

Golder Associates

CONSULTING GEOTECHNICAL ENGINEERS

GOLDER ASSOCIATES LTD. IN ASSOCIATION WITH PD-NCB CONSULTANTS LTD. AND WRIGHT ENGINEERS LTD. REPORT NO. 6 HAT CREEK GEOTECHNICAL STUDY VOLUME 3 - APPENDICES 2-6

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March, 1977

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APPENDIX 2

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PETROGRAPHIC REPORTS

APPENDIX 2

PETROGRAPHIC REPORTS

in order to substantiate the findings of the geotechnical test results and visual descriptions, thin sections were cut of a number of representative rock types. The sections were cut and described by Vancouver Petrographics Ltd.

A number of petrographic descriptions were also provided by Dolmage-Campbell & Associates in a draft report. These are not reproduced in this appendix; they confirm the descriptions made on the GA geological logs.



Vancouver Petrographics Ltd.

JAMES VINNELL, Manager JOHN G. PAYNE, Ph. D. Geologist

216 EAST 28TH AVENUE VANCOUVER, B.C. V5V 3M1

PHONE (604) 874-1650

PETROGRAPHIC EXAMINATION FOR

GOLDER BRAWNER & ASSOCIATES LTD.

#803 - 206.2 and #803 - 353 examined over transmitted light.

September 1976

Pilsum P. Master M.Sc.

803 - 206.2 : TUFF

The rock is fragmental. The fragments can be distinguished from the matrix by: (1) the groundmass is hydrated to palagonite (yellow colour), (2) the larger size of the glass beads. In general, the fragments are etched and are subangular.

There is a great abundance of pore spaces, which have an irregular shape and distribution.

Upto 5% (visual estimate) of the rock is made up of subhedral medium sized grains of feldspar (K-spar and plagioclase). These crystal grains have an irregular distribution, and occur as individual grains rather than in clots or mosaics.

The glass is variable in form, size and amount of devitrification. The glass beads are generally round in shape(in X section), or oblong. Some of the beads have iron rich (limonite?) rims. Part of the groundmass is a microcrystalline aggregate in the shape of shards (montmorillonite).

Before devitrification and chemical alteration to montmorillonite, the rock was most probably a TUFF ---an admixture of glass fragments, rock fragments and whole crystals. The "rock" fragments were most probably older tuff of similar composition. Due to the relatively large size and subangular shape of the fragments the rock may be classified as an agglomerate.

<u>803 - 353</u> : TUFF

This is a relatively uniform rock. The groundmass is a microcrystalline aggregate of shards (montmorillonite). Scattered

in the groundmass are fairly uniform sized glass beads. The distribution of these beads is fairly uniform and show no flow texture or lineation.

There are also a few medium sized grains of feldspar scattered through the thin section. In comparison with 803-206.2, there appears to be little or no pore space and no palagonite.

Before devitrification and chemical alteration to montmorillonite the rock was an admixture of vitric and lithic tuff.

Admaolur.



Vancouver Petrographics Ltd.

JAMES VINNELL, Manager JOHN G. PAYNE, Ph. D. Geologist P.O. BOX 39 B887 NASH STREET FORT LANGLEY, B.C. VOX 1JO

PHONE (604) 533-1155

Report for: Graham Rawlings, Golder-Brawner

Samples: 809-433, 814-596, 898-227.4 (no section)

<u>Sample 809-433</u> Bentonite with Volcanic Fragments

The rock consists of fragments of mineral grains and fine grained porphyritic volcanic rocks (andesite, basalt(?)) in a groundmass of montmorillonite.

Mineral fragments include quartz, plagioclase, and muscovite; they occupy about 10-15% of the rock, with quartz most abundant and muscovite rare. Fragments range from very fine (0.02mm) up to 0.3 mm, with most obvious fragments being from 0.1 to 0.2 mm in size. The quartz fragments are very angular and plagioclase less angular. Other resistant mineral grains include zircon (one grain 0.025 mm long) and sphene (0.1%) as fractured grains.

Rock fragments include the following types, their compositions are probably andesite, but a few may be basalt. (10-15% of rock)

- 1) Patches of strongly altered(?) plagioclase grains to 0.05 mm and a few strongly zoned plagioclase phenocrysts of similar size occur in a groundmass of abundant plagioclase laths to 0.025 mm and a very fine grained matrix (0.001-0.005 mm) of unidentified minerals.
- 2) Uniform rock composed of plagioclase laths to 0.02 mm long.
- 3) Lathy plagioclase to 0.025 mm with abundant Ti-oxide and opaque up to 0.5 mm across.
- 4) Lathy plagioclase to 0.1 mm, some showing prominent flow foliation, with abundant interstitial opaque (5-30% in different fragments) and a brown platy mineral (possibly montmorillonite).
- 5) Sedimentary rock(?) with a few fragments of quartz and plagioclase to 0.1 mm in a very fine grained, strongly interlocking matrix (0.005 mm) of quartz, plagioclase, and clay(?).
- 6) Sedimentary rock or altered rock: very fine grained interlocking clay minerals up to 0.1 mm across.

As well the rock contains patches of montmorillonite consisting of fibrous aggregates of grains. Patches are up to 0.2 mm across, with grains up to 0.02 mm long. Identifying properties are low relief (R.I. less than quartz), colorless to brown, biaxial -'ve, 2V about 30°, length slow, subparallel to parallel extinction.

A few fragments consist of cryptocrystalline(?) grains with a deep olive green-brown color.

The groundmass (75% of the rock) consists of very fine fragments of minerals in montmorillonite.

The rock fragments range from rounded to semi angular, and are much more rounded than the quartz and plagioclase, perhaps reflecting a high content of montmorillonite in their matrices.

Sample 814-596 Reworked Volcanic Tuff - Bentonite

The rock is layered, the small layer at the corner of the section is described first.

This layer consists of subangular to subrounded fragments of quartz(10%), plagioclase(10%), cryptocrystalline quartz(?)(3%), and muscovite (1\%) from 0.01 to 0.1 mm across in a matrix (0.001-0.01 mm) of montmorillonite with limonite staining. The rock contains lenses (15%) from very fine up to 0.4 mm across of coal (opaque). These are parallel to layering.

The main layer contains 30% fragments of quartz and plagioclase up to 0.1 mm (locally 0.15 mm) across. Plagioclase is slightly altered to sericite and dusty opaque, and is more abundant than quartz. Quartz is angular in outline. A few grains of apatite are 0.025 mm long.

The rock contains patches (10%) up to 0.2 mm of fine grained aggregates of montmorillonite. Coarser fragments tend to contain fibrous aggregates and parallel growths ranging in color from white to light brown. In some extinction is irregular. Optical properties are similar to those of montmorillonite described in section 809-433. Some patches contain abundant inclusions of Ti-oxide (0.002-0.005 mm).

As well the rock contains several large fragments up to 10 mm long consisting of brown montmorillonite-chlorite(?) with 5% opaque as fine grained spots and lenses. These fragments are also flattened parallel to compositional layers.

One fragment is dark brown in color, very fine grained, and apparently isotropic; it is rimmed by fine grained brown montmorillonite or chlorite.

The groundmass consists of irregularly grained (0.001-0.005 mm) montmorillonite with minor limonite stain; grains are interlocking to granular. A similar texture occurs in some coarser grained patches of montmorillonite; these may represent altered fragments or just more coarsely recrystallized and altered groundmass.

One patch 5 mm across consists of opaque (coal).

The degree of rounding of fragments, especially in the layer at one end of the section, and the lack of fragments of volcanic rocks suggests that this sample is further from the source and has been more reworked than sample 809-433. The abundance of angular fragments, particularly of quartz, suggests that the degree of reworking is still not great.

It may be significant that the thin layer at one end of the section contains the most-rounded mineral grains and also contains the major coal seam; suggesting that it is more reworked than the other part of the section.

John Payse

John Payne, November, 1976.

2.

Thin section: Golder Brawner D.D. 44 - 2200'

Mineralogy and mode:

major (>5%)	major (>5%)		minor (<5%)		
plagioclase	26	biotite	4	zircon	
sanidine	12	glass	4	apatite	
white mica	14	quartz	4	amphibole	
carbonate	8	zeolites	4	opaques	

Fabric and texture:

Fragmental fabric consisting of sub-angular to sub-rounded lithic fragments and mineral grains in a fine-grained matrix. Tentatively, the matrix is composed of varying proportions of white mica, carbonate, clays, and zeolites. Positive identification of the constituents in the matrix is precluded by the extremely fine grain size.

Suspended in the matrix are lithic fragments of variable composition and shards of mineral grains. The mineral grains are sub-angular to subrounded fragments of former euhedral to subhedral plagioclase (An), sanidine, and quartz. Combined carlsbad-albite twinning of the plagioclase is common, whereas only carlsbad twinning predominates in the sanidine. The feldspar grains are often shattered in situ. Quartz grains are generally sub-rounded, but embayment of the grain boundaries is not evident. Faint undulatory extinction is occassionally visible. Deformed biotite flakes are locally part of the matrix, as well as rounded grains of zircon and opaque minerals.

Lithic fragments range from andesitic to dacitic in composition, with approximately a 5:1 andesite:dacite ratio. The fragments are in general holocrystalline, panidiomorphic-granular, porphyritic rocks with a pilotaxitic groundmass. Euhedral to subhedral phenocrysts of plagioclase, and less commonly biotite and/or quartz, are in a groundmass of crowded plagioclase microlites disposed in a sub-parallel manner. The fragments are most often sub-rounded in shape. Occurring less frequently are lithic fragments of hypocrystalline, panidiomorphic-granular, porphyritic texture. The groundmass consists of dark brown glass, occasionally microspherulitic, in which euhedral zoned plagioclase, biotite, and sanidine phenocrysts are set.

Alteration:

There is no evidence for hypogene hydrothermal alteration. Supergene (or diagenetic) processes account for the alteration assemblages which occur. The degree of alteration is variable within the fragments; some are fresh whereas others are pervasively replaced by white mica and carbonate. The phenocrysts in both the groundmass and the lithic fragments are fresh, although a few are incipiently altered to carbonate.

Classification and discussion:

The rock is a tuffaceous conglomerate in the sense that it resembles and in large part derived from pyroclastic debris or extrusive volcanic flows. Several attributes suggest that it is of sub-aqueous and perhaps fluvial origin. There is an absence of grading which would be expected in a sub-areal ash-fall. Moreover, there is no evidence of welding or flow banding in the matrix suggestive of the higher temperatures attendant pyroclastic origin. The lightic fragments are partially rounded; however, the phenocryst shards in the groundmass are more often sub-angular. This is suggestive of minimal transport from the source to the depositional site. The lithic fragments are most certainly derived from the underlying Cedar volcanics.

Mark J. Bloom

Thin Section:Golder Brawner D.D. 816 - 777.5'

Mineralogy and mode:

andesine-oligoclase groundmass	90
zeolites	8
opaques	2

Fabric and texture:

Pilotaxitic groundmass, i.e., crowded euhedral to subhedral plagioclase microlites disposed in a sub-parallel manner. Elongated areas shaded by increased opaque mineral content are possibly relic lithic fragments.

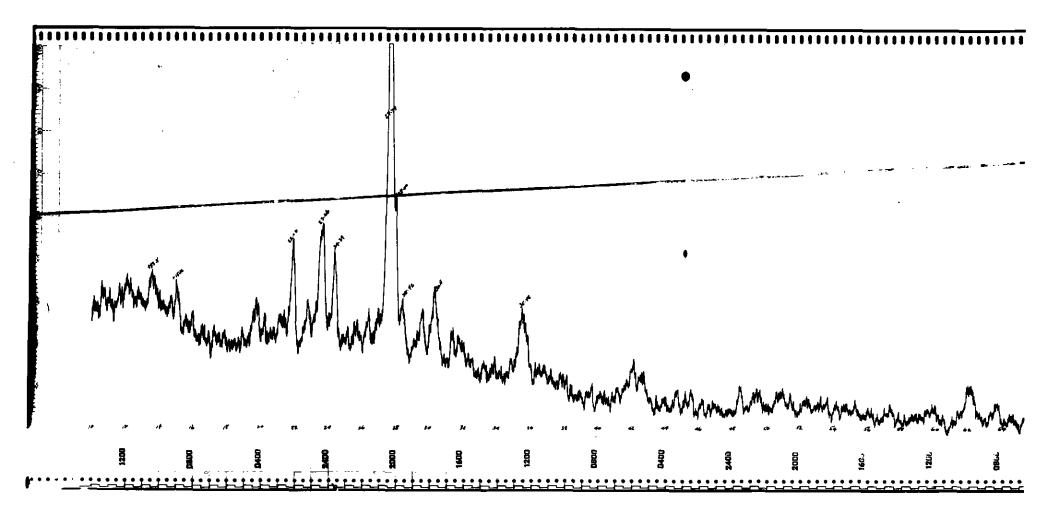
Elongated amygdaloidal cavaties prescribe to a regular concentric sequence of mineralization. From the groundmass into the amygdule, this sequence is a brown, colloidal material (possibly chlorite) which is in turn covered by a colloform, fibrous zeolite. The final phase of mineralization is crystallization of euhedral to subhedral zeolites in the core.

Classification and discussion:

On the basis of the information at hand, I suggest that this rock is an amygdaloidal andesite. The exceedingly fine grain size renders microscopic identification of groundmass const-tuents at best tentative; however, an X-ray powder pattern confirms the presence of andesine-oligoclase. There is no evidence for hypogene hydrothermal alteration, and the filled amygdules are unaltered as well. There is no evidence for strong shearing of the rock; plagioclase microlites are regularly oriented, euhedral, and optically continuous.

Mark & Bloom





X-RAY DIFFRACTION PATTERN OF ROCK SAMPLE FROM DDH 76-816 AT 777.5'.

APPENDIX 3

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X-RAY DIFFRACTION STUDIES

APPENDIX 3

X-RAY DIFFRACTION STUDIES

Analysis of the mineralogy of the rocks of the Coldwater Formation sequence by X-ray diffraction has been undertaken by the University of Western Ontario for GA and by the University of British Columbia directly for BCH. The University of Western Ontario reports are included in this appendix in their entirety. A summary of the UBC results is also included.

Four analyses of clay samples arising from the coal sampling for Birtley Engineering are also contained in this appendix.

The previous X-ray diffraction work carried out by the University of Western Ontario for Dolmage-Campbell & Associates is not included here, but may be found in the DCA Rock Mechanics Report dated 1975.

A3-1

JUL 200 AL



The University of Western Ontario, London, Canada

Faculty of Engineering Science

26 July 1976

Mr. G. Rawlings Golder, Brawner & Associates Ltd. 224 West 8th Avenue Vancouver, British Columbia V5Y 1N5

Dear Mr. Rawlings:

Hat Creek Project - Mineralogical Analyses

I am pleased to enclose two copies of our first set of x-ray and carbonate data for nine separate specimens received between June 24 and July 15, 1976. As I mentioned by phone, we are set up with a scheme that will enable us to mail you back the x-ray and carbonate data within one week of receipt of the samples.

Since we seem to be receiving samples from two or three people, and since the samples are not arriving in any particular order, I have presented the data in the sequence received as noted on the table.

Basically, the soils received so far all contain abundant montmorillonite plus quartz and feldspar as noted on the x-ray powder patterns. Two samples contain abundant carbonate (DH 803, 595' - 596' and DDH 803, 316' - 318'). For the present time, we have tentatively identified the carbonate as an impure siderite since peaks for calcite and dolomite are absent on the x-ray traces.

I hope that this format meets with your approval, and look forward to your comments. Selected glycol retentions and Na^+ analyses will be run when we have a more complete suite of samples or at your instruction.

Yours sincerely,

igley

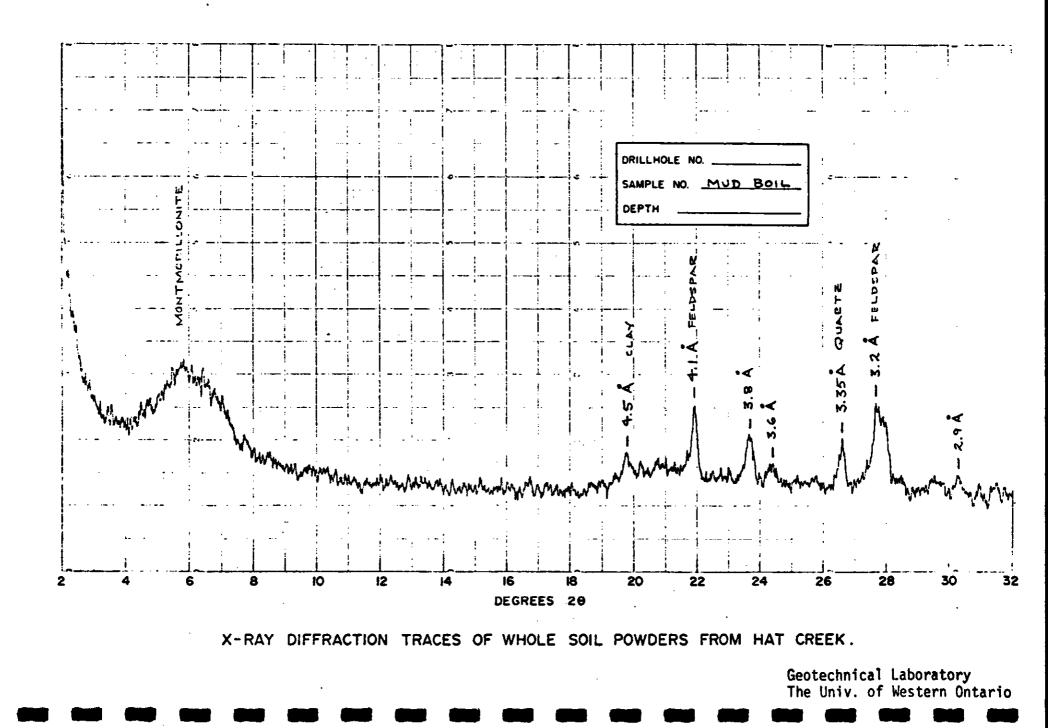
R.M. Quigley Professor and Head Geotechnical Section

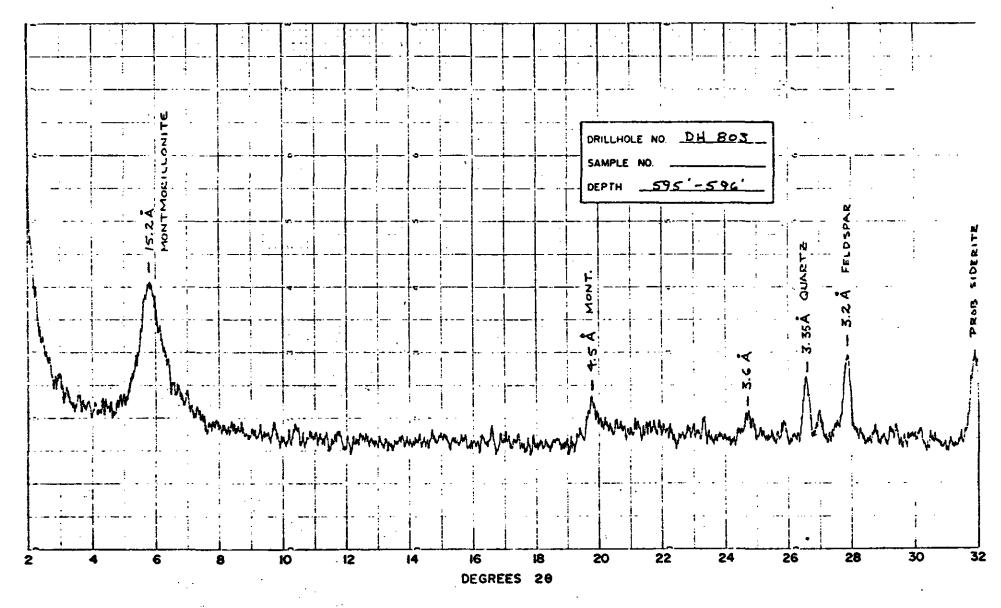
RMQ:em Enclosures HAT CREEK PROJECT

ACCOUNT 1319- 402

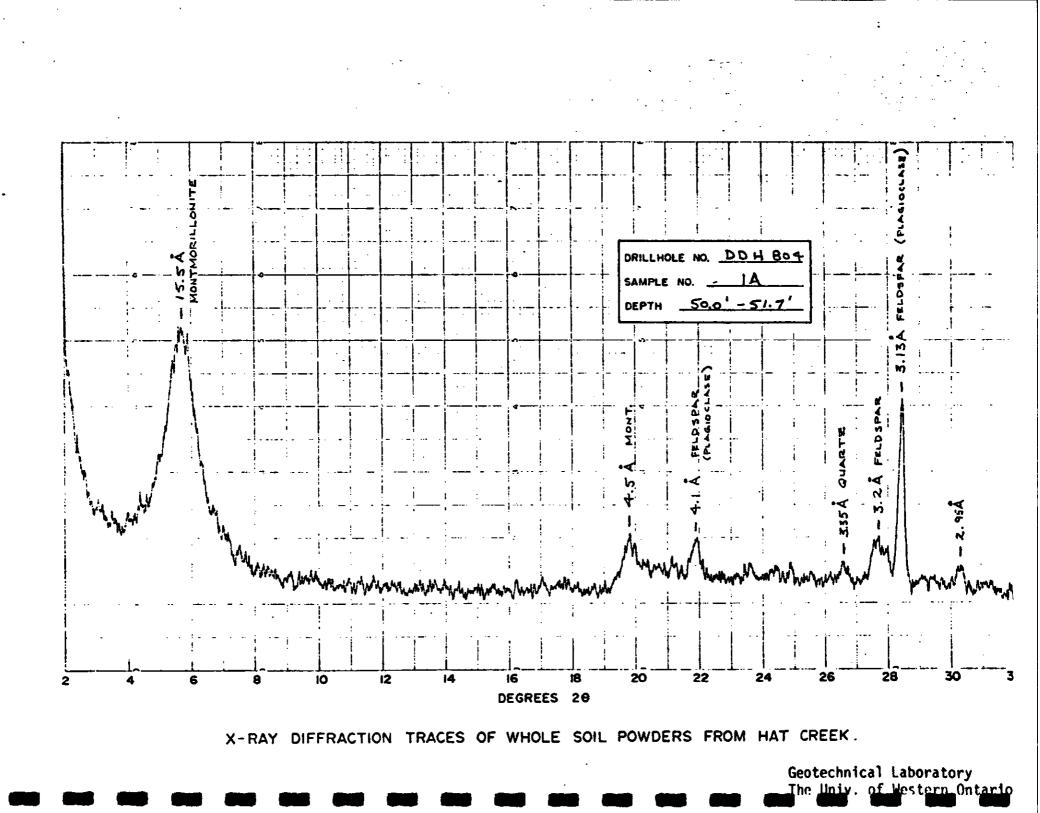
LIST OF SAMPLES RECEIVED FROM GOLDER BRAWNER + ASSOC.

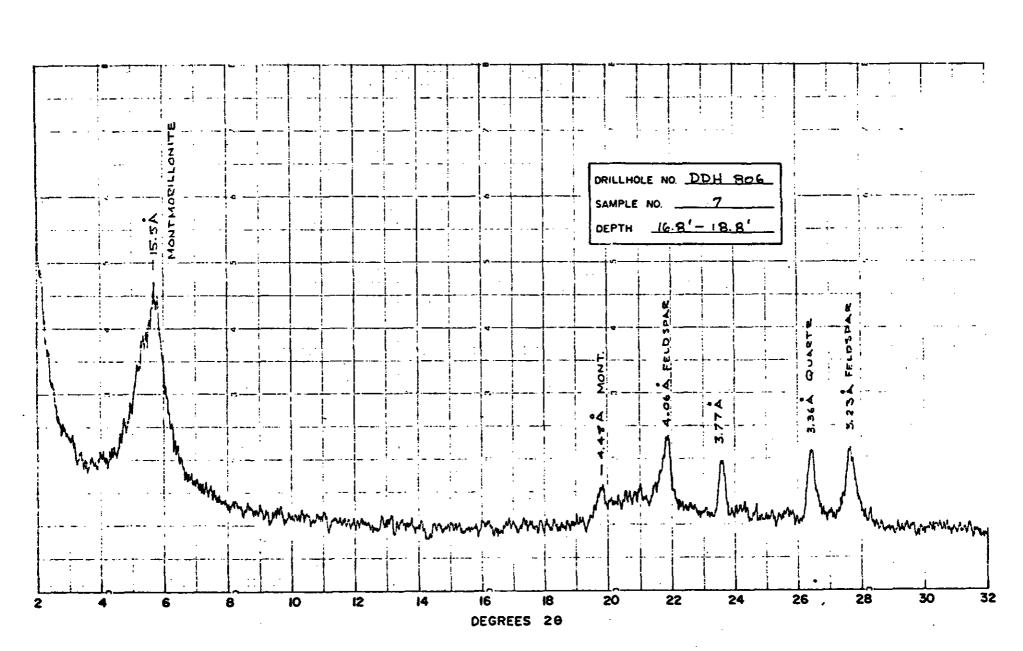
DRILL	SAMPLE	DEPTH	DATE	TESTING COMPLETED						
HOLE	NO.		REC'D				CARBONATE	GLYCOL	Na ⁺	
NO.				WET P.O.	ADPO	GPO.	POWDER		RETENTION	(PPM)
	MUD Boil		JUNE 24	~ ~		~	~	4.0		
DH 803	NO T GIVEN	595-596	JULY	~	.~	~	~	17.1		
DDH 804	1A	50.0'-51.7	JULY 13	~	-	~	~	1.7		
DDH 806	7	16.8-18.8'	JULY 13	~	~	~ ~	~	1.3		
DDH 803	28	1360 -1370 +35.0 -136.0	JULY	~	~	~	~	1.7		
DDH 803	29	316-0'-3127	JULY 15	V	~	~	~	32.4		
DDH 805	16 BLACK	61.5 - 62.5	JULY 15	~	~		~	5.3		
DDH BOT	12	22.0-24.0	JULY 15	~	~	~	~	2.4		
DDH 807	14	158.3'-159.5	JULY 15	~	~	~	~	1.7		
				2						
								GEOTECHNICAL LABORATORY UNIN. OF WESTERN ONTARIO R. W. Quigley July 23 /76		



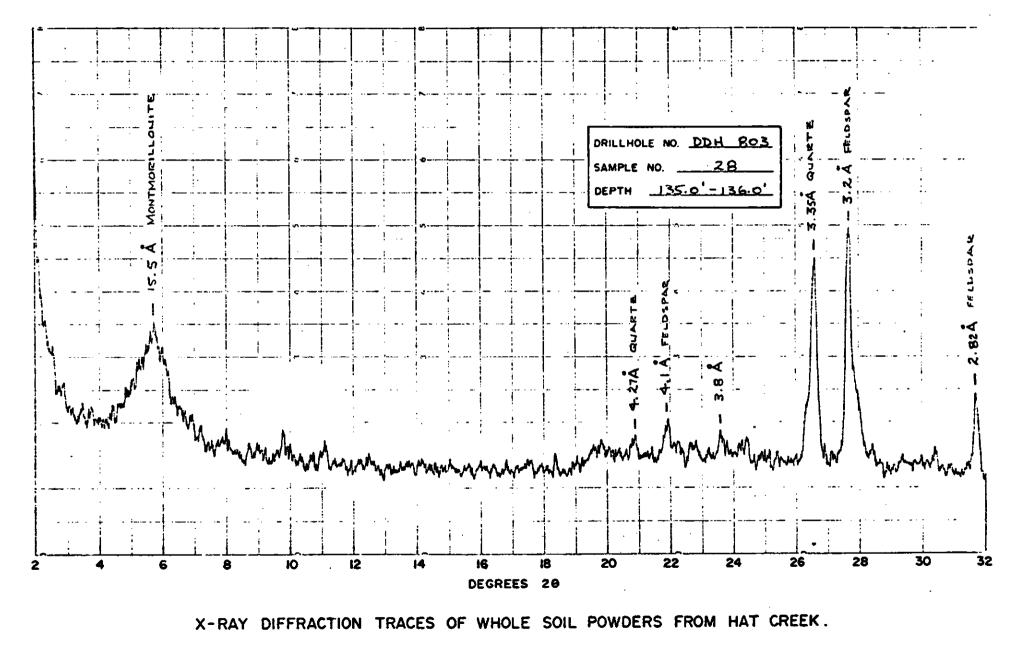


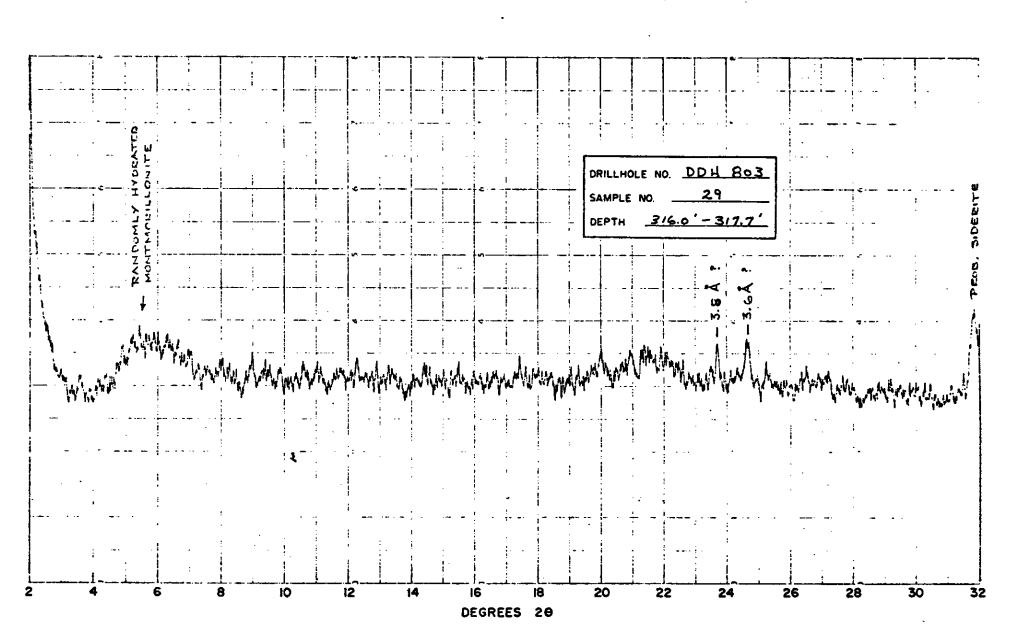
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



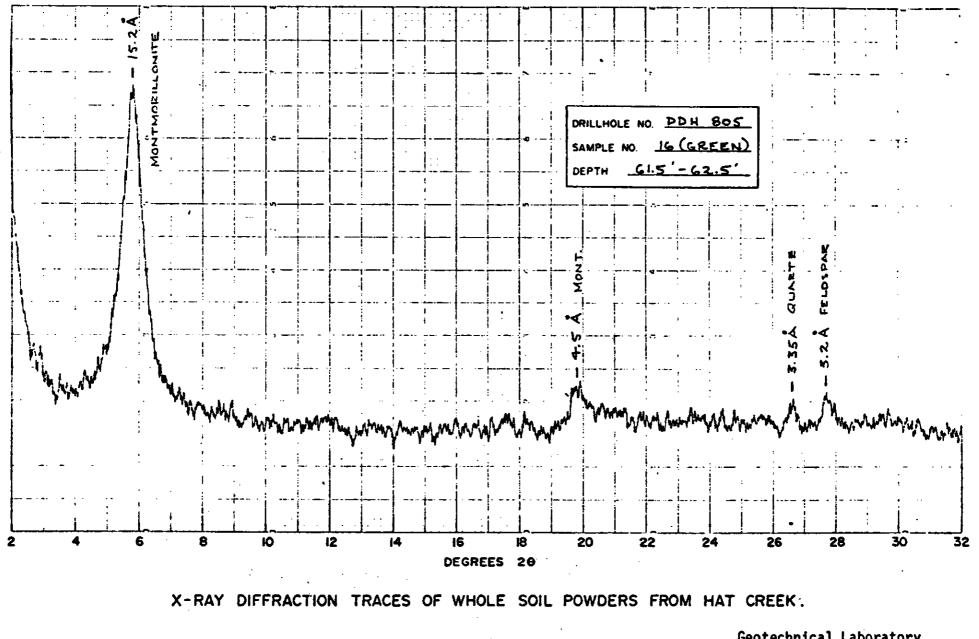


X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.





X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



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DRILLHOLE NO. DDH 805 SAMPLE NO. 16 (BLACK)

DEPTH

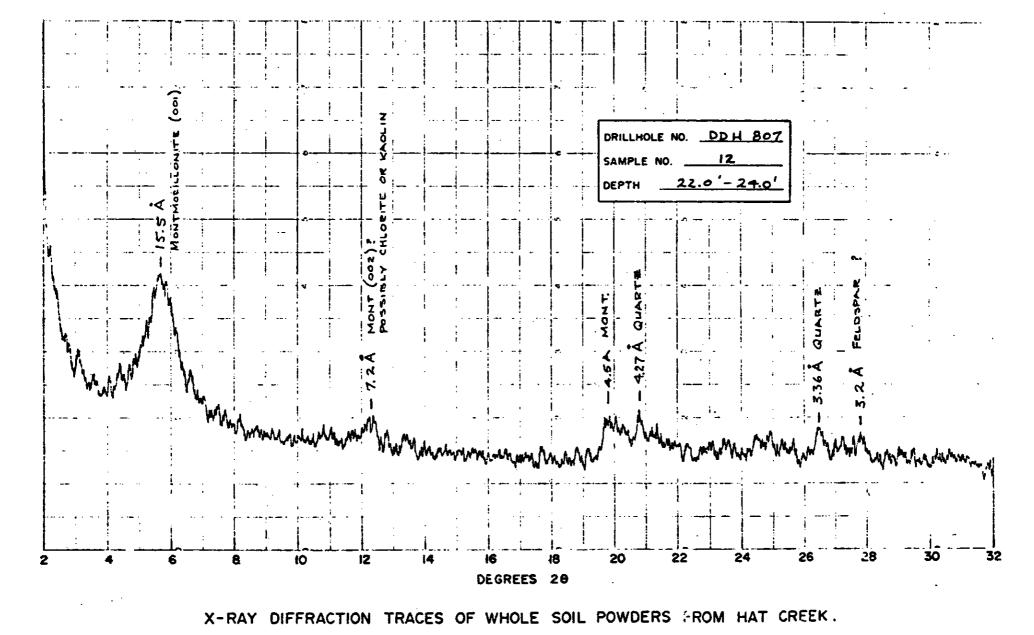
61.5' -62.

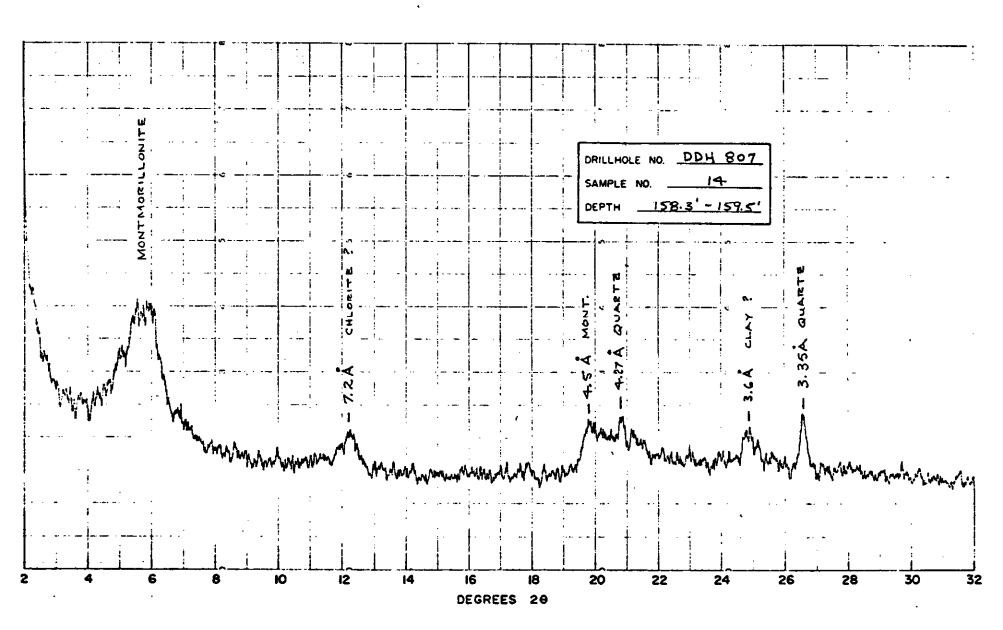
Fizo

2

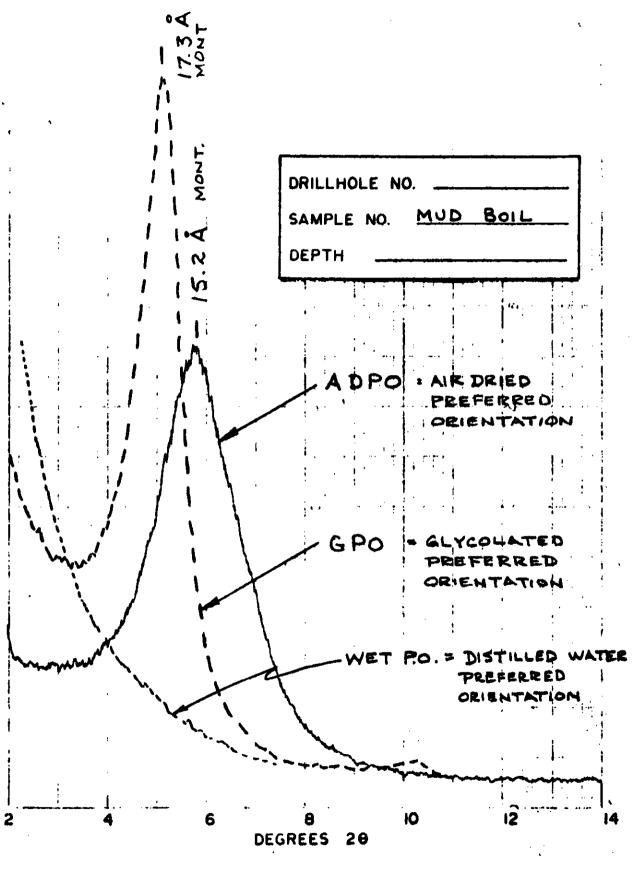
Geotechnical Laboratory The Univ. of Western Ontario

Gentechnical Laboratory

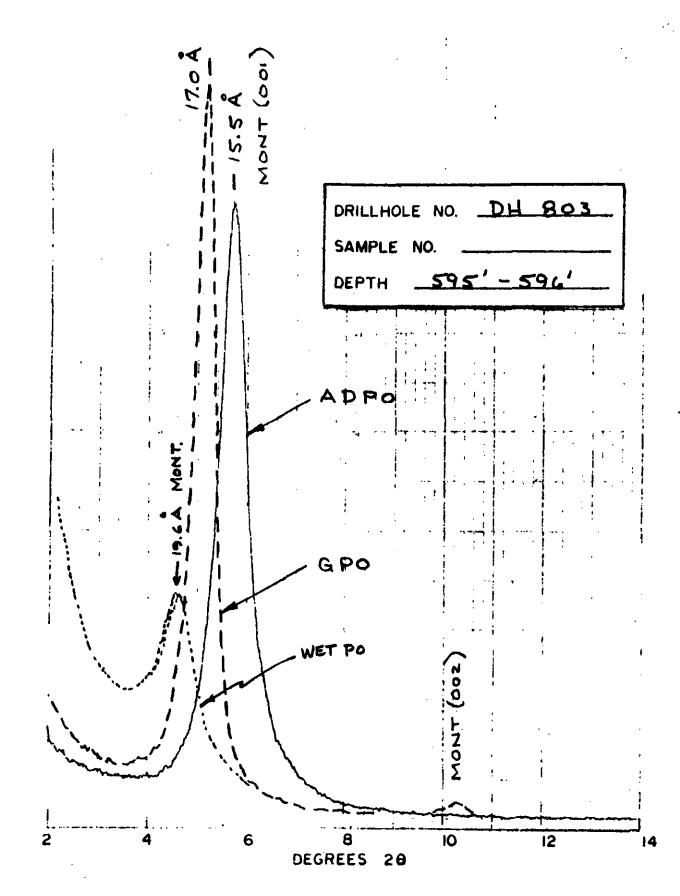




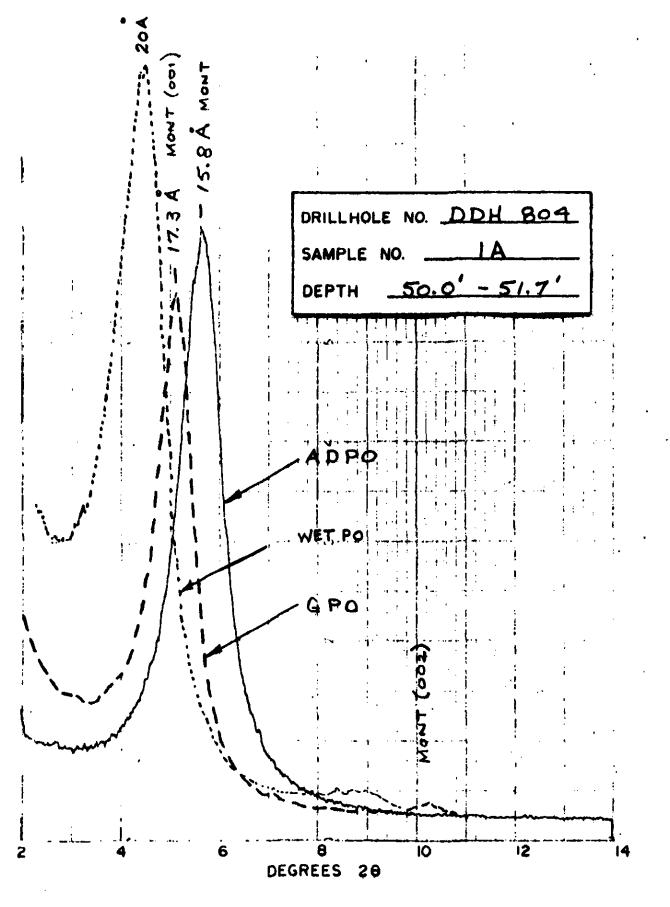
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



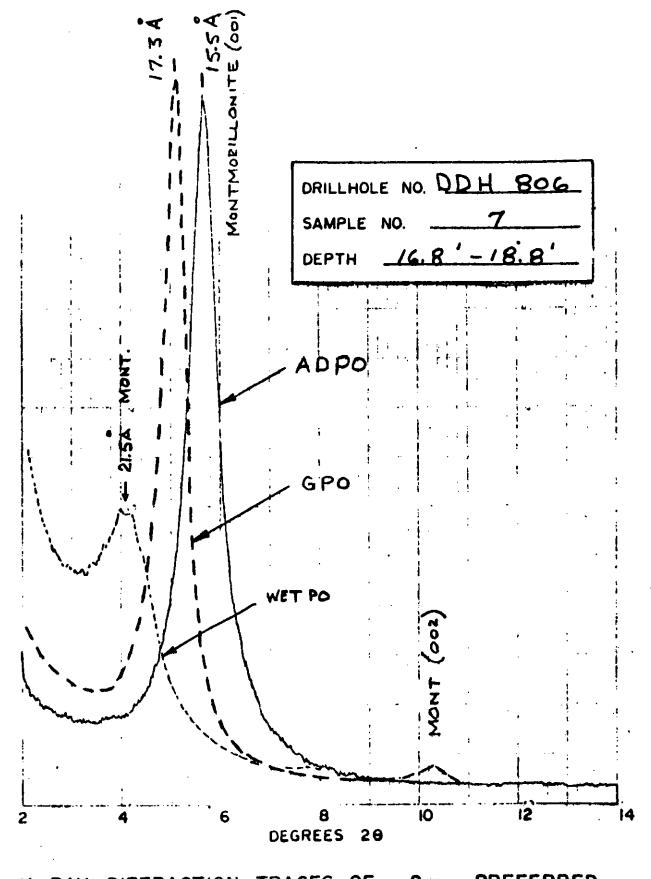
X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK



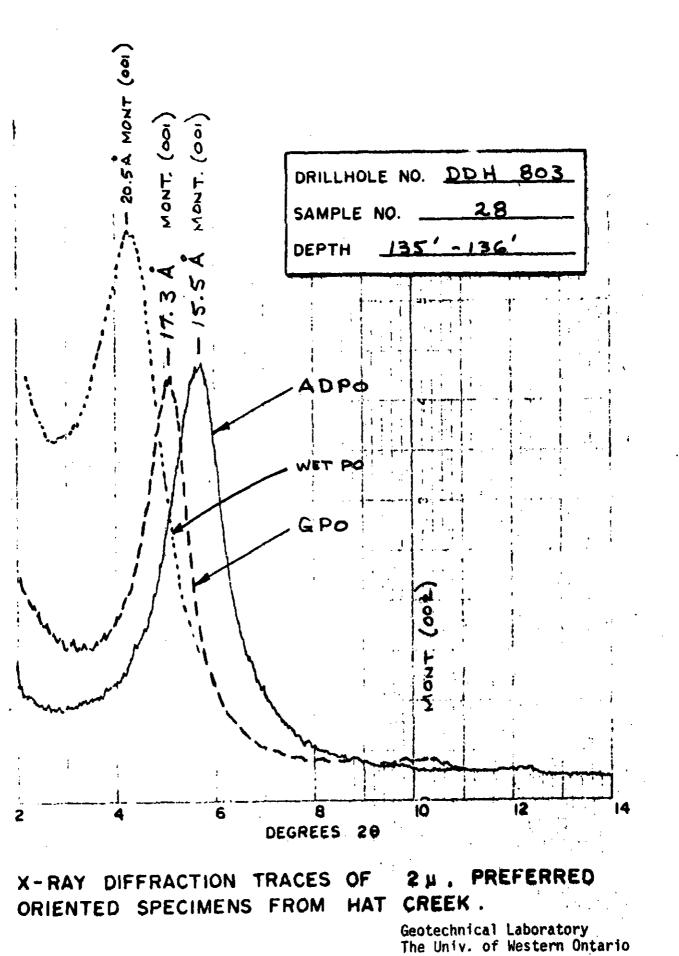
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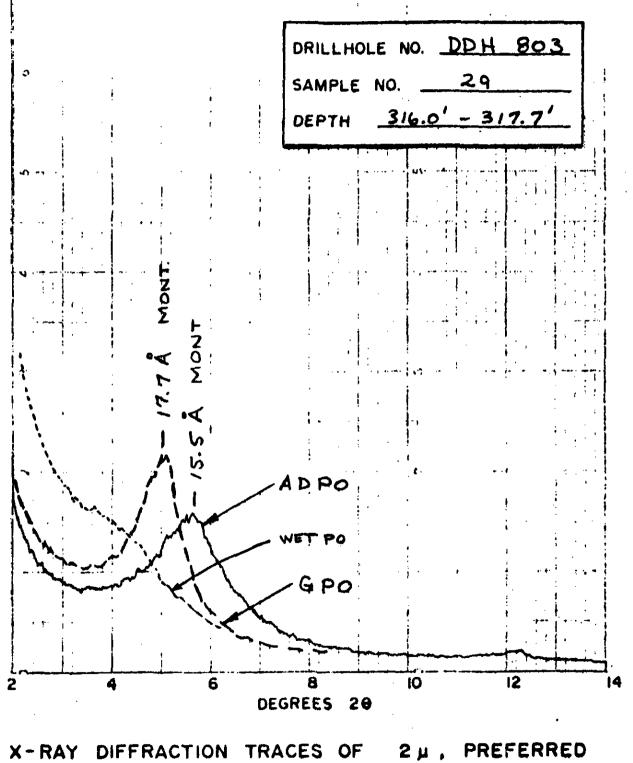


X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



X-RAY DIFFRACTION TRACES OF 2 ... PREFERRED ORIENTED SPECIMENS FROM HAT CREEK .

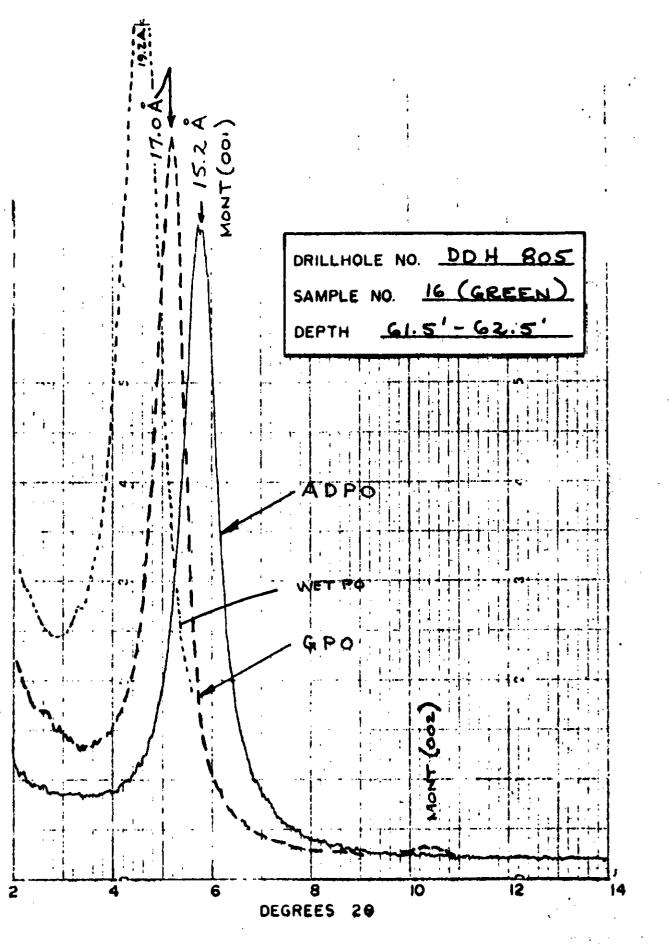




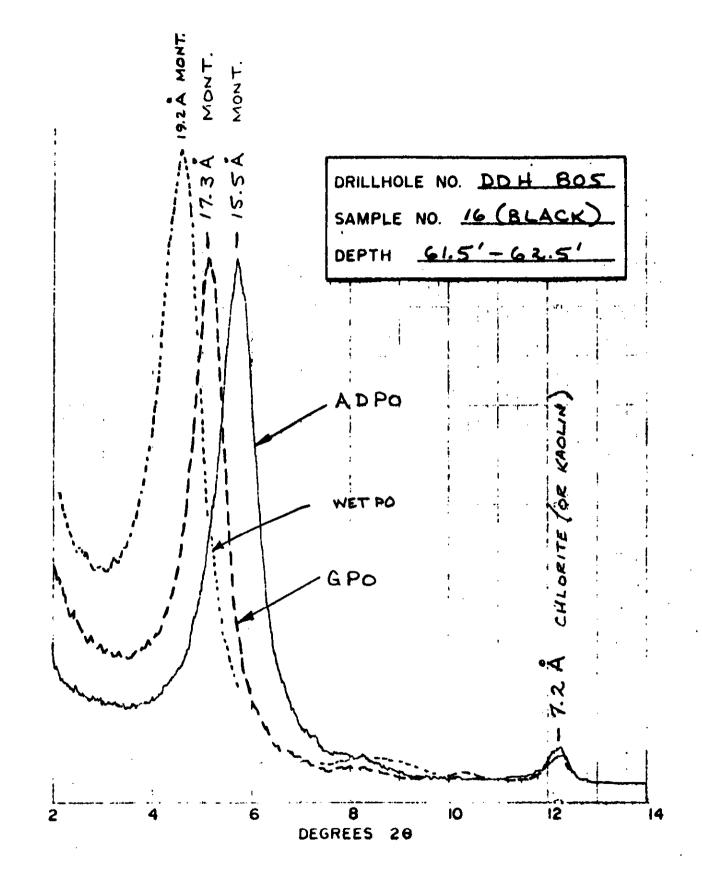
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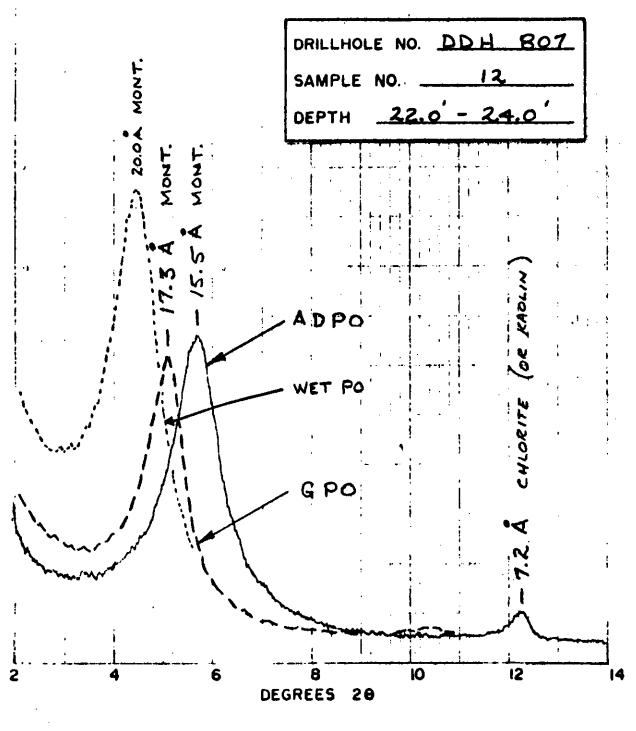
ORIENTED SPECIMENS FROM



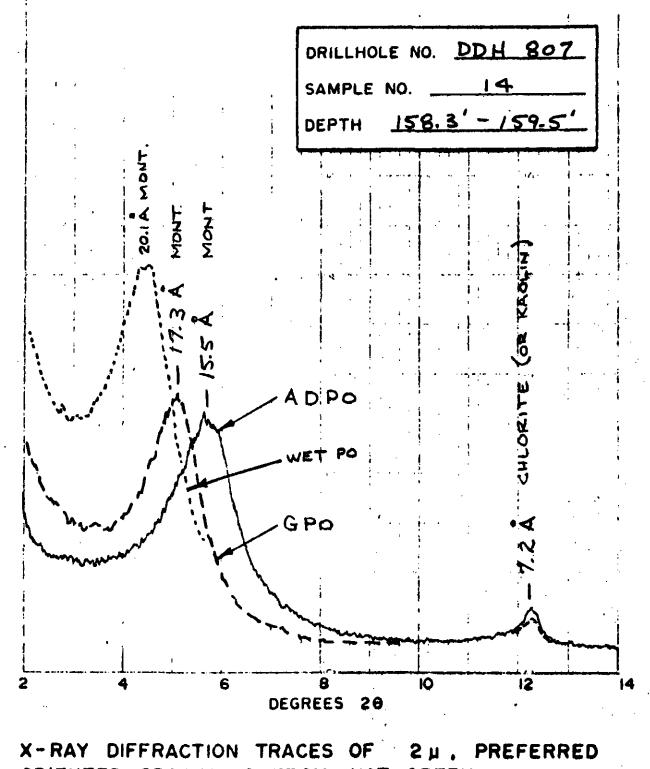
X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK



X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



ORIENTED SPECIMENS FROM HAT CREEK .

Geotechnical Laboratory The Univ. of Western Ontario



Faculty of Engineering Science London, Canade N6A 589

August 13, 1976

Mr. G. Rawlings Golder, Brawner & Associates Ltd. 224 West 8th Avenue Vancouver, B.C. V5Y 1N5

Dear Mr. Rawlings:

Report #2 Hat Creek Project - Mineralogical Analyses August 13, 1976

We have completed x-ray and carbonate analyses on 9 of the 25 samples received on August 3, 1976 from Mr. H. Hawson. The results, which are all for B.H. 74-28, are reported in our Report #2 attached.

The delay in processing has been caused by the indurated nature of many of the samples making disaggregation into finer fractions very difficult.

The current suite of samples from Borehole 74-28 shows a highly variable carbonate content, most of which appears to be an impure siderite (see Table). Where siderite is of lesser importance, the silicate minerals quartz and feldspar become the dominant non-clay mineral components.

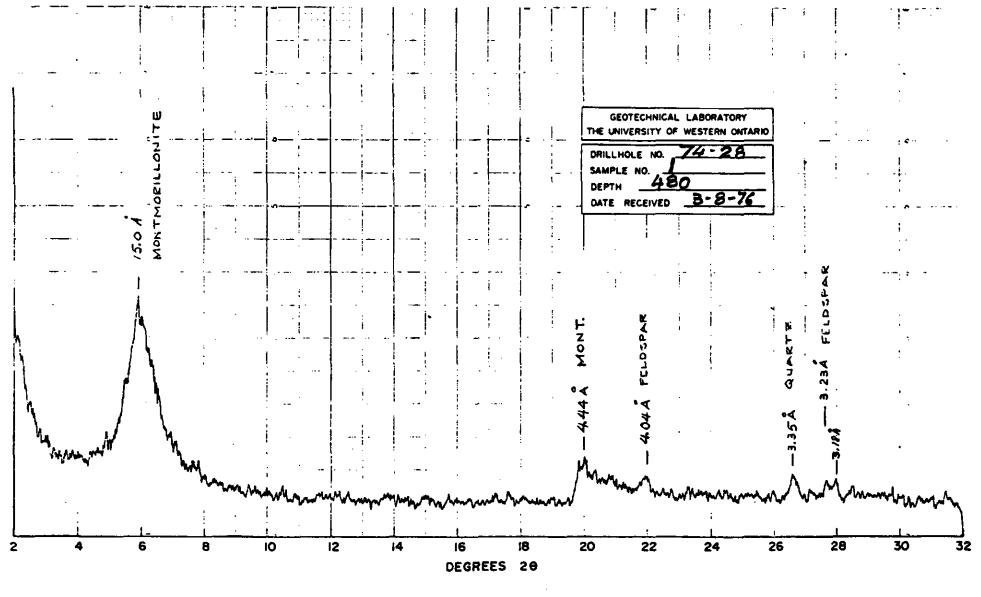
In the $<2\mu$ fraction, montmorillonite dominates, yielding the very strong (001) peaks shown in the traces for the preferred orientation samples.

Sincerely Yours

R.M. Quigley, P.Eng. Professor and Head Geotechnical Section

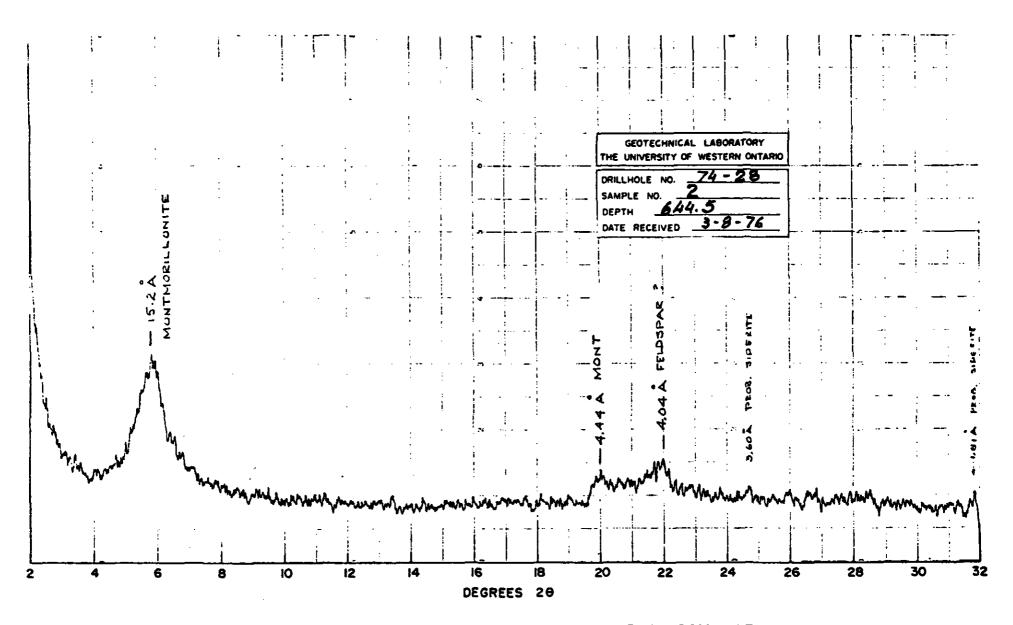
RMQ/jl Attach. cc. Mr. H. Hawson //

HAT CREEK PROJECT GEOTECHNICAL LABORATORY LIST OF SAMPLES RECEIVED FROM GOLDER BRAWNER & ASSOCIATES THE UNIVERSITY OF WESTERN ONTARIO Testing Completed Drill Sample Depth Date Hole X-ray Glycol (Feet) Carbonate Na⁺ No. Received No. Retention Wet P.O. ADP0 GPO Powder (%) (mg/g)(PPM) 480 3-2-76 74-2B 2.0 ~ 644.5 3-8-76 74-22 2 -~ ~ 6.4 3 738 3-2.16 74-22 1 ~ 7.5 4 74-22 763 ---31.6 767.5 3-5-76 1 74 : 17 5 ~ ~ 1 26.5 74-22 3-7-76 6 789.5 1 --44.3 7 451 74-22 7-2-16 1 1 12.9 8 537 71-22 3-8-16 --2.7 9 74-25 588 V 3-2-76 1.5 REPORT 2 Aug. 13, 1976 R. 21. Quin

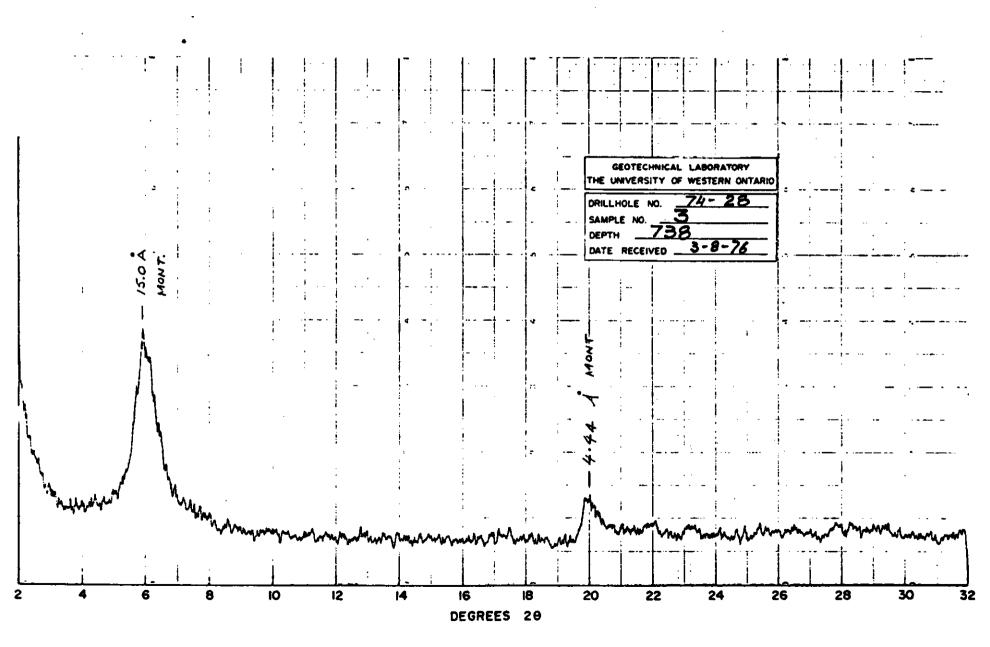


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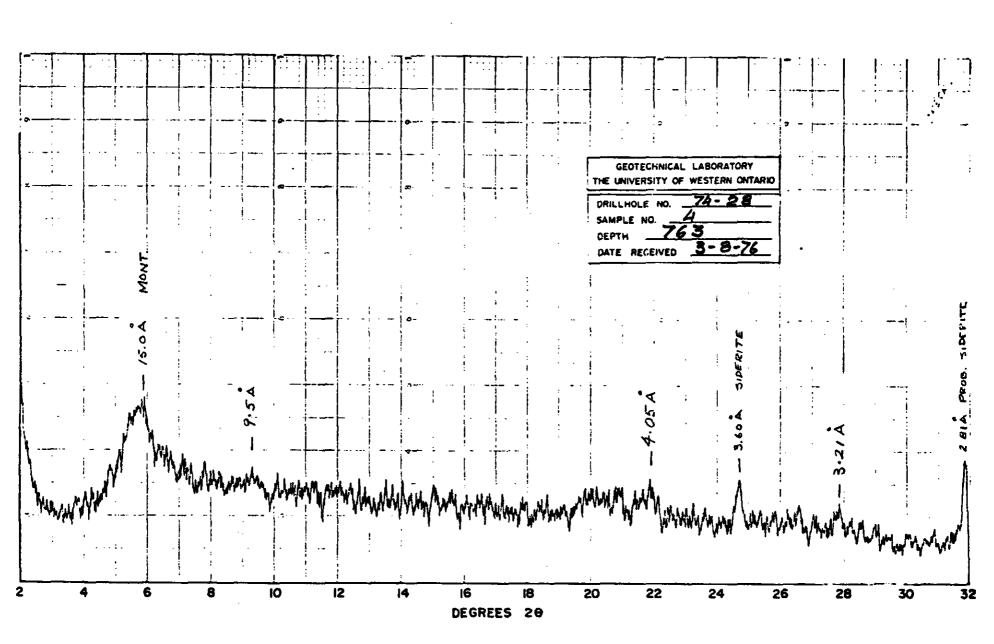
X-RAY CREEK . POWDERS FROM DIFFRACTION TRACES OF WHO SO HAT

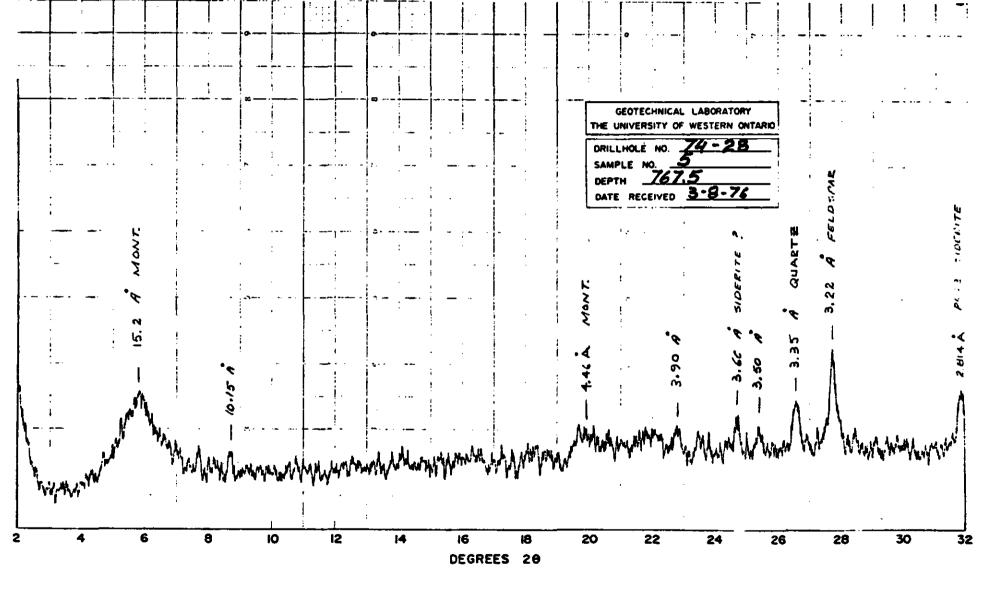


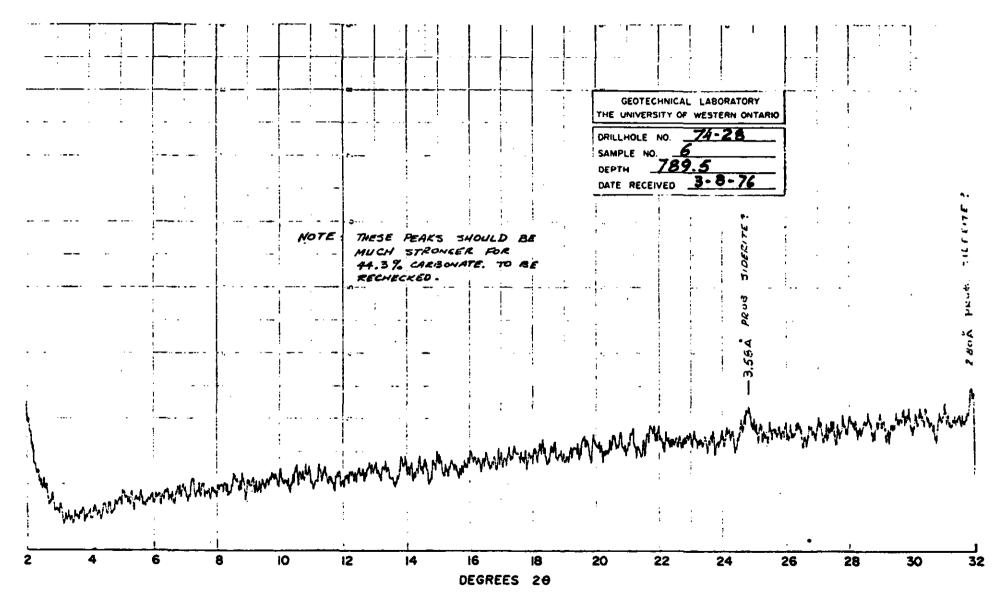
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.

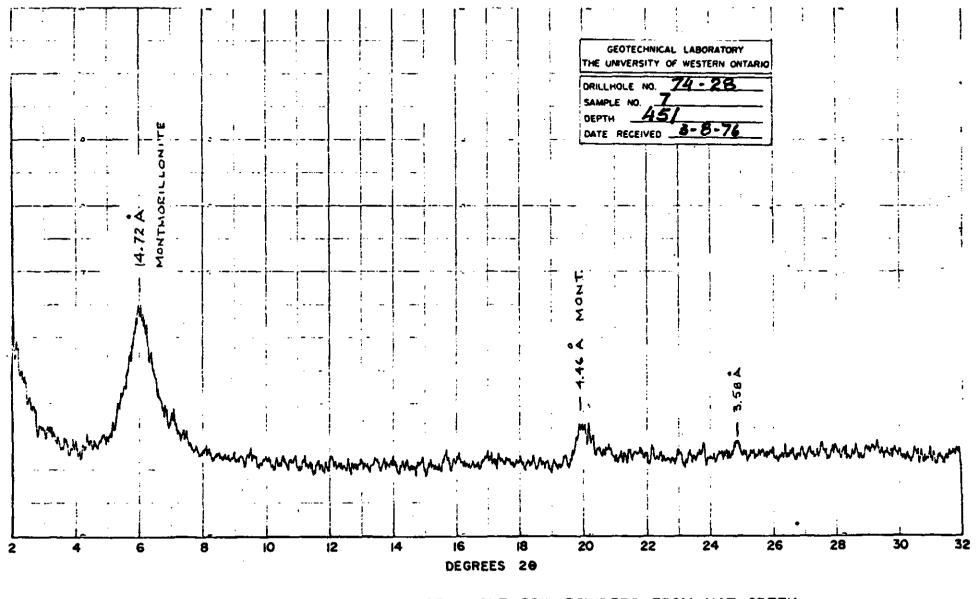


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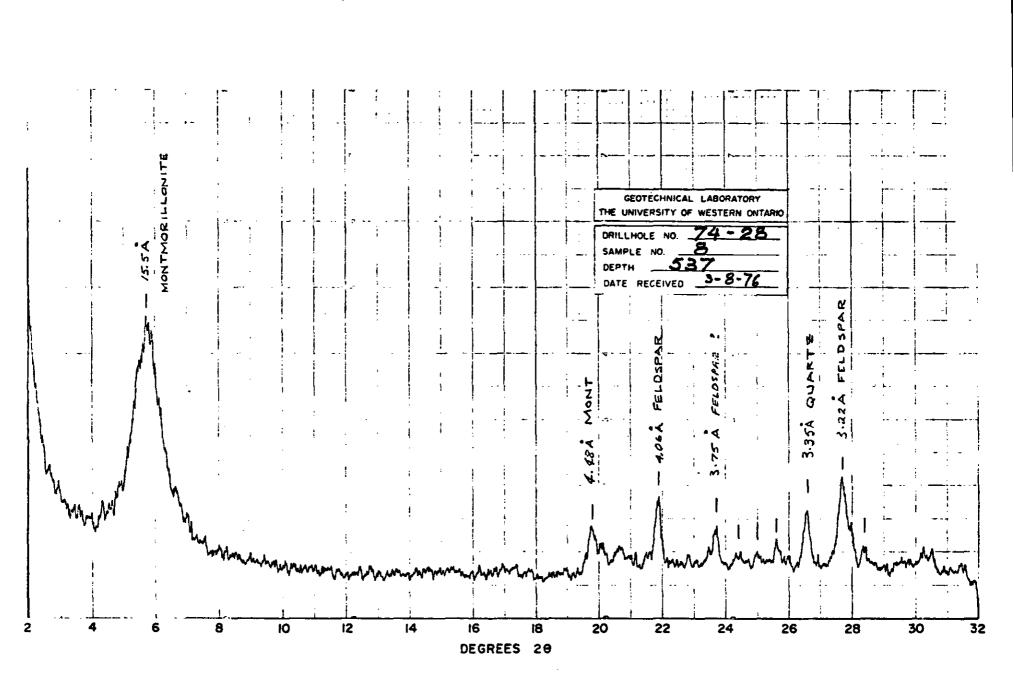


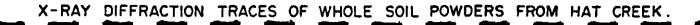


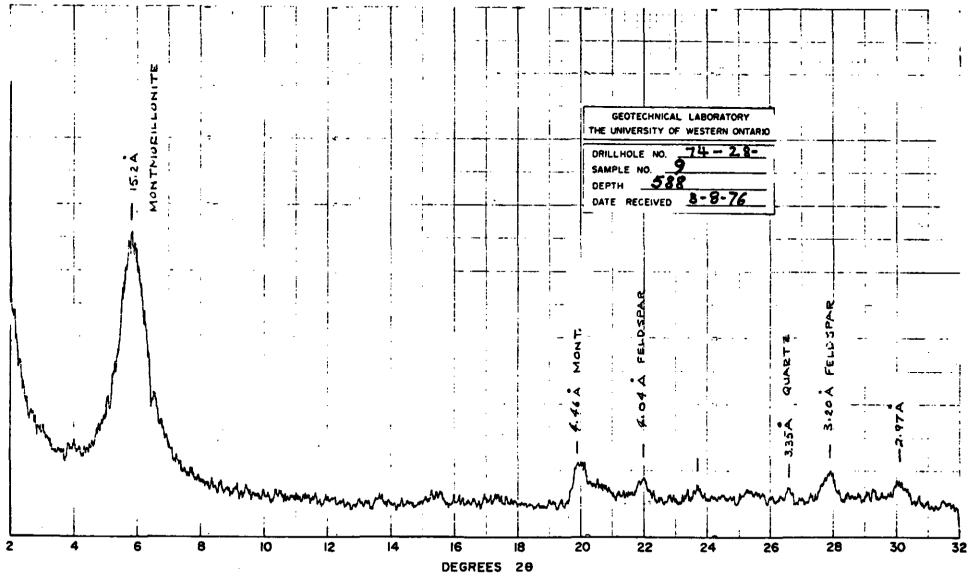


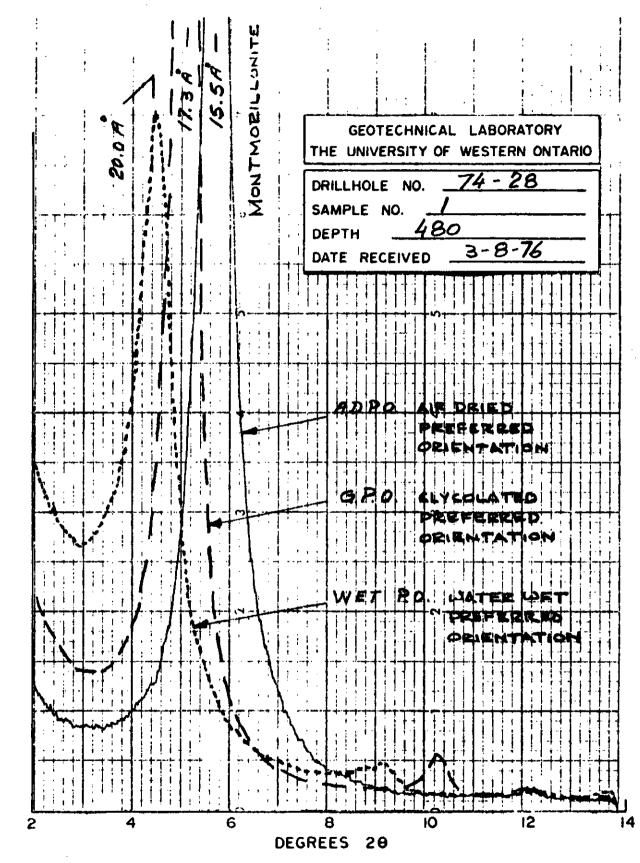


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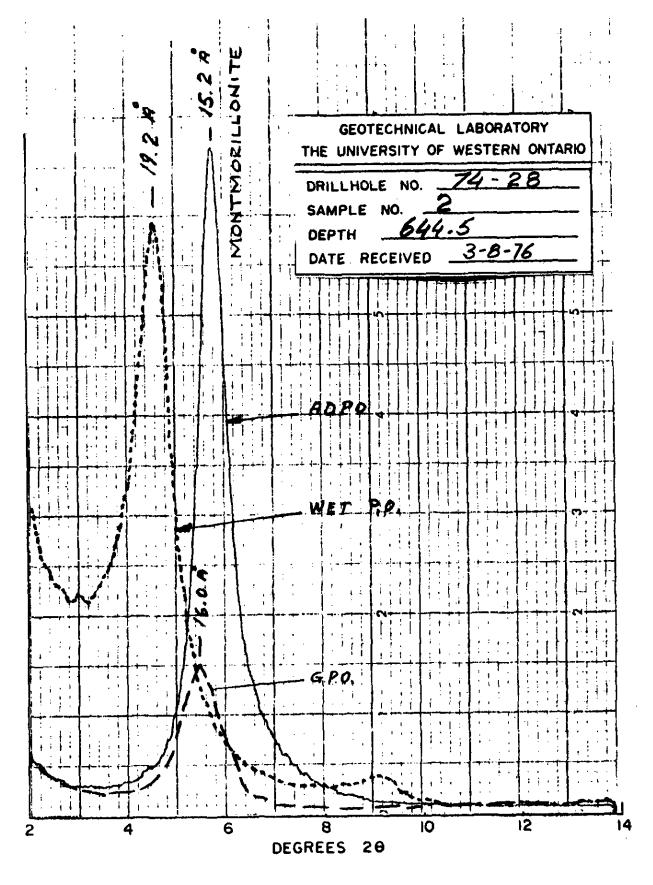




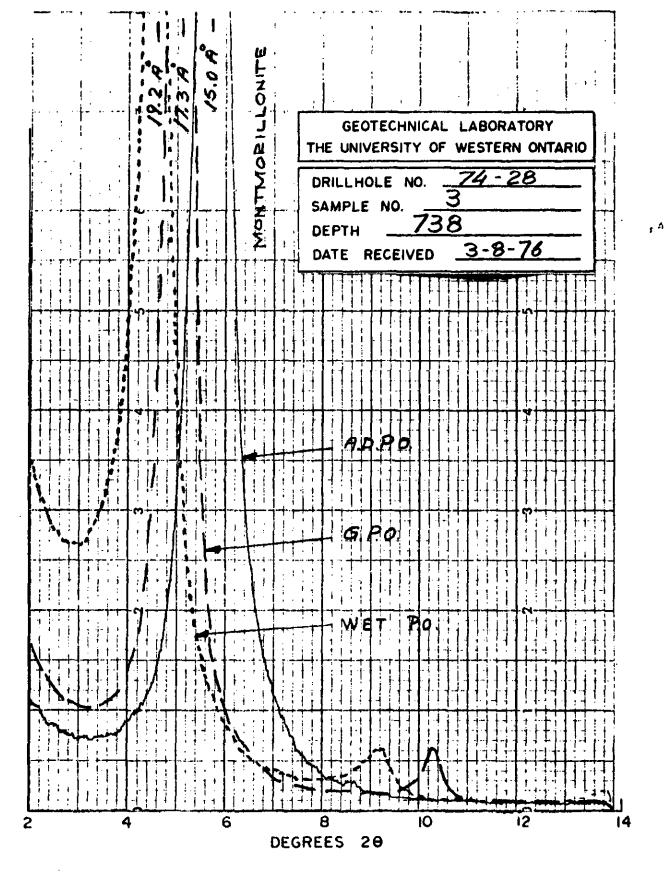




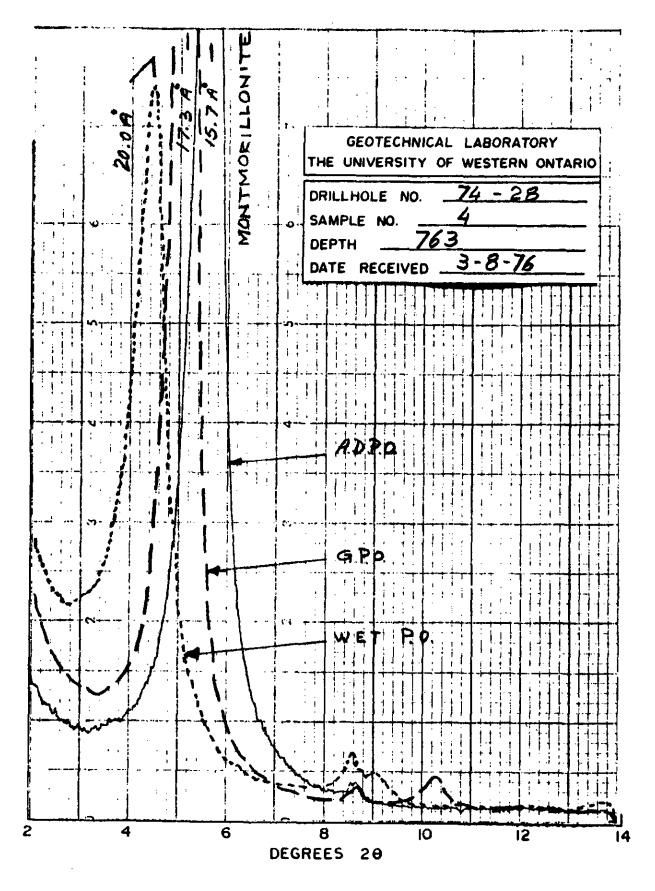




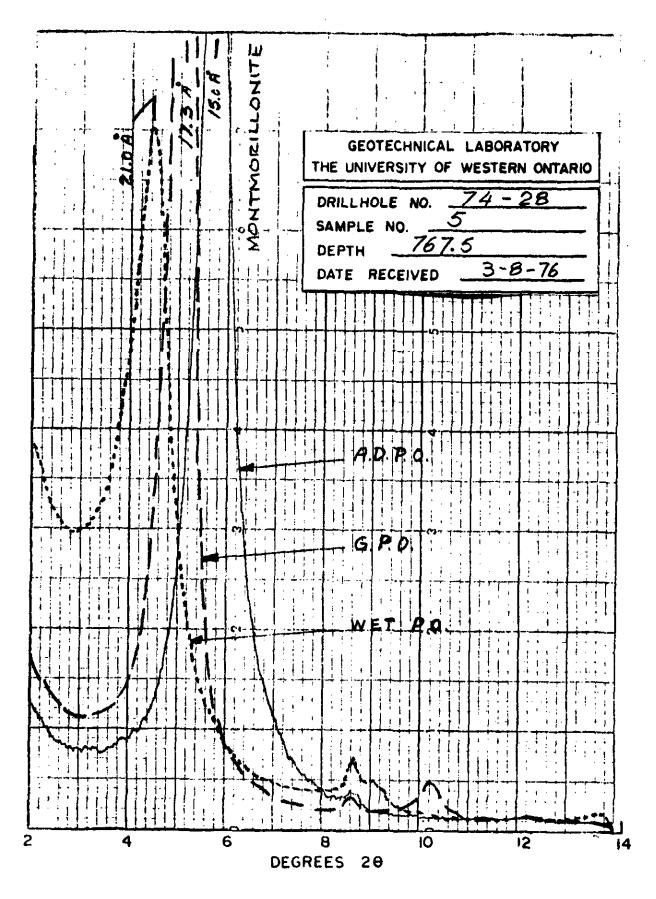
X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK .



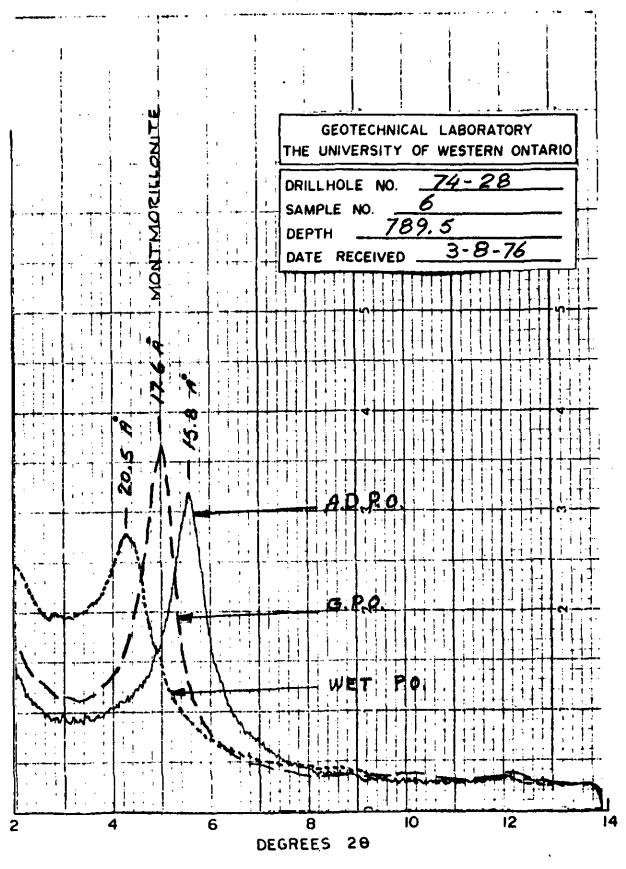




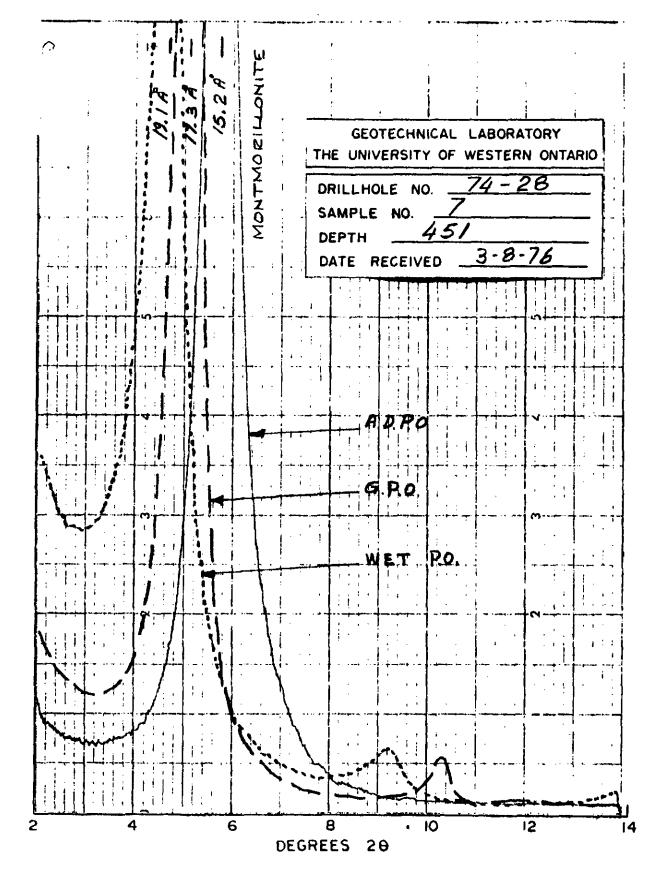
X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



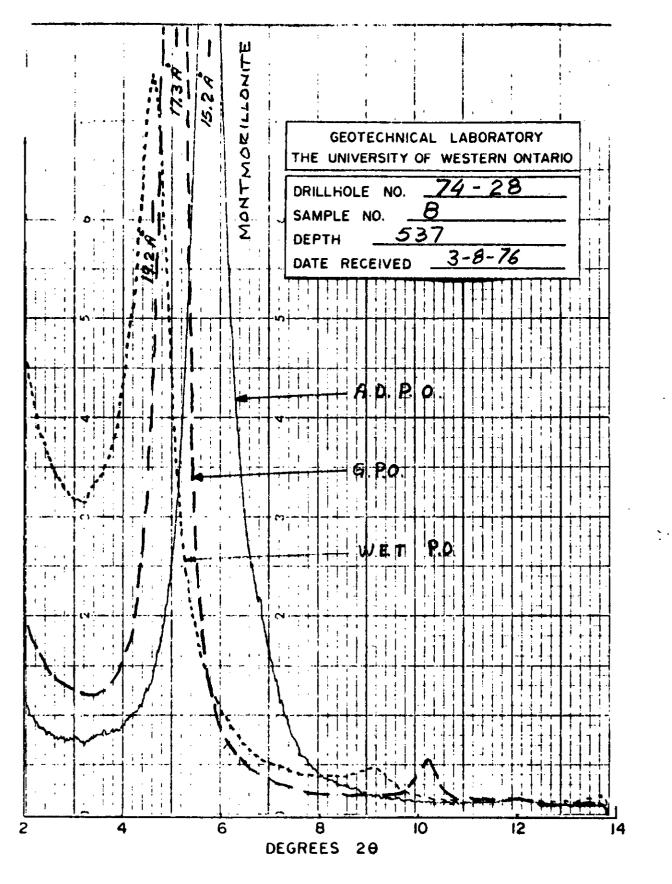
X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK .



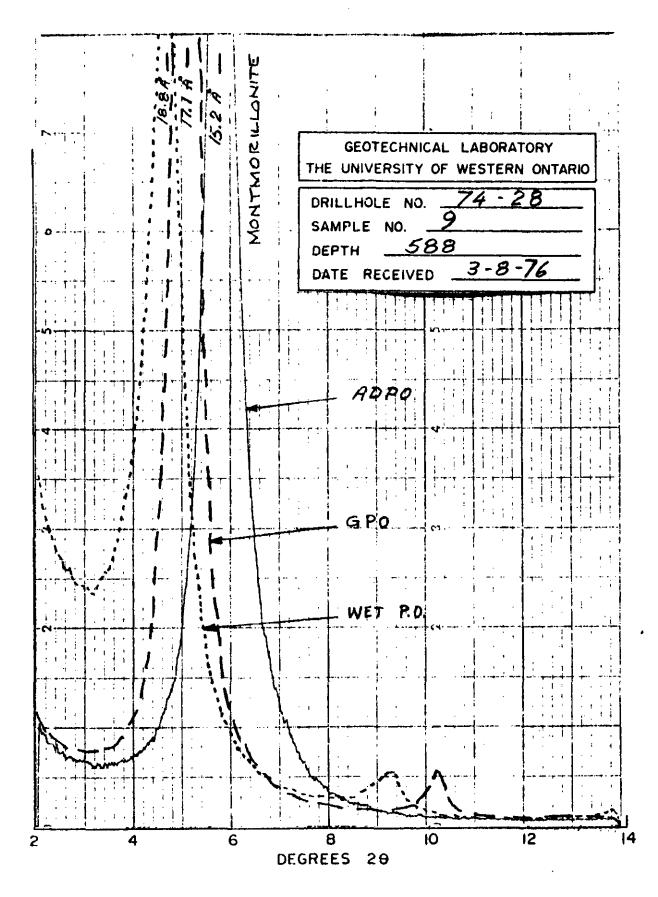
X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK .

The University of Western Ontario

Faculty of Engineering Science London, Canada NGA 589

August 17, 1976

Mr. G. Rawlings Golder, Brawner & Associates Ltd. 224 West 8th Avenue Vancouver, B.C. V5Y 1N5

Dear Mr. Rawlings:

FEB 15 1927

Report #2 - Supplement Hat Creek Project - Mineralogical Analyses August 17, 1976

This supplement to Report #2 contains reruns of all powder x-rays on samples for B.H. #74-28. The traces were obtained on rocks more finely ground (<200 mesh) in an attempt to strengthen the x-ray peaks.

The traces are essentially as in the original report with strengthening of some of the peaks, especially those for siderite.

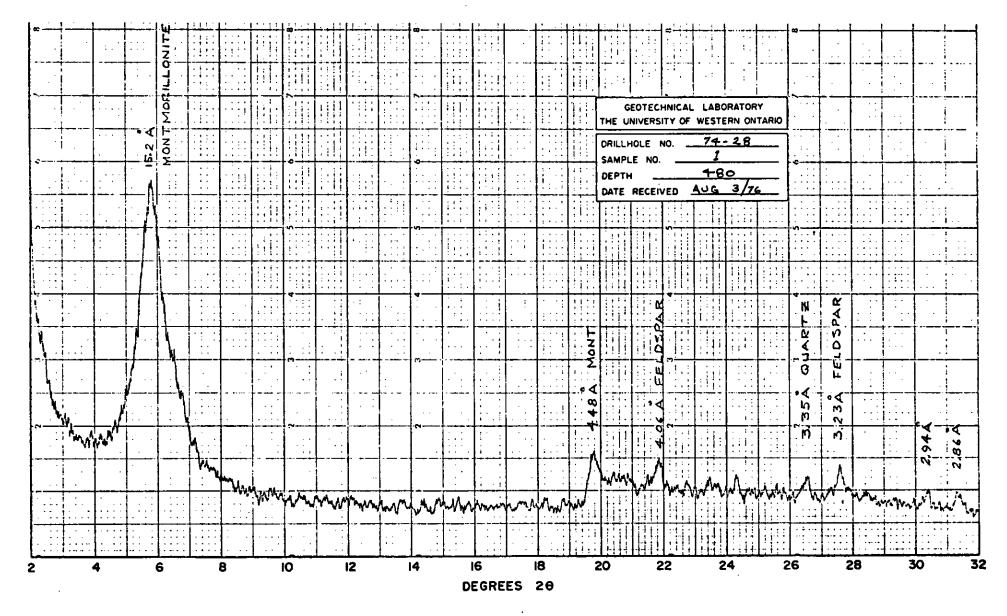
The most remarkable aspect of the powder patterns is the great size of the montmorillonite 15Å peak in all traces except B.H. #78-28 sample #6 where it is virtually absent. Montmorillonite is still present as shown in the preferred orientation traces for this sample in our Report #2.

There is little evidence of cristobalite and other ash derived minerals in the rocks analyzed to date except possibly sample 74-28-2 in which a 4.06Å peak without other feldspar peaks could possibly be cristobalite.

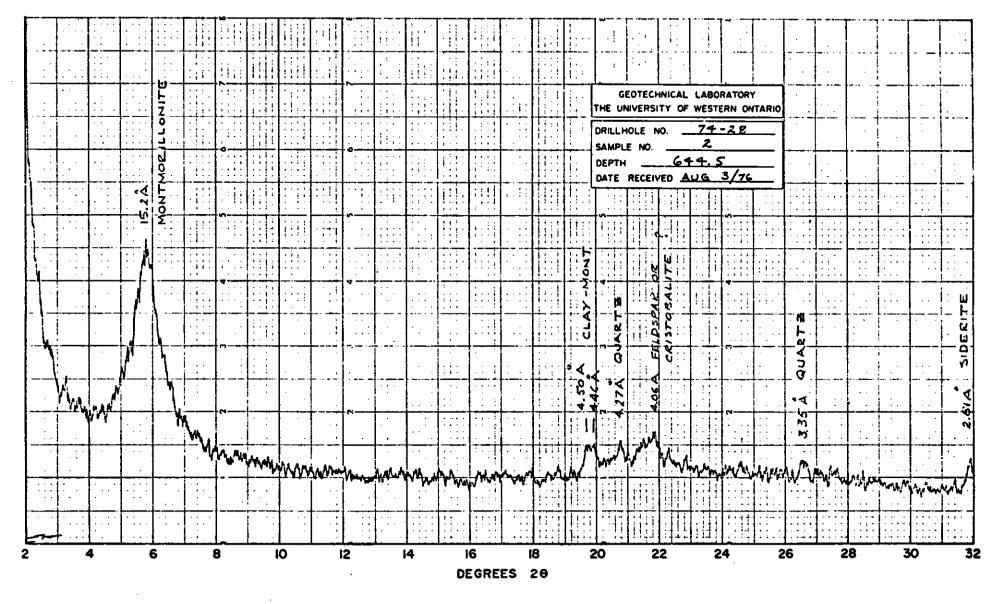
Yours Fincerely,

R.M. Quigley, P.Ehg. Professor of Geotechnical Engineering

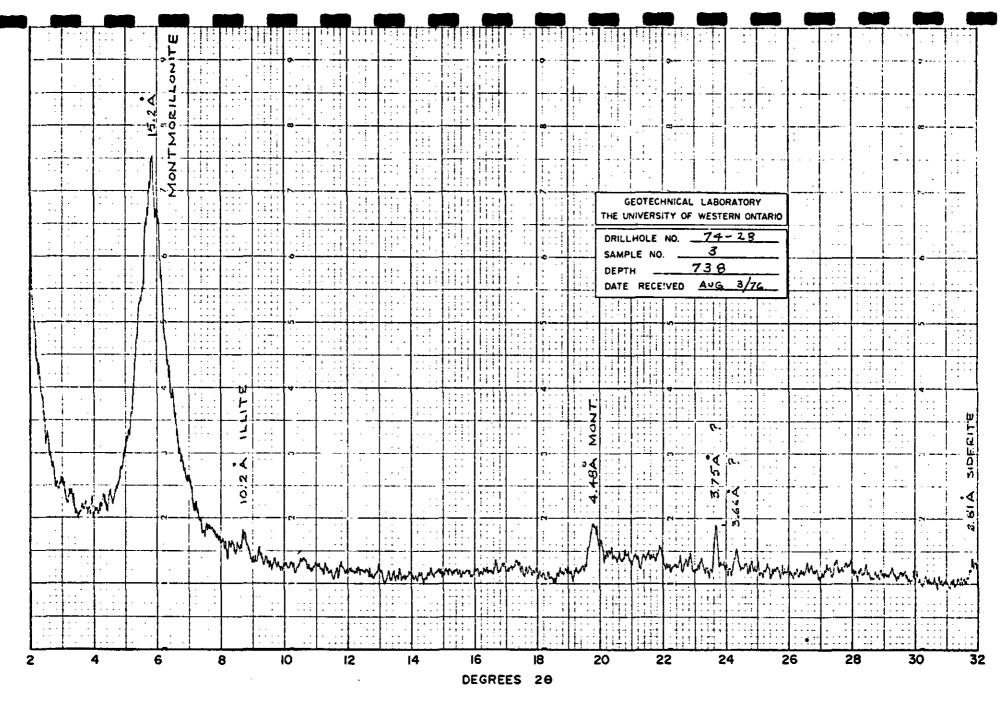
RMQ/jl Attach. cc. Mr. H. Hawson,/



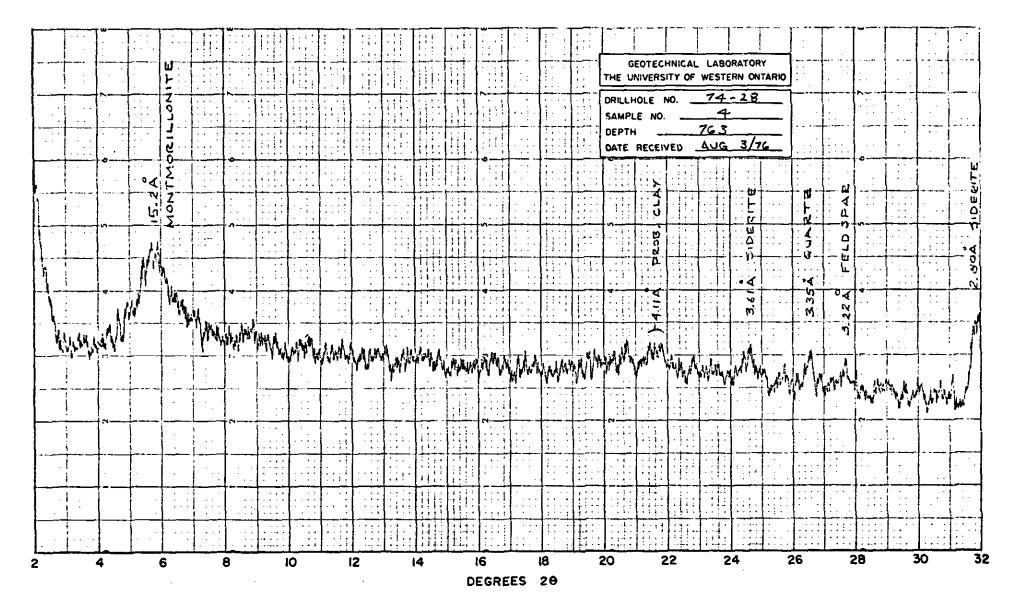
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.

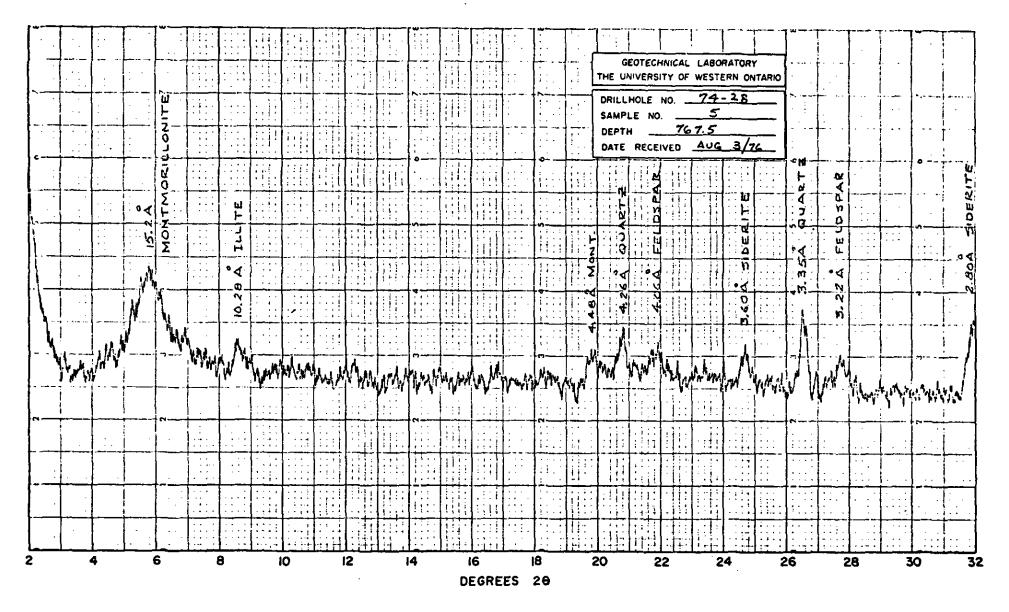


X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.

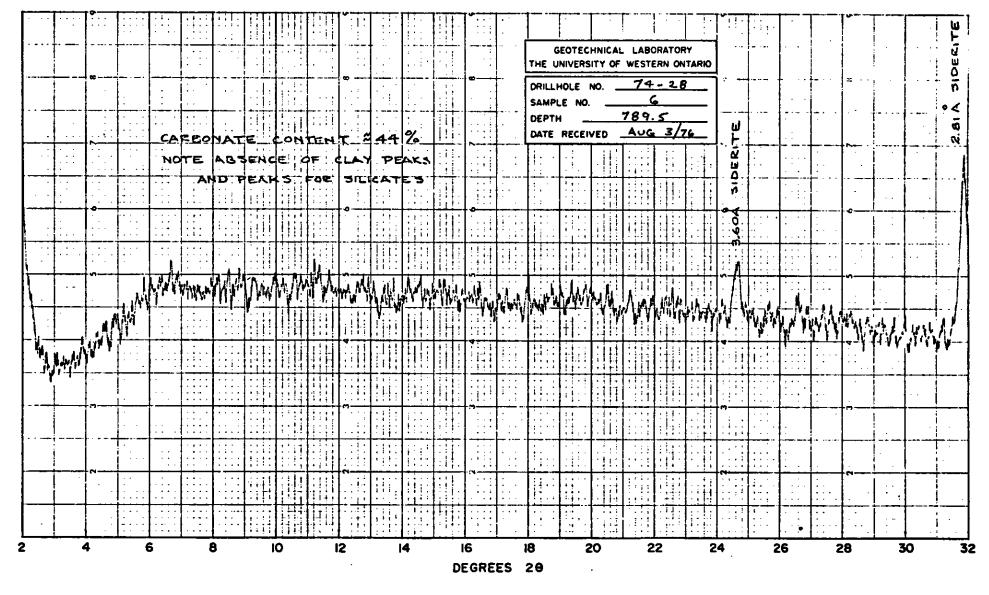






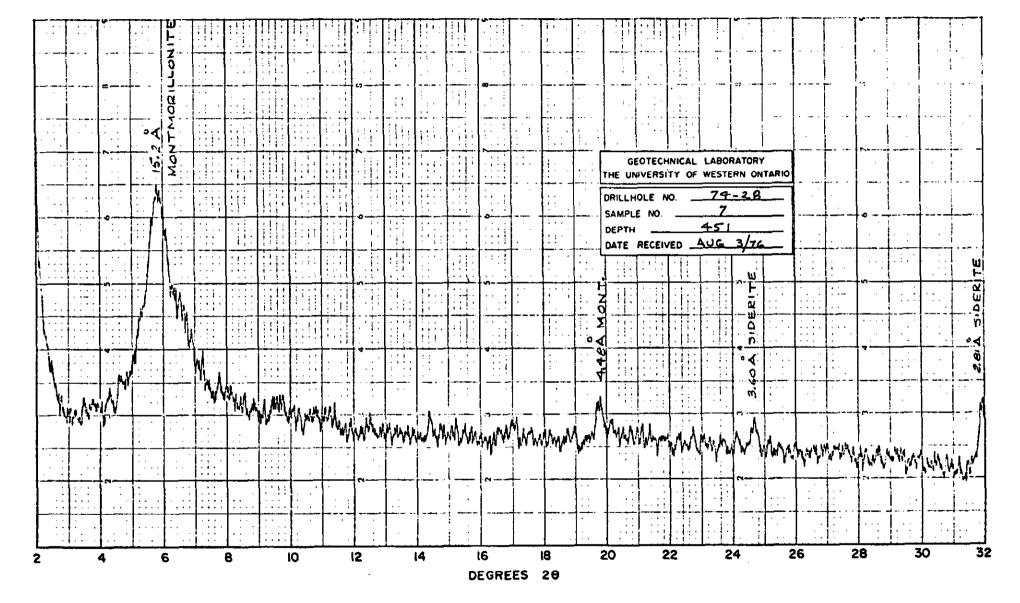


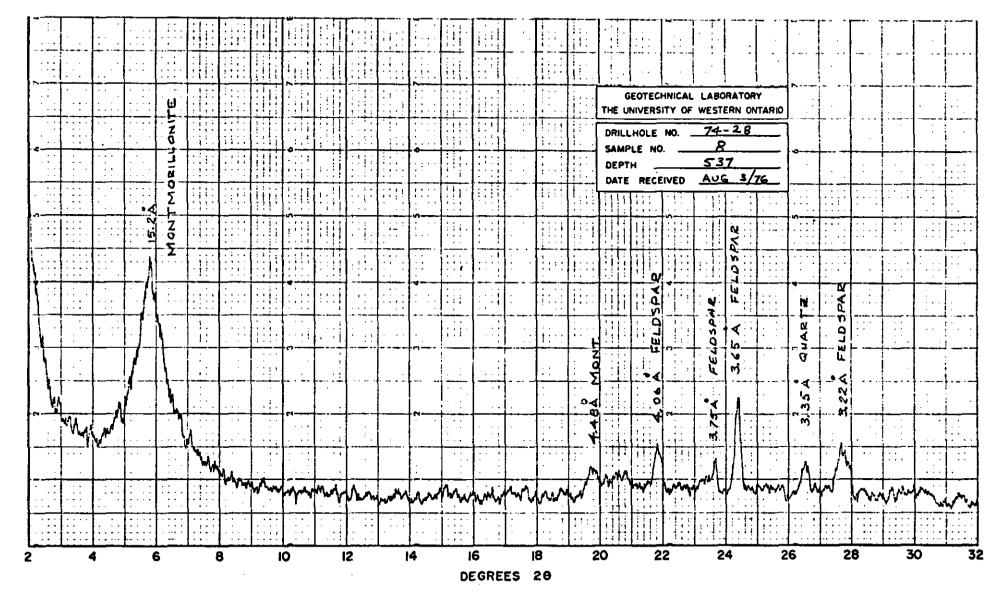
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.

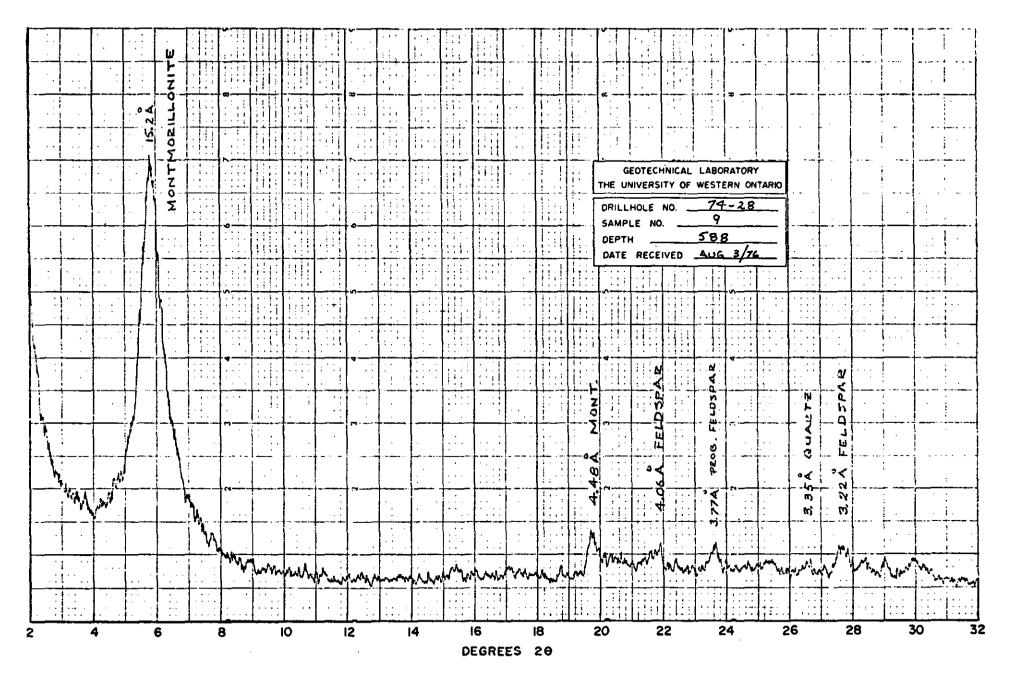


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The University of Western Ontario, London, Canada

Faculty of Engineering Science London, Canada N6A 589

20 August 1976

Mr. G. Rawlings Golder, Brawner & Associates Ltd. 224 West 8th Avenue Vancouver, British Columbia V5Y 1N5

Dear Mr. Rawlings:

Report #3 - Hat Creek Project - Mineralogical Analyses August 20, 1976

We have completed x-ray and carbonate analyses on eight samples from borehole 76-815 received from Mr. H. Hawson on August 3, 1976. We have yet to complete the x-ray and carbonate analyses on eight further samples, however, these will be forwarded to you in early September.

During September we will also run the selected Na⁺ analyses and glycol retention values on the samples received to date.

Comments on Borehole 76-815

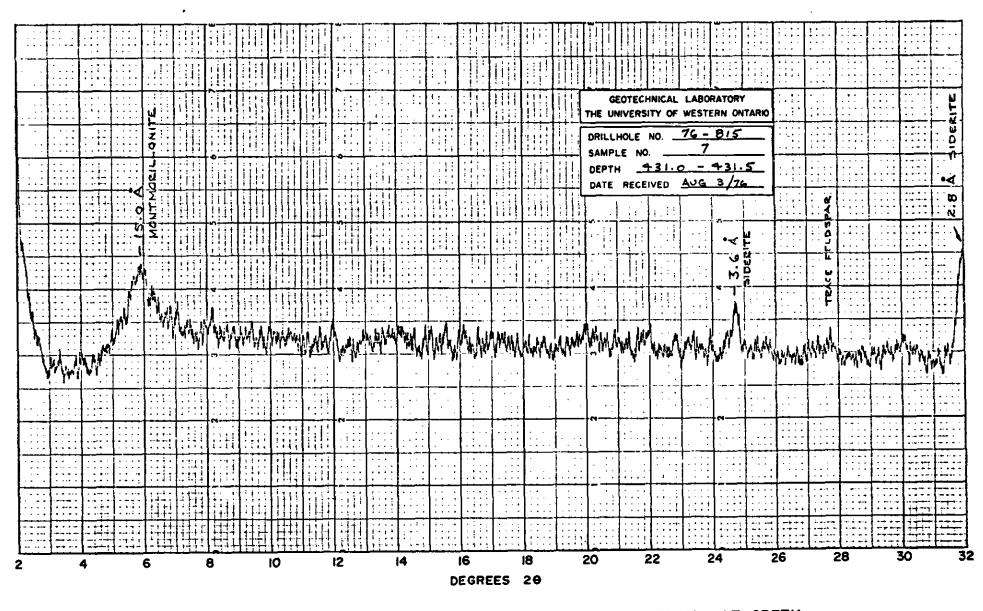
- Carbonate analyses supplemented by the x-ray powder patterns showed the heavily indurated rocks to consist of 34 to 68% siderite. All rocks supplied from this hole reacted with HCl (when powdered) indicating some carbonate.
- 2. Where siderite was very abundant (Sa. #7, 9, 18, 22 and 29) the montmorillonite peaks were very weak or absent on the powder patterns. An absence of other peaks indicates a scarcity of silicate minerals noticed in previous rock samples.
- 3. Montmorillonite was confirmed to be present in the < 2 μ m fraction of all rocks as shown by the x-ray traces on oriented specimens.
- 4. It is concluded that the rock specimens supplied from this borehole consist dominantly of monomorillonite and siderite. Quartz and feldspar are rare (< 10%) and clearly observed only on two powder matterns for samples #12 and 20.

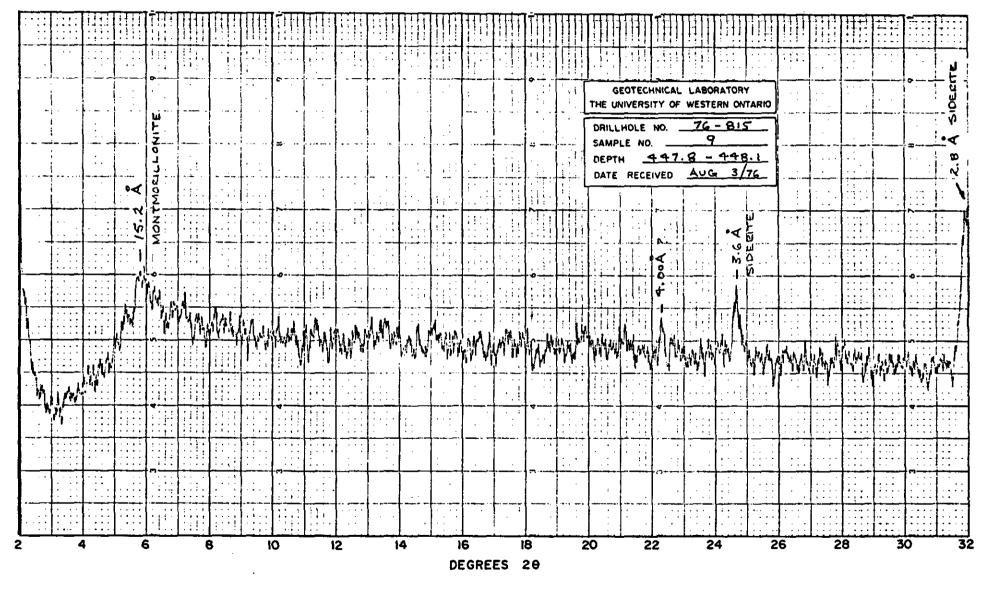
Yours sincerely,

R.M. Quigley, P.Eng. / Professor of Geotechnical Engineering

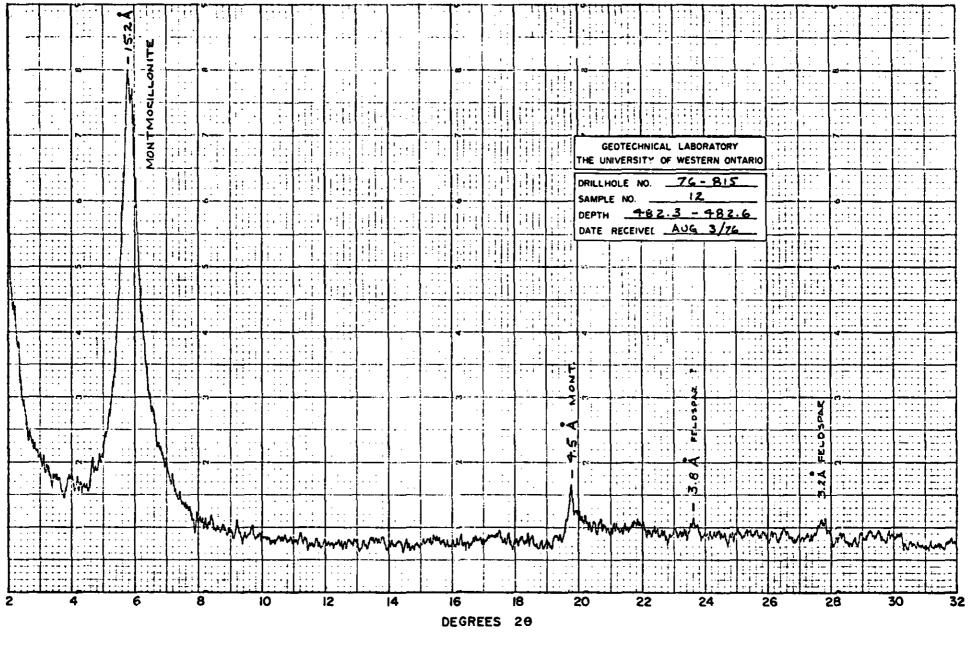
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No. No. 76-815 76-815 76-815 76-815	ample No. 7 9 12	Depth (Feet) 431.0 - 431.5 147.8 - 498.1		Wet P.O.	X-ray ADPO	GPO	Tes Powder	ting Complete Carbonate (%)	Glycol Retention	Na ⁺
Hole No.	No. 7 9	(Feet) 431.0 - 431.5	Received	}	ADPO	GPO	Powder		Retention	
NO. 76-815 76-815 76-815 76-815	7 9	431.0 - 431.5	AUG 3/76	}			Powder	(%)		
76-815 76-815 1 76-815 1	9			~	V			(%)	(mg/g)	(PPM)
76-815 1 76-815 1		447.8-448.1	,	the second s			7	34.5		
76-815	12		AUG 3/76	~	~	~	1	51.2		
		482.3 -482.6	AUG 3/76	~	~	~	~	3.5		
76-815	14	505-6-506.0	AUG 3/76	~	~	~	~	7.5		
	18	541.5-542.0	AUG 3/76	~	~	~	7	34.3		
76-815 3	20	561.7 - 562.3	AUG 3/76	~	~	~	~	9.3		
76-815 2	22	582.7 - 583.2	AUG 3/76	~	~	~	~	67.6		
76-815 2	29	669.0-669.7	AUG 3/76	~	~	~	~	35.5		
		 			 	 			EPORT *	
								1.	1. Quige aug. 20, 197	est -

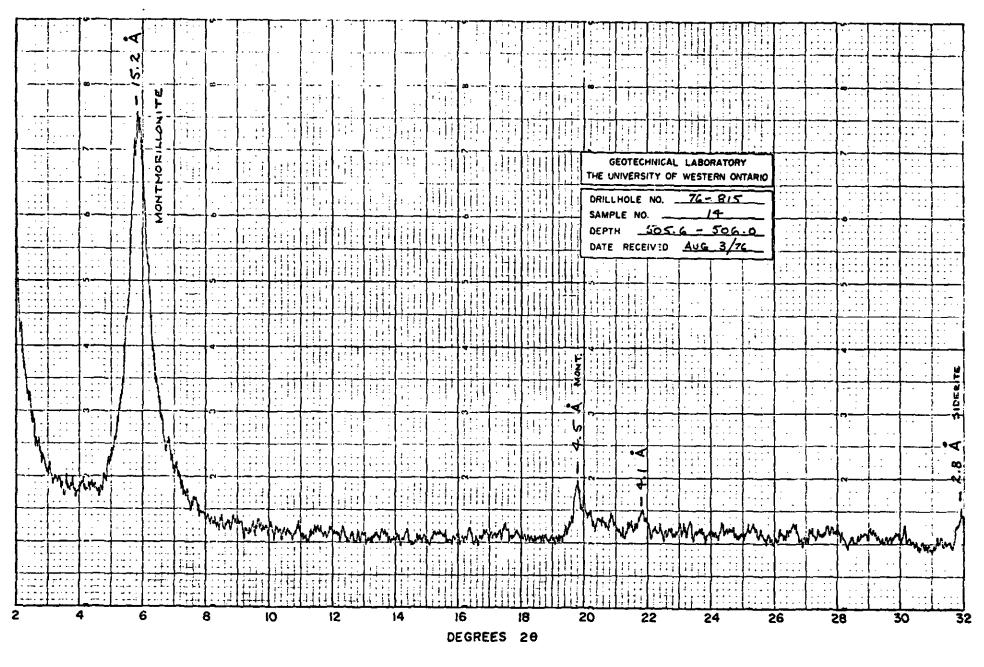




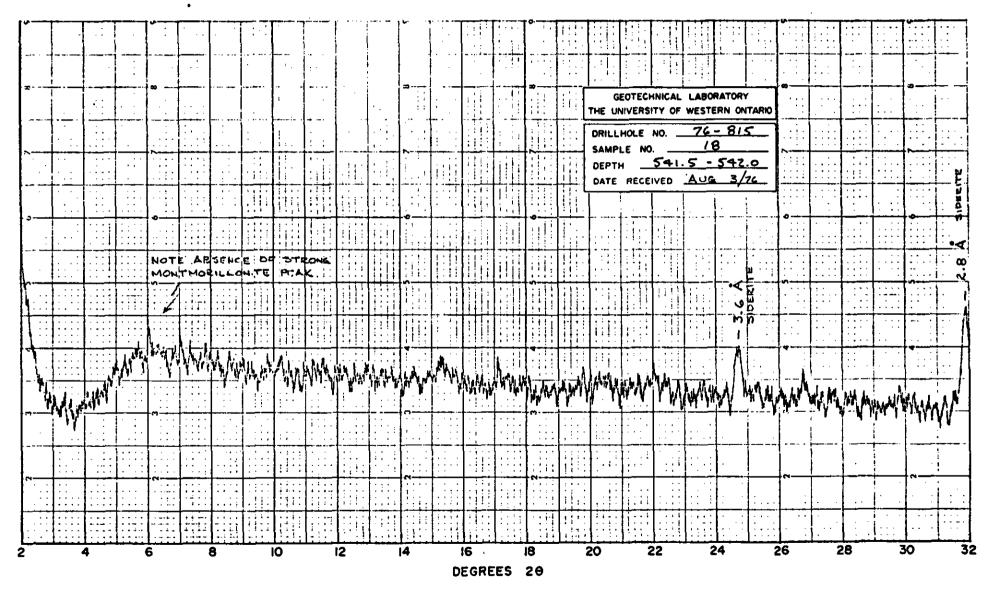
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.

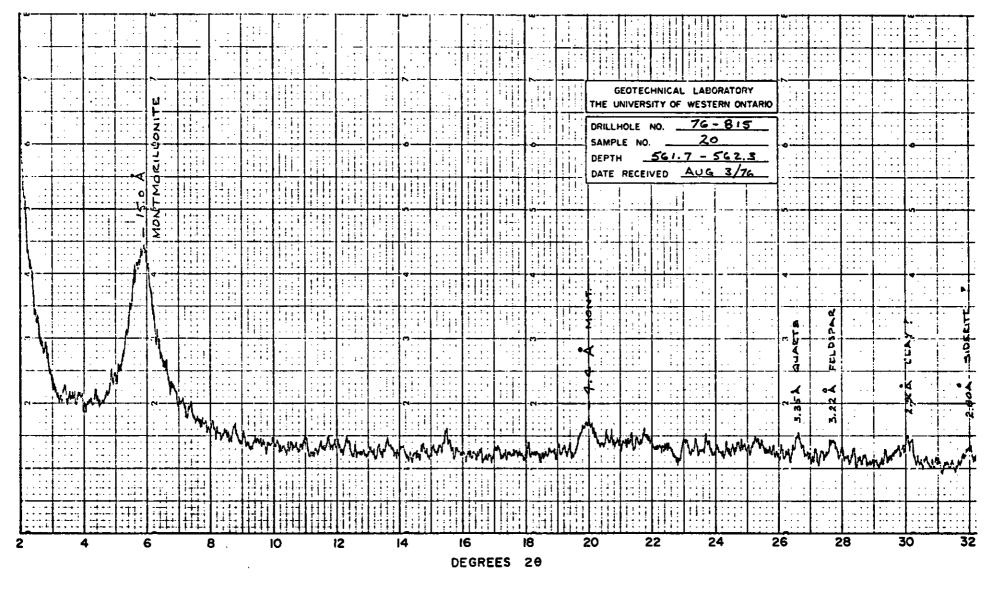


X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.

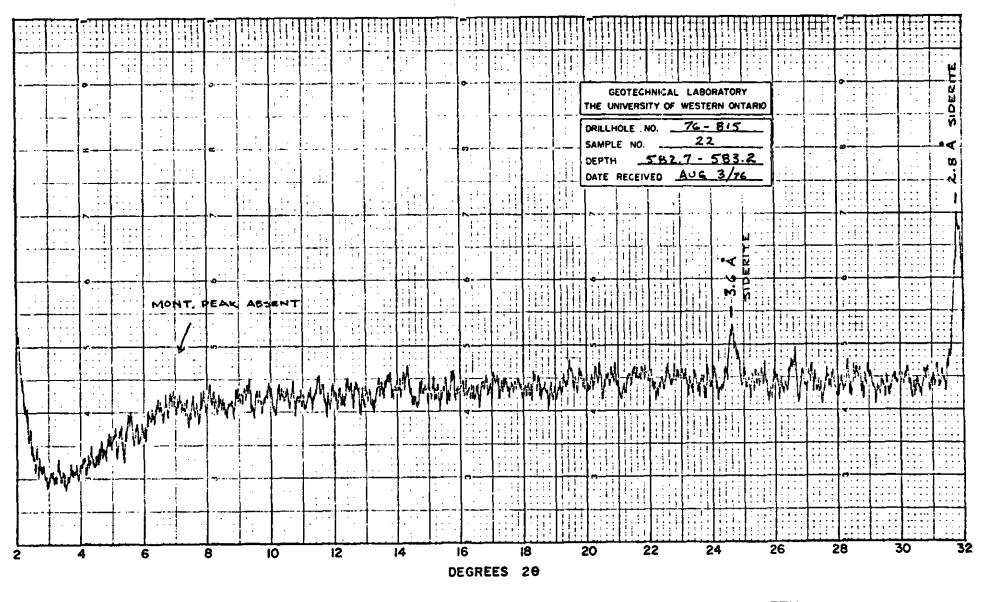








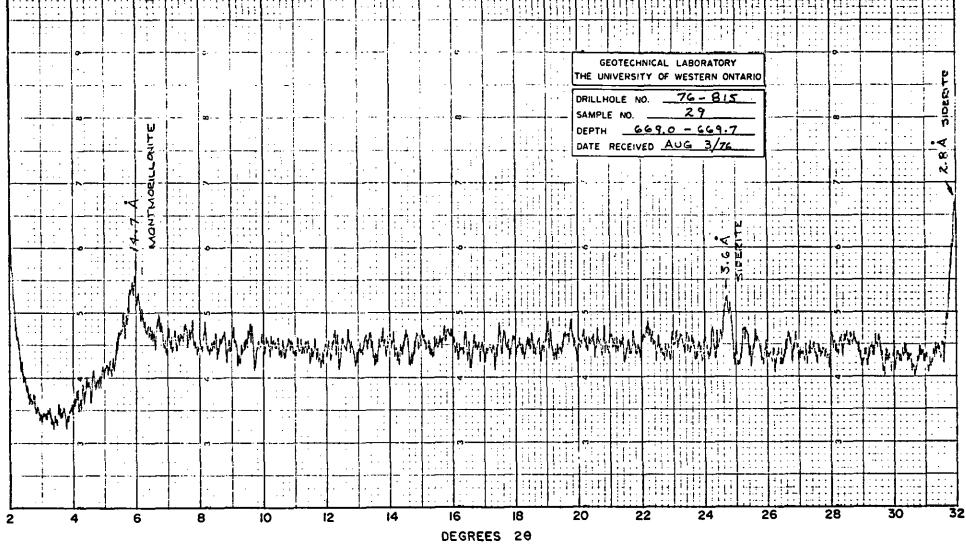
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



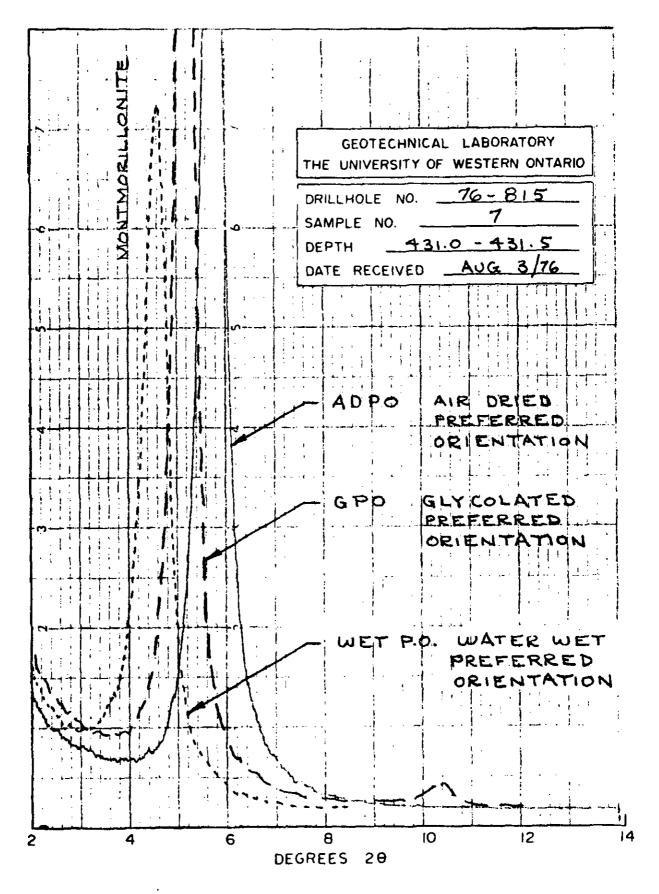
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X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



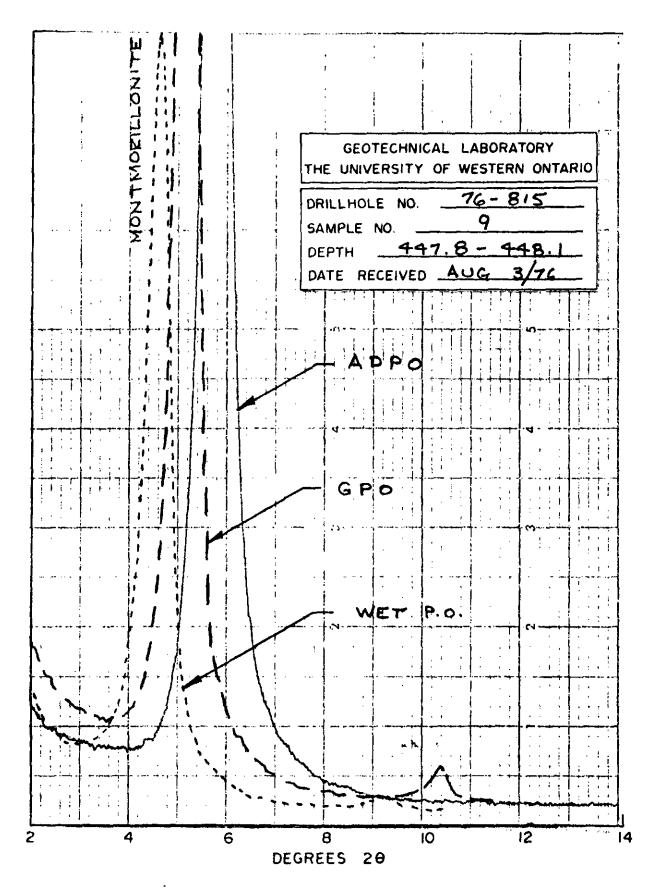


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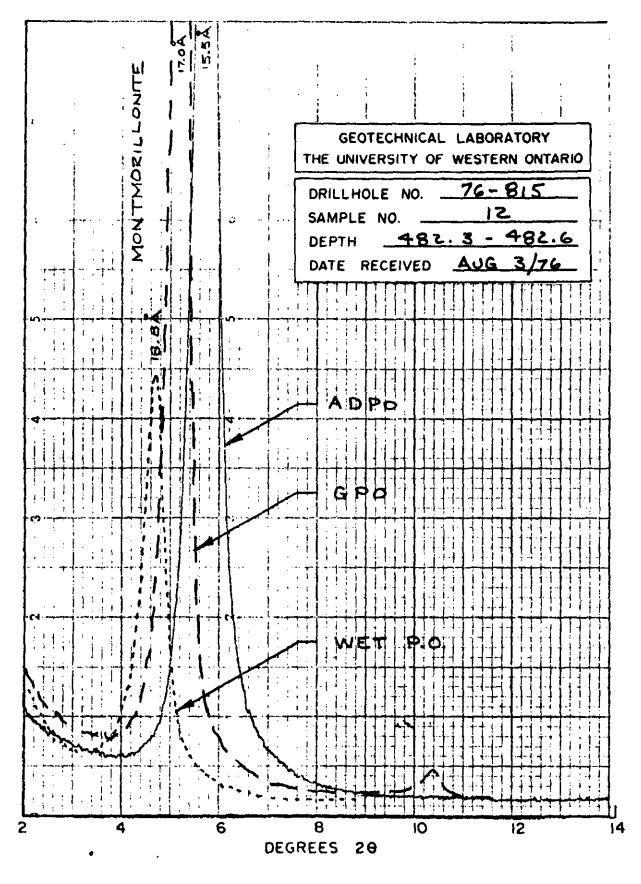




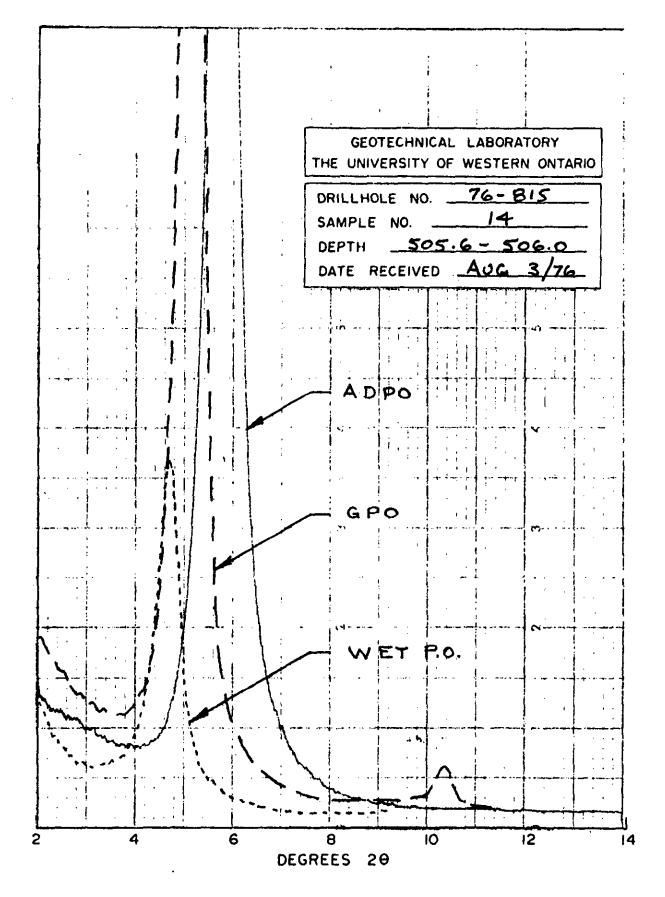
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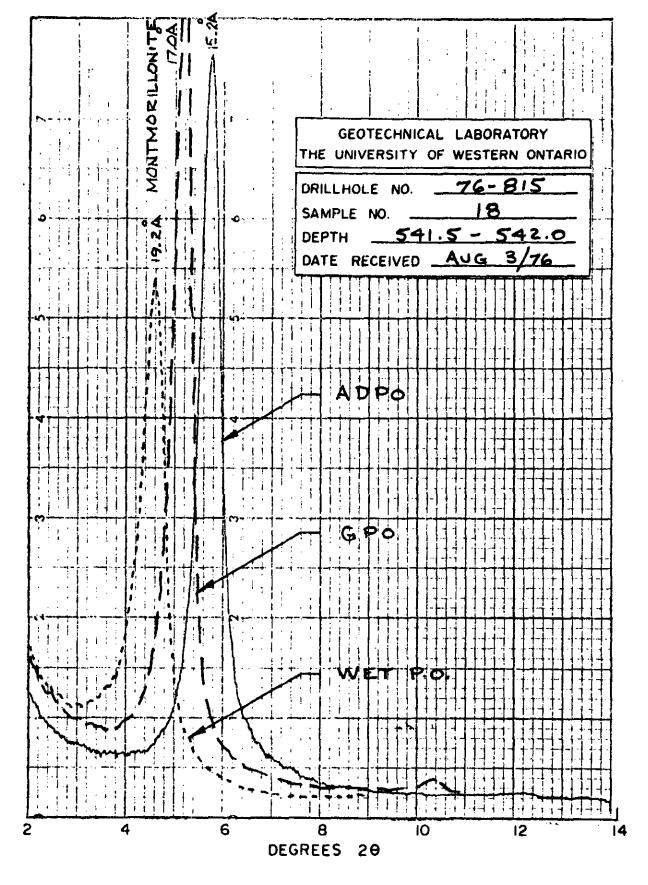




X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.

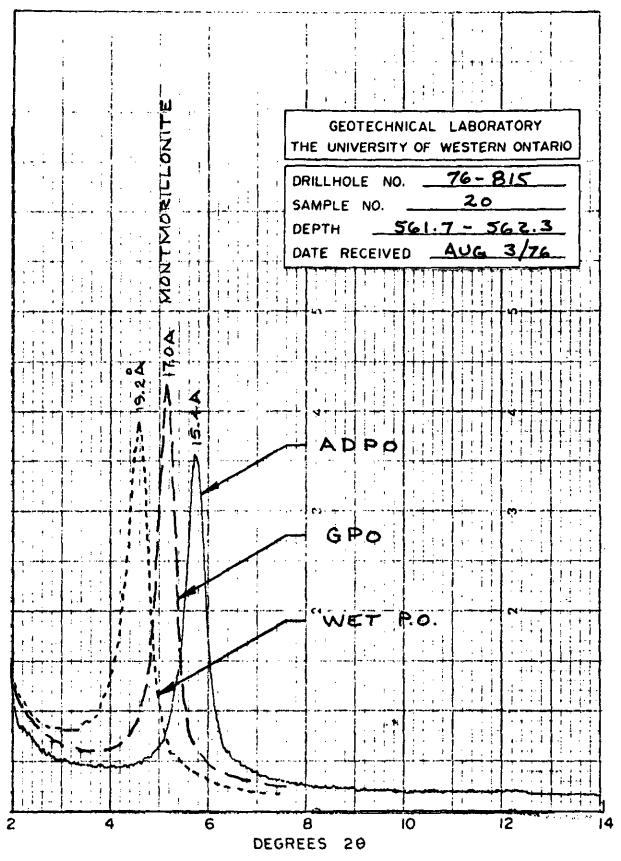




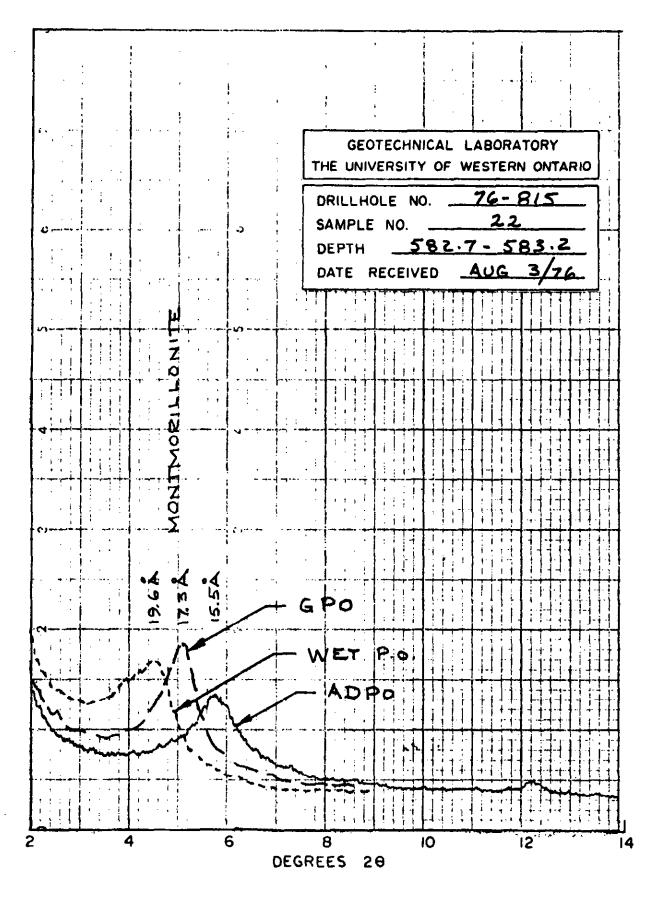


X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.

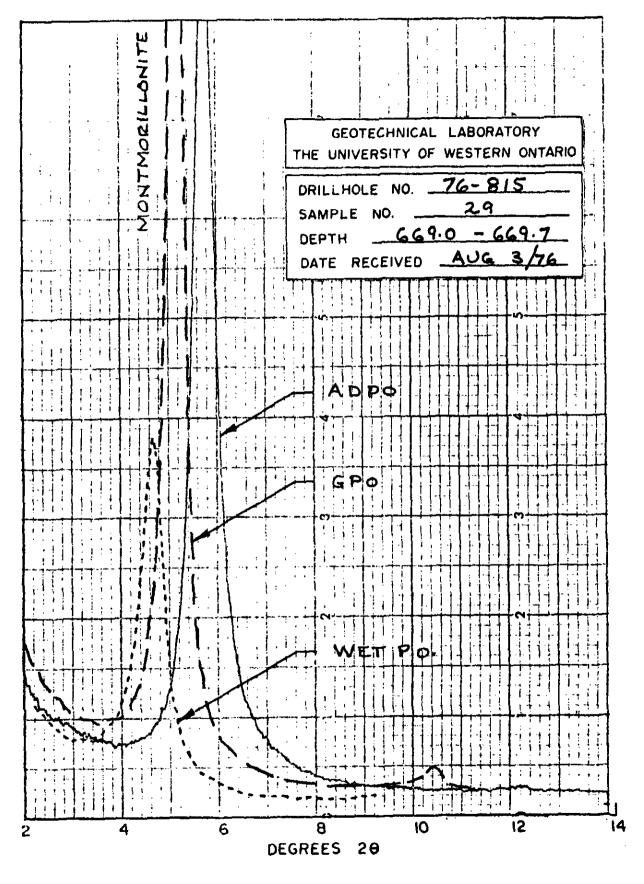
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X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK .



X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK .







FEB 15 1977

FILE No.

The University of Western Ontario, London, Canada

Faculty of Engineering Science London, Cenada N6A 689

7 September 1976

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RHC

Mr. G. Rawlings Golder, Brawner & Associates Ltd. 224 West 8th Avenue Vancouver, British Columbia V5Y 1N5

Dear Mr. Rawlings:

Report #4 - Hat Creek Project - Mineralogical Analyses Y REF

Enclosed are the x-ray and carbonate analyses on the last eight samples of Mr. Hawson's shipment of August 3, 1976.

On the basis of the cross-sections which you are sending to me, I will select samples for Na⁺ and glycol retentions. As we discussed by phone today, I will call you prior to commencing this last phase of the testing.

Specific Comments on Present Samples

- 1. Carbonate is abundant only in sample 76-816.
- 2. Most of the samples consist of montmorillonite and feldspar with trace amounts of quartz.
- 3. Sample 76-809 (#2) may contain some cristobalite.

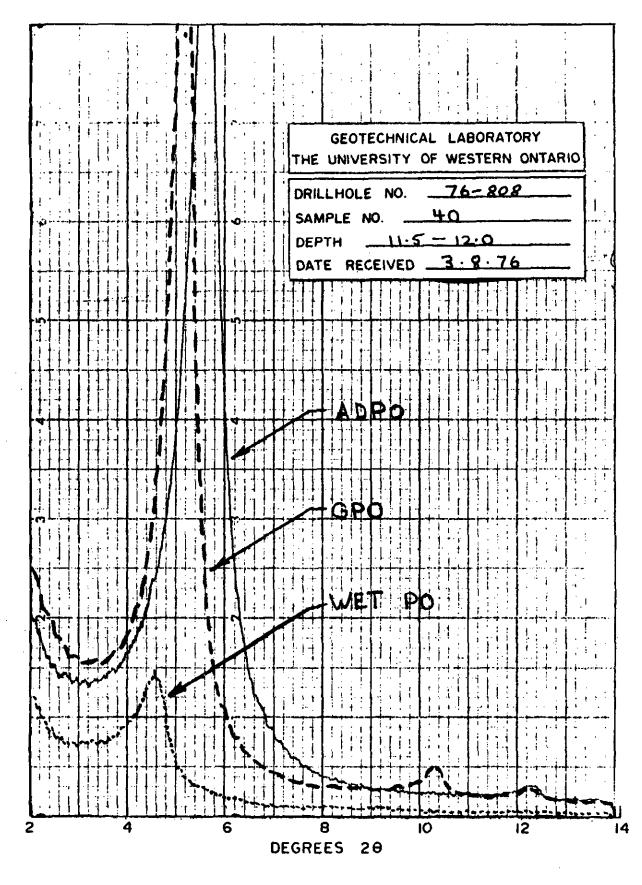
Yours sincerely,

R.M. Quigley, P.Eng. Professor of Geotechnical Engineering

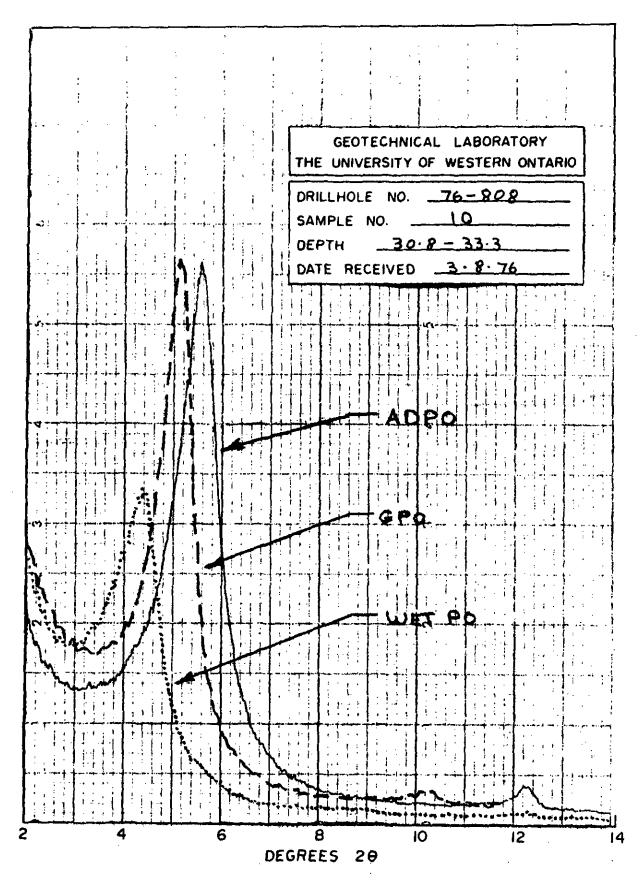
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cc: Mr. H.H. Hawson, Kamloops, B.C.

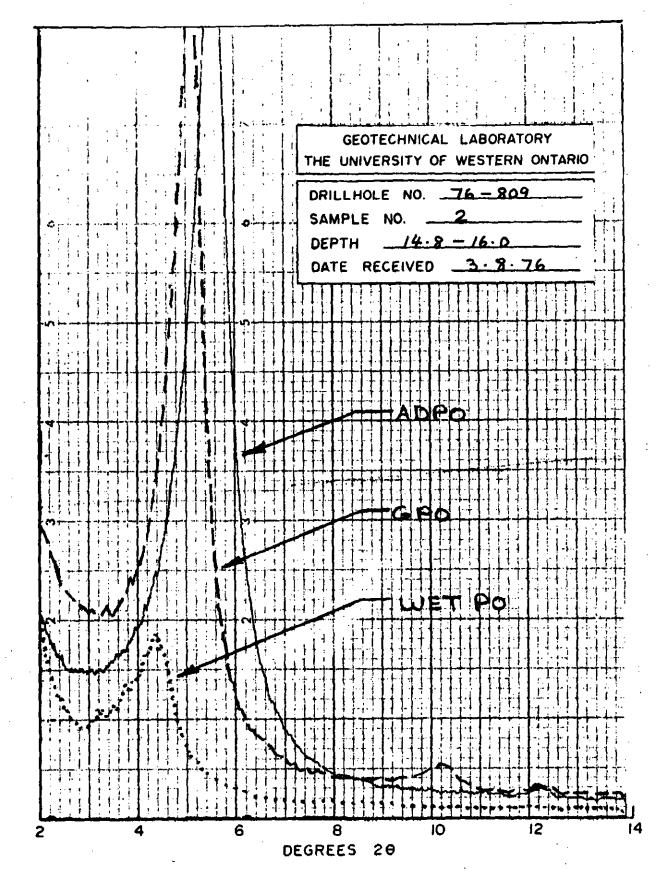
HAT CREEK PROJECT LIST OF SAMPLES RECEIVED FROM GOLDER BRAWNER A				& ASSOCIA	TES			GEOTECHNICAL LABORATORY THE UNIVERSITY OF WESTERN ONTARIO			
Drill Hole No.	Sample No.	Depth (Feet)	Date Received	Testing Completed							
				X-ray				Carbonate	Glycol Retention	Na ⁺	
				Wet P.O.	ADPO	GPO	Powder	(%)	(mg/g)	́рьм	
76-808	40	11.5 - 12.0	AUG 3/76	~	~	~	~	3.0			
76-808	10	30.8 - 33.3	AUG 3/76	~	~	~	~	1.7			
76-809	2	14.8 - 16.0	AUG 3/16	~	~	~	~	2.6			
76-809	4	32.6-33.8	AUG 3/76	~	~	~	~	2.7			
76-816	19	472.9 -473.7	AUG 3/76	/	~	-	~	30.7			
SLIDE HEADWALL	TI		AUG 3/76	~	~	~	7	2.8			
SLIDE HEADWALL	T2		AUG 3/76	7	レ	~	~	3.8			
SLIDE HEADWALL	T3_		AUG 3/76	7	~	~	~	4.2			
				· · · · · · · · · · · · · · · · · · ·					· · · · · · · · · · · · · · · · · · ·		
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								P	1. Quigly		



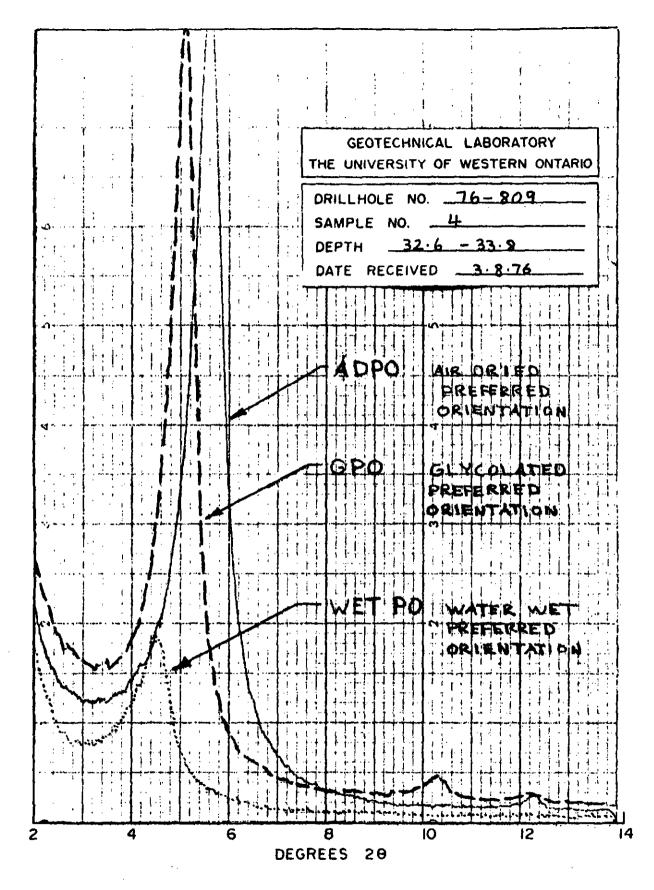
X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



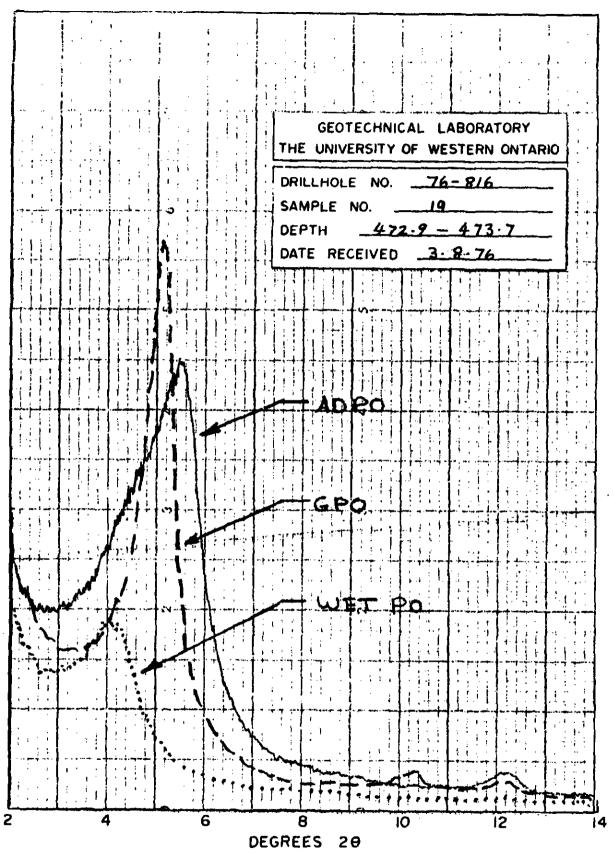




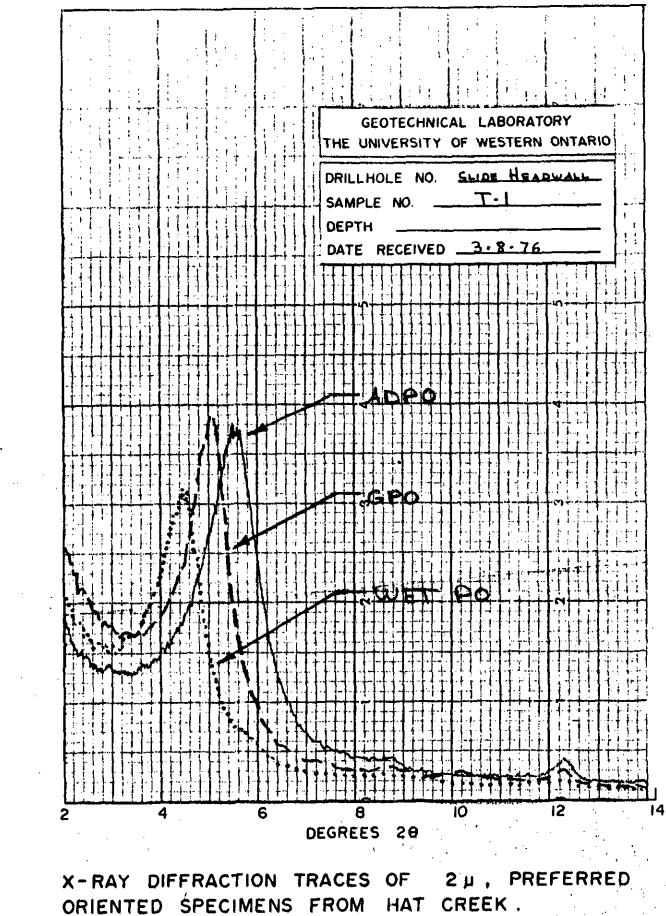




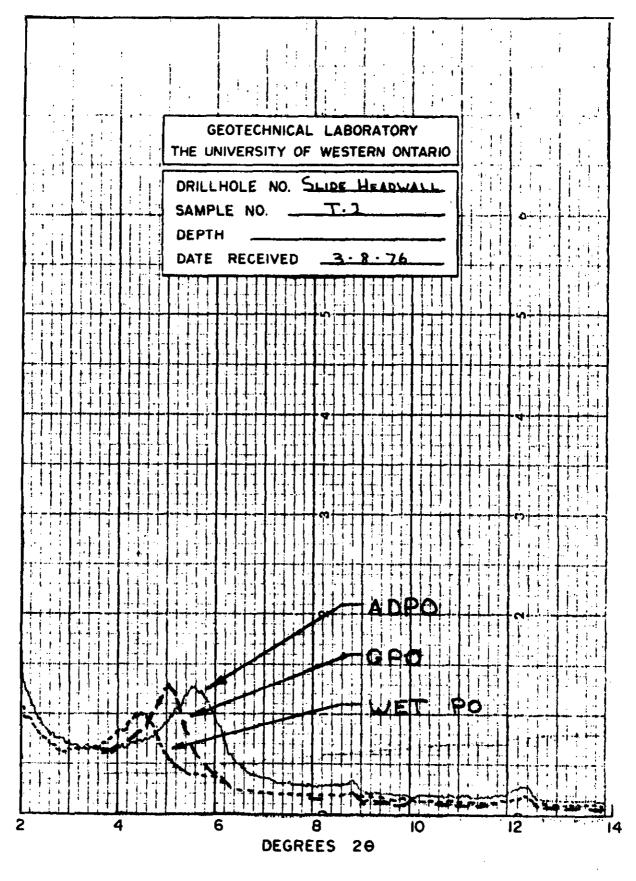




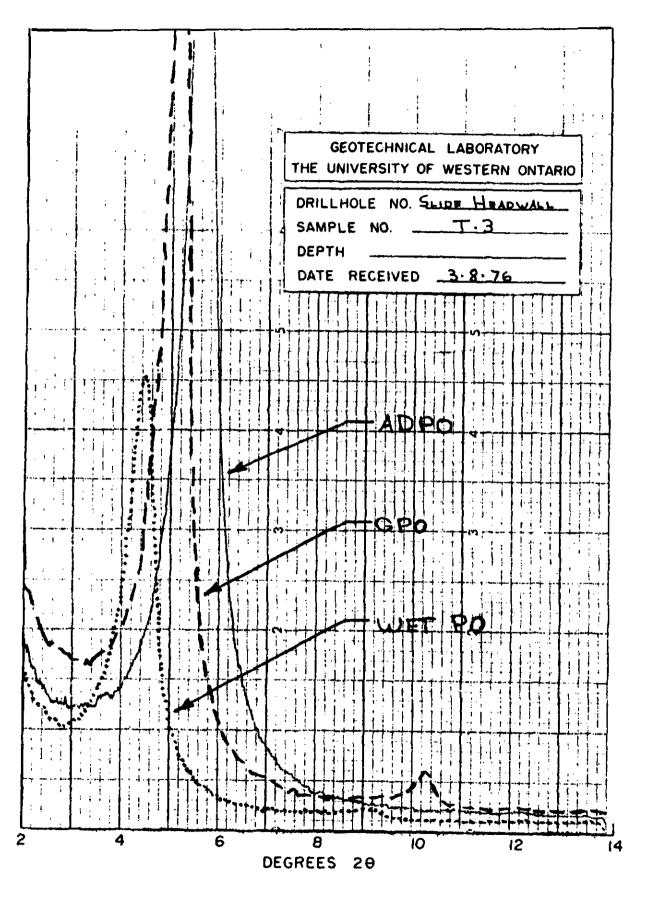
X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



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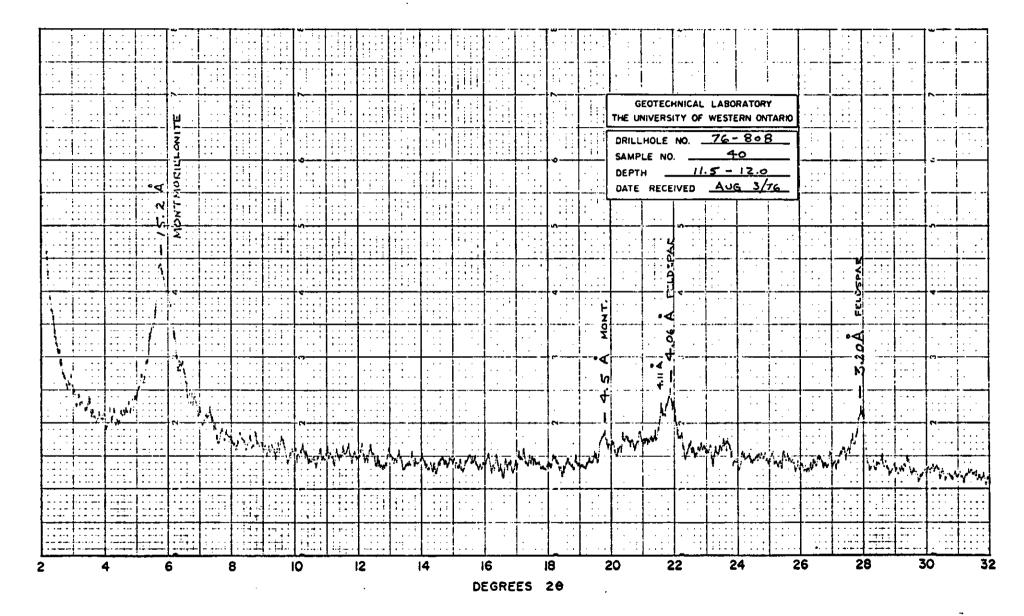


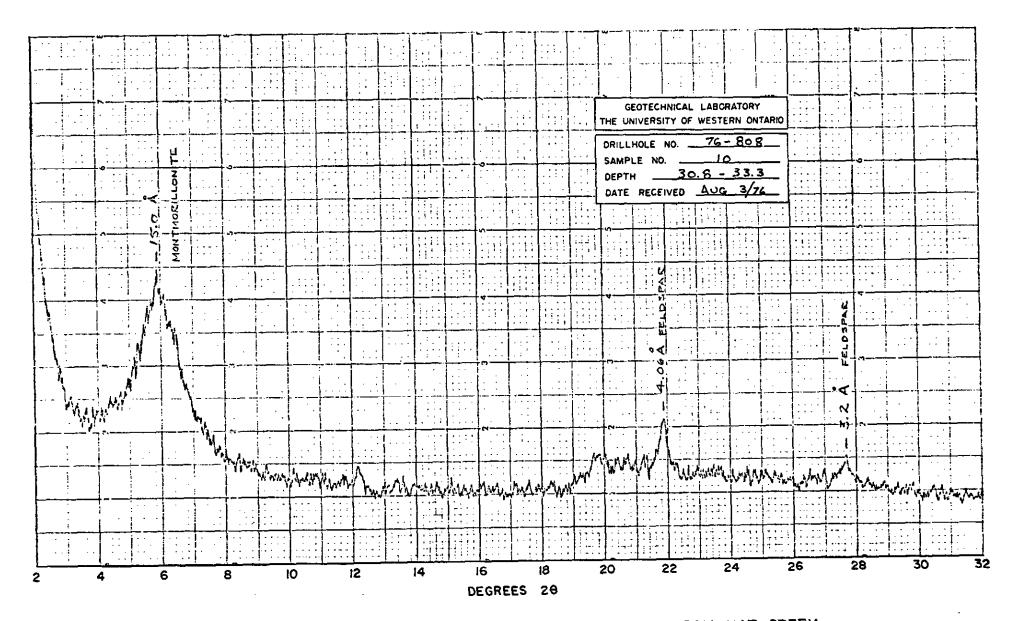
X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK





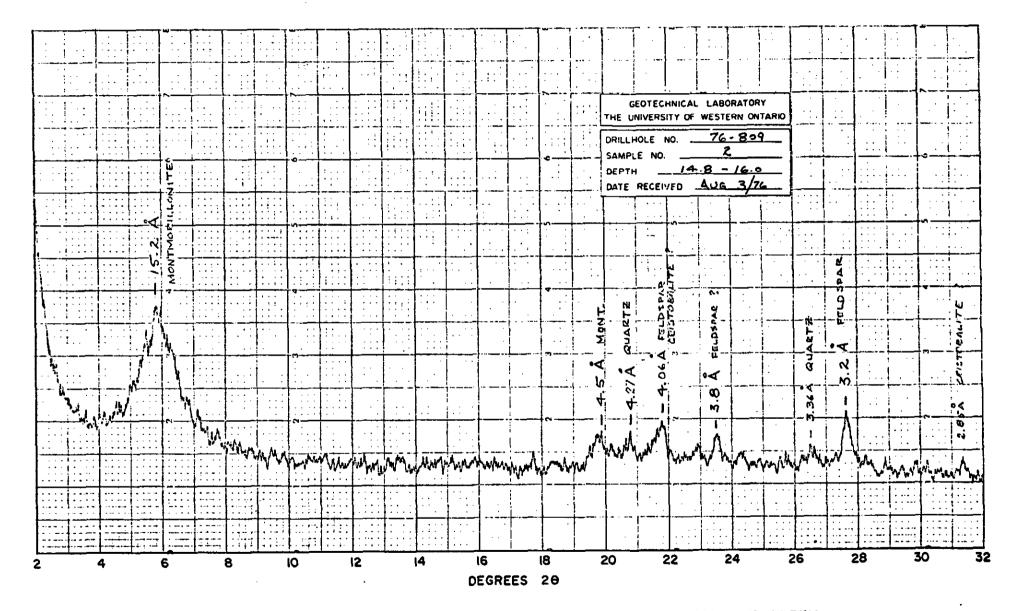


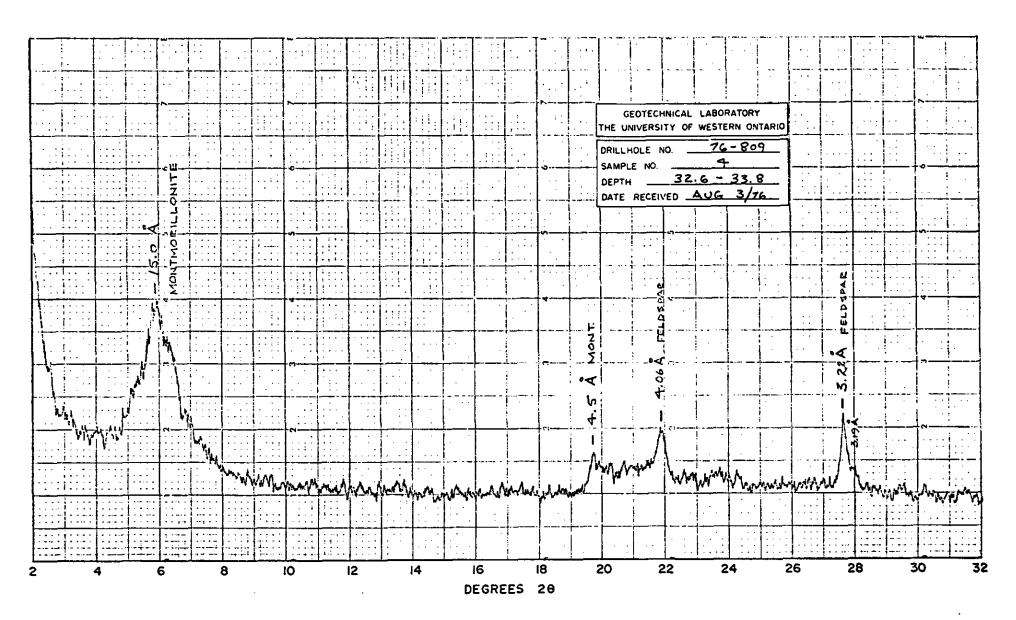




X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.

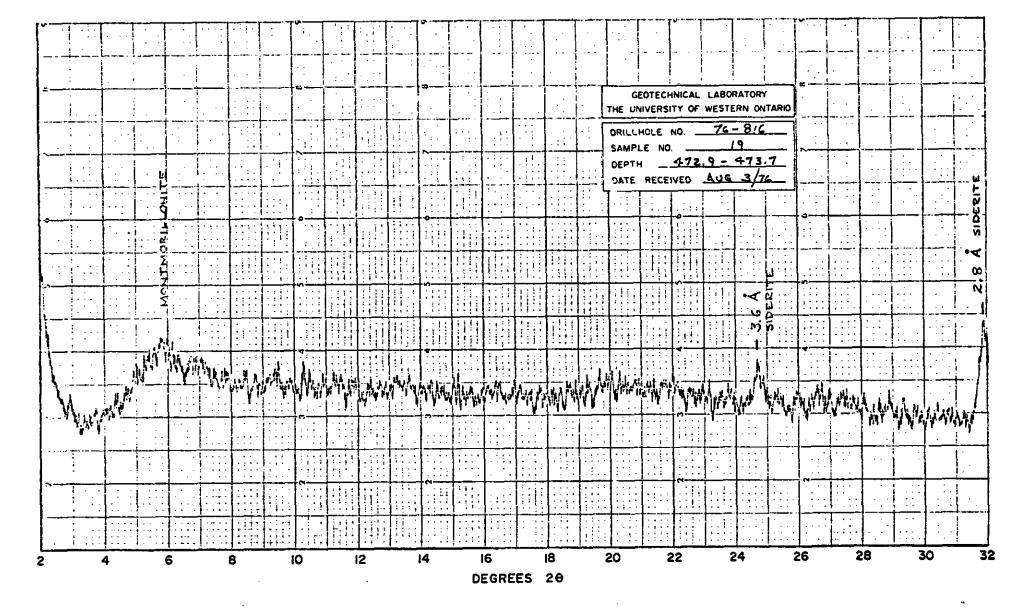




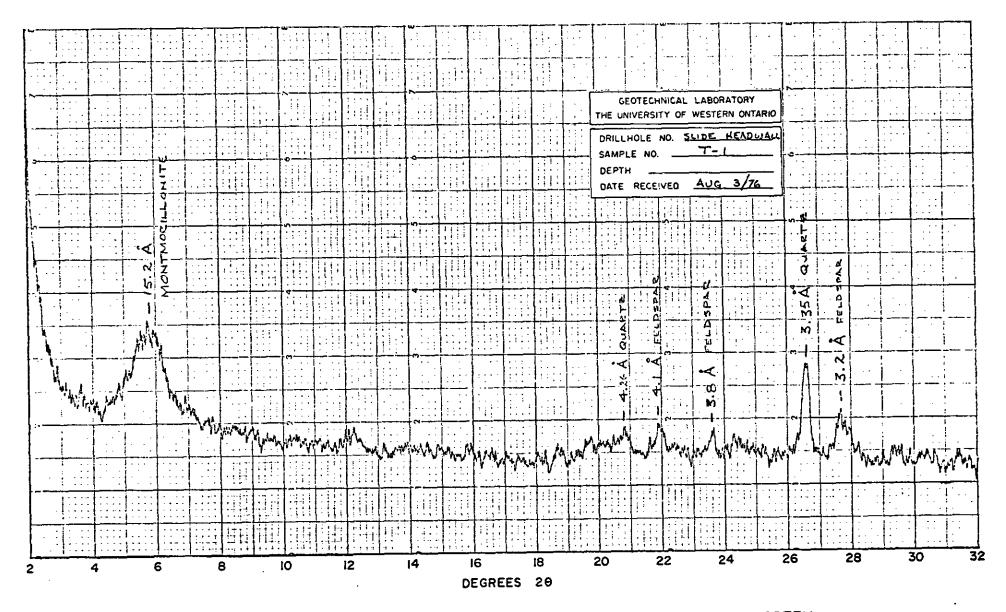


X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



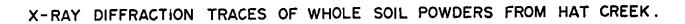


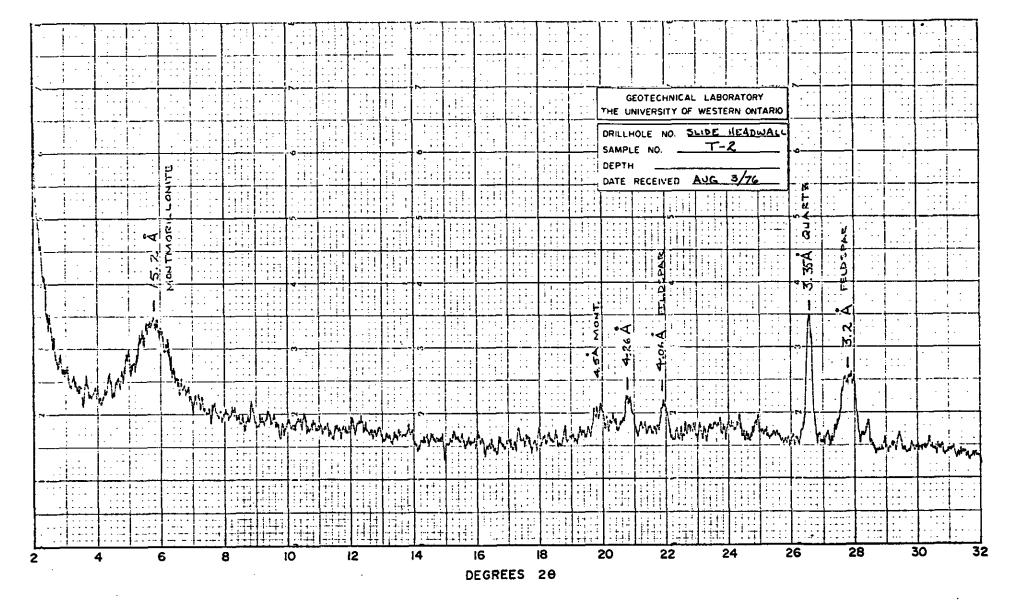
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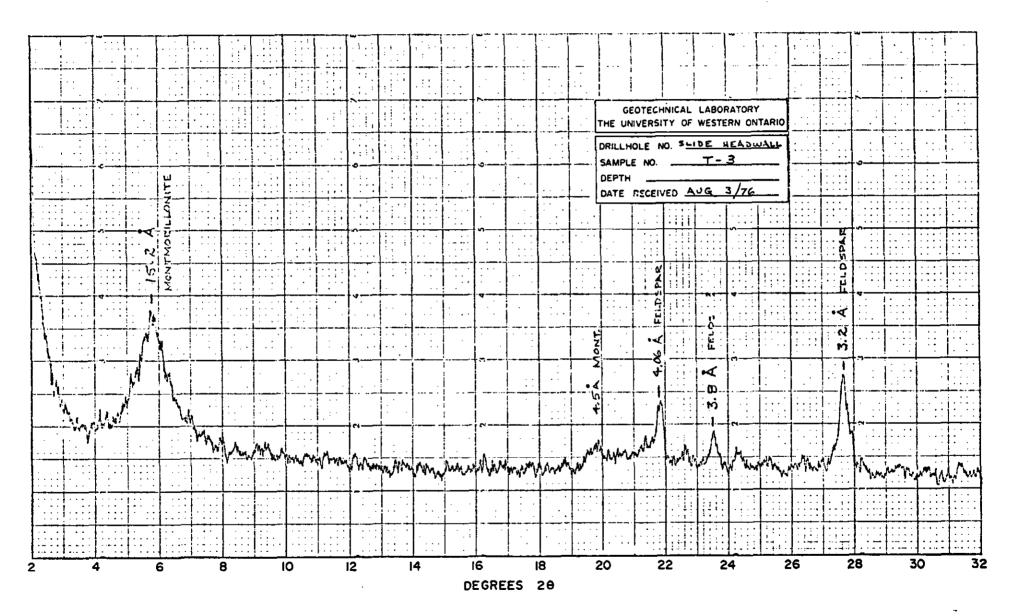
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The University of Western Ontario, London, Canada

Faculty of Engineering Science London, Canada N6A 589

8 October 1976

Mr. G. Rawlings Golder, Brawner & Associates Ltd. 224 West 8th Avenue Vancouver, British Columbia V5Y 1N5

Dear Mr. Rawlings:

Report #5 - Hat Creek Project - Mineralogical Analyses October 8, 1976

Enclosed are the x-ray and carbonate analyses on the ten samples received on September 22, 1976. These samples were generally fairly soft and waxy or soapy looking, indicating abundant contained montmorillonite.

Specific Comments on the Samples

- Carbonate is significant only in sample 74-27-1 from 569.5 feet depth, which contained about 60.4% siderite by Chittick analysis and yielded a large 2.80 Å peak on the x-ray powder pattern.
- 2. The rest of the powder patterns are characterized by large (001) montmorillonite peaks and moderate to minor amounts of feldspar and quartz.
- 3. The x-ray traces of the oriented minus 2 μm fractions indicate montmorillonite with a degree of non-regular basal spacing not noted in previous samples. This is particularly true of the wet preferred orientation traces which show only a high background above 19.6 Å. It is probable that this represents a greater degree of hydration by water and interlayer swelling than was observed for the previous samples.

Since we have not yet received cross sections of the site upon which to base our selection of samples for the glycol retention analyses, we will defer these until after our discussions in Vancouver.

Yours sincerely, R.M. Quigley, P.Eng.

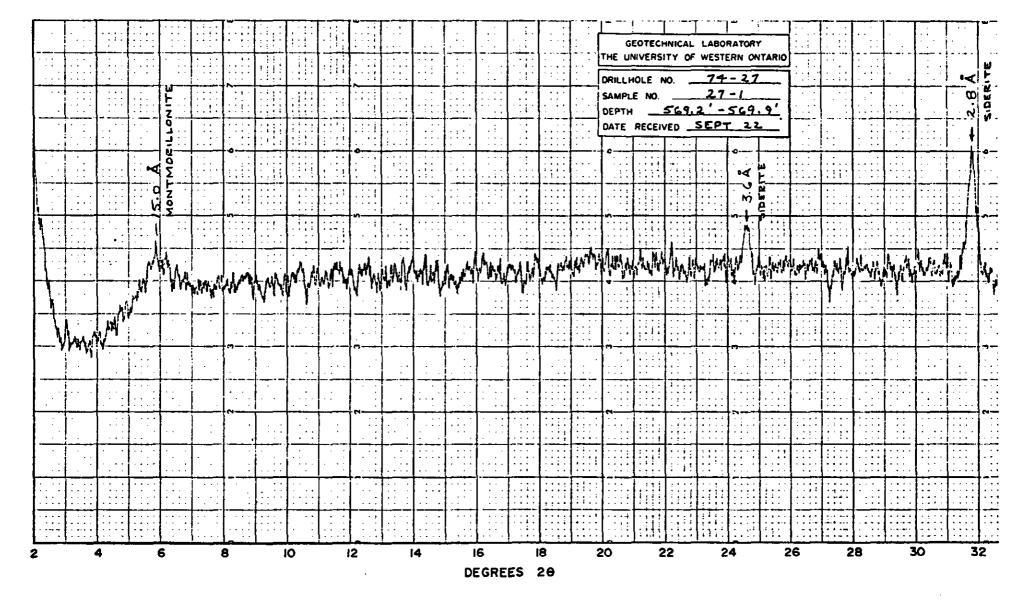
Professor of Geotechnical Engineering

RMQ:em

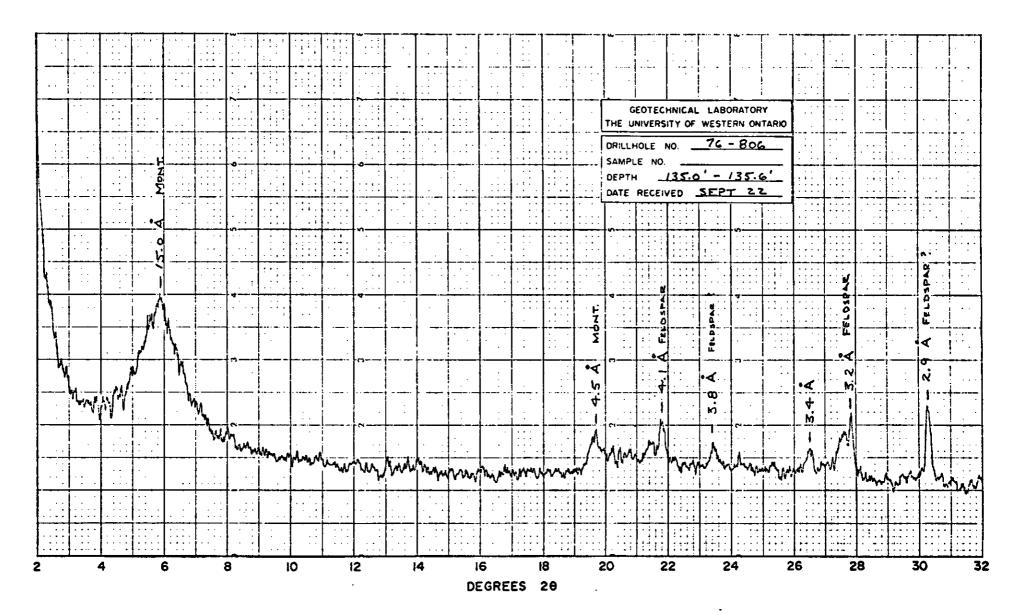
cc: Mr. II.H. Hawson Kamloops, B.C.

HAT CREEK PROJECT LIST OF SAMPLES RECEIVED FROM GOLDER BRAWNER & ASSOCIATES							GEOTECHNICAL LABORATORY THE UNIVERSITY OF WESTERN ONTARIO				
Drill Hole No.	Sample No.	Depth (Feet)	Date Received	Testing Completed							
				Wet P.O.	X-ra ADPO	GP0	Powder	Carbonate (%)	Glycol Retention (mg/g)	Na ⁺ (PPM)	
74-27	27-1	569.2-569.9	SEPT 22	~	5	~	1	60.4			
76-806	<u></u>	135.0-135.6	SEPT 22	~	~	~	~	2.5			
76-806	-	325.0-325.5	SEPT ZZ	~	~	~	~	R.1			
76 - 808	• •••	276.0-276.5	SEPT 22	~	~	~	V	2.7			
76-808		392.0-392.6	SEPT 22	~	>	V	~	1.5		· · · · · · · · · · · · · · · · · · ·	
76-811	5	41.5-42.5	SEPT. ZZ	~	>	~	~	1.3			
76-811	~~~	112.5-113.0	SEPT 22	~	\	~	~	4.5			
76-811	*=	176.5 -177.0	SEPT ZZ	~	く	~	~	2.5			
76-812	43	157.0	SEPT ZZ	~	~	~	~	2.2			
76-818	4	28.3 - 29.6	SEPT 22	~	~	~	~	2.4			
								Re	PORT #5	·	
								<u>R.</u> 7	PORT #5 (1. Dig Of. 8/16	ley	

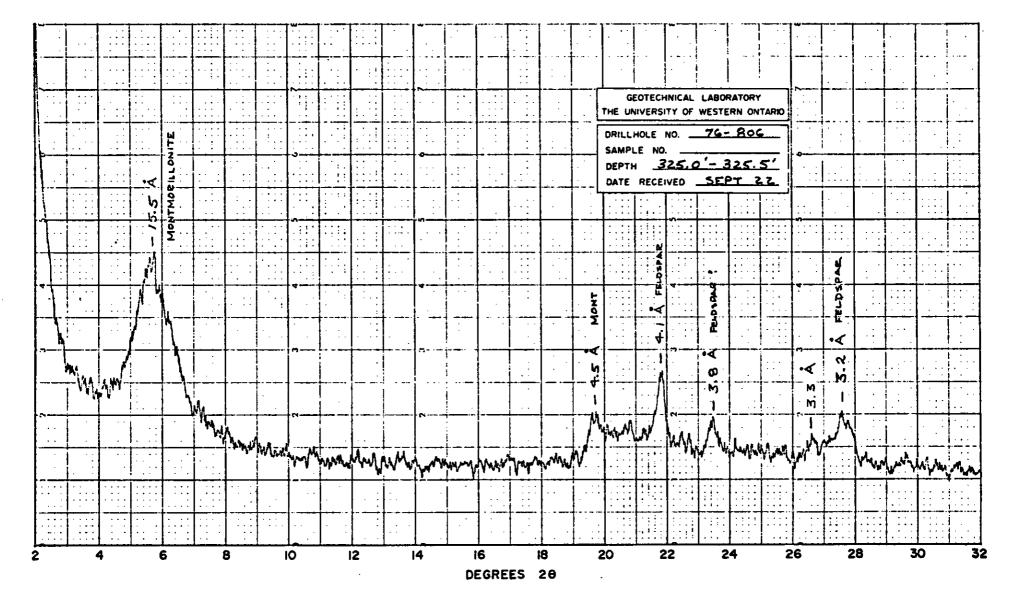


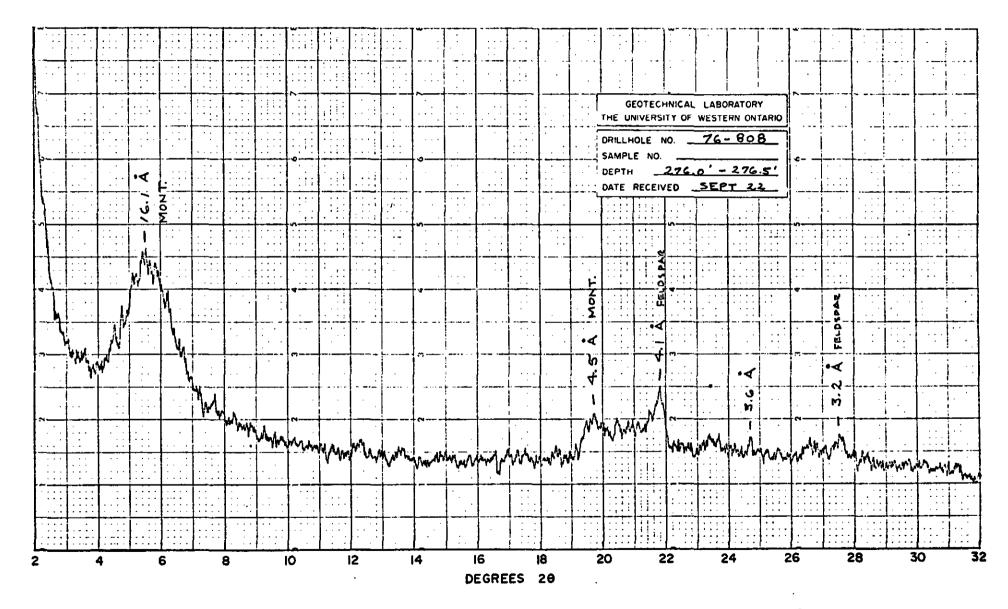


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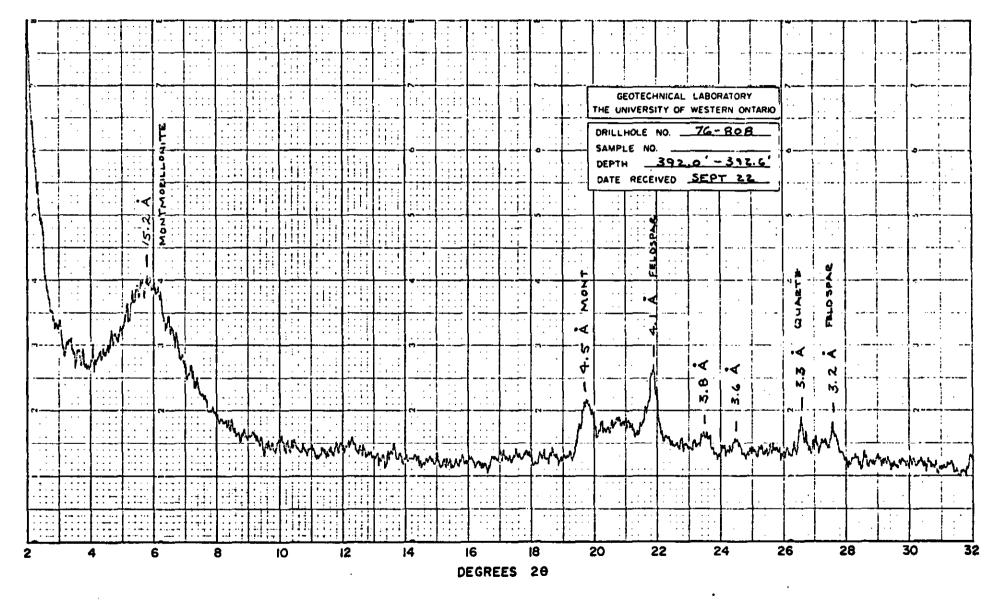


X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



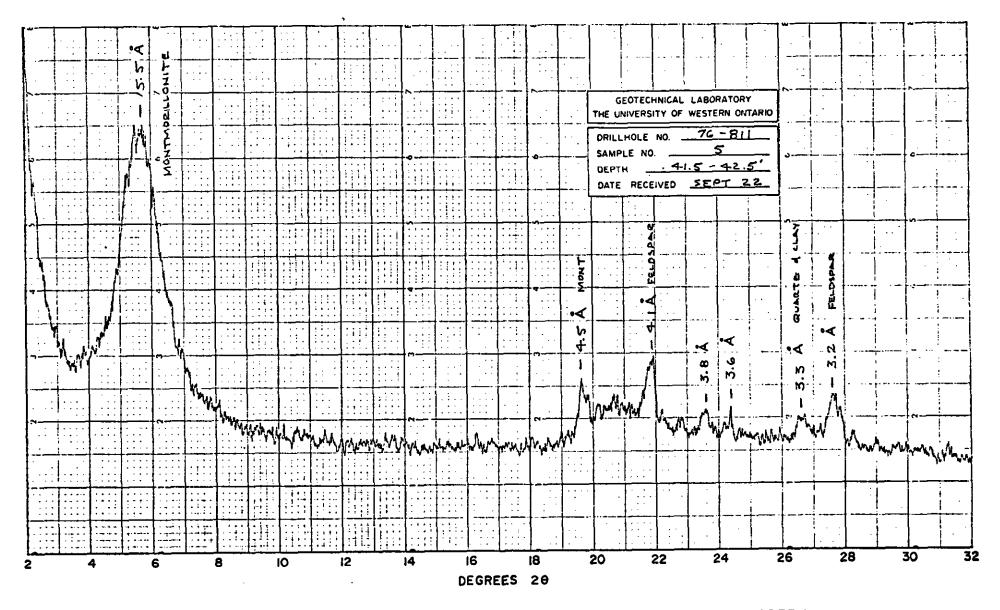


X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



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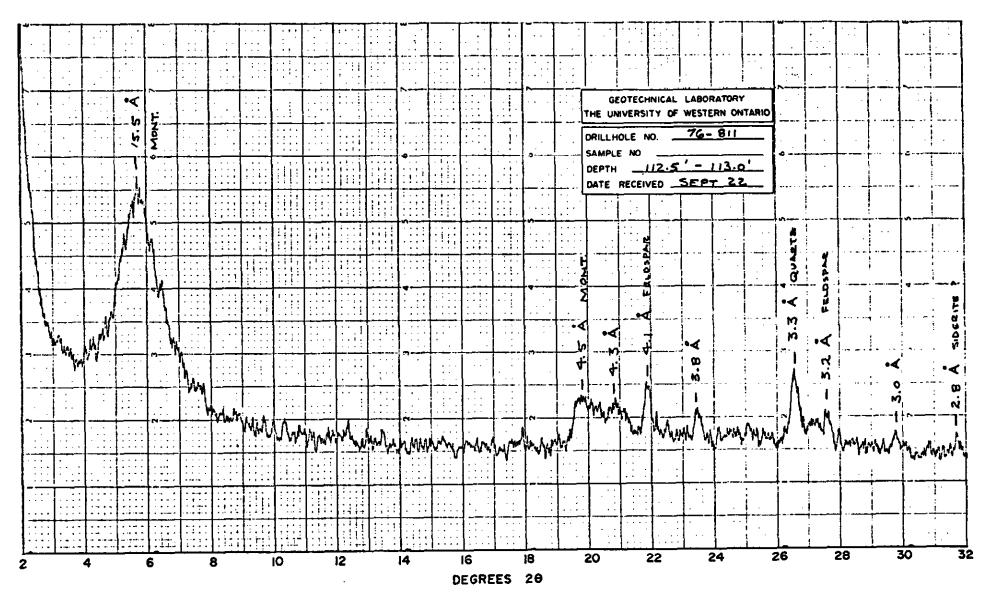
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.

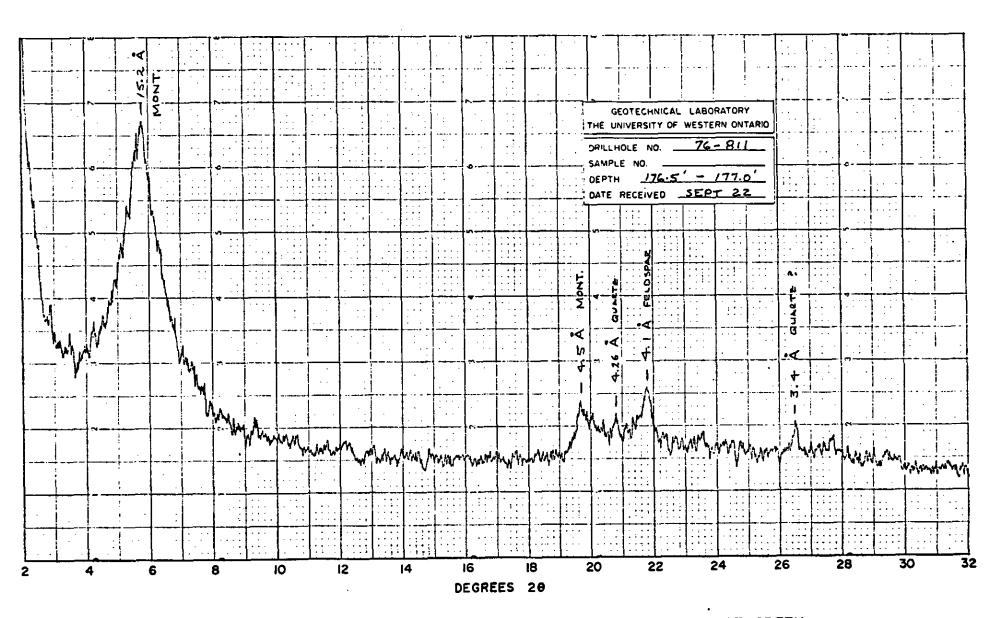


X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.

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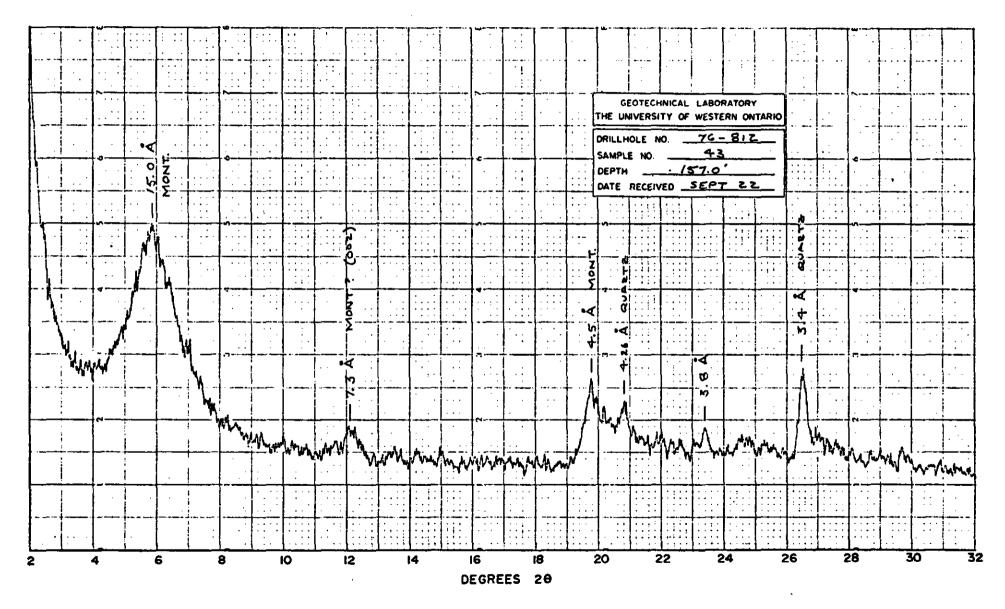


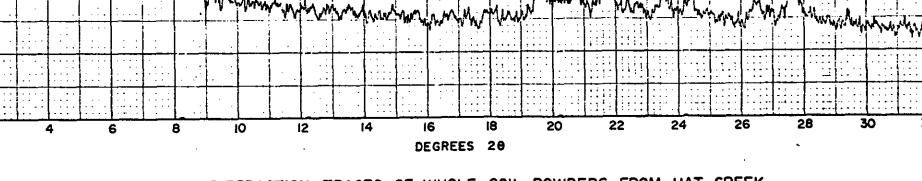


X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.

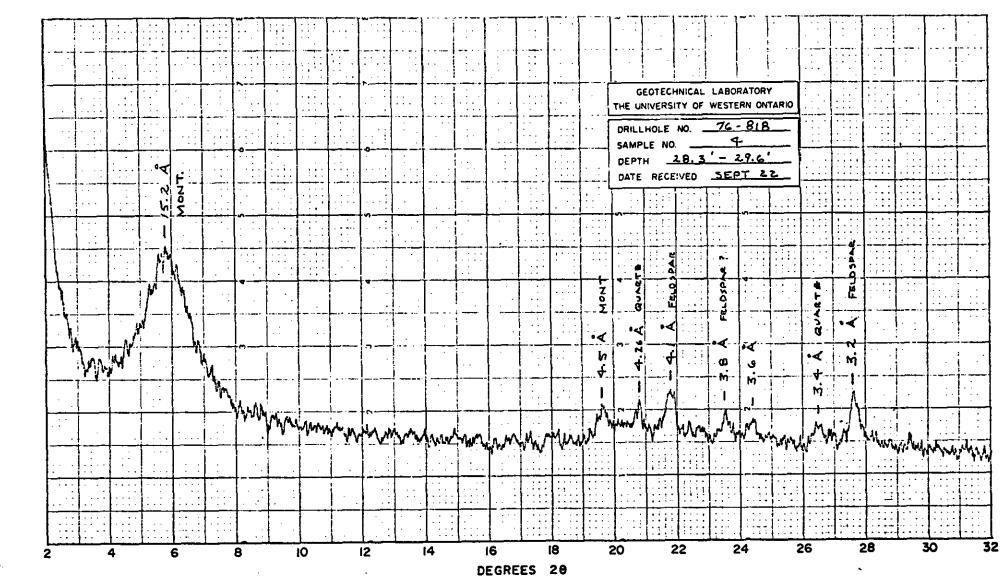
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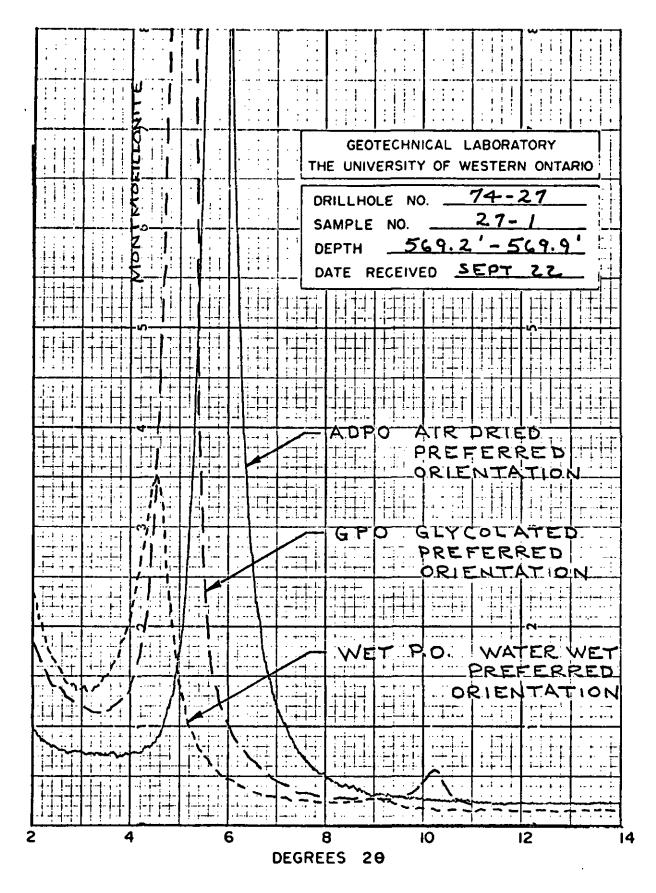
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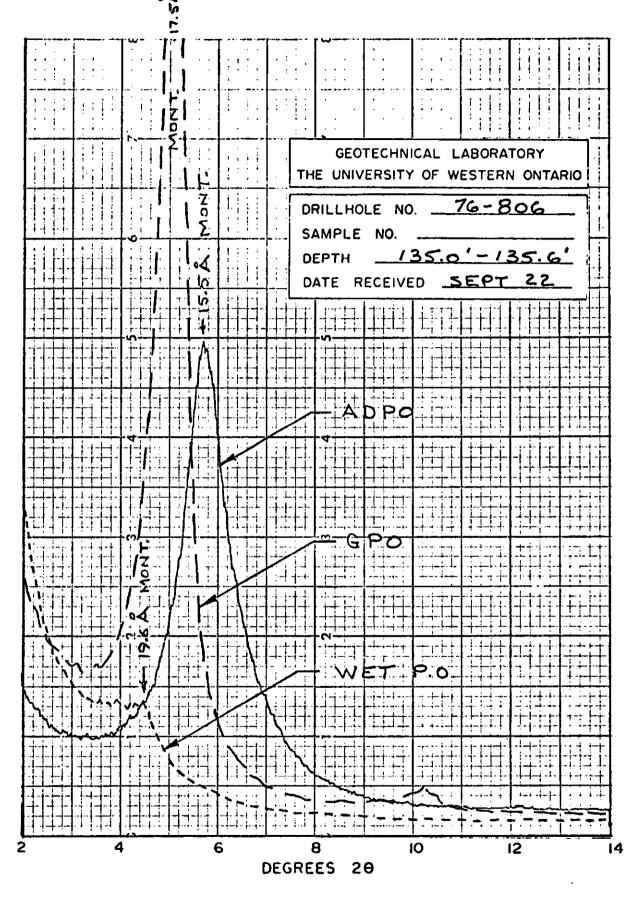


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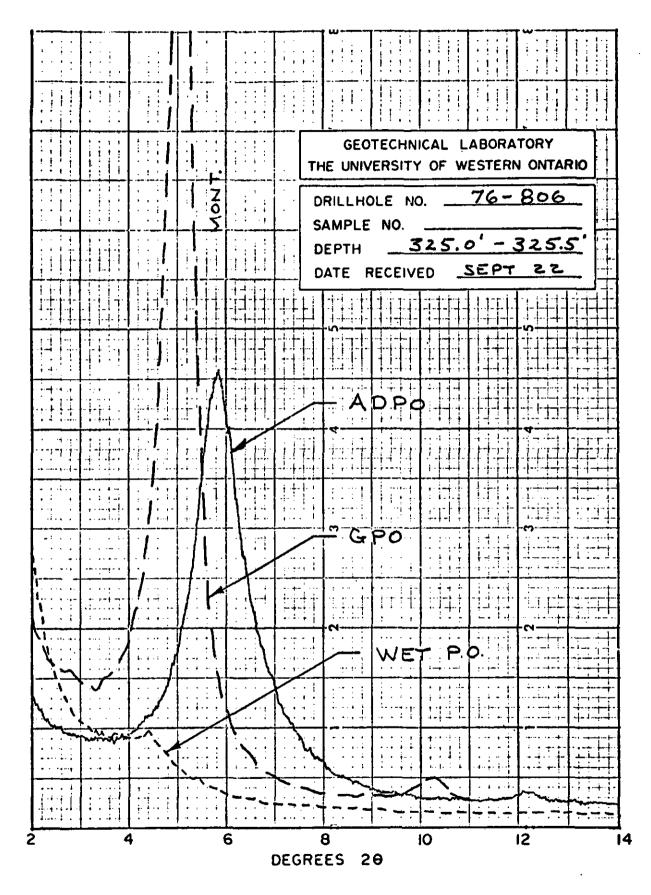




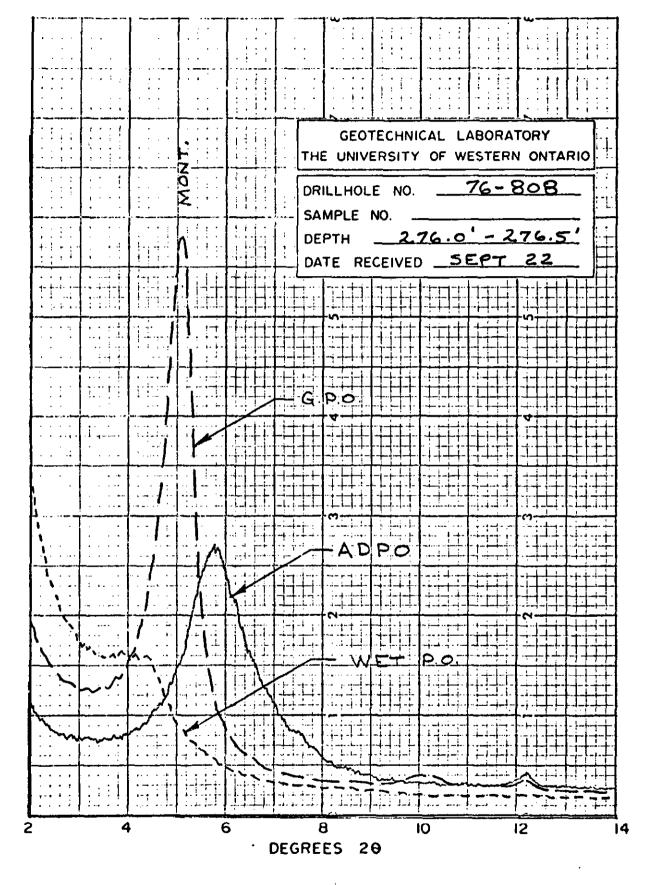
X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



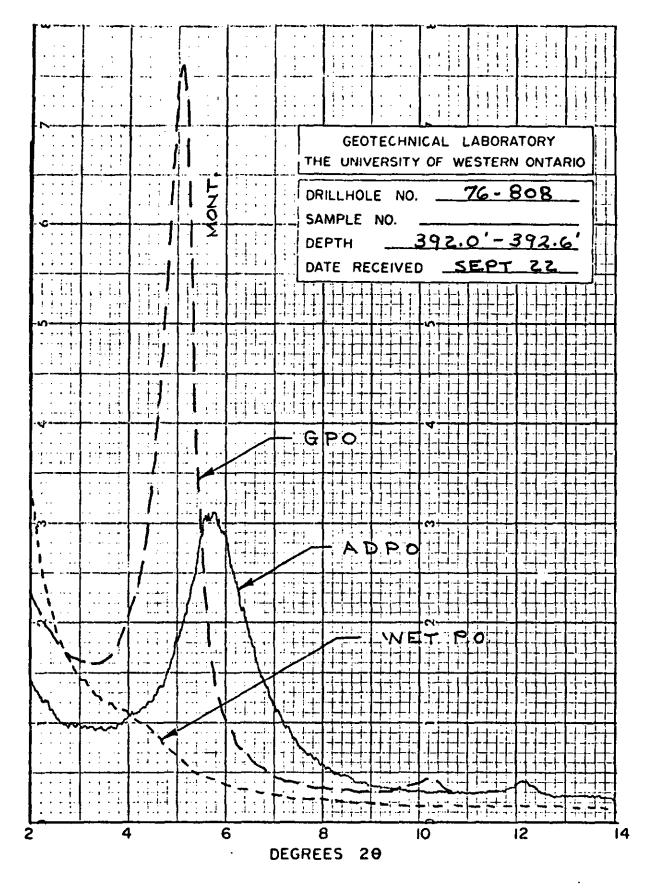




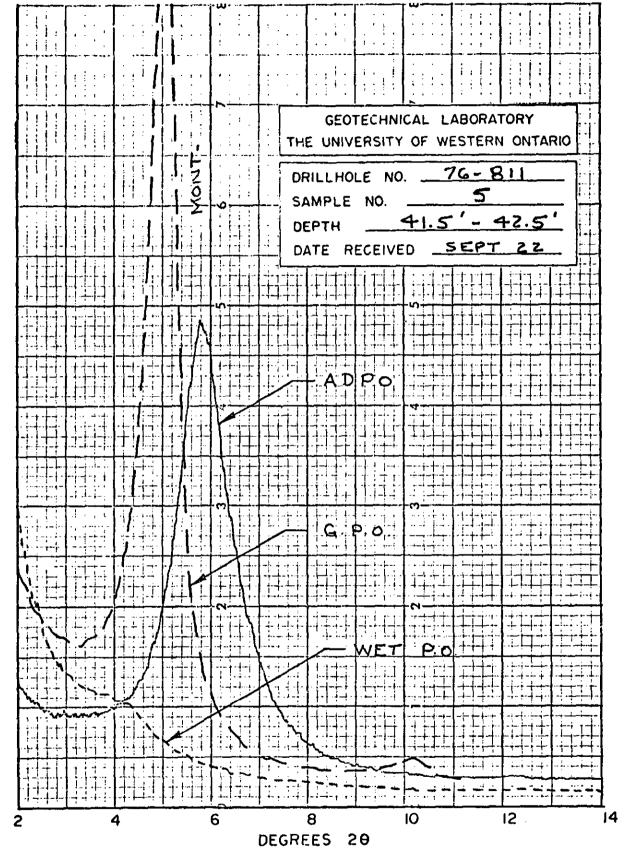
X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK .



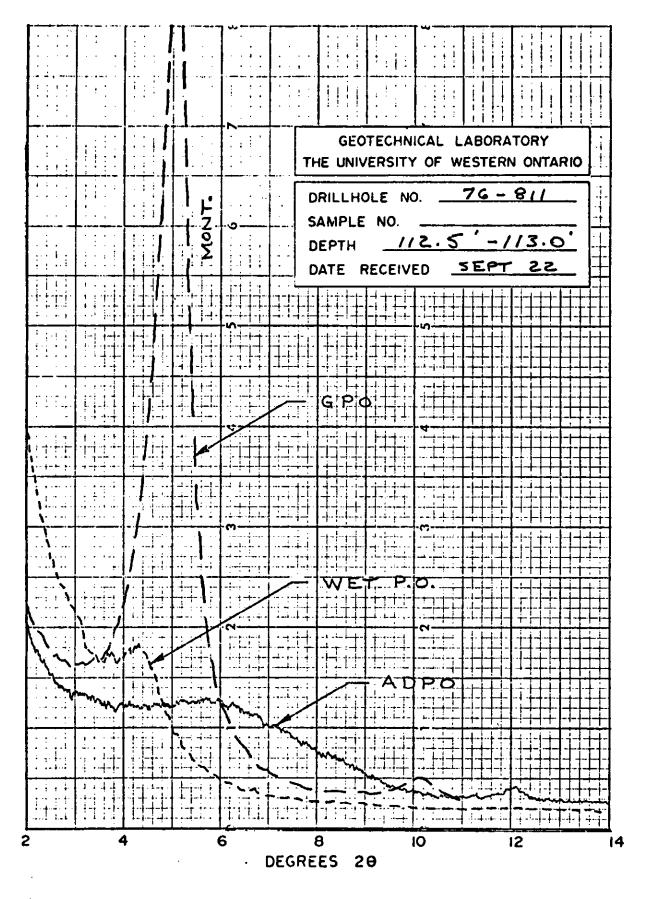
X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK .



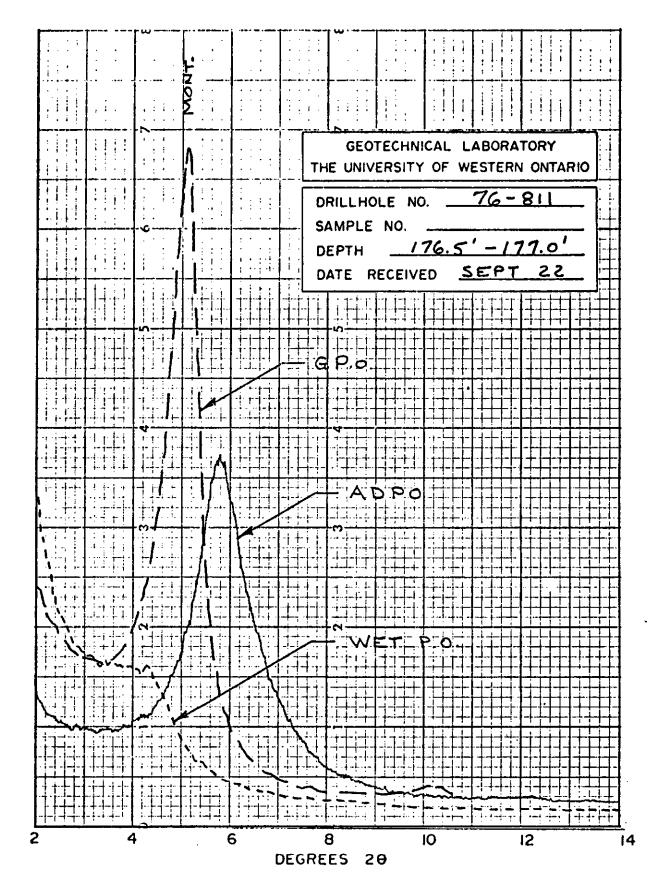
X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



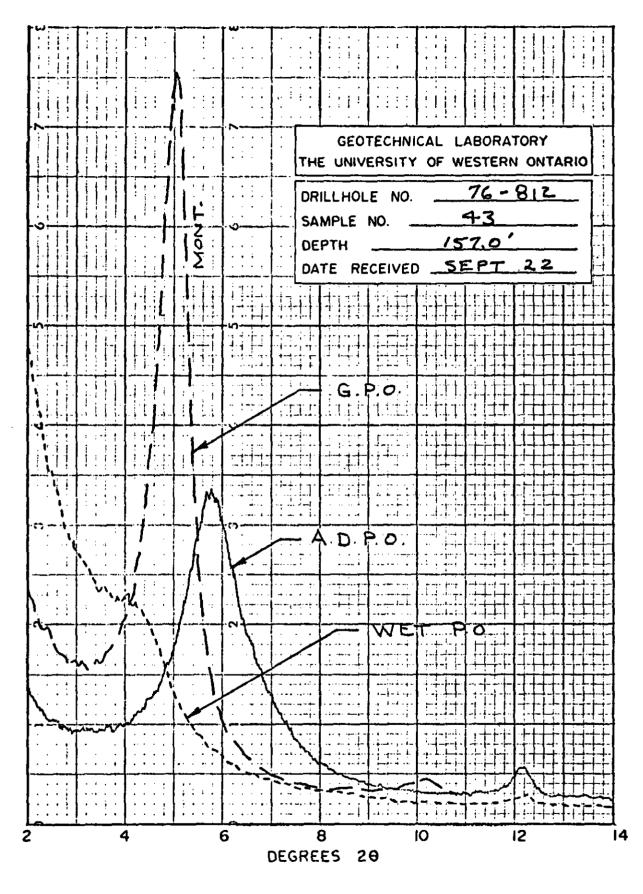




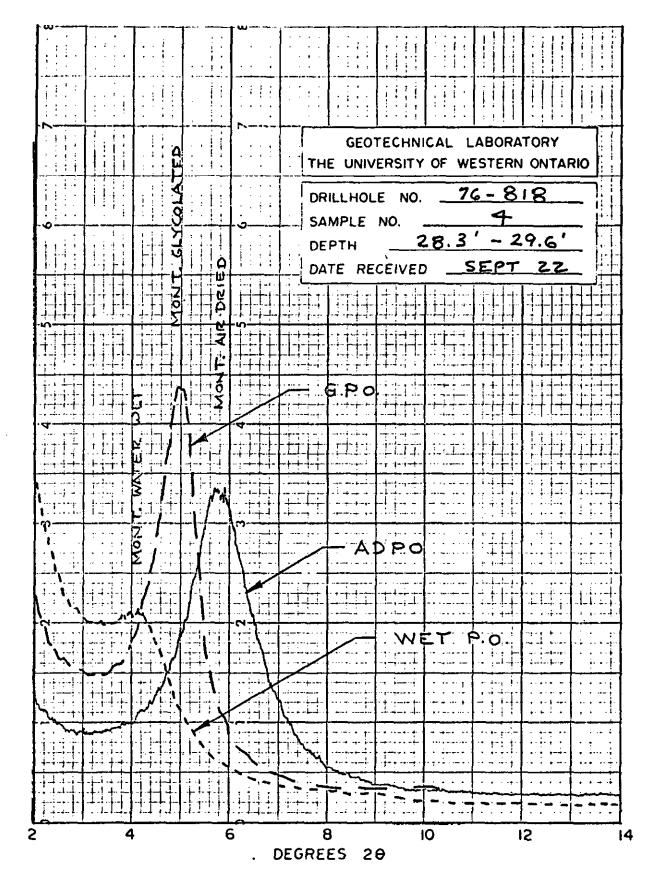
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X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



X-RAY DIFFRACTION TRACES OF 2µ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK

REPORT

to

GOLDER BRAWNER & ASSOCIATES LTD.

VANCOUVER, BRITISH COLUMBIA

on

PRELIMINARY MINERALOGICAL

AND

PHYSICO-CHEMICAL ANALYSES

HAT CREEK PROJECT, BRITISH COLUMBIA

Robert M. Quigley

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PRELIMINARY MINERALOGICAL AND PHYSICO-CHEMICAL ANALYSES, HAT CREEK PROJECT, B.C.

INTRODUCTION

This report presents a final summary of the results of mineralogical and chemical analyses carried out on 43 samples received from Golder Brawner Associates between June 24 and September 22, 1976.

X-ray powder patterns for whole soil samples, x-ray traces for oriented samples of < 2 μ m fractions, and carbonate analyses on all samples were presented in a series of five letter reports between July 26 and October 8, 1976. Only a brief summary of these results is contained in this report.

Recent glycol retention analyses and pore fluid chemistry studies run as a final phase of the project are detailed herein.

PURPOSE AND SCOPE

The purpose of the present study has been to define the clay mineralogy of the sedimentary strata above, below and at the flanks of the coal measures at the Hat Creek Project, B.C. Of special interest were; 1) the relationship of the clay mineralogy to the probable engineering behaviour, and 2) the possible presence of a marker horizon.

A total of 43 samples were received from Golder Brawner & Associates Ltd. from a variety of locations defined stratigraphically on drawing V76345-3 (Golder Assoc.).

The scope of the testing has been limited to preliminary identification of the soil and rock components by x-ray diffraction and carbonate analyses. This has been supplemented by selected glycol retention analyses on 16 samples; 8 above the coal measures and 8 below. Salinity and cation analyses have been run on 8 samples; 4 above the coal measures and 4 below.

On the basis of the glycol retentions, a rough estimate can be made of the amount of montmorillonite present.

X-RAY DIFFRACTION SUMMARY

Powder Patterns

All powdered samples except those with more than about 35% carbonate yielded strong to very strong 15.2 Å montmorillonite peaks as shown in Figures 1 to 4 which contain typical powder patterns. The carbonate present appears to be an iron rich variety similar to siderite as identified on the x-ray traces. Other constituents in the samples included moderate to trace amounts of feldspar and quartz with an occasional suggestion of cristobalite.

Summaries of the soil constituents present in each sample as observed by x-ray powder diffraction are given in Tables I and II. For clarity, the carbonate contents by gasometric analysis are also given.

From an engineering point of view, the powder patterns clearly show montmorillonite to be the dominant mineral present in all samples except the indurated carbonates. Even in these samples, montmorillonite peaks were generally easily discernible on the powder patterns.

X-Ray Diffraction Traces of Oriented < 2 µm Fraction

Typical x-ray diffraction traces of oriented specimens of the < 2 μ m fraction are given in Figures 5 to 8 inclusive. All traces are essentially similar showing strong 15.5 Å montmorillonite peaks in the air dried preferred orientation state and strong 17.0 Å peaks when glycolated. Some variation occurs in the traces for the water-wet samples, the intensity, breadth and position of the peaks varying from sample to sample. This reflects variable hydration of the clay mineral sheets and may be related in part to the quality of the distilled water used to disperse the samples as well as variable swelling characteristics of the clays.

From an engineering point of view, this tendency towards extra swell in distilled water suggests that the clays may exhibit unfavourable swelling and strength characteristics on exposure to leaching by fresh rain waters.

CHEMICAL TESTS

Chemical tests on the samples are summarized in Table III. The tests include carbonate analyses by Chittick gasometric methods, glycol retentions, pore fluid salinity and cation analyses.

Carbonate Analyses

Carbonate contents of the montmorillonite rich clays and clay-stones are generally of the order of 1 to 2%. Since the test procedure involves addition of HCL to a dried powdered sample, other gases than CO_2 from soil carbonates may occasionally be evolved. Test results of 1% carbonate, therefore, may reflect complete absence of carbonate in some of the samples.

The reaction time of the contained carbonates with HCL was delayed like dolomite, reflecting the lesser solubility of the siderite present in the rocks compared to calcite.

The x-ray traces clearly showed siderite to be the dominant carbonate. The presence of the siderite in the volcanic rich stratigraphic section would seem to reflect iron rich waters signifying volcanic activity synonymous with carbonate deposition.

Well indurated carbonate samples normally have siderite contents of about 30 to 35% with some samples containing as much as 68% carbonate. If the samples supplied to our

-4

laboratory are fully representative of the stratigraphic section, it is very apparent from Table III that the carbonate strata seem restricted to the section above the coal measures.

Glycol Retentions

The sixteen values of glycol retention are presented in Table III. Below the coal measures, values ranging from 129 to 264 were obtained on the < 2 μ m fraction of six samples. The two high values of 243 and 264 mg/g are as high as is normally obtained on pure montmorillonite. Tests were run on two whole-soil samples (in brackets in Table III) and the results are very high (186 and 202 mg/g) indicating the great abundance of montmorillonite in the samples.

Above the coal measures, the glycol retentions varied from 136 to 265 mg/g on the < 2 μ m fractions. These values are comparable in spread to those obtained on the samples from below the coal measures.

Again, the four values above 200 mg/g are indicative of a clay fraction consisting of pure montmorillonite.

Salinity and Cation Analyses

Sample preparation for pore fluid analysis involved a single addition of distilled water to air dried soil in the ratio of 5:1 by weight. The salinities were measured by conductivity meter and are referred to NaCl standard. All

values were calculated assuming an in situ moisture content of 35% which is close to the actual average value.

Extreme difficulty was experienced in obtaining a clear liquid since the montmorillonite tended to form a very stable gel, even in dilute suspension. Eventually, all samples were split into small fractions and successfully clarified by high speed centrifugation.

The pore fluid cation analyses were run on the clear, slightly brown supernatant using a Pye Unicam atomic absorption spectrophotometer. The results only represent a guide to the pore fluid composition, since pore fluid extraction by high pressure squeezing would be required to obtain more precise values. The values of the salinity and cation measurements are presented in Table III.

The salinity values on the clay-stones tested are close to 4 g/ ℓ except for sample 74-28-1 (480 ft) which has a somewhat higher value of 6.5 g/ ℓ . The lowest salinity value of 1.9 g/ ℓ was obtained on sample 803-28 (135 ft) which is understood to be a glacio-lacustrine sediment. The lower salinity is, therefore, not surprising.

The cation analyses showed Na⁺ (sodium) to be the dominant constituent of the pore fluid with values ranging from 1.15 to 2.13 g/l for the montmorillonite clay-stones. Magnesium was the next most abundant cation, ranging from 0.03 to 0.78 g/l. Iron was present in three brown coloured liquid extracts in amounts of 0.12 to 0.74 g/l and absent in

the rest of the extracts. Calcium was a negligible component of the pore fluids as extracted by the distilled water wash.

Chloride Anion Measurements

Chloride anion measurements were carried out on four selected extracts and yielded concentrations varying from 0.03 to 1.93 g/l as shown in Table III. Although the data is slim, it is speculated that high sodium values correlate with high chlorinity values in the Hat Creek deposits.

pH Measurements

The soil samples prepared for salinity analyses were also checked for pH yielding the results in Table III. The measured values range from 8.6 to 9.3 indicating a significantly alkaline environment.

DISCUSSION

The x-ray powder diffraction and carbonate data indicate that the geologic materials within the stratigraphic sequence at Hat Creek consist of:

- Essentially pure montmorillonite with trace amounts of quartz and feldspar
- Montmorillonite with moderate amounts of quartz and feldspar

- Montmorillonite with moderate amounts of siderite
- Carbonates (siderite) with moderate amounts of montmorillonite.

It appears significant that in Table I, all of the siderite rich samples occur above the coal measures.

The x-ray traces for the oriented specimens feature very strong (001) montmorillonite peaks with little or no evidence of either 10 Å illite or 7 Å kaolinite and chlorite. The very high glycol retentions of 129 to 264 reflect the abundance of montmorillonite within all < 2 μ m fractions tested, including the indurated carbonates.

If pure montmorillonite is assigned its usual glycol retention of 250 mg/g, then the two whole soil samples tested (186 and 202 mg/g) contain montmorillonite contents of about 75 and 81% respectively.

The cations present in the pore fluid extracts consisted dominantly of sodium (1.2 to 2.1 g/l) with a somewhat lower value of 0.71 in the glacio-lacustrine sample 803-28 (135 ft). Magnesium was the next most abundant species with 0.03 to 0.06 g/l in the pore fluid above the coal measures and 0.14 to 0.78 g/l in the pore fluid of samples from below the coal measures. Calcium was essentially absent from the extracts, however, HCl treatment of a couple of samples suggested that some Ca⁺⁺ may be adsorbed on the clays. Iron was detected in only the three most strongly coloured extracts.

Since magnesium (Mg^{++}) is a divalent cation it preferentially adsorbs onto the clay minerals in comparison to Na⁺, a univalent cation. Most of the cations adsorbed on the soil montmorillonites will, therefore, probably be Mg^{++} .

The total cation composition of the pore fluid extracts compares reasonably favourably with the measured salinity values. For example, the pore fluid extract from sample #74-28-1 (480 ft) has the following measured chemical constituents:

Sa #74-28-1 (480')

Salinity	=	6.46	g/l		
Sodium	=	2.07	g/L		
Magnesium	=	0.03	g/l		
Calcium	Ħ	0.04	g/l		
Σ cations	#	2.14	g/L		
Chloride	=	1.93	g/L		
Σ cations	+ c)	hlorid	le =	4.07	g/l

Other anionic constituents such as bicarbonates and sulphates probably comprise the remainder of the soluble salts. Indeed, the very high pH values suggest the presence of soluble sulphates and it is recommended that some sulphate analyses be carried out during the next phase of the investigations.

Sodium rich montmorillonites have much higher liquid limits and activities than magnesium and calcium rich

montmorillonites. They also have correspondingly lower residual friction angles. The montmorillonites above the coal measures contain significantly less divalent cations and more Na⁺⁺ cations in the pore fluid extracts, suggesting that they may be consistently more active and difficult to manage when exposed to atmospheric weathering than those below the coal measures.

Should strata be encountered that have significantly higher activities than the norm for surrounding strata, it is recommended that they receive special chemical testing to establish the pore fluid chemistry and adsorbed cation regime.

TABLE I.COMPOSITION FROM X-RAY POWDER PATTERNS; BOREHOLE SAMPLESA = Abund., Mo = Mod., Mi = Minor, T = Trace

Drill Hole Number Depth (ft) (Whole soil) (t) CONSTITUENTS FROM X-RAY POWDER ANALYSES Above coal measures: 803 28 135 1.7 Mont-A, Feldspar-A, Quartz-A 803 28 135 1.7 Mont-A, Feldspar-A, Quartz-A - 29 317 32.4 Mont-A, Feldspar-A, Quartz-T - - 595 17.1 Mont-A, Feldspar-A, Quartz-T - - 595 17.1 Mont-A, Siderite-A, Quartz-T - - 595 17.1 Mont-A, Siderite-A, Quartz-T - 9 448 51.2 Mont-A, Siderite-A, Quartz-T - 12 482.5 3.5 Mont-A, Siderite-A, Quartz-T - 18 542 34.3 Mont-A, Siderite-A, Qtz-T - 20 562 9.3 Mont-A, Siderite-M, Qtz-T - 21 569.5 35.5 Mont-7, Siderite-A, Qtz-T - 22 583 67.6 Mont-7, Siderite-A, Qtz-T 74-27 1 5	
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807 12 23 2.4 Mont-A, Felds-Mi, Qtz-Mi	
" 14 159 1.7 Mont-A, Qtz-Mo	
808 40 12 3.0 Mont-A, Felds-Mo, Qtz-T	
" 10 32 1.7 Mont-A, Felds-Mo, Qtz-Mi	
" - 276 2.7 Mont-A, Felds-M1	
" - 392 1.5 Mont-A, Felds-Mi, Qtz-Mi	
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* 4 33 2.7 Mont-A, Felds-Mo	
811 5 42 1.3 Mont-A, Felds-Mo, Qtz-Mi	
" - 113 4.5 Mont-A, Qtz-Mo, Felds-Mi, Sideri	te-Mi
" - 177 2.5 Mont-A, Qtz-Mi, Felds-Mi	
812 43 157 2.2 Mont-A, Qtz-Mo	
818 4 29 2.4 Mont-A, Felds-Mo, Qtz-Mi	

TABLE II. COMPOSITION; MUD BOIL AND SLIDE HEADWALL SAMPLES

SAMPLE		CARBONATES (Whole soil) (%)	CONSTITUENTS FROM X-RAY POWDER ANALYSES			
MUD BOIL		4.0	Mont-abund. Quartz-mod. Felds-abund. Dolomite-minor			
SLIDE HEADWALL	Tl	2.8	Mont-abund., Quartz-abund., Feldspar-moderate			
	T2	3.8	Mont-abund., Quartz-abund., Feldspar-abund.			
H	Т3	4.2	Mont-abund., Feldspar-abund., Quartz-trace			

TABLE	ш.	CHEMICAL	TEST	RESULTS;	BOREHOLE	SAMPLES
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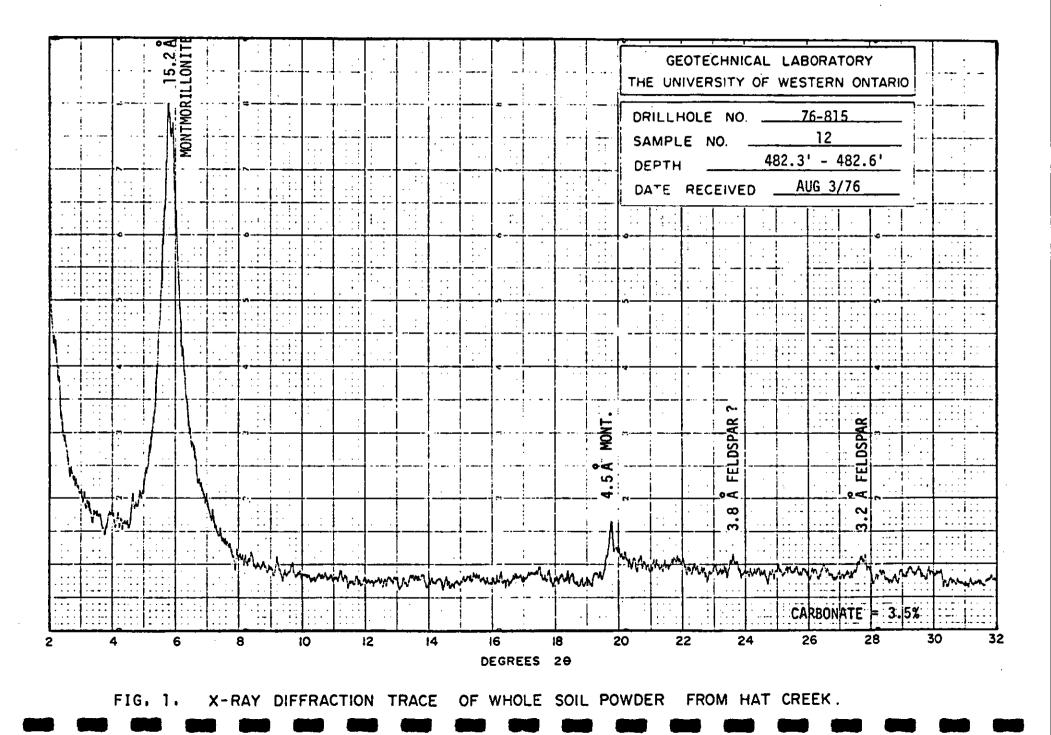
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Drill	SAMPLE		CARBONATE (Whole soil)	GLYCOL RETENTION	SALINITY	Na	Ca	Mg	Fe	CŁ	рH
Hole	Number	Depth (ft)	x	on < 2 µm mg/g	g/L	g/t	g/£	g/2	g/£	g/£	
Above	coal measu	res:							. '		
803	28	135	1.7	207	1.9	0.71	0.02	0.04	-	-	8.7
Ħ	29	317	32.4	142							
H	-	595	17.1	213	1		[]				[
815	7	431	34.5								
N	· 9	448	51.2								
M	12	482.5	3.5	233							
	14	506	7.5		1	,					
	18	542	34.3								
	20	562	9. <u>3</u>	136	3.4	1.15	0	0.06	-	-	8.
	22	583	67.6								
H	29	669.5	35.5						,		
816	19	473	30.7								
74-27	1	569.5	60.4							•	
74-28	1	480	2.0		6.46	2.07	0.04	0.03	0	1.93	8.
n	2	644	6.4	167							
n	3	738	7.5	265							1
*	4	763	31.6								
	5	767.5	26.5			· ·					
H	6	179.5	44.3								
	7	451	12.9								
*	8	537	· 2.7	190	3.9	1.24	0	0.05	0	0.96	8.
"	9	588	1.5	<u>.</u>							
Below	coal measu	res:									ļ
804	14	51	1.7								
805	16 Green Black	62	5.3 1.1								
806	7	18	1.3							2	
N	-	135	2.5			1.96	_	0.78	-	? 0.03	-
M	-	325	2.1								
807	12	23	2.4								
H	14	159	1.7				ł	• •			
808	40	12	3.0				r I				
м	10	32	1.7								
м	-	276	2.7	185	4.6	2.13	0	0.49	0.74	0.24	9.
н	. -	392	1.5	131				·			
809	2	15	2.6								ţ.
¥	4	33	2.7						·		
811	5	42	1.3	(186) 180	-						
н	-	113	4.5	129							1
	-	177	2.5	(202) 243	4.2	2.10	0	0.63	0.62	-	9.
812	43	157	2.2]
818	4	29	2.4	264	3.7	1.59	0	0.14	0.12	-	9.

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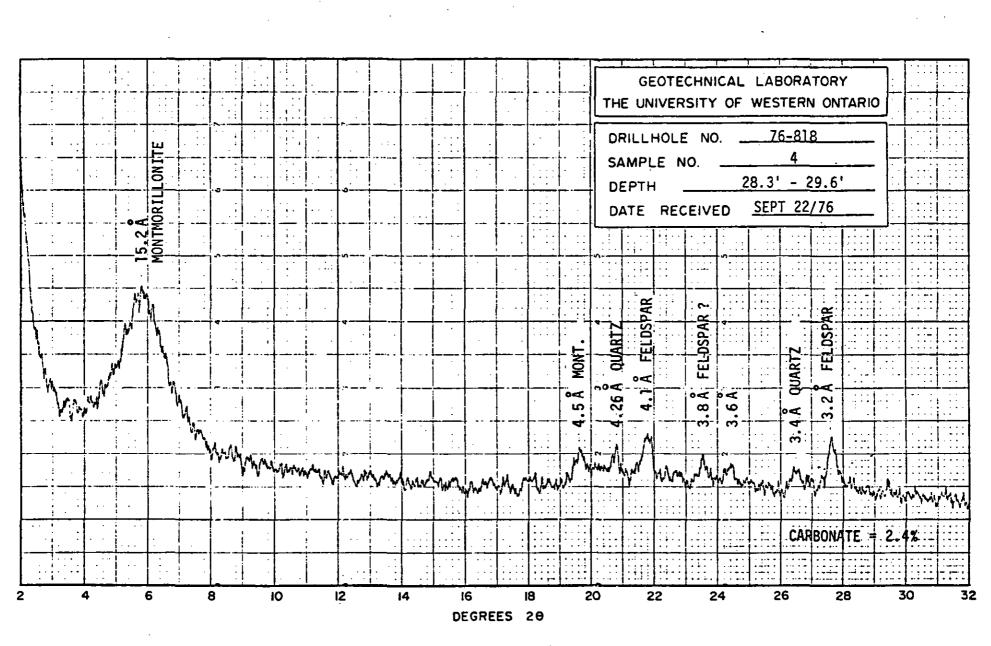


FIG. 2. X-RAY DIFFRACTION TRACE OF WHOLE SOIL POWDER FROM HAT CREEK.

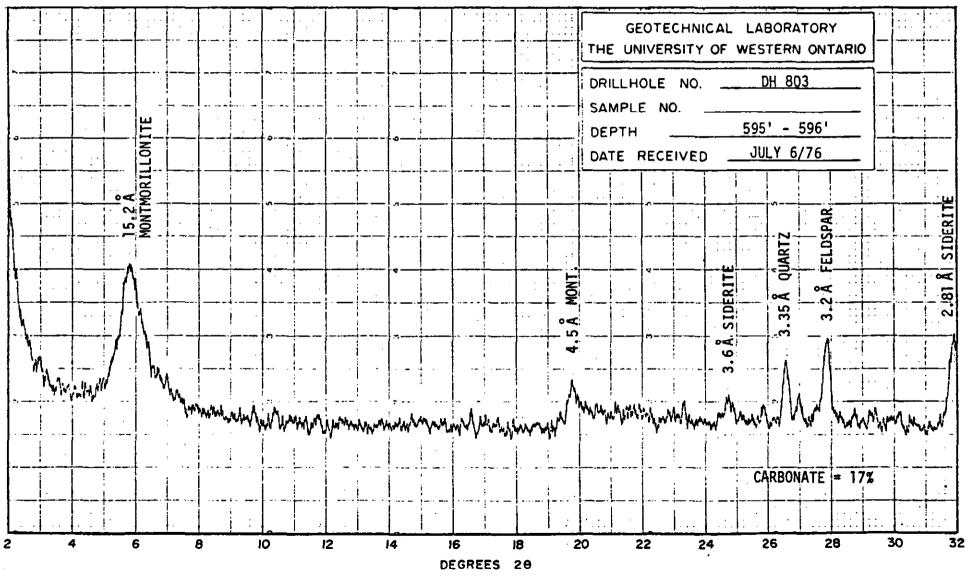
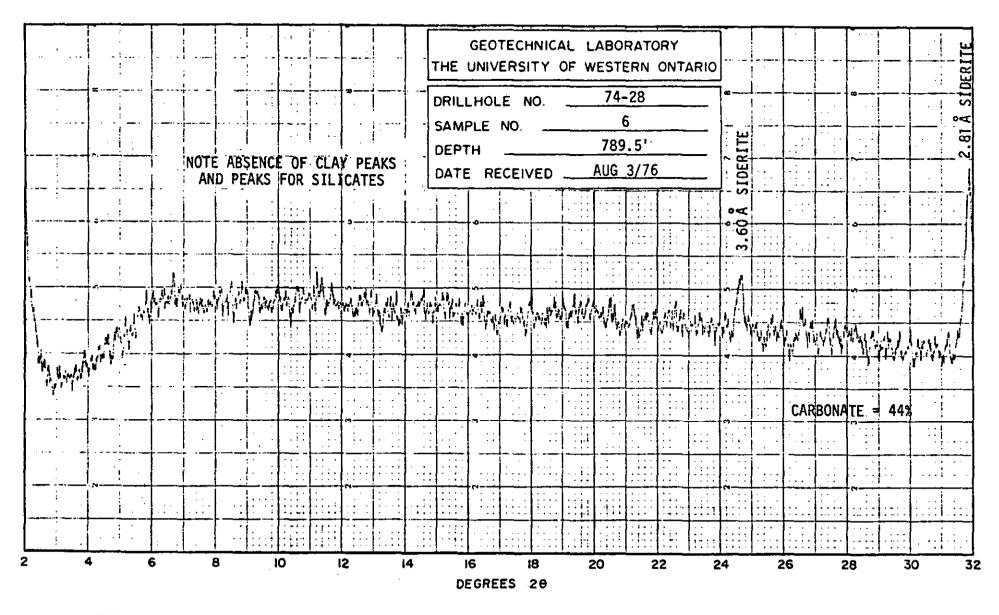
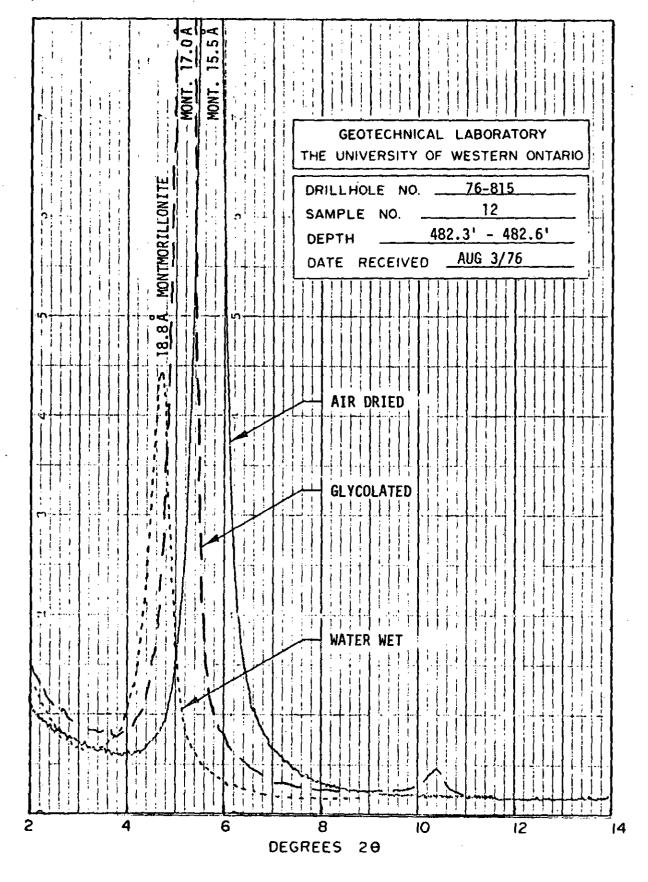


FIG. 3. X-RAY DIFFRACTION TRACE OF WHOLE SOIL POWDER FROM HAT CREEK.









FIG, 5,

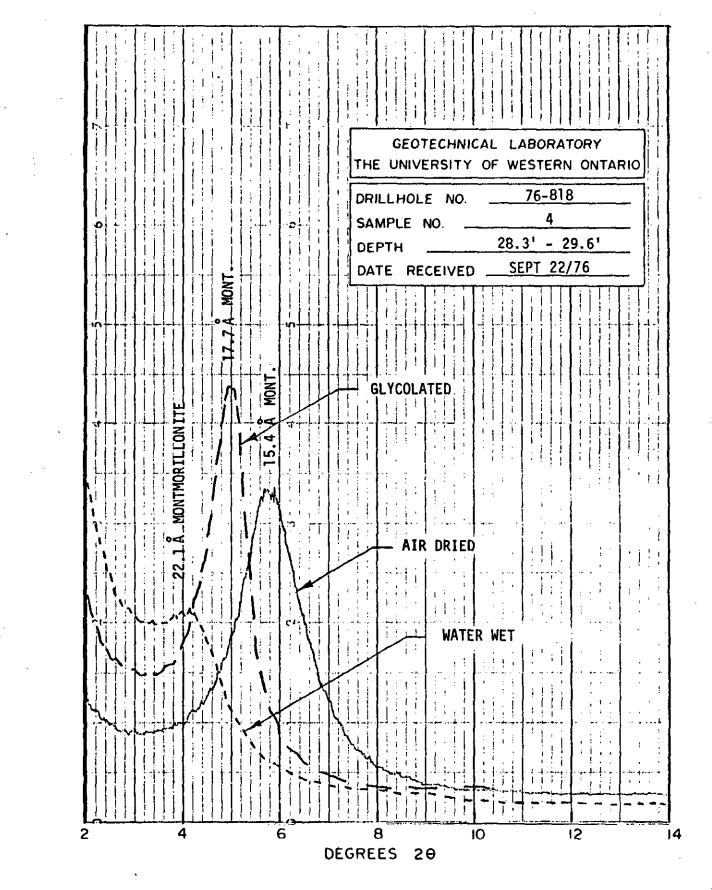
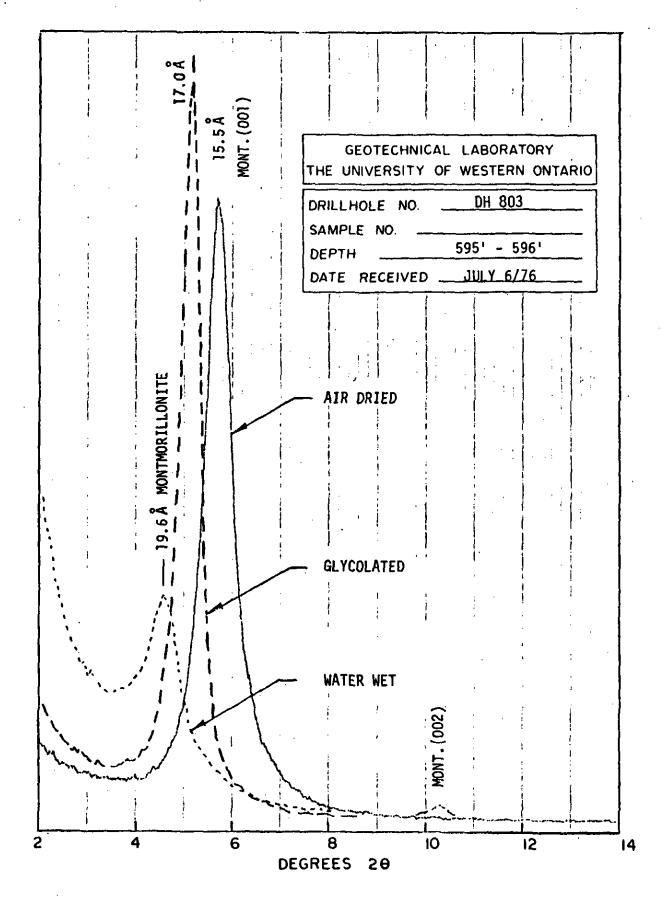


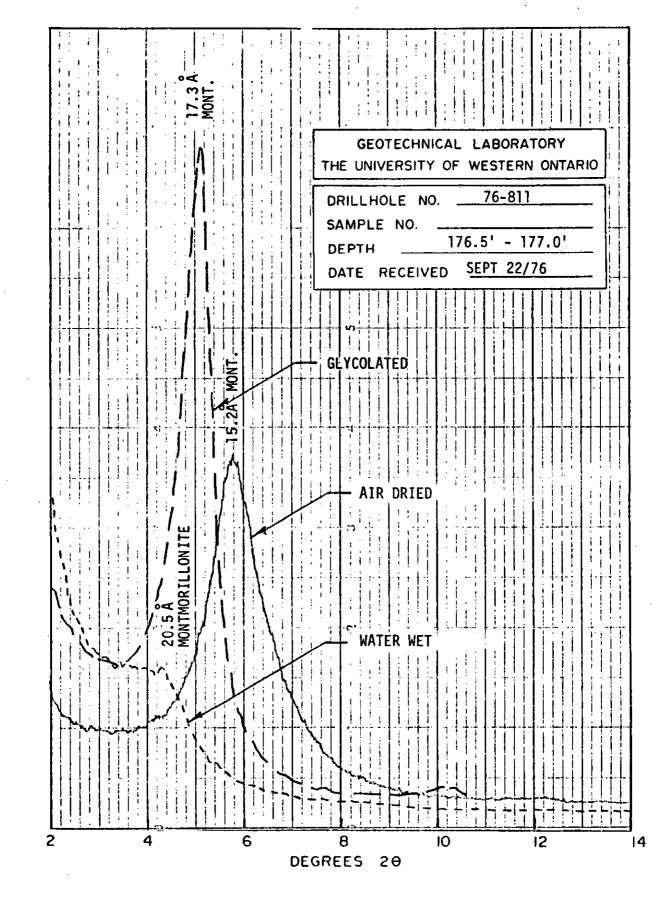


FIG. 6.



X-RAY DIFFRACTION TRACES OF < 2 µm, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK .

FIG. 7.





R.M. QUIGLEY INC. RDBERT M. QUIGLEY, PH.D., P.ENG. President

1052 Kingston Avenue London, Ontario, N6H 4C6

22 December 1976

Mr. G.E. Rawlings Golder Brawner & Associates Ltd. 224 West 8th Avenue Vancouver, British Columbia V5Y 1N5

Dear Mr. Rawlings:

The Significance of Montmorillonite in the Hat Creek Stratigraphic Section

The purpose of this letter report is to discuss the engineering characteristics of the clay mineral montmorillonite with special reference to the Hat Creek project, British Columbia. Also discussed are the significant engineering aspects of the mineralogical and physico-chemical test results contained in the University of Western Ontario research report entitled "Preliminary Mineralogical and Physico-Chemical Analyses, Hat Creek Project, British Columbia" dated November 26, 1976.

This report has been prepared in accordance with verbal arrangements made at a meeting in your Vancouver offices on October 15, 1976 and follow-up letters dated October 20 and 25, and November 2, 1976.

Crystal Structure of Montmorillonite

The clay mineral, montmorillonite, is a very fine grained, 3-layer silicate of extreme activity relative to other clays. Its crystal structure and mineralogical characteristics are illustrated in Figure 1.

As can be seen from the sketch, each 3-layer unit is comprised of a gibbsite or aluminum hydroxide sheet (G) sandwiched between two silica sheets. The gibbsite sheet carries a net negative charge of -0.3 e.s.u.

per unit cell of 10 oxygens as shown by the structural formula. This charge is balanced by adsorbed, hydrated cations that occur both between the 3-layer units and in the double layer around the entire clay particle.

The number of cations present around a clay crystal to satisfy its negative charge is normally expressed in milliequivalents/100 g of clay and for montmorillonite is of the order of 100 m.eq./100 g.

The spacing between the 3-layer units normally varies from 16 to 18 A damp and in the natural state. If dried completely, the spacing decreases to 9.3 Å. Some expandable montmorillonites in dilute, monovalent electrolytes may swell to several tens of angstroms so that, in effect, the bulk of the crystal structure is composed of weakly adsorbed water.

The very small size of the montmorillonite particles plus the interlayer area yield very high specific surfaces for montmorillonite (800 m^2/g). Generally speaking, the smaller the particles (i.e. the greater the specific surface) the more active the clay and the lower its residual friction angle.

One measure of the specific surface is the glycol retention value expressed in mg/g. Values for montmorillonite are normally about 250 mg/g, irrespective of the cations present. The ethylene glycol used for the retention measurements is believed to adsorb on the clay in a layer 2 molecules thick.

The combination of abundant interlayer and adsorbed double layer water is responsible for the high activity, marked swelling and low strength characteristics of montmorillonites.

It is particularly significant that the type of adsorbed cations and the concentration of the pore fluid electrolyte play an important role in establishing the physical properties of this clay. For example, Na⁺-Mont swells much more than Ca^{++} -Mont because twice as many hydrated cations are required to satisfy the negative charges on the particles. Also, a dilute electrolyte serves to expand the double layer around the clays since there are very large concentration differences between the adsorbed cations in the double layer relative to the free water. Conversely a high electrolyte concentration (salty pore fluid) compresses the double layers, tends to cause flocculation and normally increases the strength of the soil.

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If dried to fairly high temperatures $(450 \div 700^{\circ}C)$, some montmorillonites become useful absorbents and decolourizing agents known as Fuller's earth.

Plasticity and Activity of Montmorillonite

Typical values for the liquid limit and activity of the most important clay minerals are tabulated as follows:

Clay Mineral	Pore Fluid Salt Conc.	ω <u>ε</u> (૨)	Activity (Ip ÷ % < 2 μm)	
Kaolinite	Low → High	30 - 60	0.2 → 0.4	
Illite & Chlorite	Low → High	50 - 130	0.5 + 1.0	
Ca Mont	Low → High	100 - 250	1.5 + 1.8	
Na Mont	* High	400 - 550	3.5 + 5	
Na Mont	* Low	1000 - 1300	9 + 11	

*High = 1 to 10^{-1} Normal; Low = 10^{-3} to 10^{-4} N.

The tabulation shows that montmorillonite is very active and plastic relative to the other clays. It also shows that Na montmorillonites are much more plastic and active than Ca Mg montmorillonites and that for dilute pore fluid concentrations, montmorillonite is a truly extraordinary material.

The very high liquid limit values for Na montmorillonite are caused by interlayer expansion that is inhibited by adsorption of cations such as Ca, Mg and K. Figure 2, adapted from Rosenqvist, 1957, illustrates this phenomenon for regimes of monovalent cations. The interlayer collapse caused by K^+ adsorption relative to Na⁺ adsorption reduced the liquid limit of Rosenqvist's test clay from about 370 to 280. Similar collapse occurs with adsorption of Ca and Mg.

The data illustrated in Figure 3 were taken directly from Quigley et al, 1974 and serve to illustrate two points as follows:

1. The test montmorillonite, homoionic in Na⁺, has an activity of 5.5 compared to about 1.7 for the clay homoionic in Mg⁺⁺ (Salinity ~ 5 g/k).

- 3 -

2. The mixtures of Mg illite and Na montmorillonite produced a strong curvature in the activity curve caused by adsorption of Mg onto the montmorillonite from the illite. In other words, preferential adsorption of Mg onto the Na montmorillonite significantly reduced its activity.

Figure 3 also shows values of glycol retention obtained on the illitemontmorillonite mixtures. It is significant that for 100% montmorillonite, similar glycol retentions were obtained for the Na and Mg clay states. The glycol retentions run on the Hat Creek clays are therefore a measure of specific surface and not greatly affected by interlayer or other swelling.

Although little if any illite was observed on the x-ray traces of the Hat Creek deposits, there is enough free Mg^{++} in the pore fluid to markedly reduce the liquid limits and activity values below those for a purely Na⁺ clay.

Permeability

The permeability of montmorillonite varies within the range of 10^{-9} to 10^{-8} cm/sec over a void ratio range of 2 to 10. Sodium montmorillonite is normally at least one order of magnitude less pervious than Ca Mg montmorillonites due largely to a greater proportion of the pore water being bound by adsorption around the monovalent Na cations.

For the sodium rich Hat Creek clays with a void ratio of about 1.0 (corresponding to $\omega_n = 35$ %), the permeability would probably be in the range of 10⁻¹⁰ cm/sec or less.

Residual Drained Strength Characteristics

The shear strength data plotted in Figure 4 were taken directly from Kenney, 1967 and serve to illustrate the residual friction angles characteristic of the main clay mineral groups. The very low values for montmorillonite are characteristic and caused by gliding along the interlayer water between the 3-layer sheets.

The following tabulation shows the significance of both cation type and pore fluid concentration on the $\phi_{residual}$:

- 4 -

Clay	<u>S(g/l)</u>	we	ω _p	Ac	\$res
Na Mont	0	~ 1500	55	~ 14	~ 4°
Na Mont	30	~ 800	45	~ 7	~ 8°
Ca Mont	0	795	47	7.4	~ 9°
Ca Mont	Ca SO ₄ sat'd	775	47	7.4	~ 10°

*Data taken from Kenney, 1967 who tested pure bentonite which may be more active than the Hat Creek clays. Valid for $\bar{\sigma}_{\rm N} > 1$ ton/ft².

It is apparent that both cation type and concentration play a significant role on the values obtained for ϕ_{res} , the worst combination being a very low salinity and a Na⁺ cation regime.

The strength of montmorillonite at very low effective stresses is a matter of conjecture in this writer's opinion. There seems to be some evidence that ϕ_{res} actually increases at low values $\overline{\sigma}_N$. However, fabric-strength studies by the writer suggest that clay platelet orientation plays a vital role in determining ϕ_{res} . Above $\overline{\sigma}_N$ values of 1 tsf, parallelism in the shear plane is highly developed. At very low stresses and higher water contents, the natural tendency of montmorillonite to form a gel of more random fabric may become a significant factor and the apparent effective stress control on c_d and ϕ_d may be overwhelmed by long range physico-chemical bonds.

Discussion of the Hat Creek Montmorillonites

The University of Western Ontario research report dated November 26, 1976 identified montmorillonite as the dominant clay mineral within the clayey strata above and below the coal measures at Hat Creek, B.C. In some beds, montmorillonite appeared to be the only mineral present whereas in others, variable amounts of carbonate, quartz and feldspar were present.

The mineralogical compositions of typical clayey strata appear to be more or less as follows:

- Essentially pure montmorillonite with trace amounts of quartz and feldspar (< 10% primary silicates).
- Montmorillonite with moderate amounts of quartz, feldspar and possibly α-cristobalite (10 to 30%).

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 Montmorillonite with low to moderate amounts of carbonate (1 to 10% siderite).

The pore water composition of the clayey strata appears to be roughly as follows:

Above the coal measures:

- 1. Salinity = 3.5 to 6.5 g/ ℓ (less in glacio-lacustrine deposits)
- 2. Dominant cation is Na⁺ = 1.2 to 2.1 g/l Significant cations are Mg⁺⁺(+ Ca) = 0.05 to 0.07 g/l
- 3. Significant anions are $Cl^{-} = 1$ to 2 g/l and probably some SO_{A}^{-} (not determined).

Below the coal measures:

- 1. Salinity = 3.5 to $4.6 \, g/\ell$
- 2. Dominant cation is Na⁺ = 1.6 to 2.2 g/k Significant cations are Mg⁺⁺(+ Fe) = 0.24 to 1.23 g/k
- 3. Significant anions are Cl^{-} and probably SO_{A}^{-} not determined.

From an engineering point of view, the "pure" or "near pure" montmorillonite beds are the most significant. The carbonate rich beds are less significant, since the carbonates act to some extent as inhibitors of swelling and produce relatively higher shear strengths. Those "near pure" montmorillonites with pore fluids of lowest salinity and highest sodium content are the most significant of all beds.

The total salinity values obtained to date (3.5 to 6.5 g/l) are high enough that extraordinary swelling is probably not a problem unless fresh water leaching somehow proceeds within the deposit. Any strata that do exist with very low pore fluid salinities must be considered as extrasignificant strata requiring special attention.

Although the dominant cation is Na⁺ in all pore fluid samples tested, there is enough Mg, Ca and Fe in the pore fluid to ensure a dominantly divalent regime in the double layer. This, along with the moderate salinities, should serve to effectively reduce the liquid limits and activity values of the Hat Creek clayey strata. Very approximate calculations using Gapon's exchange equation indicate that, with the pore

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fluid compositions so far obtained, the cations present in the double layers around the montmorillonite consist of:

Above the coal measures:

Divalent ca	ations	60	-	70%
Monovalent	Na ⁺	40		30%

Below the coal measures:

Divalent cations	75	-	85%
Monovalent Na ⁺	25	-	15%

These are very approximate since the pore fluid analyses were run on a soil wash rather than squeezed out pore water and the divalent cations may be more abundant than indicated above.

Although the writer did not feel authorized to make an extensive search for geological and mineralogical references to Cordilleran bentonites, some data for Wyoming and Alberta bentonites are readily available. For example, non-marine, late Cretaceous bentonites near Edmonton (Rosalind, Alberta) are discussed by Scarfe, 1973. The major components of these bentonites are cristobalite and montmorillonite, both believed to be in situ alteration products of the glassy volcanic ash deposits. Contaminants are commonly quartz, plagioclase feldspar plus biotite and occasionally siderite. Sodium is apparently the dominant cation along with calcium and magnesium which are indicated to comprise 20 to 55% of the cation exchange capacity.

Wyoming bentonites are described by Güven and Grim, 1972, and again the dominant constituents are 70% smectite and 20% α -cristobalite in the < 5 μ m fraction. Quartz, feldspar and α -cristobalite dominate the coarse fraction (> 5 μ m).

The Hat Creek deposits are quite similar to the above bentonites although α -cristobalite having a very strong 4.04 Å peak seems to be a rather less abundant constituent.

It is understood from telephone conversations with Mr. G. Rawlings that the index properties of the Hat Creek clayey strata have been determined to be more or less as follows:

... 8

 $\omega_n \approx 35$ % $\omega_\ell \approx 109 \text{ to } 178$ % $\omega_p \approx 34 \text{ to } 39$ % Activity = 0.75 to 1.4 (est'd by R.M. Quigley)

The values of liquid limit seem characteristic of montmorillonite with abundant adsorbed divalent cations and are thus consistent with the physico-chemical test results. The activity values are likewise consistent with the mineralogical and physico-chemical test results although somewhat on the low side.

Conclusion

It is hoped that the previous discussions, comments and questions have satisfied the requirements expected of this letter report.

Yours truly, R.M. QUIGLEY INC.

R.M. Quigley, P.Eng. Designated Specialist Civil Geotechnics (Ontario APEO)

RMQ:em



Selected References

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- Quigley, R.M., Kubo, Y. and Hamilton, J.J., 1974. Activity of illitemontmorillonite mixtures. The Univ. of Western Ontario, Faculty of Engineering Science Research Report SM-3-74, 31 p.
- Rosenqvist, I.Th., 1957. Discussion. Proc. 4th Int'l. Conf. on Soil Mechanics and Foundation Eng., <u>3</u>, 257-258.
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- 9 -

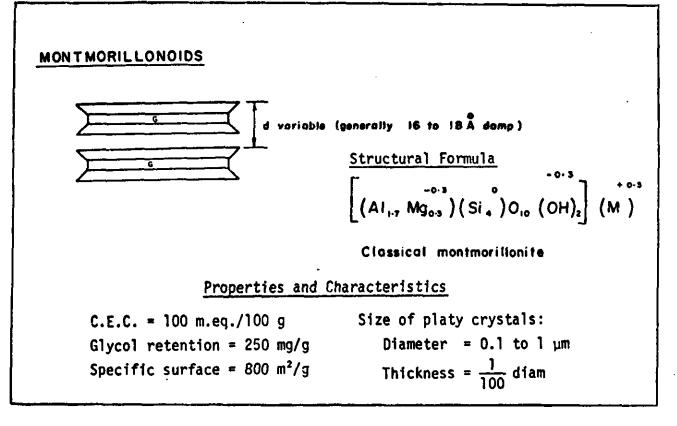


FIGURE 1. THE NATURE OF MONTMORILLONITE

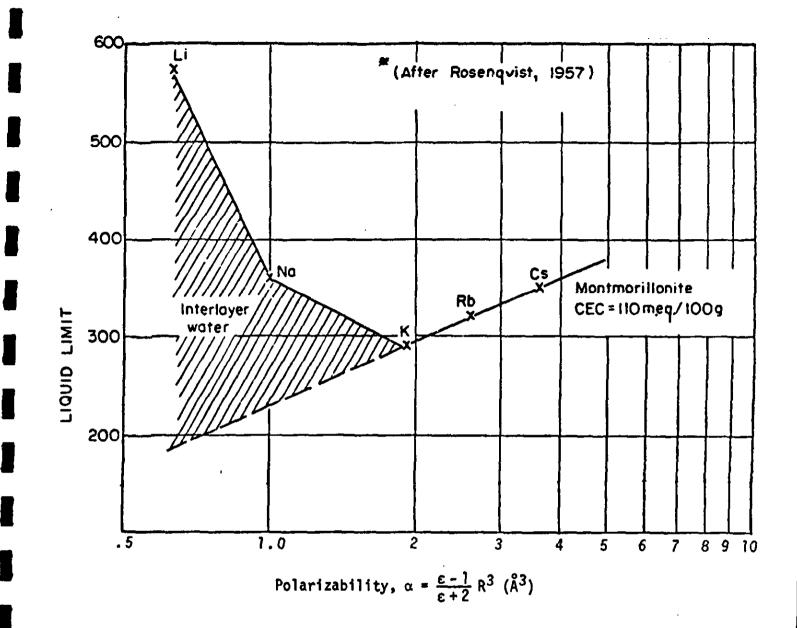
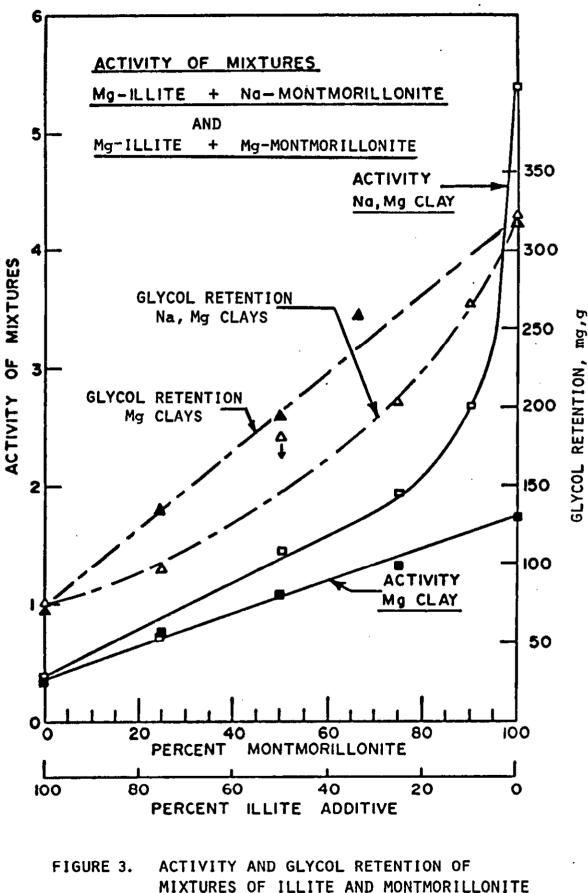


FIGURE 2. VARIATION IN LIQUID LIMIT OF MONTMORILLONITE WITH VARIOUS MONOVALENT CATIONS



(after Quigley, Kubo and Hamilton, 1974)

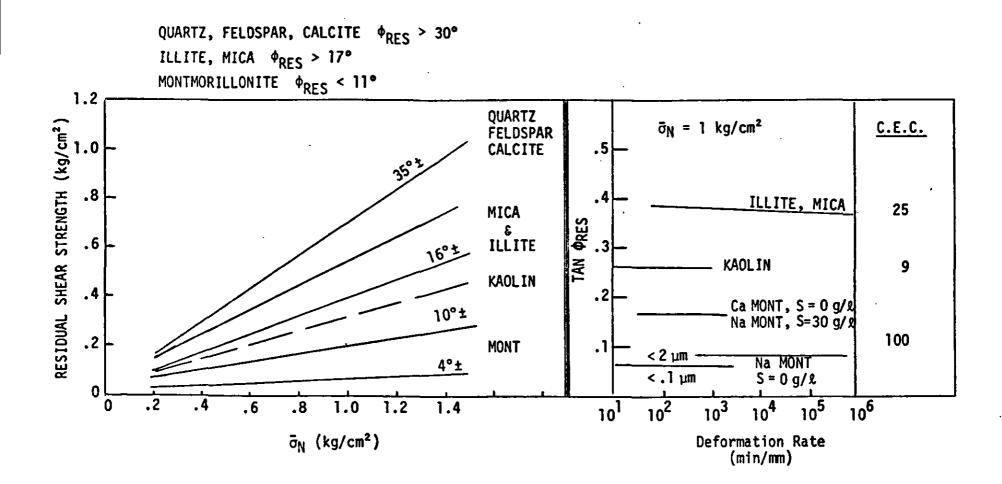


FIGURE 4. RESIDUAL DRAINED STRENGTHS OF THE CLAY MINERAL GROUPS (adapted from Kenney, 1967)



The University of Western Ontario

Faculty of Engineering Science London, Canada N&A 589

RECVD. AT GBA	VANCOUVER
JAN 17	577
FILE No.	10.2.4

11 January 1977

Mr. G.E. Rawlings Golder Brawner & Associates Ltd. 224 West 8th Avenue Vancouver, British Columbia V5Y 1N5

Dear Mr. Rawlings:

Physico-chemical and x-ray testing direct shear specimen from Hat Creek

We have now completed our physico-chemical analyses on your direct shear specimen identified as follows:

> DH 76-806 Sample 21, Depth 171.5 - 176.3 ft.

Our testing has included the following items:

- 1) X-ray powder pattern of the whole soil
- 2) X-ray diffraction of oriented < 2 μ m fraction, Wet PO, ADPO and GPO
- 3) Salinity and pH
- 4) Analysis for pore water Na^+ , Ca^{++} and Mg^{++} .

Results

The x-ray powder pattern shows the sample to consist of the

following minerals in their approximate order of abundance:

Montmorillonite	-	dominant
Feldspar and cristobalite	-	moderate
Quartz	-	moderate to minor

The actual x-ray trace is quite similar to that shown in Fig. 2 of our final report dated November 26, 1976. Carbonate peaks could not be identified on the trace indicating little if any siderite.

The x-ray diffraction traces on the oriented fines yielded traces similar to those shown in Fig. 7 of our November 26, 1976 report. Strong peaks at 20.1 Å (water wet), 15.2 Å (air dried) and 17.1 Å (glycolated) were obtained indicating a nearly pure montmorillonite since peaks at 10 Å and 7 Å were not present.

The pore water salinity, assuming a natural water content of 35%, is about 4.1 g/ \pounds which is similar to the salinities throughout the section as documented in Table III of our November 26, 1976 report. A measured pH of 9.6 is somewhat higher than the typical 9.3 reported on two other samples located stratigraphically below the coal measures.

The cation analyses yield values for Na, Ca and Mg as follows:

 $Na^+ = 2.1 g/l$ $Ca^+ = .016 g/l$ $Mg^+ = .014 g/l$

The sodium value is close to measured values of 1.59 to 2.13 on three other samples below the coal. The values for calcium are very low as in the previous testing. The value for magnesium is much lower than the 0.5 to 0.8 g/ ℓ obtained on three other samples below the coal.

Comments

On the basis of the above analyses, it is suggested that this clay stone is essentially sodium saturated and with swelling permitted would yield a residual friction angle of not greater than 7 or 8 degrees. Lower values would not be expected unless the salt content is reduced below its in situ value of 4.1 g/2.

The writer has reviewed the unsigned reports on the direct shear data supplied to him and concurs with their author that the undisturbed sample did not swell due to the exceptionally low permeability of the bentonitic clay stones. The writer also agrees that complete remoulding at a higher moisture content (more or less in equilibrium with the effective stress on the failure plane at failure) is the best way to establish the lower bound of the friction angle. The writer has found that removal of the grit from soft samples is often necessary to ensure that the lower bound friction values are obtained.

Questions which should be asked regarding direct shear procedures are as follows:

- Did the clay actually reach residual strength in terms of both clay platelet parallelism and moisture content change?
 - (a) For hard, over consolidated clays like those from Hat Creek, the moisture content should increase greatly on the failure plane.
 - (b) For soft, normally consolidated clays rich in montmorillonite, the moisture content will decrease on the failure plane yet parallelism may cause a net loss of strength.
- 2. With regard to the above, an attempt should be made to obtain the moisture content on the actual failure plane and a plot of drained strength vs water content plotted as a control against plots of the strength envelope ($\bar{\sigma}_{ff}$ vs τ_{ff}).
- 3. Did the presence of grit rolling or grinding along between the halves of the direct shear box create an artificial ϕ ? Similarly, was there unnatural gouging by large sized particles (sand) that would create a ϕ_{res} larger than representative of the field ϕ_{res} ?

- 4. Was the rate of strain slow enough to ensure drainage (i.e. no excess pore pressures during shear)? Indeed, is it possible to shear a sample of hard Na bentonite by direct shear and obtain no excess pore pressures?
- 5. At low stress levels and very low strain rates, will the natural thixotropic properties of the bentonitic clays overwhelm the usual effective stress type of relationships commonly obtained on clayey soils?

Although these comments must necessarily be incomplete at this early phase in the study of these complex clay stones, it is hoped that they meet the present needs of the project.

Yours sincerely,

R.M. Quigley, P.Eng. Professor

RMQ:em

	UN	CARRIED OUT BY THE NIVERSITY OF BRITISH COLUMBIA DECEMBER, 1966					
Hole No.	Depth (Ft.)	Quartz	Kaolinite	Bentonite	Siderite	Felspar	Epidote
76-123	399 -403	11	3	69	13	4	-
76-124	348 -350	9	10	71	-	10	-
76-135	296 -301	13	47	34	-	6	-
76-135	534.1-534.5	31	37	26	6	-	-
76-135	557 . 5 - 557.7	24	27	39	-	10	-
76-135	661.0-661.3	34	52	14	-	trace	-
76-136	219 -221	8	н	79	-	2	-
76-144	442	4 9	15	29	-	7	-
76-191	238.6-238.9	8	55	22	trace	15	-
-/		∫ 20	48	19	-	13	-
76-191	298.2-298.5	1 12	58	30	-	-	-
76-191	388.1-388.4	11	68	15	-	6	-
76-191	464.1-465.0	17	47	36	trace	-	-
76-191	532.8-533.1	22	29	38	-	11	-
76-191	645.0-645.5	19	51	-	19	-	11
76-191	706.2-706.5	47	53	trace	-	-	-
76-191	744.7-745.0	43	67	-	-	-	-
76 101	900 1 900 5	(45	51	-	4	-	-
76-191	809.1-809.5	[46	44	-	-	8	-
76-191	950.2-950.8	38	62	trace	-	-	-
76-191	1285.6-1286.0	(35	65	-	-	-	-
, <u>.</u> ,		[43	54	-	3	-	-

SUMMARY OF X-RAY DIFFRACTION ANALYSES

Note: Accuracy for quartz, kaolinite and felspar \pm 3%, for bentonite \pm 5%.

COPY OF ORIGINAL LETTER

CORE LABORATORIES-CANADA LTD. Petroleum Reservoir Engineering

P.O. Box 5670, Postal Station "A" Calgary, Alberta T2H 1Y1 Telephone: 253-3391

July 7, 1976

Birtley Engineering (Canada) Ltd. P. 0. Box 5488, Postal Station "A" Calgary, Alberta T2H 1X9

Attention: Mr. Don F. Symonds

Re:	Analysis of Clay Samples from	
	B.C. Hydro Sample A-7365/66	
	Our File Number: 7061-6268	

Gentlemen:

•

The analysis of the above samples showed the following.

Water Content Mineral Content	6.3% 83.3%			
X-Ray Diffraction	Analysis of Mine	ral Portion		
Quartz	14			
	9			
	6			
-				
	57			
Montmorillonite	10			
Water Content	6.3	2		
Mineral Content	83.8	8		
X-Ray Diffraction	Analysis of Mine	ral_Portion		
Quartz	18			
Feldspar	9			
	5			
•	5			
	50			
Montmorillonite	13			
	Mineral Content X-Ray Diffraction Quartz Feidspar Pyrite Siderite Kaolinite Montmorillonite Water Content Mineral Content X-Ray Diffraction Quartz Feidspar Pyrite Siderite Kaolinite	Mineral Content83.3X-Ray Diffraction Analysis of MineQuartz14Feidspar9Pyrite6Siderite4Kaolinite57Montmorillonite10Water Content6.3Mineral Content83.8X-Ray Diffraction Analysis of MineQuartz18Feldspar9Pyrite5Siderite50		

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CORE LABORATORIES-CANADA LTD. - 2 -

Birtley Engine	ering (Canada) Ltd.	7061-6268
Sample 3:	Water Content Mineral Content	7.6% 80.7%
	X-Ray Diffraction	Analysis of Mineral Portion
	Quartz Feldspar	16 8
	Pyrite Siderite	Trace Nil
	Kaolinite	60
	Montmorillonite	16
Sample 4:	Water Content	4.0%
	Mineral Content	94.8%
•	X-Ray Diffraction	Analysis of Mineral Portion
	Quartz	25
	Feldspar	20
	Pyrite	NTI
	Siderite	NII
	Kaolinite	48
	Montmorillonite	7

The samples were dried in a constant humidity oven at 145°F and 50% relative humidity for four days. A Dean and Stark analysis was performed to measure the remaining water; an ash analysis to determine the mineral content and an x-ray diffraction analysis to determine the type and quantity of the clay components.

Assuming that all the water present is intramicellar (inter-layer) water associated with the montmorillonite, the ratio of water to montmorillonite is 0.756/1, 0.579/1, 0.589/1 and 0.602/1 for sample one to four, respectively. By calculating, the molecular ratio between the water and montmorillonite are 15.1, 11.6, 11.8 and 12.0 for samples one to four, respectively.

The above calculations are based on the assumption that all the water is present as intramicellar water associated with the montmorillonite. The ratio of water to montmorillonite is higher than published values (0.15 to 0.20/1) for samples dried at 145°F and 50% relative humidity. This may indicate that all the free water had not been removed or that a portion of the water had been present as intermicellar (inter-particle) being adsorbed between the montmorillonite particles rather than being adsorbed within the particles.

Yours truly, CORE LABORATORIES-CANADA LTD.

APPENDIX 4

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UN#AXIAL COMPRESSION TESTS

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APPENDIX 4

UNIAXIAL COMPRESSION TESTS

Uniaxial compressive strength testing was carried out in conjunction with the field drilling operations in Hat Creek to assess the variation in strengths of the rock types encountered. On site testing was performed so that the prepared samples would be as fresh as possible avoiding moisture loss. The results of the testing were correlated to such factors as rock type, water content, grain size, and gross structural features. The mode of failure of each specimen was also noted.

DESCRIPTION OF TESTS

The test equipment included a manually operated hydraulic loading ram, a loading frame, a 10,000 lb. capacity proving ring and dial gauge, spherical platens to ensure that load application was perpendicular to the sample surface, and several sizes of flat platens.

The cylindrical rock specimens were cut with a length to diameter ratio of approximately 2, but not exceeding 2.5 nor less than 1.5. Careful end preparation of the sample was essential to ensure a smooth planar loading surface perpendicular to the axis of the specimen. In cases where the rock material was too weak or brittle to allow adequate end preparation, the ends of the specimen were cast in a mold of liquid sulfur, which hardened rapidly to a smooth planar surface. The effect of the sulfur was to minimize stress variations across the ends of the sample and thus ensure a uniform axial load.

Prior to testing, the initial length and average diameter of the samples were measured. Loading was applied relatively slowly to allow "seating" of the platens against the ends of the specimen. When "cracking" of the specimen

was heard the loading was slowed to allow the material time to adjust. When load drop off occurred, the load was noted and allowed to fall off to a stable value. At this point, depending on whether fracture of the specimen had occurred, the sample was reloaded until it could take no further load. The maximum load that the sample was capable of sustaining was judged to be the ultimate uniaxial compressive stress.

RESULTS

The results of the unlaxial compressive strength tests are shown in Table A4-1.

The salient features to be noted are as follows:

- Coal strengths varied from 400 to 2,500 psi. There is no relationship between the compressive strength and depth. The strength is more related to composition, texture, water content, and orientation of discontinuities relative to the direction of loading.
- 2. Conglomerate varied considerably in strength depending upon the degree of cementation present. A range in uniaxial compressive strength from 60 to 560 psi was noted for badly cemented and clayey conglomerate, 560 to 1,600 psi for firmly cemented conglomerate, and 1,600 1,960 psi for strongly cemented conglomerate.
- 3. The strength of the sandstones depends largely on the nature of the cement, degree of weathering and density of packing. The strengths obtained varied from 150 to 860 psi and are low in relation to fresh unweathered sandstones measured elsewhere.
- 4. Siltstone strengths ranged from 80 to 520 psi. Clayey siltstone samples with clay layers failed along the layers, and gave very

low compressive strengths varying from 7 to 40 psi. No consistent relationship between unconfined compressive strength and water content was discerned.

5. Claystone strengths varied from 10 to 140 psi and results were very consistent. There is a definite tendency for strength to decrease with increasing water content. Many of these samples were highly bentonitic.

TABLE A4-1

HAT CREEK GEOTECHNICAL STUDY

UNIAXIAL COMPRESSION TEST RESULTS

Sample	Hole No.	Depth ft.	H/Ø	Co Psi	Description
1	76-809	433	1.6	447	Tuffaceous siltstone.
2	76-809	436	2.0	285	Somewhat tuffaceous, bentonitic siltstone.
3	76-809	436	1.6	383	Greenish, highly tuffaceous siltstone.
4	76-809	443	1.9	238	Greenish, highly tuffaceous w. f. grained cement.
5	76-816	752	2.1	856	M. grained, granodioritic sandstone w. coaly debris.
6	76-816	768	2.0	835	M-f grained, coaly sandstone.
7	76-816	768	2.1	766	M-f grained, coaly sandstone.
8	76-816	748	2.0	796	M. grained, grey sandstone.
9	76-816	843	2.3	J3286	Banded basalt w. chlorite amygdales.
10	76-816	?	2.0	1721	Sheared or flow banded volcanic rock.
11	76-816	783	2.0	1924	Sheared or flow banded volcanic rock.
12	76-151	789	1.8	2479	Coal
13	76-151	855	2.0	1495	Coal
14	76-149	1539	1.9	350	Siltstone?
15	76-149	1533	1.9	800	Claystone?
16	76-149	1523	2.2	807	Siltstone?
17	76-809	216	2 <u>.</u> ì	17	Possible slide plane, bentonitic gravel.
18	76-809	216	2.0	7	Bentonitic claystone w. soft layer.
19	76-809	218	2.1	35	Bentonitic claystone w. soft layer.
20	76-809	218	2.2	42	Bentonitic tuff w. bentonite seams.
21	76-809	130	1.5	114	Carbonaceous bentonitic siltstone.
22	76-809	49	2.1	42	Bentonitic siltstone w. carbonaceous partings.
23	76-809	475	2.1	703	Altered tuffaceous sandstone.
24	76-809	475	2.0	410	Altered tuffaceous sandstone.
25	76-809	462	1.9	239	Altered tuffaceous sandstone.
26	76-809	442	2.1	102	Bentonitic siltstone.
27	76-809	416	2.0	682	Gravelly sandy aggregate of volcanic debris w. zeolite.
28	76-809	401	2.2	519	Tuffaceous silty sandstone.

Sample	Hole No.	Depth ft.	H/Ø	Co Psi	Description
29	76-809	402	2.1	466	Tuffaceous silty sandstone.
30	76-809	386	2.0	259	Tuffaceous silty sandstone.
31	76-809	395	2.0	347	Tuffaceous silty sandstone.
32	76-809	371	2.0	1454	Meta-basalt w. pyroclastic layer.
33	76-809	361	2.0	125	Coarse sandstone & bentonitic siltstone, prob. agglomeratic.
34	76-808	45	1.8	57	Carbonaceous siltstone, w. resin beads.
35	76-808	46	2.0	55	Slide debris - carbonaceous, bentonitic, tuffaceous siltstone.
36	76-808	47	2.0	90	As above with carbonaceous debris.
37	76-808	42	1.9	64	Bentonite
38	76-808	25	2.1	104	Bentonitic claystone.
39	76-808	27	2.1	83	Bentonite
40	76-810	115	2.0	57	M. grained, clayey sandstone.
41	76-810	167 ?	2.0	33	Altered tuff.
42	76-814	362	2.0	50	Bentonitic claystone.
43	76-816	641	2.0	1300	Agglomerate
44	76-816	681	2.1	708	Tuffaceous conglomerate-agglomerate.
45	76-816	718	2.1	1005	Tuff-tuffaceous sandstone.
45A	76-816	675	1.7	1952	Tuffaceous sandstone showing graded bedding.
45B	76-816	716	2.0	1036	Tuffaceous sandstone.
46	76-814	363	2.0	107	Clays tone.
47	76-814	364	1.9	137	Fine grained tuff.
48	76-814	366	1.9	225	Claystone.
49	76-814	395	2.1	115	Bentonitic tuffaceous, sandy siltstone.
50	76-810	265	2.0	81	Sheared, carbonaceous, clayey siltstone.
51	76-810	218	2.1	229	Tuffaceous, coarse grained siltstone.
52	76-814	462	2.0	290	Tuffaceous, medium grained siltstone.
53	76-810	224	1.9	290	Tuffaceous, medium grained siltstone.
54	76-814	452	2.2	78	Bentonitic, silty claystone.
55	76-814	484	2.2	103	Carbonaceous, clayey siltstone.
56	76-814	596	2.1	484	Tuff w. coal partings.
57	76-814	596	2.2	492	Tuff w. coal partings.

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Sample	Hole No.	Depth ft.	H/Ø	Co Ps I	Description
58	76-814	514	2.1	116	Sheared, carbonaceous siltstone.
59	76-814	555	1.9	158	Sheared, carbonaceous siltstone.
60	76-814	640	1.7	125	Silty claystone.
61	76-814	525	2.2	282	Silty coal.
62	76-814	676	1.8	445	Tuffaceous sandstone.
63	76-814	669	2.0	206	Coal - Failed on sheared bedding.
64	76-811	118	1.7	37	Bentonitic siltstone w. carbonaceous layer.
65	76-811	118 2	2.0	59	Bentonitic siltstone (dried).
66	76-811	88	2.0	44	Bentonitic siltstone w. coaly parting.
67	76-811	118	2.2	113	Bentonitic siltstone (dried).
68	76-811	88	1.6	47	Bentonitic siltstone w. coaly parting.
69	76-811	118	1.9	80	Bentonitic siltstone (dried).
70	76-811	107	2.0	162	Interbedded, bentonitic sandstone/siltstone.
71	76-811	107	2.1	167	Interbedded, bentonitic sandstone/siltstone.
72	76-811	142	2.0	50	Disturbed bentonitic, silty gravel - slide.
73	76-811	211	2.3	235	Bentonitic, silty sandstone.
74	76-811	70	2.0	40	Bentonitic siltstone w. coaly parting.
75	76-811	265	2.2	174	N-c. grained friable sandstone.
76	76-811	230	2.0	93	Bentonitic, silty sandstone.
77	76 - 169	388	2.0	2496	D zone – clean durain.
78	76-168	305	2.2	706	D zone - clean durain.
7 9	76-169	382	1.8	998	D zone – clean durain.
80	76-168	288	2,1	5 8 9	Slightly silty coal.
81	76-813	530	2.4	8	Brecclated & sheared, bentonitic siltstone.
82	76-813	575	2.2	325	Bentonitic siltstone.
83	76-813	583	2.4	96	Bentonitic conglomerate.
84	76-813	568	2.2	70	Bentonitic conglomerate.
85	76-813	546	2.3	340	Bentonitic sandstone intact.
86	76-168	408	2.2	599	Vitrain coal sheared.
87	76-168	464	2.0	257	Durain/vitrain silty coal.
88	76-168	368	2.2	817	Silty durain coal.
89	76-169	396	2.2	847	Clarain coal intact.

3.

Sample	Hole No.	Depth ft.	H/Ø	Co Psi	Description
90	76-813	601	2.2	325	M. grained sandstone w. coaly parting.
91	76-813	610	2.2	359	Carbonaceous siltstone - Failed along bedding.
92	76-168	656	2.2	1557	Vitrain coal intact.
93	76-813	620	2.3	420	Slightly sheared, carbonaceous siltstone.
94	76-168	607	2.2	1780	Vitrain coal intact.
95	76-168	636	2.0	2405	Slightly silty vitrain coal.
96	76-813	5 90	2.3	459	Bentonitic f. grained sandstone.
97	76-817	73	2.3	1 398	Clarain coal (D).
98	76-817	87	1.9	919	Silty durain coal.
99	76-171	391	2.3	442	Sheared durain & clarain coal.
100	76-168	686	2.3	1694	Vitrain, slightly sheared.
101	76-168	739	2.3	1164	Silty durain intact.
102	76-168	757	2.2	1438	Silty durain intact.
103	76-172	336	2.2	1814	Silty durain intact.
104	76 - 172	376	2.1	1061	Silty durain intact.
105	76-172	295	2.2	1506	Sheared durain.
106	76-812	72	2.3	53	Bentonitic, sandy siltstone.
107	76-817	201	2.2	805	Silty durain (D).
108	76-817	2 72	2.5	710	Durain sheared (D).
109	76-817	224	2.3	519	Silty durain & vitrain (D).
110	76-817	415	2.1	1197	Clarain (D).
111	76-812	198	2.2	66	Highly bentonitic, clayey siltstone.
112	76-817	436	2.2	707	Carbonaceous siltstone.
113	76-817	386	2.5	1028	Clarain intact.
114	76-812	123	2.2	133	Bentonitic, silty sandstone, intact.
115	76-812	157	2.0	27	Highly sheared, bentonitic, silty claystone.
116	76-812	112	2.0	38	Claystone?
117	76-812	170	2.2	29	Claystone?
118	76-812	?	2.0	18	Highly sheared, bentonitic, silty claystone.
119	76-812	243	2.1	60	Bentonitic gravel.
120	76-812	294	2.2	172	Slightly tuffaceous sandstone.
121	76-812	285	2.3	83	Bentonitic, sandy siltstone/sandstone intact.
122	76-812	328	2.3	510	Tuffaceous conglomerate.

Golder Associates

Sample	Hole No.	Depth ft.	H/Ø	Co Ps I	Description
123	76-812	346	2.1	276	Bentonitic sandstone.
124	76-812	285	2.2	359	Bentonitic siltstone.
125	76-812	258	2.1	113	Clayey, silty sandstone.
126	76-812	346	2.2	340	Bentonitic sandstone (dried for 17-18 hrs.).
127	76-812	381	2.3	634	Bentonitic tuff.
128	76-812	361	2.2	355	M. grained bentonitic sandstone.
129	76-812	381	2.2	321	Bentonitic conglomeratic tuff.
130	76-812	389	2.2	887	Bentonitic conglomerate.
131	76-812	258	2.3	107	Bentonitic sandstone.
1 32	76-812	361	2.1	522	N. grained bentonitic sandstone.
133	76-812	346	2.0	738	Bentonitic sandstone (dried for 20 hrs.).
134	76-812	328	2.5	1963	Calcareous cemented.

APPENDIX 5

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GEOHYDROLOGIC DATA

APPENDIX 5

GEOHYDROLOGIC DATA

Appendix 5 contains the following information:

- Summary hydrologic logs of all holes in which hydrologic installations and tests were made.
- Description of procedure used for carrying out in situ
 falling head permeability tests in standpipe piezometers.
- III) Installation and monitoring of piezometers.
- IV) Cantest Ltd. report on the inorganic chemical analyses of water samples.

1) Summary Hydrologic Logs

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I) HYDROLOGIC LOGS

The following logs summarize hydrologic information on selected boreholes where good subsurface hydrologic data has been obtained. The abbreviated lithology is based on data supplied from drillers, core log sheets and drill logs (see Appendix 1).

In order to show all data in a compact log it was necessary to use a number of abbreviations and a symbolic notation. The following notes explain these abbreviations. The note numbers correspond to the numbers shown in parenthesis at the head of each column in the following hydrologic logs:

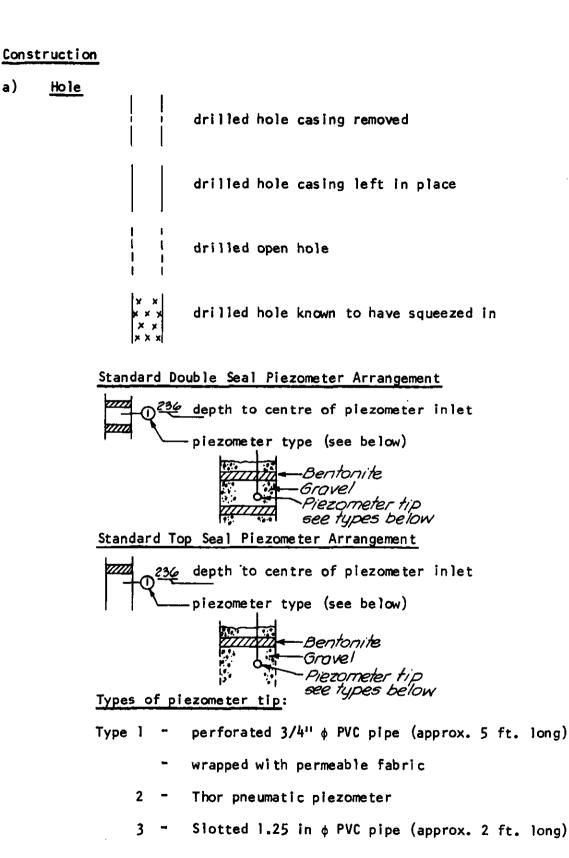
1. Lithology Abbreviations Used in Logs

Rock/Soil Type: Slst = siltstone Sst = sandstone Clst = claystone Congl = conglomerate

2. Datum

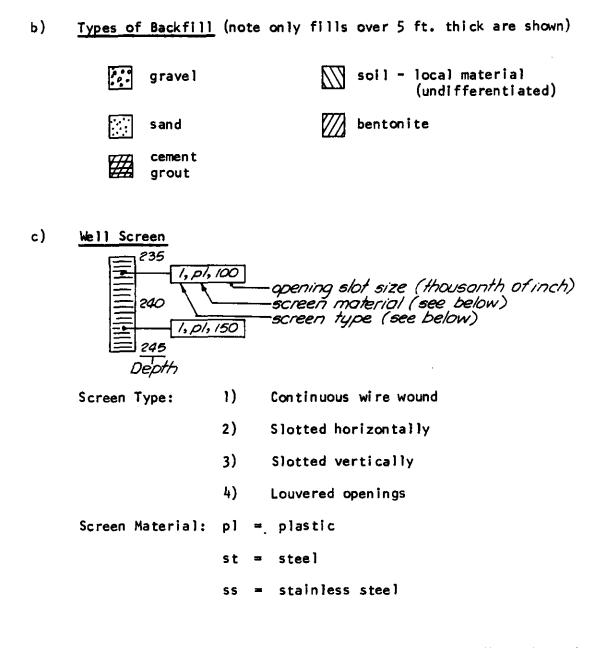
Unless otherwise stated all depth measurements are given in feet relative to existing ground level. T.D. = total depth drilled. A5-2

Golder Associates



Golder Associates

3.



4. WL = Water level measured when drilling had reached indicated depth.

5. WC = Water content of soil, as determined in laboratory (%).

Golder Associates

6.	Other:	fl	=	water flowing over top of casing
		Lw	-	losing water
	-	Mw	-	making water

7. SWL = Static water level in piezometer/well after the ground water had recovered from drilling operations (October, 1976). Positive values indicate artesian heads (i.e. above datum). These static water levels are equivalent to total piezometric heads in all piezometers.

8.	D =	Depth range for permeability test
	К =	Average formation permeability determined (cm/sec)
	M =	Method used to determine permeability
	p =	Packer test using falling head method
	f =	Falling head test in piezometer
	w =	Pumping test
		•
9.	Elevat	ions: are of three types:
		Type 1 estimated from plan

Type 1 estimated from plan Type 2 measured with an altimeter Type 3 surveyed level

Type of Drilling Rig <u>Longyea</u>	<u>r 38</u>	Wireline		E _ 1.79 N _ 759 Horizontal			Type No.	•) 	ation <u>3334</u>
Drilling Fluid <u>B</u>	enton						Purpose of	Hol	<u>Geotechnica</u> Study
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- - - Clst., Sst., - Slst., - Congl. -		3 ¹ 2"							
-	514					-38			Hole "making water" when casing pulled back to 520.
-Mixed coal -Unit -		3"							
Congl.,	834								
Slst., Sst.	931								
-Mixed coal -Unit -	1104								
- _Slst., Sst., _Congl.									
Mixed Coal Unit	1217 1271	T.D.							
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Type of Drilling Rig <u>Longvea</u> Drilling Fluid <u>Be</u>	r_38_	ry wore <u>Wireline</u> tic Mud Ang	NZZ Horizontal	027 90	2	Т	ype N	(9) 0	ration <u>3398</u> 3 <u>Geotechnic</u> Study
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- Slst., Sst., Congl.	238 260				-1				
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¥(I) Lithology	(2) Depth	Complete	(2)(3) ad	Dui	ring D	rilling		Af		rilling		Comments
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Date started =/_/ Date completed J	<u></u>	Unecke	d by <u>DF</u> 1 <u>4/2/7</u>	<u></u> [Go	lde	r	Ass	ocic	itae		Vertical scale : 1 in. to <u>100</u> ft.

	(1) (2)	Completed (2) (3)	Dur	ing D	rilling		Aft	 Drilling		<u>of _ 2</u>
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Drilling Fluid <u>B</u>	enton		Bea	ring		°A	zimuth			ITPOSE	of Hol	
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Type of Drilling Rig	year_38	<u>.Wireli</u> ne tic Mud Ang	ile from	Horizo	<u>82</u> ntat ° A	90	<u> </u>	т	ype N	(9) 0	ration <u>2896</u> <u><u> </u></u>
¥ (I) Lithology	(2) Depth	(2)(3) Completed Construction	Dur (2) Depth	ring D (2314) W.L.	+	ଣ୍ଡେ Other	Af (2) (7) S.W.L.	ier D Per	rilling meabili K (8)	tv	Comments
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Type of Drilling Rig <u>Longyea</u> Drilling Fluid <u>B</u>	<u>r 38</u>	<u>Wireline</u> Nitic Mud	-	N Z	90_		(9) Type No.	Hole_Geotecnnica
¥ (I) Lithology	(2) Depth	Completed ⁽²⁾ Construction		ring Drilling (2) (4) (5) W. L. W. C.		Afte		
Sand, Gravel								
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Type of Drilling Rig Longyeau Drilling Fluid	<u>r 38. W</u>	<u>/ireline</u>	jle from	N <u>815</u> Horizontal	<u>90</u>		Type N	(9)	ation28573 3 Geotechnical
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Construction Depth W. L. W. C. Other SWL. D(2x8) K (8) M (8)				HYDROLOG							DRILLI	<u>-2 – </u>	No. 76-150 of
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	Date started _25 Date completed _		76 Checker	4/27	77	G	olde	r	Ass	oci	ates	5	Vertical scale : 1 in. to <u>50</u> ft.

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Type of Drilling Rig Longyear Drilling Fluid Be	38 W	ireline	le from	N81 Horizontal ^ Az	<u>484</u> 90 ⁰	Type No Purpose of Hol	ation3034 3 Geotechnical Study
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(I) Lithology	(2) Depth	(2) (3) Completed Construction	Dur (2)	ing Di (2)(4) W. L		(6)	Aft (2)(7) SWL.		rilling meabili1	v	Comments
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Drilling Fluid _B	enton	itic_Mud		ring _			zimuth		P:	arpose	of Hold	Geotechnica Study
¥ (I) Lithology	(2) Depth	Complete Construct		Dui (2) Depth	ring D (29-(4) W.L.	w.C.	(6) Other	Afte (2) (7) S.W.L.	Per	rilling meabili K (8)	ty [M (8)	Comments
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Contractor <u>Coat</u> Date started <u>7/8</u> Date completed <u>2</u> /					¥ NOT			numbe				on pages <u>A5=2</u>

Type of Drilling Rig Longyear	<u>Rotar</u> _ <u>38</u> _W	<u>ireline</u>	Coor	<u>elopm</u> dinates e from	E N _	21; 81	922 _	о —	Re	ferenci voe N	e Elev (9) 0.	of <u>1</u>
Drilling Fluid <u>B</u>	(2)	Completed	Bea	ring		°A		Afi		rilling	of Hol	<u>Study</u>
Lithology	Depth	Construction	n 	(2) Depth	(2) (4) W. L.	(5) W.C.	ଶ୍ୟୁ Other	(2)(7) S.W.L.	Per D(2)(8)	meobili K (8)	ty M (8)	Comments
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Contractor <u>Coa</u> Date started <u>9/8</u> Date completed .		- Logged D	י <u>י</u> יי, הע DI	₩-1		of	this	report.				

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Drilling Fluid <u>Bel</u>	ntonii	tic Mud		ring					Pi	irpose	of Hol	Geotechnical Study
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Contractor <u>Coat</u> Date started <u>1</u> Date completed <u>1</u>	13/8/7	Checked 1 6 Date 14	2/7	7	Go	lde			ocio	ates	-	Vertical scale : 1 in. to <u>/00</u> ft.

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Project Type of Drilling Rig <u>Longyear</u> Drilling Fluid <u>.</u>	Botar 38 W	<u>ireline</u>	ordinates	E2]0 N825 Horizontal _	01 		Reference E	of _2 levation _3037 3 lole _Geotechnical
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Contractor <u>Coa</u> Date started <u>1</u> Date completed	ntes	Logged by	DFF	*NOTE : Bi	acketed this	number report.	s refer to not	es on pages <u>A5-2</u> Vertical scale :

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SUM	AR'	Y HYDROLOG	GIC	LOG	(C	ontin	ued)	D	RILLH	10LE 2	No. 76-163
(1)	(2)	Completed (2) (3)	Dui	ing D	rilling		Aft	ier D	rilling		
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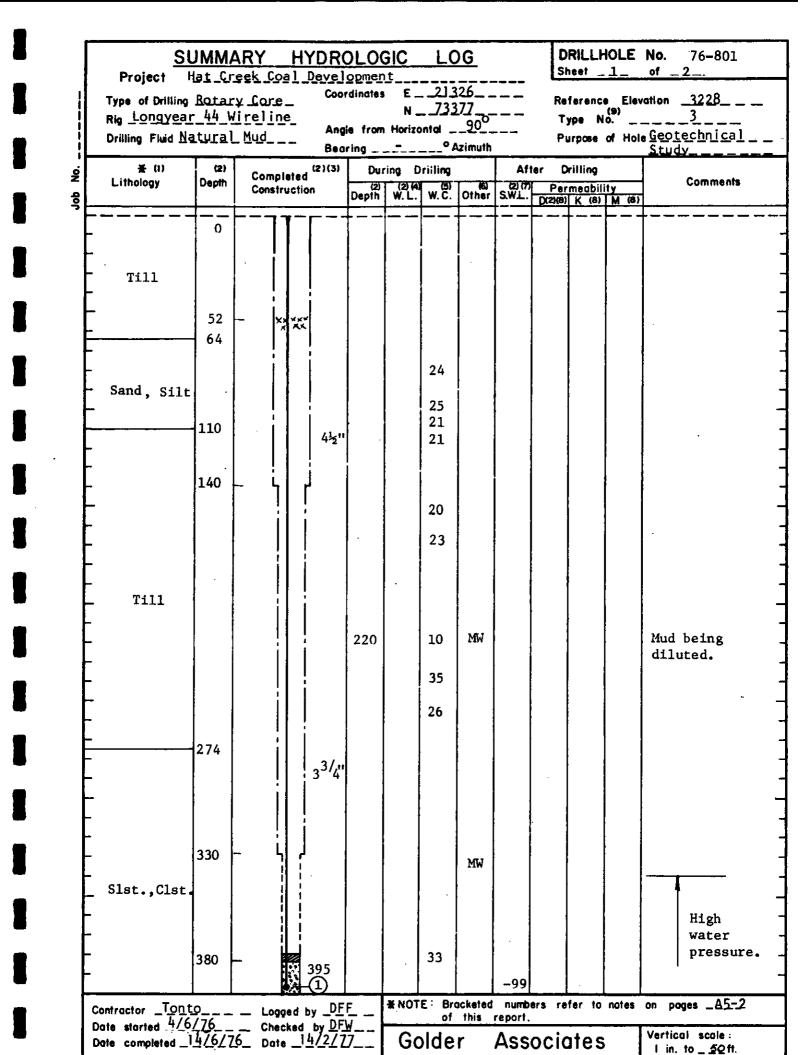
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!	<u>SUMI</u>	MAR	Y HYDROLO	SIC	LOG	(C	ontin	ued)	C Si	RILLH	IOLE	No. of	76-168 _2
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8:00 Linkology Ospit Dept Completed Construction During Dept Onter Outer Deprese Deprese <t< th=""><th>Project Type of Drilling RigLongy Drilling Fluid</th><th>Bota ear_44</th><th>ary Core Wirelin al Mud</th><th>Coo: e Ang Bea</th><th>dinates dinates from</th><th>E N Horizo</th><th>203 751 atol_</th><th>390 90 75 zimuth</th><th></th><th>Re</th><th>ferenci ype N</th><th>e Elev (9) 0</th><th>No. 76-803 of _2 atton _3169 3 Geotechnical Study</th></t<>	Project Type of Drilling RigLongy Drilling Fluid	Bota ear_44	ary Core Wirelin al Mud	Coo: e Ang Bea	dinates dinates from	E N Horizo	203 751 atol_	390 90 75 zimuth		Re	ferenci ype N	e Elev (9) 0	No. 76-803 of _2 atton _3169 3 Geotechnical Study
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		<u> HYDROLO</u>					·	Sh	eet _	2_	No. 76-803
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	Project Type of Drilling Rig <u>Longye</u> Drilling Fluid <u></u>	<u>Rotar</u> ar 44	y Core Wirelj	 	Coordinates Angle from Bearing -	E _ N _ Horizo	74	86 <u>3</u> 90 ⁰		Re1 Ty	ferenci ipe N	Elev (9) 0	of _2 vation _3531 e Geotechnical Study	
Job No.	¥ (I) Lithology	(2) Depth	Comp Constr	(2 leted ruction		ring D	Drilling	<u></u>	· · · · · · · · · · · · · · · · · · ·	Peri	rilling meabili	ty M (8)	Comments	-
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ŀ	Litholog	(1) 7	(2) Depth	Com	pleted tructio	(2) (3) N	Dur (2) Depth	'ing D (2)(4)		(6) Other	Afi (2)(7) SWL.		rilling meabili	y M (8)	Comments
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Contractor <u>Tonto</u> <u>Logged by <u>DFF</u></u> Note started <u>26/6/76</u> <u>Checked by <u>DWF</u></u> Date completed <u>29/6/76</u> <u>Date <u>2/14/77</u> <u>Golder Associates</u></u>	

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	Type of Drilling Rig <u>Longye</u> Drilling Fluid <u>N</u>	<u>ar 44</u>	ry ware Wireline 1 Mud An	ple from	N _ Horizo	79 79 79	182 90	·	T	ypa N	0	ation <u>3377</u> <u>Geotechnical_</u> Study
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	Lithology	Depth	Completed Construction	(2) Depth	-	-	(6) Other	20 (7) S.W⊥.	Per	meabili K (8)	ty M (8)	Comments
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	SUM	MAR	Y HYDROLO		LOG	(C	ontin	ued)	D		10LE	No. 76-806
	(I) Lithology	(2) Depth	Completed (2) (3)	Dur	ing D			Aft		rilling		Comments
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	Project	JMM/	<u>Cre</u>	ek.	Ço	al De		ment	LC			SI	neet _	1_	No. 76-807
	Type of Drilling Rig Longyear Drilling Fluid _N	<u>44 w</u>	l Mu	ine d	?_ _	Ang Bea	le from ring	N _ Horiza	<u>78</u> ontal _	1 <u>06</u> _90 ⁰		Т	ype N	0	ation3558 3 _Geotechnical _Study
	¥ (i) Lithology	(2) Depth	Cor Cor	mpi: Istri	eted uctio	(2)(3))N	Dui (2) Depth	ring D (2)(4) W.L.	-	(5) Other		Per	rilling meabili K (8)	ty IM (B)	Comments
	Sand, Till, Sheared - Material	0		XXX	х _к ү, к _х	(4 ¹ z"	40	-1.5	20 27 26 33	MW					
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-	Contractor To	nto 7772	L	.099	jed	by _ <u>D</u>		* NOT	E: Br	ocketed this	numb report.	ers re	fer to	notes	on poges_A5=2
ļ	Contractor To Date started _ <u>6/</u> Date completed _ ¹	<u>///6</u> 0/ <u>7/7</u>	<u>6</u> c	ihec)ate	:ked	by <u>D</u> by D 2/14	<u>rw</u> 7 <u>7</u> 7_	Go				ocio	ites		Vertical scale : 1 in. to <u>59</u> ft.

	Rig <u>Longyea</u> Drilling Fluid	<u>r 44</u> .		i <u>ne</u>	Ang		N _ Horizo 	ontal _	290		T	ype N	(9) 0	ation <u>3084</u> <u>Geotechnica</u> <u>Study</u>
	業 (I) Lithology	(2) Depth	Com Cons	plet truc	(2)(3) ed tion	Du (2) Depth	ring D (29(44) W.L.	-	(5) Other	Aft 20(7) S.WL.	Per	rilling meabili K (8)	ty M (8)	Comments
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	MAR	Y HYDROLO			(C	ontin	ued)	D		10LE 2_	No. 76-808
(1)	(2)	Completed (2) (3)	Du	ring D			Af		rilling		Comments
Lithology	Depm	Construction	(2) Depth	(2)(4) W. L.	W. C.	(B) Other	SWL.	Per 0(2)(0)	meabilit <u>K</u> (#)	M (B)	
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# 00 Lithology Depth Depth Completed Contraction Concepted Depth Concepted With With With After Drilling Commenting Sand, Gravel 15 Sheared Bentonite 15 33 33 15 33 15 33 15 33 15 33 16 33 17 33 18 33 <	SI Project Type of Drilling Rig Longyear Drilling Fluid	<u>Hat</u> <u>Rota</u> 44 W	<u>ireline</u> al Mud Ang	<u>plot</u> rdinates le from	ment E N Horizo	1723 8203	90 16 190		SI Re T	ferenc	1 Elev (9)	No. 76-809 of <u>2</u> ration <u>3079</u> <u>3</u> <u>Geotechnical</u> <u>Study</u>
Sand, Gravel 10 35 Benerofite 13 35 35 35 44 50 13 44 50 32 42 42 100 100 -22 Sheared Bentonite 35 64 -31 95 50 0 38 27 31 100 Slst. 64 95 0 34 38 31 100 Slst. 160 -6 46 36 38 38 100 205 100 19 30 36 17 Congl., (Slst., Sst.) 330 0 34 30 370 0 30 20 20 10	Lithology		(2)(3) Completed Construction	Du (2) Depth		_	ati Other	1	Per	meabil	ity M (8)	Comments
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Contractor _ Ton to Logged by _DFF _ Date started _22/7/76 Checked by _DFW Checked by _DFW Checked by _DFW Checked by _DFW	Contractor _ To Data started 22	nto /7/76			ļ	of	this	report.				

		Y HYDROLOG						SI	neet 2.	<u> </u>	No. 76-809 of <u>2</u>
(1) Lithology	(z) Depth	(2) (3) Completed Construction	Dur (2) Depth	ing D (25(4) W. L		other	Afi (2)(7) SWL.		rilling meabilit K (8)	y	Comments
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Project Type of Drilling Rig Longyea Drilling Fluid N	<u>Rotar</u> r_44_W	<u>ireline</u> Mud An	ordinate gle fror aring _	s E. N. n Horizo	6 <u>3</u> 632 832	87 _90^		Re Tj	ferenc /pe N	e Eiev (9) 0	of _1 ation _3024 3 Geotechnical Study
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-	217										
	-1217		220	-25							
_ Sheared Slst.					37						
-					5/						
-	277			-43		LW					
_ Congl.	292 300					 					Piezometer not operatio
-	314	^// 299 // *//									Squeezing.
Sst.	329	33/4				MW					
_ Gravel, _ Congl.	251										
-	354	T.D'									
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-	onto	Logged by[* NOT							on pages A5-2

		<u>Creek Coal I</u>)evelopi Coordinates		181	00				_	of _1
Type of Drilling		TATOLE		N.	825	43				(B)	ration <u>2949</u>
Rig Longyear			Angle from	horiza	_ lota	مو	0 	Т	ype N	0	
Drilling Fluid <u>N</u>	latura		learing _		°A	zimuth		P1	праве	or Hok	<u>Geotechnical</u> Study
¥ (i)	(2)	Completed (2)	3) Du	ring D	-		Afi	er D	rilling		
Lithology	Depth	Construction	C2 Depth	(214) W.L.	(G) W.C.	Other	20(7) S.W.L.	Par	meabili	ty M (8)	Comments
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Contractor _ Ton Date started 1 Date completed _ 1	to	_ Logged by _			c ∙ of	ickered this	report.	चाइ हि	nter 10	notes	on pages <u>A5-2</u>

Type of Drilling . Rig Longxear. Drilling Fluid Na	.44 .Vi	.cel ine.	- Ang	in from	N _ Horizo	<u>829</u> 901at _	9 <u>98</u> 90		т	ype N	ò	ation <u>2823</u> <u> </u>
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	SI Project Type of Orliling Rig _Longyea	- Hat. Rotary	<u>Core</u>	cal_Dev Coo	(e) op dinates	E _ N	<u>190</u> 845	5 <u>8</u>		(SI Re	eet_	<u>1_</u>	No. 76-813 of <u>2</u> chion <u>2881</u>
	Drilling Fluid		al_Mud	Ang Bea	le from ring	Horizo	°A	90 zimuth		PI	irpose	of Hold	Geotechnical Study
	불 (t) Lithology	(z) Depth	Complet Construc	(2)(3) ed tion	Dur C2) Depth	ring D (2) (4) W. L.		es Other	Afi 2) (7) S.WL.	Per	rilling meabili K (8)	ty M (6)	Comments
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		373 387	- 7//// ××	2 1 2 382	367 395	-14			-128				
Da	ntractor <u>Tor</u> ite started <u>it</u> ite completed <u>i</u>	nto 5/8/76 22/8/7	Logge Checke 6 Date _	d by _ D ed by _ D 14/2/7	FW	* NOT	lde		report.	ocic	<u></u>		on pages A5=2 Vertical scale: 1 in. to <u>50</u> ft.

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Lithology	Depth	Completed Construction	(2) (3) 20	(2) Depth	ring D (25(4) W. L		Other	Aft (2)(7) SWL.	Pen	rilling neabilit K (B)	y M (8)	Comment s
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- Slst.,				630	0	31						
(Sst.)	Í					27						Caving
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		Hat!	ARY Creek_ ry Cor	Coa]_Dev		ent_ E_	200	<u></u>		SI Re	heet _	<u>1. </u>	No. 76-814 of
	Rig Longyear Drilling Fluid _N	<u>44 W</u>	irelin 1 Mud	e_ 	Bea	ring 🔔	Horizo	<u>835</u> ontal _ °/	06 90 \zimuth		T	ype N	(9) 0	3 Geotechnical Study
	景(1) Lithology	(2) Depth	Comp Const	letec ructio	(2)(3) 5 0N	Dui 23 Depth)rilling (5) W.C.	(6) Other		Per	rilling meabili K (8)	ty M (8)	Comments
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F					415"									
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F	Till	180	Ì		4	105	50							
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Ē		328		77										
E		336 341	- (1)6 - 332 Ž			350	-14	24		-176				
F		J41				360 370	-28	33						
s:	lst.,Clst.					570	_/	36		-				
È_		400						30						
Co Do	ntractor _ Tor te started _8/§ te completed _	10 3/76	_ Log _ Che	geð i cked	by DFF			of	this	report.			-	on pages _A5=2 Vertical scale:
Do	ite completed _	/ /٥/ ٤	. <mark>P</mark> Dat	• _!	4/2/7	/	60	olde	r	ASS	0010	otes		1 in. to _52_ft.

<u>SUMI</u>	MARY	HYDROLC	GIC	LOG	(C	ontin	ued)	D St		OLE	No. 76-814 ot2
(1)	(2)	Completed (2) (3) Dur	ing D	rilling		Afi		rilling		
Lithology	Depth	Construction	(2) Depth	(2)(4) W, L	W. C.	(6) Other	(2)(7) SWL.	Per ()(2)(8)	meabilii K (8)	y M (e)	Comments
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- - -			550	-11	25						
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- - - 	645		620	-6	23 23 27						
- - _Slst.,Sst., Coal	679										
	700	T.D. 69	5	-12			-48				
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Drilling Fluid	<u>44 W</u> latura	ireline 1 Mud	- Ang	ile from	n Horiza	789 ontal _	90	,	Ť	ype N	0	Geotech	nic
분 (I)	(2)	Comple	Bed	ring	 ring D	°4	zimuth	Aft		rilling		Study	
Lithology	Depth	Constru	ted Ction	(2) Depth			es Other		Per	meabili K (8)	ty M (8)	Comme) nta
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t													
\mathbf{F}				175	0								
- - Sand,Gravel,	190	- 5 		200	-140								
- Till													
F			₃ 3/4"	230	-35								
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(1)	(2)	Completed (2) (3		ring D	مملالهم		Af		rilling		
Lithology	Depth	Completed Construction	(2) Depth			(6) Other				y M (8)	Comments
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-		#			19						
— Clayey Sl -	st.				30						
-					35						
-		₩.	585	-24	29 11						
-		12 A									
-	609	_ 274			33	LW					Squeezing
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	Type of Drilling Rig Longyea	_Bota	ary Core	Coor	dinates	E _ N _	<u>789</u>	<u>56</u>	b	Ту	vpe N	(9) 0	ation <u>3249</u>	
	Drilling Fluid _1	latura	a L. Mud	-	e from 'ing				· · ·	Pu	irpose	of Hold	<u>Geotechni</u> Study	<u>cal</u>
	꽃 (1) Lithology	(2) Depth	Completed Construction	2)(3)	Dur (2) Depth	ing D (2)(4) W.L.		(ع) Other	Aft (2) (7) S.W.L.		rilling meabili	ty M (B)	Commeni	ts
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-	Sand,Gravel, Till			4½"	155	-2		:						
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-	Clayey Slst.		X X				25 27							
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-			il I		390	-7								
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	Contractor $_$ $_$ \underline{Tc} Date started $_$ $18/$	<u>nto</u>	Logged by Checked		<u> I</u>		of	this	report	513 FC		INIES	on pages by J	A. ,

<u>50M</u>	MAR	Y HYDROLOG		LUG		-	uea)	s	heet _	10LE	No. 76-816
(1) Lithology	(2) Depth	Completed (2) (3) Construction	Dur (2) Depth	ing D (2)(4) W. L		(6) Other	Af (2)(7) SW.L.		Drilling meabili	ty M (8)	Comment
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Clayey Slst.			430	-136							
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SUN	IMAR'	Y HYDROLO	GIC	LOG	(C	ontin	ued)	C Si	RILLI	IOLE 3	No. 76-816 of <u>3_</u>
(I) Lithology	(2) Depth	(2) (3) Completed Construction	Dui (2) Depth	ring D (2)(4)		(6) Other	Af (2)(7) SWL.)rilling meabili	hy IM (0)	Comment
			Depin	W. L.	₩. €.	Umer	SRL.	0(2)(8)	<u>K (s)</u>	M (0)	
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<u>SU</u> Project	MMA Hat	RY H' Creek Coa	<u>l Dev</u>	elop	nent				SI	heet _	- 1 -	No. 76-817 of _2
Type of Drilling			C001	rdinates	E_ N_	_ <u>199</u> 814	96 - <u>-</u>		Re	ferenc	e Elev	ration2836
Rig Longyean	44 5	lireline	Ana	le from				S	Ť	ype N	o	3
Drilling Fluid Na	Lura	<u>Huu</u>		ring				,	P	urpose	of Hol	<pre>GeotechnicalStudy</pre>
* (1)	(2)	Completed	(2)(3)	Dur	ing D	rilling		Aft	er D	rilling		
Lithology	Depth	Constructio	n	(2) Depth			(5) Other	(2) (7) S.W.L.	Per	meabil	ity	Comments
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	Ì											
					1	37		[1			Drilling with
						, ,		Ì			l	water.
						- 44						
Contractor	to	Logged I Checked Date _1		F	* NOT	E: Bro	ckated	numb	ers re	fer to	notes	on pages A5-2
Date started _ 21 Date completed 27	18/76		L.DEL			10	1015	report.				Vertical scale :

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		Y HYDROLO						SI		10LE . 2	of2_
ij j	(2) Depth	(2) (3) Completed Construction	Dur (2) Depth	ring D (2)(4) W. L		(6) Other	Aft (2)(7) SW.L.		rilling meabili K (8)	ty M (8)	Comments
- Coal					39		-		·		Drilling with water.
- Silty Coal -	441 464		445	-17	22						
- - Clayey Slst/ - Sst.			500	-20							
	545 561						-30				
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Drilling Fluid _]			ile from pring	Horizo		9		Т	/pe N	ò	ation <u>3182</u> <u>3</u> <u>Geotechnical</u> Study
* (1)	(2)			ing D	rilling	-	Aft	er D	rilling		
Lithology	Depth	Construction	(2) Depth	(2) (4) W. L.	(5) W.C.	(6) Other	(2) (7) S.W.L.	Per ()(2)(8)	meabili K (8)	ity M (8)	Comments
	0	┝╼┰┓╾┎╼╴	÷	<u> </u>							
					39						
					49					,	
					33					1	
		4½" 	70	-27							
					28		[[1	ť I	
							:				Squeezing,
	110			-7							"sand" in hole
Slst., Sst.,										1	
Congl.											
			160	0						3	
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	247	-T.D.		0			~150				
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	Lithology Slst., Sst., Congl.	Lithology Depth 0 110 Slst., Sst., Congl. 229 247	0 0 4½" Slst., Sst., Congl. 110 110 229 247 T.D. 247 T.D. 244	Lithology Depth Completed Construction Depth 0 0 4 ⁴ / ₂ " 70 110 160 229 247 T.D. 244	Construction Depin WL 0 0 0 0 0 442" 70 -27 110 0 0 0 110 0 0 0 110 0 0 0 110 0 0 0 110 0 0 0 110 0 0 110 0 0 110 0 0 110 0 0 110 0 0 110 0 0 110 0 0 110 0 0 110 0 0 110 0 0 110 0 110 0 110 0 110 0 110 0 110 0 110 0 110 0 110 0 110 0 110 0 110 0 110 0 110 0 110 0 110 0 110 0	Construction Depth W.C. W.C. 0 1 442" 70 27 110 10 10 -7 28 Slst., Sst., Congl. 110 160 0 24 229 160 0 24 38 229 160 0 24 38 247 T.D. 160 0 24	Construction Depit WL". W. E. Other 0 10 442" 70 -27 28 110 110 -7 160 0 24 229 160 24 38 38 229 10 244 0 160 10 247 T.D. 14 0 160 16 16	Construction Depin W.L." W.C." Other SWL." 0 1 44/2" 70 -27 28 49 33 49 33 10 -7 28 10 -7 28 10 -7 28 10 -7 28 10 -7 28 160 0 24 160 24 38 160 24 38 -150 229 247 -T.D. 1 1 244 0 1 -150 247 -T.D. 244 0 1	Construction Depiň W.Ľ. W.Č. Omer S.WL. Depiň 0 1 412" 70 -27 28 10 110 110 1 1 -7 28 1 S1st., Sst., Congl. 110 160 0 24 160 229 229 247 -7, D. 244 0 -150	Construction Depit with with with any or state of the swith any or state of the swith any or state of the swith any or state of the swith any or state of the swith any or state of the swith any or	Construction Depit W.C. w.C. Difference 0 0 0 0 0 0 0 41211 70 -27 28 0 0 0 51st., Sst., Congl. 110 0 0 0 0 0 0 229 0 0 0 0 0 0 0 0 229 0 0 0 0 0 0 0 0 229 0 0 0 0 0 0 0 0 100 0 0 0 0 0 0 0 0 0 100 0

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Type of Drilling . Rig <u>Longyear</u>	· 44 N	Wireline	ordinate: ngle from	Ν.	837	33	<u> </u>	Т	vpe N	(9) 0	ration <u>2930</u>
Drilling Fluid		В	aring _						rpose	of Hol	Geotechnica Study
₩ (I) £ithology	(2) Depth	(2)(3 Completed Construction) Du (2) Depth	ring D (2) (4) W. L.		(6) Other	Af1 20(7) S.W.L.	Per	rilling meabili K (8)	ity M (8)	Comments
- Sand,Gravel, - Till - Slst., Sst.	0 20 164 214 224 246 319	- 44 - 44 - 33/4 - 222 - 222 - 222 - 222 - 222 - 3" - 3" - 3"	35 80 150	0 -15 -34		MW	-111				Hole uncased when W.L. re ing taken. High mud pressure.
 ContractorOn	to	Logged by)55	* NOT	F: Br	cketec	numb	ers re	fer 10	notes	on pages A5-2_

Rig Longy	<u>ear 4</u>		eveloppe Coordinate Angle fro	BSE.	228 691	84	 b	ту	rpe N	0	ration <u>3084</u>
Drilling Fluid	<u>Natu</u>		Bearing _					Pu	rpose	of Hol	• <u>Geotechnical</u>
¥ (I) Lithology	(2) Depth	Completed Construction	2)(3) D (2) Depti	uring D 2) (2)(4) h W.L.)rilling (5) W.C.	(6) Other	Af1 (2) (7) S.W.L.	Per	rilling meabil K (8)	ity [M (8)	Comments
Sand, Gravel	0 28 52 59		4 ¹ 2" 35	70	39 57 38 37 51 27 25 35 40 29 35 11 14 27	MW	-8				"Sand" in hole "Sand" in hole
Contractor <u>Ton</u> Date started <u></u> Date completed _	<u>to</u> 10/9/	Logged by			E: Bro of	icketed this	numb report.	ers re	fer to	notes	on pages A5-2

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Type of D		lireline	<u>Develo</u> Coordinate:	Proent. E N	_229 _755	29 07	ς — —		ce Elev	of <u>1</u>
	id _Natura	al Mud	Angle fron Bearing _					Purpose	of Hol	• <u>Geotechnica</u> _ <u>Study</u>
¥ () Lithology		(2) Completed Construction		ring D	rilling			er Drilling Permeabi D(2)(8) K (8)	lity	Comments
			-+							
Sand,Gra Till		e	5"							
	65		70	-7						
- Brecciato 	eđ		3"	-2						
	227 239	-T.D. 2	1) 34	-			-8			
										AF 2
Contractor _ Dote started	_ <u>Tonto</u>	Logged by Checked by 76 Date 14/			of	this	report.	ociate:		on pages A5-2_ Vertical scale :

Project Type of Drillin Rig Longyes Drilling Fluid _	n <u>Rotar</u> ar 44 M	lireline An An Be	prdinates ple from aring	i E N Horizoi	7 <u>6</u> ntal	<u>868 </u>	<u>°</u>	τ,	ype N	(9) 0	ation <u>3943</u> Geotechnica
꽃 (t) Lithology	(2) Depth	(2)(3) Completed Construction	Dur (2) Depth	ring Du (2)141 W.L.		(E) Other	Af (2) (7) S.W.L.	Per	rilling meabili	ity [M (8)]	Comments
Greenstone	149		, 100	-57		MW	Dry	148 122-	1.3x 10 ⁻⁶ 2.4x 10 ⁻⁷	f.	Caving Test throu open hole. Test throu piezometer Packer bla lost in ho caved in m all around
Contractor Date started Date completed .	Tonto	- Logged by	DFF	* NOTI		cketed	numb	ers re	fer to	notes	on pages A 5-2.

Project	Hat	ARY HY	L De	velor	unent.	3853	2		S	haet _	<u>L_</u>	No. 76-823 of1
Type of Drilling RigLongvea					N	/050	O		Re	ferenc: ype N	e Elev (9) 0	ration <u>3945_</u> _
Drilling Fluid		al_Mud_	Bea	e from ring	Horizo	ontal ° A	_ <u>90</u> _ zimuth	- - -				• <u>Geotechnical</u> Study
差 (1) 上ithology	(2) Depth	Completed Construction	(2)(3) 1	Dur (2) Depth	(2) (4) (2) (4) W.L.	-	(B) Other	Afi (2) (7) S.W.L.	Per	rilling meabili [K (8)	ty LA (R)	Comments
											<u></u>	
Gravel			4 ¹ 2''									
-	21											
	24	┝╴┖╏╏╢										
- -			3 [/] 4									
- Greenstone												
									40– 80	1.8x 10 ⁻⁵		Test through
-	66											open hole.
- -			-1					-12				
-	80	-T.D.	75									
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Contractor Tor		Logged by Checked			¥ NOT	E: Bro of	cketed this	numb report.	ers re	ifer to	notes	on pages <u>A5-2</u>
Date started <u>22</u> Date completed <u>2</u>	3/9/7	6_ Date _ 1	4/27	77_	Go	olde	r	Ass	ocio	ates	,	Vertical scale : 1 in. to <u>20</u> ft.

¥ (1) Lithology 1	(2) Depth	Complet Construct	(2) (3) tion	Dur (2) Depth	ing D (2)(4) W.L.	rilling (5) W.C.	(6)	Aft		rilling		9
- - - - - - - -	0		4 ¹ 2"				Other	S.WL.	Per D(2)(8)	meabili K (8)	ity M (8)	Comments
Greenstone	150 182 205	T.D.	+-1	115	-75 -115 -65				160-	10- 4.0x	8 f	No water encou tered in the till. 2 cave-ins - to 192' 2nd to 150' after pie installation & retrieval of H rods. 170-205' inter subsequently caved in.

	Project .		ARY HYDR	evelo	pment	- 361	<u>~~</u> 8		S	heet _	1	No. 76-825
	Type of Drilling	- Rola	art role		N	8250	28		Re	ferenc	e Elev	vation <u>4600</u>
	Rig _ Longyes			le from	Horizo		_90°			ype N		3
	Drilling Fluid	Natur	ral_MudBeo	ring		°A	zimuth		P	urpose	of Hol	•_Geotechnical _Study
	¥ (I)	(2)	(2) (3) Completed		ring D			Af		rilling		Comments
	Lithology	Depth	Construction	(2) Depth	(2) (4) W. L.	W.C.	(6) Other	(2) (7) S.W.L.		meabil K (8)	ity IM (8)	
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F	Sand	1	<u>Ч</u>								ļ	
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Ço	ontractor	nto	- Logged by $-$ D	FF	* NOT	E: Bro of	cketed this	numb report.	ers re	fer to	notes	on pages _A5=2
Do	ote started _ 인/ _	1.17.76	Checked by _D. 5 Date _14/2/7.	EW		olde		Ass				Vertical scale :

Type of Drilling Rig _ Longye Drilling Fluid <u>N</u>	ar_44_	Wireline	Angl	e from	N _ N _ Horizo	82 	<u></u>	• •	Re Ty Pi	feranci ypa N urposa	e Elev (s) o of Hol	ration4619 3 • <u>Geotechnical</u>
₩ (I) Lithology	(2) Depth	Completed Construction	2)(3)		ing D	rilling		Af1 (2) (7) S.W.L.	Per	rilling meabili	ity	<u>Study</u> Comments
Phyllite		- ////	4 ¹ / ₂ "					-13		K (8)		

Type of Drilling Rig <u>Longyear</u> Drilling Fluid	<u>44_W</u>	iceline_ al Mud	Ang Bea	dinates le from ring	N _ Harizo	_3716 _8279 ° A	98 90	0 	Ty	pe N	(9) 0	ation <u>4603</u> <u>Geotechnica</u> l <u>Study</u>
₩ (I) Lithology	(2) Depth	Completed ⁽⁾ Construction	2)(3)	Dur (2) Depth	ing D (2) 44 W. L.		(6) Other	Afi (2)(7) S.WL.	Per	rilling meabili K (8)	ty M (8)	Comments
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Drilling Fluid	atura	al Mud 🛛 🥖		from He								• <u>Geotechnical</u>
* ω	(2) Depth	Completed (2)	E	During		_	- 43			Drilling		Comments
		Construction	De	pth W	20 (4) '. L.	W.C.	Other	(2) (7) S.W.L.	D(2)(rmeabil B) K (8)	ity <u>M</u> (8)	1
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Type of Drilling Rig _ Bucyr Drilling Fluid			Angi	rdinates le from iring	Horizo	ontoi	<u>90</u> °		τv	voe No	(9) 0.	ation <u>3335</u> <u>Geotechni</u> <u>Study</u>	
₩ (1) Lithology	(2) Depth	Completed Construction	(2)(3)	Dur	ring D			Aft	Per	rilling meabilit	ty	Commer	nts
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<u>SUM</u>	MAR	Y HYDROLO	SIC LO	<u>G</u> (Con	tinued)	DRILLI Sheet	HOLE	No. RH-76-10
(I) Lithology	(z) Depth	(2) (3) Completed Construction	During (2) (2)(Depth W. L			ter Drilling Permeabili D(2)(8) K (8)		Comments
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Type of Drilling RigBu		Frie		Ν_		183	o— —	Re T	ferenc: voe N	e Elev (9) 0.	ration <u>3397</u> 3
Drilling Fluid		An	<mark>gle from</mark> arin <mark>g _</mark>	Horiza	int oi _	- 30		P	urpose	of Hole	<u>Geotechnical</u>
¥ (I)	(2)	Completed (2)(3)	Du	ring D	rilling		Af	ter D	rilling		<u>Study</u>
Lithology Comple		Construction	(2) Depth	(2) (4) W. L.	(5) W.C.	65) Other	(2) (7) S.W.L.	Per D(2)(8)	meabili K (8)	ty M (8)	Comments
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Date started _ 2/	8/76	Logged byD Checked by _D 6 Date _14/2/7	FW		of	this	report.	·			
Date completed <u>1</u>	<u>0/8/76</u>	<u> Date 14/2/7</u>	Z	Go	olde	r	Ass	ocio	ites		Vertical scale : 1 in. to <u>20</u> ft.

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Drilling Fluid		Bea	ring		^A	cimuth .				of Hou	Geotechnical Study
꽃 (I) Lithology	(2) Depth	(2)(3) Completed Construction	Du: (2) Depth	ring D (2)(4) W.L.	741	(63) Other	Aft 20(7) S.W.L.	er D <u>Per</u> D(2)(8)	rilling meabili K (8)	ty M (8)	Comments
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<u>SUM</u>	IMAR'	Y HYDROLOG	GIC	LOG	(C	ontin	ued)			No. RH-76-12 of _2
(1) Lithology	(2) Depth	(2) (3) Completed Construction	Dur (2) Depth	ing Di (2)(4) W. L		(6) Other	Af1 (2)(7) SW.L.	Drilling meabilit	ly I Mar (Ba)	Comments
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Type of Drilling Rig <u>Buc</u> Drilling Fluid	<u>yrus E</u>	rie	Cooi Ang	rdinates le from	E_ N_ Horizo	78	002 90	0	Т		(9) D	ation3427 3 Geotechnica1
¥ (i)	(2)		Bec	ring _		°A Frilling	zimuth	` `				<u>Study</u>
Lithology	Depth	Completed Constructio	n	(2) Depth	-	-		(2) (7) S.W.L.	Per	meabili K (6)	ty M (8)	Comments
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- Slst.	62											
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- - • Slst., Congl	101	-	-1 98					-77		9.5x 10-9	f	
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Type of Drilling Rig Bucyri	Kota us Er	ry ie			Ν.	<u>820</u>	<u>21</u>		Rei	ferenci /pe N	e Elev (9)	vation <u>3083 </u>
Drilling Fluid			Ang	le from	h Horiza	ontal _	- 90-		Pu	rpose	of Hol	• Geotechnical
<u>米</u> (I)	(2)	Complete		_	ring D		21119411		er Da	rilling		
Lithology	Depth	Complete Constructi	d 011 	(2) Depth	+	-	(6) Other	(2) (7) S.W.L.	Peri	meabili	ity M (8)	Comments
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<u>SU</u> Broinst		ARY	<u>H)</u>			GIC	LO	G					No. RH-76-15 of _2
SU Project Type of Drilling	Rota	<u>- LCRRK.</u> rv	. LQË	Coor	rdinates	E_	197	55		Re	faranci	n Flav	ration
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Drilling Fluid					e from					P	urpose	of Hol	Geotechnical
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¥ (I) Lithology	(2) Depth	Comple Constru	eted	(2)(3)		ring D	-	6			rilling meabili	14 M	Comments
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Type of Drilling RigBu Drilling Fluid _	icyrus	Erie	Ang	rdinates le from	N _ Horizo	<u>_76</u> ontal _			Т	vpe N	(9) Io.	ation3182 3 6eotechnical
¥ (I) Lithology	(2) Depth	Completed	(2)(3)	1	ring D	rilling		Af	ter D	rilling		Study Comments
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Type of Drilling Rig Buc Drilling Fluid	<u>yrus l</u>	Erie	Ang	le from	E N Horizonto	. <u>76561</u> x9	00	Τv	oa N	(<i>■)</i>	ation <u>3182</u> Geotechnical Study
¥ (1)	(2)	Completed			ing Drill				illing		
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Drilling Fluid A			Ang	e from ring				- .	P	urpose	of Hol	e Geotechnical Study
¥ (1)	(2)	Completed			ring D	rilling		Afi	er D	rilling		
Lithology	Depth	Constructio	n	(2) Depth	(2)(4) W.L.	(5) W.C.	(5) Other	62) (7) S.W.L.	Per D(2)(8)	meabil K (8)	ity M (8)	Comments
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,	388	T.D. 2392					-35				Reading prio
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Contractor]	onto _	Logged by Chacked by Dote <u>14/2/7</u>	<u>'</u>				report.	via (61	10 IU	HA149	

Beering
Sand, Gravel, Till 115 145 Clayey Slst. Sand, Gravel, 12" 12" 145 Clayey Slst. 388 388 388 12" 145 10 ⁻⁸ W 145 10 ⁻⁸ W 145 10 ⁻⁸ W 145 10 ⁻⁸ W 145 10 ⁻⁸ W 145 Pea size gravel pack placed in annular space or shift or end at each casing four slots 6" 10 ⁻⁸ W Pea size gravel pack placed in annular space or shift or end at each casing four slots 6" 10 ⁻⁸ W Pea size gravel pack placed in annular space or shift or end at each casing four slots 6" 10 ⁻⁸ W Pea size gravel pack placed in annular space or shift or end at each casing four slots 6" 10 ⁻⁸ W Pea size gravel pack placed in annular space or shift or end at each casing four slots 6" 10 ⁻⁸ W Pea size gravel pack placed in annular space or shift or end at each casing four slots 6" 10 ⁻⁸ W Pea size gravel pack placed in annular space or shift or end and surface.

Type of Drilling RigBuc Drilling Fluid	cyrus	crie	Ang	dinates le from ring	N _ Horiza	232 <u>752</u> ontal _ °A	2 <u>77</u> 90	0 0	Refere Type Purpo	nce Ele (9) No se of Ho	avation <u>2953</u> <u>3</u> Die Geotechnical Study
¥ (1) Lithology	(2) Depth m.	Complete Construct	d ⁽²⁾⁽³⁾	Dur	ing D	rilling	(6) Other		er Drilli Permec D(2)(8) K	ng ability	Comments
Sand,Gravel, Till Brecciated Slst.	0 55 65 70 85 105	T.D.						-25			Lithology interpreted from DDH 76-821 (RH 76-21)

II) In Situ Permeability Testing

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IN SITU PERMEABILITY TESTING

Falling head permeability tests were performed through the standpipe piezometers installed in six of the air-flush drill holes, (RH 76 Nos. 10-15) and in three diamond drill holes located in the proposed ash dump area (76-822, 76-823 and 76-824).

- The water in each standpipe was allowed to stabilize to a static level.
- Water was then poured into the standpipe to impose an excess pressure head of about 30 ft. of water at the test section.
- The water level in the tube was then monitored until it approached the original elevation.
- 4. From a plot of pressure head vs. time (or depth below a fixed datum vs. time) the permeability constant was calculated by means of the following equation:

$$k = \frac{r^2 \ln (L/R)}{2L (t_2 - t_1)} \ln (H_1/H_2)$$

where k = permeability constant

- r = radius of standpipe
- L = length of isolated borehole section
- R = radius of borehole
- H₁ = pressure head of water in standpipe above static level at some point during the test

 H_2 = pressure head at some later time

 $t_2 - t_1 = time interval between H_2 and H_1 measurement.$ The results of these tests are summarized in Table A5-1.

TABLE A5-1 SUMMARY OF ALL PIEZOMETERS INSTALLED DURING 1976

Piezometer No. 1⁽⁴⁾

Piezometer No. 2

Piezometer No. 3

Nole No.	Detum Elevation	installation ⁽¹⁾ Depth	Rock/Sol1 ⁽⁵⁾ Type	Plezoneter Type	Plezometric ⁽³⁾ Elevation	Tested ^[2] Permobility <u>(cm/sec)</u>	Installation ⁽¹⁾ Depth	Rock/Soil(S) Type	Plazom ter Type	Plezometric ⁽³⁾ Elevation	Tested ⁽²⁾ Permability <u>(ce/sec)</u>	Installation ⁽⁾⁾ Depth	Rock/Soft(5) Type	Piezoneter Type	Flozomatric (3) Elevation	Testad Permaability (cm/sec)
DOH 76-801	3228	380 - 404	Clut., Sist.	Standpipe	3130											
DON 76-802	3490	570 - 590	Sst.	Preumatic	3499		39 - 50	Cley, Congl.		non-operational						
00H 76-803 00H 76-804	3170	550 - 596	Sist.	Standpipe	3149		58 - 68 35 - 45	Sand	Standpipe	3109		Annelus	-	Standpipe		
BBH 76-805	3531 3362	361 - 382 287 - 295	Congl., Sst. Sisc.	Proventic Proventic	non-operational 3344		,, • •,	Sst.	Standpipe Pnoumstic	1503 3356						
Nen 76-806	3376	455 - 469	Sist.	Standpipe	3342			Set.	Proventic	3374						
101 76-807	3554	195 - 209	Sst.	Proventic	3514											
	3086	561 - 574	Sist.	Standpipe	2904											
BOH 76-809	3081	459 - 474	Sst.	Standpipe	3018		Annulus	-	Standpipe	3058						
DON 75-810	3023	292 - 300	-	Prountic	non-operational											
00H 76-8 11	2951	361 ~ 390	Sist.	Standpipe	2914											
101 76-812	2825	317 - 330	Congl., Sst.	Standpipe	2010											
NUN 75-813	2001	373 - 307	Sand, Gravel	Standpipe	275											
1000 76-814 1000 76-815	2971 3150	673 - 788 60 <u>9</u> - 624	Sat., Sist. Sist.	Standpipe Standpipe	2924 2844		328-336	Sand	Standpips	2754						
101 76-816	3250	867 - 864	lesalt	Standpipe	3035		326-338	51st., \$st.	Scendeline	3097						
DBH 76-817	2836	5A5 - 560	Sist.	Standplan	2806		,, ,, ,									
881 76-618	3183	729 - 247	Sist., Sst.	Standplag	3030											
BOH 76-819	2930	214 - 224	Sped, Gravel	Promitic	2819											
88H 7 <u>6-</u> 838	3004	195 - 207	Sist.	Standpipe	3078		51~54	Sist.	Standpipe	3076						
888 76-821	2963	227 - 24 8	Stat.	Standpipe	295Z	-1										
889 76-822	3943	123 - 149	Greenstone	Standpipe	dry	2.4 x 10 ⁻⁷										
100 75-823	3947	68 - 82	Greenstone	Standpipe	3907	1.8 × 10 ⁻⁵ 3.6 × 10 ⁻⁸										
10H 76-824 14H 76-825	3855	152 - 174 35 - 50	Greenstone Phyllite	Standpipe Standpipe	3700 45 86	3.6 × 10 -										
HEN 75-825	4619	35 - 50 36 - 52	Phyllite	Standpipe	4606											
New 76-827	4603	4)-50	Phylite	Standpipe	4591											
100 76-828	4613	54 - 6 8	Phyllips	Standpipe	4601											
BBN 75-134	3335	540	Cist.	Standpipe	3297		66 - 72	Gravel	Standpips	3292						
00 H 76-137	3397	238 - 259	Sist., Set.	Standpipe	3395		Annulus									
NH 76-130	3000	820 - 827	Sst. (besal)	Standplag	2627		194-202	Ceel	Standpipe	2842						
00H 76-141	3342		ilst., 5st. (basal)		3279											
HOH 76-143	2897	330 - 352	Sist., Sut.	Standplat	2874											
1001 76-144 1001 76-146	3136 2856	1074-1 09 4 140	Coel Sst.	Standpipe	3074											
1011 75-140	2969	284 - 295	Sst., Congi.	Protungtic Standpips	non-operational 2820				_							
NOH 76-149	3268	1488-1508	Sist. (besal)	Standpipe	3182		118	Clay	Proventic	3217						
0001 76-150	2891			Standplps	2638			•								
BBH 76-151	301 9	1031-1036	Cist.	Scandpipe	2867											
DEH 76-152	2823	383 - 400	Stat., Sat.	Standpipe	2812											
DOH 76-155	3169	779 - 793	Coal, Cist.	Standpipe	3109		84 - 92	Sand, Gravel		3719						
BBH 76-156	3035 3218		lst., Sst. (busal)		2870		190-284	Sand, Clay -	Scanapipe	dr v						
08H 76-158 98H 76-160	3037		lst., Sst. (basal) lst., Sst. (basal)		3032 2845		197-207	Sand, Gravel	S +	2851						
084 75-161	3133	817 - 853	Sist. (basal)	Standpipe	2932		129-176	Clut.	Standpipe	3004						
DBH 76-163	3038	497 - 516	Sist. (basal)	Standpipe	non-operational		263-276	Sand, Cos I	Standpipe .	non-operational						
DDH 76-168	2943	130 - 142	Coel	Standpipe	283											
RH 76-10	3335	174 - IBA	Sst.	Standpipe	3309	6.0 × 10 ⁻⁹	143-158	Sist., Sst.	Scandpipe	3264	5.3 × 10	121-132	Clat.	Standpipe	3253	3.2 × 19 ⁻⁹
RH 76-11	3397	136 - 150	Sist., Sst.	Standpipe	3342	5.7 × 10 ⁻⁹	115-127	Sst.	Standpipe	3336	4.1 x 10 ⁻⁹	¢] - 95	lese t	Standp pa	3332	1.8 x 18 ⁻⁶
RN 76-12	3341	159 - 176	Slat.	Standpipe	3202	1.2 x 10 ⁻⁰	133-149	Sst.	Standpipe	3286		108-120	Sst.	Stendpine	3296	
RH 76-13	3427	112 - 122	Sist., Congl.	Standpipe	3353	2.1 x 10 ⁻¹¹	86-101	Sist., Congi.		3349	9.5 x 10 ⁻⁹ 1.9 x 10 ⁻⁹	63 - 85 11 - 86	Sist., Clay	Standpipe	3355 3022	1.4 x 18 ⁻⁸ 1.8 x 18 ⁻⁹
RH 76-14	306) 2823	122 - 121	Sist.	Standpipe	2963	3.0 × 10 ⁻⁹ 5.0 × 10 ⁻⁵	94 -110	Sist.	Standpipe	2991 2002	1.9 x 10 * 1.4 x 10	73 - 86 142-155	Sist. Coel	Standpipe Standpipe	3022 2802	1.8 x 16 * 1.9 x 10 ⁻⁴
RH 76-15 RH 76-16	3182	197 - 208 149 - 159	Coel Sist.	Standpipe Pneumatic	2002 3127	3,0 X 10 °	170-181	Coal	Standpipe	2042		1-4-133	LOUI	a canap (pe	1004	
RH 76-16A	3182	384 - 388	Sist.	Preventic	3142		226-246	Sist.	Pround ic	3164						
RH 76-17	3172	390 - 403	Sist.	Preumptic	3116		267-280	Sist.	Proventic	3130		156-165	\$lst.	Pnounatic	3126	
RH 76-18	3196	387 - 400	Sist.	Proventic	3159		281-294	Sist,	Promotic	3167		182-192	\$lst.	Proventic	3176	
RH 76-20	2953	55 - 65	T 511	Standplpe	2927											
					•											

NOTES: 1) All depths are given in feet with respect to datum elevations (top of tube for stand pipes and ground level for pneumatic pizz.).

2) Permeability tests were carried in situ using the falling head method.

3) Plezometric elevation as of November 1, 1976 except for RH 76-16, 16A, 17 and 18

which are readings taken prior to pumping test.

4) Piezometers are numbered from the deepest upwards.

5) See index to abbreviations in preamble to Appendix 1, Volume 2.

III) Installation and Monitoring of Piezometers

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III) INSTALLATION AND MONITORING OF PIEZOMETERS

Two types of piezometers were used, and were set in either cored mudflush diamond-drill holes (3 to 4-inch diameter), or in air-flush rotary holes (6-inch diameter). A total of 74 standpipe piezometers and 19 pneumatic piezometers were installed. Details of the installations including typical designs are included in the last section and are summarized in Table A5-1.

All piezometer installations were designed as permanent installations to provide long-term monitoring of piezometric heads resulting from seasonal changes and pit excavation.

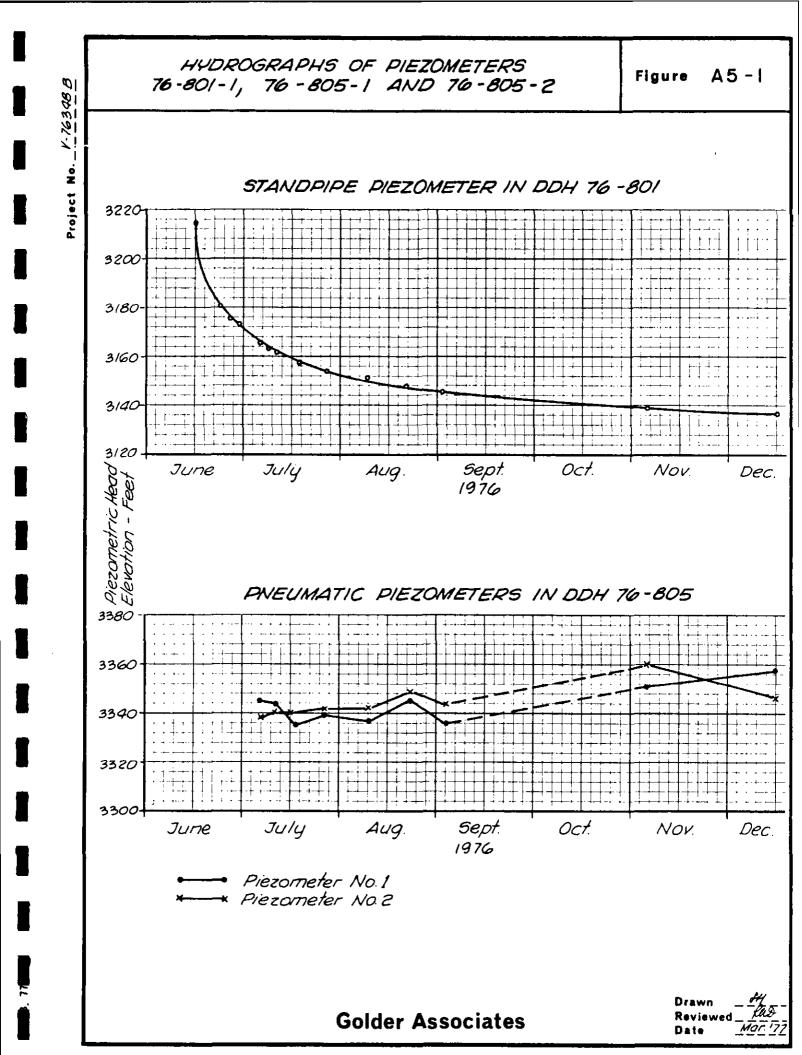
The piezometers were installed preferably in air-flush rotary holes, so that problems arising from the mudded walls of the holes were obviated. However advantage was also taken of the large number of mud-flush holes being drilled to install instruments wherever practicable. In the deeper holes, where the hole walls were difficult to stabilize, piezometer installations had to be completed through the drill rods after geophysical logging had been carried out. Piezometers were set in nests of one, two and occasionally three per hole, and only one hole had four piezometers (RH 76-15). The upper piezometers were usually set quite easily in the open hole after removal of the drill rods and before collapse of the hole.

The piezometers installed during the 1976 drilling program have been useful in providing initial piezometric head values. Many of the piezometers installed during July and August are still dropping slightly, and appear to be slowly stabilizing. The slow response in some of the standpipe piezometers is not surprising considering the low permeability of the siltstone and claystone (approx. 10⁻⁸ cm/sec.). Figure A5-1 shows hydrographs of piezometers in two holes, (DDH 76-801 and 76-805), which illustrate the response curves experienced in different areas with different piezometer types. The standpipe piezometer in

A5-88

DDH 76-801 is located in siltstone on the southeastern pit perimeter, and the hydrograph shows a gradual decline of the water level in the standpipe. The two pneumatic piezometers in DDH 76-805 showed significant changes during the same period, thus demonstrating the sensitivity of these piezometers in low permeability sediments.

A regular monthly monitoring program for all piezometers has been recommended by GA, and it is being carried out by DCA for BCH. This program should be continued.



IV) Report on Chemical Analysis of Water Samples

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IV) CANTEST LIMITED REPORT ON THE INORGANIC CHEMICAL ANALYSIS OF WATER SAMPLES

Five water samples were collected from creeks, springs and the pump test well and were submitted to Cantest Limited for inorganic chemical analyses. Their report is attached, and the following sampling sites correspond with the sampling numbers given:

GA Sample No.	Sample Site
76-1	Aleece Creek: 2,000 ft. from lake outlet
76-2	Spring: on south shore of Aleece Lake
76 - 3	Aleece Lake: at 2 ft. depth near outlet
76-4	Well RH 76-19: during development
76-5	Hat Creek: near borehole RH 76-20
76-6	Well RH 76-19: at end of pump test

These data are summarized along with isotope data in Table 3 in the Main Report.



1860 PANDORA STREET, VANCOUVER, B.C. VOL 116 . TELEPHONE 264-7278 . TELEX 04-64210

Report On Water Samples for Chemical Analysis	File No. 4780 B
	Report No
Reported to Golder Associates,	Date Nov. 9, 1976
Consulting Geotechnical Engineers,	Atten: R. Allan Dakin
224 W. 8th Avenue,	Re: Hat Creek Project
Vancouver, B.C.	

We have tested the samples of water submitted by you on October 22, 1976 and report as follows:

SAMPLE IDENTIFICATION:

The samples were submitted in plastic bottles labelled -

- Aleece Creek - 76 - 1 76 - 3 76 - 4 76 - 5 76 - 6

METHOD OF TESTING:

The samples were tested in accordance with the procedures set down in "Standard Methods for the Examination of Water and Wastewater" - 13th Edition, published by the American Public Health Association, 1975. Some of the samples were small, and for this reason Calcium, Magnesium, and Sodium were analysed by Plasma Spectroscopy rather than traditional methods.

RESULTS OF TESTING:

(on following page)

CAN TEST LTD.

Page 2 File No. 4780 B Nov. 9, 1976.

RESULTS OF TESTING:

<u>Test Parameter</u>	<u>76 - 1</u>	<u>76 - 3</u>	<u>76 - 4</u>	<u>76 - 5</u>
pH Conductivity	7.85 508.	7.60 508.	7.60 677.	8.0 462 micromhos cm
Dissolved Cations Calcium Magnesium Sodium Potassium Iron	Ca ^{**} 44.8 Mg 21.7 Na 33.0 K 9.0 Fe -	33.9 25.2 38.0 11.5 L 0.05	19.0 9.4 110. 18.0	58.0 ppm 17.1 ppm 21.3 ppm 4.0 ppm - ppm
Dissolved Anions Bicarbonates Sulfate Chloride	HCO - SO ₄ - C1 ⁴ -	265. 52.2 L 0.5	260. 47.7 L 0.5	- ppm - ppm - ppm
Total Hardness	CaCO ₃ 201.	188.	86.0	214. ppm

(con't on following page)

RESULTS OF TESTING:

76 - 6

pH Conductivity Total Hardness	CaCO3	183 20	7.60 34. 08.	micromhos/cm ppm
Dissolved Anions Alkalinity Bicarbonates Carbonates Hydroxyl lon Chlorides Sulfates Nitrates Nitrites Phosphates Fluoride	HCO ₃ CO ₃ OH ³ C1 SO ₄ N PO ₄ F			ppm ppm ppm ppm ppm ppm ppm ppm
Dissolved Cations Calcium Magnesium Potassium Sodium Iron Aluminum Arsenic Cadmium Chromium Chromium Copper Mercury Lead Zinc Boron Selenium Strontium Lithium Vanadium	Ca Mg K Na Fe Al As Cd Cr Cu Hg Pb Zn B Se Sr L V	33 L L L L L L	47.7 21.6 34.0 30. 0.05 0.004 0.005 0.001 0.001 0.007 0.0002 0.020 1.97 0.1 0.004 0.06 0.05 0.10	ppm ppm ppm ppm ppm ppm ppm ppm ppm ppm
Total Kjeldahl Nitrogen Total Dissolved Solids		2 1 6 0	22.2 D0.	ppm
Fixed Volatile L - less than		140 20 CAN TEST LT	00.	
		CAN TEST LI	LU.,	

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A. W. Maynard,MSc Chemist.

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APPENDIX 6

PUMP TEST REPORT FOR BOREHOLE RH 76-19

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APPENDIX 6

PUMP TEST REPORT FOR BOREHOLE RH 76-19

LOCATION AND CONSTRUCTION OF TEST WELL AND OBSERVATION PIEZOMETERS

A 23-day pumping test was carried out on borehole RH 76-19 which is located slightly south of the middle of the proposed pit, see Drawing 6 (main text). The hole was constructed by first drilling and casing a 12-inch diameter hole to a depth of 145 ft. and then drilling an open hole to 400 ft. depth. The hole was drilled using a rotary drilling rig with an air-flush system. An 8inch steel casing, which had perforations cut into the lower 255 ft., was then set into the hole and the annular space was backfilled with pea-gravel (see details in the Hydrologic Log for borehole RH 76-19 in Appendix 5). The completed hole was surged with air for about 3 days until the formation material had stabilized. Four observation holes were drilled within a radius of 360 ft. of this pump well, were completed at depths of about 400 ft. using biodegradable mud, and up to three piezometers were installed in each hole (see construction details, Appendix 5).

GEOLOGY AND HYDROLOGY OF TEST SITE

The pumped well (RH 76-19) was drilled into the upper claystone-siltstone member of the Coldwater Formation (see Drawing A6-1). The surficial deposits at the site were about 100 ft. thick and were comprised of till with minor inter-beds of sand and gravel. These surficial deposits were cased off to prevent vertical seepage into the well. The well screen (i.e. slotted portion of 8-inch casing) penetrated about half of the siltstone-claystone aquifer unit (see Section B-B, Drawing A6-1). This aquifer is not areally extensive as it is shaped like a

A6-1

narrow trough approximately 1,000 ft. wide and running parallel to the axis of Hat Creek. This trough rests on top of a folded 700 ft. thick layer of coal (see Sections A-A and B-B, Drawing A6-1).

An examination of the piezometric heads in the aquifer prior to the start of the pump test show the following:

- a) the piezometric heads are generally about 50-90 ft. below ground level (i.e. in the till above the Coldwater Formation) and hence the till could be acting as a confining layer for ground water in the Coldwater Formation.
- b) the sand and gravel layer around RH 76-18 is a source of local recharge to the Coldwater Formation. This is not surprising as flows of about 60 gpm were encountered while drilling this borehole.
- c) the ground water generally flows downwards and follows the general slope of the topography, except in the area of RH 76-18 where local recharge disturbs this pattern.

PUMP TEST PROCEDURE

A small (1 h.p.) submersible pump was set in the 8-inch well to a depth of 380 ft. below ground. In order to reduce the water flows and line pressures at the ground surface, a small pipe-tee with an orifice plate was installed in the drop pipe just above the submersible pump. This allowed some water to escape back into the well, and hence reduced the line pressures. The water discharge from the well was controlled by means of a small needle valve.

In order to ensure that no water could seep back into the ground the pumped water was directed into a large mud pit. The pump test was started on

September 22, 1976 and the initial pumping rate was I gpm for the first three hours. The test had to be suspended for 19 hours while a malfunctioning generator was repaired and then the | gpm pumping rate was resumed. As very little recovery had been recorded in either the well or the observation piezometers, the effects of the suspension in pumping was small in relation to the length of the test that was carried out. After two days the pumping rate was reduced to 0.5 gpm, on the 3rd day the rate was reduced again to 0.1 gpm and this pumping rate was maintained for the remainder of the 23-day test. While the pump test was running, water levels and pneumatic pressures were read in the pumped well and in the piezometers around the well (see list of all measurements in pump test data summary in this appendix). In addition samples of the water pumped from the well were collected at the start and at the end of the pump test. These samples were sent for chemical and isotope analyses (see summary of results in Table 3 of the main report). Water temperatures and the electrical conductivity of the pumped water were measured at intermittent intervals during the pumping test (see data given in remarks column of pump test data summary in this appendix).

At the end of the test the pump was turned off and the response in the piezometers were monitored. An automatic water level recorder was installed in standpipe piezometer DDH 76-149-1.

ANALYSIS OF PUMP TEST DATA

The water level and pneumatic pressure readings were converted to piezometric elevations and drawdown, and are shown plotted in Figures A6-1 and A6-2. These figures show that the piezometric levels in the pumped well and the piezometers responded very rapidly at the start of the test, but after about 6 days of pumping most piezometers had stabilized and remained relatively stable for the remainder of the test.

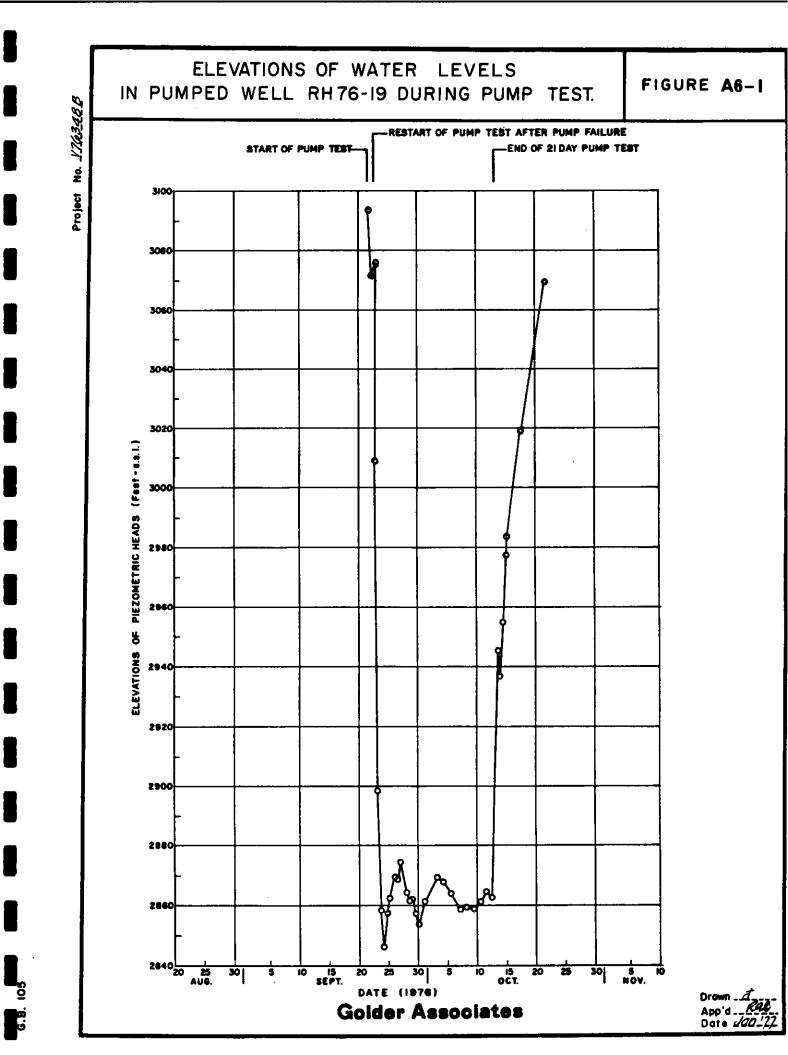
Log-log graphs of drawdown versus time since pumping started were plotted for all piezometers and type curves were constructed so that hydrogeologic parameters, transmissivity and storage coefficients could be calculated. The type curves were constructed by modifying the standard Theis curve to account for the following:

- 1) partial penetration of the aquifer (Walton, 1972 p. 215);*
- 2) aquifer anisotropy: vertical permeability (k_v) to horizontal permeability k_h ratio is assumed to be 1:10 (Boulton and Streltsova, 1976);
- 3) large diameter of well relative to pumping rate (Boulton and Streltsova, 1976);
- 4) leakage of water from more permeable sand and gravel zones in the surficial till unit above the aquifer (Walton, 1972, p. 217).

Examples of plotted data and calculations using the modified type curve are given in pump test data summary sheets for plezometers RH 76-17-1, RH 76-18-2, DDH 76-149-1 and DDH 76-149-2. A summary of the results of calculations for all plezometers are given in Table A6-1. Similar type curves were used to calculate parameters from log-log distance-drawdown plots. These type curves incorporated the modifications previously described. The results of these calculations are shown in Table A6-2 for the periods 12 days and 23 days after the test started.

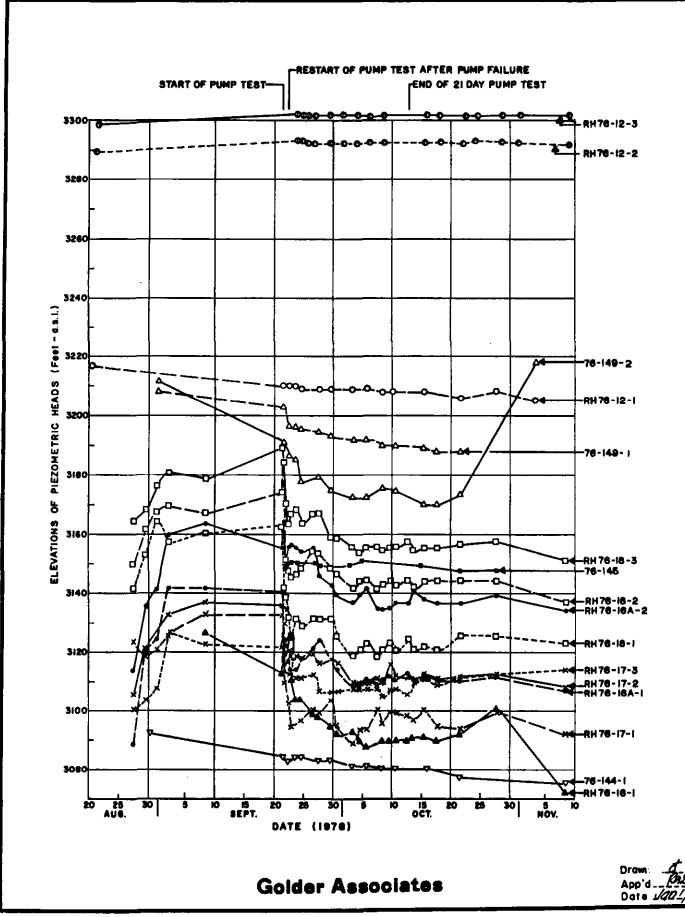
Because of the large diameter of the pumped well relative to the aquifer permeability, the recovery method of aquifer analysis (Walton, 1972) would not be easy to analyze and hence was not used.

*See List of References and Glossary in Section 9. of the main text.



ELEVATIONS OF PIEZOMETRIC HEADS IN OBSERVATION HOLES : BEFORE, DURING AND SUBSEQUENT TO PUMPING TEST OF RH76-19.

FIGURE A6-2



Project No. 1/2639,88

DISCUSSION OF RESULTS

- 1) The calculated aquifer transmissivity ("T") of the siltstoneclaystone aquifer ranges between 0.20-1.15 gpd/ft. and averages 0.7 gpd/ft. for the piezometers around the well (Table A6-1). If we assume that the average aquifer thickness is about 600 ft., then the calculated horizontal permeability of the aquifer would be 5.3 x 10^{-8} cm/sec. This figure is in reasonable agreement with the permeability figures determined using the falling head method in standpipe piezometers, see Table A5-1. For example in piezometer RH 76-12-1 which is located 1,400 ft. from the pumped well the calculated permeability is k = 1.2×10^{-8} cm/sec.
- 2) The calculated storage coefficients (S) ranged from 0.21×10^{-7} to 9×10^{-7} and averaged 4×10^{-7} for the piezometers around the well (Table A6-1). Assuming a 600 ft. aquifer thickness the average specific storage (see Glossary) would be $4 \times 10^{-7}/600 = 6.7 \times 10^{-10}$ ft⁻¹ = 2.2×10^{-11} cm⁻¹.
- 3) The pump test showed that ground water in the sands and gravels in the till above the aquifer was recharging water to the siltstone-claystone aquifer. Evidence for this was observed in both the piezometric head pattern near the well (see Section A-A, Drawing A6-1) and in the response shown in piezometer DDH 76-149-2. This latter piezometer is located in the till and showed a 25-ft. decline in piezometric head during the pump test.
- 4) The pump test showed that there is a hydraulic connection between the A-zone coal, B-zone coal and sandstone-siltstone unit below. This statement is based on observations in piezometers DDH 76-149-1 and DDH 76-144-1 which both show a response as a result of pumping well RH 76-19.

5) The more permeable coal ($k = 10^{-4}$ cm/sec.) zones are sufficiently far from the well to have no influence on the calculations for transmissivity.

CONCLUSIONS

- The pump test has shown that some depressurization had taken place in the sediments around the pump test site.
- 2) The siltstone-claystone (Coldwater Formation) sediments have a permeability of about 10^{-8} cm/sec. and specific storage of about 2×10^{-11} cm⁻¹.
- 3) The test demonstrated that the surficial deposits are recharging the Coldwater Formation and that it will be essential to dewater these surficial deposits before the siltstone can be effectively depressurized.

TABLE A6-1

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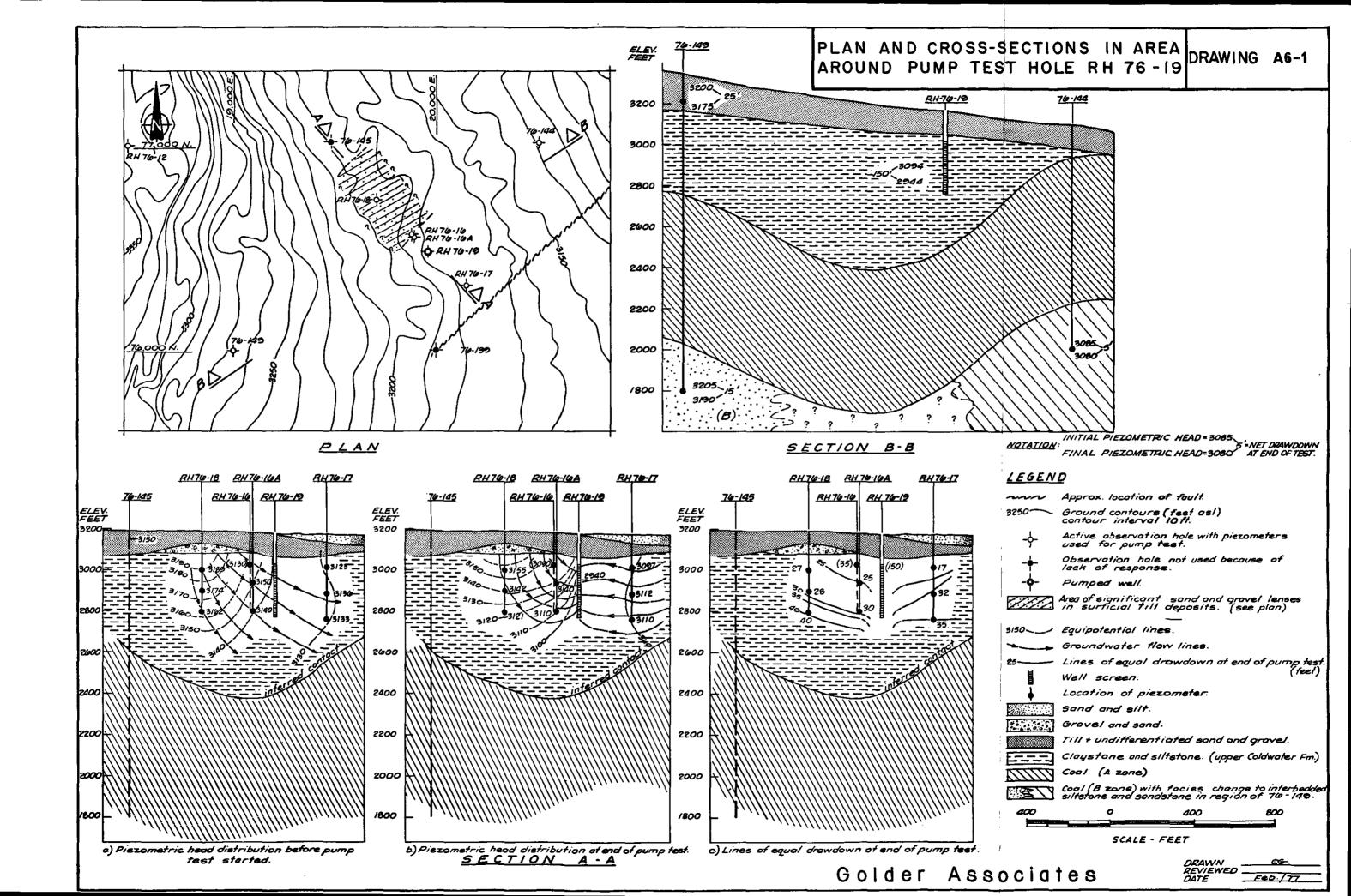
		Aguife	Aquifer Parameter				
Observation	Distance From		Storage Coefficient				
Point	Pumped <u>Well (ft)</u>	_T (gpd/ft)	5×10^{-7}				
RH 16A-1	105	0.21	5.3				
RH 16A-2	105	0,20	6				
RH 16-1	115	0.7	2				
RH 17-1	249	0.64	0.35				
RH 17-2	249	1.04	1.13				
RH 17-3	249	0.76	9				
RH 18-1	357	0.76	0.21				
RH 18-2	357	0.96	0.28				
RH 18-3	357	1.15	0.67				
Average		0.71	4.1				
DDH 144-1	760	1.15	0.66				
DDH 149-1	1080	0.5	0.52				
DDH 149-1	1080	0.5	0.52				
DDH 149-2	1080	0.29	0.91				

HYDROGEOLOGIC PARAMETERS CALCULATED FROM TIME-DRAWDOWN CURVES

TABLE A6-2

HYDROGEOLOGIC PARAMETERS CALCULATED FROM DISTANCE-DRAWDOWN CURVES

Time Since Pumping	Aquifer	Parameter
Started (days)	Transmissivity T gpd/ft.	Storage Coefficient S
12	0.2	2×10 ⁻⁵
23	0.13	7.8×10 ⁻⁶



P D D D D	umi AT/ atu ept	ned A O m p h to	T Well N OBSERV oint static wate	Hot Cree Cache Cree RH 76 ATION PO Top of	INT:		Type:	D Screen Unscr vation_ static_w	Observations in RH_76-12-1 Sheet 1 Sheet 1 Of 1 ATE: StartSept.22,1976 Finish_Oct.14,1976 med well Pneumatic piezo sened well X Standpipe piezo 3346 FT- ater level_3210 FT- aned intervaltoa.s.1
W	'ell 'ell	depi diar		400 feet Binches ctric Subr	ND AQUIFE	_	Aquifer thi	scription ickness. ump suc	Coldwater Fm (Siltstone) 800 feet 10n370 feet 570
	łm		Elapsed Time "t" (mins.)		Pressure (Pneumatic piezometers only)	Water (ft.)	Drawdown (ft.)	Pump Rate Q (i.g.p.m)	Remarks
-	_	Min.			(p.s.i)	a.s.l.			
		00		136.1	<u> </u>	3209.9	-		
		00 20	0	-	 	[-		Pump started
23		30 30	1170 2850	136.4		3209.6 3209.6	7.4		
24 25		<u> </u>	4200	136.4		3209.6	7.6		
22 28	-		8550	136.7		3209.4	7.0		· · · · · · · · · · · · · · · · · · ·
30			11400	130.7		3209.5	8.0	ļ	
4		30	16890	137.2		3208.8	8.2		
6		F	20220	137.3		3208.7	8.3	<u> </u>	
	_	00	24120	138		3208	9.0		
11			27300	138		3208	9.0		L
14			31871	-	······	-	-		Pump stopped
16		00		138.1		3207.9	9.1		
		20		-	1	-	-		
22				141.9		3204.1	12.9		
28	5	30		138.2		3207.8	9.2		
10	5	30		1 39		3207.0	10.0		·
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F	, n wi	ped	T	Hat Cree Cache Cre RH 76				D	Observations in <u>RH_76-12-2</u> Sheetof ATE: StartSept.22,1976 FinishOct.14,1976 hed wellPneumatic pie
0	atu ept	m p h to	N OBSERV Dint static wate /open hole				Type: Datum elev Elevation	Unscri ation_ static_w	sened well X Standpipe pie 3346 FT 0.1 rater level 3201 FT 0.1 aned interval to 0.1
- V - V - V	/ell Veli	depi dian	······	400 fee 8 inches ctric Subi	ND AQUIFE		Aquifer thi	ickness. ump suc	confined unconfined Coldwater Fm (Siltstone) 800 feet tion370 feet Z constant rate step drawdown
	'im	e Min	Elapsed Time "t" (mins.)	Depth to Water (ft.)	Pressure (Pneumatic piezometers only) { p.s.i }		Drawdown (ft.)	Pump Rate Q (ig.p.m)	Remarks
		╞═╡		52.2	(p.s.i)				
		00 00	0	53.3	<u> </u>	3292.7	-		Dump stanted
		00 30		- 52.0	i	- 3294			Pump started
		30 30		52.6	<u> </u>	3293.4	3.0		
_		00	4200	52.0		3293.5	2.4		
		30		52.5		3293.5	2.5		
20 30		00	11400	52.5	<u> </u>		2.5		
30 4	_	30		52.4		3293.5	2.5		
6		00	20220	52.6		3293.6 3293.4	2.0	· · · · <u>-</u>	
		00	24120		<u> </u>		-		
	L	00							
		11	31871	-					Pump stopped
16	-	00		52.5		3293.5	2.5		
_		20	<u></u>	-		-	-		
	15			52.6		3293.4	2.4		
	15			52.4	<u> </u>	3293.6	2.6	ļ	
		30		52.9		3293.1	2.1		
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		┝╴┨							
		┝──┨						<u> </u>	
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F L	PRO .ecc Pum	JEC ition ped		Hot Cree	DATA S k Coal bek, Ø.C.			1	Observations in_RH_76-12-3 Sheet ATE: StartSept. 22, 1976 FinishOct. 14, 1976
0)atu)ept	m po h to	static wat	Top of	INT : tube 46 FT.	~ ~ ~	Type: Datum elev Elevation	Unscre tion_ static_w	ned well Pneumatic piez sened well X Standpipe piez 3346 FT,
V V	Veli Veli	depi dian		400 fee 8 inches ctric Subi	nD AQUIFE	_	Aquifer Co Aquifer det Aquifer thi Depth to p Type of te	cription ckness_ ump_suc	Coldwater Fm (Siltstone) 800 feet 10n 370 feet 370 feet 10n 510 constant rate 10 step drawdown
	im Hr.	e Min.	Elapsed Time "t" (mins.)	Depth to Water (ft.)	Pressure (Pneumatic plezometers only) (p.s.l)		Drawdøwn (ft.)	Pump Rate Q (i.g.p.m)	Remarks
-	_	00	0	44.2		3301.8			
		00	0			-	-		Pump started
23	11	30	1170	43.5	<u> </u>	3302.5	2.5		
24	15	30	2850	43.6	·	3302.4	2.4	·	· · · · · · · · · · · · · · · · · · ·
25	14	00	4200	43.5		3302.5	2.5		
28	14	30	8550	43.6		3302.4	2.4		
30	14	00	11400	43.6		3302.4	2.4		
4		30		43.5	•	3302.5	2.5		
6	17	00	20220	43.8		3302.2	2.2		
-		00	24120	-		-	-		
	_	00	27300	-			-		
-	19		31871	-		-	-		Pump stopped
	11		<u> </u>	43.8	 	3302.2	2.2		· · · · · · · · · · · · · · · · · · ·
		20		-		-		ļ 	
	15			43.8	<u> </u>	3302.2	2.2		
	15			43.8	·	3302.2	2.2		
10	15	30		44.0	ļ	3302	2.0		
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F	PROJE ocati	ст_			DATA S k Cool ek, B.C.			I	Observations in RH 76-16 Sheet 1 of 2 ATE: Start Sept 22,1976 Finish Oct.14,1976
	DATA Datum Depth	ON poin to st	OBSERV t atic_wate	ATION POI	INT:		Elevation	Unscri ation_ static_w	ned well X Pneumatic piez sened well Standpipe piez 31P2-1 FT. 0. 8. ater level 0. 8. ened interval 0. 8.
v v	Vell de Vell di	opth amet	er Eie	400 feet	nersible		Aquifer thi	ickness_ ump_suc	Coldwater Fm (Siltstone) 800 feet tion370 feet Z constant rate step drawdown
	⊺ime Hr.M	, ,	lapsed Time "†" mins.)	Depth to Water (ft.)	Pressure (Pneumatic piezometers only)	Elevation of Water (ft.)	Drawdown (ft.)	Pump Rate Q (i.g.p.m)	Remarks
_	9 0				(p.s.i)	a.s.i.		<u> </u>	
44	160		0		38	3126.1	-		Durning stant-d
	163		30	48.4	47	-			Pumping started
	190		180	60.0	47	3133.7 3122.1	4.0		
22	113		1170	57.7	42	3124.4	1.7		
2) 	193		1650	71.5	43 37	3110.6	15.5		
24	153		2850	78.5	34	3103.6	22.5		
	133		4170	78.5	34	3103.6	22.5		
	140		7080	83.1	32	3099.0	27.1		
	143		8550	89.2	-	2097.9	28.2		
	140		1400	87.7	30	3094.4	31.7		
1	154	_	2945	90.0	29	3092.1	34.0		· · · · · · · · · · · · · · · · · · ·
4	9 3		6890	90.0	29	3092.1	34.0		
5	130	-	8540	92.3	25	3089.8	36.3		
6	170		0220	94.6	23	3087.5	38.6	L	
8	110		2840	-		-	-		
9	9 0		4060	92.3	28	3089.8	36.3		
10			5890	92.3	28	3089.8	36.3		
11	150		7300	92.3	28	3089.8	36.3		
13			0120	92.3	28	3089.8	36.3		
	173		1770	91.2	28.5	3090.9	35.2		Pumping stopped (19:11)
	1111	_		91.2	28.5	3090.9	35.2		
	160			92.3	28	3089.8	36.3		
22	153	1		90.0	29	3092.1	34.0		
28	153	, 		80.8	33	3101.3	24.8	-·	· · · · · · · · · · · · · · · · · · ·

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L	oca	tion	THot	Creek Co e Creek, E			<u>KY</u> 	l	Observations in <u>RH 76-16</u> <u>Sheet</u> <u>2</u> of <u>2</u> DATE: <u>Start Sept. 22, 1976</u> Finish Oct. 14, 1976				
	ime	1	Elapsed Time "t" (mins.)	Depth to Water (fl.)	Pressure (Pneumatic piezometers only) (p.s.i)	Elevation of	Drawdown (ft.)	Pump Rate Q (i.g.p.m	Remarks				
10	15	30		109.6	20.5	3024.1	53.6						
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-				<u> </u>									
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f L F	PRO Loca Pumj	JEC tion		Hot Cree	DATA S k Coal ek, B.C.			L	Observations in <u>RH</u> 76-16 Sheet <u>1</u> of <u>2</u> ATE: Start Sept. 22, 1976 Finish Oct. 14, 1976
C C S	Datu Dept Screi	m p h to sned,	/open hole i	Top_of er level interval	tube 40.6 FT	 	Elevation	Unscr ution_ static_w	hed well X Pneumatic pie eened well Standpipe pie 3182,1 FT. ater ievel 3141,5 a. ened interval to a.
v	Voli Veli	dept dian	ih	400 fee 8 inches ctric Subi			Aguifer thi	ickness_ ump_suc	Coldwater Fm (Siltstone) BOO feet tion370 feet J constant rate step drawdown
	rim:		Elapsed Time "t" (mins.)	Depth to Water (fl.)	Pressure (Pneumatic piezometers only)	(11.)	Drawdown (ft.)	Pump Rate Q (i.g.p.m)	Remarks
_	Hr.				(p.s.i)	a.s.l.			
22	9		0	41.5	150	3140.6			
	16		0	10.5	-	-	-		Pumping started
	16		30	40.3	150.5	3141.8	0		
	19		180	66.9	139	3115.2	26.3		
23	11	-	1180	64.6	140	3117.5	24.0		
		30 20	1650	68.1	138.5	3114.0	27.5		
	15		2850	68.1	138.5	3114.0	27.5		· · · · · · · · · · · · · · · · · · ·
_	13		4170 7080	64.6 61.1	140	3117.5	24.0		
_	14				141.5	3121.0	20.5		
	14		8550 11400	58.8	142.5	3123.3	18.2	· 	· · · · · · · · · · · · · · · · · · ·
30			12945	64.6 68.1	140	3117.5 3114.0	24.0	<u> </u>	
4	15 9		16890	73.8	138.5 136	[27.5		
+ 5	9 13	30	18540	73.8	136	3108.3 3108.3	33.2		·
		00	20220	71.5	130	3110.6	33.2 30.9		· · · · · · · · · · · · · · · · · · ·
8	/ 11		20220	73.8	137	3108.3	33.2		,
		00	24060	71.5	138	3110.6	30.9		
	-		25890	70.4	137.5	3111.7	29.8		
			27300	71.5	137.5	3110.6	30.9	·	
	14		30120	69.2	138	3112.9	28.6		· · · · · · · · · · · · · · · · · · ·
	17		31770	71.5	137	3110.6	30.9		Pump stopped (19:11)
	11			70.4	137.5	3111.7	29.8	· · · · · · · · · · · · · · · · · · ·	- and acobles (13111)
	16			71.5	137	3110.6	30.9		· · · · ·
	15			71.5	137	3110.6	30.9		
_		30							

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FL	PRO .occ	JEC ped	T Hat	Creek Co he Creek, E	DATA S		<u>RY</u>		Observations in RH 76-161-1 Sheet of _2 DATE: Start_Sept. 22, 1976 Finish_Oct. 14, 1976				
	im Hr.	e Min.	Elopsed Time "t" (mins.)	Depth to Water (tt.)	Pressure (Pneumatic piezometers only) (p.s.i)	Elevation of Water (ft.) a.s.t.	Drawdown	Pump Rate Q (i.g.p.m)	Remark s				
10	5	30		75	135.5	3107.1	34.4						
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		$\left \right $			<u></u>	<u> </u>							
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P	RO	JEC.			DATA S k Coal ek, B.C.				Observations in <u>RH 76-16</u> Sheet <u>I</u> of <u>2</u>
L P	.oca 'umi	ition ped	Well	RH 76	-19			D	ATE: StartSept. 22, 1976 FinishOct. 14, 1976
0	atu ept	m pi h to	N OBSERV pint static wat	ATION PO Top of er levei	INT:		Type: Datum elev Elevation	Unscri ation_ static_w	ned well
N N	Yeli Yeli	dept dian	h	400 feet Binches ctric Subr	AQUIFE		Aduiter thi	scription lokness_ ump_suc	Coldwater Fm (Silfstone) 800 feet 110n370 feet 21 constant rate 31 step drawdowi
T	'im		Etapsed Time "t" (mins.)	Depth to Water (fl.)	Pressure (Pneumatic piezometers only) (p.s.l)	Elevation of Water (ft.) a.s.l.	Drawdown (ft.)	Pump Rate Q (i.g.p.m)	Remarks
22		00	0	26.9	94	3155.2			
		00	-	-	-	-	_		Pumping started
		30	30	17.6	98	3164.5			
		00	180	33.8	91	3148.3	15.2		
	11		1170	26.9	94	3155.2	8.3		
_	19	30	1650	25.7	94.5	3156.4	7.1		
	15	30	2850	26.9	94	3155.2	8.3		
	13		4170	28.0	93.5	3154.1	9.4		
27	14	00	7080	26.9	94	3155.2	8.3		
28	14	30	8550	36.1	90	3146.0	17.5		
30	14	00	11400	39.6	88.5	3142.5	21.0		· · · · · · · · · · · · · · · · · · ·
T	15	45	12945	43.0	87	3139.1	24.4		
4	9	30	16890	45.3	86	3136.8	26.7		
5	13	00	18540	43.0	87	3139.1	24.4		
6	17	00	20220	40.7	88	3141.4	22.1		· · · · · · · · · · · · · · · · · · ·
8	11	00	22740	47.6	85	3134.5	29.0		
	9	00	24060	47.6	85	3134.5	29.0		-
		30	25890	47.6	85	3134.5	29.0		
		00	27300	45.3	86	3136.8	26.7		
		00	30120	45.3	86	3136.8	26.7		•
		30	31770	41.9	87.5	3140.2	23.3		Pumping stopped (19:11
		15		44.2	86.5	3137.9	25.6		
		00		45.3	86	3136.8	26.7		
		30		45.3	86	3136.8	26.7		
28	15	30		43.0	87	3139.1	24.4		

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F	R0.	JEC tion	T Hat T Cad WellRH	Creek Co ne Creek, E					Observations in <u>RH</u> 76-16 Sheet 2 of 2 ATE: Start <u>Sept. 22, 1976</u> Finish Oct. 14, 1976
т	im		Elapsed Time "t" (mins.)	Depth to Water (ft.)	Pressure (Pneumotic piezometers only) (p.s.1)		Drawdown (ft.)	Pump	Remarks
10	15	30		47.6	85	3134.5	29.0		
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F	PRO	JEC		Hot Cree Coche Cre	DATA S k Cogi ek, <u>B.C.</u>			L	Observations in RH 17-1 Sheet 1 of 3 ATE: Start Sept. 22, 1976 Finish Oct. 14, 1976
)AT/)otu)ept	n pi h to	N OBSERV	ATION PO Top of			Elevation	Unscru ration static_w	rinish ed well Pneumatic piez pened well Standpipe piez 3179 FT G. s ater level3132.5 FT G. s ined interval to G. s
- - -	Vell Vell	dept dian		400 feet 8 inches ctric Subr	nersible		Aquifer Co Aquifer des Aquifer thi Depth to p Type of te	scription ickness_ ump_suci	Image: Constant rate Image: Constant rate Image: Constant rate Image: Constant rate
1	r I m		Elapsed Time "t" (mins.)	Depth to Water (ft.)	Pressure (Pneumatic piezometers only) (p.s.l)	Elevation of Water (ft.) a.s.l.	Drawdown (ft.)	Pump Rate Q (igp.m)	Remark s
22	9 9	00	0	46.3	154	3132.7			
-	16	┢╍╼┿	0		-	<u> </u>	-		Pump started .
	16	30	30	55.5	150	3123.5	0		······································
	19	00	180	69.4	144	3109.6	22.9		Pump stopped @ 150 mins.
23	11	30	1170	76.3	141	3102.7	29.8		
	19	30	1650	84.4	137.5	2094.6	37.9		Pump restarted @ 1290
24	15	30	2850	75.1	141.5	3103.9	28.6		
25	13	30	4170	82.1	138.5	3096.9	35.6		
		00	7080	78.6	140	3100.4	32.1		
28	14	30	8550	79.8	139.5	3099.2	33.3		
30	14	00	11400	75.1	141.5	3103.9	28.6		
1	15	45	12945	84.4	137.5	3094.6	37.9		
4	9	30	16890	90.1	135	3088.9	43.6		
	13		18540	85.5	137	3093.5	39.0		
	17		20220	85.5	137	3093.5	39.0		
	11		22740	78.6	140	3100.4	32.1		
9		00	24060	83.2	138	3095.8	36.7		
	15		25890	79.8	139.5	3099.2	33.3		
	15		27300	79.8	139.5	3099.2	33.3		·
	14		30120	80.9	139	3098.1	34.4		•
	17		31770	82.1	L	3096.9	35.6		Pump stopped (19:11)
	11			88.6	140	3100.4	32.1		
	16			84.4	137.5	3094.6	37.9		
	15			85.5	137	3093.5	39.0		
28	15	30		79.8	139.5	3099.2	33.3		

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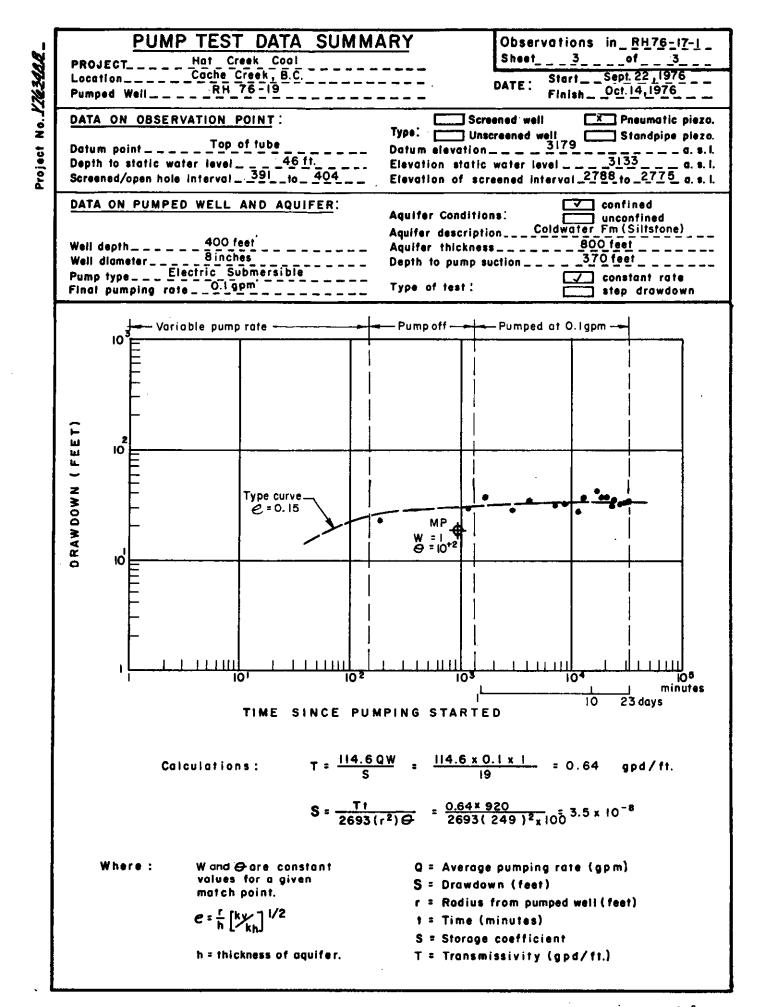
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P	RO	JEC	<u>FUNP</u> THot Cod	TEST Creek Con		Observations inRH_17-1 Sheet2of3 DATE: Start_Sept. 22, 1976				
P	'um; 'um; 'im;	bed 	WellRH Elapsed Time	76-19 Depth to	Pressure (Pneumatic	Elevation of	Drawdown	Pump	ATE: Finish Oct. 14, 1976	
		Min.	"1" (mins.)	Water (ft.)	piezomaters only) (p.s.i)			Q (i.g.p.m)	Remarks	
10	15	30		86.7	136.5	3092.5	40.2			
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F	PR0	JEC' ation	T	Hat Cree Cache Cre	DATA S				Observations in <u>RH 17-2</u> Sheet Jot <u>2</u> ATE: Start Sept 22,1976 Oct.14,1976
P	2 Vm	ped	Well	RH 76	-19			D	ATE: Finish_ Oct. 14, 1976
0)atu)epi	m po h to					Datum elev Elevation	Unscre dion static_w	ned well X Pneumotic pi bened well Standpipe pi 3179 FT a. ater level <u>3136 FT_s</u> a. aned intervalto a.
V V V	Vell Veli	dept dian		400 feet Binches ctric Subr	ID AQUIFE		Aquifer thi	cription ckness_ ump_suci	Coldwater Fm (Siltstone) 800 feet ion370 feet Constant rate step drawdowr
1	r i m		Elapsed Time "t" (mins.)	Depth to Water (ft.)	Pressure (Pneumotic piezometers only)	(ft.)	Drawdown (ft.)	Pump Rate Q (i.g.p.m)	Remarks
-		╞──╞			(p.s.l)	a.s.l.			
22	F	00	0	43.2	102.5	3135.8	 		· · · · · · · · · · · · · · · · · · ·
		00	0	-		-			Pump started
		30	30	44.4	102	3134.6	8.4		
	-	00	180	60.5	95	3118.5	24.5		
	<u> </u>	30	1170	58.2	96	3120.8	22.2		
		30	1650	60.5	95	3118.5	24.5		
		30	2850	60.5	95	3118.5	24.5		· · · · · · · · · · · · · · · · · · ·
	_	30 00	4170	61.7	94.5	3117.3	25.7		<u> </u>
		30	8550	59.4	95.5	3119.6	23.4		
		00	11400	62.9	94	3116.1	26.9		
_		45	12945	61.7	94.5	3117.3	25.7		
4		30	16890	62.9	94	3116.1	26.9		· · · · · · · · · · · · · · · · · · ·
		00	18540	69.8	91	3109.2	33.8		
		╞╍╍┠		69.8	91	3109.2	33.8		
ь 8		00 00	20220 22740	69.8	91	3109.2	33.8	<u> </u>	
_		00	24060	67.5	92	3111.5	31.5	L	
9 10		30	25890	69.8 62.9	91 94	3109.2	33.8		
		00	27300			3116.1	26.9		
		00	30120	67.5	92	3111.5	31.5		· · · · · · · · · · · · · · · · · · ·
		30	31770	67.5 67.5	92 92	3111.5	31.5		Dump storred (10-11)
		15	<u> </u>	66.3	92.5	3111.5 3112.7	31.5 30.3		Pump stopped (19:11)
		00		68.6	92.5	3110.4	32.6		
		30		67.5	91.5	3111.5	31.5		
		30		66.3	72		21+2		

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F	RO	JEC	T Hat	Creek Co				Į	Observations in_RH_17-2 Sheet2of2 of2 ATE: Start_Sept. 22, 1976 Start_Sept. 24, 1976
P	.0¢a 1001	tior bed	Well RH	76 - 19	········			C	DATE: Finish_Oct. 14, 1976_
т	im	•	Elapsed Time "t" (mins.)	Depth to Water (ft.)	Pressure (Pneumatic piezometers only)	Elevation of Water (ft.)	Drawdown	Pump Rate Q (i.g.p.m)	Remarks
-		Min.			(p.s.i)	a.s.l.		 	
10	15	30		70.9	90.5	3108.1	34.9		
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F	RO	JEC			DATA S			L	Observations in RH 76-17-3 Sheet 1 of 2 ATE: Start Sept. 22,1976
	.oca 'ump	rion Ied	Well	RH 76	-19			D	ATE: StartSept. 22,1970 FinishOct. 14,1976
			N OBSERV		,		<u> </u>		ned well T Pneumatic piezo
	atu epfi	m po n to	oint static wate	Top_of			Elevation	Unscr ation_ static_w	aened well \Box Standpipe pleza $3179 \text{ FT}_{\bullet}$ a, s, s, s ater level $3122 \cdot 5 \text{ FT}_{\bullet}$ a, s, s ined interval $-2122 \cdot 5 \text{ FT}_{\bullet}$ a, s, s
	/eli Veli	depi dian	h	400 feet Binches			Aquifer thi	scription ickness_ ump_suc	Coldwater Fm (Silfstone) 800 feet ion 370 feet 2 constant rate 3 step drawdown
	'im		Elapsed Time "t"	Depth to Water (ft.)	Pressure (Pneumatic piezometers	Elevation of Water (fl.)	Drawdown (ft.)	Pump	Remarks
Dy.	Hr.	Min.	(mins.)	(16.)	only) (p.s.i)	d.s.l.	(11.)	(rgpar)	
22	9	00	0	57.4	47	3121.6			
	16	00	0		-	-	-		Pump started
	16	30	30	49.3	50.5	3129.7	-		
	19	00	1 80	66.7	43	3112.3	10.2		
23	11	30	1170	66.7	43	3112.3	10.2		
	19	30	1650	66.7	43	3112.3	10.2		
24	15	30	2850	67.8	42.5	3111.2	11.3		
25	13	30	4170	67.8	42.5	3111.2	11.3		
27	14	00	7080	66.7	43	3112.3	10.2		
28	14	30	8550	72.4	40.5	3106.6	15.9		
30	14	00	11400	72.4	40.5	3106.6	15.9		
1	15	45	12945	72.4	40.5	3106.6	15.9		
4	9	30	16890	71.3	41	3107.7	14.8		
5	13	00	18540	71.3	41	3107.7	14.8		
6	17	00	20220	71.3	41	3107.7	14.8		
8	11	00	22740	71.3	41	3107.7	14.8		
9		00	24060	74.8	39.5	3104.2	18.3		-
	15	-	25890	71.3	41	3107.7	14.8	L	
11	15	00	27300	71.3	41	3107.7	14.8		
	14		30120	73.6	40	3105.4	17.1		
	17	-	31770	69.0	42	3110.0	12.5		Pump stopped (19:11)
		15		67.8	42.5	3111.2	11.3		
	16			70.1	41.5	3108.9	13.6		
	15			67.8	42.5	3111.2	11.3		
28	15	30		66.7	43	3112.3	10.2	ļ	

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F L	PRO	JEC	THot	Creek Coo he Creek, E	DATA S		<u>RY</u>		Observations in RH 76-17-3 Sheet2of2 DATE: Start_Sept. 22, 1976
Т	'um, 'im	ped	WellRH Elapsed Time "t" (mins.)	76-19 Depth to Water (ft.)	Pressure (Pneumatic piezometers only) (p.s.i)	Elevation of	Drawdown (f1.)	Pump	Remarks
10	15	30		71.3	41	3107.7	14.8		
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F _ L	PRO .occ	JEC ition ped	<u>PUMP</u>	Hot Cree Cache Cre	DATA S k Coal ek, B.C.		<u>RY</u> 	L	Observations in <u>RH 76-18-1</u> Sheet <u>1</u> of <u>2</u> ATE: <u>Start Sept 22,1976</u> Finish Oct.14,1976
0	atu ept	m p h to		Top_of			Type: Datum elev Elevation	Unscru ation_ static_w	ed well X Pneumatic pie sened well Standpipe pie 3195 FTa. ater level <u>3160.3 FTa.</u> aned intervaltoa.
N N	/all /eil	dept dian		400 feet 8 inches ctric Subr	ND AQUIFE	-	Aquifer thi	scription ickness_ ump_suc	Image: Contined Coldwater Fm (Siltstone) 800 feet 10n370 feet Image: Constant rate Image: Step drawdown
Ţ	im	•	Elopsed Time "t" (mins.)	Depth to Water (ft.)	Pressure (Pneumatic piezometers only)	Elevation of Water (ft.)	Drowdown (ft.)	Pump Rate Q (i.g.p.m)	Remarks
Dy.	Hłr.	Min.			(p.s.i)	a. s. l.			
22	9	00	0	32.6	156	3162.4			
	16	00	0						Pump started
	16	30	30	46.5	150	3198.5	11.8		
	19	00	180	<u>56.</u> 9	145.5	3138.1	22.2	L	
23	11	30	1170	<u>63.</u> 8	142.5	3131.2	29.1		
		30	1650	69.6	140	3125.4	34.9		
		30	2850	63.8	142.5	3131.2	29.1		
25	13	30	4170	66.1	141.5	3128.9	31.4		
	_	00	7080	62.7	143	3132.3	28.0		
28	14	30	8550	62.7	143	3132.3	28.0		
30	14	00	11400	62.7	143	3132.3	28.0		
1	15	45	12945	69.6	140	3125.4	34.9		
4	9	30	16890	76.5	137	3118.5	41.8		
5	13	00	18540	74.2	138	3120.8	39.5		
_	17	00	20220	71.9	1 39	3123.1	37.2		
		00	22740	76.5	137	3118.5	41.8		
9	9	00	24060	74.2	138	3120.8	39.5		-
		30	25890	71.9	139	3123.1	37.2		
		00	27300	74.2	138	3120.8	39.5		
13	14	00	30120	70.8	139.5	3124.2	36.1		
14	17	30	31770	74.2	138	3120.8	39.5		Pump stopped (19:11)
16	11	15	_ · ·	73.1	138.5	3121.9	38.4		·
18	16	00		74.2	138	3120.8	39.5		
22	15	30		69.6	140	3125.4	34.9		
28	15	30		69.6	140	3125.4	34.9		

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P Li Pi	RO. oca ump	JEC tion bed	<u>PUMP</u> T <u>Hot</u> VellRH	Creek Co he Creek, E	DATA S		<u>RY</u>	l	Observations in RH 76-18- Sheet2of2 of2_ ATE: Start_Sept. 22, 1976_ Finish Oct. 14, 1976
	ime	5	Elapsed Time "t" (mins.)	Depth to Water (ft.)	Pressure (Pneumatic piezometers only) (p.s.i)		Drawdown (ft.)	Pump Rate Q {i.g.p.m)	Remarks
10	15	30		71.9	139	3123.1	37.2		
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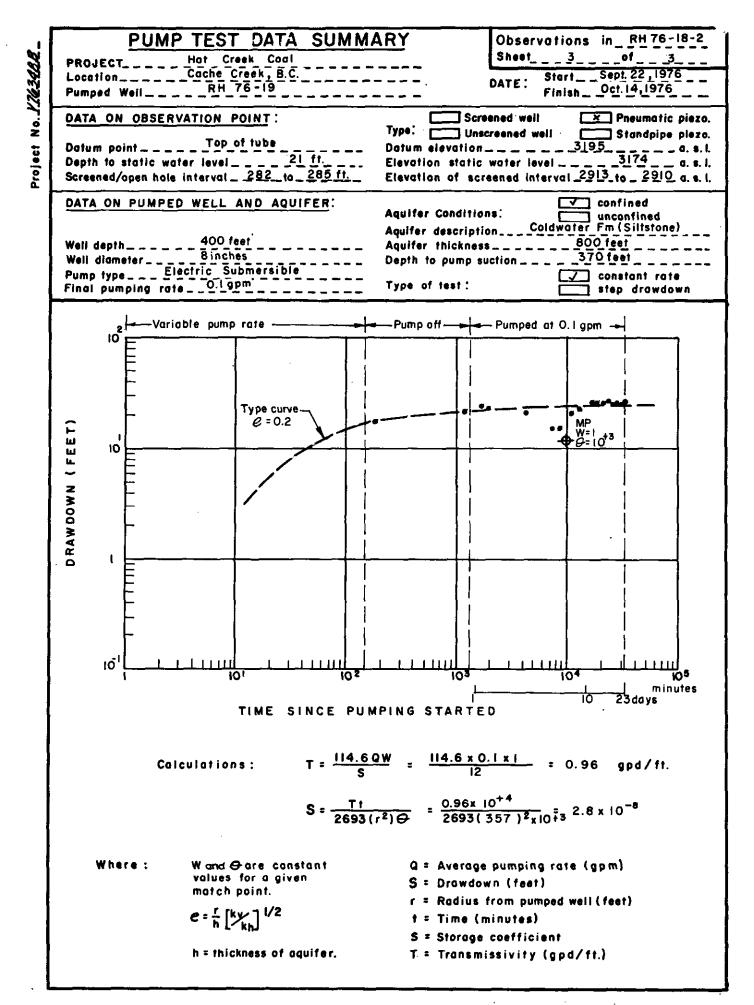
F	PRO .occ Pum	JEC Ition ped	PUMP	Hot Cree Cache Cre	DATA S k Cool ek, B.C.	SUMMA	<u>RY</u>	L	Observations in <u>RH</u> 76-18-2 Sheetof3 ATE: StartSept. 22,1976 FinishOct. 14,1976				
)atu)ept	m po h to		Top_of er levei			Screened well X Pneumatic pieze Type: Unscreened well Standpipe pieze Datum elevation 3195 FT. a. s. Elevation static water level 3169.5 FT. a. s. Elevation of screened interval						
v v	Veli Veli	dept dian	h	400 fee 8 inches ctric Subi	ND AQUIFE		Aquifer Conditions: vn confined Aquifer description Coldwater Fm (Siltstone) Aquifer thickness 800 feet Depth to pump suction 370 feet Type of test : vt constant rate						
	- i m 	e Min	Elapsed Time "t" (mins.)	Depth to Water (f1.)	Pressure (Pneumatic piezometers only) (p.s.i)	Elevation of Water (ft.) a.s.t.	Drawdown (ft.)	Pump Rate Q (igp.m)	Remarks				
22		00	0	20.9	118	3174.1							
	<u> </u>	00	0	-		-		·	Pump started				
	· -	30	30	10.5	122.5	3184.5							
	<u> </u>	00	180	44.0	108	3151.0	18.5						
23	11	30	1170	47.5	106.5	3147.5	22						
	19	30	1650	49.8	105.5	3145.2	24.3						
24	15	30	2850	48.4	110	3146.6	22.9						
25	13	30	4170	46.3	107	3148.7	20.8						
		00	7080	40.6	109.5	3154.4	15.1						
28	14	30	8550	41.7	109	3153.3	16.2						
30	14	00	11400	46.3	107	3148.7	20.8		· · · · · · · · · · · · · · · · · · ·				
1	15	45	12945	48.4	106	3146.4	23.1						
4	Ð	30	16890	53.3	104	3141.7	27.8						
5	13	00	18540	50.9	105	3144.1	25.4		· · · · · · · · · · · · · · · · · · ·				
6	17	00	20220	50.9	105	3144.1	25.4						
8	11	00	22740	53.3	104	3141.7	27.8						
9	9	00	24060	52.1	104.5	3142.9	26.6						
10	15	30	25890	50.9	105	3144.1	25.4						
	15		27300	52.1	104.5	3142.9	26.6						
	14		30120	50.9	105	3144.1	25.4						
	17		31770	53 .3	104	3141.7	27.8		Pump stopped (19:11)				
	11			50.9	105	3144.1	25.4						
	16			50.9	105	3144.1	25.4						
22				50.9	105	3144.1	25.4		· · · · · · · · · · · · · · · · · · ·				
28	15	30		50.9	105	3144.1	25.4						

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No /	PRO	JEC	<u>РИМР</u> т <u>но</u> т	TEST		UMMA	<u>RY</u>		Observations in_RH_76-18-2 Sheet2of3 ATE: Start_Sept. 22, 1976 Finish Oct. 14, 1976
	Loci Pum	otior ped	WellRH	he_Creek,_E _76-19	1. <u>C</u>			(DATE: Start_Sepi. 22, 1976 Finish_Oct. 14, 1976
	ſim Hr.	e Min.	Elapsed Time "t" (mins.)	Depth to Water (ft.)	Pressure (Pneumatic piezometers only) (p.s.1)	Elevation of Water (ft.) a.s.l.	Drawdown (ft.)	Pump Rate Q (i.g.p.m	Remarks
	15	30		57.9	102	3137.1	32.4		
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F	RO	JEC		Hat Cree		UMMA	<u>RY</u>		Observations in <u>RH 76-18-3</u> Sheet 1 of 2
L P	.ocd 'um	rtion ped	T 	RH 76	5-19 			D	ATE: Start_Sept. 22, 1976 Finish_Oct. 14, 1976
0	atu ept	m p h to	N OBSERV	ATION PO Top of er level	INȚ:		Elevation	Unscrution_ static_w	hed well X Pneumatic pi bened well Standpipe pi 3195 FT. ater level 3181 FT. aned intervala
v v	Veli Veli	depi dian		400 fee 8 inches ctric Subi	ND AQUIFE	<u></u>	Aquifer th	scription ckness_ ump_suc	Coldwater Fm (Siltstone) 800 feet ion370 feet Step drawdown
	'n		Elopsed Time "t" (mins.)	Depth to Water (fl.)	Pressure (Pneumatic piezometers only)	Elevation of Water (ft.)	Drawdown (ft.)	Pump Rote Q (i.g.p.m)	Remarks
-		Min.			(p.s.i)	a.s. (.			
22		00	0	6.0	80.5	3189	-		
		00	0		-	-	-		Pump started
		30	30	14.1	77	3180.9	.1		
	_	00	180	24.5	72.5	3170.5	10.5		
_		30	1170	31.5	69.5	3163.5	17.5		
	-	30	1650	28	71	3167.0	14.0	_	
24	15	30	2850	26.8	71.5	3168.2	12.8		
25	13	30	4170	31.5	69.5	3163.5	17.5		
27	14	00	7080	28	71	3167.0	14.0		
28	14	30	8550	28	71	3167.0	14.0		
30	14	00	11400	36.1	67.5	3158.9	22.1		
1	15	45	12945	36.1	67.5	3158.9	22.1		
4	9	30	16890	39.5	66	3155.5	25.5		
5	13	00	18540	41.8	65	3153.2	27.8		
6	17	00	20220	39.5	66	3155.5	25.5		
8]]	00	22740	39.5	66	3155.5	25.5		
9	9	00	24060	40.3	65.5	3154.7	26.3		-
10	15	30	25890	39.5	66	3155.5	25.5		
11	15	00	27300	39.5	66	3155.5	25.5		· · · · · · · · · · · · · · · · · · ·
13	14	00	30120	37.2	67	3157.8	23.2		
14	17	30	31770	40.3	65.5	3154.3	26.7		Pump stopped (19:11)
16	11	15		39.5	66	3155.5	25.5		
18	16	00		39.5	66	3155.5	25.5		
22	15	30		38.4	66.5	3156.6	24.4		
28	15	30		37.2	67	3157.8	23.2		

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P	R0. 0ca	JEC tion			DATA S		<u>RY</u>		Observations in <u>RH</u> 76-11 Sheet <u>2</u> of <u>2</u> ATE: Start <u>SEPT</u> , 22, 1976 Finish <u>Oct</u> , 14, 1976
	ime	•	Well Elapsed Time "t" (mins.)		Pressure (Pneumatic piezometers anly) (p.s.i)	Elevation of	Drawdown (ft.)	Pump	Remark s
10	15	30		44.2	64	3150.8	30.2		<u></u>
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P	ROJEC ocation umped	T	TEST Hat Cree Cache Cre RH 76	DATA S k Coal ek, B.C.			L	Observations inRH_76_19 SheetIof of6 ATE: StartSept.22,1976_ FinishOct.14,1976 FinishOct.14,1976_
D D D	ATA OI otum pe epth to	N OBSERV	ATION PO Top of er level			Type: Datum elev Elevation ::	Unscreation_ static_w	ed well Pneumatic pie ened well Standpipe ple <u>3183.5 FT.</u> a. ater ievel <u>3194.2 FT.</u> a. ned interval <u>1094.2 FT.</u> a.
W W P	fell dept fell dian	h heter Ele	_ 400 fee	ND AQUIFE		Aquifer Co Aquifer des Aquifer thi Depth to p Type of te	cription ckness_ ump_suci	Image: Confined unconfined Coldwater Fm (Siltstone) 800 feet ion370 feet Image: Constant rate Image: Step drawdown
Ť	'i m e Hr. Min	Elapsed Time "t" (mins.)	Depth to Water (ft.)	Pressure (Pneumatic piezometers oniy) (p.s.i)	Elevation of Water (ft.) a.s.l.	Drawdown (ft.)	Pump Rate Q (i.g.p.m)	Remarks
	16/00	0	89.3		3094.2	0	1.0	W.L. probe on the blink
	1 <u>1</u>	1/2	-		-	_	1.0	W.L. probe on the blink
	1	1	-			-	1.0	
	11	11	93.4		3090.1	4.1	1.0	
	2	2	90.2		3093.3	0.9	1.0	
	21/2	2 <u>1</u>	90.3		3093.2	1.0	1.0	
	3	3	90.4		3093.1	1.1	1.0	
	31	3 1	90.5		3093.0	1.2	1.0	
	4	4	90.7		3092.8	1.4	1.0	Q varied from 0.9-1.1
	41	412	90.9		3092.6	1.6	1.0	due to siltation in val
	5	5	91.0		3092.5	1.7	1.0	
	6	6	91.3		3092.2	2.0	1.0	
	7	7	91.5		3092.0	2.2	1.0	
	8	8	-		-	-	1.0	W.L. probe problems
	9	9	92.3		3091.2	3.0	1.0	
	10	10	92.5		3091.0	3.2	1.0	
	12	12	93.2		3090.3	3.9	1.0	ب
	14	14	93.7		3089.8	4.4	1.0	
_	16	16	94.2		3089.3	4.9	1.0	Water temp = $9.5^{\circ}C$
	18	18	94.7		3088.8	5.4	1.0	
	20	20	95.2		3088.3	5.9	1.0	
	25	25	96.7		3086.8	7.4	1.0	
	30	30	98.4	- <u></u>	3085.1	9.1	1.0	
	45	45	102.6		3080.9	13.3	1.0	
22	170	60	-	1	- 1	- 1	1.0	Generator problems

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L	.000	ation	T	AT CREEK	DATA S			l	Observations in_RH_76-19_ Sheet2of6_ ATE: Start_SEpt. 22/76
P	បភា	ped	Well F	0 Depth	Pressure			Pump	ATE: Finish_OCT. 14/76
	i m	• Min	Time "t" (mins.)	to Water (ft.)	(Pneumatic piezometers only) (p.s.i)	of Water (ft.) a.s.l.	Drawdown {ft.}	Rate Q (i.g.p.m)	Remark s
	_	30	90	105.8		3077.7	16.5	1.0	Conductivity = 1300 micro
	18		120	111.2		3072.3	21.9	1.0	mhos/cm.
	8	30	150	113.9		3069.6	24.6	1.0	
-	19	00	180			-	-	1.0	Test discontinued due to
						· · ·			generator problems
23	13	<u>30뉲</u>	1290 1	105.1		3078.4	15.8	1.0	Pumping resumed
		31	1291	105.3		3078.2	16.0	1.0	Water - creamy, silty
		311	12911	105.4		3078.1	16.1	1.0	
		32	1292	105.6		3077.9	16.3	1.0	
		32월	1292 1	105.6		3077.9	16.3	1.0	
		33	1293	105.7		3077.8	16.4	1.0	
		33±	1293 1	105.8		3077.7	16.5	1.0	
		34	1294	105.9		3077.6	16.6	1.0	
		341	1294 1	106.0		3077.5	16.7	1.0	
		35	1295	106.1		3077.4	16.8	1.0	
		36	1296	106.3		3077.2	17.0	1.0	
		37	1297	106.5		3077.0	17.2	1.0	
		38	1298	106.7		3076.8	17.4	1.0	
		39	1299	106.9		3076.6	17.6	1.0	
		40	1300	107.2		3076.3	17.9	1.0	·
		42	1302	107.7		3075.8	18.4	1.0	
		44	1 30 4	108.0		3075.5	18.7	1.0	
		46	1306	108.4		3075.1	19.1	1.0	
		48	1308	108.8		3074.7	19.5	1.0	
		50	1310	109.4		3074.1	20.1	1.0	
		55	1315	110.5		3073.0	21.2	1.0	
	14	0	1320	112.1		3071.4	22.8	1.0	
		10	1330	114.2		3069.3	24.9	1.0	
		20	1340	116.9		3066.6	27.6	1.0	
		30	1350				-	1.0	
		50	1370	120.0		3063.5	30.7	1.0	
	15	10	1 390	122.5		3061.0	33.2	1.0	
23		35	1415	128.2		3055.3	38.9	1.0	

Logged by____ROE__

P	ROJI	ECT	P TEST	COAL				Observations in <u>RH 76-19</u> Sheet3of6_
Pi	ocati umpê	on d Well	CACHECREE RH7619				C	ATE: Stort SEPT 22/76
	ime Hr. M	Elapsed Time "t" (mins.)	to Water	Pressure (Pneumatic plezometers only)	(ft.)	Drawdown (ft.)	Pump Rate Q (i.g.p.m)	Remarks
-	6 0		131.5	(p.s.i)	c.s.l. 3052.0	42.2	1.0	
2)	4		137.4	<u> </u>			1.0	Water colour - very silt
	73		143.4		3046.1	48.1	1.0	dirty appearance
	8 2		145.3		3040.1 3038.2	54.1	1.0	<u> </u>
	9 1					56.0	1.0	
			147.2		3036.3	57.9	1.0	
		1680	154.3		3029.2	65.0	1.0	l
	20 5		-		-	-	1.0	
	1 4		159.9		3023.6	70.6	1.0	
	2 3		163.2		3020.3	73.9	1.0	
	3 2		168.2		3015.3	78.9	1.0	
240			176.7		3006.8	87.4	1.0	
[0	1980	182.5		3001.0	93.2	1.0	i
-	50		189.6		2993.9	100.3	1.0	
[⁴	30		-		-	-	1.0	
Б			214.6		2968.9	125.3	1.0	
[50		242.8	·	2940.7	153.5	1.0	
B			253.6		2929.9	164.3	1.0	
P			260.3		2923.2	171.0	1.0	
	0 2(269.8		2913.7	180.5	1.0	
	1 10		278.7		2904.8	189.4	1.0	
	20	2640	284.3		2899.2	195.0	1.0	
	2 50	2690	290.2		2893.3	200.9	1.0	
	3 40	2740	298.4		2885.1	209.1	1.0	
	4 30	2790	302.9		2880.6	213.6	1.0	
1	5 20	2840	307.8		2875.7	218.5	1.0	
	6 10	2890	310.8		2872.7	221.5	$\frac{1}{2}$	Flow adjusted to $\frac{1}{2}$ gpm.
Ī	70	2940	312.4	· · · · · ·	2871.1	223.1	$\frac{1}{2}$	
-	7 50	2990	317.4		2866.1	228.1	1 <u>2</u>	
	8 40	3040	-		-		1/2	Adjustment to flow
	9 30	3090	317.2		2866.3	227.9	1/2	
-2	0 20	3140	318.8		2864.7	229.5	1/2	······
- 12	1 10		320.6		2862.9	231.3	1/2	
242	2 00	3240	321.9		2861.6	232.6	1	

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Golder Associates

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	PROJEC		PUMP	TEST		Observations in <u>RH 76-19</u> Sheet4of6			
E	.oca	itio	wellRH	CHE CREEK	<u></u>	 	 	D	ATE: Start_SEPt_ 22/76 Finish_0ct_ 14/76
1	Time		Elapsed Time "t"	Depth to Water	Pressure (Pneumatic piezometers		Drawdown	Pump Rate Q	Remarks.
Dy.	Hr.	Min.	(mins.)	(ft.)	only) (p.s.i)	(ft.) a.s.i.	(ft.)	(i.g.p.m)	
24	22	50	3290	322.9		2860.6	233.6	<u>1</u>	
	23	40	3340	324.5		2859.0	235.2	<u>1</u>	
25	0	30	3390	326.0		2857.5	236.7	1 <u>2</u>	
	1	20	3440	327.2		2856.3	237.9	<u>1</u>	
	2	10	3490	329.5		2854.0	240.2	<u>1</u>	
	3	00	3540	330.4		2853.1	241.1	1/2	
	3	50	3590	331.4		2852.1	242.1	ł	
	4	40	3640	331.4		2852.1	242.1	1/2	
	5	30	3690	332.6		2850.9	243.3	ł	
	6	20	3740	334.3		2849.2	245.0	ł	Adjustment of flow
	7	10	3790	336.0		2847.5	246.7	1/2	
	8	00	3840	338.0		2845.5	248.7	$\frac{1}{2}$	· · · · · · · · · · · · · · · · · · ·
	10	0	3960	335.4		2848.1	246.1	1/2	
	11	0	4020	336.7		2846.8	247.4	1/2	Water clearing; still si
	11	50	4070	336.5		2847.0	247.2	1/2	
	15	00	4260	337.3		2846.2	248.0	20 oz/m.	Flow adjusted to 20 oz/m
	17	00	4380	339.0		2844.5	249.7	20 oz/m.	
	18	00	4440	337.5		2846.0	248.2	4 oz/m.	
25	21	00	4620	334.5		2849.0	245 2	10 oz/m.	Flow adjusted to 10 oz/m
26	2	00	4920	325.3		2858.2	236.0	10 oz/m.	· · · · · · · · · · · · · · · · · · ·
	6	00	5160	326.1		2857.4	236.8	-	Difficult to keep valve
	12	00	5520	320.2		2863.3	230.9	20 oz/m.	unsilted, therefore caus
	16	00	5760	315.7		2867.8	226.4	oz/m. 15 oz/m.	uneven Q rates
27	8	00	6720	313.0		2870.5	223.7	15 oz/m.	
	14	00	7080	313.8		2869.7	224.5	15 oz7m.	Water clearer, less silt
	19	00	7280	314.0		2869.5	224 7	15	
28		30	8190	307.9		2875.6	218.6	oz/m. 10 oz/m. 20	Temp. = 13 ^o C, Cond. = 16
	14	00	8520	316.3		2867.2	227.0	20 07/m	Water - light grey, br.
29			9630	318.7		2864.8	229.4	oz/m. 15 oz/m.	
	19	00	10260	320.9		2862.6	231.6	15 oz/m.	
30	8	30	11070	320.7		2862.8	231.4	15 oz/m.	
			11670	325.7		2857.8	236.4	15 oz/m.	·····
T	8	30	12510	329.3		2854.2	240.0	15 oz/m.	Water fairly clear

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F	PROJEC			TEST	Observations in_ <u>RH_76-19</u> _ Sheet5of6				
E	Location) Well	CACHE CR	DATE: Start_SEPT_ 22/76 Finish_0CT14/76				
1	Time		Elapsed Time "t"	Depth to Water	Pressure (Pneumatic plezometers	Elevation of Water	Drawdown	Q	Remarks
Dy.	Hr,	Min.	(mins.)	(ft.)	only) (p.s.i)	(ft.) a.s.l.	(ft.)	(i.g.p.m	
1	15	45	12945	327.7		2855.8	238.4	10 oz/m.	Rained at night
2	β	30	13950	321.7		2861.8	232.4	7 oz/m.	When first meas. = 7 oz Valve shaken-Q inc. to
4	10	00	16920	313.3		2870.2	224.0	12 oz/m.	Rained at night
5	13	00	18540	314.9		2868.6	225.6	10 oz/m.	
6	17	30	20250	318.8		2864.7	229.5	 oz/m.	Water fairly clear
8	10	00	22680	324.0		2859.5	234.7	10 oz/m.	
9	0	00	24120	323.0		2860.5	233.7	10 oz/m.	
10	5	00	25860	324.Ö		2859.5	234.7	10 oz/m.	
11	15	00	27300	322.0		2861.5	232.7	10 oz/m.	
12	14	30	28710	318.0		2865.5	228.7	9 oz/m.	
13	4	00	30120	320.0		2863.5	230.7	10 oz/m.	
14	8	00	31800	237.4		2946.1	148.1	oz/m.	Low Q, due to silting
14	9	11	31871	246.5		2937.0	157.2	GPM	PUMP SHUT OFF
			t'(min)						
14	9		1/2	1		-	-		RECOVERY
	9	12	1	246.4		2937.1	157.1		
		12불	11	246.3		2937.2	157.0		
		13	2	246.3		2937.2	157.0		
		13 <u>1</u>		246.3		2937.2	157.0		
		14	3	246.2		2937.3	156.9		
		141		246.2		2937.3	156.9		
		15	4	246.2		2937.3	156.9		
		15 1		246.2		2937.3	156.9		
		16	5	246.2		2937.3	156.9		
		17	6			-	-		
		18	7	246.1		2937.4	156.8		
		19	8	246.1		2937.4	156.8		
		20	9	246.1		2937.4	156.8		
		21	10	246.1		2937.4	156.8		
		23	12	246.0		2937.5	156.7		
		25	14	246.0		2937.5	156.7		
		27	16	245.9		2937.6	156.6		
		29	18	245.9		2937.6	156.6		

Golder Associates

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1	PRO	JEC	τ	HAT CREEK	DATA S		<u>KI</u>	l	Observations in <u>RH 76-19</u> Sheet <u>6</u> <u>of 6</u> Start SEPT 22/76
F	-occ	ped	Well	RH 76-19				D	ATE: Start_SEP1. 22/76 Finish_OCT. 14/76
	Time		Elapsed Time "t" (mins.)	Depth to Water (ft.)	Pressure (Pneumotic piezometers	Elevation of Water	Drawdown (ft.)	Pump Rate Q (i.g.p.m)	Romarks
Dy.	Hr.	Min.	(mins.)	(11.)	only) (p.s.i)	(ft.) a.s.l.	10.7	\r.g.p.m	
14	19	31	20	245.9		2937.6	156.6		RECOVERY
		36	25	245.8		2937.7	156.6		
		41	30	245.6		2937.9	156.3		
		46	35	245.5		2938.0	156.2		
		51	40	245.4		2938.1	156.1		
		01	50	245.2		2938.3	155.9		
		11	60	244.9		2938.6	155.6		
_		26	75	244.6		2938.9	155.3		
		51	100	243.6		2939.9	154.3		
	21	41	150	241.8		2941.7	152.5		
	22	31	200	240.8		2942.7	151.5		
	23	21	250	239.0		2943.6	150.6		
15	0	11	300	239.0		2944.5	149.7		
	8	31	800	228.9		2954.6	139.6		
	11	51	1000	227.9		2955.6	138.6		Pump Removed
	18	31	1400	219.6		2963.9	130.3		
16		41	2250	204.4		2979.1	115.1		
	15		2650	198.7		2984.8	109.4		
18	16	01	5570	163.4		3020.1	74.1		
		11	11400	114.2		3069.3	24.9		After reading - added wat
	18	51	11500	97.8		3085.7	8.5		
28	15	21	19930	91.8		3091.7	2.5		
						-			

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)atu)atu)apt	A Ol im pi ih to ened,	open hole	ATION PO Top of ar level interval	INT :		DATE: Finish_Oct.14,1976 Finish_Oct.14,1976 Screened well Pneumatic pieze Type: Unscreened well Datum elevation3137.1 FT. Elevation static water level3085 FT. Elevation of screened intervaltoa.s.					
				400 fee	t mersible		Aquifer Conditions: vnconfined Aquifer description Coldwater Fm (Siltstone) Aquifer thickness 800 feet Depth to pump suction 370 feet Type of test: step drawdown					
	Time		Elapsed Time "t" (mins.)	Depth to Water (ft.)	Pressure (Pneumatic piezometers only)	Elevation of Water (ft.)	Drawdown (ft.)	Pump Rate Q (i.g.p.m)	Remarks			
	·	Min.			(p.s.1)	0.8.1.						
22	<u> </u>	╉╼╾╋	0	53.1	<u> </u> ,	3084						
		00	0	-	 _	-	-		Pump started			
		30	1170	54.6	·····	3082.5	2.5					
		30	2850	52.9		3084.2	0.8					
		00	4200	53.1		3084	1.0		·			
		30	8550	53.7	<u> </u>	3083.4	1.6					
		00	11400	54.3	<u>_</u>	2082.8	2.2		<u>. </u>			
4		30	16890	55.9		3081.2	3.8					
		00	20220	56.3		3080.8	4.2					
	_	00	24120	57.0		3080.1	4.9					
		00	27300	57.0		3080.1	4.9					
14 16		11 00	31871	-	 	-	-		Pump stopped			
\vdash		20		57.3		3079.8	5.2					
22				-		-] 			
28				58 . 1		3079 -	6.0					
	_	30		- 60.3		- 3076.8	8.2		-			

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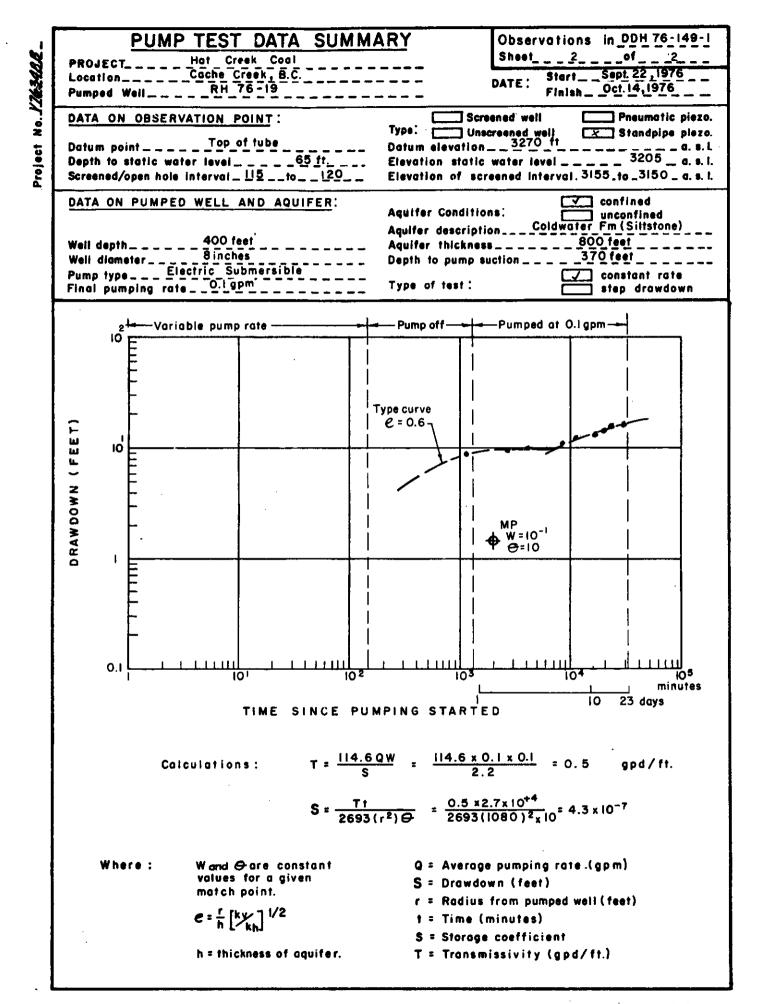
0	AT/ atu ept	m po h to	Well	Hat Cree Coche Cree RH 76 ATION PO Top of er level			Type: X	D Screen Unscreation_ static_w	Observations inDDH_76145 Sheetlofl ATE: StartSept.22,1976 FinishOct.14,1976 ned well Pneumatic pie 3196.5 FT
W	eii eii	dept dian	h heter	400 fee 8 inches	ND AQUIFE	_ 	Aquifer Co Aquifer des Aquifer thi Depth to p Type of te	icription ickness_ ump_suci	Coldwater Fm (Silfstone) 800 feet tion 370 feet Step drawdown
	Time		Elapsed Time "t" (mins.)	Depth to Water (ft.)	Pressure (Pneumatic piezometers only)	Elevation of Water (ft.)	Drawdown (ft.)	Pump Rate Q (i.g.p.m)	Remarks
-	_	Min.			(p.s.i)	a.s. ł.			
		00	0		-				Pump started
+		30	1170	46.7		3149.8	1.2		
		30 20	2850	46.4		3150.1	0.9	 	
		00	4200	46.3		3150.2	0.8		- <u></u>
	_	30 00	8550 11400	46.6	·	3149.9	1.1		
4		30	16890	47.4		3149.1 3149.7	1.9 1.3	· -	
6		00	20220	45.8		3150.7	0.3		
	<u> </u>	11	31871		· · · · · · · · · · · · · · · · · · ·	5150.7	0.5		Pump stopped
16	_		51071	47.5		3149.0	2.0		
221				48.8		3147.7	3.3		
281	-	30		48.8	·	3147.7	3.3	<u> </u>	
-	<u> </u>								
╈		_							<u> </u>
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Logged by_ RAD__

D	atu ept	n p h to	N OBSERV	ATION PO Top of er level			DATE: Finish_Oct.14,1976 Screened well Pneumatic piez Type: Unscreened well Standpipe piez Datum elevation_3270 FTa.s. Elevation static water level_3205 FTa.s. Elevation of screened intervaltoa.s.					
W W	ieli ieli	dept dian		400 fee 8 inches ctric Subi	nd AQUIFE		Aquifer Co Aquifer des Aquifer thi Depth to p Type of te	cription ickness_ ump_suc	Coldwater Fm (Siltstone) 800 feet tion 370 feet			
	Time	e Min.	Elapsed Time "t" (mins.)	Depth to Water (ft.)	Pressure (Pnaumatic piezometers only)	(ft.)	Pump Drawdown Rate Q Rei (ff.) (i.g.p.m)	Remark s				
÷	_	┢╼═╪		(- 1	(p.s.i)	a.s.i.						
		00 00	0	67.4		3202.6	-		Pump started			
		30	1170	- 73.5		-	- 8.5		Pump started			
		30 30	2850	74.1		3195.9	9.1					
		00	4200	74.5		3195.5	9.5					
		30	8550	75.5		3194.5	10.5					
		00	11400	76.7		3193.3	11.7	<u> </u>	<u></u>			
4		30	16890	77.7		3192.3	12.7					
		00	20220	78.3		3191.7	13.3					
		00	24120	80.0		3190	15.0					
		00	27300	80.0		3190	15.0					
14	19	11	31871	-		-	-		Pump stopped			
16	1	00		80.8		3189.2	15.8					
18	5	20		81.6		3188.4	16.6					
22	15	30		81.6		3188.4	16.6					
28	5	30		-								
10	15	30										
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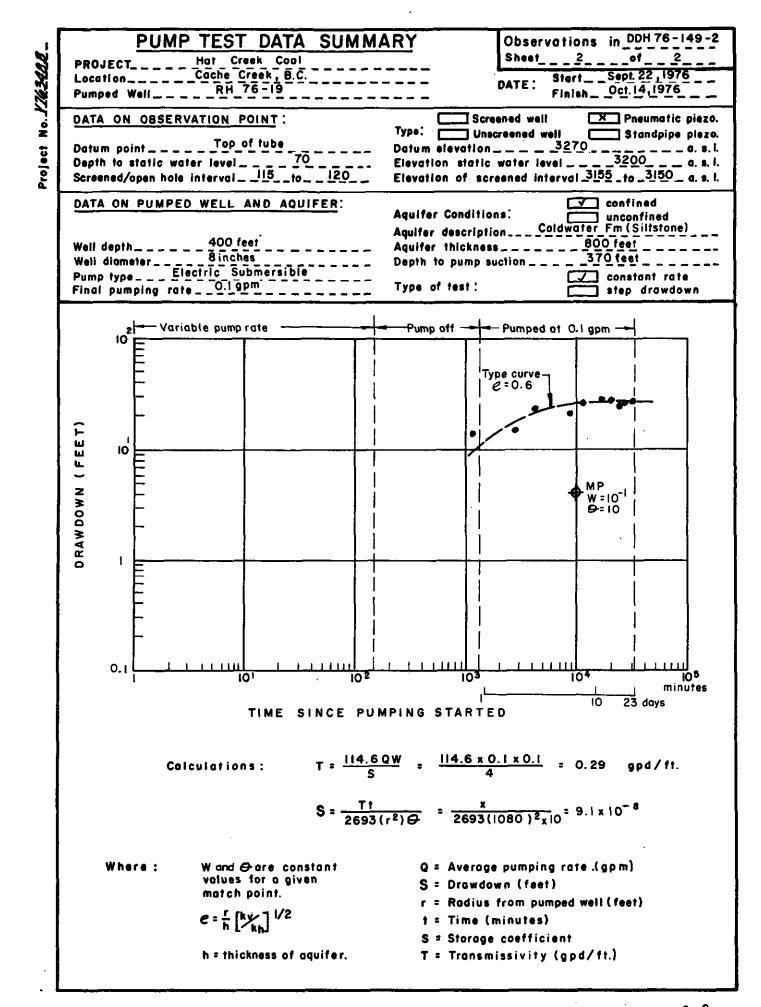
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P	PRO .oca 'umi	JEC tion ped		Hot Cree Cache Cre	DATA S k Coal ek, B.C.			E	Observations in <u>DDH</u> 76-149- SheetIof2 ATE: StartSept 22,1976 FinishOct.14,1976
D	atu ept	m p h to	static wate	Top_of	INT : fube 70 FT		Type: Datum elev Elevation	Unscri ation_ static_w	ater leveltotoa.
W W P	/eli Voli	depi dian	h neter a Ele	400 feet 8 inches ctric Subr	ID AQUIFE	 	Aquifer Co Aquifer des Aquifer thi Depth to p Type of te	cription ckness_ ump_suc	Coldwater Fm (Silfstone) 800 feet 370 feet Constant rate step drawdown
Time Dy. Hr. Min.			Elapsed Time "t" (mins.)	Depth to Water (fl.)	Pressure (Pneumatic piezometers only) (p.s.i)	Elevation of Water (ft.) a.s.l.	Drawdown	Pump Rate Q (i.g.p.m)	Remark s
-		00	0	79.1	19	3190.9			
		00	0	-		-			Pump started .
		30	1170	83.7	17	3186.3	13.7		
		30	2850	84.9	16.5	3185.1	14.9		
		00	4200	93	13	3177	23.0		
-		30	8550	90.7	14	3179.3	20.7		
		00	11400	95.3	12	3174.7	25.3		
4		30	16890	97.6	11	3172.4	27.6		
		00	20220	97.6	11	3172.4	27.6		
_	10	+	24120	94.1	12.5	3175.9	24.1		· · · · · · · · · · · · · · · · · · ·
11		00	27300	95.3	12	3174.7	25.3		
14		11	31871	-	-	-	-		Pump stopped
16	11	00		99.9	10	3170.1	29.9		
18	15	20		99.9	10	3170.1	29.9		
_	15		······································	96.5	11.5	3173.5	26.5		
28	15	30			-	-	-		
10	15	30		53.7	30	3216.3	-		-
-+									

Logged by_ Pro



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