31	9.0	98.8	1.36	
				CBSH	510	166.80	167.20	510																

	Cross-refe		Head (raw)	samples	Geoph	ysical lo	g interpret	tation				Sample	e chara	cterisation			Head ı	aw anal	ysis (air d	ried bas	sis unles	s otherwis	se stated)		
Borehole	Birtley lab	Composito	Dirtloy Joh	Sample			De	pth		Dep	oth	Thic	kness		Core recovery		Proxi	mate an	alysis			Addition	al analysi	S	Comments
	no.	no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	(percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-10C			187356	4633	С	501	168.95	169.80	501	168.95	169.80	0.85	0.82	Coal	70.6%	1.74	0.54	4.12	16.79	78.55	0.74	2.0	99.4	1.33	
WC18-10C			188215	4969	С	502	170.60	171.05	502	170.60	171.05	0.45	0.45	Coal	8.9%	2.09	0.37	16.36	15.45	67.82	0.75	0.5	99.1	1.43	Rounded, ground out coal - very bad recovery and hard to separate the coal from the carb. mudstone and surrounding rock. Not a representative sample.
	$\downarrow \qquad \downarrow$				CBSH	520	174.40	174.80	520																
WC18-10C	-		188216	4970	CR	none	176.95	177.15	F40					Coaly mudstone	40.0%	1.61	0.49	51.96	10.78	36.77				1.81	
WC18-10C	+		187357	4634	C	540 630	177.15 189.70	177.40 189.90	540	177.15	177.40	0.25	0.25	Coal	68.0%	6.56	0.41	6.96	17.71	74.91	0.92	2.5	98.3	1.34	
WC18-10C			187359	4636	CR	none	189.90	190.20	630	189.70				Coal	60.0%	2.52	0.40	17.93	16.74			2.5	97.1	1.42	
WC18-10C			187360	4637	DC	610	191.20	191.40	610	191.20	191.40	0.20	0.20	Coaly mudstone	25.0%	2.36	0.61	31.91	16.28	51.20	2.04	4.0	97.1	1.57	
WC18-10C			187361	4638	C DC	601	192.50 193.40	193.40 193.60	601	192.50	193.60	1.10	1.08	Coal	78.2%	2.54	0.83	3.38	16.95	78.84	0.66	0.5	98.3	1.33	
WC18-10C			187362	4639	CR	none 600	193.80 194.00	194.00 194.65	600	193.80	194.65	0.85	0.82	Coal	24.7%	4.16	0.76	26.09	13.24	59.91	0.58	0.5	98.3	1.33	
	+ +				CBSH	770	204.10	204.60	770						+			-		-		<del> </del>		-	
	+ +				CBSH	750	207.60	207.80	750									-		-		<u> </u>		1	
	+ +				CR	none	211.55															1			
WC18-10C			187358	4635	C	730	211.80	212.00	730	211.55	212.00	0.45	0.43	Coal	42.2%	1.40	0.37	14.97	16.38	68.28	0.96	3.0	98.3	1.41	
					CR	710	214.05	214.25	710																
WC18-11C					CR	none	15.20	15.40		15.20	15.30	0.10	0.10	Siltstone locally carb	100.0%										
WC18-11C			187363	4640	С	300	15.40	15.60	300	15.30	15.60	0.30	0.30	Coal	100.0%	1.57	0.51	14.79	19.02	65.68	0.82	4.5	97.4	1.41	Thickness adjusted: 20 to 30cm
WC18-11C					CR	none	15.60	15.80		15.60	15.80	0.20	0.20	Mudstone with coal lens	100.0%										
					CBSH	320	19.00	19.70	320																
					CBSH		22.15	23.05																	
					R	340	23.05	23.85	340																
	-				CBSH		23.85	24.65	- "													-			
14040 440	-				Fault	Poss.	28.55	28.65	Fault	40.70	40.05	0.05	0.04	0.1	C4 00/							-			
WC18-11C					CR Foult	430	43.70	43.95	430	43.70	43.95	0.25	0.24	Carb mudstone	64.0%										
WC18-11C	+		187364	4641	Fault C	Poss. 410	44.35 46.50	44.40 47.20	Fault 410	46.50	47.20	0.70	0.69	Coal	97.1%	1.77	0.84	6.23	18.60	7/ 22	0.59	0.5	98.8	1.32	
	+ +		107304	4041		410			410					Siltstone and		1.//	0.04	0.23	10.00	14.33	0.56	0.5	30.0	1.32	
WC18-11C					CR	none	48.15	48.40		48.15	48.40	0.25	0.24	carbonaceous rock	52.0%										
14040 440			407005	40.40	C		48.40	49.65	46.4	40.40	40.00		, , -		10.70		0.04	7.04	40.00	70.00			00.4	, , ,	
WC18-11C			187365	4642	DC	401	49.65	49.70	401	48.40	49.90	1.50	1.45	Coal	46.7%	2.26	0.81	7.21	18.92	73.06	0.38	1.0	99.1	1.30	
					С		49.70	49.90			<u> </u>						ļ								

		ference to	Head (raw)	samples	Geophy	ysical lo	g interpret	tation				Sample	e charac	cterisation			Head r	aw anal	ysis (air d	ried bas	is unles	s otherwis	se stated)		
Borehole	Dirtloy lob	Composite	Dirtloy Joh	Cample			De	pth		Dep	oth	Thick	kness		Core		Proxi	mate an	alysis			Addition	nal analysi	S	Comments
	no.	no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
					DC		49.90	49.95							<u> </u>										
WC10 11C			187366	4643	С	400	49.95	52.13	400	40.00	EO 40	2.50	2 45	Cool	EG 00/	2.42	0.60	2 52	24.25	75 15	0.20	4.0	97.1	1 20	
WC18-11C			107300	4043	DC	400	52.13	52.28	400	49.90	52.40	2.50	2.45	Coal	56.0%	2.42	0.68	2.52	21.35	75.45	0.39	4.0	97.1	1.28	
					С		52.28	52.40																	
					CR	none	52.40	52.50																	T
WC18-11C			188217	4971	DC		62.50	52.62	420	52.40	E2 0E	0.65	0.64	Carbonaceous mudstone	21.5%	2.91	0.52	68.58	13.08	17.82	0.12			2.07	Two partings (carbonaceous mudstone and ash layer) back to
WC10-11C			100217	4971	CR	420	52.62	52.80	420	32.40	33.03	0.05	0.04	and ash parting / coal	21.5%	2.91	0.52	00.30	13.00	17.02	0.12			2.07	back.
					DC		52.80	52.95																	back.
					С		55.42	55.60																	
					DC		55.60	55.85																	
WC18-11C			187367	4644	С	440	55.85	56.00	440	55.42	56.30	0.88	0.88	Coal, ash band, coal	46.6%	0.94	0.49	5.37	23.34	70.80	1.16	8.5	98.3	1.29	5cm ash band parting
					DC		56.00	56.10																	
					С		56.10	56.30																	
					CBSH	442	58.15	58.65	442																
					CBSH	463	66.25	66.85	463																
WC18-11C					CR	460	70.75	70.90	460	70.75				Jarosite	33.3%										
WC18-11C					DC		70.90	71.02		70.90	71.02	0.12	0.12	Coal	33.3%										
					CBSH	483	78.95	79.32	483																
WC18-11C			187368	4645	DC	480	82.15 82.80	82.80 83.00	480	82.15	83.00	0.85	0.81	Coal	8.2%	1.75	0.62	29.80	28.05	41.53	0.75	3.5	98.0	1.62	Dirty sample due to crushed coal with mixed mudstone
WC18-11C			187369	4646	DC	A71	88.30	88.60	A71	88.30	88.60	0.30	0.29	Coal	60.0%	1.39	0.66	25.01	16.65	57.68	0.51	1.0	98.6	1.50	
WC18-11C					CR	none	89.70	89.98		89.70		0.28		Carb mudstone	32.1%										
			407070	10.17	С		89.98	90.65						İ	1	4.04		20.00	04.00			1.0	00.4	4.54	
WC18-11C			187370	4647	DC	A7	90.65	90.90	A7	89.98	90.90	0.92	0.79	Coal	8.7%	1.81	0.62	32.90	21.93	44.55	0.69	4.0	99.4	1.54	
WC18-11C					CR		98.80	99.10		98.80	99.10	0.30	0.29	0111	100.0%										
WC18-11C					DC	A5	99.10	99.20	A5	99.10		0.10		Siltstone with coal spars	100.0%										
					CBSH	170	16.45	16.80	170																
WC18-12C					CR	none	21.60	21.70		21.60	21.70	0.10	0.07	Muddy siltstone	100.0%										
					DC		21.70	21.90						<u> </u>						İ					
					С	1	21.90	22.10																	
WC18-12C			187371	4648	DC	150	22.10	22.22	150	21.70	22.80	1.10	0.74	Coal	88.2%	3.72	1.32	26.56	21.93	50.19	0.76	0.5	97.7	1.50	
					C		22.22	22.60																	
					DC		22.60	22.80																	
WC18-12C					DC	400	29.08	29.20	400	29.08	29.20	0.12	0.08	Not recovered	0.0%										
WC18-12C					CR	130	29.20	29.45	130					Mudstone with coal spars	100.0%								İ		

Depth   Birtley lab   Composite   Birtley lab   no.   Depth   no.   De	
No.   No.	Comments
WC18-12C   187373   4650   CR   111   35.30   35.50	
WC18-12C   187374   4651   DC   35.50   35.92   35.50   35.92   35.50   35.92   0.42   0.38   Coal   88.1%   1.71   0.64   13.82   25.45   60.09   0.88   5.0   9.74   1.43	
WC18-12C         187375         4652         C         110         37.25         37.50         110         37.25         37.50         110         37.25         37.90         0.65         0.50         Coal         36.9%         1.99         0.63         2.97         24.08         72.32         0.73         8.0         97.4         1.26           WC18-12C         187376         4653         DC         101         39.80         40.18         101         139.80         41.10         1.30         1.06         Coal         100.0%         1.59         0.52         11.46         20.65         67.37         0.41         2.0         97.7         1.34           WC18-12C         187377         4654         C         100         41.10         44.80         45.05         0.25         0.22         Carbonaceous mudstone         60.0%         1.59         0.52         11.46         20.65         67.37         0.41         2.0         97.7         1.34           WC18-12C         187378         4655         C         201         53.20         54.30         201         53.00         54.60         1.60         1.13         Coal         23.8%         2.87         0.47         9.02         22	
WC18-12C   187375   4652   C   DC   DC   37.50   37.90   37.	
WC18-12C   187376   4654   C   101   39.80   41.10   101   39.80   41.10   1.30   1.06   Coal   100.0%   1.59   0.52   11.46   20.65   67.37   0.41   2.0   97.7   1.34	
WC18-12C         187376         4653         DC C C C No. 101         101 39.80 40.18 40.18 40.10	
WC18-12C   187376   4654   C   100   41.10   44.80   100   41.10   44.80   3.70   3.24   Coal   80.3%   1.59   0.57   2.72   24.44   72.27   0.42   8.0   97.7   1.35	
WC18-12C         187377         4654         C         40.18         41.10         44.80         3.70         3.24         Coal         80.3%         1.59         0.57         2.72         24.44         72.27         0.42         8.0         97.7         1.25           WC18-12C         187378         4655         C         201         53.00         53.20         54.30         54.30         54.30         54.60         1.60         1.13         Coal         23.8%         2.87         0.47         9.02         22.57         67.94         0.71         7.0         97.7         1.30           WC18-12C         187389         4656         C         201         56.40         56.60         57.10         57.35         57.55         57.55         57.50         57.10         57.55         57.50         57.55         57.90         57.55         57.90         57.55         57.90         57.55         57.90         330         20.2         57.10         57.55         57.90         57.55         57.90         330         20.2         57.10         57.55         57.90         330         20.2         57.55         57.90         330         20.2         20.2         57.10         57.55         57.	5cm parting of coaly rock sample
WC18-12C         CR         none         44.80         45.05         0.25         0.22         Carbonaceous mudstone         60.0%         0.0% <th< td=""><td>in 4653</td></th<>	in 4653
WC18-12C         187378         4655         C C DC         201 53.20 54.30 54.60 54.60         201 53.00 54.60 1.60 1.13 Coal         23.8% 2.87 0.47 9.02 22.57 67.94 0.71 7.0 97.7 1.30           WC18-12C         187379 4656 C DC GC ACT COAL COAL COAL COAL COAL COAL COAL COAL	
WC18-12C         187378         4655         C DC         201         53.20         54.30 54.60         201         53.00 54.60         1.60 1.13 Coal         23.8% 2.87 0.47 9.02 22.57 67.94 0.71 7.0 97.7 1.0 97.7 1.30         70.0 97.7 1.30         1.30           WC18-12C         187379 4656 CR         DC CR CR         56.40 56.60 57.10 57.35 57.55 57.95 57.55 57.90         56.40 57.10 57.55 57.90         57.10 57.55 57.90 0.35 0.45 0.39 Ash         35.6% 1.89 0.71 80.10 12.90 6.29 0.63 2.31         4.33 0.62 70 6.29 0.63 2.31           WC18-12C         187381 4658 C         CBSH 330 62.70 62.90 330 57.55 57.90 57.55 57.90 57.55 57.90 57.55 57.90 0.35 0.31 Coal         57.55 57.90 0.35 0.31 Coal         85.7% 1.40 0.51 6.77 25.41 67.31 0.80 8.0 97.1 1.31           WC18-12C         188218 4972 DC         4972 DC         340 71.15 71.50 71.50 71.50 71.50 71.50 71.50 71.50 71.50 71.50 0.35 0.24 Dirty coal         14.3% 1.03 0.35 25.91 10.43 54.31 0.69 6.5 98.0 1.47	
WC18-12C   187379   4656   DC   56.40   56.60   57.10   57.35   57.55   57.90   57.55   57.9	
WC18-12C         187379         4656         DC C C S6.60         56.40         56.40 57.10 57.35 57.55         57.10 57.35 57.55         57.55 57.90         57.55 57.90         56.40 57.10 57.35 57.55         57.55 57.90<	
WC18-12C         187389         4650 CR         C         56.60 57.10 57.35 57.55         202 57.10 57.55 57.90         57.10 57.55 57.90         57.55 57.90	
WC18-12C         187380         4657         R CR         202 57.10 57.35 57.55         57.55 57.90         57.55	
WC18-12C         187380         4657         CR         57.35         57.55         57.55         57.55         57.55         57.50         57.55         57.50         57.55         57.50         57.55         57.90         0.35         0.31         Coal         85.7%         1.40         0.51         6.77         25.41         67.31         0.80         8.0         97.1         1.31           WC18-12C         Fault Poss.         62.90         63.00         Fault Fault Poss.         62.90         63.00         Fault Fault Poss.         62.90         63.00         Fault Poss.         62.90         63.75         330         68.75         330         68.75         330         68.75         330         68.75         330         68.75         330         71.15         71.50         0.35         0.24         Dirty coal         14.3%         1.03         0.35         25.91         10.43         54.31         0.69         6.5         98.0         1.47	
WC18-12C         187381         4658         C         57.55         57.90         57.55         57.90         0.35         0.31         Coal         85.7%         1.40         0.51         6.77         25.41         67.31         0.80         8.0         97.1         1.31           CBSH         330         62.70         62.90         330         8.00         Fault         85.7%         1.40         0.51         6.77         25.41         67.31         0.80         8.0         97.1         1.31           Fault         Poss.         62.90         63.00         Fault         85.7%         1.40         0.51         6.77         25.41         67.31         0.80         8.0         97.1         1.31           CBSH         330         68.50         68.75         330         80         80         80         80         97.1         1.31           WC18-12C         188218         4972         DC         310         71.15         71.50         0.35         0.24         Dirty coal         14.3%         1.03         0.35         25.91         10.43         54.31         0.69         6.5         98.0         1.47	
CBSH         330         62.70         62.90         330         9	
Fault   Poss.   62.90   63.00   Fault	<u> </u>
WC18-12C         188218         4972         DC         310         68.50         68.75         330         71.15         71.50         0.35         0.24         Dirty coal         14.3%         1.03         0.35         25.91         10.43         54.31         0.69         6.5         98.0         1.47	
WC18-12C 188218 4972 DC 310 71.15 71.50 310 71.15 71.50 0.35 0.24 Dirty coal 14.3% 1.03 0.35 25.91 10.43 54.31 0.69 6.5 98.0 1.47	
1.4004014001 $1.400040140791700173717460174661737174601746610461046104610461046104610001106106106160671496610071496610001114060610461046104610461046104610$	
WC18-12C	
WC48 43C	
WC18-12C   187382   4659   C   300   74.13   74.53   300   73.90   75.12   1.22   0.80   Coal/Dirty coal   65.6%   3.05   0.56   23.96   18.18   57.30   0.53   1.0   98.8   1.46	
C 74.00 74.00 75.12	
WC18-12C	+
WC16-12C 187363 4000 C 320 79.80 80.28 320 79.80 80.28 0.48 0.31 C0al 79.2% 2.44 0.47 7.91 19.30 72.00 0.74 2.0 98.8 1.33	+
CR 85.80 85.90	
CBSH 85.90 86.15	
CR 86.15 86.30	
CBSH 340 86.30 86.55 340	
R 86.55 87.45	
CBSH 87.45 88.00	
R 88.00 88.15	
CBSH 88.15 88.35	

	Cross-ref	erence to osites	Head (raw)	samples	Geophy	ysical lo	g interpret	tation				Sample	e charac	terisation			Head r	aw analy	/sis (air d	ried bas	is unles	s otherwis	se stated)		
Borehole	Pirtlov lah	Composito	Birtley lab	Cample			De	pth		Dep	oth	Thick	kness		Core		Proxi	mate an	alysis			Addition	nal analysi	S	Comments
	no.	no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery - (percent )	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-12C					DC	410	118.85	119.20	410	118.85	119.20				48.6%										
WC18-12C					CR	none	120.00	120.20		120.00	120.20		-	Mudstone	100.0%							ļ			
WC18-12C			187384	4661	С	401	120.20	121.85	401	120.20	121.85			Dirty coal	14.5%	1.62	0.64	22.17		55.12		2.0	98.6	1.48	
WC18-12C			187385	4662	С	400	121.85	123.70	400	121.85	123.70	1.85	1.31	Coal	20.0%	5.11	0.60	18.46	19.82	61.12	0.40	4.0	98.6	1.40	
WC18-12C					CR	none	123.70	124.00			124.00			Carbonaceous muddy siltstone	33.3%										
WC18-12C					С	420	125.50	125.75	420	125.50	125.75	0.25	0.18	Coal with ash parting	44.0%							ļ			
					DC		127.22	127.34																	
WC18-12C			187386	4663	С		127.34	127.80		127.22	128 20	0.98	0.69	Coal	90.8%	2.07	0.74	14.59	18.45	66.22	0.59	2.0	98.8	1.38	
17010120			101000	1000	DC	440	127.80	127.90	440	127.22	120.20	0.00	0.00	- Codi	00.070	2.01	0.7	11.00	10.10	00.22	0.00	2.0	00.0	1.00	
					С	'''	127.90	128.20																	
WC18-12C			187387	4664	CR		128.20	128.38		128.20					83.3%	1.27		80.58	12.08	6.82		-	-	2.37	
WC18-12C			187388	4665	С		128.38	128.70		128.38	128.70	0.32	0.23	Coal	12.5%	1.34	0.63	41.46	15.40	42.51	0.41	-	-	1.64	
11/0/0 /00					CR	442	131.56	131.75	442	100.00	400.00	2.12			10 -0/							-		-	
WC18-12C					CR	100	132.80	133.20		132.80	133.20	0.40	0.30	Coal	12.5%									-	
14/040 400					CBSH	463	136.60	137.00	463	440.40	440.70	0.00	0.05	D: (	00.70/							-		-	
WC18-12C					DC	460	143.40	143.70	460	143.40	143.70	0.30	0.25	Dirty coal	36.7%							-		-	
14/040 400					CBSH	483	150.32	150.50	483	450.00	450.05	0.45	0.40	0.31	400.00/										
WC18-12C					CR	none	159.20	159.35		159.20	159.35	0.15	0.10	Silty mudstone	100.0%							-		-	
					OPOLL		159.35	159.60																	
WC18-12C			187389	4666	CBSH DC	480	159.60	159.75 159.95	480	159.35	160.70	1.35	0.90	Coal, Coaly mudstone, Dirty coal	68.9%	3.00	0.46	19.51	28.22	51.81	0.86	7.5	98.6	1.47	
					С		159.75 159.95	160.70						Dirty coal											
WC18-12C					DC	A71	175.45	175.80	A71	175 15	175 00	0.25	0.24	Coal/Dirty coal	31.4%										
WC 10-12C					С	A/I	177.25	178.30	A/I						31.4%					-		1			
WC18-12C			187390	4667	DC	A7	177.23	178.50	A7	177.25	178.50	1.25	0.84	Coal/Coaly mudstone	13.6%	1.29	0.51	20.17	17.45	61.87	0.79	2.5	99.1	1.43	
	<del>                                     </del>				CBSH	$\vdash$	186.70	187.60		-			<del>                                     </del>		+		<del>                                     </del>	$\vdash$		<del>                                     </del>	<del>                                     </del>	+	<del> </del>	+	
					CR	A5	187.60	187.90	A5	1										<del>                                     </del>	<del>                                     </del>	<del> </del>	1	<del> </del>	-
					CBSH	,	187.90	188.10	, 10	1												1	<u> </u>	1	-
WC18-12C					DC	A3	193.95		A3	193.95	194 30	0.35	0.23	Coal	45.7%							1		1	
1.0.0 120					CBSH	A1	195.30		A1	100.00	10 1.00	0.00	1		10.770							1		1	
					DC	, , ,	3.00	3.15	, , ,																
					C		3.15	3.65		1															
					CR		3.65	3.80		1															
WC18-13C			187391	4668	C	150	3.80	3.95	150	3.00	4.60	1.60	1.07	Coal	31.3%	8.53	3.37	25,57	22.52	48.54	0.76	0.5	9.4	1.55	
					DC	.50	3.95	4.10	. 30	3.00				1		2.50	5.5.					5.0			
					C		4.10	4.30		1															
					DC		4.30	4.60		1															

	Cross-reference to composites	Head (raw	) samples	Geoph	ysical lo	g interpre	tation				Sample	e charac	cterisation			Head r	aw anal	ysis (air d	ried bas	is unles	s otherwis	se stated)		
Borehole	Didley lab Companie	Dietlass Jak	0			De	pth		Dep	oth	Thic	kness		Core		Proxi	mate an	alysis			Addition	al analysi	S	Comments
	Birtley lab Composite no. no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-13C				CR	none	4.60	4.85		4.60	4.85	0.25	0.17	Not recovered	0.0%									ĺ	
WC18-13C				CR	none	5.85	6.20		5.85	6.20	0.35	0.23	Powdered mudstone	37.1%										
WC18-13C				CR	none	6.35	6.80		6.35	6.80	0.45		Muddy siltstone	31.1%										
WC18-13C				DC	none	6.80	7.10		6.80	7.10	0.30	0.20	Not recovered	0.0%										
WC18-13C		188220	4974	CR	130	11.32	11.80	130	11.32	11.80	0.48	0.32	Powdered mudstone and coal	41.7%	5.35	0.77	64.67	11.77	22.79	0.42			1.97	Bad recovery with mudstone contamination - hard to separate
		187392	4669	DC C		16.70 16.85	16.85 17.00		16.70	17.00	0.30	0.22	Coal	86.7%	1.74	0.66	7.59	26.23	65.52	0.87	7.0	85.8	1.33	17.00 to 17.20 picked as dirty coal, however core shows a small
WC18-13C		187393	4670	DC [R]	111	17.00	17.20	111	17.00	17.20	0.20		Sandy siltstone	80.0%	1.40		87.86	5.52	5.92	0.09	-	-	2.40	sandy siltstone [rock] interval separating the coals
		187394	4671	С		17.20	17.60		17.20	17.60	0.40			90.0%	1.51	0.54	10.96	25.43	63.07	0.80	7.5	97.1	1.40	
WC18-13C		187395	4672	С	110	19.45	20.20	110	19.45	20.20	0.75	0.47	Coal	14.7%	2.07	1.51	10.12	22.27	67.10	0.79	7.0	92.3	1.38	
WC18-13C		187396	4673	DC C	101	28.45 28.60	28.60 29.95	101	28.45	29.95	1.50	1.18	Coal	30.0%	2.75	1.05	18.20	19.63	71.12	0.50	1.5	99.1	1.35	
WC18-13C		187397	4674	C DC	100	29.95 32.65	32.65 32.90	100	29.95	32.90	2.95	2.32	Coal	57.6%	5.75	0.85	10.32	21.39	67.44	0.49	3.5	91.1	1.35	
WC18-13C		187398	4675	С	201	39.95	40.90	201	39.95	40.90	0.95	0.64	Coal/Coaly rock	33.7%	3.69	0.45	15.63	22.47	61.45	0.66	7.5	98.0	1.37	Carbonaceous mudstone on either side of the coal has been ground into small pieces and are hard to pick out of the crushed coal. A 1cm intact ash layer was bagged.
WC18-13C		187399	4676	DC C		46.90 47.00	47.00 47.40		46.90	47.40	0.50	0.38	Coal	96.0%	1.82	0.65	7.26	20.25	71.84	0.74	<mark>2.2</mark>	97.7	1.33	
WC18-13C		187400	4677	CBSH	202	47.40	47.60	202	47.40	47.60	0.20	0.15	Ash layer	85.0%	1.33	0.64	77.07	13.94	8.35	0.10	-	-	2.27	Carbonaceous shale> Ash layer.
WC18-13C		187401	4678	CR C		47.60 47.80	47.80 48.30		47.60	48.30	0.70	0.53	Coal	58.6%	1.75	0.61	9.90	23.43	66.06	0.81	9.0	98.3	1.32	
				CBSH	330	54.55	55.10	330																
				CBSH	310	58.00	58.55	310																
				CR	none	68.25	68.40																	The geophysical picks and the geo-
				С	4	68.40	68.62																	physical log display a ~50cm parting, labelled as carbonaceous shale and
				DC	1	68.62	68.85																	rock, with a small amount of coal on
				R	4	68.85	69.15																	either side. In the box there is
WC18-13C		187402	4679	CBSH	4	69.15	69.35	300	68.25	69 65	1 40	l n ga	Coal	64.3%	2.53	0.58	14 30	19.64	65.48	0.70	4.0	97.1	1.39	evidence that this parting of rock does not exist. The amount of coal (as
				С	300	69.35	69.65																	seen in photo and box) is a relatively intact broken stick and exceeds the predicted amount of coal. There is a small (9cm) ash layer uphole of the coal, followed by 90cm of broken stick coal, directly followed by rock.
WC18-13C		187403	4680	C	320	74.62	75.18	320	74.62	75.18	0.56	0.36	Coal, dirty coal	96.4%	1.47	0.57	19.56	18.93	60.94	0.86	4.5	98.3	1.42	

	1	ference to osites	Head (raw)	samples	Geoph	ysical lo	g interpret	tation				Sample	e chara	cterisation			Head r	aw anal	ysis (air d	Iried bas	sis unles	s otherwi	se stated)		
Borehole	Distless leb	Commonito	Dimtles dele	Cample			De	pth		Dep	th	Thic	kness		Core		Proxi	mate an	alysis			Addition	nal analysi	S	Comments
	no.	no.	Birtley lab no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
					CBSH		81.20	81.90		( )					<del>                                     </del>										
				1	CR	1	81.90	82.05																	1
					CBSH	]	82.05	82.15																	
					CR	340	82.15	82.32	340												ļ				
					CBSH		82.32	82.80									-				-				_
					R CBSH	-	82.80 83.85	83.85 85.30																1	_
					CBSH	360	90.55	90.95	360						+								+	-	
					CR		112.75	112.85							+								1		
WC18-13C					C	430	112.85	113.15	430	112.75	113.15 	0.40	0.29	Coal	55.0%										
					DC		115.60	115.85															1		Contamination from adjacent rock
WC18-13C			187404	4681	С	410	115.85	117.05	410	115.60	117.05	1.45	0.87	Coal	66.2%	1.91	0.73	7.79	18.23	73.25	0.54	1.0	99.7	1.34	- a lot of broken up rounded mudstone pebbles, hard to sort out from blocky, pieced coal.
WC18-13C			187405	4682	С	401	117.55	119.60	401	117.55	119.60	2.05	1.23	Coal	96.1%	4.06	0.76	4.91	19.74	74.59	0.43	2.0	99.7	1.31	
WC18-13C			187406	4683	С	400	119.60	122.80	400	119.60	122.80	3.20	1.93	Coal	61.9%	3.10	0.81	9.69	20.25	69.25	0.37	4.5	96.8	1.33	
					DC		125.60	125.75																	A thin 5cm ash band is found in
WC18-13C			187407	4684	DC	420	125.75 126.00	126.00 126.20	420	125.60	126.20 	0.60	0.39	Coal, ash parting	20.0%	2.70	0.69	63.06	13.08	23.17	0.18	-	-	2.03	between the coal.
WC18-13C					DC		130.18	130.28		130.18	130.28	0.10	0.06	Carbonate coal	50.0%										Coal with ample carbonate veins running through it at contact between rock and coal. Not sampled as it abuts the uphole rock and is not in between mineable coal.
					C	440	130.28	130.63	440																The geophysical interpretation
WC18-13C			187408	4685	DC	- 440	130.63 130.75	130.75 130.90	440	130.28	131.05	0.77	0.48	Coal/ upper thin ash parting	31.2%	1.93	0.63	23.05	19.07	57.25	0.51	5.5	99.4	1.45	was altered within the 440 band in
					DC	-	130.73	131.05						parting											order to adjust for two ash bands being labelled as rock and dirty
					R	1	131.05	131.20															<u> </u>		coal. Two samples were taken
WC10 12C			107400	4000	С			131.35		124 05	124 60	0.55	0.25	lower thicker ash	10.70/	1 40	0.60	04.62	10.70	EC OF	0.54	4.5	00.4	1 40	(1st bag with coal and thin parting
WC18-13C			187409	4686	DC		131.35	131.45		131.05	131.60	0.55	0.35	parting/coal	12.7%	1.48	0.62	24.63	16.70	56.05	0.51	4.5	99.4	1.48	and coal, 2nd bag with thin parting
					С		131.45																		and remaining coal).
					DC	442	133.72	133.90	442																
					CBSH	463	139.85	140.30	463				-												
					DC CBSH	460 483	145.50 157.00	145.65 157.50	460 483				-		+								+		
WC18-14C					CBSH	none	14.95	157.50	400	14.95	15 10	0.15	0.15	Siltstone	100.0%						<u> </u>		1		
					C		15.10	15.70							1		1.			l .	<u> </u>		+	<u> </u>	Dirty sample due to crushed coal
WC18-14C			187933	4687	DC	150	15.70	15.95	150	15.10		0.85			22.4%	3.12	1.47	34.17	19.16	45.20	0.69	1.5	76.8	1.57	with mixed coaly mudstone
WC18-14C					CR	130	20.50	20.70	130	20.50	20.70	0.20	0.20	Siltstone with coal spars	0.0%										

	Cross-refe		Head (raw)	) samples	Geoph	ysical lo	g interpret	ation				Sample	e chara	cterisation			Head r	aw anal	ysis (air d	ried bas	is unles	s otherwis	se stated)		
Borehole	D'alla Lab	0	District Lab	0			De	oth		Dep	th	Thicl	kness		Core		Proxi	mate an	alysis			Addition	al analysi	S	Comments
	Birtley lab (	no.	no.	Sample no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-14C			187934	4688	С	111	24.00	24.50	111	24.00	24.50	0.50	0.50	Coal	102.0%	1.74	0.50	15.90	28.73	54.87	0.75	6.5	96.5	1.44	Interval changed, more coal in box than in geophysics log
WC18-14C			187935	4689	С	110	25.30	25.60	110	25.30	25.60		0.30	Coal	140.0%	1.74	0.71	5.88	23.70	69.71		8.0	96.5	1.30	More coal in box than in geophysics log
WC18-14C			187936	4690	С	101	27.00	28.12	101	27.00	28.12	1.12	1.11	Coal/Ash	90.2%	1.98	0.80	10.08	21.14	67.98	0.44	2.0	97.7	1.36	1cm ash band included in sample
WC18-14C			187937	4691	C DC	100	28.12 30.00	30.00 30.18	100	28.12	30.18	2.06	2.04	Coal/Ash	87.9%	1.93	0.65	3.06	24.38	71.91	0.40	8.0	97.7	1.28	1cm ash band included in sample
WC18-14C			187938	4692	CR	none	30.18	30.40		30.18	30.40	0.22	0.22	Coaly mud	54.5%	3.34	0.57	21.35	21.60	56.48	0.35	7.5	97.7	1.41	coaly mud, soft, black
WC18-14C			187939	4693	CR		34.82	35.05		34.82	35.05	0.23	0.22	Coaly mudstone	65.2%	1.52	0.60	52.28	14.79	32.33	0.30	-	-	1.81	
WC18-14C			187940	4694	С	201	35.05	35.80	201	35.05	35.80	0.75	0.70	Coal	84.0%	2.37	0.61	7.88	22.65	68.86	0.64	8.0	97.7	1.30	
WC18-14C			187941	4695	CR		35.80	36.00		35.80	36.00	0.20	0.19	Coaly mudstone	15.0%	1.45	0.79	59.04	14.28	25.89	0.24	-	-	1.89	
WC18-14C			187942	4696	DC		37.15	37.22		37.15	37.22	0.07	0.07	Coaly mudstone	71.4%	1.20	0.55	59.84	14.47	25.14	0.25	-	-	1.94	
WC18-14C			187943	4697	С	200	37.22	37.50	202	37.22	37.50	0.28	0.26	Coal	142.9%	2.65	0.81	4.85	20.80	73.54	0.61	3.0	99.1	1.30	More coal in box than in geophysical log
WC18-14C			187944	4698	DC	202	37.50	37.87	202	37.50	37.87	0.37	0.35	Ash/Coal	97.3%	1.92	0.43	33.40	20.12	46.05	0.50	7.5	96.0	1.55	6cm ash band sampled with 30cm of coal
					С		37.87	38.10																	
WC18-14C					CR	none	46.35	46.60		46.35	46.60	0.25	0.23	Carb. mudstone	88.0%										
WC18-14C			187945	4699	С		48.45	48.80		48.45	10 NN	0.55	0.51	Dirty coal/Coal	80.0%	3.14	0.53	19.52	18.26	61.69	0.55	2.0	97.4	1.42	
VVO10-140			107343	4033	DC	300	48.80	49.00	300	+0.+3	43.00	0.55	0.51	Dirty Coai/Coai	00.070	J. 14	0.55	13.52	10.20	01.03	0.55	2.0	37.4	1.72	
WC18-14C			187946	4700	С		49.00	49.15		49.00	49.40	0.40	0.37	Ash(?)/Coal	85.0%	1.53	0.40	15.70	26.88	57.02	0.46	4.0	96.2	1.45	Sample includes a 7cm ash(?)
					CR	none	49.15	49.40																	band
WC18-14C			187947	4701	С	320	51.75	52.12	320	51.75	52.12	0.37	0.35	Coal	89.2%	1.35	0.38	16.70	21.01	61.91	0.66	3.0	97.4	1.40	
					CBSH		54.80	55.35	2.12			2.42	0.10		22.22/										
WC18-14C					CR		55.35	55.45	340	55.35	55.45	0.10	0.10	Coaly mudstone	20.0%										
					CBSH	340	55.45	55.50																	
				-	R		55.50	55.90					-		ļ			-		<u> </u>					
W040 440				ļ	CBSH	140	55.90	56.55	440	77.00	70.00	0.46	0.00		0.00/									ļ	
WC18-14C			407040	4700	CR	410	77.60	78.00	410	77.60	78.00			Not recovered	0.0%	0.54	0.07	07.00	00.05	54.05	0.40	0.5	07.7	4.55	
WC18-14C			187948	4702	C	401	78.60	79.05	401	78.60	79.05	0.45	0.44	Coal	66.7%	2.51	0.37	27.93	20.35	51.35	0.42	0.5	97.7	1.55	
WC18-14C			187949	4703	DC C	400	79.05 79.40	79.40 80.00	400	79.05	80.00	0.95	0.93	Ash/Coal	101.1%	5.50	0.66	4.38	20.18	74.78	0.45	1.0	92.0	1.30	2cm ash parting in sample

	Cross-refe		Head (raw)	samples	Geoph	ysical lo	g interpre	ation				Sample	e charac	cterisation			Head r	aw anal	ysis (air d	ried bas	is unles	s otherwi	se stated)		
Borehole	Birtley lab	Composite	Rirtley lah	Sample			De	pth		Dep	th	Thick	kness		Core		Proxi	mate an	alysis			Addition	nal analysi	S	Comments
	no.	no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	(percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
					Fault	Estab.	80.00	80.10							1 1										
					С	401	80.10	81.20	401/400																
					DC C	400	81.20 81.75	81.75 81.80	40 1/400																Crushed coal, not able to
WC18-14C			187950	4704	Fault	Poss.	81.80	81.85	Fault	80.00	86.90	6.90	6.77	Coal/Dirty coal	40.1%	5.30	0.61	4.79	21.09	73.51	0.43	4.0	96.8	1.29	separate 401 from 400
					С	400	81.85	85.05																	Separate 401 IIOIII 400
					DC		85.05	85.40																	
					Fault	Estab.	85.40	85.50	Fault																
					С	400	85.50	86.90	400																
WC18-14C			187951	4705	DC	400	86.90	87.38	400	86.90				Coaly mudstone/Coal	37.5%	7.48	0.79	50.75	14.40	34.06	0.28	-	-	1.78	
WC18-14C					CR	none	88.45	88.70		88.45				Silty mudstone	100.0%								ļ		
WC18-14C			187952	4706	С	420	88.70	88.95	420	88.70	88.95				64.0%	2.92	0.54	23.70				1.0	97.1	1.50	
WC18-14C			187953	4707	DC		92.25	92.32		92.25				Coaly mudstone	214.3%	1.78	0.65	55.21	11.84	32.30		-	<u> </u>	1.80	
WC18-14C			187954	4708	С		92.32	92.70		92.32	92.70	0.38	0.37	Coal/Ash	97.4%	3.02	0.51	9.89	18.24	71.36	0.62	1.0	97.4	1.34	2cm ash parting in sample
WC18-14C			187955	4709	DC C	440	92.70 92.90	92.90 93.05	440	92.70	93.30	0.60	0.59	Ash/Coal	38.3%	1.42	0.56	33.58	18.21	47.65	0.46	3.5	97.7	1.56	7cm ash parting in sample
					DC		93.05	93.30																	
					CBSH	442	95.50	96.00	442																
					CBSH	463	102.10	102.60	463																
					CBSH	460	106.90	107.05	460																
WC18-14C					CR		107.05	107.30		107.05	107.30	0.25	0.25	Coal	20.0%								ļ	<u> </u>	
					CBSH	483	114.20	114.70	483																
WC18-14C			187956	4710	DC	480	118.80 119.15	119.15 119.30	480	118.80	119.30	0.50	0.50	Coal	62.0%	1.52	0.45	11.31	25.19	63.05	1.00	8.0	95.4	1.36	
					CBSH	none	127.00	127.20																	Carbonaceous shale> dirty coal,
WC18-14C			188230	4984	DC	A71	127.20	127.45	A71	127.00	127.45	0.45	0.45	Dirty coal, Coal	82.2%	1.66	0.58	31.38	16.42	51.62	0.79	8.0	98.6	1.52	picks were combined in order to accommodate for high amount of coal logged.
WC18-14C			187957	4711	DC C	A7	127.95 128.40	128.40 128.95	A7	127.95					86.0%	1.76	0.54					5.0	98.0	1.40	
WC18-14C			187958	4712	DC		128.95	129.10		128.95	129.10	0.15	0.15	Stony coal	126.7%	1.34	0.60	38.62	16.04	44.74	0.76	7.0	98.3	1.59	
					CBSH	A5	135.70	136.40	A5																
					CBSH	] ]	5.20	5.42															<u> </u>		
WC18-15C					DC	310	5.42	5.60	310	5.42				Not recovered	0.0%								<del>                                     </del>	<u> </u>	
WC18-15C					CR		5.60	5.82		5.60	5.82	0.22	0.21	Not recovered	0.0%								<u> </u>	<u> </u>	
WC18-15C			187959	4713	DC C	300	11.95 12.10	12.10 12.60	300	11.95	12.60	0.65	0.65	Coal	73.8%	4.17	0.74	21.84	17.84	59.58	0.67	0.5	79.0	1.46	
	+ +				CBSH	320	15.60	16.50	320				-		+ -		-			-			+		

		ference to osites	Head (raw)	) samples	Geoph	ysical lo	g interpre	tation				Sample	e charac	eterisation			Head r	aw anal	ysis (air d	ried bas	is unles	s otherwis	se stated)		
Borehole	Dietlasslah	Camanaaita	Diatlesslah	Camania			De	pth		Dep	oth	Thick	ness		Core		Proxi	mate an	alysis			Addition	al analysi	S	Comments
	no.	no.	Birtley lab no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
					CBSH		19.40	20.70							1 / 1										
					R	340	20.70	22.35	340																
					CBSH	1	22.35	23.20																	
					CBSH	360	32.72	32.90	360																
WC18-15C					DC	430	41.70	42.05	430	41.70	42.05	0.35	0.33	Carbonaceous rubble	28.6%										
					DC		45.12	45.35																	Hard to cleanly separate broken
WC18-15C			187960	4714	С	410	45.35	46.18	410	45.12	46.18	1.06	1.04	Coal	12.3%	1.35	0.65	6.33	18.10	74.92	0.65	1.0	98.6	1.32	siltstone/mudstone from the broken coal. There may be some mixing
WC18-15C					CR		47.38	47.58		47.38	47.58	0.20	0.20	Muddy siltstone	0.0%										Not sampled - muddy siltstone
WC18-15C			187961	4715	С	401	47.58	48.55	401	47.58	48.55	0.97	0.95	Coal	89.7%	1.59	0.58	4.32	19.36	75.74	0.45	3.0	96.0	1.29	No parting found between seams
WC18-15C			187962	4716	DC		48.55	48.65		48.55	50.30	1.75	1.71	Cool	28.6%	1.67	0.39	2.98	21.43	75.20	0.44	5.0	96.0	1.28	401/400. Distinction between
WC 10-13C			107902	47 10	С	400	48.65	50.30	400	40.55	30.30	1.73	1.7 1	Coal	20.0 /0	1.07	0.59	2.90	21.43	75.20	0.44	5.0	30.0	1.20	seams was chosen based on a
WC18-15C			187963	4717	DC	400	50.30	50.65	400	50.30	50.65	0.35	0.34	Ash parting, coal	37.1%	2.99	0.70	37.47	17.25	44.58	0.34	1.0	96.2	1.60	slightly harder coal that transitioned into ground up softer coal
WC18-15C					CR		50.65	50.85		50.65	50.85	0.20	0.20	Carbonaceous silty mudstone	0.0%										
WC18-15C					DC	420	51.05	51.30	420	51.05	51.30	0.25	0.24	Coal	12.0%										
					С	]	53.82	54.27																	
WC18-15C			187964	4718	DC	]	54.27	54.37		53.82	54.45	0.63	0.61	Coal	39.7%	1.38	0.37	12.54	18.21	68.88	0.57	2.5	98.0	1.37	
					С	440	54.37	54.45	440																
WC18-15C			187965	4719	DC	1	54.45	54.52		54.45	54.85	0.40	0.38	Ash, Coal	45.0%	1.02	0.37	51.80	16.39	31.44	0.28	_	_	1.82	
W040 450	-				C	440	54.52	54.85	110	FC 70	F7 40	0.40		·	0.00/		1			-				-	
WC18-15C	-				CR CBSH	442 463	56.70 63.90	57.10 64.50	442 463	30.70	57.10	0.40	0.36	Siltstone	0.0%								1	-	
WC18-15C	-				DC	460	68.60	68.80	460	68.60	68.80	0.20	0.20	Dirty coal	55.0%		1			<u> </u>				-	
WC18-15C			187966	4720	C	400	79.05	79.20	400	79.05		0.20			80.0%	1.45	0.52	10.99	24.29	64.20	1.03	7.0	97.7	1.38	
VVO10-130			107300	7/20	DC	1	79.20	79.35			i				00.070	1.40	0.02	10.55	24.25	04.20	1.00	7.0	37.7	1.50	
WC18-15C			187967	4721	C	480	79.35	79.80	480	79.20	80.00	0.80	0.79	Ash parting,Coal/Dirty Coal	103.8%	2.78	0.62	20.59	22.36	56.43	0.91	7.5	97.7	1.45	
					DC	1	79.80	80.00				0.00	••	Coal	1.00.070		5.52				0.0.		••••		
WC18-15C			187968	4722	С	A71	85.70	86.12	A71	85.70	86.12	0.42	0.40	Coal	69.0%	1.37	0.54	7.92	24.78	66.76	1.10	8.0	97.1	1.31	
					С		87.10	87.50							1 1		1								
WC18-15C			187969	4723	DC	A7	87.50	87.60	A7	87.10	87.60	0.50	0.46	Coal dust	20.0%	7.62	0.58	25.18	18.42	55.82	0.85	7.0	96.5	1.46	
WC18-15C					DC	A72	88.13	88.30	A72	88.13	88.30	0.17	0.13	Not recovered	0.0%										
					CR	A5	95.72	96.00	A5																
WC18-16C					DC	110	2.50	2.90	110	2.50				Not recovered	0.0%										Inside casing not recovered
WC18-16C			187970	4724	С	101	8.80	9.25	101	8.80		0.45			88.9%	1.76	0.64	10.64	20.48			2.0	92.3	1.37	
WC18-16C			187971	4725	С	100	9.25	10.65	100	9.25	10.65	1.40	1.35		35.7%	6.60	0.55	5.86	27.06	66.53	0.53	7.5	89.4	1.28	
WC18-16C					CR		10.65	10.93		10.65	10.93	0.28		Carbonaceous muddy siltstone	60.7%										

	1	ference to	Head (raw)	samples	Geoph	ysical lo	g interpre	tation				Sample	e charac	cterisation			Head r	aw anal	ysis (air d	ried bas	sis unles	s otherwis	se stated)		
Borehole			Birtley lab	Sample			De	pth		Dep	oth	Thicl	kness		Core		Proxi	mate an	alysis			Addition	nal analysi	S	Comments
	no.	no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	(percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-16C			187972	4726	C DC	201	15.40 16.00	16.00 16.15	201	15.40	16.15	0.75	0.72	Coal	16.0%	2.44	0.72	25.77	20.36	53.15	0.58	7.0	94.0	1.48	
WC18-16C			187973	4727	CR		18.55	18.70		18.53	18.62	0.09	0.09	Ashy/Coaly mudstone?	100.0%	1.25	0.52	72.84	12.39	14.25	0.20	-	-	2.17	Less than 35cm - however it is the abutting roof of seam 202 and appears coaly.
WC18-16C			187974	4728	С		18.70	18.85		18.62	19.03	0.41	0.39	Coal	100.0%	1.78	0.62	11.53	18.85	69.00	0.66	1.5	99.7	1.37	Picks for seam 202 were expanded up and
WC18-16C			187975	4729	DC	202	18.85	19.20	202	19.03	19.35	0.32	0.31	Ash parting, coal	100.0%	1.87	0.69	44.36	17.61	37.34	0.45	-	-	1.70	downhole to accommodate for the large amount of recovered coal in the box. Ash bands present in coal seam.
WC18-16C			187976	4730	CBSH		37.55	37.75		37.55	37.75	0.20	0.18	Coal and altered coaly rock?	95.0%	1.04	0.48	35.14	35.21	29.17	0.49	1.0	98.0	1.86	Carb, shale> Coaly rock/Coal. Carbonaceous shale was cho-sen to represent this interval of coal and coaly rock.
WC18-16C			187977	4731	С	300	37.75	38.12	300	37.75	38.12	0.37	0.34	Coal	59.5%	4.60	0.62	13.61	20.82	64.95	0.82	6.5	96.8	1.37	
					CBSH		41.20	41.45																	
WC18-16C					CR	320	41.45	41.60	320	41.45	41.60	0.15	0.13	Carbonaceous siltstone	0.0%										
					CBSH		41.60	41.85																	
					CBSH	]	44.85	45.45	]																
WC18-16C					CR	340	45.45	45.60	340	45.45	45.60	0.15	0.13	Carbonaceous silty mudstone	53.3%										
					CBSH	340	45.60	45.85	340																
					R	]	45.85	46.63																	
					CBSH	ļ	46.63	47.50																	
WC18-16C					DC	430	66.12	66.40	430	66.12	66.40				29.6%										
WC18-16C			187978	4732	C	410	68.55	68.95	410	68.55	68.89	0.34	0.32		100.0%	5.09	0.61	16.91	17.52	64.96		1.0	98.6	1.42	Picks were changed in order to
WC18-16C			187979	4733	Fault	Poss.	68.95	69.05	Possible	68.89	69.03	0.14		Siltstone parting	92.9%	2.49	1.07	87.47	5.72		0.70	-	-	2.41	accommodate for large amount of
WC18-16C			187980	4734	C	410	69.05	69.30	410	69.03	69.30	0.27		Coal	96.3%	7.92	0.66	8.71	18.03	72.60		1.5	98.3	1.35	coal recovery in box.
WC18-16C			187981	4735	C DC	401	70.28 71.00	71.00 71.38	401	70.28	71.00	0.72	0.67	Coal	51.4%	5.32	0.71	13.70	17.99	67.60	0.41	0.5	99.4	1.39	Coal-on-coal contact between 401 and 400 was chosen based on the 400's
WC18-16C			187982	4736	C	400	71.00	72.60	400	71.00	72 00	2 00	104	Dirty Coal/Coal	82.7%	2.78	0.63	8.45	19.44	71.48	0.40	2/5	98.3	1 25	harder dirty coal (ground out at upper
VVC10-10C			107902	4730	DC	400	72.60	73.08	400	71.00	13.00	2.00	1.94	Dirty Coai/Coai	02.7%	2.70	0.03	0.43	19.44	11.40	0.40	2/3	90.3	1.35	contact) underlying the top 401's extremely crushed and pulverised coal.
WC18-16C			187983	4737	DC	420		73.95	420	73.80	73 95	0.15	0 14	Coal	33.3%	1.88	0.61	18 88	18.88	61 63	0.40	4.0	96.8	1.45	ordania dna parvensea soai.
WC18-16C			187984	4738	CR	720	73.95	74.20	720	73.95	1			Ash Parting/Coal	60.0%	0.75		48.11		33.17	1	- 4.0	30.0	1.80	CR mislabelled - ash band and coal rather
																							00.4		than CR
WC18-16C WC18-16C			187985	4739	С	1	77.70	77.92	-	77.70				Ash parting/Coal	40.0%	1.72	0.50		19.52			4.5	99.1 98.6	1.36 1.57	Picks were changed in order to
WC18-16C WC18-16C	<del>                                     </del>		187986 187987	4740 4741	DC	440	77.92	78.28	440	77.90 78.09				Ash parting/Coal	89.5% 90.9%	1.33 0.72	0.55	30.46 62.21	19.12 15.64				90.0	2.05	accommodate for one thin and
WC18-16C	-		187988	4741	С	-	78.28	78.50	1					Coal/Dirty coal	96.7%	1.79	0.54		20.01			5.5	98.0	1.34	one thick ash parting.
VVC 10-10C			107300	4142	CBSH	442	79.90	80.30	442	10.20	10.50	0.30	0.20	Coal/Dirty Coal	30.170	1.18	0.42	9.50	20.01	10.07	0.70	0.0	30.0	1.34	
					CBSH	463	84.75	85.15	463				<del>                                     </del>				1	-			+		+	-	
WC18-16C					CBSH	460	89.22	89.55	460	89.22	89 55	0.33	0.31	Coal	39.4%		1			-	<del>                                     </del>		<del>                                     </del>	-	
440 10-100		ļ		ļ		1 700	00.22	09.00	1 700	00.22	100.00	0.00	0.01	Joodi	JJ.470				ļ	L	<u> </u>	I	1		

	Cross-refere composit		Head (raw)	samples	Geoph	ysical lo	g interpre	tation				Sample	e charac	cterisation			Head r	aw analy	sis (air d	ried bas	is unles	s otherwis	se stated)		
Borehole	Birtley lab Co	mnocito	Pirtley Joh	Cample			De	pth		Dep	oth	Thicl	kness		Core recovery		Proxi	mate an	alysis			Addition	al analysis	S	Comments
	no.	no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	(percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-16C			187989	4743	DC		101.30	101.53		101.30	101.53	0.23	0.22	Coal/Coaly rock	43.5%	1.69	0.41	29.87	35.04	34.68	0.63	8.0	92.5	1.75	
WC18-16C			187990	4744	DC	480	101.53 102.10	102.10 102.30	480	101.53	102.30	0.77	0.74	Coal	83.1%	2.59	0.54	16.72	21.26	61.48	1.00	2.0	97.1	1.39	
WC18-16C			187991	4745	CBSH		102.30	102.48		102.30	102.48	0.18	0.17	Coaly mudstone/ Mudstone	83.3%	2.48	0.69	57.95	13.06	28.30	1.01	-	-	1.86	Carbonaceous shale> Coaly rock, this interval was chosen to reflect the coaly mudstone
WC18-16C			187992	4746	С	A71	108.00	108.35	A71	108.00	108.35	0.35	0.34	Coal/Dirty Coal	80.0%	1.25	0.40	12.30	20.50	66.80	0.97	8.5	97.7	1.34	
WC18-16C			187993	4747	DC	A7	109.30 110.15	110.15 110.30	A7	109.30	110.30	1.00	0.86	Coal/Dirty coal	52.0%	1.46	0.50	14.22	19.41	65.87	0.85	1.5	97.7	1.36	
					CR	A5	117.00	117.15																	
WC18-16C					DC	A3	122.45	122.75	A3	122.45	122.75	0.30	0.27	Not recovered	0.0%										
WC18-16C					CBSH CR	A1	123.40 123.60	123.60 123.75	A1	123.40	123.75	0.35	0.32	Coaly mdst	20.0%										
WC18-17C		ĺ	187994	4748	С	150	16.80	17.00	150	16.80	17.00	0.20	0.19	Coal	25.0%	3.31	0.97	15.01	21.57	62.45	0.90	1.0	91.7	1.36	
WC18-17C			187995	4749	DC	150	17.00	17.60	150	17.00	17.60	0.60	0.58	Ash parting/Coal	61.7%	3.32	1.14	35.19	18.43	45.24	0.69	1.5	94.2	1.58	
WC18-17C					CR	130	21.35	21.80	130	21.35		0.45		Carbonaceous siltstone	15.6%										
WC18-17C			187996	4750	С	111	27.05	27.35	111	27.05		0.15		ļ	93.3%	3.49	0.96		19.48	59.26		0.0	94.5	1.45	Picks were altered in order to
WC18-17C			187997	4751	CBSH		27.35	27.60		27.20	27.60	0.40		Dirty ashy coal?, Coal	97.5%	3.48	1.10	20.20	23.93	54.77		0.0	97.4	1.51	accommodate for ashy dirty coal
WC18-17C			187998	4752	С	110	28.30	28.65	110	28.30	28.65	0.35	0.35	<del> </del>	62.9%	3.33	0.83	5.05	22.37	71.75	0.66	0.5	96.2	1.34	
WC18-17C					CR		28.65	28.80		28.65	28.80			Not recovered (brown mud?)	33.3%										Brown mud with little evidence of being coaly rock
WC18-17C			187999	4753	С	101	29.40	30.35	101	29.40	30.35	0.95	0.94	Coal	70.5%	2.04	0.65	10.26	20.42	68.67	0.47	2.0	98.3	1.38	Coal on coal contact was chosen
WC18-17C			188000	4754	С	100	30.35	32.05	100	30.35	32.05		1.68		86.5%	1.74	0.58	3.17	24.29	71.96		8.0	96.5	<mark>1.02</mark>	based on slight change of coal quality within a broken stick
WC18-17C			188001	4755	С		39.60	40.12		39.60	40.00				50.0%	2.53	0.49	7.73	19.93	69.85		7.0	97.4	1.33	Picks adjusted to change dirty
WC18-17C			188002	4756		201			201	40.00		0.12		Ash parting, Coal	83.3%	1.57	0.43	30.37	19.51	49.69		7.0	96.8	1.54	coal to ash and coal layers
WC18-17C			188003	4757	DC		40.12	40.20		40.12	40.20			Ash parting, Coal	87.5%	4.93	0.56	37.45	18.17	43.82		6.0	97.7	1.62	,
WC18-17C			188004	4758	C		43.40	43.75		43.40	43.75	0.35	0.34	Coal	71.4%	1.77	0.53	7.00	19.26	73.21	0.68	2.5	98.6	1.34	
WC18-17C			188005	4759	CR	202	43.75	43.85	202	43.75	43.89	0.14	0.13	Dirty Ash	85.7%	1.13	0.43	74.54	14.62	10.41	0.13	-	-	2.26	Coaly rock width changed to accommodate thick ash layer.
111040 470			400000	4700	DC		43.85	43.98	<b></b>	40.00	14.00			0 1/2: 1 0 1	00.70/	4.00		47.0.	00.47	04.75	0.00	7.0	07.4	, ,,	
WC18-17C			188006	4760	CR	-	43.98	44.08		43.89	44.20	0.31	0.30	Coal/Dirty Coal	38.7%	4.20	0.44	17.34	20.47	61./5	0.68	7.0	97.4	1.41	
WC10 170					DC		44.08	44.20		44.00	44.20	0.40	0.40	Ciltatana	100.00/		-								
WC18-17C					CR CBSH	240	44.20	44.30	210	44.20	44.30	0.10	0.10	Siltstone	100.0%		-								
	<del>                                     </del>					310	52.80	53.20	310						<del>                                     </del>		-					-	-	-	Badly crushed and pulverised with
WC18-17C			188007	4761	С	300	64.45	64.83	300					Dirty coal and siltstone?	28.9%	5.66		54.12	13.36			0.5	98.6	1.86	mixed rock.
WC18-17C			188008	4762	CR	320	68.00	68.20	320	68.00	68.20	0.20	0.19	Coal	15.0%	1.91		28.01	16.18			1.0	99.7	1.52	
WC18-17C			188009	4763	DC		68.20	68.40	320	68.20	68.40	0.20	J 0.19	Ash/Coal	70.0%	1.84	0.53	48.42	15.48	35.5/	0.50	-	-	1.79	

	Cross-refe		Head (raw)	samples	Geophy	ysical lo	g interpret	tation				Sample	charac	cterisation			Head r	aw anal	ysis (air d	Iried bas	is unles	ss otherwis	se stated)		
Borehole	Birtley lab	Composite	Rirtley lah	Sample			De	pth		Dep	th	Thick	ness		Core		Proxi	mate an	alysis			Addition	nal analys	is	Comments
	no.	no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	(percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
					CBSH		74.25	74.60																	
					R		74.60	74.92																	
					CBSH		74.92	75.39																	
					R	340	75.39	75.80	340																
					CBSH		75.80	76.20																	
					R		76.20	79.20																	
					CBSH		79.20	79.80																	
WC18-17C					DC	430	93.90	94.20	430	93.90	94.20	0.30		Not recovered	0.0%										
WC18-17C			188010	4764	С	410	97.48	98.30	410	97.48	98.30	0.82			70.7%	2.36	0.63	15.77	17.14	66.46	0.51	1.0	98.0	1.42	
WC18-17C					CR		98.80	99.03		98.80	99.03			Siltstone	100.0%										
WC18-17C			188011	4765	С	401	99.03	99.80	401	99.03	99.80	0.77	0.70	Coal	62.3%	2.35	0.73	5.14	19.53	74.60	0.40	2.0	98.6	1.33	
					DC		99.80	100.00																	
WC18-17C			188012	4766	С	400	100.00	101.20	400	99.80	101.50	1.70	1.54	Coal	75.3%	2.55	0.54	6.30	20.19	72.97	0.37	2.5	97.4	1.33	
					DC		101.20	101.50																	
WC18-17C			188228	4982	DC	420	104.25	104.40	420		104.40				33.3%	2.08	0.39	15.22	22.78			5.0	98.3	1.41	
WC18-17C			188229	4983	CR	720	104.40	104.60	720		104.60	0.20	0.18	Ash parting and coal	75.0%	1.40	0.51	43.25	18.78	37.46				1.70	
WC18-17C			188013	4767	С		107.00	107.20		107.00	107.20	0.20	0.18	Coal	110.0%	1.40	0.45	7.06	19.62	72.87	0.67	3/5	98.8	1.34	
WC18-17C			188014	4768	DC		107.20	107.30		107.20	107.42	0 22	0.20	Ash/Coal	45.5%	0.95	0.55	44.80	18.17	36.48	0.38	4.0	97.1	1.74	
W010 170			100014	4700	С	440	107.30	107.42	440	107.20	107.42	0.22	0.20	7 torii oodi	10.070	0.50	0.00	11.00	10.17	00.40	0.00	7.0	37.1	1.74	
WC18-17C			188015	4769	DC		107.42	107.58		107 42	107.85	0.43	0.40	Carb. siltstone/Ash/Coal	62.8%	1.11	0.50	37.85	17.16	44.49	0.42	1.0	97.7	1.65	
W010 170			100010	4700	С		107.58	107.85		107.42	107.00	0.40	0.40		02.070	1.11	0.00	07.00	17.10	14.40	0.72	1.0	57.7	1.00	
WC18-17C					DC	442	109.05	109.20	442	109.05	109.20	0.15	0.14	Coal, Dirty coal, Coaly rock	106.7%										
					CBSH	463	113.30	113.80	463																
					CBSH		117.60	117.80																<u> </u>	
WC18-17C					CR	460	117.80	118.00	460	117.80	118.00	0.20	0.19	Coal	50.0%		ļ							<u> </u>	
					CBSH		118.00	118.12																	
WC18-17C			188016	4770	С	480	126.26	127.10	480	126.26	127 20	0.04	0.02	Coal/Dirty coal	98.9%	1.39	0.42	31.05	22.80	45.73	0.85	1.0	97.7	1.59	
VV C 10-17 C			100010	4110	DC	400	127.10	127.20	400	120.20	121.20	0.34	0.92	Oddi/Dirty Codi	30.370	1.09	0.42	31.03	22.00	+3.73	0.03	1.0	91.1	1.03	
WC18-17C			188017		DC	A71		133.75	A71	133.35					67.5%				23.05				98.3	1.31	
WC18-17C			188018	4772	С			134.65		134.45					30.0%			37.25					97.1	1.61	
WC18-17C			188019	4773	DC	A7		135.05	A7	134.65	135.05	0.40	0.36	Carb. Mdst/DC/C	45.0%	1.61	0.80	31.03	16.47	51.80	0.66	5.0	99.1	1.55	
WC18-17C			188020	4774	CR DC	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	135.05 135.15	135.15 135.35	Λ/	135.05	135.35	0.30	0.27	Carb. mudstone / Coal and mudstone	123.3%	1.16	0.53	48.11	12.79	38.57	0.58	6.5	99.1	1.73	
WC18-18C					CR		11.15							Silty mudstone	100.0%		1							<del> </del>	

		ference to osites	Head (raw)	samples	Geoph	ysical lo	g interpre	tation				Sample	e chara	cterisation						•		ss otherwis			
Borehole			Dirtley Joh	Cample	·		De	pth		Dep	oth	Thick	kness		Core		Proxi	mate an	alysis			Addition	al analysi	s	Comments
	no.	Composite no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-18C			188021	4775	С		11.43	11.60		11.43	11.64	0.21	0.14	Coal	100.0%	5.27	1.44	19.55	21.66	57.35	0.92	0.5	62.8	1.49	
WC18-18C			188022	4776	R		11.60	11.80		11.64	11.80	0.16	0.11	Coaly siltstone?	31.3%	1.29	0.83	66.24	15.33	17.60	0.29	0.0	93.1	2.12	
					DC	150	11.80	12.05	150																
WC18-18C			188023	4777	С		12.05	12.15		11.80	12.15	0.35	0.24	Coal	51.4%	5.03	1.12	18.94	20.57	59.37	0.85	0.5	91.1	1.40	
WC18-18C			188024	4778	DC		12.15	12.45		12.15	12.46	0.31	0.21	Coaly mudstone	100.0%	3.01	1.20	54.30	12.71	31.79	0.44	0.0	94.0	1.85	
WC18-18C					CR	130	18.85	19.20	130	18.90	19.30	0.40	0.24	Not recovered	0.0%										
WC18-18C			188025	4779	DC		23.05	23.38		23.05	23.38	0.33	0.23	Coal	51.5%	3.82	1.14	10.03	22.80	66.03	0.76	0.0	95.4	1.40	
WC18-18C			188026	4780	CR DC	111	23.38 23.48	23.48 23.80	111	23.38	23.80	0.42	0.29	Ash/Coal	35.7%	2.88	1.11	19.35	25.41	54.13	0.61	0.0	93.4	1.52	
WC18-18C			188027	4781	С	110	25.30	25.75	110	25.30	25.75	0.45	0.31	Coal	68.9%	3.11	1.12	4.07	22.68	72.13	0.65	0.5	94.8	1.32	
WC18-18C			188028	4782	С	101	27.65	29.30	101	27.65	29.30	1.65	1.13	Coal/Ash	86.7%	2.82	1.23	9.48	20.00	69.29	0.47	0.0	98.0	1.40	5cm ash band in sample
WC18-18C			188029	4783	C DC	100	29.30 31.50	31.50 31.75	100	29.30	31.75	2.45	1.67	Coal/Dirty coal/Coalified wood	50.2%	2.74	0.89	2.37	24.13	72.61	0.52	3.5	97.4	1.29	6cm coalified wood in sample
WC18-18C					CR		31.75	32.05		31.75	32.05	0.30	0.15	Carbonaceous mudst.	40.0%		1					†			
WC18-18C			188030	4784	C	201	40.30	41.35	201	40.30	41.35		0.60		14.3%	6.97	0.64	35.50	16.58	47.28	0.57	3.5	98.3	1.57	
WC18-18C			188031	4785	DC C		45.70 45.90	45.90 46.40	-	45.70		0.70			55.7%	1.65	0.50	12.60		68.05		1.5	98.6	1.39	
WC18-18C			188032	4786	CBSH		46.40	46.60		46.40	46 60	0.20	0.13	Δeh	80.0%	1.09	0.66	79.39	14.92	5.03	0.08	<del> </del>	_	2.37	Carb. shale> ash layer.
VVO 10-100			100002	4700	CR	202	46.60	46.82	202	70.70	70.00	0.20	0.10	I AGII	00.070	1.00	0.00	75.55	14.52	0.00	0.00			2.01	Carb. Shale — ash layer.
WC18-18C			188033	4787	C	1	46.82	47.05		46.60	47.23	0.63	0.40	Coal/Dirty coal	38.1%	1.30	0.45	9.05	21.56	68.94	0.75	7.5	98.0	1.33	
W010 100			100000	4707	DC		47.05	47.23		40.00	17.20	0.00	0.40	Coan Birty coan	00.170	1.00	0.40	0.00	21.00	00.54	0.70	1.0	00.0	1.00	
					CBSH	310?	58.70	59.75	310?													1			
WC18-18C					CR		76.05	76.30		76.05	76.30	0.25	0.15	Carb. mudstone / ash	100.0%										Not sampled - ash
			100004	4700	DC		76.30	76.55							1	1 10	0.50	10.00	16.00	64.47	0.50	1 22	00.7	1 47	'
WC18-18C			188034	4788	С	1	76.55	76.75		76.30	/0./5	0.45	0.26	Coal	28.9%	1.13	0.58	18.92	16.03	64.47	0.56	2.0	99.7	1.47	
WC18-18C			188035	4789	R	300	76.75	77.00	300	76.75	77.00	0.25	0.15	Carbonaceous mudst.	68.0%	1.58	0.71	82.78	6.90	9.61	0.15	-		2.34	
WC18-18C			188036	4790	DC		77.00	77.08		77.00	77.60	0.60	0 35	Cool/Dirty cool	85.0%	1.59	0.48	5.44	21.03	73.05	0.82	7.0	98.6	1.30	
VVC 10-10C			100030	4190	С		77.08	77.60						Coal/Dirty coal		1.59	0.40	5.44	21.03	13.03	0.02	7.0	90.0	1.30	
WC18-18C					CR	320	81.80	82.00	320	81.80	82 22	0.42	0.26	powdered mudstone and coal	33.3%										
VVC 10-10C					С	320	82.00	82.22	J2U	01.00	02.22	0.42	0.20	coal	JJ.J /0										
					CBSH		90.80	92.60																	
					R		92.60	94.30														ļ			
					CBSH	340	94.30	95.45	340																
					R		95.45	95.65														ļ			
					CBSH		95.65	95.95							$\downarrow$									ļ	
					CBSH	360	101.60	101.80	360																

	Cross-refer		Head (raw)	samples	Geoph	ysical lo	g interpret	tation				Sample	e charac	cterisation			Head r	aw anal	ysis (air d	ried bas	is unles	s otherwis	se stated)		
Borehole	Birtley lab C	`omnosita	Rirtley lab	Sample			De	pth		Dep	oth	Thick	ness		Core recovery		Proxi	mate an	alysis			Addition	al analysi	S	Comments
	no.	no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	(percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-18C			188037	4791	CR DC CR	430	121.15 121.25 121.40	121.25 121.40 121.65	430	121.15	121.65	0.50	0.39	Dirty coal/Coal	98.0%	1.34	0.49	21.32	16.58	61.61	0.89	1.0	99.7	1.47	
WC18-18C					CR		125.70	125.97		125 70	125 97	0.27	0.19	Siltstone	100.0%										
WC18-18C			188038	4792	C	410	125.97	126.50	410	125.97				Coal/mudstone	32.1%	3.19	0.48	58.77	14.93	25.82	0.31	-	-	2.00	
WC18-18C			188039	4793	Fault	Prob- able	126.50	126.63		126.50					53.8%	2.44	0.46	80.64	20.02	<mark>-1.12</mark>		-	-	2.41	
WC18-18C					С	410	126.63	126.95	410	126.63	126.95	0.32	0.32		0.0%										
WC18-18C			188040	4794	R		126.95	127.40		126.95	127.40	0.45	0.33	Coal/Dirty coal	64.4%	2.32	0.85	58.73	10.65	29.77	0.24	-	-	1.95	
WC18-18C			188041	4795	С	401	127.40	128.40	401	127.40	128.40	1.00	0.74	Coal	75.0%	2.76	0.61	3.14	19.60	76.65	0.43	1.0	98.0	1.32	
WC18-18C			188042	4796	DC C	400	128.40 128.60	128.60 130.15	400	128.40	130.40	2.00	1.49	Coal	91.0%	2.13	0.52	5.52	20.79	73.17	0.43	4.5	98.6	1.34	
					DC		130.15	130.40															ļ	ļ	
WC18-18C					DC	420	133.50	133.70	420	133.50	133.70	0.20	0.15	Coal	60.0%										
WC18-18C			188043	4797	DC C		139.00 139.10	139.10 139.40		139.00	139.41	0.41	0.30	Coal	100.0%	1.16	0.54	3.91	19.29	76.26	0.69	1.5	99.1	1.29	
WC18-18C			188044	4798	DC	440	139.40	139.52	440	139.41	139.53	0.12	0.09	Ash/Coal	100.0%	1.06	0.50	35.19	18.88	45.43	0.43	4.0	98.8	1.59	4cm ash parting was included in sample
WC18-18C			188045	4799	CR		139.52	139.75			139.75			Mudstone/Ash	86.4%	0.56	0.36	67.63	15.41	16.60		-	-	2.13	
WC18-18C			188046	4800	DC		139.75	140.15		139.75		0.40		Coal/Dirty coal	85.0%	1.06	0.47	6.03	20.69	72.81		5.5	98.0	1.35	4cm ash band in sample
WC18-18C			188047	4801	CR		140.15	140.60		-				Mudstone with coal	100.0%	0.72	0.48	63.93	9.91	25.68	0.25	-	-	1.90	Floor sample
WC18-18C					С		142.65	143.05		142.65	143.05	0.40	0.28	Dirty coal	27.5%										
11/0/0 /00			100010	1000	CBSH	310?	8.15	8.55	310?	10.00	40.50				100.00/			44.0-	40.00						
WC18-19C	<u> </u>		188048	4802	C	300	16.00	16.52	300	16.00	16.52	0.52	0.51	Coal	100.0%	3.28	1.14	14.95	18.39	65.52	0.67	0.5	95.7	1.41	
					CBSH CBSH	320	19.80 25.40	20.60 25.50	320																
					CBSH	340	25.50 30.20	30.20 30.80	340											-			-	-	
	<del>                                     </del>				CBSH	360	36.25	36.75	360						+ +								-	1	
WC18-19C	+ +	+			DC	430	46.80	47.05	430	46.80	47 05	0.25	0.23	Not recovered	0.0%					<del>                                     </del>		<del>                                     </del>	<del>                                     </del>		
WC18-19C			188221	4975	DC C	410	50.45 50.60	50.60 51.40	410					Coaly rock	21.1%	1.12	0.54	22.55	17.45	59.46	0.51	1.0	99.4	1.48	Bad recovery
WC18-19C			188049	4803	Č	401	52.95	53.90	401	52.95	53.90	0.95	0.88	Coal, ash	107.4%	2.08	0.52	14.50	19.85	65.13	0.37	1.5	99.1	1.40	
					DC		53.90	54.10						,			T				T	1		1	
WC18-19C					С	400	54.10	55.40	400	53.90	55.85	1.95	1.84	Not recovered	0.0%										
WC18-19C					DC C DC	420	55.40 55.85 56.00	55.85 56.00 56.10	420	55.85	56.10	0.25	0.24	Not recovered	0.0%										

	Cross ra	ference to			1			T						<b>,</b>	,							<u> </u>			1
		osites	Head (raw)	samples	Geoph	ysical lo	g interpre	tation				Sample	e chara	cterisation			Head r	aw anal	ysis (air d	ried bas	is unles	s otherwis	e stated)		
Borehole	Pirtley Jah	Composite	Dirtloy Joh	Cample			De	pth		Dep	oth	Thicl	kness		Core recovery		Proxi	mate an	alysis			Addition	al analysi	S	Comments
	no.	no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	(percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-19C					CR		56.10	56.30		56.10	56.30	0.20	0.19	Not recovered	0.0%										
					С		57.60	57.90																	
					DC		57.90	58.00																	
WC18-19C					С	440	58.00	58.10	440	57.60	58 50	0.90	0.83	Not recovered	0.0%										]
VVC10-13C					DC	1 440	58.10	58.20	440	37.00	30.50	0.30	0.00	INOT recovered	0.070										_
					С		58.20	58.30									ļ								_
					DC		58.30	58.50									ļ								
WC18-19C	<u> </u>	ļļ			DC	442	60.30	60.60	442	60.30	60.60	0.30	0.28	Not recovered	0.0%										
					CBSH	463	68.00	68.80	463		ļ														
WC18-19C					DC	460	72.52	72.90	460	72.52	72.90	0.38	0.35	Not recovered	0.0%		ļ								
	-				CBSH	483	75.70	76.00	483						1										
WC18-19C			188050	4804	С	480	82.50	83.18	480	82.50	83.18	0.68	0.65	Dirty coal/Coal	13.2%	1.12	0.42	9.62	25.54	64.42	1.01	7.5	98.0	1.35	Bad recovery
WC18-20C			188051	4805	C		9.70	9.90		9.70	10.00	0.30	0.26	Coal	83.3%	6.18	1.34	17.29	22.26	59.11	0.97	1.0	42.8	1.40	
	-				DC	150	9.90	10.00	150						1		ļ -								
WC18-20C			188052	4806	C		10.00	10.15		10.00	10.50	0.50	0.43	Powdered mudstone,	32.0%	5.53	0.87	56.29	13.14	29.70	0.52	-	-	1.81	
	-				DC CBSH	120	10.15 16.30	10.50 16.70	130	1	<u> </u>			coal, coaly rock	+		1							-	
WC18-20C	-		188053	4807	С	130 111	19.55	20.45	111	19.55	20.45	0.90	0.70	Dirty coal/Coal	84.4%	1.62	0.57	10.10	25.89	63.44	0.91	5.5	97.4	1.36	
WC18-20C	+		188054	4808	CR	1111	21.40	21.65	1111		21.65			Coaly mudstone	52.0%	1.02	0.57	34.97	16.99			2.0	98.3	1.58	
WC18-20C	<del> </del>		188055	4809	C	110	21.65	22.05	110					Dirty coal	95.0%	1.37	0.75		19.59			1.5	97.4	1.40	
					DC		22.05	22.40						İ	1 1					İ					
WC18-20C			188056	4810	C	101	22.40	22.65	101	22.05	22.65	0.60	0.52	Dirty coal / Coaly rock	93.3%	1.77	0.78	28.58	18.54	52.10	0.55	3.0	98.6	1.53	
			4000	1011	C		22.65	24.25			21.50			Coal/Coaly rock/Dirty	1				0.4.=0						
WC18-20C			188057	4811	DC	100	24.25	24.50	100	22.65	24.50	1.85	1.75	coal/powdered mudstone	66.5%	3.27	0.87	15.45	21.59	62.09	0.42	7.5	97.7	1.41	
WC18-20C			188058	4812	С	201	28.25	28.80	201	28.25	28.80	0.55	0.52	Dirty Coal/Coal	61.8%	4.37	0.79	18.15	21.37	59.69	0.56	7.5	97.1	1.41	
WC18-20C					CR		28.80	29.00		28.80	29.00	0.20	0.19	Carbonaceous mudst.	60.0%										
WC19 20C			188059	4813	С		30.55	30.75		20.55	20.02	0.27	0.27	Cool	70.49/	1 27	0.60	1.67	20.24	7/ 2/	0.57	4.0	97.1	1 22	
WC18-20C					CR	]	30.75	30.85		30.55		0.27	0.27		70.4%	1.27	0.68	4.67	20.34	74.31		4.0	37.1	1.32	
WC18-20C			188060	4814	DC	202	30.85	30.98	202	30.82	31.00	0.18	0.18	Carb. mudstone/Ash	83.3%	1.33		81.24	14.46	3.53	0.12	-	-	2.38	
WC18-20C			188061	4815	CR		30.98	31.07		31.00	31 32	0.32	0 31	Dirty coal/Coal	71.9%	3.17	0.66	17.80	20.47	61.07	0.57	7.0	98.0	1.42	
VVO 10-200				7010	DC		31.07	31.32		31.00	01.02	0.52	0.51	Dirty Coai/Coai											
					CBSH	310?	37.00	37.20	310?																
WC18-20C			188062	4816	С	300	41.70	42.35	300	41.70	42 45	0.75	0.70	Coal	49.3%	2.03	0.52	12.03	19.56	67.89	0.65	4.5	98.3	1.37	
VVO 10-200	ļ		100002	7010	DC		42.35	42.45		71.70	72.73	0.73	0.70	Jour	75.570	2.00	0.02	12.00	10.00	01.03	0.00	7.5	30.0	1.57	
					CBSH	320	44.65	44.85																	
WC18-20C			188063	4817	DC	430	70.65	71.10	430	70.65	71.10	0.45	0.44	Coaly mudstone	20.0%	0.72	0.53	25.32	16.03	58.12	0.78	1.0	98.8	1.52	

	Cross-reference composites	- 11	Head (raw)	samples	Geoph	ysical lo	g interpre	tation				Sample	e charac	eterisation			Head r	aw anal	ysis (air d	lried bas	sis unles	ss otherwis	se stated)		
Borehole	Dirtley Joh Com	nacita	Dietlov Joh	Cample			De	pth		Dep	oth	Thicl	kness		Core		Proxi	mate an	alysis			Addition	al analysi	s	Comments
	Birtley lab Com no. n	10.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-20C			188064	4818	_	440	74.00	74.00	440	74.20	74.27	0.07	0.07	Sub-canneloid coal/ash	100.0%	0.68	0.44	69.20	14.06	16.30	0.27	-	-	2.21	
WC18-20C			188065	4819	С	410	74.20	74.80	410	74.27	74.80	0.53	0.52	Sub-canneloid coal	86.8%	1.04	0.53	8.31	18.25	72.91	0.71	1.5	99.1	1.41	
WC18-20C			188066	4820	С	401	76.00	76.75	401	76.00	76.75	0.75	0.72	Coal	89.3%	1.67	0.57	6.25	19.63	73.55	0.63	1.5	98.6	1.35	
WC18-20C			188067	4821	С	400	82.42	83.00	400	82.42	83.21	0.79	0.73	Coal	50.6%	1.18	0.44	2.51	21.34	75.71	0.63	5.5	98.8	1.31	Interval from 83.42 to 83.55 was either entirely lost or was partly mixed in with sample 4822.
WC18-20C			188068	4822	DC		83.00	83.42		83.21	83.42	0.21	0.19	Ash/Coal	85.7%	3.54	0.41	22.96	18.36	58.27	0.39	1.5	98.3	1.48	Ash band from 83.26 to 83.28 included in sample
WC18-20C			188069	4823	C DC	420	83.55 83.70	83.70 83.80	420	83.55	83.85	0.30	0.28	Coal	83.3%	1.31	0.38	2.84	20.19	76.59	0.42	4.0	98.6	1.31	
WC18-20C			188070	4824	С	420	83.80	83.90	420	83.85	83.95	0.10	0.09	Ash/Coal	60.0%	0.78	0.53	65.32	15.42	18.73	0.12	1.0	99.1	2.06	Ash band from 83.80 to 83.84 included in sample
WC18-20C			188071	4825	С		84.95	85.30		84.95	85.30	0.35	0.34	Coal	74.3%	1.25	0.52	15.88	17.21	66.39	0.43	2.0	99.4	1.41	
					DC	440	85.30	85.40	440																
WC18-20C			188072	4826	С	"""	85.40	85.65	770	85.30	85.85	0.55	0.53	Ash/Coal	94.5%	1.13	0.54	26.71	18.99	53.76	0.41	2.0	98.3	1.52	From 85.30 to 85.35, ash band
					DC		85.65	85.85						-											
WC18-20C			188073	4827	DC	442	86.50	86.75	442	86.50	86.75	0.25	0.24	Coal	100.0%	1.86	0.61	8.13	21.56	69.70	0.66	7.5	99.1	1.33	
					CBSH	463	97.50	97.75																	
WC18-20C	<del>                                     </del>				CBSH CR	460	103.35	103.50 103.70	460	103.50	102.70	0.20	0.20	Cool	55.0%								-	-	
WC 16-20C					CBSH	400	103.50 103.70	103.70	400	103.50	103.70	0.20	0.20	Coai	35.0%							-		-	
					CBSH	483	106.40	106.75	483																
					C	700	109.15	100.75	700						+ +							+	<del> </del>	<del>                                     </del>	
WC18-20C			188074	4828	DC	480	109.45	109.60	480	109.15	110.20	1.05	0.98	Coal	83.8%	1.69	0.51	14.41	21.64	63.44	0.86	7.0	99.4	1.40	
				.020	C		109.60	110.20					0.00				""				""				
WC18-20C			188075	4829	DC		114.60	114.80		114.60	114.80	0.20	0.20	Coaly mudstone	85.0%	0.71	0.47	46.78	13.23	39.52	0.53	1.0	99.7	1.74	
WC18-20C			188076	4830	CR	A71	114.80	114.90	A71	114.80	114.95	0.15	0.15	Ash	100.0%	0.58	0.32	45.51	42.84	11.33	0.30	1.5	98.8	2.22	Very poor quality sample
WC18-20C			188077	4831	DC		114.90	115.00		114.95	115.15	0.20	0.20		80.0%	1.19	0.56	10.23	21.03	68.18	1.10	9.0	99.4	1.34	
WC18-20C			188078	4832	С	A7	117.70	117.95	A7	117.70	117.95	0.25	0.25	Coal & Carb siltstone	100.0%	1.28	0.67	29.81	17.59	51.93	0.75	7.5	99.4	1.55	
					CR	A72	119.20	119.45	A72																
					CBSH		125.30	125.80																	
					CR	A5	125.80	125.90	A5																
14/0/10 000			400070	1000	CBSH	10	125.90	126.15		100.75	100.15	0.40	0.00	D. ( 0 1/0 1	00.00/	4.00	0.54	40.04	10.00	00.50	0.00		00.4	1.05	
WC18-20C			188079	4833	DC	A3	132.75	133.15	A3	132.75	133.15	0.40	0.39	Dirty Coal/Coal	60.0%	1.30	0.51	10.31	19.66	69.50	0.99	7.5	99.1	1.35	The decident
WC18-20C			188080	4834	С	A1	135.50	136.15	A1	135.50					95.3%	1.09		12.21	19.37				99.4	1.40	The density tool was unable to pick the bottom of the seam, therefore thickness was changed
WC18-21C			188081	4835	DC	430	24.85	25.15	430					Coal/Coaly Rock	66.7%	2.65	0.66	20.26	17.30	61.78	0.93	1.0	97.7	1.49	
WC18-21C					CR		28.40	28.55		28.40	28.55	0.15	0.15	Siltstone	100.0%										

	Cross-refe		Head (raw)	samples	Geoph	ysical lo	g interpre	tation				Sample	e charac	cterisation			Head r	aw anal	ysis (air d	ried bas	sis unles	ss otherwis	se stated)		
Borehole	Birtley lab (	Composito	Dirtloy Joh	Cample			De	pth		Dep	oth	Thic	kness		Core		Proxi	mate an	alysis			Addition	nal analysi	S	Comments
	no.	no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-21C			188082	4836	С	410	28.55	29.35	410	28.55	29.35	0.80	0.78	Dirty Coal	20.0%	1.96	0.61	15.69	16.63	67.07	0.91	1.0	99.1	1.44	
WC18-21C			188083	4837	С	401	30.85	31.80	401	30.85	31.80	0.95		Coal/Dirty Coal	74.7%	7.22	0.73	7.39	19.15	72.73	0.70	1.5	93.1	1.36	
WC18-21C					CR		31.80	32.00		31.80	32.00	0.20	0.20	Carbonaceous siltstone	100.0%										
WC18-21C			188084	4838	DC	400	34.20 35.75	35.75 35.90	400	34.20	35.90	1.70	1.59	Coal/Dirty Coal	44.1%	2.28	0.52	8.06	20.92	70.48	0.49	6.0	97.7	1.34	
WC18-21C			188085	4839	C	420	35.90	36.05	420	35.90	36.08	0.18	0.17	Coal/Dirty Coal	100.0%	2.09	0.62	3.00	19.35	77.03	0.35	2.0	98.8	1.33	
WC18-21C				1000	CR		36.05	36.30	1=0	36.08	36.30				22.7%				70100	1	-			1100	
WC18-21C			188086	4840	С		37.10	37.40	440	37.10	37.55	0.45	0.42	Coal/Dirty Coal	84.4%	2.10	0.56	21.92	19.51	58.01	0.35	2.5	97.4	1.48	
WC18-21C			188087	4841	DC	440	37.40	37.70		37.55	37.65	0.10	0.09	Ash	50.0%	1.52	0.53	79.49	14.79	5.21	0.14	-	-	2.24	Ash band is consistently seen in
WC18-21C			188088	4842	С		37.70	38.00	440	37.65	38.00	0.35	0.33	Coal/Dirty Coal	91.4%	5.54	0.56	11.26	19.44	68.74	0.47	3.0	99.7	1.37	440 seam, thickness of the ash was picked off the resistivity log.
WC18-21C			188089	4843	С	442	38.80	39.10	442	38.80	39.10	0.30	0.28	Coal	100.0%	4.65	0.57	13.45	23.66	62.32	0.63	8.5	97.4	1.36	
WC18-21C			188222	4976	CBSH		55.05	55.25		55.05				Dirty coal	35.0%	1.27	0.49	15.61	29.89	54.01		7.0	98.3	1.46	Carbonaceous shale> dirty coal Fines that may have come from underneath the altered ashy layer are in this bag. Small mm-cm scale shards of carb.mdst were sorted out as best as possible.
WC18-21C			188223	4977	CR	460	55.25	55.40	460	55.25	55.40	0.15	0.14	Altered ash?	73.3%	0.42	0.23	63.62	40.86	<mark>-4.71</mark>	9.98			2.91	coaly rock> ash with high sulphide content
WC18-21C					CBSH		55.40	55.50		55.40	55.50	0.10	0.09	Missing coal? and carbonaceous mudstone pieces	0.0%										Small (mm-cm scale) carb.mdst pieces were found mixed in with the dirty coal an ash. Upper interval of the next unit has been ground out - any coal after the parting as well as carbonaceous mudstone lost in coring process?
					CBSH	483	57.90	60.00	483						0.0%										Ĭ.
WC18-21C			188224	4978	CBSH		60.55	60.70		60.55	60.70	0.15	0.15	Coaly rock	46.7%	0.39	0.39	40.89	20.57	38.15	2.37			1.80	There did not appear to be 15cm of carbonaceous shale in the box, hence wh I used this interval to describe the coaly rock seen in the box/core log. Large pieces of pyrite (2mm-3cm) were sorted out as best as possible however some of the finer pieces may have ended up in the
WC18-21C			188090	4844	С	480	60.70	61.55	480	60.70	61.55	0.85	0.79	Dirty coal/Coal	69.4%	2.23	0.42	17.71	23.29	58.58	1.21	7.0	98.0	1.45	bag.
WC18-21C			188225	4979	CDCII		64.00	GE 40		64.80	64.92	0.12	0.11	Dirty coal	91.7%	1.40	0.39	31.63	36.34	31.64	0.76	7.5	97.7	1.74	Carbonaceous shale> dirty coal and parting. Picks were changed in order to
WC18-21C			188226	4980	CBSH	A71	64.80	65.10	A71	64.92	65.10	0.18	0.17	Coaly-ashy rock?	88.9%	0.68	0.32	56.15	49.08	<mark>-5.55</mark>	0.18			2.76	accommodate for dirty coal and large parting - inconsistent width
WC18-21C			188091	4845	CR		65.10	65.30		65.10			0.19		105.0%	2.11	0.42	15.48	23.35	60.75	1.04	8.5	98.0	1.41	
WC18-21C					С	A7	67.70	68.20	A7	67.70	68.20	0.50	0.47	Carb. mudstone	72.5%		<u> </u>					ļ	ļ	ļ	
WC18-21C			188227	4981	DC	A72	69.10	69.50	A72	69.10	69.50	0.40	0.37	Pulverised coal and carbonaceous mudstone	25.0%	4.00	0.48	40.12	17.29	42.11	0.77			1.62	Sorted out carbonaceous mud-stone pieces as best as possible, however as the coal and carb.mdst is pulverised so fine there will be contamination.

	1	ference to	Head (raw)	) samples	Geoph	ysical lo	g interpret	tation				Sample	e charac	terisation			Head	aw anal	ysis (air d	ried bas	sis unles	s otherwis	se stated)		
Borehole			Dimboolah	Camania			De	pth		Dep	oth	Thick	kness		Core		Proxi	mate an	alysis			Addition	nal analysi	S	Comments
	no.	Composite no.	no.	Sample no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-22C			188092	4846	C DC	450	9.30 9.45	9.45 9.80	450	9.30	9.80	0.50	0.48	Coal	64.0%	4.43	1.27	16.72	21.80	60.21	0.93	1.5	70.2	1.46	Bottom ply was thickened
WC18-22C			188093	4847	CR	150	9.80	9.95	150	9.80	9.95	0.15	0.14	Siltstone	40.0%	3.22	1.05	67.48	10.53	20.94	0.28			2.06	because more coal in the core box than the picks indicated.
WC18-22C			188094	4848	DC CR		9.95 10.05	10.05 10.10		9.95	10.20	0.25	0.24	Coal	84.0%	3.92	0.43	36.76	16.96	45.85	0.66	0.5	84.1	1.62	Same situation for the coaly rock under the seam.
WC18-22C			188095	4849	CBSH		10.10	10.90		10.20	10.35		0.14	Carbonaceous siltstone	73.3%	3.22	0.99	54.32	12.69	32.00				1.88	dider the seam.
WC18-22C			188096	4850	CBSH	130	14.95	15.50	130	14.95	15.50			Dirty Coal	16.4%	8.11	0.74	52.50	14.88	31.88				1.84	
WC18-22C			188097	4851	С	111	18.20	19.15	111	18.20	19.15				100.0%	5.36	1.04	9.89	22.21	66.86		1.5	60.1	1.36	
WC18-22C			188098	4852	l c		20.85	21.30	440	20.85		0.15		Coal	26.7%	1.87	0.37	38.11	16.75	44.77		1.5	94.0	1.62	Coal interval broken into 2
WC18-22C			188099	4853	D0	110			110	21.00	21.30	0.30		Ash parting/Coal	80.0%	1.86	0.36	20.93	18.56	60.15		1.0	96.5	1.44	samples due to thin ash parting
WC18-22C WC18-22C			188100 188101	4854 4855	DC	101	21.30 21.60	21.60 22.05	101	21.30 21.60	21.60 22.05	0.30		Carb siltstone Dirty coal/coal	53.3%	2.14	0.71	60.68 13.80	10.95 18.90	27.66 66.85		3.5	96.0	1.89 1.39	Dirty coal actually carb siltstone
WC18-22C			188102	4856	C	101	22.05	23.70	101	22.05	23.50			<u>.                                      </u>	62.8%	4.59	0.45	5.92	22.38	71.25		7.5	93.4	1.31	
WC18-22C			188103	4857		100			100	23.50	23.80	0.30	0.29	Carbonaceous siltstone	73.3%	3.05	0.71	51.27	13.93	34.09	0.61			1.74	This interval was chosen based on the geophysical logs increase in density over ~30cm which is believed to correspond to the carb siltstone parting.
WC18-22C			188104	4858	DC		23.70	24.12		23.80	24.12	0.32	0.31	Pulverised coal and pulverised siltstone	75.0%	4.06	0.56	42.40	15.23	41.81	0.59			1.63	This interval includes the remaining coal of the 100 pick
WC18-22C			188105	4859	С	201	27.55	28.10	201	27.55		0.55		Coal	100.0%	2.36	0.48	15.85	22.41	61.26	0.67	7.0	97.7	1.38	
WC18-22C					CR		28.10	28.30		28.10		0.20		Carbonaceous siltstone	10.0%			ļ							Very carbonaceous siltstone.
WC18-22C			188106	4860	C	_	29.80	30.20	,	29.80	30.20	0.40	0.39	Coal	92.5%	2.19	0.33	9.69	19.06	70.92	0.67	2.5	98.8	1.34	
WC18-22C			188107	4861	CR		30.20	30.30		30.20	30.30	0.10		Carb siltstone	140.0%	1.43	0.47	80.62	12.39	6.52				2.33	14cm parting of carbonaceous siltstone and ash in box
WC18-22C			188108	4862	DC	202	30.30	30.40	202	30.30	30.40	0.10	0.10	Dull banded coal	150.0%	2.68	0.39	9.72	20.84	69.05	0.78	4.5	98.3	1.34	15cm dull banded coal in box
WC18-22C			188109	4863	DC CR		30.40	30.50		30.40	30.72	0.32	0.31	Carb siltstone	28.1%	2.67	0.72	82.09	6.96	10.23	0.18			2.27	Carbonaceous siltstone with ground bottom end. No dirty coal as in picks. Ground top end on sandy siltstone that follows
WC18-22C			188110	4864	С	300	42.60	43.10	300	42.60	43.10	0.50	0.50	Coal	94.0%	3.91	1.02	10.37	17.773	70.88	0.57	0.5	98.3	1.38	
WC18-22C			188111	4865	CR		43.10	43.35		43.10	43.35	0.25	0.25	Carbonaceous siltstone parting / coal	68.0%	3.63	0.70	13.17	18.43	67.70	0.61	0.5	97.4	1.38	1 cm parting with possible coaly rock
WC18-22C					CBSH CR CBSH	320	46.50 46.70 46.90	46.70 46.90 47.20	320	46.50	47.20	0.70		Carbonaceous siltstone interlayer with coal	65.7%										Interlayered carbonaceous muddy siltstone

	1	ference to	Head (raw)	) samples	Geoph	ysical lo	g interpre	tation				Sample	e charac	cterisation			Head r	aw anal	ysis (air d	ried bas	sis unles	ss otherwis	se stated)		
Borehole	Dirtley Joh	Composito	Dirtlov Joh	Cample			De	pth		Dep	oth	Thic	kness		Core		Proxi	mate an	alysis			Addition	nal analysi	s	Comments
	no.	Composite no.	no.	Sample no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-22C					CBSH		60.05	61.05		60.05	61.05	1.00	0.96	Carbonaceous siltstone, pyrite band, coal	73.0%										Interlayered carbonaceous siltstone/pyrite/minor coal
					R	340	61.05	64.60	340																
WC18-22C					CBSH	340	64.60	65.00	340	61.05	66.40	5.35	5.12	siltstone, mudstone	71.8%										
					R		65.00	65.85																	
					CBSH		65.85 66.40	66.40 75.10					-										1		
					CR		75.10	75.25						Coal, subcanneloid coaly			<del>                                     </del>							<b>.</b>	
WC18-22C			188242	4996	C	430	75.25	75.60	430	75.10	75.60	0.50	0.46	rock?	56.0%	1.09	0.36	17.70	17.47	64.47	0.97	2.0	99.1	1.43	
WC18-22C			188112	4866	CR		79.20	79.40		79.20	79.40	0.20	0.19	Coaly rock	40.0%	0.97	0.43	42.57	15.76	41.24	0.44			0.69	
WC18-22C			188113	4867	С	410	79.40	80.10	410	79.40	80.10	0.70	0.65	9 cm ash parting / 54 cm coal	90.0%	2.18	0.41	20.06	17.46	62.07	0.53	2.0	99.1	1.47	
					DC		81.65	81.85																	Coaly rock at base ground up with
WC18-22C			188114	4868	C	401	81.85	82.45	401	81.65	82.60	0.95	0.87	Coal / Dirty Coal	82.1%	2.09	0.52	4.34	19.51	75.63	0.39	2.5	97.4	1.31	dirty coal/coal. Not separable
WC18-22C			188115	4869	CR C	400	82.45 82.95	82.60 84.60	400	82.95	04.60	1 65	1.51	Coaly rock/dirty coal/coal	84.8%	1.73	0.50	6.44	23.40	69.66	0.20	6.0	98.0	1.33	,
					-		i		i					4 cm mudstone parting /	1										
WC18-22C			188116	4870	С	420	84.60	85.15	420	84.60	85.15	0.55	0.50	51 cm coal and dirty coal	100.0%	2.40	0.50	26.90	19.51	53.09	0.33	6.5	96.5	1.51	
WC18-22C					CR		85.15	85.40		85.15	85.40	0.25	0.23	Carbonaceous mudstone	56.0%										Carbonaceous mudstone; good coal above
WC18-22C			188117	4871	C DC		86.35 86.50	86.50 86.60		86.35	86.58	0.23	0.21	Coal	100.0%	1.39	0.43	19.42	18.07	62.08	0.42	1.5	96.3	1.45	440 coal above 4cm ash band parting (base of pick changed)
					С	440	86.60	86.70	440																Darting plus and below (top piets
WC18-22C			188118	4872	DC		86.70	86.85		86.58	87.15	0.57	0.72	Ash parting/Coal	61.2%	1.33	0.44	16.50	19.70	63.36	0.48	4.5	97.7	1.41	Parting plus coal below (top pick changed)
14040.000					С	110	86.85	87.15	440	20.00	00.00	0.00	0.07		100.00/										onangou,
WC18-22C					C CBSH	442 463	88.30 99.50	88.60 99.70	442 463	88.30	88.60	0.30	0.27	Coal	100.0%										
WC18-22C			188119	4873	CR	460	103.75	104.15	460	103.75	104 15	0.40	0.37	Dirty Coal	40.0%	1.10	0.23	16.16	27.60	56.01	0.95	8.5	97.4	1.46	Sampled as dirty coal
77010 220			100110	1070	CBSH	100	10.00	10.15	100	100.70	101.10	0.10	0.07	Dirty Cour	10.070	1.10	0.20	10.10	21.00	00.01	0.00	0.0	07.1	1.10	Campion do unity com
					R			10.30	1																
					CBSH	]	10.30	10.60																	
					R		10.60	11.50																	
					CBSH	340	11.50	11.65	340																
					R CBSH	-	11.65 14.60	14.60 15.10																	
					R	1	15.10	15.10																	
					CBSH		15.85	16.10																	

	Cross-ref	erence to osites	Head (raw)	samples	Geophy	ysical lo	g interpre	tation				Sample	e charac	cterisation			Head r	aw anal	ysis (air d	Iried bas	is unles	s otherwis	se stated)		
Borehole	Dirtley Joh	Composito	Birtley lab	Cample			De	pth		Dep	oth	Thic	kness		Core		Proxi	mate an	alysis			Addition	nal analysi	S	Comments
	no.	no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-23C			188120	4874	CR		30.60	30.80		30.60	30.80	0.20	0.19	Coaly rock	75.0%	1.72	0.84	15.52	17.98	65.66	0.93	0.5	97.7	1.43	Sampled as upper shoulder to missing coal
WC18-23C					С	430	30.80	31.15	430	30.80	31.15			Not recovered	0.0%										
WC18-23C			188121	4875	CR		34.90	35.05		34.90	35.05			Coaly mudst. / dirty coal	66.7%	0.93	0.53	13.44	17.67	68.36		2.0	99.4	1.41	
WC18-23C			188122	4876	С	410	35.05	35.80	410	35.05	35.80	0.75	0.65	Coal	41.3%	1.52	0.56	4.05	18.90	76.49	0.62	2.5	98.0	1.33	
WC18-23C					CR		35.80	35.95		35.80	35.95	0.15	0.13	Carbonaceous mudst.	20.0%										No apparent coaly rock at base, Coal shattered at base in contact with shattered carbonaceous mudstone
WC18-23C			188123	4877	CR		37.15	37.40		37.15	37.40	0.25	0.23	Coaly rock	20.0%	0.99	0.49	37.56	14.46	47.49	0.28	1.5	98.8	1.64	
WC18-23C			188124	4878	C DC	401	37.40 38.05	38.05 38.30	401	37.40	38.30	0.90	0.85	Coal	28.9%	2.06	0.70	3.16	19.74	76.40	0.39	1.0	98.3	1.30	
WC18-23C			188125	4879	CR		38.30	38.45		38.30	38.45	0.15	0.14	Dirty coal/Coaly mudst.	33.3%	2.00	0.97	67.62	9.00	22.41	0.16			2.03	
WC18-23C			188126	4880	C DC	400	38.45 39.80	39.80 39.90	400	38.45		1.45		Coal/dirty coal	73.1%	1.97	0.70	7.71	22.75	68.84	0.34	3.0	98.0	1.37	Alternating clean/dirty coal, with very dirty looking last 10cm (dirty coal). Ground up coal at start of box 19 clean (420?)
WC18-23C			188127	4881	С	420	39.90	40.32	420	39.90	40.32	0.42	0.39	Coal	21.4%	1.25	0.32	5.21	22.17	72.30	0.39	7.0	97.4	1.30	
					CBSH	440	40.75	40.90	440																
					CBSH	442	41.60	41.85	442																
WC18-23C					CR		41.85	42.05		41.85	42.05	0.20	0.19	Coal	60.0%										
					CBSH	463	52.85	53.35	463																
WC18-23C					CBSH	460	57.70	58.03	460	57.70	58.03	0.33	0.32	Coal	81.8%										
					CBSH	483	61.70	62.10																	
					С		65.35	65.70																	
					DC		65.70	65.85																	
WC18-23C			188128	4882	С	480	65.85	65.90	480	65.35	66.20	0.85	0.82	Dirty coal	50.6%	1.92	0.56	17.62	27.42	54.40	0.81	7.5	97.4	1.48	
					DC		65.90	66.00																	
111010 000			100100	4000	U		66.00	66.20		20.00	00.40	0.00	0.40		05.00/	0.00	0.50	00.40	00.50		0.04		-		
WC18-23C			188129	4883	CR		66.20	66.40		66.20	66.40	0.20	0.19	Coaly rock	25.0%	0.93	0.59	68.18	23.52	7.71	0.24			2.36	
			400400	4004	DC	410	3.95	4.20	410				, ,,		00.40/			40.50	40.50						Unit completely crushed at top of
WC18-24C			188130	4884	C		4.20	5.05		3.95	5.35	1.40	1.19	Coal	32.1%	8.44	2.74	10.50	18.50	68.26	0.67	0.0	32.0	1.42	hole with casing; coaly rock included as indecipherable
WC18-24C					CR CR		5.05 8.15	5.35 8.50		8.15	8.50	0.35	0.30	Carbonaceous mudstone?	20.0%										Ground end of mudstone. Coaly rock likely carbonaceous
WC18-24C			188131	4885		401	8.50	10.00	401	8.50	10.00	1.50	1.27	Coal	42.0%	3.48	0.41	3.29	10.76	76.54	0.44	2.0	97.4	1.30	mudstone.
					C		10.00	12.15						1									1		
WC18-24C			188132	4886	DC	400	12.15	12.13	400	10.00	12.35	2.35	1.99	Coal/Dirty coal	55.7%	3.55	0.54	5.12	20.63	73.71	0.46	4.0	98.3	1.31	

	Cross-refere composit		Head (raw)	samples	Geoph	ysical lo	g interpre	tation				Sample	e charac	cterisation			Head r	aw anal	ysis (air d	ried bas	sis unles	s otherwis	se stated)		
Borehole	Birtley lab Co	mnaaita	Dirtley Joh	Comple			De	pth		Dep	oth	Thick	kness		Core		Proxi	mate an	alysis			Addition	nal analysi	S	Comments
	no.	no.	no.	Sample no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent )	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-24C			188133	4887	С		12.35	12.70		12.35	12.70	0.35	0.30	Coal	62.9%	3.53	0.81	6.56	21.87	70.76	0.47	8.0	82.0	1.30	
WC18-24C			188134	4888	DC C	420	12.70 12.80	12.80 12.95	420	12.70	12.95	0.25	0.21	Ash band/coal	32.0%	2.15	0.25	69.30	15.07	15.38	0.14			2.14	
WC18-24C					CR		12.95	13.20		12.95	13.20	0.25	0.21	Carb mudstone	100.0%										High carbon content mudstone with ground end.
WC18-24C			188135	4889	CR		14.40	14.60		14.40	14.60	0.20	0.19	(Coal-Coaly mudstone?)	20.0%	0.99	0.28	5.29	18.98	75.45	0.52	2.5	98.0	1.35	
WC18-24C			188136	4890	С	440	14.60	14.80	440	14.60	14.80		0.19		100.0%	1.73	0.53	8.20	19.28	71.99		3.5	99.1	1.33	Sampled as part of larger 440 seam (2 samples due to parting)
WC18-24C			188137	4891	DC	1 440	14.80	14.90	440	14.80	14.90			Dirty coal with ash	80.0%	7.82	0.48	39.72	18.30	41.50		4.5	98.8	1.63	
WC18-24C			188138	4892	C	110	14.90	15.45	110	14.90	15.45			Ash band/coal	65.5%	2.27	0.83	16.54	18.58	64.05		1.0	98.6	1.43	
WC18-24C			188139	4893	DC	442	17.50	17.90	442	17.50	17.90	0.40	0.37	Coal	70.0%	460	0.68	7.55	21.43	70.34	0.99	2.5	95.4	1.32	
WC18-24C			188140	4894	CBSH DC	463 460	26.60 31.35	27.00 31.70	463 460	31.35	21 70	0.35	0.34	Cool	40.0%	4.00	0.32	21.59	27.49	50.60	1.82	6.5	99.4	1.53	
VVC 10-24C	+		100140	4094	CBSH	483	35.10	35.35	483	31.33	31.70	0.55	0.54	Coai	40.076	4.00	0.32	21.59	21.43	30.00	1.02	0.5	33.4	1.55	
WC18-24C			188141	4895	C	480	41.50	42.50	480	41.50	42.50	1.00	0.98	Coal	48.0%	3.77	0.52	19.57	25.13	54.78	0.99	7.0	97.7	1.47	
WC18-24C					CR		46.65	46.90		46.65	46.90	0.25		Siltstone with coal spars	100.0%	-									Minor coal spars and coalified wood only.
WC18-24C			188142	4896	С	A71	46.90	47.25	A71	46.90	47.25	0.35	0.34	Dirty Coal	45.7%	2.03	0.58	24.49	29.84	45.09	0.83	1.5	95.7	1.59	Sampled as combined with the coaly rock it is thick enough
WC18-24C			188143	4897	С	A7	48.85	49.20	A7	48.85	49.20	0.35	0.33	Coal	34.3%	2.96	0.55	22.74	18.12	58.59	0.97	1.0	96.8	1.47	Sampled as combined with the
WC18-24C			188144	4898	CR	Ai	49.20	49.30	A/	49.20	49.30	0.10	0.09	Coal (laminated)	70.0%	2.82	0.88	25.68	18.54	54.90	0.88	0.5	98.3	1.69	coaly rock it is thick enough
					CBSH		49.80	50.00														-			
					CR	A72	50.00	50.15	A72						-							-			
					CBSH CR	A5	50.15 58.05	50.35 58.25	A5													-			
WC18-24C			188145	4899	DC	A3	64.10	64.50	A3	64.10	64.50	0.40	0.39	Coaly mudstone / Dirty Coal / Coal	50.0%	1.93	0.42	45.96	15.20	38.42	0.76	5.0	98.8	1.72	
		İ			CBSH	170	6.55	6.90	170													<u> </u>			
WC18-25C			188146	4900	С	150	14.95	15.10	150	14.95	15.10	0.15	0.14	Dirty Coal	60.0%	1.54	0.35	23.49	22.55	53.61	0.87	6.5	97.7	1.47	Sampled as part of the larger 150 total seam
WC18-25C			188147	4901	DC C	150	15.10 15.20	15.20 15.60	150	15.10	15.60	0.50	0.46	Ash parting/coal	22.0%	1.64	0.41	32.27	22.22	45.10	0.79	7.5	96.8	1.54	
WC18-25C					CR		15.60	15.90		15.60	15.90	0.30	0.28	Mudst with coal spars	36.7%										Coal spar rich mudstone
WC18-25C					CR	130	20.80	21.05	130	20.80				Mudst and coal powder	96.0%										Coal fragments mixed with mudstone
WC18-25C		Ţ	188148	4902	С	111	23.60	24.30	111					Coal/Dirty Coal	100.0%	2.33	0.51	6.20	24.10			7.0	97.1	1.34	
WC18-25C			188149	4903	CR	110	25.20	25.45	110					Dirty Coal	48.0%	1.96	0.54	9.80	22.72			6.5	94.5	1.35	
WC18-25C			188150	4904	C		25.45	26.12						Dirty Coal/Coal	82.1%	2.03	0.47	10.32	20.39			2.0	95.7	1.37	
WC18-25C			188151	4905	L C	101	26.12	26.60	101	26.12	26.60	0.48	0.44	Coaly Rock/Coal	83.3%	1.87	0.64	9.56	22.12	67.58	0.57	3.0	98.0	1.37	

	Cross-reference composites	e to H	lead (raw)	samples	Geoph	ysical lo	g interpret	ation				Sample	e chara	cterisation			Head r	aw anal	ysis (air d	ried bas	is unles	s otherwis	se stated)		
Borehole	Birtley lab Comp	osito B	Pirtlov Joh	Sample			De	pth		Dep	oth	Thicl	kness		Core		Proxi	mate an	alysis			Addition	nal analysi	S	Comments
	no. no		no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-25C			188152	4906	С	100	26.60	28.50	100	26.60	28.50	1.90	1.75	Coal/Dirty Coal	67.9%	2.74	0.63	3.49	24.84	71.04	0.44	8.0	96.8	1.29	
WC18-25C					CR		28.50	29.10		28.50	29.10	0.60	0.55	ash band/trace coal grindings/carb mudstone	80.0%										Carbonaceous mudstone beneath the ash band.
WC18-25C			188153	4907	DC C	201	32.10 32.25	32.25 32.80	201	32.10	32.80	0.70	0.64	Dirty Coal/Coal	100.0%	5.09	0.38	23.96	20.24	55.42	0.52	6.5	95.7	1.46	
WC18-25C					CR		32.80	33.10		32.80	33.10	0.30	0.27	Carbonaceous mudstone	33.3%										Carbonaceous mudstone at base.
					DC	1	34.60	34.80																	
WC18-25C			188154	4908	С	1	34.80	35.03		34.60	35.23	0.63	0.61	Coal/Dirty Coal	52.4%	1.49	0.36	5.93	20.49	73.22	0.58	3.5	98.0	1.32	
					DC	202	35.03	35.23	202													-			Culit as an as mula hatus as 20
WC18-25C			188157	4911	R		35.23	35.40		35.23	35.40			Muddy siltstone/Ash band	100.0%	1.45	0.68	65.88	13.47	19.97		1.5	98.6	2.06	Split seam sample between 20- 35cm
WC18-25C			188155	4909	С		35.40	35.65		35.40		0.25		Coal	100.0%	1.34	0.15	7.15	25.68	67.02	0.65	7.0	95.7	1.31	
WC18-25C		-			CR	300	50.80	51.00	300	50.80	51.00	0.20	0.19		25.0%							-			
		-+			CBSH	320	53.05	53.60	320													-		-	
WC18-25C			188156	4910	DC	430	81.00 81.18	81.18 81.45	430	81.00	81.45	0.45	0.44	Coal/Coaly mudstone	75.6%	1.82	0.63	20.64	16.84	61.89	0.82	1.5	96.2	1.46	
WC18-25C			188158	4912	CR		85.15	85.35		85.15	85.35	0.20	0.20	Ash band, Coaly mudstone/Dirty coal	90.0%	1.13	0.64	29.90	16.29	53.17	0.48	0.5	99.1	1.57	
WC18-25C		+	188159	4913	С	410	85.35	86.18	410	85.35	86.18	0.83	0.82	Coal	24.1%	1.80	0.67	5.00	18.29	76.04	0.65	2.0	97.1	1.33	
WC18-25C	1		188160	4914	С	401	87.38	88.40	401	87.38	88.40		1.00		78.4%	2.00	0.59	4.26	20.83	74.32		3.5	96.2	1.31	
WC18-25C			188161	4915	C		90.75	92.10		90.75	92.10		1.32		98.5%	2.08	0.42	2.27	20.95	76.36		6.0	96.8	1.28	
WC18-25C			188162	4916	DC	400	92.10	92.60	400	92.10	92.60	0.50		Coal Dust/Drill Mud	40.0%	10.40	0.40	43.37	17.02	39.21		1.5	96.8	1.66	
WC18-25C			188163	4917	С	420	92.60	92.80	420	92.60	92.80	0.20	0.20	Coal	50.0%	10.95	0.40	8.87	19.31	71.42	0.44	2.5	98.3	1.33	
WC18-25C			188164	4918	DC	420	92.80	93.00	420	92.80	93.00	0.20	0.20	Ash Band/Coal	95.0%	1.72	0.48	27.91	19.36	52.25	0.36	6.5	98.6	1.50	
WC18-25C			188165	4919	CR		94.05	94.35		94.05	94.35	0.30	0.30	Coaly mudstone	100.0%	1.74	0.71	15.86	18.75	64.68	0.51	3.0	99.7	1.40	
WC18-25C			188166	4920	DC C	440	94.35 94.70	94.70 95.10	440	94.35	95.10	0.75	0.74	Ash parting/Dirty coal	68.0%	2.18	0.75	18.11	18.22	62.92	0.53	3.0	99.4	1.40	
WC18-25C			188167	4921	С	442	96.00	96.45	442	96.00	96.45	0.45	0.44	Dirty Coal/Coal	57.8%	2.38	0.36	12.90	21.05	65.69	0.83	9.0	99.7	1.33	
					CBSH	463	105.70	105.95	463																
					CBSH		111.20	111.40																	
WC18-25C					CR	460	111.40		460	111.40	111.55	0.15	0.15	Coal, ash parting, coal	173.3%										
					CBSH		111.55																		
		$\perp$			CBSH	483	114.90		483						1.2.2.2.2									<u> </u>	
WC18-25C			188168	4922	CR		118.55			118.55	118.65	0.10	0.10	Coal	100.0%	3.24	0.23	25.91	28.13	45.73	0.69	5.0	97.7	1.55	
WC18-25C			188169	4923	DC C	480	118.65 118.98	118.98 119.50	480	118.65	119.50	0.85	0.84	Ash/Dirty coal/Coal	63.5%	2.06	0.44	26.33	21.35			6.0	98.3	1.48	
WC18-25C			188170	4924	С	A71	124.00	124.48	A71	124.00	124.48	0.48	0.45	Coal	95.8%	3.11	0.37	15.47	20.50	63.66	0.99	9.0	98.0	1.34	
WC18-25C					DC	A7	126.75	127.07	A7	126.75	127.07	0.32	0.30	Coal	75.0%										

	Cross-reference composites	O Head (ra	w) sample	s Geoph	nysical lo	g interpre	tation				Sample	e charac	cterisation			Head r	aw anal	ysis (air d	Iried bas	sis unles	s otherwis	se stated)		
Borehole	Birtley lab Compo	sito Birtlov la	h Samal			De	pth		Dep	oth	Thick	ness		Core recovery		Proxi	mate an	alysis			Addition	nal analysi	S	Comments
	no. no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	(percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-25C		188171	4925	CR	A72	128.40	128.80	A72	128.40	128.80	0.40	0.40	Coaly rock and Coal	37.5%	3.57	0.36	22.09	19.03	58.52	0.91	7.5	97.7	1.41	
WC18-25C				CR	A5	135.40	135.60	A5	135.40	135.60	0.20	0.20	Coal	45.0%										
				CBSH	320	2.70	3.00	320																
				CBSH		18.70	18.80	240																
WC18-26C				CR	_	18.80	18.95	340	18.80	18.95	0.15	0.13	Coal	60.0%										
				CBSH	340	18.95	19.10	]																
				R		19.10	22.60																	
WC18-26C				CBSH		22.60	22.80		22.60				Carbonaceous siltstone	25.0%					ļ					
WC18-26C				CBSH	430	29.40	29.85	430	29.40	29.85	0.45	0.44	Canneloid? mudstone	13.3%					ļ					
WC18-26C		188172	4926	CR	none	34.00	34.25	410	34.00	34.90	0.90	0.87	Coal	25.6%	1.11	0.55	20.01	17.66	61.78	0.57	1.5	97.1	1.43	Majority of coal destroyed in coring process. Sampled with coaly rock above as mixed together subrounded fragments
				С	410	34.25	34.90																	
WC18-26C		188173	4927	С	401	36.30	37.15	401	36.30	37.15	0.85	0.82	Coal	96.5%	1.88	0.94	6.97	19.73	72.36	0.56	4.0	98.6	1.34	
				С	400	42.30	43.40	400																
				С		43.40	43.65	]																Almost total core loss. Combined
WC18-26C		188174	4928	DC	420	43.65	43.75	420	42.30	44.20	1.90	1.68	Coal/Ash	11.1%	1.35	0.56	5.16	19.27	75.01	0.54	2.0	99.4	1.32	all units/seams
				С		43.75	43.90		_															a
				CR		43.90	44.20								. = -									
WC18-26C		188175		<u> </u> с	440	45.00	45.75	440	45.00		0.16			100.0%	1.76	0.49	10.34	18.73	70.44		3.5	98.8	1.36	Divided coal unit due to parting
WC18-26C		188176	4930					440	45.16				Ash/Coal	100.0%	1.55	0.69	14.18	18.37	66.76	0.46	1.5	99.1	1.39	
WC18-26C				C	442	46.30	46.65	442	46.30	46.65	0.35	0.31	Coal	97.1%					-					
				CBSH	460	62.70	63.05	460									-		-	-				
WC10 06C		188177	4931	CBSH	483	65.25	65.85	483	60.50	60.40	0.00	0.07	Coal/Dirty coal	42.2%	1 10	0.42	17.01	10.00	60.74	0.01	2.0	00.0	1.44	
WC18-26C WC18-26C		188178		DC	480	68.50 69.40	69.40 69.50	480					Coaly rock	100.0%	1.19 1.54	0.43	17.91 18.78	18.92	62.74 62.78		3.0 6.0	98.8 99.1	1.44	
WC18-26C	1	100170	4932	CR	A71	74.30	74.60	A71	74.30				Coaly mudst. and coal	36.7%	1.04	0.30	10.70	10.00	02.76	0.07	0.0	99.1	1.41	
		-		DC		78.45	78.65		1			i	1				<del>                                     </del>	-					1	
WC18-26C			$\dashv$	C 20	- A7	78.65	78.75	A7	78.45	78.75	0.30	0.28	Not recovered	0.0%		1		<del>                                     </del>	-	$\vdash$		<del>                                     </del>	<del>                                     </del>	-
WC18-26C	+ + + - +	188179	4933	CR	A72	79.90	80.30	A72	79 90	80.30	0.40	0.38	Dirty Coal/Coal	37.5%	1.01	0.65	19.71	18.35	61 29	0.92	6.5	99.4	1.44	
11010-200		100173	1300	CBSH	A5	86.35	87.20	A5	7 0.00	00.00	0.70	0.00	Dirty Councoun	01.070	1.01	0.00	10.71	10.00	01.23	0.02	1 0.0	33.4	1.77	
WC18-26C				DC	A3	94.20	94.45	A3	94.20	94.45	0.25	0.22	Coal	60.0%		1								
WC18-26C		188180	4934	C	A1	96.35	96.95	A1	96.35	96.95	0.60	0.56	Coal/Dirty Coal	46.7%	1.20	0.39	21.55	16.40	61.66	0.76	2.0	99.7	1.47	
			1	CBSH	†	11.45	11.65							1								1	1	
				CR	170	11.65	11.75	1						<u> </u>										
				CBSH	1	11.75	12.00	1										1						
WC18-27C				С	150	18.75	19.60	150	18.75	19.60	0.85	0.74		0.0%										
WC18-27C	1	188181	4935	CR	none	19.60	19.80		19.60				Ash/Coal	60.0%	1.22	0.39	25.32	22.16	52.13	0.87	7.0	98.3	1.49	

	Cross-refere composit		Head (raw)	samples	Geoph	ysical lo	g interpre	tation				Sample	e charac	cterisation			Head r	aw anal	ysis (air d	ried bas	is unles	ss otherwis	se stated)		
Borehole	Birtley lab Cor	mnosita	Rirtley lah	Sample			De	pth		Dep	th	Thicl	kness		Core		Proxi	mate an	alysis			Addition	nal analysi	s	Comments
	1	no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	(percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
					CBSH	130	24.10	24.60	130																
WC18-27C			188182	4936	С	111	27.05	28.00	111	27.05	28.00	0.95	0.92	Coal	89.5%	1.70	0.46	9.45	23.45	66.64	0.77	8.0	97.4	1.35	
WC18-27C			188183	4937	С	110	28.70	29.00	110	28.70	28.96	0.26	0.25	Dirty Coal	38.5%	1.40	0.48	27.95	19.96	51.61	2.03	3.5	98.3	1.54	Changed pick - more of a dirty coal than coal
WC18-27C			188184	4938	DC C	110	29.00 29.10	29.10 29.35	110	28.96	29.35	0.39	0.38	Ash band/Coal	100.0%	1.21	0.50	14.40	20.96	64.14	0.50	3.0	98.6	1.40	
					DC		29.35	29.50	,																
WC18-27C			188185	4939	С	101	29.50	29.65		29.35	29.81	0.46	0.44	Dirty Coal/Coal	97.8%	1.82	0.46	12.19	23.81	63.54	0.37	2.0	99.1	1.44	
					DC	] '''	29.65	29.80	101																Changed pick. Matches well with
WC18-27C			188186	4940	C		29.80	29.95		29.81	31.50	1.69	1.63	Coal	100.0%	1.41	0.41	3.46	24.52	71.61	0.42	8.0	98.3	1.29	coal characteristics and logging
					C DC	100	29.95	31.50	400														-		_
WC18-27C WC18-27C			188187	4941		nana	31.50	31.55 31.75	100	31.50				Ashy siltstone/Coal	100.0%	2.49	0.43	53.18	15.31	31.08	0.34			1.81	Carbanassassasiltatana
WC18-27C					CR CR	none	31.55 34.70	34.90		31.62 34.70		0.13			100.0% 15.0%							-	+	<u> </u>	Carbonaceous siltstone Carbonaceous siltstone
					C		34.70	35.30		34.70			0.19		i								<del> </del>		Carbonaceous sitistorie
WC18-27C			188188	4942	DC	201	35.30	35.45	201	34.90	35.45		0.53		29.1%	4.94	0.31	6.98	23.42	69.29		6.5	97.4	1.31	
WC18-27C			188189	4943	CR	none	35.45	35.60		35.45	35.60	0.15		Coaly rock	46.7%	0.93	0.48	37.26	17.79	44.47	0.38	5.5	98.6	1.63	
WC18-27C					DC		36.95	37.15		36.95	37.15				0.0%										
WC18-27C					U	202	37.15	37.30	202	37.15		0.15			0.0%										<u> </u>
WC18-27C					DC	_	37.30	37.85		37.30	37.85	0.55	0.53		0.0%							-	-	ļ	Destruction Coallity mixed
WC18-27C			188190	4944	CR	300	53.20	53.35	300	53.20	53.35	0.15	0.14	Coal/mixed coal and mud	93.3%	6.86	0.60	72.80	8.72	17.88	0.23			2.14	Destroyed core. Coal bits mixed with mud
MC40 07C					CBSH	200	56.75	56.97 57.12	200	EC 07	E7 40	0.15	044		66.70/					-			-		Coulo ano access dilitatana
WC18-27C					CR CBSH	320	56.97 57.12	57.12	320	56.97	57.12	0.15	0.14		66.7%								+		Carbonaceous siltstone
	<del>                                     </del>				CBSH		71.10	71.50															+		
	+ +				R	1	71.50	74.10					<del>                                     </del>							<del>                                     </del>		<del>                                     </del>	+	<del>                                     </del>	
					R	340	74.35	75.10	340													1	<del>                                     </del>	1	
					CBSH	1	75.10	75.50															†		
WC18-27C			188191	4945	C	430	82.05	82.45	430	82.05	82.45	0.40	0.39	Dirty Coal/Coal	75.0%	2.82	0.49	19.32	17.47	62.72	0.81	2.5	97.1	1.45	
WC18-27C			188192	4946	C	410	86.85	87.40	410	86.85					83.6%	1.78	0.57		18.03			1.0	99.4	1.36	
WC18-27C					CR		87.40	87.70						Coal/coaly rock particles	26.7%										The last 5cm was crushed (coal and coaly rock particles) and the next mudstone unit not carb
WC18-27C			188193	4947	С	401	88.55	89.45	401					Coal, dirty coal	44.44%	2.28	0.33		19.63			2.0	99.7	1.33	
WC18-27C			188194	4948	С	400	95.35	96.08	400	95.35	96.08	0.73	0.70	Coal	86.30%	1.29	0.28	4.33	20.45	74.94	0.63	4.5	99.1	1.31	
WC18-27C			188195	4949	C DC	420	96.08 96.30	96.30 96.45	420	96.08	96.45	0.37	0.35	Coal	48.65%	1.90	0.48	12.15	21.33	66.04	0.56	8.0	96.8	1.36	

	1	ference to osites	Head (raw)	samples	Geoph	ysical lo	g interpre	tation				Sample	charac	eterisation			Head	raw anal	ysis (air d	ried basi	s unles	s otherwis	se stated)		
Borehole	Dirtlov loh	Composite	Dirtloy lob	Cample			De	pth		Dep	oth	Thick	ness		Core		Prox	imate an	alysis			Addition	al analysis	S	Comments
	no.	no.	no.	no.	Lithology	Bed	From (m)	To (m)	Bed	From (m)	To (m)	Appar- ent	True	Lithological details	recovery (percent	Mar	Mad	Aad	VMad	FCad	Sad	FSlad	%LT	SGad	
WC18-27C			188196	4950	DC C	440	97.80 98.15	98.15 99.00	440	97.80	99.00	1.20	1.18	Coaly Ash/Dirty Coal	29.17%	1.68	0.59	26.47	18.04	54.90	0.44	2.5	98.3	1.51	It is possible the coring process destroyed the whole 440 coal seam and this is just the dirty coal upper portion.
WC18-27C			188243	4997	С	442	99.50	99.75	442	99.45	99.85	0.40	0.39	Coal	97.50%	1.58	0.48	17.26	19.39	62.87	0.60	7.5	98.6	1.40	Changed pick from 99.5 to 99.75, to 99.45 to 99.85 due to amount of coal in box
					CBSH	460	116.95	117.30	460						48.6%										
					CBSH	483	120.55	121.00	483						100%										
WC18-27C			188244	4998	CR		123.95	124.20		123.95	124.20	0.25	0.24	Dirty Coal	68.0%	0.85	0.52	37.85	15.29	46.34	0.52	1,0	98.8	1.67	
WC18-27C			188245	4999	DC C	480	124.20 124.35 124.50	124.35 124.50 125.00	480	124.20	125.00	0.80	0.77	Coal/Dirty Coal	0.00%	1.19	0.48	12.24	23.29	63.99	0.97	8.0	98.8	1.39	
WC18-27C			188246	5000	CR	A71	129.00	129.20	A71	129.00	129.20	0.20	0.19	Coaly Ash	85.00%	0.40	0.29	38.20	40.63	20.88	0.52	1.5	98.8	1.97	
WC18-27C			188247	5251	DC	A/ I	129.20	129.40	A/I	129.20	129.40	0.20	0.19	Coal	30.00%	0.66	0.39	12.41	23.02	64.18	1.15	8.5	98.3	1.37	
WC18-27C			188248	5252	DC		133.05	133.30		133.05	133.30	0.25	0.24	Coal	20.00%	1.02	0.45	12.82	19.60	67.13	1.01	8.0	98.6	1.36	Crushed sample. Looks like chunks of coaly rock in with coal
WC18-27C			188249	5253	CR	A7	133.30	133.45	A7	133.30	133.45	0.15	0.14	Carb. mudstone	13.33%	1.50	0.67	80.15	6.70	12.48	0.15			2.24	Sampled as possibly the very end of coaly rock. Likely coaly rock in sample 5252
WC18-27C			188250	5254	CR	A72	134.50	134.88	A72	134.50	134.88	0.38	0.36	Coal/mudstone	10.53%	3.43	0.50	53.06	13.83	32.61	0.52			1.80	Seam lost to coring process.  Tried to separate out coal shards from mudstone shards

Willow 2018 borehole head analyses\_190313e.doc



CLIENT:

CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

PO#:

326969WC

HOLE:

WC18-01C

LAB#:

186371-380

REPORT DATE:

November 14, 2018

Coreceted December 31,2018

Gwil Industries Inc.

7784 - 62nd St SE Calgary, AB T2C 5K2

Tel: (403) 253-8273 Email: info@birtley.ca

www.birtley.ca

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

LAB#	Sample	Wet	Dry	Retain	ADM%	W ANALYSIS, MOIST%	ASH%	VOL%	F.C.%	S%	FSI	0/17		DAOIG
	ID:	Wt(g)	Wt (g)	Wt (g) 7/8	7121170		A01170	VOL /6	1.0.70	3/0	FOI	%LT	SG	BASIS
186371	4501	678	655	561	3.39	0.67	37.97	30.58	30.78	0.59	1.5	94.8	1.81	adi
						4.04	36.68	29.54	29.74	0.57				art
							38.23	30.79	30.99	0.59				di
186372	4502	6227	6161	5357	1.06	0.72	4.09	21.35	73.84	0.54	3.0	97.4	1.32	adt
						1.77	4.05	21.12	73.06	0.53				art
							4.12	21.50	74.38	0.54				dk
186373	4503	276	272	238	1.45	0.66	11.25	19.05	69.04	0.52	2.0	98.0	1.40	adb
						2.10	11.09	18.77	68.04	0.51				arb
							11.32	19.18	69.50	0.52				db
186374	4504	1369	1362	1165	0.51	0.86	69.74	9.90	19.50	0.24	-		2.07	adb
				-		1.37	69.38	9.85	19.40	0.24				arb
							70.34	9.99	19.67	0.24				db
186375	4505	244	242	217	0.82	0.83	50.15	13.94	35.08	0.43	-	-	1.82	adb
						1.64	49.74	13.83	34.79	0.43				arb
							50.57	14.06	35.37	0.43				db
186376	4506	1621	1595	1405	1.60	0.76	12.41	18.23	68.60	0.72	2.0	96.5	1.38	adb
						2.35	12.21	17.94	67.50	0.71				arb
							12.51	18.37	69.13	0.73				db
186377	4507	2795	2704	2355	3.26	0.76	19.51	20.10	59.63	0.42	6.5	98.3	1.42	adb
_						3.99	18.87	19.45	57.69	0.41				arb
							19.66	20.25	60.09	0.42				db
86378	4508	333	314	270	5.71	0.74	17.77	18.56	62.93	0.69	4.0	98.3	1.42	adb
-						6.40	16.76	17.50	59.34	0.65				arb
							17.90	18.70	63.40	0.70				db
86379	4509	2570	2545	2204	0.97	0.66	14.92	24.89	59.53	0.90	7.0	94.8	1.44	adb
						1.63	14.77	24.65	58.95	0.89				arb
							15.02	25.06	59.93	0.91				db
86380	4510	999	988	850	1.10	0.64	13.67	17.82	67.87	0.87	3.0	98.6	1.39	adb
				1		1.73	13.52	17.62	67.12	0.86				arb
							13.76	17.93	68.31	0.88				db

<sup>\*</sup>Prox & SG checked

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CLIENT:

CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

PO#:

326969WC

HOLE:

WC18-02C

LAB#:

186381-394

REPORT DATE:

November 14, 2018

Gwil Industries Inc. 7784 - 62nd St SE Calgary, AB T2C 5K2

Tel: (403) 253-8273 Email: info@birtley.ca www.birtley.ca

Coreceted December 31,2018

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

						W ANALYSIS,						2/1-		DACIC
LAB#	Sample	Wet	Dry	Retain	ADM%	MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASIS
	ID:	Wt(g)	Wt (g)	Wt (g) 7/8					4.490				4.00	11
186381	4511	172	170	152	1.16	1.57	12.64	17.94	67.85	0.70	2.5	98.3	1.39	adt
						2.71	12.49	17.73	67.06	0.69				arl
							12.84	18.23	68.93	0.71				dl
186382	4512	1748	1721	1494	1.54	0.74	4.08	21.84	73.34	0.45	4.0	97.7	1.33	adl
						2.27	4.02	21.50	72.21	0.44				ar
							4.11	22.00	73.89	0.45				d
186383	4513	2303	2253	1952	2.17	0.74	10.22	23.94	65.10	0.43	8.5	96.2	1.35	ad
						2.90	10.00	23.42	63.69	0.42				ar
							10.30	24.12	65.59	0.43				d
186384	4514	1443	1426	1236	1.18	0.86	13.38	20.15	65.61	0.57	4.0	94.2	1.38	ad
						2.03	13.22	19.91	64.84	0.56				ar
							13.50	20.32	66.18	0.57		no aren		d
186385	4515	1227	1212	843	1.22	0.68	8.05	19.85	71.42	0.64	3.0	98.3	1.35	ad
100000						1.89	7.95	19.61	70.55	0.63				ar
							8.11	19.99	71.91	0.64				
186386	4516	825	823	727	0.24	0.62	81.24	13.67	4.47	0.07	-	-	2.37	ac
	10.10					0.86	81.04	13.64	4.46	0.07				aı
							81.75	13.76	4.50	0.07				
186387	4517	1107	1096	945	0.99	0.60	6.74	22.41	70.25	0.75	8.5	97.1	1.31	ac
100001						1.59	6.67	22.19	69.55	0.74				aı
							6.78	22.55	70.67	0.75				C
186388	4518	1621	1534	1282	5.37	0.87	22.98	21.49	54.66	0.60	1.5	95.4	1.50	ac
100000	10.0					6.19	21.75	20.34	51.73	0.57				а
							23.18	21.68	55.14	0.61				(
186389	4519	1343	1316	1132	2.01	1.09	11.55	17.04	70.32	0.44	1.0	98.3	1.36	a
100000	40.0	10.0				3.08	11.32	16.70	68.91	0.43				а
							11.68	17.23	71.09	0.44				
186390	4520	1166	1154	1009	1.03	0.60	22.19	26.81	50.40	0.55	1.5	98.6	1.61	a
100330	4020	1100	1101			1.62	21.96	26.53	49.88	0.54				а
							22.32	26.97	50.70	0.55				
186391	4521	983	971	832	1.22	0.70	6.17	20.80	72.33	0.73	1.5	98.0	1.34	a
10003	4021	000	0			1.91	6.09	20.55	71.45	0.72				а
							6.21	20.95	72.84	0.74				40.00
186392	4522	436	433	369	0.69	0.70	19.53	18.81	60.96	0.65	3.0	98.6	1.44	а
100392	4522	430	400	000	0.00	1.38	19.40	18.68	60.54	0.65				a
							19.67	18.94	61.39	0.65				
186393	4523	751	748	659	0.40	0.48	16.33	18.48	64.71	0.80	2.5	99.1	1.46	а
100393	4523	131	140	000	0.40	0.48	16.26	18.41	64.45	0.80				a
						0.00	16.41	18.57	65.02	0.80				
10005	450:	2005	2640	2291	0.71	0.49	15.76	20.27	63.48	0.89	7.0	99.1	1.46	а
186394	4524	2665	2646	2291	0.71	1.20	15.65	20.13	63.03	0.88				ā
						1.20	15.84	20.13	63.79	0.89				

<sup>\*</sup>SG checked

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CLIENT:

CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

PO#:

326969WC

HOLE:

WC18-03C

LAB#:

186395-415

REPORT DATE: November 14, 2018

Gwil Industries Inc. 7784 - 62nd St SE Calgary, AB T2C 5K2 Tel: (403) 253-8273 Email: info@birtley.ca www.birtley.ca

Coreceted December 31,2018

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

					HEAD RA	W ANALYSIS	, air dried	l basis						
LAB#	Sample ID:	Wet Wt(g)	Dry Wt (g)	Retain Wt (g) 7/8	ADM%	MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASI
86395	4525	3536	3503	3038	0.93	0.75	36.96	21.59	40.70	2.69	5.0	96.2	1.63	ad
						1.68	36.62	21.39	40.32	2.66				ar
							37.24	21.75	41.01	2.71				d
186396	4526	2044	2025	1738	0.93	0.73	28.83	20.30	50.14	0.82	7.5	99.4	1.52	ad
						1.65	28.56	20.11	49.67	0.81				ar
186397	4507	1000	1010	077			29.04	20.45	50.51	0.83				d
100397	4527	1022	1012	877	0.98	0.57	4.20	23.77	71.46	0.93	8.0	98.0	1.31	ad
						1.54	4.16	23.54	70.76	0.92				ar
186398	4528	1874	1858	1627	0.85	0.81	4.22	23.91	71.87	0.94				d
	1020	1074	1000	1027	0.00	1.66	4.39 4.35	20.40 20.23	74.40 73.76	0.59	2.0	99.1	1.32	ad
						1.00	4.43	20.23	75.76	0.58 0.59				ari
86399	4529	5300	5203	4556	1.83	0.97	2.48	22.73	73.82	0.53	4.5	98.8	1.29	d ad
						2.78	2.43	22.31	72.47	0.52	4.5	50.0	1.29	ari
							2.50	22.95	74.54	0.54				d
86400	4530	2599	2569	2248	1.15	0.65	8.19	22.43	68.73	0.71	7.0	98.8	1.32	ad
						1.80	8.10	22.17	67.94	0.70				art
							8.24	22.58	69.18	0.71				di
86401	4531	1484	1469	1282	1.01	0.79	7.13	20.61	71.47	0.58	2.5	98.3	1.33	adl
						1.79	7.06	20.40	70.75	0.57				arl
00400	4500	4455	1165				7.19	20.77	72.04	0.58				d
36402	4532	1122	1120	954	0.18	0.60	82.96	12.62	3.82	0.05	-	-	2.41	adl
						0.78	82.81	12.60	3.81	0.05				art
86403	4533	164	160	144	4.00	2.05	83.46	12.70	3.84	0.05				dl
30403	4555	104	162	144	1.22	0.65	17.55	18.55	63.25	0.63	3.0	98.8	1.42	adl
						1.86	17.34	18.32	62.48	0.62				arl
36404	4534	1559	1514	1299	2.89	0.66	17.66 38.16	18.67	63.66	0.63	0.5	00.0	4.04	di
	1001	1000	1514	1299	2.03	3.53	37.06	16.04 15.58	45.14 43.84	0.39	2.5	98.6	1.61	adh
- 1						3.33	38.41	16.15	45.44	0.38 0.39				art
36405	4535	611	605	530	0.98	0.61	6.60	19.93	72.86	0.59	2.5	98.6	1.33	db
						1.59	6.54	19.73	72.14	0.58	2.5	90.0	1.33	adb
			1			1.00	6.64	20.05	73.31	0.59				arb db
36406	4536	569	447	378	21.44	0.86	33.90	15.24	50.00	0.40	1.0	94.5	1.56	adb
ı						22.12	26.63	11.97	39.28	0.31	1.0	54.5	1.50	arb
							34.19	15.37	50.43	0.40				db
6407	4537	1536	1528	1320	0.52	0.52	33.44	17.72	48.32	0.60	2.5	95.4	1.58	adt
1						1.04	33.27	17.63	48.07	0.60				art
							33.61	17.81	48.57	0.60				db
36408	4538	2322	2305	2000	0.73	0.48	16.64	26.41	56.47	1.08	7.0	98.6	1.46	adb
						1.21	16.52	26.22	56.06	1.07				arb
0400	4500	000					16.72	26.54	56.74	1.09				db
6409	4539	968	961	835	0.72	0.73	10.63	19.78	68.86	0.94	3.0	98.8	1.36	adb
			1			1.45	10.55	19.64	68.36	0.93				arb
6410	4540	1297	1211	1040	0.00		10.71	19.93	69.37	0.95				db
00410	4540	1291	1211	1040	6.63	0.64	17.89	18.35	63.12	0.99	9.0	97.4	1.41	adb
						7.23	16.70	17.13	58.93	0.92				arb
6411	4541	2121	2086	1002	1.05	0.00	18.01	18.47	63.53	1.00				db
10411	4541	2121	2000	1803	1.65	0.83	25.60	18.28	55.29	0.78	8.0	98.6	1.47	adb
						2.47	25.18	17.98	54.38	0.77				arb
6412	4542	432	424	272	1.05	0.00	25.81	18.43	55.75	0.79				db
112	7072	432	424	373	1.85	0.83	46.43	14.13	38.61	0.59	-	-	1.72	adb
	1					2.67	45.57	13.87	37.90	0.58				arb
6413	4543	459	453	394	1.31	0.94	46.82	14.25	38.93	0.59		04.5	4.50	db
		400	700	334	1.51		35.16	21.92	41.98	3.07	5.5	94.5	1.58	adb
						2.23	34.70	21.63	41.43	3.03				arb
6414	4544	3182	3148	2716	1.07	0.87	35.49	22.13	42.38	3.10			4.00	db
		3102	3140	2710	1.07	1.93	61.51 60.85	17.22 17.04	20.40	0.31	-	-	1.96	adb
	1			111		1.55	62.05	17.04	20.18	0.31				arb
6415	4545	2221	2205	1939	0.72	0.74	8.85	23.99	20.58 66.42	0.31	7.0	08.0	1 26	db
				1003	0.12	1.46	8.79	23.99	65.94	0.57 0.57	7.0	98.0	1.36	adb
			1			1.70	U.13	20.02	JJ.34	0.07				arb

<sup>\*</sup>Sulphur checked

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<sup>\*</sup>SG checked



CLIENT:

CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

PO#:

326969WC

HOLE:

WC18-04C

LAB#:

186416-425

REPORT DATE:

November 14, 2018

Gwil Industries Inc. 7784 - 62nd St SE Calgary, AB T2C 5K2 Tel: (403) 253-8273

Tel: (403) 253-8273 Email: info@birtley.ca www.birtley.ca

Coreceted December 31,2018

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

					HEAD RA	W ANALYSIS	, air dried	basis	4.000					
LAB#	Sample	Wet	Dry	Retain	ADM%	MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASIS
	ID:	Wt(g)	Wt (g)	Wt (g) 7/8										
186416	4546	10030	9903	8696	1.27	0.81	2.95	21.08	75.16	0.51	3.0	98.3	1.29	adl
						2.07	2.91	20.81	74.21	0.50				art
							2.97	21.25	75.77	0.51			1.00	dl
186417	4547	2642	2582	2264	2.27	0.78	13.67	21.22	64.33	0.66	7.0	98.0	1.36	adl
						3.03	13.36	20.74	62.87	0.65				arl
							13.78	21.39	64.84	0.67			105	d
186418	4548	2806	2776	2429	1.07	0.71	11.24	20.73	67.32	0.58	4.0	97.1	1.35	ad
						1.77	11.12	20.51	66.60	0.57				arl
		1					11.32	20.88	67.80	0.58				d
186419	4549	1178	1173	1012	0.42	0.68	74.09	14.47	10.76	0.12	-	-	2.15	ad
						1.10	73.78	14.41	10.71	0.12				ar
							74.60	14.57	10.83	0.12				d
186420	4550	2211	2186	1918	1.13	0.65	7.13	25.57	66.65	0.77	8.5	96.0	1.32	ad
						1.77	7.05	25.28	65.90	0.76				ar
							7.18	25.74	67.09	0.78				d
186421	4551	617	608	530	1.46	0.60	24.58	29.63	45.19	0.49	2.5	97.7	1.60	ad
						2.05	24.22	29.20	44.53	0.48				ar
							24.73	29.81	45.46	0.49				d
186422	4552	2873	2792	2389	2.82	0.76	9.62	23.97	65.65	0.58	4.5	97.1	1.37	ad
						3.56	9.35	23.29	63.80	0.56				ar
							9.69	24.15	66.15	0.58			1.00	d
186423	4553	7683	7336	6376	4.52	0.75	2.85	19.94	76.46	0.47	2.0	95.7	1.29	ad
						5.23	2.72	19.04	73.01	0.45				aı
							2.87	20.09	77.04	0.47				d
186424	4554	2493	2483	2165	0.40	0.55	16.90	19.80	62.75	0.78	4.0	95.4	1.42	ac
						0.95	16.83	19.72	62.50	0.78				aı
							16.99	19.91	63.10	0.78				
186425	4555	707	700	1008	0.99	0.61	8.41	20.46	70.52	1.01	7.0	97.1	1.34	ac
.55 .20						1.59	8.33	20.26	69.82	1.00				aı
							8.46	20.59	70.95	1.02				C

<sup>\*</sup>SG checked

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Operations Manager



CLIENT:

CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

PO#:

326969WC

HOLE:

WC18-05C

LAB#:

186426-432

REPORT DATE:

November 14, 2018

7784 - 62nd St SE Calgary, AB T2C 5K2 Tel: (403) 253-8273 Email: info@birtley.ca www.birtley.ca

Gwil Industries Inc.

Coreceted December 31,2018

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

					HEAD RAV	V ANALYSIS,	air dried	basis						
LAB#	Sample ID:	Wet Wt(g)	Dry Wt (g)	Retain Wt (g) 7/8	ADM%	MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASI
186426	4546	2237	2203	1908	1.52	0.79	2.77	21.03	75.41	0.49	3.5	96.8	1.31	adl
						2.30	2.73	20.71	74.26	0.48				arl
							2.79	21.20	76.01	0.49				db
186427	4547	1481	1458	1269	1.55	0.67	19.60	25.08	54.65	0.68	5.0	98.0	1.47	adl
						2.21	19.30	24.69	53.80	0.67				art
100100							19.73	25.25	55.02	0.68				db
186428	4548	1483	1465	1265	1.21	0.79	24.74	17.32	57.15	0.75	2.5	98.6	1.49	adb
						1.99	24.44	17.11	56.46	0.74				arb
100.00							24.94	17.46	57.61	0.76				db
186429	4549	9181	8965	7795	2.35	0.81	7.56	18.79	72.84	0.51	1.0	98.3	1.35	adb
						3.14	7.38	18.35	71.13	0.50				arb
100100							7.62	18.94	73.43	0.51				db
186430	4550	2139	2118	1860	0.98	0.71	25.05	18.04	56.20	0.55	2.0	98.8	1.48	adb
	1					1.68	24.80	17.86	55.65	0.54				arb
100101							25.23	18.17	56.60	0.55				db
186431	4551	2917	2888	2518	0.99	0.61	18.44	26.58	54.37	0.85	7.0	98.0	1.49	adb
						1.60	18.26	26.32	53.83	0.84				arb
100100							18.55	26.74	54.70	0.86				db
186432	4552	2067	2046	1597	1.02	0.83	6.80	19.56	72.81	0.96	6.5	98.0	1.32	adb
						1.84	6.73	19.36	72.07	0.95				arb
							6.86	19.72	73.42	0.97				db

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CLIENT:

CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

PO#:

326969WC

HOLE:

WC18-06C

LAB#:

186433-442

REPORT DATE:

November 14, 2018

Gwil Industries Inc. 7784 - 62nd St SE Calgary, AB T2C 5K2

Tel: (403) 253-8273 Email: info@birtley.ca

www.birtley.ca

Coreceted December 31,2018

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

					HEAD RA	W ANALYSIS,								DACIO
LAB#	Sample	Wet	Dry	Retain	ADM%	MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASIS
	ID:	Wt(g)	Wt (g)	Wt (g) 7/8									- 10	11
186433	4563	1836	1776	1555	3.27	0.97	81.70	13.44	3.89	0.24	-	-	2.19	adb
						4.21	79.03	13.00	3.76	0.23				arb
							82.50	13.57	3.93	0.24				db
186434	4564	1732	1702	1445	1.73	0.70	15.38	22.96	60.96	0.74	3.0	97.4	1.41	adb
						2.42	15.11	22.56	59.90	0.73				art
							15.49	23.12	61.39	0.75			1.00	dt
186435	4565	1919	1718	1487	10.47	1.06	41.49	16.92	40.53	0.31	1.0	92.8	1.63	adb
						11.42	37.14	15.15	36.28	0.28				art
Y							41.93	17.10	40.96	0.31				dl
186436	4566	2830	2769	2378	2.16	0.82	10.85	22.47	65.86	0.64	7.0	95.4	1.32	adl
						2.96	10.62	21.99	64.44	0.63				ar
							10.94	22.66	66.40	0.65				
186437	4567	1858	1839	1596	1.02	0.80	8.10	20.26	70.84	0.65	3.5	97.1	1.35	ad
.00 .0.						1.81	8.02	20.05	70.12	0.64				ar
							8.17	20.42	71.41	0.66				d
186438	4568	1101	1093	954	0.73	0.75	74.04	13.37	11.84	0.10	-	-	2.15	ad
.00.00						1.47	73.50	13.27	11.75	0.10				ar
							74.60	13.47	11.93	0.10				d
186439	4569	2206	1964	1707	10.97	0.75	7.96	18.99	72.30	0.39	1.5	96.8	1.35	ad
100 100	1000					11.64	7.09	16.91	64.37	0.35				ar
							8.02	19.13	72.85	0.39				d
186440	4570	700	681	597	2.71	0.69	8.03	20.70	70.58	0.70	3.5	94.2	1.36	ad
100110	10.0					3.39	7.81	20.14	68.66	0.68				ar
							8.09	20.84	71.07	0.70				d
186441	4571	1180	1149	991	2.63	0.70	8.08	23.94	67.28	1.07	8.0	94.2	1.32	ad
100441	4011	1100				3.31	7.87	23.31	65.51	1.04				ar
							8.14	24.11	67.75	1.08				d
186442	4572	2242	2205	1926	1.65	0.68	9.27	22.05	68.00	0.83	6.0	95.4	1.35	ad
100442	4012	2272	2200	1020		2.32	9.12	21.69	66.88	0.82				aı
							9.33	22.20	68.47	0.84				C

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Operations Manager



CLIENT:

**CONUMA COAL RESOURCES** 

PROJECT:

Willow Creek development drilling

PO#:

326969WC

HOLE:

WC18-07C

LAB#:

186857-894

REPORT DATE:

November 29, 2018

Corrected December 31,2018

Page 1 of 4

Gwil Industries Inc. 7784 - 62nd St SE

Tel: (403) 253-8273 Email: info@birtley.ca

Calgary, AB T2C 5K2

www.birtley.ca

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

						W ANALYSIS	, air dried	basis						
LAB#	Sample ID:	Wet Wt(g)	Dry Wt (g)	Retain Wt (g) 7/8	ADM%	MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASIS
186857	4573	657	627	549	4.57	1.12	20.15	23.75	54.98	0.98	1.5	58.1	1.47	adb
						5.64	19.23	22.67	52.47	0.94				arb
							20.38	24.02	55.60	0.99				db
186858	4574	715	692	604	3.22	1.32	83.71	7.70	7.27	0.14	n/a	n/a	2.35	adb
						4.49	81.02	7.45	7.04	0.14				arb
							84.83	7.80	7.37	0.14				db
186859	4575	1430	1303	1136	8.88	0.76	27.01	22.05	50.18	0.82	6.5	91.1	1.50	adb
						9.57	24.61	20.09	45.72	0.75				arb
							27.22	22.22	50.56	0.83				db
186860	4576	1470	1453	1262	1.16	0.63	10.97	26.35	62.05	0.87	7.5	88.0	1.39	adb
						1.78	10.84	26.05	61.33	0.86				arb
							11.04	26.52	62.44	0.88				db
186861	4577	2466	2438	2128	1.14	0.57	15.16	25.53	58.74	0.74	6.0	94.2	1.44	adb
						1.70	14.99	25.24	58.07	0.73				arb
							15.25	25.68	59.08	0.74				db
186862	4578	1682	1657	1451	1.49	0.62	2.52	22.70	74.16	0.65	5.0	95.7	1.31	adb
						2.10	2.48	22.36	73.06	0.64				arb
100000							2.54	22.84	74.62	0.65				db
186863	4579	5963	5839	5111	2.08	0.60	5.74	24.59	69.07	0.50	5.5	93.7	1.32	adb
						2.67	5.62	24.08	67.63	0.49				arb
100001							5.77	24.74	69.49	0.50				db
186864	4580	1999	1958	1697	2.05	0.46	11.45	21.92	66.17	0.69	6.5	97.1	1.38	adb
						2.50	11.22	21.47	64.81	0.68				arb
10000=							11.50	22.02	66.48	0.69				db
186865	4581	432	426	375	1.39	0.73	46.91	16.98	35.38	0.39	n/a	n/a	1.77	adb
-						2.11	46.26	16.74	34.89	0.38				arb
							47.25	17.10	35.64	0.39				db
186866	4582	1591	1569	1378	1.38	0.74	5.61	20.44	73.21	0.73	3.5	98.6	1.33	adb
						2.11	5.53	20.16	72.20	0.72				arb
							5.65	20.59	73.76	0.74				db

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CLIENT:

**CONUMA COAL RESOURCES** 

PROJECT:

Willow Creek development drilling

PO#:

326969WC

HOLE:

WC18-07C

LAB#:

186857-894

REPORT DATE:

November 29, 2018

Corrected December 31,2018

7784 - 62nd St SE Calgary, AB T2C 5K2 Tel: (403) 253-8273

Gwil Industries Inc.

Email: info@birtley.ca

Page 2 of 4

www.birtley.ca

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

					HEAD RA	W ANALYSIS	, air dried	basis						
LAB#	Sample	Wet	Dry	Retain	ADM%	MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASIS
	ID:	Wt(g)	Wt (g)	Wt (g) 7/8										
186867	4583	341	339	299	0.59	0.66	11.00	21.70	66.64	0.72	3.5	97.7	1.36	adb
						1.24	10.94	21.57	66.25	0.72				arb
							11.07	21.84	67.08	0.72				db
186868	4584	986	971	849	1.52	0.56	5.49	22.15	71.80	0.67	4.0	97.4	1.33	adb
						2.07	5.41	21.81	70.71	0.66				arb
							5.52	22.27	72.20	0.67				db
186869	4585	805	795	696	1.24	0.61	13.53	19.24	66.62	0.73	2.5	98.3	1.39	adb
						1.84	13.36	19.00	65.79	0.72				arb
							13.61	19.36	67.03	0.73				db
186870	4586	1482	1444	1249	2.56	0.64	15.48	18.04	65.84	0.41	1.5	99.1	1.39	adb
						3.19	15.08	17.58	64.15	0.40				
							15.58	18.16	66.26	0.41				
186871	4587	416	409	359	1.68	0.79	48.43	14.17	36.61	0.50	n/a	n/a	1.76	adb
						2.46	47.62	13.93	35.99	0.49				arb
							48.82	14.28	36.90	0.50			*****	db
186872	4588	408	406	360	0.49	0.60	23.31	23.99	52.10	0.83	6.5	98.6	1.50	adb
						1.09	23.20	23.87	51.84	0.83				arb
							23.45	24.13	52.41	0.84				db
186873	4589	1178	1126	992	4.41	0.72	44.45	16.95	37.88	1.35	n/a	n/a	1.70	adb
						5.10	42.49	16.20	36.21	1.29				arb
							44.77	17.07	38.15	1.36				db
186874	4590	214	212	185	0.93	0.50	27.82	16.48	55.20	0.57	1.0	96.0	1.59	adb
						1.43	27.56	16.33	54.68	0.56				arb
							27.96	16.56	55.48	0.57				db
186875	4591	913	894	789	2.08	0.57	2.67	24.23	72.53	0.96	9.0	96.5	1.28	adb
	1				,	2.64	2.61	23.73	71.02	0.94				art
							2.69	24.37	72.95	0.97				dt
186876	4592	241	239	209	0.83	0.66	23.43	17.67	58.24	0.69	4.0	98.3	1.49	adb
. 500.0						1.48	23.24	17.52	57.76	0.68				art
							23.59	17.79	58.63	0.69				dł

<sup>\*</sup>SG checked

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CLIENT:

CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

PO#:

326969WC

HOLE:

WC18-07C

LAB#:

186857-894

REPORT DATE:

November 29, 2018

Corrected December 31,2018

Page 3 of 4

Gwil Industries Inc. 7784 - 62nd St SE

Tel: (403) 253-8273 Email: info@birtley.ca

Calgary, AB T2C 5K2

www.birtley.ca

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

					HEAD RA	W ANALYSIS	, air dried	basis						
LAB#	Sample ID:	Wet Wt(g)	Dry Wt (g)	Retain Wt (g) 7/8	ADM%	MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASIS
186877	4593	1951	1936	1687	0.77	0.63	13.96	17.82	67.59	0.74	2.5	98.3	1.39	adb
						1.39	13.85	17.68	67.07	0.73				arb
							14.05	17.93	68.02	0.74				db
186878	4594	564	560	493	0.71	0.54	14.85	19.16	65.45	0.85	7.5	97.1	1.40	adb
						1.25	14.74	19.02	64.99	0.84				arb
							14.93	19.26	65.81	0.85				db
186879	4595	901	891	784	1.11	0.50	8.46	23.75	67.29	0.80	7.0	92.5	1.35	adb
						1.60	8.37	23.49	66.54	0.79				arb
							8.50	23.87	67.63	0.80				db
186880	4596	871	848	741	2.64	0.67	26.73	16.16	56.44	0.45	0.0	96.5	1.53	adb
						3.29	26.02	15.73	54.95	0.44				arb
							26.91	16.27	56.82	0.45				db
186881	4597	7525	7064	6131	6.13	0.69	6.81	19.10	73.40	0.44	1.0	96.0	1.35	adb
						6.77	6.39	17.93	68.90	0.41				arb
							6.86	19.23	73.91	0.44				db
186882	4598	8788	8461	7413	3.72	0.42	13.23	19.42	66.93	0.38	4.0	96.8	1.37	adb
						4.13	12.74	18.70	64.44	0.37				arb
							13.29	19.50	67.21	0.38				db
186883	4599	998	958	833	4.01	0.37	14.31	19.67	65.65	0.45	6.0	95.7	1.40	adb
						4.36	13.74	18.88	63.02	0.43				arb
							14.36	19.74	65.89	0.45				db
186884	4600	1950	1886	1643	3.28	0.46	9.05	19.09	71.40	0.64	2.5	96.2	1.36	adb
						3.73	8.75	18.46	69.06	0.62				arb
							9.09	19.18	71.73	0.64				db
186885	4601	1633	1615	1417	1.10	0.30	21.28	27.66	50.76	0.73	5.5	96.0	1.55	adb
						1.40	21.05	27.36	50.20	0.72				arb
							21.34	27.74	50.91	0.73				db
186886	4602	1875	1822	1592	2.83	0.44	14.14	18.50	66.92	0.81	3.5	94.0	1.41	adb
						3.25	13.74	17.98	65.03	0.79				arb
							14.20	18.58	67.22	0.81				db

<sup>\*</sup>Prox, SG checked

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CLIENT:

CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

PO#:

326969WC

HOLE:

WC18-07C

LAB#:

186857-894

REPORT DATE:

November 29, 2018

Corrected December 31,2018

Gwil Industries Inc. 7784 - 62nd St SE Calgary, AB T2C 5K2 Tel: (403) 253-8273

Tel: (403) 253-8273 Email: info@birtley.ca

www.birtley.ca

Page 4 of 4

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

					HEAD RA	W ANALYSIS	, air dried	basis						
LAB#	Sample	Wet	Dry	Retain	ADM%	MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASIS
	ID:	Wt(g)	Wt (g)	Wt (g) 7/8							-4.000			
186887	4603	4765	4637	4068	2.69	0.48	6.95	22.76	69.81	0.54	5.0	92.3	1.33	adb
						3.15	6.76	22.15	67.93	0.53				arb
							6.98	22.87	70.15	0.54			-ues	db
186888	4604	238	235	209	1.26	0.77	46.14	15.04	38.05	0.35	n/a	n/a	1.80	adb
						2.02	45.56	14.85	37.57	0.35				arb
							46.50	15.16	38.35	0.35				db
186889	4605	1805	1772	1516	1.83	0.61	5.63	20.50	73.26	0.71	3.5	97.1	1.33	adb
						2.43	5.53	20.13	71.92	0.70				arb
							5.66	20.63	73.71	0.71				db
186890	4606	1050	1040	896	0.95	0.58	84.82	12.94	1.66	0.03	n/a	n/a	2.51	adb
						1.53	84.01	12.82	1.64	0.03				
							85.31	13.02	1.67	0.03				
186891	4607	1056	1034	902	2.08	0.49	9.62	23.13	66.76	0.75	8.0	94.8	1.34	adb
						2.56	9.42	22.65	65.37	0.73				arb
							9.67	23.24	67.09	0.75				db
186892	4608	2739	2701	2338	1.39	0.63	7.04	18.39	73.94	0.56	0.5	99.4	1.35	adb
						2.01	6.94	18.13	72.91	0.55				arb
							7.08	18.51	74.41	0.56				db
186893	4609	3002	2958	2576	1.47	0.56	4.61	19.97	74.86	0.41	2.0	98.3	1.32	adb
						2.02	4.54	19.68	73.76	0.40				art
							4.64	20.08	75.28	0.41				db
186894	4610	3171	2974	2613	6.21	0.59	9.64	20.62	69.15	0.39	4.0	98.8	1.37	adb
						6.77	9.04	19.34	64.85	0.37				art
							9.70	20.74	69.56	0.39				db

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We accept no responsibility for the origin of the sample, nor for any deviation between the sample and the bulk of the material it purports to represent.





CLIENT:

CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

PO#:

326969WC

HOLE:

WC18-08C

LAB#:

187334-353

December 10, 2018

REPORT DATE:

Corrected December 31,2018

Page 1 of 3

Gwil Industries Inc. 7784 - 62nd St SE Calgary, AB T2C 5K2 Tel: (403) 253-8273 Email: info@birtley.ca

www.birtley.ca

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

LAB#	Sample ID:	Wet Wt(g)	Dry Wt (g)	Retain Wt (g) 7/8	ADM%	W ANALYSIS MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASIS
187334	4611	2875	2831	2427	1.53	0.64	22.44	18.83	58.09	0.55	3.5	96.2	1.45	ad
						2.16	22.10	18.54	57.20	0.54	0.0	50.2	1.45	ar
							22.58	18.95	58.46	0.55				d
187335	4612	499	490	401	1.80	0.57	21.45	30.80	47.18	0.69	2.5	96.8	1.57	ad
						2.36	21.06	30.24	46.33	0.68				ar
							21.57	30.98	47.45	0.69				d
187336	4613	1555	1541	1301	0.90	0.65	23.20	17.85	58.30	0.70	5.0	98.6	1.48	adl
	1 1					1.54	22.99	17.69	57:78	0.69				ari
187337	4044	504	540	101	2.22		23.35	17.97	58.68	0.70				di
10/33/	4614	531	519	404	2.26	1.23	5.64	23.31	69.82	1.21	1.5	65.6	1.33	adl
						3.46	5.51	22.78	68.24	1.18				art
187338	4615	235	234	175	0.43	0.75	5.71 69.62	23.60 15.62	70.69	1.23			0.00	dl
70,000	40.0	200	204	173	0.43	1.17	69.32	15.55	14.01 13.95	0.22 0.22	-	-	2.09	adt
						1.17	70.15	15.74	14.12	0.22				art
187339	4616	468	457	368	2.35	0.96	35.12	18.92	45.00	0.69	1.5	74.7	1.57	db adb
						3.29	34.29	18.48	43.94	0.67	1.5	17.1	1.51	art
							35.46	19.10	45.44	0.70				db
187340	4617	1342	1319	1104	1.71	0.69	7.52	21.74	70.05	0.75	4.5	96.5	1.33	adb
						2.39	7.39	21.37	68.85	0.74				arb
							7.57	21.89	70.54	0.76				db
187341	4618	2437	2406	2075	1.27	0.84	9.32	20.18	69.66	0.45	1.5	98.3	1.35	adb
						2.10	9.20	19.92	68.77	0.44				arb
187342	4040	5004	50.40	1000			9.40	20.35	70.25	0.45				db
15/342	4619	5381	5340	4622	0.76	0.84	3.45	22.90	72.81	0.44	7.0	98.6	1.29	adb
						1.60	3.42	22.73	72.26	0.44				arb
187343	4620	2420	2393	2053	1.12	0.54	3.48 11.57	23.09	73.43	0.44	7.5	00.0	1.00	db
10.010	4020	2420	2555	2000	1.12	1.65	11.44	22.38 22.13	65.51 64.78	0.70 0.69	7.5	98.0	1.36	adb
				1		1.00	11.63	22.50	65.87	0.70				arb db
187344	4621	1461	1447	1216	0.96	0.69	7.18	20.56	71.57	0.66	3.0	98.6	1.35	adb
						1.64	7.11	20.36	70.88	0.65	0.0	50.0	1.00	arb
							7.23	20.70	72.07	0.66				db
187345	4622	860	855	718	0.58	0.62	74.12	12.87	12.39	0.13	0.0	99.4	2.21	adb
1	1					1.20	73.69	12.80	12.32	0.13				arb
							74.58	12.95	12.47	0.13				db
187346	4623	513	508	414	0.97	0.78	17.83	22.13	59.26	0.64	7.5	98.3	1.47	adb
						1.75	17.66	21.91	58.68	0.63				arb
187347	4624	1345	1329	4400	4.40	2.00	17.97	22.30	59.73	0.65				db
107347	4024	1345	1329	1102	1.19	0.68	26.19	18.05	55.08	0.48	1.5	98.8	1.50	adb
						1.86	25.88	17.84	54.42	0.47				arb
187348	4625	2080	1965	1695	5.53	0.91	26.37 10.99	18.17 19.28	55.46 68.82	0.48	2.0	07.4	1.00	db
			.555	,000	0.00	6.39	10.38	18.21	65.02	0.37	2.0	97.4	1.38	adb
						0.00	11.09	19.46	69.45	0.37				arb db
187349	4626	4109	4034	3500	1.83	0.84	15.77	18.65	64.74	0.55	3.0	98.3	1.41	adb
						2.65	15.48	18.31	63.56	0.54	0.0	30.5	1.71	arb
							15.90	18.81	65.29	0.55				db
187350	4627	1312	1304	1102	0.61	0.73	31.79	22.75	44.73	0.90	4.5	98.8	1.61	adb
						1.34	31.60	22.61	44.46	0.89				arb
							32.02	22.92	45.06	0.91				db
187351	4628	2579	2535	2175	1.71	0.85	11.00	19.25	68.90	0.84	7.0	99.1	1.35	adb
				1		2.54	10.81	18.92	67.72	0.83				arb
							11.09	19.42	69.49	0.85				db
187352	4629	841	837	701	0.48	0.46	14.29	17.01	68.24	0.73	1.5	99.1	1.41	adb
-						0.93	14.22	16.93	67.92	0.73				arb
107050	4005	100-	100-				14.36	17.09	68.56	0.73				db
187353	4630	1083	1069	890	1.29	0.55	17.47	17.15	64.83	0.69	2.0	99.4	1.42	adb
	1					1.84	17.24	16.93	63.99	0.68				arb
							17.57	17.24	65.19	0.69				db

\* Ash, SG checked

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Heather Dexter Operations Manager



CLIENT:

CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

PO#:

326969WC

HOLE:

WC18-10C

LAB#:

187354-362

REPORT DATE:

December 10, 2018

Corrected December 31,2018

Gwil Industries Inc. 7784 - 62nd St SE Calgary, AB T2C 5K2 Tel: (403) 253-8273

Email: info@birtley.ca

www.birtley.ca

Page 2 of 3

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

					HEAD RA	W ANALYSIS	, air dried	basis						
LAB#	Sample	Wet	Dry	Retain	ADM%	MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASIS
	ID:	Wt(g)	Wt (g)	Wt (g) 7/8										
187354	4631	752	745	610	0.93	0.49	35.71	15.19	48.61	0.79	2.5	99.4	1.59	adb
						1.42	35.38	15.05	48.16	0.78				arb
							35.89	15.26	48.85	0.79				db
187355	4632	521	517	412	0.77	0.44	9.35	21.41	68.80	1.31	9.0	98.8	1.36	adb
						1.20	9.28	21.25	68.27	1.30				arb
							9.39	21.50	69.10	1.32				db
187356	4633	1992	1968	1685	1.20	0.54	4.12	16.79	78.55	0.74	2.0	99.4	1.33	adb
						1.74	4.07	16.59	77.60	0.73				arb
							4.14	16.88	78.98	0.74				db
187357	4634	583	547	438	6.17	0.41	6.96	17.72	74.91	0.92	2.5	98.3	1.34	adb
						6.56	6.53	16.63	70.28	0.86				
							6.99	17.79	75.22	0.92			***	
187358	4635	675	668	544	1.04	0.37	14.97	16.38	68.28	0.96	3.0	98.3	1.41	adb
						1.40	14.81	16.21	67.57	0.95				arb
							15.03	16.44	68.53	0.96				db
187359	4636	1220	1194	1010	2.13	0.40	17.93	16.74	64.93	0.91	2.5	97.1	1.42	adb
						2.52	17.55	16.38	63.55	0.89				arb
							18.00	16.81	65.19	0.91				db
187360	4637	341	335	275	1.76	0.61	31.91	16.28	51.20	2.04	4.0	97.1	1.57	adb
		,				2.36	31.35	15.99	50.30	2.00				arb
							32.11	16.38	51.51	2.05				db
187361	4638	3303	3246	2811	1.73	0.83	3.38	16.95	78.84	0.66	0.5	98.3	1.33	adb
						2.54	3.32	16.66	77.48	0.65				art
							3.41	17.09	79.50	0.67				dt
187362	4639	1166	1126	955	3.43	0.76	26.09	13.24	59.91	0.58	0.5	98.6	1.51	adb
						4.16	25.19	12.79	57.85	0.56				art
							26.29	13.34	60.37	0.58				dt

<sup>\*</sup> Ash, SG checked

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<sup>\*\*</sup> Sulphur checked



CLIENT:

CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

PO#:

326969WC

HOLE:

WC18-11C

LAB#:

187363-370

REPORT DATE:

December 10, 2018

Corrected December 31,2018

Gwil Industries Inc. 7784 - 62nd St SE Calgary, AB T2C 5K2 Tel: (403) 253-8273 Email: info@birtley.ca www.birtley.ca

Page 3 of 3

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

					HEAD RA	W ANALYSIS	, air dried	basis						
LAB#	Sample	Wet	Dry	Retain	ADM%	MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASIS
	ID:	Wt(g)	Wt (g)	Wt (g) 7/8										۵, ۱۵.۵
187363	4640	1028	1017	859	1.07	0.51	14.79	19.02	65.68	0.82	4.5	97.4	1.41	adb
						1.57	14.63	18.82	64.98	0.81				arb
							14.87	19.12	66.02	0.82				db
187364	4641	2565	2541	2170	0.94	0.84	6.23	18.60	74.33	0.58	0.5	98.8	1.32	adb
						1.77	6.17	18.43	73.63	0.57				arb
							6.28	18.76	74.96	0.58				db
187365	4642	2669	2630	2270	1.46	0.81	7.21	18.92	73.06	0.38	1.0	99.1	1.30	adb
						2.26	7.10	18.64	71.99	0.37				arb
							7.27	19.07	73.66	0.38				db
187366	4643	3942	3873	3348	1.75	0.68	2.52	21.35	75.45	0.39	4.0	97.1	1.28	adb
			-			2.42	2.48	20.98	74.13	0.38				arb
					-		2.54	21.50	75.97	0.39				db
187367	4644	660	657	544	0.45	0.49	5.37	23.34	70.80	1.16	8.5	98.3	1.29	adb
						0.94	5.35	23.23	70.48	1.15				arb
107000							5.40	23.45	71.15	1.17				db
187368	4645	176	174	110	1.14	0.62	29.80	28.05	41.53	0.75	3.5	98.0	1.62	adb
						1.75	29.46	27.73	41.06	0.74				arb
							29.99	18.55	41.79	0.75				db
187369	4646	1902	1888	1632	0.74	0.66	25.01	16.65	57.68	0.51	1.0	98.6	1.50	adb
						1.39	24.83	16.53	57.26	0.51				arb
							25.18	16.76	58.06	0.51				db
187370	4647	250	247	190	1.20	0.62	32.90	21.93	44.55	0.69	4.0	99.4	1.54	adb
						1.81	32.51	21.67	44.02	0.68				arb
							33.11	22.07	44.83	0.69				db

<sup>\*\*</sup> Sulphur checked

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CLIENT:

CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

PO#:

326969WC

HOLE:

WC18-12C

LAB#:

187371-390

REPORT DATE:

December 28, 2018

Gwil Industries Inc. 7784 - 62nd St SE Calgary, AB T2C 5K2 Tel: (403) 253-8273 Email: info@birtley.ca www.birtley.ca

Page 1 of 2

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

1.45 "	10-	100		T		W ANALYSIS								
LAB#		1	Dry	Retain	ADM%	MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BAS
	ID:	Wt(g)	Wt (g)	Wt (g) 7/8										
187371	4648	3543	3457	3001	2.43	1.32	26.56	21.93	50.19	0.76	0.5	97.7	1.50	ac
						3.72	25.92	21.40	48.97	0.74				a
407070							26.92	22.22	50.86	0.77				c
187372	4649	959	947	801	1.25	0.67	10.24	25.86	63.23	0.84	7.0	98.3	1.37	ac
						1.91	10.11	25.54	62.44	0.83				ar
107070	1070	1010					10.31	26.03	63.66	0.85				d
187373	4650	1240	1233	1048	0.56	0.44	47.81	43.54	8.21	0.29		-	2.27	ad
						1.00	47.54	43.29	8.16	0.29				ar
187374	4054	1000	1010				48.02	43.73	8.25	0.29				d
10/3/4	4651	1023	1012	845	1.08	0.64	13.82	25.45	60.09	0.68	5.0	97.4	1.43	ad
						1.71	13.67	25.18	59.44	0.67				ar
187375	4652	074	000	744			13.91	25.61	60.48	0.68				d
10/3/3	4032	874	862	714	1.37	0.63	2.97	24.08	72.32	0.73	8.0	97.4	1.26	ad
						1.99	2.93	23.75	71.33	0.72				ar
187376	4653	5199	5143	4460	4.00	0.50	2.99	24.23	72.78	0.73				d
101010	4000	3199	3143	4460	1.08	0.52	11.46	20.65	67.37	0.41	2.0	97.7	1.34	ad
						1.59	11.34	20.43	66.64	0.41				ar
187377	4654	10153	10049	0000	1.00	0.67	11.52	20.76	67.72	0.41				d
.01011	7554	10133	10049	8823	1.02	0.57	2.72	24.44	72.27	0.42	8.0	97.7	1.25	ad
						1.59	2.69	24.19	71.53	0.42				ari
187378	4655	1618	1579	1413	2.41	0.47	2.74	24.58	72.68	0.42				d
101010	4000	1010	13/9	1413	2.41	0.47	9.02	22.57	67.94	0.71	7.0	97.7	1.30	adl
						2.87	8.80	22.03	66.30	0.69				ari
187379	4656	1676	1658	1442	1.07	0.81	9.06	22.68	68.26	0.71	2.0	00.0	4.00	d
		1010	1000	1772	1.07	1.88	4.33	20.33	74.31	0.63	3.0	98.6	1.28	adl
			1			1.00	4.23	20.72	73.51	0.62				ari
187380	4657	1597	1578	1412	1.19	0.71	80.10	12.90	74.92 6.29	0.64			0.04	di
						1.89	79.15	12.75	6.22	0.62	•	-	2.31	adi
				- 1		1.00	80.67	12.73	6.33	0.62				ari
187381	4658	1454	1441	1270	0.89	0.51	6.77	25.41	67.31	0.80	8.0	97.1	1 21	di
					0.00	1.40	6.71	25.18	66.71	0.79	6.0	97.1	1.31	adl
						1.40	6.80	25.54	67.66	0.80				art
187382	4659	2631	2565	2229	2.51	0.56	23.96	18.18	57.30	0.53	1.0	98.8	1.46	di adi
						3.05	23.36	17.72	55.86	0.52	1.0	30.0	1.40	art
							24.09	18.28	57.62	0.53				dt
187383	4660	1263	1238	1083	1.98	0.47	7.91	19.56	72.06	0.74	2.0	98.8	1.33	adk
						2.44	7.75	19.17	70.63	0.73	2.0	00.0	1.00	art
							7.95	19.65	72.40	0.74				db
187384	4661	1012	1002	864	0.99	0.64	22.17	22.07	55.12	0.40	2.0	98.6	1.48	adb
			1	1		1.62	21.95	21.85	54.58	0.40			1.10	arb
							22.31	22.21	55.48	0.40				db
187385	4662	1212	1157	1011	4.54	0.60	18.46	19.82	61.12	0.40	4.0	98.6	1.40	adb
						5.11	17.62	18.92	58.35	0.38			0	arb
							18.57	19.94	61.49	0.40				db
87386	4663	3347	3302	2924	1.34	0.74	14.59	18.45	66.22	0.59	2.0	98.8	1.38	adb
						2.07	14.39	18.20	65.33	0.58		00.0	1.00	arb
							14.70	18.59	66.71	0.59				db
87387	4664	1599	1587	1400	0.75	0.52	80.58	12.08	6.82	0.08	-	-	2.37	adb
						1.27	79.98	11.99	6.77	0.08			2.01	arb
							81.00	12.14	6.86	0.08				db
87388	4665	139	138	121	0.72	0.63	41.46	15.40	42.51	0.41	-	-	1.64	adb
						1.34	41.16	15.29	42.20	0.41	-	•	1.04	
							41.72	15.50	42.78	0.41				art
87389	4666	3951	3850	3378	2.56	0.46	19.51	28.22	51.81	0.86	7.5	98.6	1.47	db
						3.00	19.01	27.50	50.49	0.84	1.5	30.0	1.47	adb
						0.00	19.60	28.35	52.05	0.86				arb
87390	4667	634	629	559	0.79	0.51	20.17	17.45	61.87	0.79	2.5	99.1	1.43	db
						1.29	20.01	17.43	61.38	0.79	2.5	99. I	1.43	adb
				- 1			_0.0.		31.00	5.70				arb

<sup>\*%</sup> Volatile checked

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<sup>\*\*</sup> Prox & SG checked



CLIENT: CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

PO#:

326969WC

HOLE:

WC18-13C

LAB#:

187391-409

REPORT DATE:

December 28, 2018

Gwil Industries Inc. 7784 - 62nd St SE Calgary, AB T2C 5K2 Tel: (403) 253-8273 Email: info@birtley.ca

www.birtley.ca

Page 2 of 2

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

		101	Des	Dot-!-	ADM%	W ANALYSIS MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASIS
LAB#	Sample	Wet	Dry	Retain	ADW1%	WO13 1 76	ASIT /0	VOL 78	1,0.70	0 / 0		,,,,		
07004	ID:	Wt(g)	Wt (g) 1721	Wt (g) 7/8 1498	5.34	3.37	25.57	22.52	48.54	0.76	0.5	9.4	1.55	ad
87391	4668	1818	1/21	1496	5.54	8.53	24.21	21.32	45.95	0.72				ar
						0.55	26.46	23.31	50.23	0.79				d
	1000	000	912	787	1.08	0.66	7.59	26.23	65.52	0.87	7.0	85.8	1.33	ad
87392	4669	922	912	101	1.00	1.74	7.51	25.95	64.81	0.86				ar
						1.74	7.64	26.40	65.96	0.88				d
		1070	1000	4404	0.71	0.70	87.86	5.52	5.92	0.09		-	2.40	ad
187393	4670	1272	1263	1121	0.71	1.40	87.24	5.48	5.88	0.09				ar
						1.40	88.48	5.56	5.96	0.09				d
				1000	0.07	0.54	10.96	25.43	63.07	0.80	7.5	97.1	1.40	ac
187394	4671	1539	1524	1330	0.97	1.51	10.95	25.43	62.46	0.79	1.0	•		aı
						1.51	11.02	25.57	63.41	0.80				c
				100	4.57	0.51		22.27	67.10	0.79	7.0	92.3	1.38	ad
187395	4672	575	566	489	1.57		10.12 9.96	21.92	66.05	0.78	1.0	32.0	1.00	a
						2.07			67.44	0.79				C
						4.05	10.17	22.38	71.12	0.50	1.5	99.1	1.35	ac
187396	4673	2383	2342	2028	1.72	1.05	8.20	19.63 19.29	69.90	0.49	1.5	33.1	1.00	а
						2.75	8.06		71.87	0.43				
							8.29	19.84	67.44	0.49	3.5	97.1	1.35	ac
187397	4674	5484	5213	4516	4.94	0.85	10.32	21.39		0.49	5.5	37.1	1.00	a
						5.75	9.81	20.33	64.11	0.47				(
							10.41	21.57	68.02		7.5	98.0	1.37	a
187398	4675	1381	1336	1170	3.26	0.45	15.63	22.47	61.45	0.66	7.5	90.0	1.37	a
					1	3.69	15.12	21.74	59.45	0.64				١
							15.70	22.57	61.73	0.66	2.2	97.7	1.33	a
187399	4676	2122	2097	1811	1.18	0.65	7.26	20.25	71.84	0.74	2.2	97.7	1.33	
						1.82	7.17	20.01	70.99	0.73				а
							7.31	20.38	72.31	0.74			0.07	
187400	4677	1436	1426	1237	0.70	0.64	77.07	13.94	8.35	0.10	-	-	2.27	a
						1.33	76.53	13.84	8.29	0.09				a
							77.57	14.03	8.40	0.10			4.00	
187401	4678	1750	1730	1498	1.14	0.61	9.90	23.43	66.06	0.81	9.0	98.3	1.32	а
					1	1.75	9.79	23.16	65.31	0.80				a
							9.96	23.57	66.47	0.81				
187402	4679	3566	3496	3037	1.96	0.58	14.30	19.64	65.48	0.70	4.0	97.1	1.39	а
						2.53	14.02	19.25	64.19	0.69				8
							14.38	19.75	65.86	0.70				
187403	4680	1996	1978	1730	0.90	0.57	19.56	18.93	60.94	0.86	4.5	98.3	1.42	а
107 100						1.47	19.38	18.76	60.39	0.85				a
							19.67	19.04	61.29	0.86				
187404	4681	2104	2079	1806	1.19	0.73	7.79	18.23	73.25	0.54	1.0	99.7	1.34	а
101707	700.	1 2.0.				1.91	7.70	18.01	72.38	0.53				a
							7.85	18.36	73.79	0.54				
187405	4682	5117	4947	4348	3.32	0.76	4.91	19.74	74.59	0.43	2.0	99.7	1.31	а
101400	4002	) 3111	4041	10.10		4.06	4.75	19.08	72.11	0.42				
							4.95	19.89	75.16	0.43				
107100	4683	7116	6952	6040	2.30	0.81	9.69	20.25	69.25	0.37	4.5	96.8	1.33	a
187406	4003	/110	0932	0040	2.50	3.10	9.47	19.78	67.65	0.36				
					1	5.10	9.77	20.42	69.82	0.37				
107:05	4551	1005	1000	924	2.03	0.69	63.06	13.08	23.17	0.18	-	-	2.03	ä
187407	4684	1085	1063	924	2.03	2.70	61.78	12.81	22.70	0.18				
						2.10	63.50	13.17	23.33	0.18				
					101	0.00		19.07	57.25	0.51	5.5	99.4	1.45	
187408	4685	2369	2338	2064	1.31	0.63	23.05		56.50	0.50	5.5	33.4	1.40	
						1.93	22.75	18.82		0.50				
							23.20	19.19	57.61	0.51	4.5	99.4	1.48	
187409	4686	1735	1720	1519	0.86	0.62	24.63	18.70	56.05		4.5	55.4	1.40	
						1.48	24.42		55.57	0.51				
	1	1			1		24.78	18.82	56.40	0.51				

<sup>\*%</sup> Volatile checked

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CLIENT:

CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

PO#: **326969WC** 

HOLE:

WC18-14C

LAB#:

187933-188012

UPDATED:

February 14, 2019

7784 - 62nd St SE Calgary, AB T2C 5K2 Tel: (403) 253-8273 Email: info@birtley.ca www.birtley.ca

Gwil Industries Inc.

Page 1 of 4

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

LAB#	Sample	Wet	Dry	Retain		W ANALYSIS								
LAD#	ID:	Wt(g)	Wt (g)	Wt (g) 7/8	ADM%	MOIST%	ASH%	VOL%	F.C.%	<b>S</b> %	FSI	%LT	SG	BASIS
187933	4687	957	941	823	1.67	1.47	34.17	19.16	45.20	0.69	1.5	76.8	1.57	adb
						3.12	33.60	18.84	44.44	0.68				art
							34.68	19.45	45.87	0.70				db
187934	4688	1770	1748	1509	1.24	0.50	15.90	28.73	54.87	0.75	6.5	96.5	1.44	adb
						1.74	15.70	28.37	54.19	0.74				art
407005	4000	4.450	=				15.98	28.87	55.15	0.75				db
187935	4689	1450	1435	1261	1.03	0.71	5.88	23.70	69.71	0.68	8.0	96.5	1.30	adb
						1.74	5.82	23.45	68.99	0.67				arb
187936	4690	3708	2004	2222	4.40		5.92	23.87	70.21	0.68				db
107930	4090	3708	3664	3203	1.19	0.80	10.08	21.14	67.98	0.44	2.0	97.7	1.36	adb
						1.98	9.96	20.89	67.17	0.43				arb
187937	4691	6199	6119	5350	1.29	0.65	10.16	21.31	68.53	0.44				db
07507	4001	0133	0119	5550	1.29	1.93	3.06	24.38	71.91	0.40	8.0	97.7	1.28	adb
						1.93	3.02 3.08	24.07 24.54	70.98	0.39				arb
187938	4692	646	628	507	2.79	0.57	21.35	21.60	72.38 56.48	0.40	7.5	97.7	1.41	db
		- 10	323	00.	2.13	3.34	20.76	21.00	54.91	0.34	1.5	97.7	1.41	adb
						0.04	21.47	21.72	56.80	0.35				arb db
187939	4693	760	753	652	0.92	0.60	52.28	14.79	32.33	0.30			1.81	adb
						1.52	51.80	14.65	32.03	0.30	-	-	1.01	arb
							52.60	14.88	32.53	0.30				db
87940	4694	1697	1667	1434	1.77	0.61	7.88	22.65	68.86	0.64	8.0	97.7	1.30	adb
						2.37	7.74	22.25	67.64	0.63	0.0	01.7	1.00	arb
							7.93	22.79	69.28	0.64				db
87941	4695	151	150	121	0.66	0.79	59.04	14.28	25.89	0.24	-	-	1.89	adb
- 1						1.45	58.65	14.19	25.72	0.24				arb
							59.51	14.39	26.10	0.24				db
87942	4696	461	458	404	0.65	0.55	59.84	14.47	25.14	0.25	-	-	1.94	adb
			I			1.20	59.45	14.38	24.98	0.25				arb
07040					No.		60.17	14.55	25.28	0.25				db
87943	4697	1510	1482	1304	1.85	0.81	4.85	20.80	73.54	0.61	3.0	99.1	1.30	adb
- 1						2.65	4.76	20.41	72.18	0.60				arb
87944	4698	45.40	4540	1000			4.89	20.97	74.14	0.61				db
0/944	4698	1542	1519	1329	1.49	0.43	33.40	20.12	46.05	0.50	7.5	96.0	1.55	adb
						1.92	32.90	19.82	45.36	0.49				arb
87945	4699	1639	1596	1411	2.62	0.50	33.54	20.21	46.25	0.50			-	db
31343	4033	1039	1390	1411	2.02	0.53 3.14	19.52	18.26	61.69	0.55	2.0	97.4	1.42	adb
- 1						3.14	19.01	17.78	60.07	0.54				arb
37946	4700	1147	1134	991	1.13	0.40	19.62 15.70	18.36 26.88	62.02 57.02	0.55	4.0	00.0	4.45	db
			1104	331	1.13	1.53	15.70	26.58	56.37	0.55	4.0	96.2	1.45	adb
						1.55	15.76	26.99	57.25	0.56				arb
87947	4701	717	710	627	0.98	0.38	16.70	21.01	61.91	0.66	3.0	97.4	1.40	db
				02.	0.50	1.35	16.54	20.80	61.31	0.65	3.0	97.4	1.40	adb
						1.00	16.76	21.09	62.15	0.66				arb db
37948	4702	977	956	827 .	2.15	0.37	27.93	20.35	51.35	0.66	0.5	97.7	1.55	adb
	_					2.51	27.33	19.91	50.25	0.42	0.5	31.1	1.35	
						2.01	28.03	20.43	51.54	0.41				arb
37949	4703	3799	3614	3125	4.87	0.66	4.38	20.18	74.78	0.45	1.0	92.0	1.30	db adb
		-		•		5.50	4.17	19.20	71.14	0.43	1.0	32.0	1.30	adb
						0.00	4.41	20.31	75.28	0.45				arb db
7950	4704	8837	8420	7306	4.72	0.61	4.79	21.09	73.51	0.43	4.0	96.8	1.29	adb
						5.30	4.56	20.09	70.04	0.43	7.0	30.0	1.23	arb
			İ			0.00	4.82	21.22	73.96	0.43				db
7951	4705	1394	1300	1125	6.74	0.79	50.75	14.40	34.06	0.43	-	-	1.78	adb
						7.48	47.33	13.43	31.76	0.26	-	-	1.10	adb
							51.15	14.51	34.33	0.28				arb db
7952	4706	585	571	490	2.39	0.54	23.70	20.63	55.13	0.38	1.0	97.1	1.50	adb
						2.92	23.13	20.03	53.81	0.37	1.0	31.1	1.50	anb
1	1		1				23.83	20.74	55.43	0.38				db

<sup>\*</sup> SG checked

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<sup>+</sup> Ash checked

<sup>-</sup> Volatile checked



CLIENT:

CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

326969WC PO#:

HOLE:

WC18-14C, WC18-15C & WC18-16C

LAB#:

187933-188012

UPDATED:

February 14, 2019

Page 2 of 4

Gwil Industries Inc. 7784 - 62nd St SE

Email: info@birtley.ca www.birtley.ca

Calgary, AB T2C 5K2 Tel: (403) 253-8273

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

LAB#	Sample	Wet	Dry	Retain	ADM%	W ANALYSIS, MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASIS
LAB#	Sample ID:	Wt(g)	Wt (g)	Wt (g) 7/8	ADIVI /0	1010170	A01170			- /0	. •.			
87953	4707	616	609	531	1.14	0.65	55.21	11.84	32.30	0.35	-	-	1.80	adl
.0,000						1.78	54.58	11.71	31.93	0.35				arl
							55.57	11.92	32.51	0.35	,			dl
187954	4708	873	851	724	2.52	0.51	9.89	18.24	71.36	0.62	1.0	97.4	1.34	ad
						3.02	9.64	17.78	69.56	0.60				arl
							9.94	18.33	71.73	0.62				dl
187955	4709	1382	1370	1179	0.87	0.56	33.58	18.21	47.65	0.46	3.5	97.7	1.56	adi
101000						1.42	33.29	18.05	47.24	0.46				art
							33.77	18.31	47.92	0.46				di
187956	4710	1020	1009	872	1.08	0.45	11.31	25.19	63.05	1.00	8.0	95.4	1.36	adl
						1.52	11.19	24.92	62.37	0.99				arl
							11.36	25.30	63.34	1.00				d
187957	4711	2361	2332	2021	1.23	0.54	19.45	17.85	62.16	0.79	5.0	98.0	1.40	adl
						1.76	19.21	17.63	61.40	0.78				art
							19.56	17.95	62.50	0.79				dl
187958	4712	1073	1065	939	0.75	0.60	38.62	16.04	44.74	0.76	7.0	98.3	1.59	adi
						1.34	38.33	15.92	44.41	0.75				ar
							38.85	16.14	45.01	0.76				d
187959	4713	1706	1647	1461	3.46	0.74	21.84	17.84	59.58	0.67	0.5	79.0	1.46	ad
						4.17	21.08	17.22	57.52	0.65				ar
			_				22.00	17.97	60.02	0.67				d
187960	4714	423	420	360	0.71	0.65	6.33	18.10	74.92	0.65	1.0	98.6	1.32	ad
						1.35	6.29	17.97	74.39	0.65				ar
							6.37	18.22	75.41	0.65				d
187961	4715	3247	3214	2825	1.02	0.58	4.32	19.36	75.74	0.45	3.0	96.0	1.29	ad
						1.59	4.28	19.16	74.97	0.45				ar
							4.35	19.47	76.18	0.45				d
187962	4716	1554	1534	1320	1.29	0.39	2.98	21.43	75.20	0.44	5.0	96.0	1.28	ad
						1.67	2.94	21.15	74.23	0.43				ar
							2.99	21.51	75.49	0.44			4.00	d
187963	4717	607	593	523	2.31	0.70	37.47	17.25	44.58	0.34	1.0	96.2	1.60	ad
						2.99	36.61	16.85	43.55	0.33				ar
							37.73	17.37	44.89	0.34	0.5	00.0	4.07	d
187964	4718	691	684	593	1.01	0.37	12.54	18.21	68.88	0.57	2.5	98.0	1.37	ad
						1.38	12.41	18.03	68.18	0.56				ar
							12.59	18.28	69.14	0.57			1.82	ad
187965	4719	921	915	799	0.65	0.37	51.80	16.39	31.44	0.28	-	-	1.02	au
						1.02	51.46	16.28	31.24	0.28				C
			-				51.99	16.45	31.56	0.28	7.0	97.7	1.38	ac
187966	4720	532	527	457	0.94	0.52	10.99	24.29	64.20	1.03	7.0	91.1	1.30	
						1.45	10.89	24.06	63.60	1.02				aı
					0.10	0.00	11.05	24.42	64.54	1.04	7.5	97.7	1.45	a
187967	4721	3444	3369	2931	2.18	0.62	20.59	22.36	56.43	0.91	6.1	91.1	1.43	ac
						2.78	20.14	21.87	55.20	0.89				a
						0.54	20.72	22.50	56.78	0.92	8.0	97.1	1.31	ac
187968	4722	842	835	727	0.83	0.54	7.92	24.78	66.76	1.10	0.0	91.1	1.51	a
						1.37	7.85	24.57	66.20	1.09				a
					+		7.96	24.91	67.12	1.11	7.0	96.5	1.46	a
187969	4723	494	459	392	7.09	0.58	25.18	18.42	55.82	0.85	7.0	90.5	1.40	a
						7.62	23.40	17.11	51.87	0.79				(
					<b></b>		25.33	18.53	56.15	0.85	2.0	92.3	1.37	a
187970	4724	2302	2276	1975	1.13	0.64	10.64	20.48	68.24	0.54	2.0	92.3	1.37	
						1.76	10.52	20.25	67.47	0.53				а
							10.71	20.61	68.68	0.54	7.	00.4	1.00	
187971	4725	1233	1158	1001	6.08	0.55	5.86	27.06	66.53	0.53	7.5	89.4	1.28	а
						6.60	5.50	25.41	62.48	0.50				а
							5.89	27.21	66.90	0.53				
187972	4726	521	512	432	1.73	0.72	25.77	20.36	53.15	0.58	7.0	94.0	1.48	а
						2.44	25.32	20.01	52.23	0.57				а
	1	1					25.96	20.51	53.54	0.58				

<sup>\*</sup> SG checked

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<sup>+</sup> Ash checked

<sup>-</sup> Volatile checked



CLIENT:

CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

PO#:

326969WC

HOLE:

WC18-16C 187933-188012

UPDATED:

February 14, 2019

Gwil Industries Inc. 7784 - 62nd St SE Calgary, AB T2C 5K2 Tel: (403) 253-8273 Email: info@birtley.ca www.birtley.ca

Page 3 of 4

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

AB#	Sample	Wet	Dmr	Dotain		W ANALYSIS								
AD#	ID:	Wt(g)	Dry Wt (g)	Retain Wt (g) 7/8	ADM%	MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASIS
37973	4727	546	542	474	0.73	0.52	72.84	12.39	14.25	0.2			2.17	adb
						1.25	72.31	12.30	14.15	0.18				arb
			-				73.22	12.45	14.32	0.18				db
37974	4728	1540	1522	1328	1.17	0.62	11.53	18.85	69.00	0.66	1.5	99.7	1.37	adb
						1.78	11.40	18.63	68.19	0.65				arb
7075	4700						11.60	18.97	69.43	0.66				db
7975	4729	1677	1657	1432	1.19	0.69	44.36	17.61	37.34	0.45	-	-	1.70	adb
						1.87	43.83	17.40	36.89	0.44				arb
7976	4730	894	889	775	0.56	0.48	44.67 35.14	17.73 35.21	37.60	0.45	4.0	00.0	1.00	db
	1,00	054	003	,,,	0.50	1.04	34.94	35.21	29.17 29.01	0.49	1.0	98.0	1.86	adb
						1.04	35.31	35.38	29.31	0.49				arb db
7977	4731	825	792	690	4.00	0.62	13.61	20.82	64.95	0.82	6.5	96.8	1.37	adb
						4.60	13.07	19.99	62.35	0.79	0.0	50.0	1.07	arb
							13.69	20.95	65.36	0.83				db
7978	4732	1287	1229	1085	4.51	0.61	16.91	17.52	64.96	0.54	1.0	98.6	1.42	adb
						5.09	16.15	16.73	62.03	0.52				arb
7070							17.01	17.63	65.36	0.54				db
7979	4733	835	823	716	1.44	1.07	87.47	5.72	5.74	0.70	-	-	2.41	adb
1			1			2.49	86.21	5.64	5.66	0.69				arb
7980	4734	903	837	735	7.04	0.00	88.42	5.78	5.80	0.71		-		db
7 900	4134	903	637	735	7.31	0.66	8.71	18.03	72.60	0.58	1.5	98.3	1.35	adb
						7.92	8.07 8.77	16.71 18.15	67.29	0.54				arb
7981	4735	1420	1354	1180	4.65	0.71	13.70	17.99	73.08 67.60	0.58	0.5	99.4	1.39	db
					1.00	5.32	13.06	17.15	64.46	0.39	0.5	99.4	1.39	adb arb
						0.02	13.80	18.12	68.08	0.41				db
7982	4736	5812	5686	4942	2.17	0.63	8.45	19.44	71.48	0.40	2.5	98.3	1.35	adb
-						2.78	8.27	19.02	69.93	0.39				arb
							8.50	19.56	71.93	0.40				db
7983	4737	313	309	271	1.28	0.61	18.88	18.88	61.63	0.40	4.0	96.8	1.45	adb
1						1.88	18.64	18.64	60.84	0.39				arb
7984	4738	700	700				19.00	19.00	62.01	0.40				db
904	4/30	702	700	605	0.28	0.47	48.11	18.25	33.17	0.27	-	-	1.80	adb
				-		0.75	47.97 48.34	18.20	33.08	0.27				arb
985	4739	327	323	283	1.22	0.50	10.18	18.34 19.52	33.33 69.80	0.27	4.5	00.1	1.20	db
			020	200	1.22	1.72	10.16	19.28	68.95	0.65	4.5	99.1	1.36	adb arb
						, 2	10.23	19.62	70.15	0.66				db
986	4740	896	889	779	0.78	0.55	30.46	19.12	49.87	0.52	6.5	98.6	1.57	adb
						1.33	30.22	18.97	49.48	0.52	0.0	00.0	1.07	arb
							30.63	19.23	50.15	0.52				db
987	4741	567	566	489	0.18	0.54	62.21	15.64	21.61	0.23	-	-	2.05	adb
				1		0.72	62.10	15.61	21.57	0.23				arb
	17.17						62.55	15.72	21.73	0.23				db
988	4742	1235	1218	1067	1.38	0.42	9.50	20.01	70.07	0.70	5.5	98.0	1.34	adb
						1.79	9.37	19.73	69.11	0.69				arb
989	4743	050	040	720	4.00	0.41	9.54	20.09	70.37	0.70				db
203	4143	859	848	732	1.28	0.41	29.87	35.04	34.68	0.63	8.0	92.5	1.75	adb
			1			1.69	29.49	34.59	34.24	0.62				arb
990	4744	2326	2278	1990	2.06	0.54	29.99	35.18	34.82	0.63	0.0	07.1	4.00	db
	7177	2320	2210	1990	2.00	2.59	16.72 16.37	21.26	61.48	1.00	2.0	97.1	1.39	adb
						2.59	16.81	20.82	60.21	0.98				arb
991	4745	610	599	528	1.80	0.69	57.95	21.38 13.06	61.81 28.30	1.01			1.00	db
		5.5	555	323	1.00	2.48	56.91	12.82		1.01 0.99	-	-	1.86	adb
						2.40	58.35	13.15	27.79 28.50	1.02				arb
992	4746	1412	1400	1227	0.85	0.40	12.30	20.50	66.80	0.97	8.5	97.7	1.34	db adb '
			-			1.25	12.20	20.33	66.23	0.96	0.5	31.1	1.54	arb
1							12.35	20.58	67.07	0.97				db

<sup>\*</sup> SG checked

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<sup>+</sup> Ash checked

<sup>-</sup> Volatile checked



CLIENT:

CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

326969WC PO#:

HOLE:

WC18-16C & WC18-17C

LAB#:

187933-188012

UPDATED:

February 14, 2019

Gwil Industries Inc. 7784 - 62nd St SE Calgary, AB T2C 5K2 Tel: (403) 253-8273 Email: info@birtley.ca www.birtley.ca

Page 4 of 4

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

						W ANALYSIS			E 0 2/	00'	ECI	9/ ! T	22	BASIS
LAB#	Sample	Wet	Dry	Retain	ADM%	MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASIS
	ID:	Wt(g)	Wt (g)	Wt (g) 7/8		2.50	11.00	40.44	CE 07	0.85	1.5	97.7	1.36	adl
87993	4747	2280	2258	1946	0.96	0.50	14.22	19.41	65.87		1.5	91.1	1.50	ar
						1.46	14.08	19.22	65.23	0.84				d
							14.29	19.51	66.20	0.85	1.0	91.7	1.42	ad
87994	4748	169	165	147	2.37	0.97	15.01	21.57	62.45	0.90	1.0	91.7	1.42	ar
						3.31	14.65	21.06	60.97	0.88				d
							15.16	21.78	63.06	0.91	1.5	94.2	1.58	ad
87995	4749	2132	2085	1779	2.20	1.14	35.19	18.43	45.24	0.69	1.5	94.2	1.50	ar
						3.32	34.41	18.02	44.24	0.67 0.70				d
							35.60	18.64	45.76 59.26	0.75	0.0	94.5	1.45	ad
87996	4750	706	688	595	2.55	0.96	20.30	19.48		0.73	0.0	34.5	1.45	ar
						3.49	19.78	18.98	57.75 59.83	0.75				d
							20.50	19.67	54.77	0.78	0.0	97.4	1.51	ad
87997	4751	1621	1582	1382	2.41	1.10	20.20	23.93		0.56	0.0	31.4	1.51	ar
						3.48	19.71	23.35	53.45	0.57				d
				<u> </u>			20.42	24.20	55.38	0.66	0.5	96.2	1.34	ad
87998	4752	911	888	771	2.52	0.83	5.05	22.37	71.75	0.64	0.5	90.2	1.54	ar
						3.33	4.92	21.81	69.94	0.67				c
					4.40	0.05	5.09	22.56	72.35	0.47	2.0	98.3	1.38	ac
87999	4753	2637	2600	2250	1.40	0.65	10.26	20.42 20.13	68.67 67.71	0.47	2.0	30.3	1.50	a
						2.04	10.12		69.12	0.40				0
						0.50	10.33	20.55	71.96	0.47	8.0	96.5	1.02	ac
188000	4754	5805	5737	4974	1.17	0.58	3.17		71.96	0.43	0.0	30.5	1.02	a
						1.74	3.13	24.01	72.38	0.44				0
				7.0	0.05	0.40	3.19	24.43	69.85	0.45	7.0	97.4	1.33	ac
88001	4755	880	862	746	2.05	0.49	7.73	21.48	68.42	0.93	7.0	31.4	1.00	a
						2.53	7.57	22.04	70.19	0.95				-
				450	111	0.43	7.77 30.37	19.51	49.69	0.65	7.0	96.8	1.54	a
188002	4756	525	519	452	1.14		30.02	19.31	49.12	0.64	1.0	30.0	1.01	a
						1.57	30.50	19.59	49.90	0.65				-
		455	405	388	4.40	0.56	37.45	18.17	43.82	0.60	6.0	97.7	1.62	a
188003	4757	455	435	366	4.40	4.93	35.80	17.37	41.89	0.57	0.0	•		а
						4.93	37.66	18.27	44.07	0.60				
100001	4750	4400	1112	962	1.24	0.53	7.00	19.26	73.21	0.68	2.5	98.6	1.34	a
188004	4758	1126	1112	962	1.24	1.77	6.91	19.02	72.30	0.67				а
				1		1.77	7.04	19.36	73.60	0.68				
400005	4759	1135	1127	1000	0.70	0.43	74.54	14.62	10.41	0.13	-	-	2.26	a
188005	4/59	1133	1121	1000	0.10	1.13	74.01	14.52	10.34	0.13				а
						1.10	74.86	14.68	10.45	0.13				
100006	4760	636	612	526	3.77	0.44	17.34	20.47	61.75	0.68	7.0	97.4	1.41	а
188006	4/00	030	012	320	0.77	4.20	16.69	19.70	59.42	0.65				a
						4.20	17.42	20.56	62.02	0.68				
188007	4761	693	658	576	5.05	0.64	54.12	13.36	31.88	0.43	0.5	98.6	1.86	а
100001	4/01	093	000	3,0	0.00	5.66	51.39	12.69	30.27	0.41				á
						0.00	54.47	13.45	32.09	0.43				
188008	4762	205	202	164	1.46	0.45	28.01	16.18	55.36	0.63	1.0	99.7	1.52	а
100008	4102	200	202	104	1.40	1.91	27.60	15.94	54.55	0.62				á
						1.01	28.14	16.25	55.61	0.63				
188009	4763	681	672	585	1.32	0.53	48.42	15.48	35.57	0.50	-	-	1.79	a
100009	4/03	001	012	303	1.02	1.84	47.78	15.28	35.10	0.49				
						1.0-4	48.68	15.56	35.76	0.50				
400040	4764	2352	2311	1961	1.74	0.63	15.77	17.14	66.46	0.51	1.0	98.0	1.42	ē
188010	4/64	2352	2311	1901	1.74	2.36	15.50	16.84	65.30	0.50				
						2.30	15.87	17.25	66.88	0.51				
10051	4=4=	4057	1005	1050	1.64	0.73	5.14	19.53	74.60	0.40	2.0	98.6	1.33	
188011	4765	1957	1925	1658	1.04		5.14	19.33	73.38	0.39	2.0	30.0		
	-					2.35	5.18	19.67	75.15	0.40				
			F. 65	4504	0.00	0.54		20.19	72.97	0.40	2.5	97.4	1.33	
188012	4766	5245	5139	4504	2.02	0.54	6.30		71.50	0.36	2.5	31.4	1.00	
	1	1			1	2.55	6.17	19.78	11.50	0.36				,

<sup>\*</sup> SG checked

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<sup>+</sup> Ash checked

Volatile checked



CLIENT:

CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

PO#:

326969W0

HOLE:

WC18-17C & WC18-18C

LAB#:

188013-188092

UPDATED:

February 14, 2019

Gwil Industries Inc. 7784 - 62nd St SE Calgary, AB T2C 5K2 Tel: (403) 253-8273 Email: info@birtley.ca www.birtley.ca

Page 1 of 4

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

						W ANALYSIS	, air drie	d basis						
LAB#	Sample ID:	Wet Wt(g)	Dry Wt (g)	Retain Wt (g) 7/8	ADM%	MOIST%	ASH%	VOL%	F.C.%	5%	FSI	%LT	SG	BASI
188013	4767	834	826	729	0.96	0.45	7.06	19.62	72.87	0.67	3.5	98.8	1.34	ad
						1.40	6.99	19.43	72.17	0.66				ar
188014	4768	741	738	646	0.40		7.09	19.71	73.20	0.67				d
100014	4/00	741	738	646	0.40	0.55	44.80	18.17	36.48	0.38	4.0	97.1	1.74	ad
						0.95	44.62	18.10	36.33	0.38				ar
188015	4769	1145	1138	836	0.61	0.50	45.05 37.85	18.27 17.16	36.68 44.49	0.38	4.0			d
		1140	1100	550	0.01	1.11	37.62	17.16	44.49	0.42 0.42	1.0	97.7	1.65	adi
							38.04	17.25	44.71	0.42				art di
188016	4770	3277	3245	2812	0.98	0.42	31.05	22.80	45.73	0.85	1.0	97.7	1.59	adl
						1.39	30.75	22.58	45.28	0.84	1.0	31.1	1.55	art
							31.18	22.90	45.92	0.85				di
188017	4771	959	953	831	0.63	0.41	6.97	23.05	69.57	1.13	8.5	98.3	1.31	adh
				İ		1.03	6.93	22.91	69.13	1.12				art
							7.00	23.14	69.86	1.13				db
188018	4772	568	556	479	2.11	0.59	37.25	15.90	46.26	0.64	4.5	97.1	1.61	adb
						2.69	36.46	15.56	45.28	0.63				art
188019	4773	739	733		224		37.47	15.99	46.53	0.64				db
100019	4//3	139	133	637	0.81	0.80	31.03	16.37	51.80	0.66	5.0	99.1	1.55	adb
						1.61	30.78	16.24	51.38	0.65				arb
188020	4774	1590	1580	1384	0.63	0.53	31.28	16.50	52.22	0.67				db
100020	7,,,	1550	1300	1304	0.63	1.16	48.11 47.81	12.79	38.57	0.58	6.5	99.1	1.73	adb
						1.10	48.37	12.71 12.86	38.33 38.78	0.58 0.58				arb
188021	4775	977	939	829	3.89	1.44	19.55	21.66	57.35	0.92	0.5	62.8	1.49	db adb
				520	0.00	5.27	18.79	20.82	55.12	0.88	0.5	02.6	1.49	adb
							19.84	21.98	58.19	0.93				db
188022	4776	216	215	179	0.46	0.83	66.24	15.33	17.60	0.29	0.0	93.1	2.12	adb
						1.29	65.93	15.26	17.52	0.29	0.0	00.1		arb
							66.79	15.46	17.75	0.29				db
188023	4777	911	875	774	3.95	1.12	18.94	20.57	59.37	0.85	0.5	91.1	1.40	adb
						5.03	18.19	19.76	57.02	0.82				arb
							19.15	20.80	60.04	0.86				db
188024	4778	1313	1289	1119	1.83	1.20	54.30	12.71	31.79	0.44	0.0	94.0	1.86	adb
						3.01	53.31	12.48	31.21	0.43				arb
188025	4779	517	503	441	2.71	444	54.96	12.86	32.18	0.45				db
100025	4113	317	503	441	2.71	1.14 3.82	10.03	22.80	66.03	0.76	0.0	95.4	1.40	adb
				1		3.62	9.76 10.15	22.18 23.06	64.24 66.79	0.74				arb
188026	4780	1005	987	862	1.79	1.11	19.35	25.41	54.13	0.77	0.0	93.4	1.52	db
			007	002	1.13	2.88	19.00	24.95	53.16	0.60	0.0	93.4	1.52	adb
						2.00	19.57	25.70	54.74	0.62				arb db
188027	4781	1195	1171	1017	2.01	1.12	4.07	22.68	72.13	0.65	0.5	94.8	1.32	adb
- 1			1			3.11	3.99	22.22	70.68	0.64	0.0	34.0	1.02	arb
							4.12	22.94	72.95	0.66				db
188028	4782	6665	6558	5733	1.61	1.23	9.48	20.00	69.29	0.47	0.0	98.0	1.40	adb
						2.82	9.33	19.68	68.18	0.46				arb
							9.60	20.25	70.15	0.48				db
188029	4783	5567	5463	4766	1.87	0.89	2.37	24.13	72.61	0.52	3.5	97.4	1.29	adb
1						2.74	2.33	23.68	71.25	0.51				arb
10005							2.39	24.35	73.26	0.52				db
188030	4784	1005	941	841	6.37	0.64	35.50	16.58	47.28	0.57	3.5	98.3	1.57	adb
						6.97	33.24	15.52	44.27	0.53				arb
100004	4705	4047	4705	4555	4.45		35.73	16.69	47.58	0.57				db
88031	4785	1817	1796	1550	1.16	0.50	12.60	18.85	68.05	0.66	1.5	98.6	1.39	adb
						1.65	12.45	18.63	67.26	0.65				arb
88032	4786	1104	1150	4046	0.46		12.66	18.94	68.39	0.66	***************************************			db
00032	4/80	1164	1159	1010	0.43	0.66	79.39	14.92	5.03	80.0	-	-	2.37	adb
				1		1.09	79.05	14.86	5.01	0.08				arb
					~		79.92	15.02	5.06	0.08				db

<sup>\*</sup> SG checked

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<sup>+</sup> Ash checked

<sup>-</sup> Volatile checked



CLIENT:

CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

PO#:

326969WC

HOLE:

WC18-18C, WC18-19C & WC18-20C

LAB#:

188013-188092

UPDATED:

February 14, 2019

Page 2 of 4

Gwil Industries Inc. 7784 - 62nd St SE

Email: info@birtley.ca www.birtley.ca

Calgary, AB T2C 5K2 Tel: (403) 253-8273

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

						ANALYSIS, a					501	0/17		DACIC
LAB#	Sample ID:	Wet Wt(g)	Dry Wt (g)	Retain Wt (g) 7/8	ADM%	MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASIS
88033	4787	1058	1049	910	0.85	0.45	9.05	21.56	68.94	0.75	7.5	98.0	1.33	ad
00033	4101	1030	1043	0.0	0.00	1.30	8.97	21.38	68.35	0.74				ar
						7.00	9.09	21.66	69.25	0.75				d
88034	4788	542	539	488	0.55	0.58	18.92	16.03	64.47	0.56	2.0	99.7	1.47	ad
100034	4100	542	000	100	0.00	1.13	18.82	15.94	64.11	0.56				ar
							19.03	16.12	64.85	0.56				d
188035	4789	798	791	696	0.88	0.71	82.78	6.90	9.61	0.15	-	-	2.34	ad
100033	4103	130	101	000	0.00	1.58	82.05	6.84	9.53	0.15				ar
							83.37	6.95	9.68	0.15				d
188036	4790	1787	1767	1553	1.12	0.48	5.44	21.03	73.05	0.82	7.0	98.6	1.30	ad
100000	4.00	1101				1.59	5.38	20.79	72.23	0.81				ar
							5.47	21.13	73.40	0.82				d
188037	4791	1867	1851	1620	0.86	0.49	21.32	16.58	61.61	0.89	1.0	99.7	1.47	ad
100001	4,5.	1007				1.34	21.14	16.44	61.08	0.88				ar
							21.42	16.66	61.91	0.89				d
188038	4792	440	428	386	2.73	0.48	58.77	14.93	25.82	0.31	-	-	2.00	ad
. 20000						3.19	57.17	14.52	25.12	0.30				a
							59.05	15.00	25.94	0.31				C
188039	4793	403	395	351	1.99	0.46	80.64	20.02	-1.12	0.13	-	-	2.41	ac
						2.44	79.04	19.62	-1.10	0.13				a
							81.01	20.11	-1.13	0.13				
188040	4794	1217	1199	1045	1.48	0.85	58.73	10.65	29.77	0.24	-	-	1.95	ac
						2.32	57.86	10.49	29.33	0.24				aı
							59.23	10.74	30.03	0.24				
188041	4795	3055	2989	2629	2.16	0.61	3.14	19.60	76.65	0.43	1.0	98.0	1.32	ac
						2.76	3.07	19.18	74.99	0.42	•	•		a
							3.16	19.72	77.12	0.43				
188042	4796	6416	6312	5513	1.62	0.52	5.52	20.79	73.17	0.43	4.5	98.6	1.34	ac
						2.13	5.43	20.45	71.98	0.42				a
							5.55	20.90	73.55	0.43		00.4	1.29	ac
188043	4797	1593	1583	1384	0.63	0.54	3.91	19.29	76.26	0.69	1.5	99.1	1.29	
						1.16	3.89	19.17	75.78	0.69				a
							3.93	19.39	76.67	0.69	4.0	98.8	1.59	
188044	4798	887	882	777	0.56	0.50	35.19	18.88	45.43	0.43	4.0	98.8	1.59	a
						1.06	34.99	18.77	45.17	0.43				(
							35.37	18.97	45.66	0.43			2.13	a
188045	4799	1016	1014	902	0.20	0.36	67.63	15.41	16.60	0.15 0.15	-	-	2.13	a
						0.56	67.50	15.38	16.57	0.15				(
							67.87	15.47	16.66		5.5	98.0	1.35	a
188046	4800	1514	1505	1323	0.59	0.47	6.03	20.69	72.81	0.65 0.65	5.5	90.0	1.33	a
						1.06	5.99	20.57	72.38 73.15	0.65				١
	1	165:	1050	4100		0.40	6.06	9.91	25.68	0.65	_		1.90	a
188047	4801	1261	1258	1108	0.24	0.48	63.93	9.91	25.68	0.25	-	-	1.50	a
						0.72	63.78 64.24	9.89	25.80	0.25				
	10	4001	4050	1010	2.40	1 14	14.95	18.39	65.52	0.23	0.5	95.7	1.41	a
188048	4802	1894	1853	1618	2.16	1.14		17.99	64.10	0.66	0.5	33.1		a
						3.28	14.63	18.60	66.28	0.68				
				0.100	4.57	0.50	15.12	19.85	65.13	0.37	1.5	99.1	1.40	а
188049	4803	3576	3520	3120	1.57	0.52	14.50	19.55	64.11	0.36	1.5	33.1	1.40	á
						2.08	14.27	19.54	65.47	0.37				
			100	050	0.74	0.40	14.58	25.54	64.42	1.01	7.5	98.0	1.35	а
188050	4804	425	422	350	0.71	0.42	9.62		63.97	1.00	1.5	30.0	1.55	á
						1.12	9.55	25.36 25.65	64.69	1.00				•
				<u> </u>	1		9.66			0.97	1.0	42.8	1.40	a
188051	4805	1122	1067	934	4.90	1.34	17.29	22.26	59.11		1.0	42.0	1.40	
						6.18	16.44	21.17	56.21	0.92				,
					<u> </u>		17.52	22.56	59.91	0.98			1.81	
188052	4806	425	405	368	4.71	0.87	56.29	13.14	29.70	0.52	-	-	1.61	č
				1		5.53	53.64	12.52	28.30	0.50				,
	1						56.78	13.26	29.96	0.52				

<sup>\*</sup> SG checked

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<sup>+</sup> Ash checked

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CLIENT:

CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

PO#:

326969WC

HOLE:

WC18-20C 188013-188092

UPDATED:

February 14, 2019

Page 3 of 4

Gwil Industries Inc. 7784 - 62nd St SE Calgary, AB T2C 5K2

Tel: (403) 253-8273 Email: info@birtley.ca

www.birtley.ca

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

	1				HEAD RA	W ANALYSIS	, air dried	d basis		-				
LAB#	Sample	1	Dry	Retain	ADM%	MOIST%	ASH%	VOL%	F.C.%	5%	FSI	%LT	SG	BASI
100050	ID:	Wt(g)	Wt (g)	Wt (g) 7/8		T-17-17-1								
188053	4807	2743	2714	2378	1.06	0.57	10.10	25.89	63.44	0.91	5.5	97.4	1.36	ac
						1.62	9.99	25.62	62.77	0.90				aı
	-						10.16	26.04	63.80	0.92				c
188054	4808	860	854	738	0.70	0.58	34.97	16.99	47.46	0.45	2.0	98.3	1.58	ad
						1.27	34.73	16.87	47.13	0.45				ar
							35.17	17.09	47.74	0.45				d
188055	4809	1281	1273	1112	0.62	0.75	13.30	19.59	66.36	0.42	1.5	97.4	1.40	ad
						1.37	13.22	19.47	65.95	0.42				ar
400050	1010						13.40	19.74	66.86	0.42				d
188056	4810	2195	2173	1895	1.00	0.78	28.58	18.54	52.10	0.55	3.0	98.6	1.53	ad
						1.77	28.29	18.35	51.58	0.54				ar
100057	4044	5055	5400				28.80	18.69	52.51	0.55				d
188057	4811	5255	5128	4466	2.42	0.87	15.45	21.59	62.09	0.42	7.5	97.7	1.41	ad
						3.27	15.08	21.07	60.59	0.41				ari
188058	4812	1000	4000	4400			15.59	21.78	62.63	0.42				dl
100036	4012	1690	1629	1498	3.61	0.79	18.15	21.37	59.69	0.56	7.5	97.1	1.41	adl
						4.37	17.49	20.60	57.54	0.54				arl
188059	4813	678	674	507	0.50	0.00	18.29	21.54	60.17	0.56				dl
100039	4013	0/6	674	587	0.59	0.68	4.67	20.34	74.31	0.57	4.0	97.1	1.32	adl
						1.27	4.64	20.22	73.87	0.57				art
188060	4814	1033	1027	204	0.50	0.75	4.70	20.48	74.82	0.57				dl
100000	4014	1033	1027	894	0.58	0.75	81.24	14.48	3.53	0.12	-	-	2.38	adh
						1.33	80.77	14.40	3.51	0.12				art
188061	4815	830	809	715	2.52	0.00	81.86	14.59	3.55	0.12				di
100001	4013	030	009	/15	2.53	0.66	17.80	20.47	61.07	0.57	7.0	98.0	1.42	adl
						3.17	17.35	19.95	59.52	0.56				art
188062	4816	1186	1168	1034	1.52	0.52	17.92	20.61	61.48	0.57				dl
.00002	4010	1100	1100	1034	1.52	2.03	12.03	19.56	67.89	0.65	4.5	98.3	1.37	adl
						2.03	11.85 12.09	19.26 19.66	66.86	0.64				art
188063	4817	514	513	443	0.19	0.53	25.32	16.03	68.24 58.12	0.65	1.0	00.0	4.50	dt
		• • •	0.0	110	0.13	0.72	25.27	16.00	58.01	0.78	1.0	98.8	1.52	adh
			-			0.72	25.45	16.12	58.43	0.78 0.78				art
188064	4818	421	420	358	0.24	0.44	69.20	14.06	16.30	0.78			2.21	dt
				-	0.21	0.68	69.04	14.03	16.26	0.27	-	-	2.21	adb
						0.00	69.51	14.12	16.37	0.27				arb db
188065	4819	1958	1948	1703	0.51	0.53	8.31	18.25	72.91	0.71	1.5	99.1	1.41	adb
						1.04	8.27	18.16	72.54	0.71	1.5	33.1	1.71	arb
							8.35	18.35	73.30	0.71				db
188066	4820	2264	2239	1932	1.10	0.57	6.25	19.63	73.55	0.63	1.5	98.6	1.35	adb
						1.67	6.18	19.41	72.74	0.62		55.0	1.55	arb
							6.29	19.74	73.97	0.63				db
188067	4821	1214	1205	934	0.74	0.44	2.51	21.34	75.71	0.63	5.5	98.8	1.31	adb
						1.18	2.49	21.18	75.15	0.63	2.0	55.0		arb
							2.52	21.43	76.04	0.63				db
188068	4822	892	864	742	3.14	0.41	22.96	18.36	58.27	0.39	1.5	98.3	1.48	adb
						3.54	22.24	17.78	56.44	0.38	1.5	55.5	170	arb
							23.05	18.44	58.51	0.39				db
88069	4823	751	744	647	0.93	0.38	2.84	20.19	76.59	0.42	4.0	98.6	1.31	adb
						1.31	2.81	20.00	75.88	0.42	4.0	30.0	1.51	arb
							2.85	20.27	76.88	0.42				db
88070	4824	400	399	342	0.25	0.53	65.32	15.42	18.73	0.12	1.0	99.1	2.08	adb
						0.78	65.16	15.38	18.68	0.12	1.0	33.1	2.00	arb
							65.67	15.50	18.83	0.12				
88071	4825	948	941	825	0.74	0.52	15.88	17.21	66.39	0.12	2.0	99.4	1 / 1	db
					<b>○</b> ⊤	1.25	15.76	17.08	65.90	0.43	2.0	55.4	1.41	adb
						1.20	15.76	17.30	66.74					arb
88072	4826	2015	2003	1442	0.60	0.54	26.71	18.99	53.76	0.43	2.0	00.2	1 50	db
					0.00	1.13	26.55	18.88	53.44		2.0	98.3	1.52	adb
1						1.10	26.86	19.09	54.05	0.41				arb
					-		20.00	13.03	37.00	0.41		v		di

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CLIENT:

CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

PO#:

WC18-20C, WC18-21C &18C-22C

HOLE: LAB#:

188013-188092

326969WC

UPDATED:

February 14, 2019

Page 4 of 4

Gwil Industries Inc. 7784 - 62nd St SE

Email: info@birtley.ca www.birtley.ca

Calgary, AB T2C 5K2 Tel: (403) 253-8273

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

AD # 1	C	Wet	D	Retain	ADM%	W ANALYSIS MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASI
AB#	Sample		Dry		ADIVI76	IVIOIS 176	ASII //	VOL 76	1.0.70	<b>5</b> /0		,,_,		
88073	ID: 4827	Wt(g) 1115	Wt (g) 1101	Wt (g) 7/8 829	1.26	0.61	8.13	21.56	69.70	0.66	7.5	99.1	1.33	ad
000/3	4021	1113	1101	025	1.20	1.86	8.03	21.29	68.82	0.65				а
							8.18	21.69	70.13	0.66				(
88074	4828	3866	3820	3350	1.19	0.51	14.41	21.64	63.44	0.86	7.0	99.4	1.40	a
00014	4020	0000	0020			1.69	14.24	21.38	62.69	0.85				а
							14.48	21.75	63.77	0.86				(
88075	4829	814	812	691	0.25	0.47	46.78	13.23	39.52	0.53	1.0	99.7	1.74	a
000.0	4020	011	• .=			0.71	46.67	13.20	39.42	0.53				а
							47.00	13.29	39.71	0.53				
88076	4830	1165	1162	998	0.26	0.32	45.51	42.84	11.33	0.30	1.5	98.8	2.22	а
00010	1000					0.58	45.39	42.73	11.30	0.30				а
							45.66	42.98	11.37	0.30				
88077	4831	634	630	552	0.63	0.56	10.23	21.03	68.18	1.10	9.0	99.4	1.34	a
						1.19	10.17	20.90	67.75	1.09				а
							10.29	21.15	68.56	1.11				
88078	4832	1472	1463	1286	0.61	0.67	29.81	17.59	51.93	0.75	7.5	99.4	1.55	а
						1.28	29.63	17.48	51.61	0.75				a
							30.01	17.71	52.28	0.76				
88079	4833	1007	999	889	0.79	0.51	10.31	19.68	69.50	0.99	7.5	99.1	1.35	а
						1.30	10.23	19.52	68.95	0.98				a
							10.36	19.78	69.86	1.00				
88080	4834	2981	2963	2618	0.60	0.49	12.21	19.37	67.93	0.75	3.0	99.4	1.40	а
						1.09	12.14	19.25	67.52	0.75				á
							12.27	19.47	68.26	0.75			1.46	
88081	4835	899	881	772	2.00	0.66	20.26	17.30	61.78	0.93	1.0	97.7	1.49	a
						2.65	19.85	16.95	60.54	0.91				1
							20.39	17.41	62.19	0.94		00.4	1.44	
88082	4836	662	653	573	1.36	0.61	15.69	16.63	67.07	0.91	1.0	99.1	1.44	a
						1.96	15.48	16.40	66.16	0.90				•
							15.79	16.73	67.48	0.92	4.5	93.1	1.36	a
88083	4837	3000	2804	2448	6.53	0.73	7.39	19.15	72.73	0.70 0.65	1.5	93.1	1.30	
						7.22	6.91	17.90	67.98	0.65				'
							7.44	19.29	73.26	0.71	6.0	97.7	1.34	ā
88084	4838	2087	2050	1772	1.77	0.52	8.08	20.92	70.48	0.49	0.0	91.1	1.54	•
						2.28	7.94	20.55	69.23 70.85	0.49				
						0.00	8.12	21.03	77.03	0.49	2.0	98.8	1.33	8
188085	4839	608	599	528	1.48	0.62	3.00	19.35 19.06	75.89	0.34	2.0	30.0	1.00	
						2.09	2.96		77.51	0.35				
					4.55	0.50	3.02	19.47 19.51	58.01	0.35	2.5	97.4	1.48	- 6
188086	4840	1616	1591	1381	1.55	0.56	21.92			0.33	2.5	31.4	1.40	,
						2.10	21.58	19.21 19.62	57.11 58.34	0.35				
				004	4.00	0.53	22.04 79.47	14.79	5.21	0.14			2.24	
188087	4841	300	297	264	1.00		78.68	14.79	5.16	0.14				
						1.52		14.87	5.10	0.14				
				4077	5.04	0.50	79.89	19.44	68.74	0.17	3.0	99.7	1.37	
188088	4842	1536	1459	1277	5.01	0.56	11.26	18.47	65.29	0.47	3.0	33.1	1.01	
						5.54	10.70	19.55	69.13	0.43				
	<u> </u>	1			4.10	0.57	11.32 13.45	23.66	62.32	0.47	8.5	97.4	1.36	i
188089	4843	1000	959	833	4.10		12.90	22.69	59.76	0.60	0.5	57.4	1.50	
						4.65		23.80	62.68	0.63				
	1000		0101	2004	4.04	0.40	13.53	23.29	58.58	1.21	7.0	98.0	1.45	,
188090	4844	3253	3194	2801	1.81	0.42	17.71	23.29	57.52	1.19	1.0	30.0	1,-10	
						2.23	17.39		57.52 58.83	1.19				
					+,	0.10	17.78	23.39		1.04	8.5	98.0	1.41	
188091	4845	825	811	700	1.70	0.42	15.48	23.35	60.75		0.0	90.0	11	
						2.11	15.22	22.95	59.72	1.02 1.04				
						1.0=	15.55	23.45	61.01	0.93	1,5	70.2	1.46	
188092	4846	1435	1389	1220	3.21	1.27	16.72	21.80		0.93	1.5	10.2	1.40	5
	1	1			1	4.43	16.18 16.94	21.10 22.08	58.28 60.98	0.90				

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CLIENT:

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PROJECT:

Willow Creek development drilling

PO#:

326969WC

HOLE:

WC18-22C

REPORT DATE:

188093-171 February 20, 2019

Page 1 of 4

Gwil Industries Inc. 7784 - 62nd St SE Calgary, AB T2C 5K2

Tel: (403) 253-8273 Email: info@birtley.ca

www.birtley.ca

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

LAB#	Sample ID:	Wet Wt(g)	Dry Wt (g)	Retain Wt (g) 7/8	ADM%	MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BAS
188093	4847	364	356	317	2.20	1.05	67.48	10.53	20.94	0.28	-		2.06	ac
						3.22	66.00	10.30	20.48	0.27			2.00	a
							68.20	10.64	21.16	0.28				(
188094	4848	1113	1074	947	3.50	0.43	36.76	16.96	45.85	0.66	0.5	84.1	1.62	ac
						3.92	35.47	16.37	44.24	0.64				а
							36.92	17.03	46.05	0.66				C
188095	4849	709	693	619	2.26	0.99	54.32	12.69	32.00	0.45	-	-	1.88	ac
						3.22	53.09	12.40	31.28	0.44				a
188096	4850	525	486	437	7.40	0.74	54.86	12.82	32.32	0.45				
100030	4030	323	400	437	7.43	0.74 8.11	52.50 48.60	14.88	31.88	0.63	-	-	1.84	ac
						0.11	52.89	13.77 14.99	29.51 32.12	0.58 0.63				a
188097	4851	3759	3595	3130	4.36	1.04	9.89	22.21	66.86	0.84	1.5	60.1	1.36	ac
		.,	0000	0.00	4.00	5.36	9.46	21.24	63.94	0.80	1.5	00.1	1.30	aı
						0.00	9.99	22.44	67.56	0.85				d
188098	4852	533	525	462	1.50	0.37	38.11	16.75	44.77	0.72	1.5	94.0	1.62	ad
						1.87	37.54	16.50	44.10	0.71				ar
							38.25	16.81	44.94	0.72				d
188099	4853	1265	1246	1083	1.50	0.36	20.93	18.56	60.15	0.45	1.0	96.5	1.44	ad
						1.86	20.62	18.28	59.25	0.44				ar
							21.01	18.63	60.37	0.45	-			d
188100	4854	764	753	656	1.44	0.71	60.68	10.95	27.66	0.65	-	-	1.89	ad
						2.14	59.81	10.79	27.26	0.64				ar
188101	4855	1070	4000	000	4.70	0.45	61.11	11.03	27.86	0.65				d
100101	4000	1079	1060	922	1.76	0.45	13.80	18.90	66.85	2.09	3.5	96.0	1.39	ad
						2.20	13.56	18.57	65.67	2.05				ar
188102	4856	3799	3641	3170	4.16	0.45	13.86 5.92	18.99 22.38	67.15 71.25	2.10	7.5	02.4	1 21	d
100 102		0,00	0041	3110	4.10	4.59	5.67	21.45	68.29	1.22 1.17	7.5	93.4	1.31	ad
						4.55	5.95	22.48	71.57	1.23				ar d
188103	4857	1189	1161	1027	2.35	0.71	51.27	13.93	34.09	0.61			1.74	ad
						3.05	50.06	13.60	33.29	0.60			1.7	ar
							51.64	14.03	34.33	0.61				d
188104	4858	1193	1151	1004	3.52	0.56	42.40	15.23	41.81	0.59	-	-	1.63	ad
1						4.06	40.91	14.69	40.34	0.57				ar
		20.20					42.64	15.32	42.05	0.59				d
188105	4859	2016	1978	1727	1.88	0.48	15.85	22.41	61.26	0.67	7.0	97.7	1.38	ad
1						2.36	15.55	21.99	60.11	0.66				аг
100100	4000	4555	4500	1000			15.93	22.52	61.56	0.67				d
188106	4860	1555	1526	1339	1.86	0.33	9.69	19.06	70.92	0.67	2.5	98.8	1.34	ad
1						2.19	9.51	18.70	69.60	0.66				arl
188107	4861	930	921	807	0.97	0.47	9.72 80.62	19.12 12.39	71.15	0.67			2.22	d
100.01	4001	330	321	807	0.51	1.43	79.84		6.52		-	-	2.33	adl
						1.43	81.00	12.27 12.45	6.46 6.55	0.14				ari
188108	4862	696	680	601	2.30	0.39	9.72	20.84	69.05	0.14	4.5	98.3	1.34	di adi
		300	555	301	2.00	2.68	9.50	20.36	67.46	0.76	4.3	90.3	1.34	adi
						2.00	9.76	20.92	69.32	0.78				arı di
188109	4863	663	650	566	1.96	0.72	82.09	6.96	10.23	0.18			2.27	adl
					•	2.67	80.48	6.82	10.03	0.18	-	-	4.41	arl
							82.69	7.01	10.30	0.18				di
188110	4864	2020	1961	1708	2.92	1.02	10.37	17.73	70.88	0.57	0.5	98.3	1.38	adl
						3.91	10.07	17.21	68.81	0.55				ari
							10.48	17.91	71.61	0.58				di
188111	4865	577	560	496	2.95	0.70	13.17	18.43	67.70	0.61	0.5	97.4	1.38	ad
1						3.63	12.78	17.89	65.71	0.59				ar
							13.26	18.56	68.18	0.61				di
188112	4866	369	367	326	0.54	0.43	42.57	15.76	41.24	0.44	-	-	1.69	adi
						0.97	42.34	15.67	41.02	0.44				art
	1		1	- 1			42.75	15.83	41.42	0.44				di

<sup>+</sup> Ash checked

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<sup>-</sup> Volatile checked



CLIENT:

CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

326969WC PO#:

HOLE:

WC18-22C, WC18-23C & WC18-24C

LAB#:

188093-171

REPORT DATE:

February 20, 2019

Gwil Industries Inc. 7784 - 62nd St SE Calgary, AB T2C 5K2 Tel: (403) 253-8273 Email: info@birtley.ca www.birtley.ca

Page 2 of 4

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

						W ANALYSIS								D.4.010
LAB#	Sample	Wet	Dry	Retain	ADM%	MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASIS
	ID:	Wt(g)	Wt (g)	Wt (g) 7/8				17.10	20.07	0.50	2.0	99.1	1.47	odh
188113	4867	2929	2877	2519	1.78	0.41	20.06	17.46	62.07	0.53	2.0	99.1	1.47	adb arb
						2.18	19.70	17.15	60.97	0.52				db
						0.50	20.14	17.53	62.33	0.53	2.5	97.4	1.31	adb
188114	4868	2729	2686	2332	1.58	0.52	4.34	19.51	75.63	0.39	2.5	97.4	1.31	arb
						2.09	4.27	19.20	74.44	0.38				db
				1000	101	0.50	4.36	19.61	76.03	0.39	6.0	98.0	1.33	adb
188115	4869	5009	4947	4320	1.24	0.50	6.44	23.40	69.66	0.38	6.0	96.0	1.55	arb
						1.73	6.36	23.11	68.80	0.38				db
			0050	1704	4.04	0.50	6.47	23.52 19.51	70.01 53.09	0.38	6.5	96.5	1.51	adb
188116	4870	2099	2059	1794	1.91	0.50	26.90			0.32	0.5	30.5	1.51	arb
						2.40	26.39 27.04	19.14	52.08 53.36	0.32				db
				070	0.07	0.43	1000 0000000000000000000000000000000000	19.61	62.08	0.33	1.5	98.3	1.45	adb
188117	4871	1138	1127	979	0.97		19.42		61.48	0.42	1.5	30.3	1.45	arb
						1.39	19.23	17.90 18.15	62.35	0.42				db
			0000	1707	0.89	0.44	19.50 16.50	19.70	63.36	0.42	4.5	97.7	1.41	adb
188118	4872	2021	2003	1707	0.89	1.33		19.70	62.80	0.48	4.5	31.1	1.41	arb
						1.33	16.35 16.57	19.79	63.64	0.48				db
100440	4072	687	681	596	0.87	0.23	16.16	27.60	56.01	0.45	8.5	97.4	1.46	adb
188119	4873	180	180	290	0.01	1.10	16.02	27.36	55.52	0.94	0.0	51.4	1.45	arb
						1.10	16.20	27.66	56.14	0.95				db
400400	4874	565	560	493	0.88	0.84	15.52	17.98	65.66	0.93	0.5	97.7	1.43	adb
188120	40/4	303	360	493	0.00	1.72	15.38	17.82	65.08	0.92	0.0	01.7		arb
						1.72	15.65	18.13	66.22	0.94				db
188121	4875	493	491	428	0.41	0.53	13.44	17.67	68.36	0.60	2.0	99.4	1.41	adb
100121	46/3	493	431	420	0.41	0.93	13.39	17.60	68.08	0.60				arb
						0.00	13.51	17.76	68.72	0.60				db
188122	4876	1859	1841	1599	0.97	0.56	4.05	18.90	76.49	0.62	2.5	98.0	1.33	adb
100122	4010	1000	1041	1000	0.01	1.52	4.01	18.72	75.75	0.61				art
							4.07	19.01	76.92	0.62				dt
188123	4877	199	198	177	0.50	0.49	37.56	14.46	47.49	0.28	1.5	98.8	1.64	adb
100120						0.99	37.37	14.39	47.25	0.28				art
							37.74	14.53	47.72	0.28				db
188124	4878	1318	1300	1121	1.37	0.70	3.16	19.74	76.40	0.39	1.0	98.3	1.30	adh
						2.06	3.12	19.47	75.36	0.38				art
							3.18	19.88	76.94	0.39				di
188125	4879	383	379	331	1.04	0.97	67.62	9.00	22.41	0.16	-	-	2.03	adi
						2.00	66.91	8.91	22.18	0.16				art
							68.28	9.09	22.63	0.16				di
188126	4880	4388	4332	3797	1.28	0.70	7.71	22.75	68.84	0.34	3.0	98.0	1.37	adl
						1.97	7.61	22.46	67.96	0.34				art
							7.76	22.91	69.33	0.34				di
188127	4881	320	317	269	0.94	0.32	5.21	22.17	72.30	0.39	7.0	97.4	1.30	adi
						1.25	5.16	21.96	71.62	0.39				arl
							5.23	22.24	72.53	0.39				di
188128	4882	2416	2383	2101	1.37	0.56	17.62	27.42	54.40	0.81	7.5	97.4	1.48	adl
_						1.92	17.38	27.05	53.66	0.80				arl
							17.72	27.57	54.71	0.81				d
188129	4883	294	293	259	0.34	0.59	68.18	23.52	7.71	0.24	-		2.36	adi
						0.93	67.95	23.44	7.68	0.24				ari
							68.58	23.66	7.76	0.24				d
188130	4884	1588	1495	1293	5.86	2.74	10.50	18.50	68.26	0.67	0.0	32.0	1.42	ad
						8.44	9.89	17.42	64.26	0.63				ar
							10.80	19.02	70.18	0.69				d
188131	4885	2726	2642	2280	3.08	0.41	3.29	19.76	76.54	0.44	2.0	97.4	1.30	ad
						3.48	3.19	19.15	74.18	0.43				ar
							3.30	19.84	76.86	0.44				d
188132	4886	4787	4642	4014	3.03	0.54	5.12	20.63	73.71	0.46	4.0	98.3	1.31	ad
.00102						3.55	4.96	20.01	71.48	0.45				ar
							5.15	20.74	74.11	0.46				d

<sup>\*</sup> SG checked

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CLIENT:

CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

PO#:

326969WC

HOLE:

WC18-24C & WC18-25C

LAB#:

188093-171

REPORT DATE:

February 20, 2019

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Gwil Industries Inc. 7784 - 62nd St SE Calgary, AB T2C 5K2

Tel: (403) 253-8273 Email: info@birtley.ca

www.birtley.ca

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

LAB#	Sample	Wet	Dry	Retain	ADM%	MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASIS
188133	ID: 4887	Wt(g) 1130	Wt (g) 1099	Wt (g) 7/8 948	2.74	0.81	6.56	21.87	70.76	0.47	8.0	82.0	1.30	adl
	1.00.	1100	1000	340	2.74	3.53	6.38	21.27	68.82	0.46	8.0	02.0	1.30	ar
							6.61	22.05	71.34	0.47				dl
188134	4888	473	464	407	1.90	0.25	69.30	15.07	15.38	0.14	-	-	2.14	ad
						2.15	67.98	14.78	15.09	0.14				arl
100105	1000						69.47	15.11	15.42	0.14				di
188135	4889	140	139	121	0.71	0.28	5.29	18.98	75.45	0.52	2.5	98.0	1.35	adl
						0.99	5.25 5.30	18.84 19.03	74.91	0.52 0.52				art
188136	4890	746	737	640	1.21	0.53	8.20	19.03	75.66 71.99	0.52	3.5	99.1	1.33	di adi
						1.73	8.10	19.05	71.12	0.51	0.0	55.1	1.00	arl
							8.24	19.38	72.37	0.52				dl
188137	4891	502	465	402	7.37	0.48	39.72	18.30	41.50	0.36	4.5	98.8	1.63	adt
						7.82	36.79	16.95	38.44	0.33				art
188138	4892	4507	4504	4000		2.22	39.91	18.39	41.70	0.36				dt
100130	4892	1587	1564	1380	1.45	0.83	16.54	18.58	64.05	0.55	1.0	98.6	1.43	adb
						2.27	16.30 16.68	18.31 18.74	63.12 64.59	0.54 0.55				art
188139	4893	964	926	803	3.94	0.68	7.55	21.43	70.34	0.99	2.5	95.4	1.32	dt adt
		•••	020		0.01	4.60	7.25	20.59	67.57	0.95	2.5	33.4	1.52	art
							7.60	21.58	70.82	1.00				db
188140	4894	1003	966	847	3.69	0.32	21.59	27.49	50.60	1.82	6.5	99.4	1.53	adb
						4.00	20.79	26.48	48.73	1.75				art
							21.66	27.58	50.76	1.83				db
188141	4895	2666	2579	2248	3.26	0.52	19.57	25.13	54.78	0.99	7.0	97.7	1.47	adb
						3.77	18.93	24.31	52.99	0.96				art
188142	4896	685	675	586	1.46	0.58	19.67 24.49	25.26 29.84	55.07 45.09	1.00 0.83	1.5	05.7	1.50	db
100142	4000	000	0,3	300	1.40	2.03	24.49	29.40	44.43	0.83	1.5	95.7	1.59	adb arb
						2.00	24.63	30.01	45.35	0.83				db
188143	4897	783	764	669	2.43	0.55	22.74	18.12	58.59	0.97	1.0	96.8	1.47	adb
						2.96	22.19	17.68	57.17	0.95				art
							22.87	18.22	58.91	0.98				db
188144	4898	153	150	138	1.96	0.88	25.68	18.54	54.90	0.88	0.5	98.3	1.69	adb
1						2.82	25.18	18.18	53.82	0.86				arb
188145	4899	859	846	732	1.51	0.42	25.91	18.70	55.39	0.89		00.0	4.70	db
100143	4033	009	040	132	1.51	1.93	45.96 45.26	15.20 14.97	38.42 37.84	0.76 0.75	5.0	98.8	1.72	adb
	1					1.95	46.15	15.26	38.58	0.76				art db
188146	4900	334	330	285	1.20	0.35	23.49	22.55	53.61	0.87	6.5	97.7	1.47	adb
						1.54	23.21	22.28	52.97	0.86				arb
							23.57	22.63	53.80	0.87				db
188147	4901	567	560	491	1.23	0.41	32.27	22.22	45.10	0.79	7.5	96.8	1.54	adb
						1.64	31.87	21.95	44.54	0.78				arb
100110							32.40	22.31	45.29	0.79				db
188148	4902	2576	2529	2201	1.82	0.51	6.20	24.10	69.19	0.87	7.0	97.1	1.34	adb
	Ì					2.33	6.09	23.66	67.93	0.85				arb
188149	4903	420	414	360	1.43	0.54	6.23	24.22	69.54	0.87	0.5	04.5	4.05	db
100149	4903	420	414	360	1.43	1.96	9.80 9.66	22.72 22.40	66.94 65.98	0.58 0.57	6.5	94.5	1.35	adb
1						1.90	9.85	22.84	67.30	0.57				arb db
188150	4904	2228	2193	1911	1.57	0.47	10.32	20.39	68.82	0.40	2.0	95.7	1.37	adb
		-				2.03	10.16	20.07	67.74	0.39	2.0	55.1	1.01	arb
							10.37	20.49	69.14	0.40				db
188151	4905	1780	1758	1533	1.24	0.64	9.66	22.12	67.58	0.57	3.0	98.0	1.37	adb
1						1.87	9.54	21.85	66.74	0.56				arb
							9.72	22.26	68.02	0.57				db
88152	4906	5130	5021	4382	2.12	0.63	3.49	24.84	71.04	0.44	8.0	96.8	1.29	adb
-						2.74	3.42	24.31	69.53	0.43				arb
							3.51	25.00	71.49	0.44				db

<sup>\*</sup> SG checked

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<sup>+</sup> Ash checked

<sup>-</sup> Volatile checked



CLIENT:

CONUMA COAL RESOURCES

PROJECT: PO#:

Willow Creek development drilling

326969WC

HOLE:

WC18-25C

LAB#:

188093-171

REPORT DATE: February 20, 2019

Gwil Industries Inc. 7784 - 62nd St SE Calgary, AB T2C 5K2 Tel: (403) 253-8273 Email: info@birtley.ca www.birtley.ca

Page 4 of 4

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

LAB#	Sample	Wet	Dry	Retain	ADM%	MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASIS
	ID:	Wt(g)	Wt (g)	Wt (g) 7/8										
188153	4907	2794	2662	2318	4.72	0.38	23.96	20.24	55.42	0.52	6.5	95.7	1.46	adl
						5.09	22.83	19.28	52.80	0.50				art
							24.05	20.32	55.63	0.52				dt
188154	4908	1058	1046	923	1.13	0.36	5.93	20.49	73.22	0.58	3.5	98.0	1.32	adh
						1.49	5.86	20.26	72.39	0.57				art
							5.95	20.56	73.48	0.58				dt
188155	4909	755	746	653	1.19	0.15	7.15	25.68	67.02	0.65	7.0	95.7	1.31	adh
						1.34	7.06	25.37	66.22	0.64				art
							7.16	25.72	67.12	0.65				dł
188156	4910	1586	1567	1361	1.20	0.63	20.64	16.84	61.89	0.82	1.5	96.2	1.46	adl
						1.82	20.39	16.64	61.15	0.81				arl
							20.77	16.95	62.28	0.83				dl
188157	4911	1154	1145	1003	0.78	0.68	65.88	13.47	19.97	0.19	1.5	98.6	2.06	adl
						1.45	65.37	13.36	19.81	0.19				art
							66.33	13.56	20.11	0.19				di
188158	4912	804	800	711	0.50	0.64	29.90	16.29	53.17	0.48	0.5	99.1	1.57	adt
						1.13	29.75	16.21	52.91	0.48				art
							30.09	16.39	53.51	0.48				di
188159	4913	878	868	764	1.14	0.67	5.00	18.29	76.04	0.65	2.0	97.1	1.33	adl
						1.80	4.94	18.08	75.17	0.64				ar
							5.03	18.41	76.55	0.65				dl
188160	4914	3109	3065	2673	1.42	0.59	4.26	20.83	74.32	0.55	3.5	96.2	1.31	adl
						2.00	4.20	20.54	73.27	0.54				arl
							4.29	20.95	74.76	0.55				d
188161	4915	4693	4615	4044	1.66	0.42	2.27	20.95	76.36	0.57	6.0	96.8	1.28	adi
						2.08	2.23	20.60	75.09	0.56				art
							2.28	21.04	76.68	0.57				d
188162	4916	1026	923	820	10.04	0.40	43.37	17.02	39.21	0.29	1.5	96.8	1.66	ad
						10.40	39.02	15.31	35.27	0.26				ar
							43.54	17.09	39.37	0.29				di
188163	4917	576	515	447	10.59	0.40	8.87	19.31	71.42	0.44	2.5	98.3	1.33	ad
						10.95	7.93	17.27	63.86	0.39				ar
							8.91	19.39	71.71	0.44				d
188164	4918	1126	1112	971	1.24	0.48	27.91	19.36	52.25	0.36	6.5	98.6	1.50	ad
						1.72	27.56	19.12	51.60	0.36				ar
							28.04	19.45	52.50	0.36				ď
188165	4919	1155	1143	998	1.04	0.71	15.86	18.75	64.68	0.51	3.0	99.7	1.40	ad
100100	10.0	7,00				1.74	15.70	18.56	64.01	0.50				ar
				1			15.97	18.88	65.14	0.51				d
188166	4920	2150	2119	1799	1.44	0.75	18.11	18.22	62.92	0.53	3.0	99.4	1.40	ad
100100	4520	2100	2110	1.00		2.18	17.85	17.96	62.01	0.52				ar
							18.25	18.36	63.40	0.53				d
188167	4921	1087	1065	812	2.02	0.36	12.90	21.05	65.69	0.83	9.0	99.7	1.33	ad
100101	4521	1007	1000	0.2	2.02	2.38	12.64	20.62	64.36	0.81				ar
						2.00	12.95	21.13	65.93	0.83				d
188168	4922	398	386	320	3.02	0.23	25.91	28.13	45.73	0.69	5.0	97.7	1.55	ad
100100	4322	330	300	020	0.02	3.24	25.13	27.28	44.35	0.67				ar
						0.2	25.10	28.19	45.84	0.69				d
100160	4923	2208	2172	1988	1.63	0.44	26.33	21.35	51.88	0.81	6.0	98.3	1.48	ad
188169	4923	2200	2112	1300	1.03	2.06	25.90	21.00	51.03	0.80	3.0	50.0		ar
						2.00	26.45	21.44	52.11	0.81				0
400470	4004	1700	1704	1400	2.75	0.37	15.47	20.50	63.66	0.99	9.0	98.0	1.34	ac
188170	4924	1780	1731	1493	2.15				61.91	0.99	9.0	30.0	1.04	a
						3.11	15.04	19.94						(
	-		100	101	0.00	0.00	15.53	20.58	63.90	0.99	7 5	97.7	1 //1	ac
188171	4925	496	480	424	3.23	0.36	22.09	19.03	58.52	0.91	7.5	91.1	1.41	
		1				3.57	21.38	18.42	56.63	0.88				aı
	1	1		1			22.17	19.10	58.73	0.91				

<sup>\*</sup> SG checked

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<sup>+</sup> Ash checked



CLIENT: CONUMA COAL RESOURCES

WC18-26C & WC18-27C

PROJECT: Willow Creek development drilling

PO#: 326969WC

HOLE:

LAB#: 188172-188250

REPORT DATE: March 12, 2019

Gwil Industries Inc. 7784 - 62nd St SE Calgary, AB T2C 5K2 Tel: (403) 253-8273 Email: info@birtley.ca www.birtley.ca

Page 1 of 4

# Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

1.45 "						W ANALYSIS								
LAB#	Sample ID:	Wet Wt(g)	Dry Wt (g)	Retain Wt (g) 7/8	ADM%	MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASI
188172	4926	705	701	615	0.57	0.55 1.11	20.01 19.90	17.66 17.56	61.78 61.43	0.57 0.57	1.5	97.1	1.43	ac
							20.12	17.76	62.12	0.57				(
188173	4927	3273	3242	2813	0.95	0.94	6.97	19.73	72.36	0.56	4.0	98.6	1.34	a
						1.88	6.90	19.54	71.67	0.55				а
							7.04	19.92	73.05	0.57				
188174	4928	505	501	433	0.79	0.56	5.16	19.27	75.01	0.54	2.0	99.4	1.32	ac
						1.35	5.12	19.12	74.42	0.54				а
100177	1000						5.19	19.38	75.44	0.54				
188175	4929	625	617	538	1.28	0.49	10.34	18.73	70.44	0.47	3.5	98.8	1.36	ac
	1 1					1.76	10.21	18.49	69.54	0.46				а
188176	4930	2761	2737	2385	0.87	0.60	10.39	18.82	70.79	0.47		00.4	4.00	
100170	4930	2/01	2131	2365	0.87	0.69 1.55	14.18	18.37	66.76	0.46	1.5	99.1	1.39	ac
	1 1					1.55	14.06 14.28	18.21 18.50	66.18 67.22	0.46				aı
188177	4931	1181	1172	1021	0.76	0.43	17.91	18.92	62.74	0.46	3.0	98.8	1.44	ac
				702.	0.70	1.19	17.77	18.78	62.26	0.80	5.0	30.0	1.44	aı
							17.99	19.00	63.01	0.81				C
188178	4932	589	582	511	1.19	0.36	18.78	18.08	62.78	0.87	6.0	99.1	1.41	ad
						1.54	18.56	17.87	62.03	0.86				ar
							18.85	18.15	63.01	0.87				d
188179	4933	554	552	475	0.36	0.65	19.71	18.35	61.29	0.92	6.5	99.4	1.44	ad
						1.01	19.64	18.28	61.07	0.92				aı
							19.84	18.47	61.69	0.93				d
188180	4934	1100	1091	942	0.82	0.39	21.55	16.40	61.66	0.76	2.0	99.7	1.47	ad
			1	1		1.20	21.37	16.27	61.16	0.75				ar
100404	4005	470	475	107			21.63	16.46	61.90	0.76				d
188181	4935	479	475	407	0.84	0.39	25.32	22.16	52.13	0.87	7.0	98.3	1.49	ad
						1.22	25.11	21.97	51.69	0.86				ar
188182	4936	3360	3318	2886	1.25	0.46	25.42 9.45	22.25	52.33 66.64	0.87	8.0	07.4	4.05	d
100102	4550	3300	3310	2000	1.25	1.70	9.45	23.45	65.81	0.77 0.76	8.0	97.4	1.35	ad
						1.70	9.49	23.56	66.95	0.77				ari di
188183	4937	648	642	557	0.93	0.48	27.95	19.96	51.61	2.03	3.5	98.3	1.54	adi
						1.40	27.69	19.78	51.13	2.01	0.0	00.0	1.04	ari
							28.08	20.06	51.86	2.04				di
188184	4938	1677	1665	1156	0.72	0.50	14.40	20.96	64.14	0.50	3.0	98.6	1.40	adl
İ				1		1.21	14.30	20.81	63.68	0.50				arl
							14.47	21.07	64.46	0.50				dl
188185	4939	1832	1807	1583	1.36	0.46	12.19	23.81	63.54	0.37	2.0	99.1	1.44	adl
			-	1		1.82	12.02	23.49	62.67	0.36				arl
00400	40.40	7000					12.25	23.92	63.83	0.37				dl
88186	4940	5983	5923	5175	1.00	0.41	3.46	24.52	71.61	0.42	8.0	98.3	1.29	adl
ĺ						1.41	3.43	24.27	70.89	0.42				arl
88187	4941	670	-004	500	0.00	0.40	3.47	24.62	71.90	0.42				di
88187	4941	678	664	583	2.06	0.43	53.18	15.31	31.08	0.34	-	-	1.81	adl
						2.49	52.08	14.99	30.44	0.33				art
88188	4942	581	554	473	4.65	0.21	53.41	15.38	31.21	0.34	0.5	07.4	4.04	dl
50,00	4042	501	554	713	4.00	0.31 4.94	6.98 6.66	23.42 22.33	69.29	0.58	6.5	97.4	1.31	adt
						7.04	7.00	23.49	66.07 69.51	0.55 0.58				ari di
88189	4943	444	442	377	0.45	0.48	37.26	17.79	44.47	0.38	5.5	98.6	1.63	adl
						0.93	37.09	17.73	44.27	0.38	0.0	55.0	1.00	ari
							37.44	17.88	44.68	0.38				di
88190	4944	937	878	768	6.30	0.60	72.80	8.72	17.88	0.23	-		2.14	adl
						6.86	68.22	8.17	16.75	0.22				ari
							73.24	8.77	17.99	0.23				dt
88191	4945	1279	1249	1098	2.35	0.49	19.32	17.47	62.72	0.81	2.5	97.1	1.45	adl
						2.82	18.87	17.06	61.25	0.79				art
							19.42	17.56	63.03	0.81				dt
88192	4946	2144	2118	1862	1.21	0.57	7.44	18.03	73.96	0.61	1.0	99.4	1.36	adh
				l		1.78	7.35	17.81	73.06	0.60				art
							7.48	18.13	74.38	0.61				

<sup>\*\*</sup> Ash, VOL & SG checked

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<sup>+</sup> Possibly carbonates present (vigorously fizzed with 10% hot HCI)



CLIENT: CONUMA COAL RESOURCES

PROJECT: Willow Creek development drilling

PO#: 326969WC

HOLE: WC18-27C , WC18-01C, WC18-02C, WC18-05C, WC18-06C , WC18-07C, WC18-08C& WC18-09

LAB#: 188172-188250

REPORT DATE: March 12, 2019 Page 2 of 4

Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

Gwil Industries Inc.

7784 - 62nd St SE Calgary, AB T2C 5K2

Tel: (403) 253-8273 Email: info@birtley.ca

www.birtley.ca

	Ţ					W ANALYSIS			******					
LAB#	Sample ID:	Wet Wt(g)	Dry Wt (g)	Retain Wt (g) 7/8	ADM%	MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASIS
188193	4947	1533	1503	1304	1.96	0.33	5.60	19.63	74.44	0.57	2.0	99.7	1.33	adl
						2.28	5.49	19.25	72.98	0.56				art
400404	4040	0504	0500	2000	101		5.62	19.69	74.69	0.57				dl
188194	4948	2564	2538	2203	1.01	0.28	4.33	20.45	74.94	0.63	4.5	99.1	1.31	adl
						1.29	4.29	20.24	74.18	0.62				arl
188195	4949	771	760	658	4.40	0.40	4.34	20.51	75.15	0.63				dl
100190	4545	771	760	658	1.43	0.48	12.15	21.33	66.04	0.56	8.0	96.8	1.36	adl
	1 1					1.90	11.98	21.03 21.43	65.10	0.55				arl
188196	4950	1557	1540	1343	1.09	0.59	12.21 26.47	18.04	66.36	0.56	2.5	00.2	4.54	d
100130	4330	1551	1540	1343	1.09	1.68	26.47	17.84	54.90	0.44	2.5	98.3	1.51	ad
	1 1					1.00	26.63	18.15	54.30 55.23	0.44 0.44				ari di
188197	4951	587	586	518	0.17	0.61	54.91	14.67	29.81	0.25		-	1.92	adl
100.01	1001	00.	000	0.0	0.17	0.78	54.82	14.65	29.76	0.25	-	-	1.92	
	1 1					0.70	55.25	14.76	29.70	0.25				arl di
188198	4952	4126	4015	3550	2.69	0.84	58.65	12.41	28.10	0.53			1.89	ad
			1010	0000	2.00	3.51	57.07	12.08	27.34	0.52	-	•	1.09	ari
						0.01	59.15	12.52	28.34	0.53				di
188199	4953	1493	1472	1276	1.41	0.36	22.65	30.35	46.64	0.75	2.0	97.7	1.60	adi
	1000	1 100	1772	1270	1.41	1.76	22.33	29.92	45.98	0.74	2.0	51.1	1.00	
						1.70	22.73	30.46	46.81	0.75				ari
188200	4954	1219	1189	1032	2.46	0.66	20.95	21.72	56.67	0.75	8.0	97.4	1 46	di
.00200	4004	1210	1100	1002	2.40	3.10	20.43	21.12	55.28	0.82	0.0	97.4	1.46	adl
						3.10	21.09	21.19	57.05	0.85				ari
188201	4955	532	530	468	0.38	0.37	49.11	43.54	6.98	Action to the second		-	2.27	dl
100201	4000	002	550	400	0.50	0.74	48.93	43.38	6.95	0.24 0.24	-	-	2.37	adl
						0.74	49.29	43.70	7.01	0.24				ari di
188202	4956	730	723	634	0.96	0.49	20.89	20.90	57.72	0.60	7.5	93.4	1.42	
	1000	700	, 20	004	0.50	1.44	20.69	20.70	57.17	0.59	1.5	93.4	1.42	adh
						1.44	20.99	21.00	58.00	0.60				art
188203	4957	1432	1393	1222	2.72	0.81	19.74	18.36	61.09	0.49	1.0	92.8	1.44	dt
.00200	4001	1-102	1000	1222	2.12	3.51	19.20	17.86	59.43	0.48	1.0	92.0	1.44	aut
						3.51	19.20	18.51	61.59	0.49				db
188204	4958	896	876	764	2.23	0.41	26.10	30.61	42.88	0.49	1.5	97.7	1.67	adh
	1000	000	0,0	,04	2.20	2.63	25.52	29.93	41.92	0.39	1,5	91.1	1.07	
				-		2.00	26.21	30.74	43.06	0.40				art
188205	4959	422	418	374	0.95	0.58	61.79	13.16	24.47	0.40			1.00	dh
.00200	4000	744	710	3/4	0.33	1.52	61.20	13.10	24.24	0.35	-	-	1.96	adb
				1		1.02	62.15	13.24	24.61	0.35				arb
188206	4960	1048	1040	907	0.76	0.62	79.24	11.86	8.28	0.08			2.36	db adb
		1010	.0.0	007	0.10	1.38	78.64	11.77	8.22	0.08	-	-	2.30	arb
1			-	J		1.50	79.73	11.93	8.33	0.08				db
188207	4961	647	646	556	0.15	0.51	66.72	14.43	18.34	0.17			2.16	adb
.00207	1001	011	040	000	0.10	0.66	66.62	14.41	18.31	0.17	-	-	2.10	
						0.00	67.06	14.50	18.43	0.17				arb
188208	4962	519	516	462	0.58	0.51	15.49	19.57	64.43	0.17	3.0	98.8	1.42	db
.00200	1002	0.0	0.0	402	0.50	1.09	15.40	19.46	64.06	0.79	3.0	90.0	1.42	adb
1						1.09	15.57	19.40						arb
188209	4963	352	347	300	1.42	0.67	37.81	13.77	64.76 47.75	0.79	0 E	00.7	1.60	db
100200	4500	002	341	300	1.72					0.66	0.5	99.7	1.69	adb
			1			2.08	37.27	13.57	47.07	0.65				arb
188210	4964	863	853	744	1.16	0.51	38.07	13.86	48.07	0.66		00.7	4.50	db
100210	7004	003	000	1-44	1.10		26.68	17.93	54.88	1.11	8.0	99.7	1.50	adb
1	1		}	1		1.66	26.37	17.72	54.24	1.10				arb
188211	4965	84	83	35	1.19	0.71	26.82	18.02	55.16	1.12	2.0	CC 1	4.00	db
100211	4000	04	03	33	1.19		9.78	21.58	67.93	0.79	2.0	66.4	1.39	adb
	1			1		1.89	9.66	21.32	67.12	0.78				arb
00212	4966	154	150	120	4.00	0.45	9.85	21.73	68.42	0.80				db
88212	4900	154	152	133	1.30	0.45	11.72	18.65	69.18	0.43	4.0	98.8	1.41	adb
				1		1.74	11.57	18.41	68.28	0.42				art
00242	4067	024	004	000	4.07	0.50	11.77	18.73	69.49	0.43				db
88213	4967	934	924	803	1.07	0.50	32.37	19.98	47.15	0.37	8.0	99.4	1.56	adb
				1		1.57	32.02	19.77	46.65	0.37				arb
0/6-5-5			0.00 -1-				32.53	20.08	47.39	0.37				db

<sup>\* %</sup>S checked \*\* Ash, VOL & SG checked

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CLIENT:

CONUMA COAL RESOURCES

PROJECT:

Willow Creek development drilling

PO#:

326969WC

HOLE:

WC18-10C,WC18-11C,WC18-12C,WC18-13C, WC18-19C,WC18-21C,WC18-17C,WC18-14C & WC18-05C

LAB#:

188172-188250

REPORT DATE: March 12, 2019

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Gwil Industries Inc.

7784 - 62nd St SE Calgary, AB T2C 5K2

Tel: (403) 253-8273 Email: info@birtley.ca

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## Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

LAB#	Sample	Wet	Dry	Retain	ADM%	W ANALYSIS MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BAS
	ID:	Wt(g)	Wt (g)	Wt (g) 7/8										
188214	4968	423	398	347	5.91	0.60	54.18	14.56	30.66	0.28	-	-	1.84	a
	1 1					6.47	50.98	13.70	28.85	0.26				а
400045	1000						54.51	14.65	30.85	0.28				
188215	4969	58	57	34	1.72	0.37	16.36	15.45	67.82	0.75	0.5	99.1	1.43	a
						2.09	16.08	15.18	66.65	0.74				а
188216	4970	444	439				16.42	15.51	68.07	0.75				
100216	4970	444	439	384	1.13	0.49	51.96	10.78	36.77	0.40	-	-	1.81	a
						1.61	51.37	10.66	36.36	0.40				a
188217	4971	1080	1054	005	0.44	0.50	52.22	10.83	36.95	0.40				-
100217	4971	1000	1054	935	2.41	0.52	68.58	13.08	17.82	0.12	-	-	2.07	a
						2.91	66.93	12.77	17.39	0.12				а
188218	4972	294	200	050	0.00	205	68.94	13.15	17.91	0.12				(
100210	4972	294	292	259	0.68	0.35	25.91	19.43	54.31	0.69	6.5	98.0	1.47	a
						1.03	25.73	19.30	53.94	0.69				а
100010	4070	F00		45:			26.00	19.50	54.50	0.69				
188219	4973	569	567	491	0.35	0.61	58.67	12.55	28.17	0.38	-	-	1.86	a
						0.96	58.46	12.51	28.07	0.38				а
100000	4071						59.03	12.63	28.34	0.38	Maria Para			
188220	4974	542	517	445	4.61	0.77	64.67	11.77	22.79	0.42	-	-	1.97	a
						5.35	61.69	11.23	21.74	0.40				а
		- Watton Low Committee Co.					65.17	11.86	22.97	0.42				
188221	4975	690	686	597	0.58	0.54	22.55	17.45	59.46	0.51	1.0	99.4	1.48	a
						1.12	22.42	17.35	59.12	0.51				а
			THE RESIDENCE OF THE PERSON OF				22.67	17.54	59.78	0.51				(
188222	4976	510	506	439	0.78	0.49	15.61	29.89	54.01	1.30	7.0	98.3	1.46	a
						1.27	15.49	29.66	53.59	1.29				а
							15.69	30.04	54.28	1.31				(
188223	4977	534	533	451	0.19	0.23	63.62	40.86	-4.71	9.98	-	-	2.91	a
						0.42	63.50	40.78	-4.70	9.96				a
							63.77	40.95	-4.72	10.00				c
188224	4978	140	140	112	0.00	0.39	40.89	20.57	38.15	2.37	-	-	1.80	ac
1						0.39	40.89	20.57	38.15	2.37				aı
							41.05	20.65	38.30	2.38				C
188225	4979	493	488	420	1.01	0.39	31.63	36.34	31.64	0.76	7.5	97.7	1.74	ac
						1.40	31.31	35.97	31.32	0.75				a
							31.75	36.48	31.76	0.76				d
188226	4980	1374	1369	1210	0.36	0.32	56.15	49.08	-5.55	0.18	-	-	2.76	ac
1			1			0.68	55.95	48.90	-5.53	0.18				aı
							56.33	49.24	-5.57	0.18				d
88227	4981	198	191	163	3.54	0.48	40.12	17.29	42.11	0.77	-	-	1.62	ad
						4.00	38.70	16.68	40.62	0.74				aı
			1			-	40.31	17.37	42.31	0.77				ď
88228	4982	236	232	197	1.69	0.39	15.22	22.78	61.61	0.53	5.0	98.3	1.41	ad
				-		2.08	14.96	22.39	60.57	0.52	0	55.0		ai
							15.28	22.87	61.85	0.53				d
88229	4983	892	884	762	0.90	0.51	43.25	18.78	37.46	0.38	-	<u>-</u>	1.70	ad
						1.40	42.86	18.61	37.12	0.38	-	-	1.70	ar
							43.47	18.88	37.65	0.38				ai d
88230	4984	917	907	790	1.09	0.58	31.38	16.42	51.62	0.79	8.0	98.6	1.52	ad
						1.66	31.04	16.24	51.02	0.79	0.0	30.0	1.52	au
- 1						1.00	31.56							
88231	4985	270	267	234	1.11	0.38	ALC: N. C. C. C. C. C. C. C. C. C. C. C. C. C.	16.52	51.92	0.79			4.00	d
30231	-300	210	201	254	1.11		52.38	14.65	32.59	0.27	-	-	1.83	ad
			1			1.49	51.80	14.49	32.23	0.27				ar
88232	4986	178	170	105	4.40	0.54	52.58	14.71	32.71	0.27				d
00232	4300	1/6	170	125	4.49	0.54	47.23	17.18	35.05	0.65	-	-	1.73	ad
Ì	1		1	Ì		5.01	45.11	16.41	33.47	0.62				ar
							47.49	17.27	35.24	0.65				d

<sup>\* %</sup>S checked \*\* Ash, VOL & SG checked

<sup>+</sup> Possibly carbonates present (vigorously fizzed with 10% hot HCI)

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CLIENT: CONUMA COAL RESOURCES

PROJECT: Willow Creek development drilling

PO#: 326969WC

HOLE: WC18-02C, WC18-03C, WC18-22C& WC18-27C

LAB#: 188172-188250

REPORT DATE: March 12, 2019 Page 4 of 4

# Samples were air dried & crushed to pass 9.5mm homogenized & representative split taken out for HR (1/8th) and prepped for lab analysis

Gwil Industries Inc. 7784 - 62nd St SE Calgary, AB T2C 5K2

Tel: (403) 253-8273 Email: info@birtley.ca

www.birtley.ca

LAB#	Sample	Wet	Dry	Retain	ADM%	W ANALYSIS MOIST%	ASH%	VOL%	F.C.%	S%	FSI	%LT	SG	BASIS
	ID:	Wt(g)	Wt (g)	Wt (g) 7/8										
188233	4987	596	588	519	1.34	0.47	17.08	26.30	56.15	0.92	4.5	96.8	1.45	adl
						1.81	16.85	25.95	55.40	0.91				art
							17.16	26.42	56.42	0.92				di
188234	4988	736	727	644	1.22	0.61	64.23	12.95	22.21	0.30	-	-	1.97	adl
						1.83	63.44	12.79	21.94	0.30				arl
							64.62	13.03	22.35	0.30				dl
188235	4989	524	515	462	1.72	0.47	33.51	17.72	48.30	0.46	1.5	98.6	1.59	adl
						2.18	32.93	17.42	47.47	0.45				ar
							33.67	17.80	48.53	0.46				dl
188236	4990	492	489	434	0.61	0.36	57.71	16.11	25.82	0.26	-	-	1.96	adl
						0.97	57.36	16.01	25.66	0.26				ari
							57.92	16.17	25.91	0.26				di
188237	4991	473	472	404	0.21	0.46	44.98	12.46	42.10	0.44	-	-	1.68	adl
						0.67	44.88	12.43	42.01	0.44				arl
							45,19	12.52	42.29	0.44				dl
188238	4992	1031	1004	864	2.62	0.51	56.50	14.93	28.06	0.66	_	-	1.93	adi
						3.12	55.02	14.54	27.33	0.64				arl
							56.79	15.01	28.20	0.66				di
188239	4993	740	693	613	6.35	0.46	60.43	11.73	27.38	0.35		-	1.91	ad
					0.00	6.78	56.59	10.98	25.64	0.33			1.01	arl
						0.70	60.71	11.78	27.51	0.35				di
188240	4994	699	698	596	0.14	0.38	10.63	19.35	69.64	0.71	3.5	98.3	1.36	adi
.002.10	4004	000	000	555	0.14	0.52	10.61	19.32	69.54	0.71	0.0	30.5	1.00	ari
						0.02	10.67	19.42	69.91	0.71				dl
188241	4995	293	290	211	1.02	0.34	39.44	27.63	32.59	2.55	2.5	96.2	1.80	adl
100241	4990	293	250	211	1.02	1.36	39.04	27.35	32.26	2.52	2.5	90.2	1.00	
1				1		1.30	39.57	27.72	32.70	2.52				arl
188242	4996	1085	1077	939	0.74	0.36	CORPUS TUROPETTO PROVIDENCE	PARTY BEAUTY DOUBLE THE PROPERTY OF		FEBRUARY STANDARD	2.0	99.1	1.40	di
100242	4990	1000	1077	939	0.74		17.70	17.47	64.47	0.97	2.0	99.1	1.43	adl
						1.09	17.57	17.34	63.99	0.96				art
188243	4997	4700	4704	1100	1.10	2.42	17.76	17.53	64.70	0.97				dł
188243	4997	1720	1701	1482	1.10	0.48	17.26	19.39	62.87	0.60	7.5	98.6	1.40	adl
1						1.58	17.07	19.18	62.18	0.59				arl
100011	4000	000	005			2.52	17.34	19.48	63.17	0.60				dk
188244	4998	306	305	224	0.33	0.52	37.85	15.29	46.34	0.52	1.0	98.8	1.67	adb
1				1		0.85	37.73	15.24	46.19	0.52				art
							38.05	15.37	46.58	0.52				dl
188245	4999	3097	3075	2718	0.71	0.48	12.24	23.29	63.99	0.97	8.0	98.8	1.39	adb
						1.19	12.15	23.12	63.54	0.96				art
					•••		12.30	23.40	64.30	0.97				db
188246	5000	916	915	815	0.11	0.29	38.20	40.63	20.88	0.52	1.5	98.8	1.97	adb
1			Ì			0.40	38.16	40.59	20.86	0.52				art
							38.31	40.75	20.94	0.52				db
188247	5251	368	367	275	0.27	0.39	12.41	23.02	64.18	1.15	8.5	98.3	1.37	adb
						0.66	12.38	22.96	64.01	1.15				ark
							12.46	23.11	64.43	1.15				dk
188248	5252	350	348	259	0.57	0.45	12.82	19.60	67.13	1.01	8.0	98.6	1.36	adb
						1.02	12.75	19.49	66.75	1.00				art
1				1			12.88	19.69	67.43	1.01				dì
188249	5253	119	118	49	0.84	0.67	80.15	6.70	12.48	0.15			2.24	adb
					0.01	1.50	79.48	6.64	12.38	0.15			7	art
						1.50	80.69	6.75	12.56	0.15				dk
188250	5254	34	33		2.94	0.50	53.06	13.83	32.61	0.15			1.80	
	0204	04	33	- 1	2.34		51.50			0.52	•	-	1.00	adb
100230	1		1	1		3.43		13.42	31.65					arb

<sup>\*%</sup>S checked

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<sup>\*\*</sup> Ash, VOL & SG checked