



Golder Associates
CONSULTING GEOTECHNICAL ENGINEERS

GOLDER ASSOCIATES LTD.
IN ASSOCIATION WITH
PD-NCB CONSULTANTS LTD.
AND
WRIGHT ENGINEERS LTD.
REPORT NO. 6
HAT CREEK GEOTECHNICAL STUDY
VOLUME 3 - APPENDICES 2-6

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March, 1977

V 76349

TABLE OF CONTENTS

VOLUME 3

Appendix 2	Petrographic Reports
Appendix 3	X-ray Diffraction Studies
Appendix 4	Uniaxial Compression Tests
Appendix 5	Geohydrologic Data
Appendix 6	Pump Test Report for Borehole RH 76-19

APPENDIX 2

PETROGRAPHIC REPORTS

APPENDIX 2
PETROGRAPHIC REPORTS

In order to substantiate the findings of the geotechnical test results and visual descriptions, thin sections were cut of a number of representative rock types. The sections were cut and described by Vancouver Petrographics Ltd.

A number of petrographic descriptions were also provided by Dolmage-Campbell & Associates in a draft report. These are not reproduced in this appendix; they confirm the descriptions made on the GA geological logs.



Vancouver Petrographics Ltd.

JAMES VINNELL, Manager
JOHN G. PAYNE, Ph. D. Geologist

216 EAST 28TH AVENUE
VANCOUVER, B.C. V5V 3M1

PHONE (604) 874-1650

PETROGRAPHIC EXAMINATION FOR

GOLDER BRAWNER & ASSOCIATES LTD.

#803 - 206.2 and #803 - 353 examined over transmitted
light.

September 1976

Pilsum P. Master M.Sc.

803 - 206.2 : TUFF

The rock is fragmental. The fragments can be distinguished from the matrix by: (1) the groundmass is hydrated to palagonite (yellow colour), (2) the larger size of the glass beads. In general, the fragments are etched and are subangular.

There is a great abundance of pore spaces, which have an irregular shape and distribution.

Upto 5% (visual estimate) of the rock is made up of sub-hedral medium sized grains of feldspar (K-spar and plagioclase). These crystal grains have an irregular distribution, and occur as individual grains rather than in clots or mosaics.

The glass is variable in form, size and amount of devitrification. The glass beads are generally round in shape (in X section), or oblong. Some of the beads have iron rich (limonite?) rims. Part of the groundmass is a microcrystalline aggregate in the shape of shards (montmorillonite).

Before devitrification and chemical alteration to montmorillonite, the rock was most probably a TUFF ---an admixture of glass fragments, rock fragments and whole crystals. The "rock" fragments were most probably older tuff of similar composition. Due to the relatively large size and subangular shape of the fragments the rock may be classified as an agglomerate.

803 - 353 : TUFF

This is a relatively uniform rock. The groundmass is a microcrystalline aggregate of shards (montmorillonite). Scattered

in the groundmass are fairly uniform sized glass beads. The distribution of these beads is fairly uniform and show no flow texture or lineation.

There are also a few medium sized grains of feldspar scattered through the thin section. In comparison with 803-206.2, there appears to be little or no pore space and no palagonite.

Before devitrification and chemical alteration to montmorillonite the rock was an admixture of vitric and lithic tuff.

Bomas



Vancouver Petrographics Ltd.

JAMES VINNELL, Manager
JOHN G. PAYNE, Ph. D. Geologist

P.O. BOX 39
8887 NASH STREET
FORT LANGLEY, B.C.
VOX 1J0

Report for: Graham Rawlings,
Golder-Brawner

PHONE (604) 533-1155

Samples: 809-433, 814-596, 898-227.4 (no section)

Sample 809-433 Bentonite with Volcanic Fragments

The rock consists of fragments of mineral grains and fine grained porphyritic volcanic rocks (andesite, basalt(?)) in a groundmass of montmorillonite.

Mineral fragments include quartz, plagioclase, and muscovite; they occupy about 10-15% of the rock, with quartz most abundant and muscovite rare. Fragments range from very fine (0.02mm) up to 0.3 mm, with most obvious fragments being from 0.1 to 0.2 mm in size. The quartz fragments are very angular and plagioclase less angular. Other resistant mineral grains include zircon (one grain 0.025 mm long) and sphene (0.1%) as fractured grains.

Rock fragments include the following types, their compositions are probably andesite, but a few may be basalt. (10-15% of rock)

- 1) Patches of strongly altered(?) plagioclase grains to 0.05 mm and a few strongly zoned plagioclase phenocrysts of similar size occur in a groundmass of abundant plagioclase laths to 0.025 mm and a very fine grained matrix (0.001-0.005 mm) of unidentified minerals.
- 2) Uniform rock composed of plagioclase laths to 0.02 mm long.
- 3) Lathy plagioclase to 0.025 mm with abundant Ti-oxide and opaque up to 0.5 mm across.
- 4) Lathy plagioclase to 0.1 mm, some showing prominent flow foliation, with abundant interstitial opaque (5-30% in different fragments) and a brown platy mineral (possibly montmorillonite).
- 5) Sedimentary rock(?) with a few fragments of quartz and plagioclase to 0.1 mm in a very fine grained, strongly interlocking matrix (0.005 mm) of quartz, plagioclase, and clay(?).
- 6) Sedimentary rock or altered rock; very fine grained interlocking clay minerals up to 0.1 mm across.

As well the rock contains patches of montmorillonite consisting of fibrous aggregates of grains. Patches are up to 0.2 mm across, with grains up to 0.02 mm long. Identifying properties are low relief (R.I. less than quartz), colorless to brown, biaxial -ve, 2V about 30°, length slow, subparallel to parallel extinction.

A few fragments consist of cryptocrystalline(?) grains with a deep olive green-brown color.

The groundmass (75% of the rock) consists of very fine fragments of minerals in montmorillonite.

The rock fragments range from rounded to semi angular, and are much more rounded than the quartz and plagioclase, perhaps reflecting a high content of montmorillonite in their matrices.

Sample 814-596

Reworked Volcanic Tuff - Bentonite

The rock is layered, the small layer at the corner of the section is described first.

This layer consists of subangular to subrounded fragments of quartz(10%), plagioclase(10%), cryptocrystalline quartz(?)(3%), and muscovite (1%) from 0.01 to 0.1 mm across in a matrix (0.001-0.01 mm) of montmorillonite with limonite staining. The rock contains lenses (15%) from very fine up to 0.4 mm across of coal (opaque). These are parallel to layering.

The main layer contains 30% fragments of quartz and plagioclase up to 0.1 mm (locally 0.15 mm) across. Plagioclase is slightly altered to sericite and dusty opaque, and is more abundant than quartz. Quartz is angular in outline. A few grains of apatite are 0.025 mm long.

The rock contains patches (10%) up to 0.2 mm of fine grained aggregates of montmorillonite. Coarser fragments tend to contain fibrous aggregates and parallel growths ranging in color from white to light brown. In some extinction is irregular. Optical properties are similar to those of montmorillonite described in section 809-433. Some patches contain abundant inclusions of Ti-oxide (0.002-0.005 mm).

As well the rock contains several large fragments up to 10 mm long consisting of brown montmorillonite-chlorite(?) with 5% opaque as fine grained spots and lenses. These fragments are also flattened parallel to compositional layers.

One fragment is dark brown in color, very fine grained, and apparently isotropic; it is rimmed by fine grained brown montmorillonite or chlorite.

The groundmass consists of irregularly grained (0.001-0.005 mm) montmorillonite with minor limonite stain; grains are interlocking to granular. A similar texture occurs in some coarser grained patches of montmorillonite; these may represent altered fragments or just more coarsely recrystallized and altered groundmass.

One patch 5 mm across consists of opaque (coal).

The degree of rounding of fragments, especially in the layer at one end of the section, and the lack of fragments of volcanic rocks suggests that this sample is further from the source and has been more reworked than sample 809-433. The abundance of angular fragments, particularly of quartz, suggests that the degree of reworking is still not great.

It may be significant that the thin layer at one end of the section contains the most-rounded mineral grains and also contains the major coal seam; suggesting that it is more reworked than the other part of the section.



John Payne,
November, 1976.

Thin section: Golder Brawner D.D. 44 - 2200'

Mineralogy and mode:

major (>5%)		minor (<5%)		trace (<1%)
plagioclase	26	biotite	4	zircon
sanidine	12	glass	4	apatite
white mica	14	quartz	4	amphibole
carbonate	8	zeolites	4	opaques

Fabric and texture:

Fragmental fabric consisting of sub-angular to sub-rounded lithic fragments and mineral grains in a fine-grained matrix. Tentatively, the matrix is composed of varying proportions of white mica, carbonate, clays, and zeolites. Positive identification of the constituents in the matrix is precluded by the extremely fine grain size.

Suspended in the matrix are lithic fragments of variable composition and shards of mineral grains. The mineral grains are sub-angular to sub-rounded fragments of former euhedral to subhedral plagioclase (An), sanidine, and quartz. Combined carlsbad-albite twinning of the plagioclase is common, whereas only carlsbad twinning predominates in the sanidine. The feldspar grains are often shattered in situ. Quartz grains are generally sub-rounded, but embayment of the grain boundaries is not evident. Faint undulatory extinction is occasionally visible. Deformed biotite flakes are locally part of the matrix, as well as rounded grains of zircon and opaque minerals.

Lithic fragments range from andesitic to dacitic in composition, with approximately a 5:1 andesite:dacite ratio. The fragments are in general holocrystalline, panidiomorphic-granular, porphyritic rocks with a pilotaxitic groundmass. Euhedral to subhedral phenocrysts of plagioclase, and less commonly biotite and/or quartz, are in a groundmass of crowded plagioclase microlites disposed in a sub-parallel manner. The fragments are most often sub-rounded in shape. Occurring less frequently are lithic fragments of hypocrystalline, panidiomorphic-granular, porphyritic texture. The groundmass consists of dark brown glass, occasionally microspherulitic, in which euhedral zoned plagioclase, biotite, and sanidine phenocrysts are set.

Alteration:

There is no evidence for hypogene hydrothermal alteration. Supergene (or diagenetic) processes account for the alteration assemblages which occur. The degree of alteration is variable within the fragments; some are fresh whereas others are pervasively replaced by white mica and carbonate. The phenocrysts in both the groundmass and the lithic fragments are fresh, although a few are incipiently altered to carbonate.

Classification and discussion:

The rock is a tuffaceous conglomerate in the sense that it resembles and in large part derived from pyroclastic debris or extrusive volcanic flows. Several attributes suggest that it is of sub-aqueous and perhaps fluvial origin. There is an absence of grading which would be expected in a sub-areal ash-fall. Moreover, there is no evidence of welding or flow banding in the matrix suggestive of the higher temperatures attendant pyroclastic origin. The lithic fragments are partially rounded; however, the phenocryst shards in the groundmass are more often sub-angular. This is suggestive of minimal transport from the source to the depositional site. The lithic fragments are most certainly derived from the underlying Cedar volcanics.

Mark S. Bloom

Thin Section:Golder Brawner D.D. 816 - 777.5'

Mineralogy and mode:

andesine-oligoclase groundmass	90
zeolites	8
opaques	2

Fabric and texture:

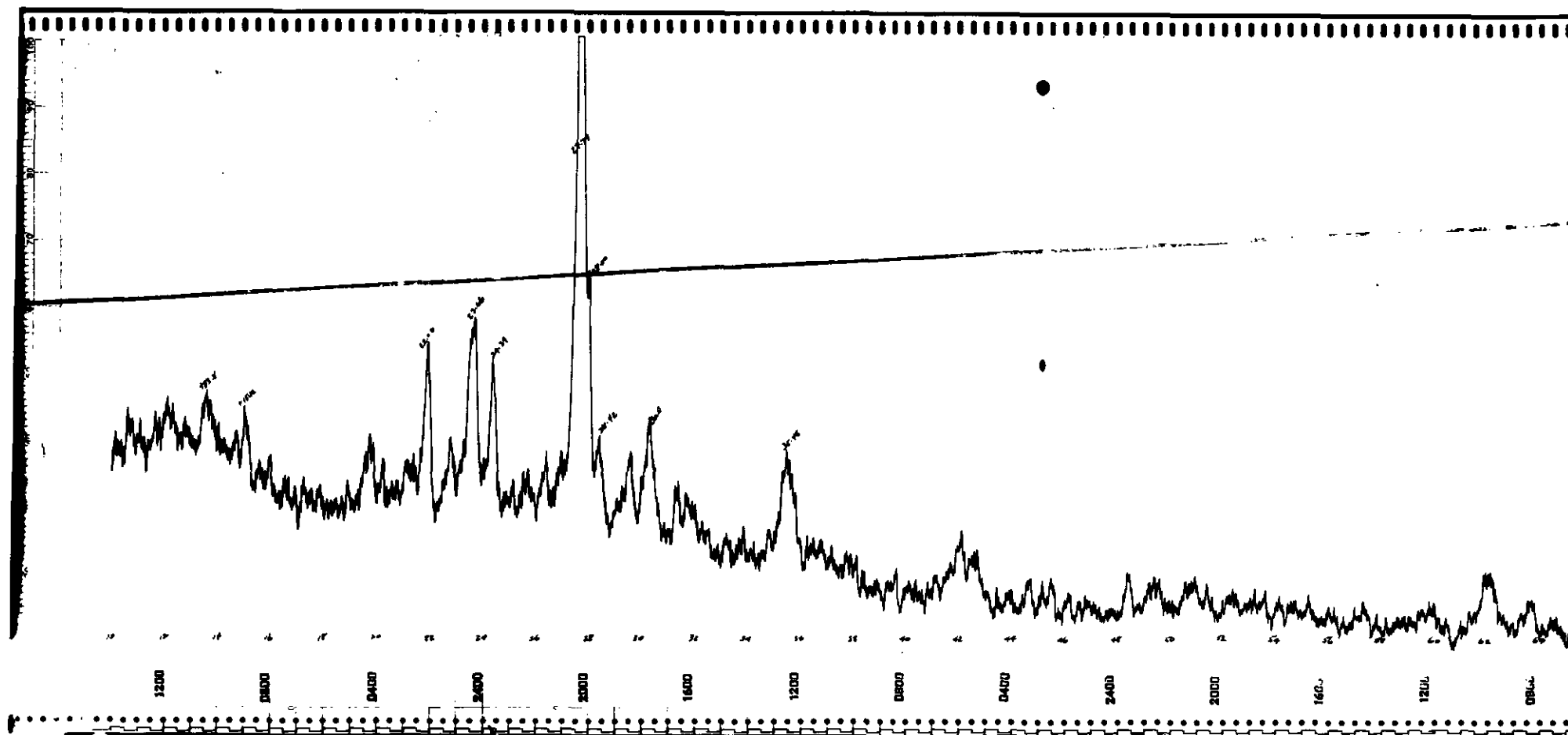
Pilotaxitic groundmass, i.e., crowded euhedral to subhedral plagioclase microlites disposed in a sub-parallel manner. Elongated areas shaded by increased opaque mineral content are possibly relic lithic fragments.

Elongated amygdaloidal cavities prescribe to a regular concentric sequence of mineralization. From the groundmass into the amygdule, this sequence is a brown, colloidal material (possibly chlorite) which is in turn covered by a colloform, fibrous zeolite. The final phase of mineralization is crystallization of euhedral to subhedral zeolites in the core.

Classification and discussion:

On the basis of the information at hand, I suggest that this rock is an amygdaloidal andesite. The exceedingly fine grain size renders microscopic identification of groundmass constituents at best tentative; however, an X-ray powder pattern confirms the presence of andesine-oligoclase. There is no evidence for hypogene hydrothermal alteration, and the filled amygdules are unaltered as well. There is no evidence for strong shearing of the rock; plagioclase microlites are regularly oriented, euhedral, and optically continuous.

Mark S. Bloom



X-RAY DIFFRACTION PATTERN OF ROCK SAMPLE FROM DDH 76-816 AT 777.5'.

APPENDIX 3

X-RAY DIFFRACTION STUDIES

APPENDIX 3
X-RAY DIFFRACTION STUDIES

Analysis of the mineralogy of the rocks of the Coldwater Formation sequence by X-ray diffraction has been undertaken by the University of Western Ontario for GA and by the University of British Columbia directly for BCH. The University of Western Ontario reports are included in this appendix in their entirety. A summary of the UBC results is also included.

Four analyses of clay samples arising from the coal sampling for Birtley Engineering are also contained in this appendix.

The previous X-ray diffraction work carried out by the University of Western Ontario for Dolmage-Campbell & Associates is not included here, but may be found in the DCA Rock Mechanics Report dated 1975.



The University of Western Ontario, London, Canada

JUL 27 1976

Faculty of Engineering Science

26 July 1976

Mr. G. Rawlings
Golder, Brawner & Associates Ltd.
224 West 8th Avenue
Vancouver, British Columbia
V5Y 1N5

Dear Mr. Rawlings:

Hat Creek Project - Mineralogical Analyses

I am pleased to enclose two copies of our first set of x-ray and carbonate data for nine separate specimens received between June 24 and July 15, 1976. As I mentioned by phone, we are set up with a scheme that will enable us to mail you back the x-ray and carbonate data within one week of receipt of the samples.

Since we seem to be receiving samples from two or three people, and since the samples are not arriving in any particular order, I have presented the data in the sequence received as noted on the table.

Basically, the soils received so far all contain abundant montmorillonite plus quartz and feldspar as noted on the x-ray powder patterns. Two samples contain abundant carbonate (DH 803, 595' - 596' and DDH 803, 316' - 318'). For the present time, we have tentatively identified the carbonate as an impure siderite since peaks for calcite and dolomite are absent on the x-ray traces.

I hope that this format meets with your approval, and look forward to your comments. Selected glycol retentions and Na^+ analyses will be run when we have a more complete suite of samples or at your instruction.

Yours sincerely,

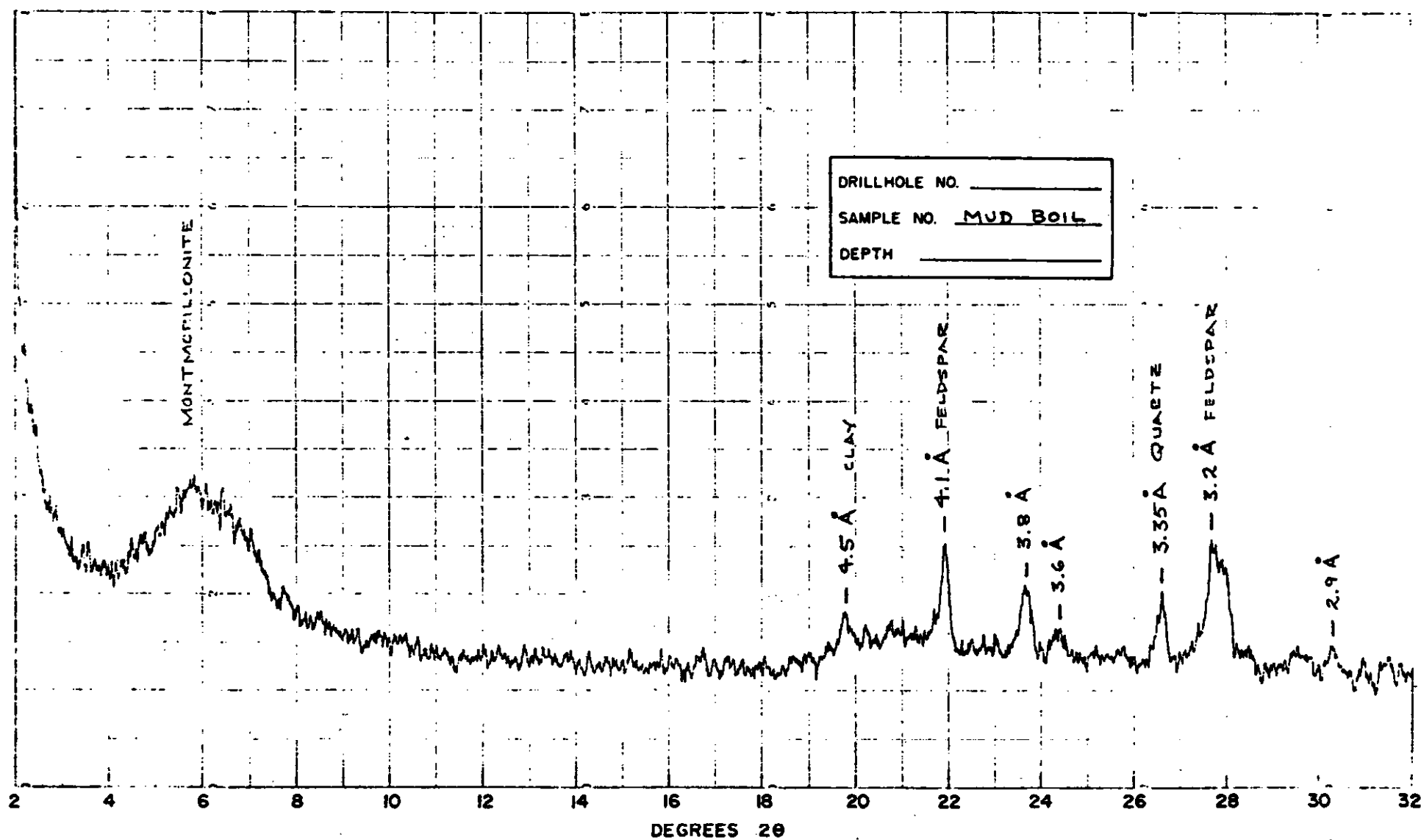
R.M. Quigley
Professor and Head
Geotechnical Section

RMQ:em
Enclosures

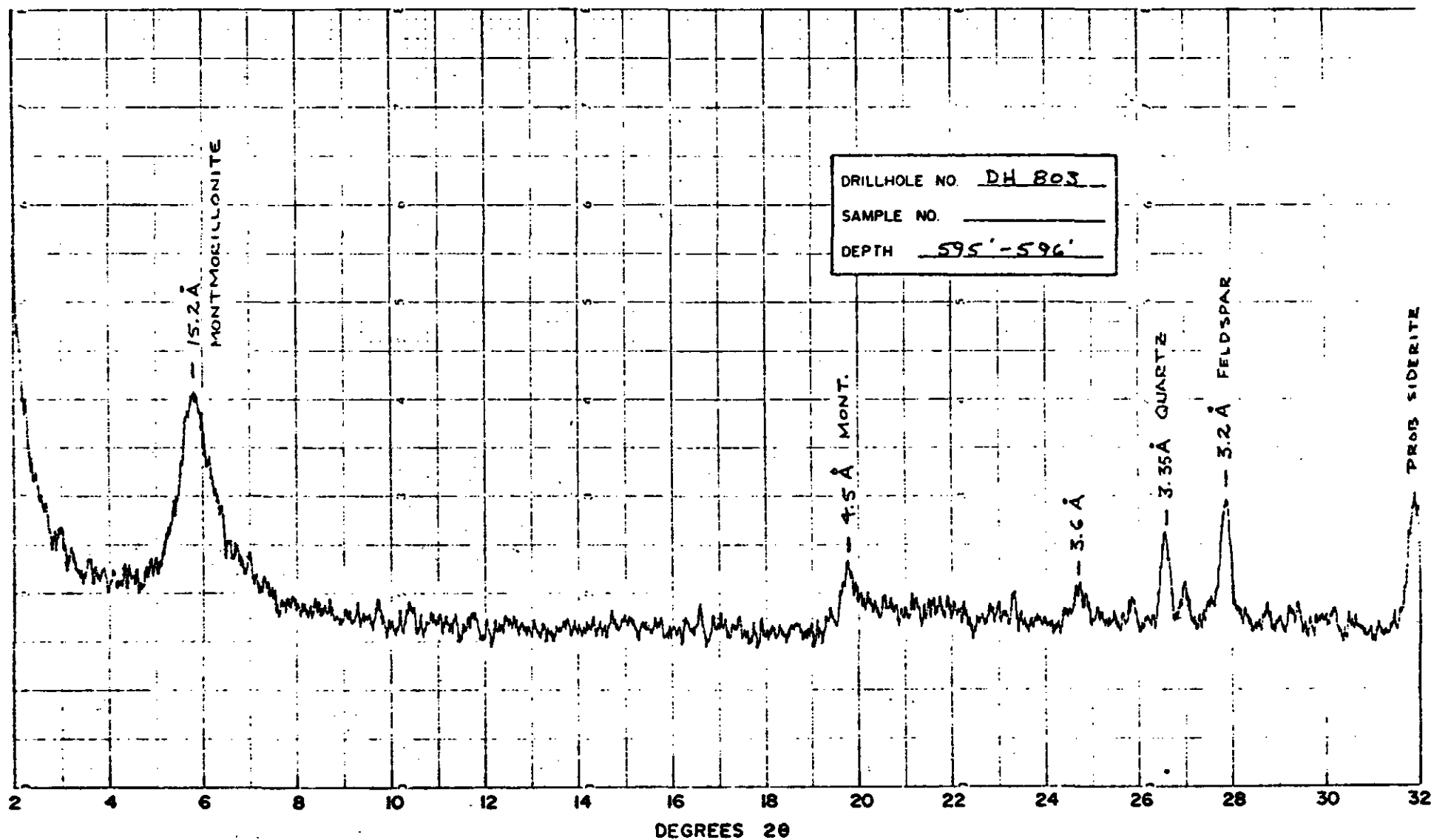
ACCOUNT 1319-502

DRILL HOLE NO.	SAMPLE NO.	DEPTH	DATE REC'D	TESTING COMPLETED						
				X - RAY				CARBONATE	GLYCOL RETENTION	Na ⁺ (PPM)
				WET P.O.	ADPO	GPO.	POWDER			
	MUD BOIL		JUNE 24	✓	✓	✓	✓	4.0		
DH 803	NOT GIVEN	595-596	JULY 6	✓	✓	✓	✓	17.1		
DDH 804	1A	50.0'-51.7'	JULY 13	✓	✓	✓	✓	1.7		
DDH 806	7	16.8'-18.8'	JULY 13	✓	✓	✓	✓	1.3		
DDH 803	28	136.0-137.0 135.0-136.0	JULY 15	✓	✓	✓	✓	1.7		
DDH 803	29	316.0'-317.7'	JULY 15	✓	✓	✓	✓	32.4		
DDH 805	16	GREEN BLACK	61.5'-62.5'	✓	✓	✓	✓	5.3 1.1		
DDH 807	12	22.0'-24.0'	JULY 15	✓	✓	✓	✓	2.4		
DDH 807	14	158.3'-159.5'	JULY 15	✓	✓	✓	✓	1.7		

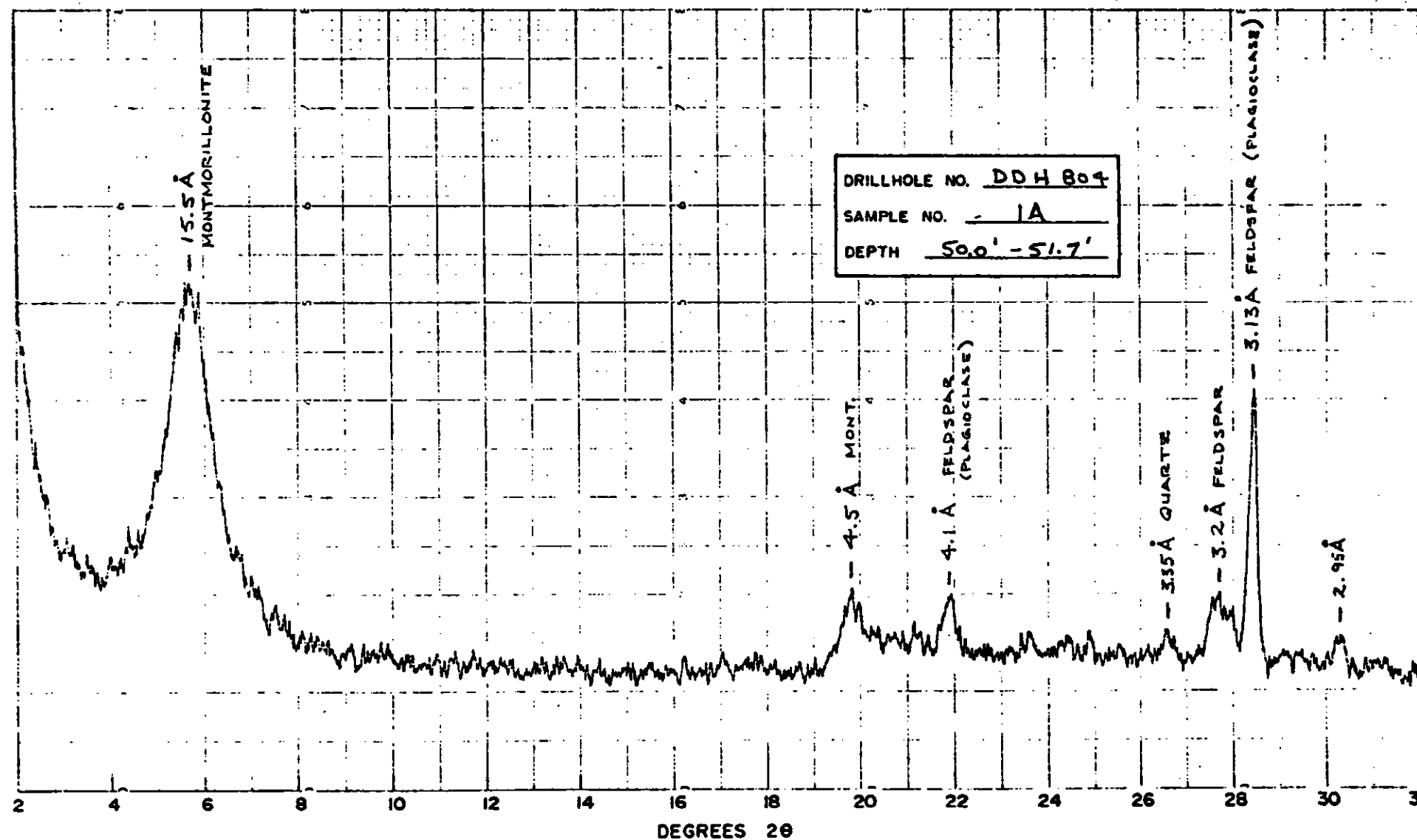
GEOTECHNICAL LABORATORY
 UNIV. OF WESTERN ONTARIO
R. M. Quigley
 July 23 /76



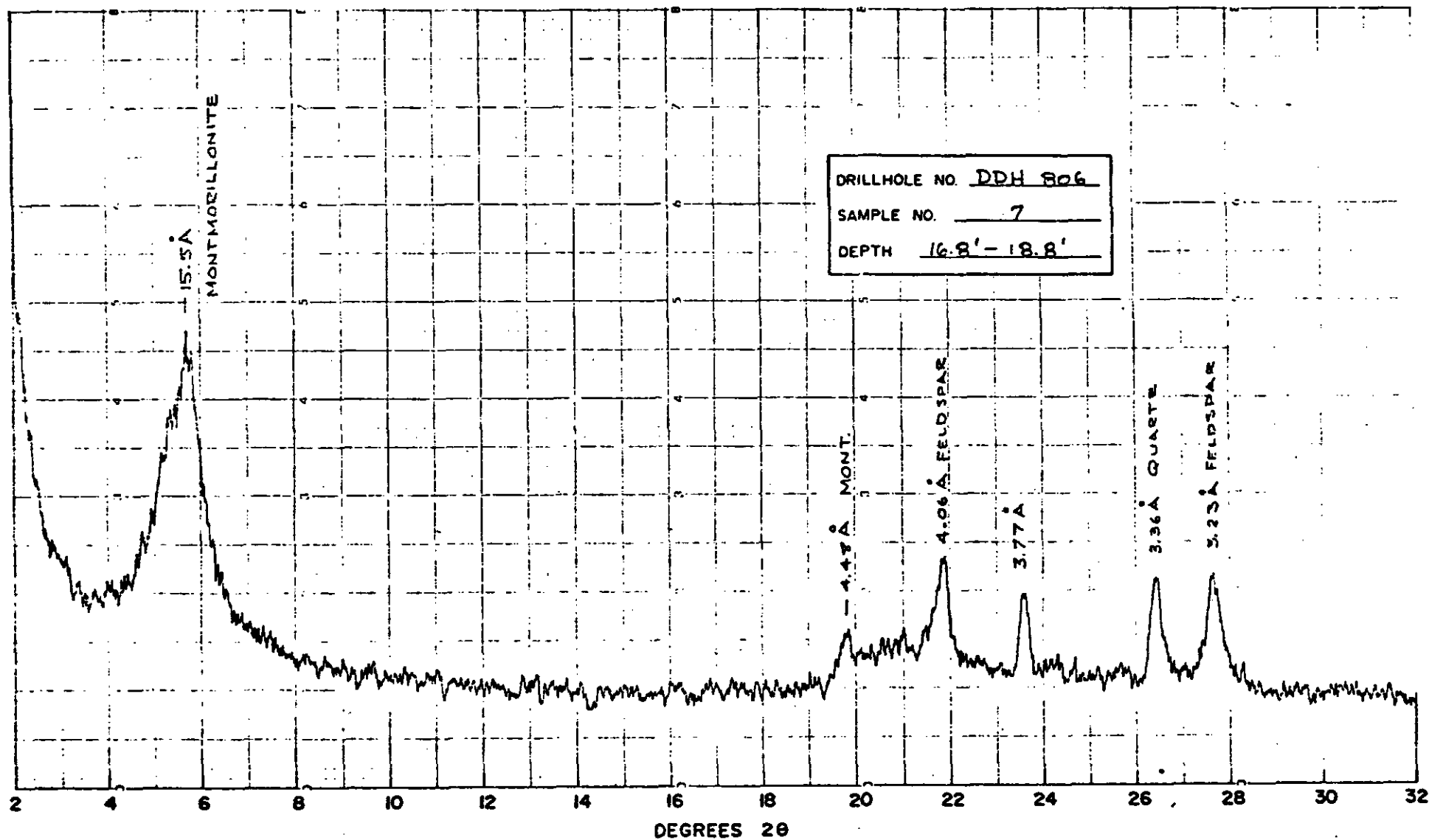
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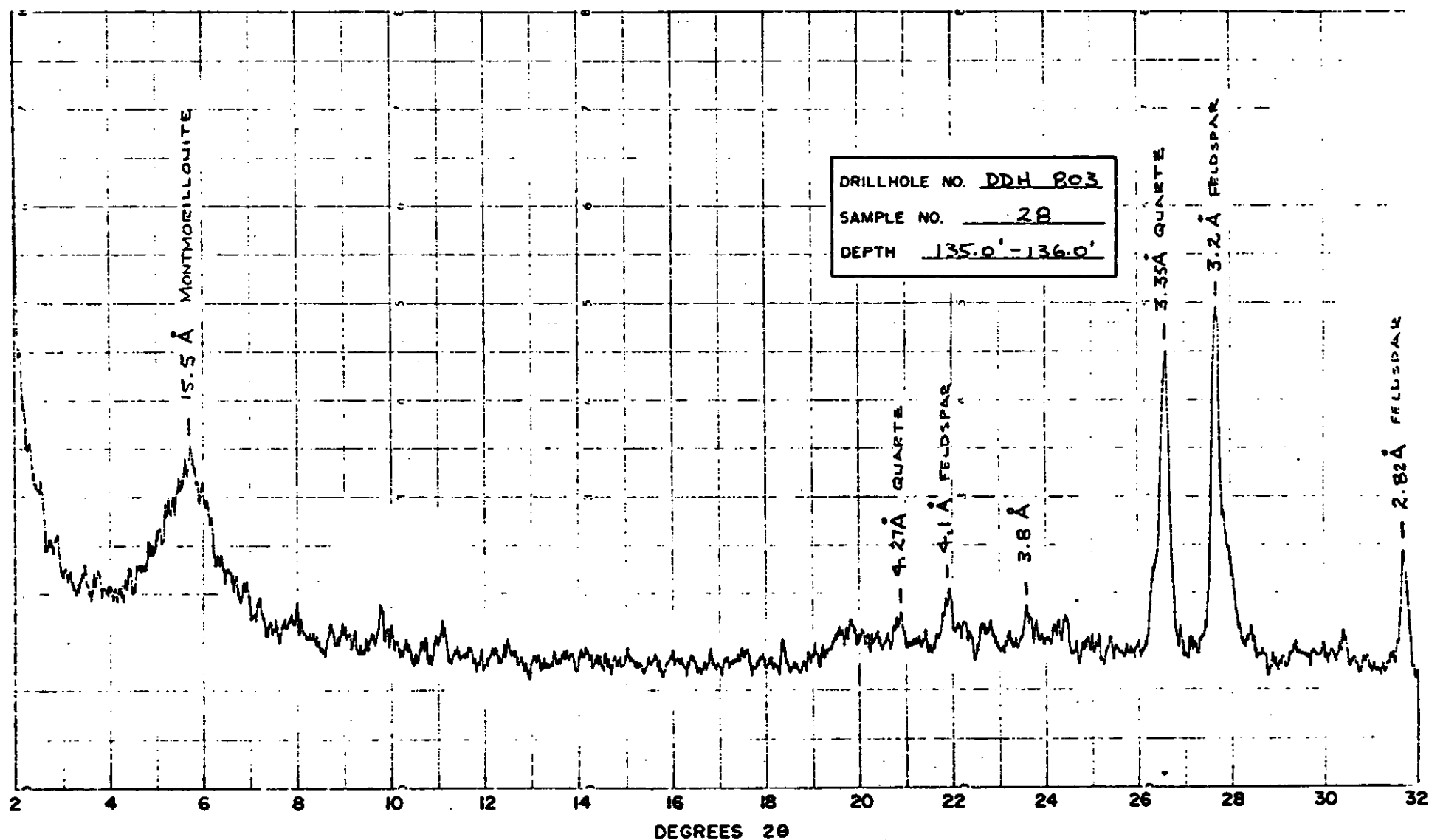
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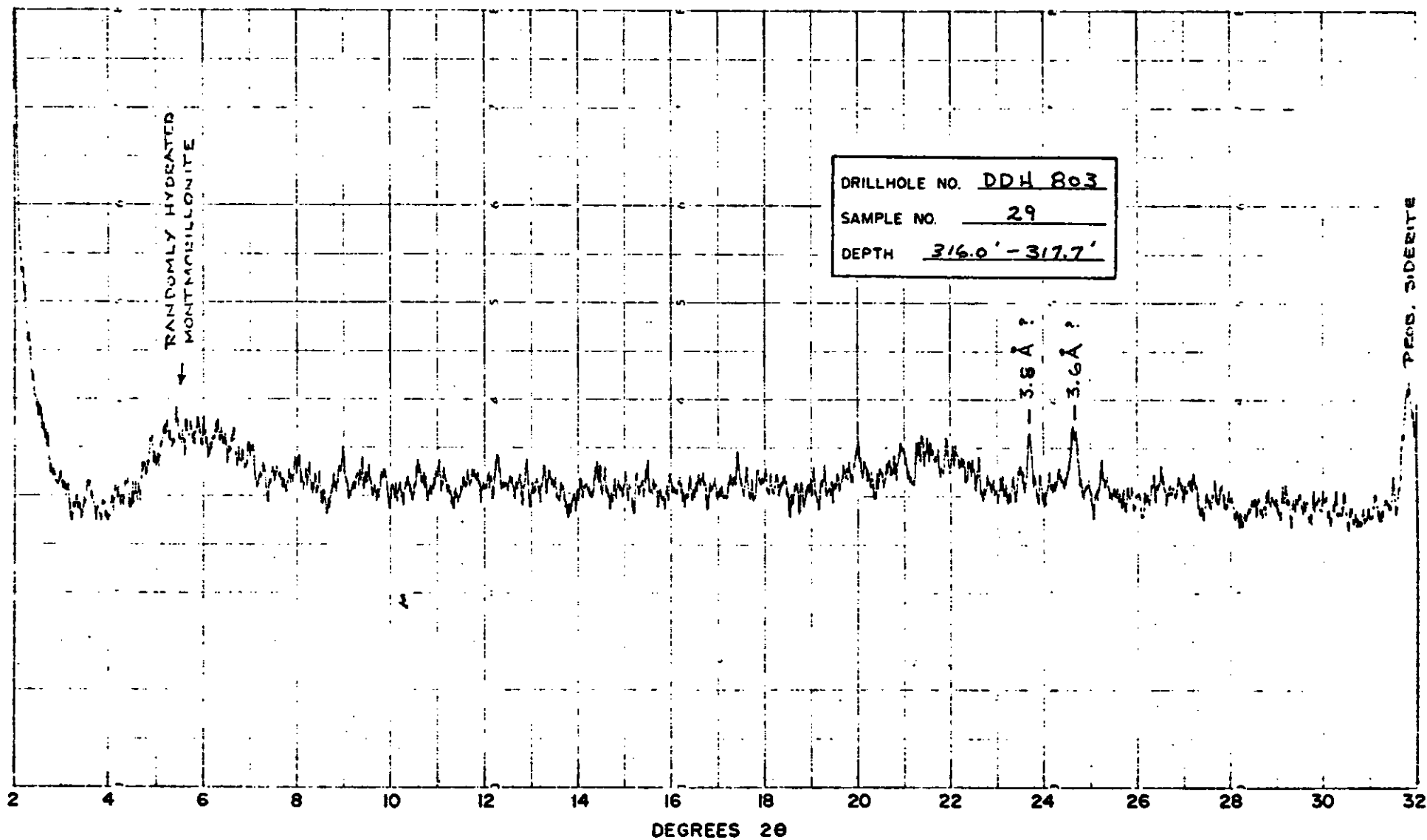
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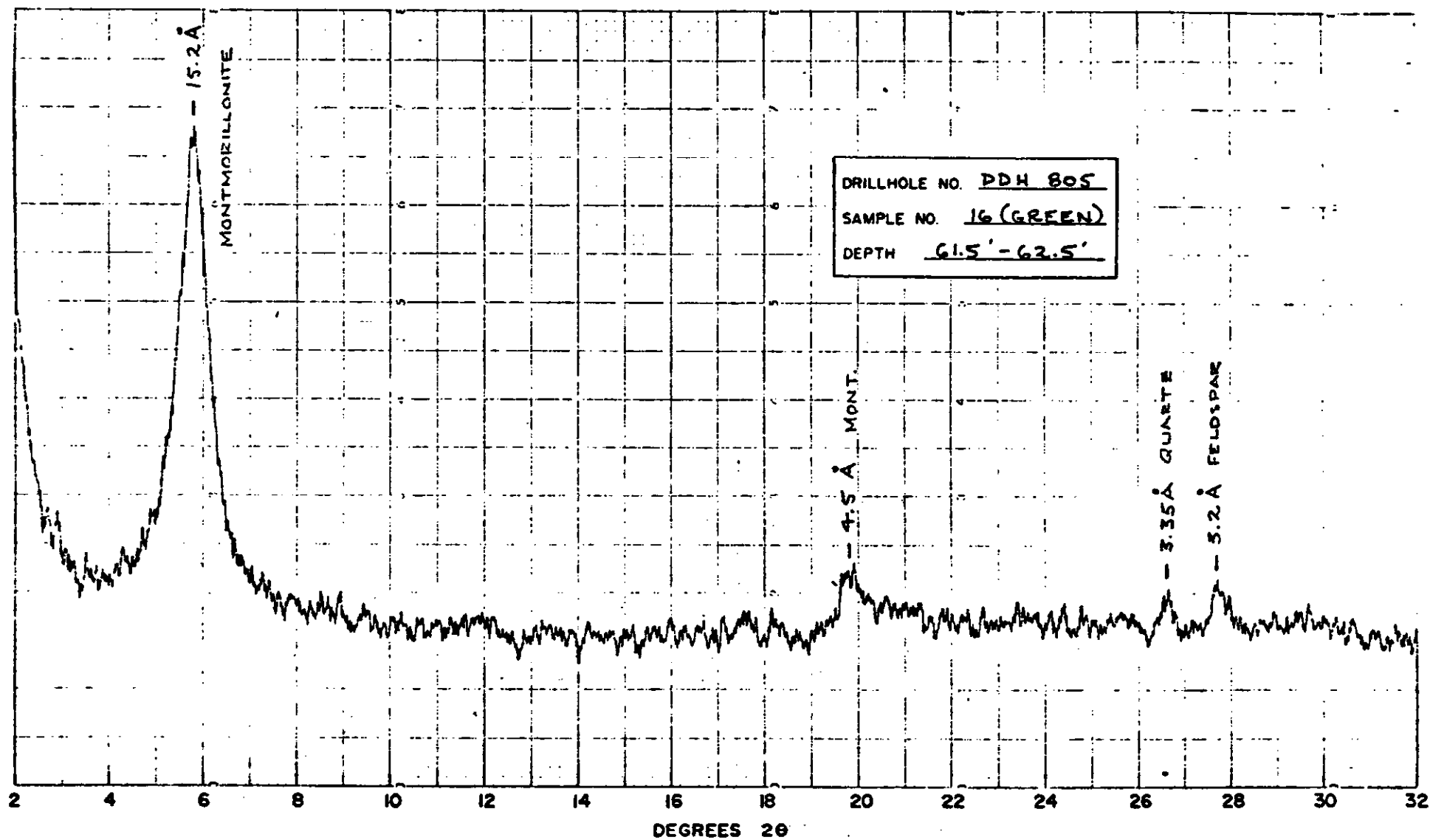
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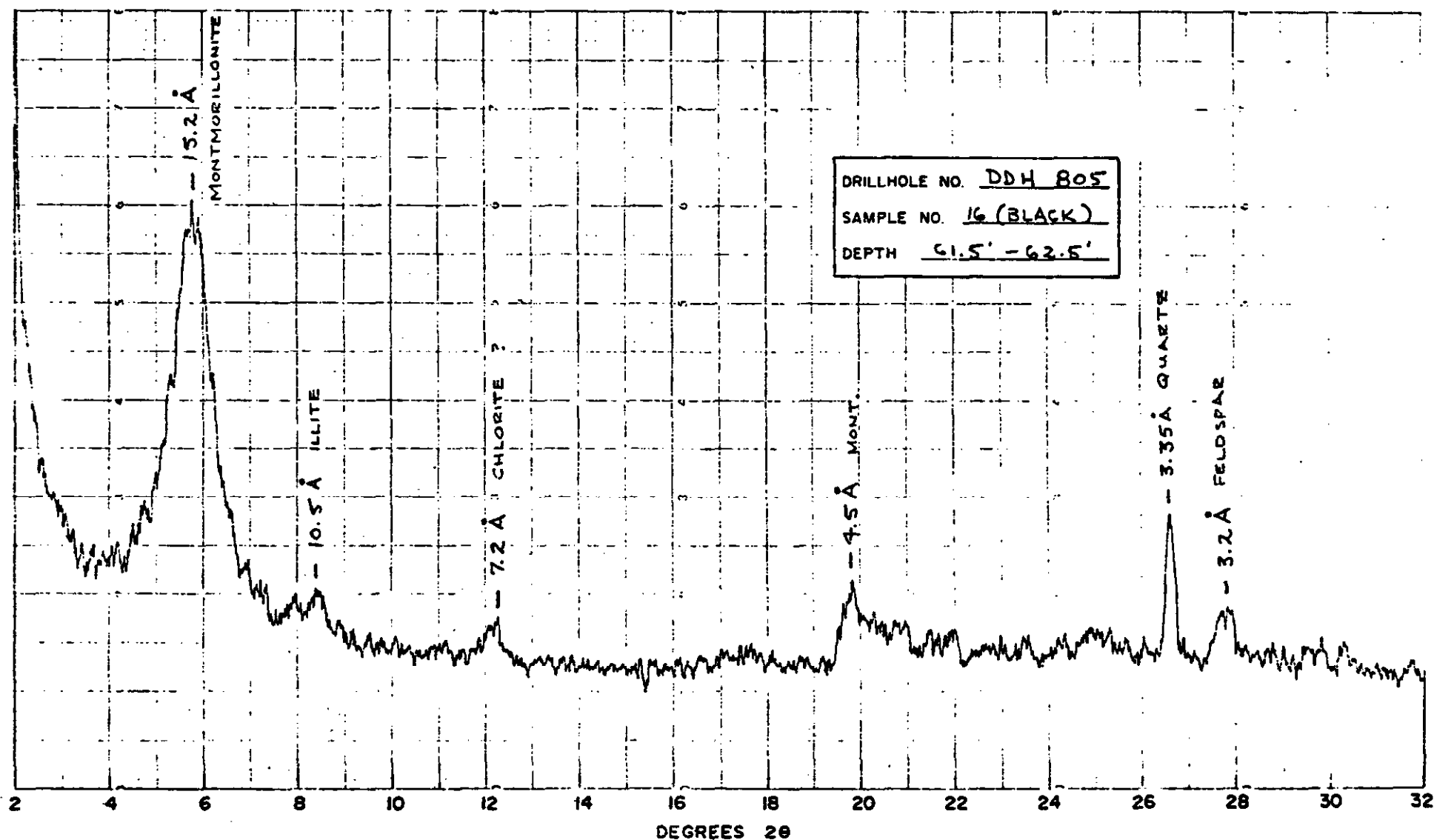
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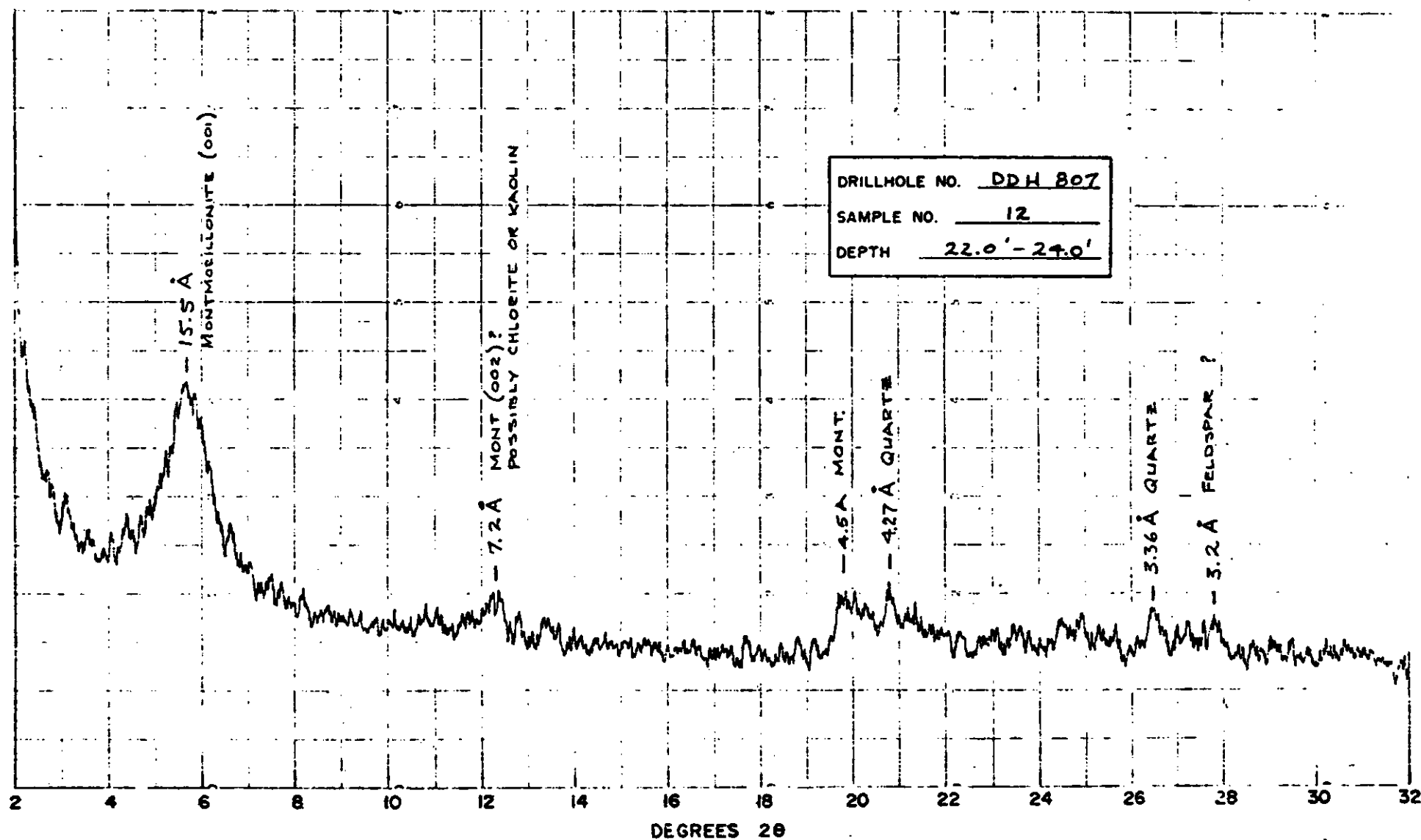
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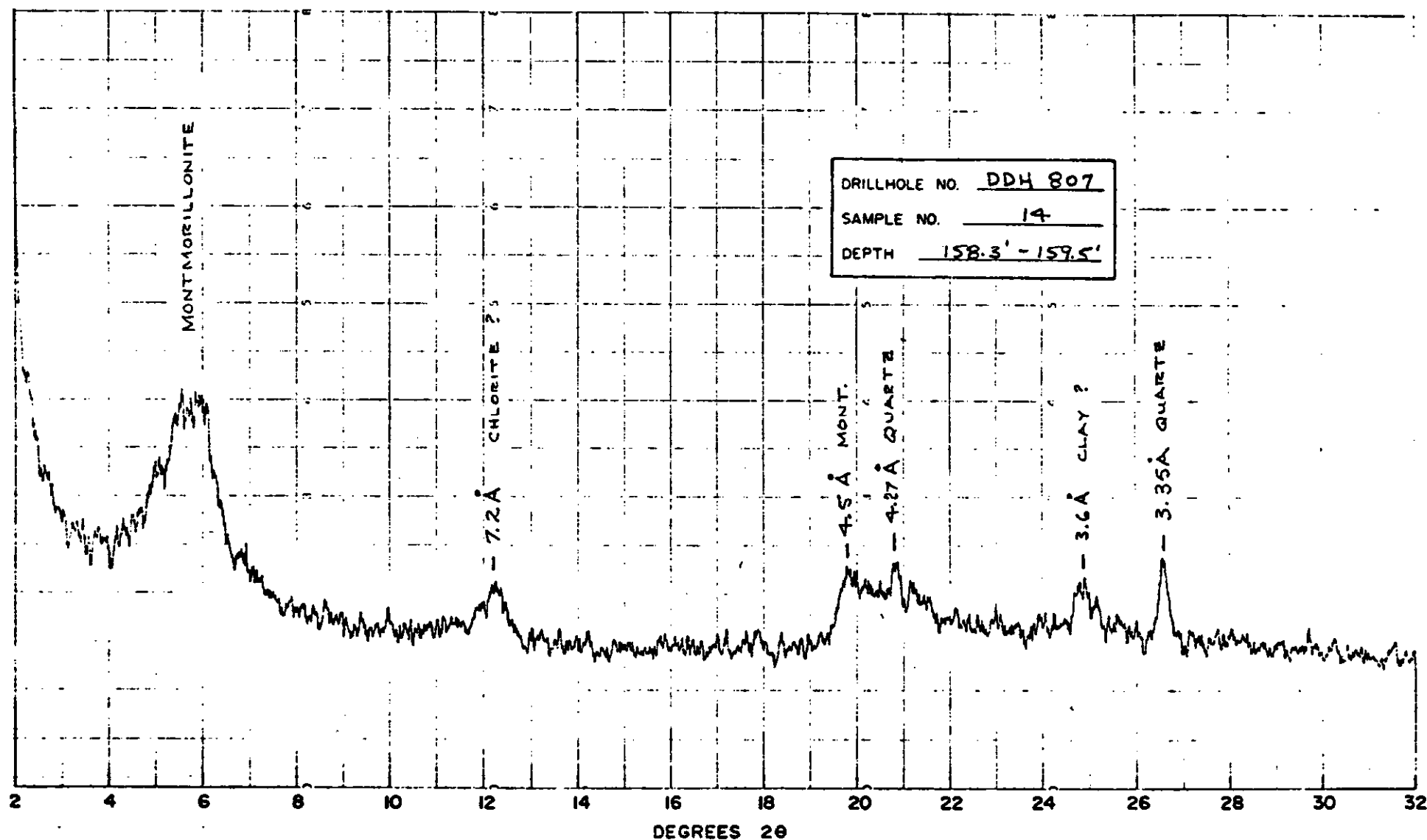
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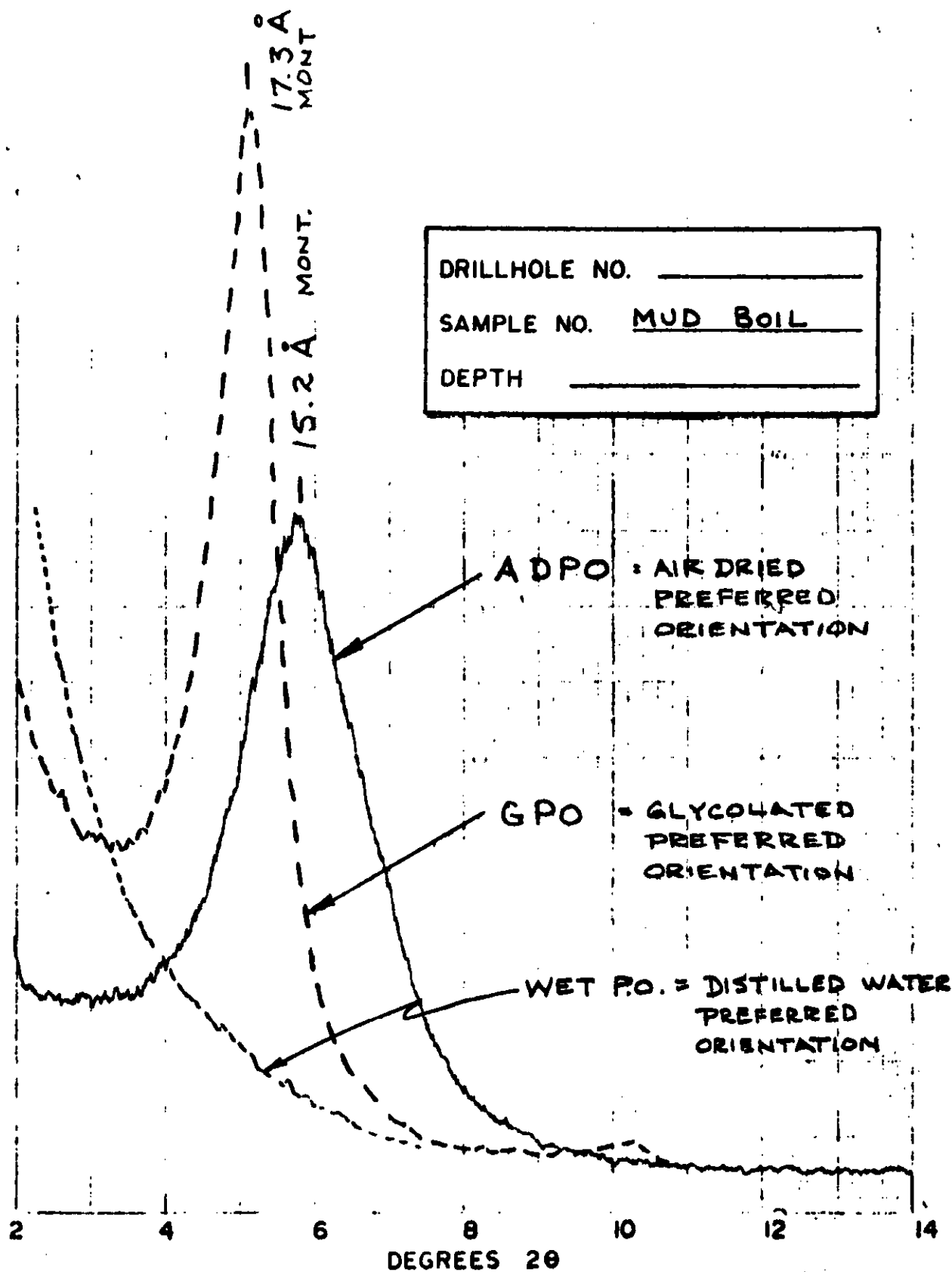
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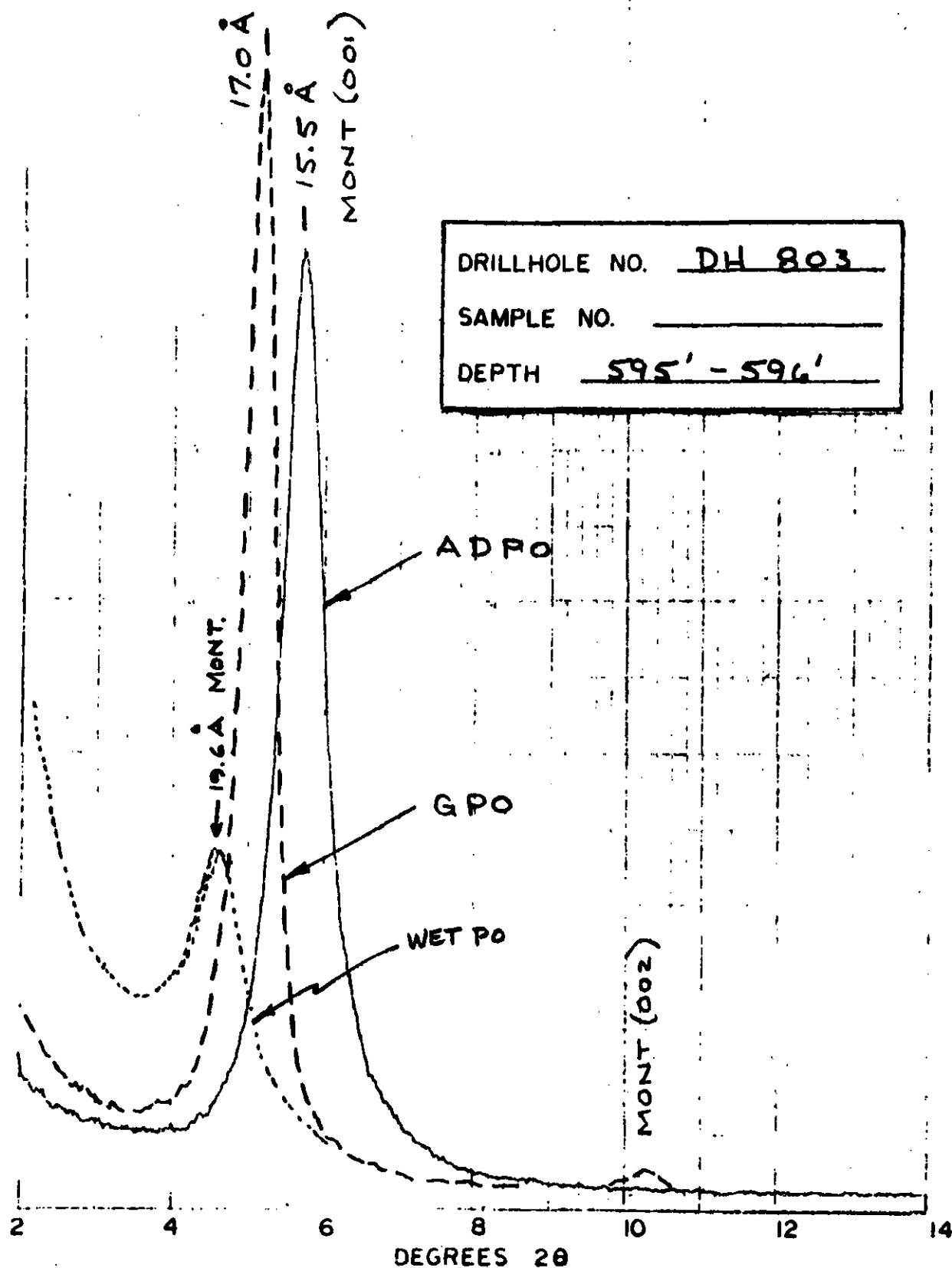
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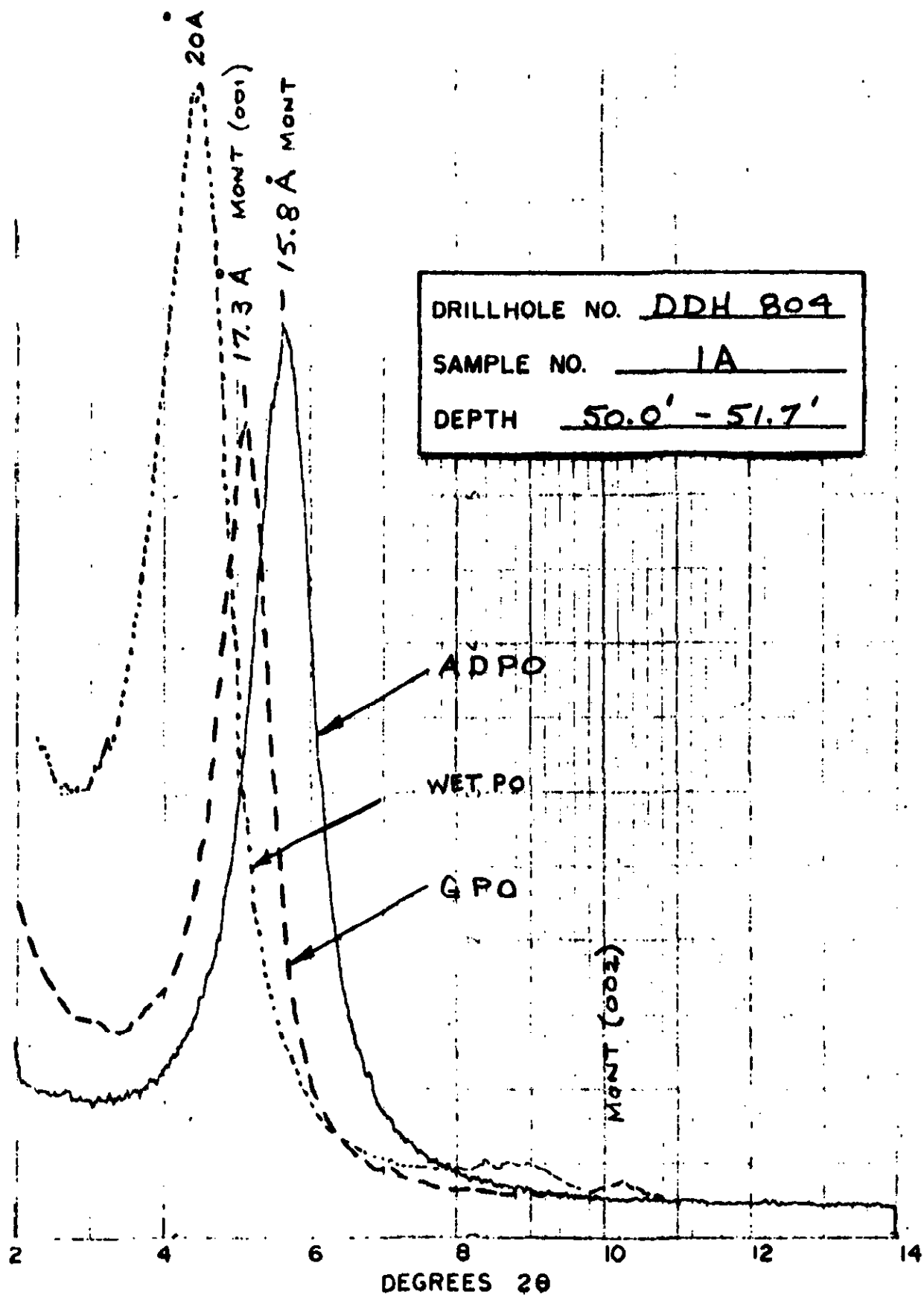
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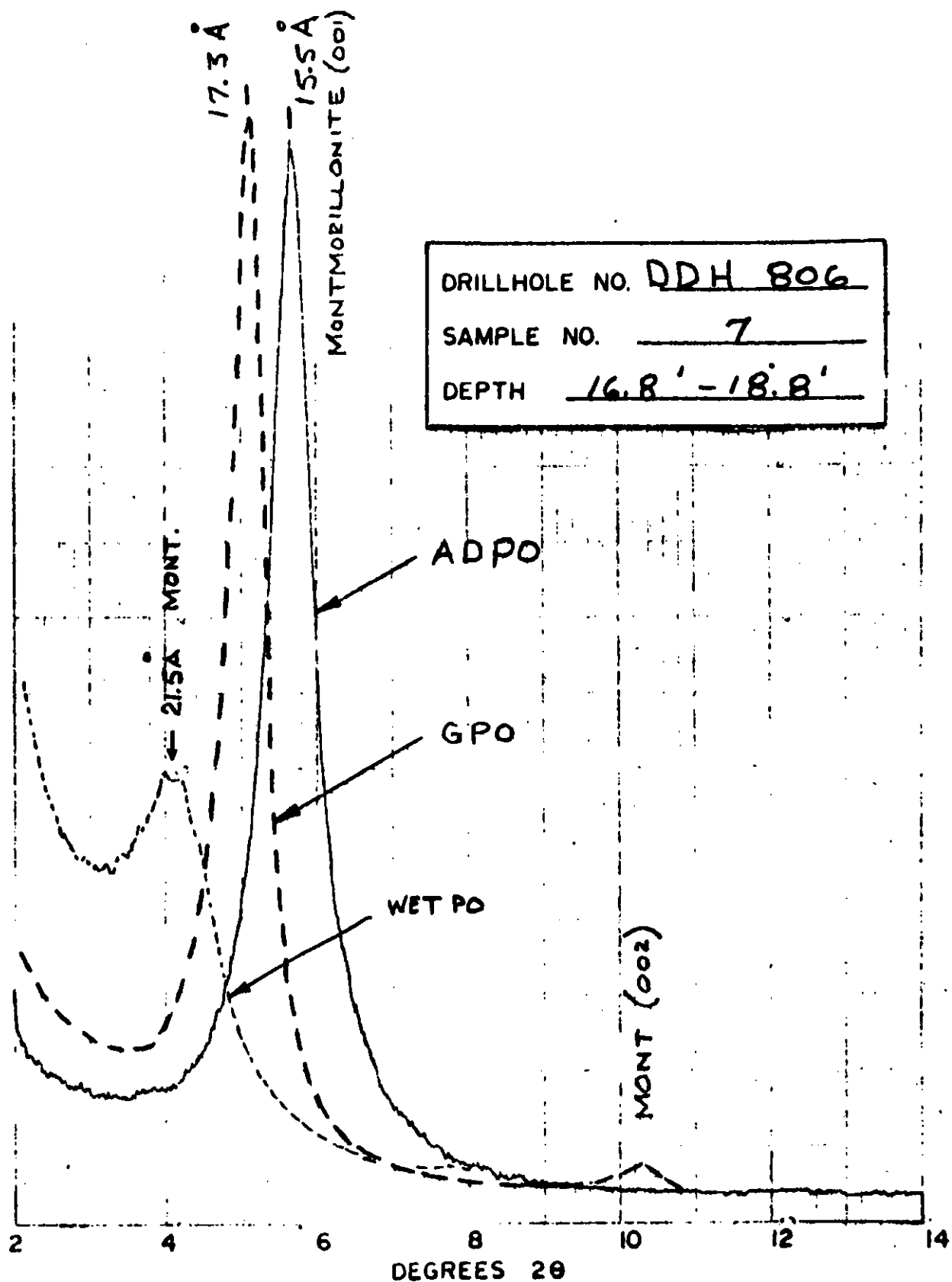
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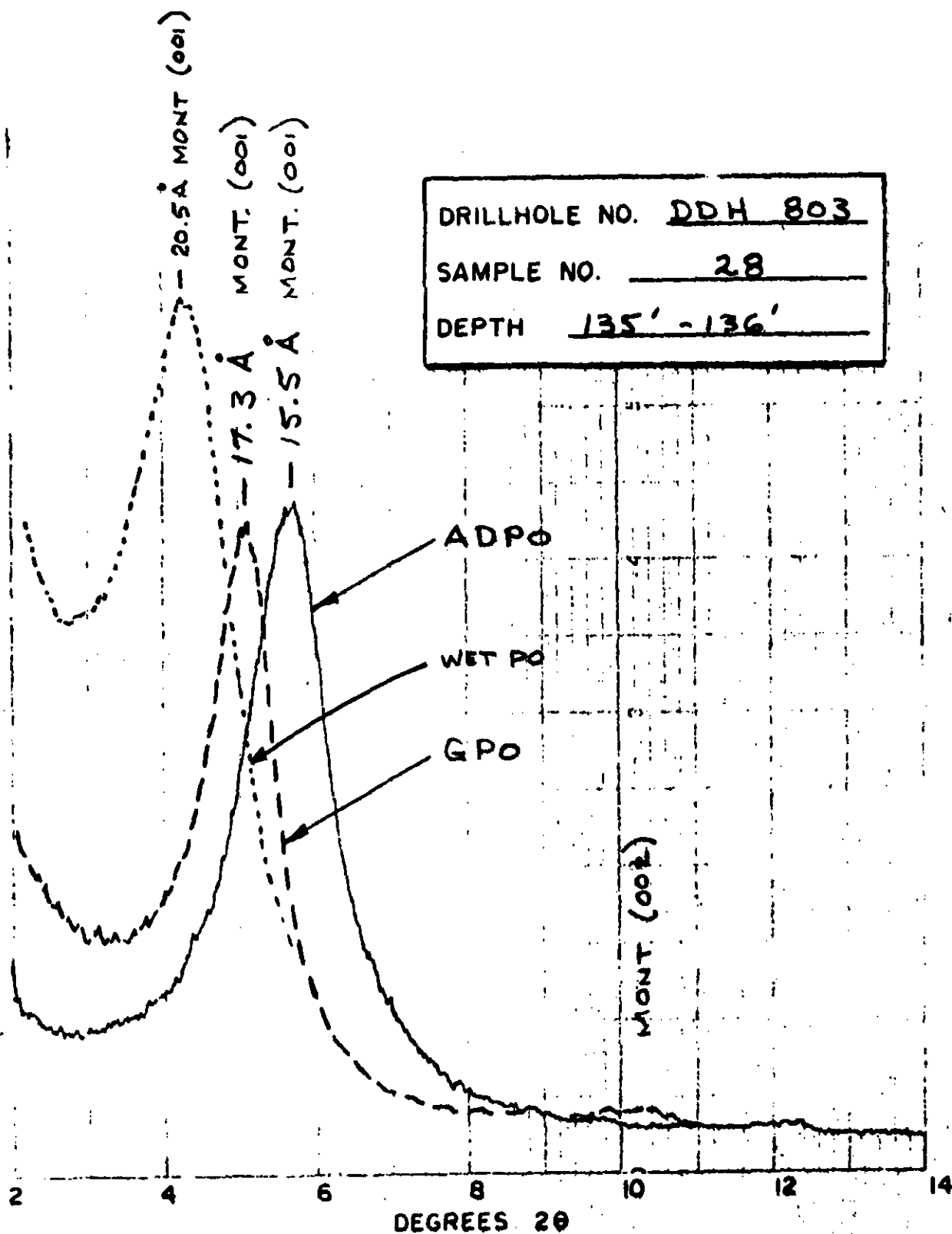
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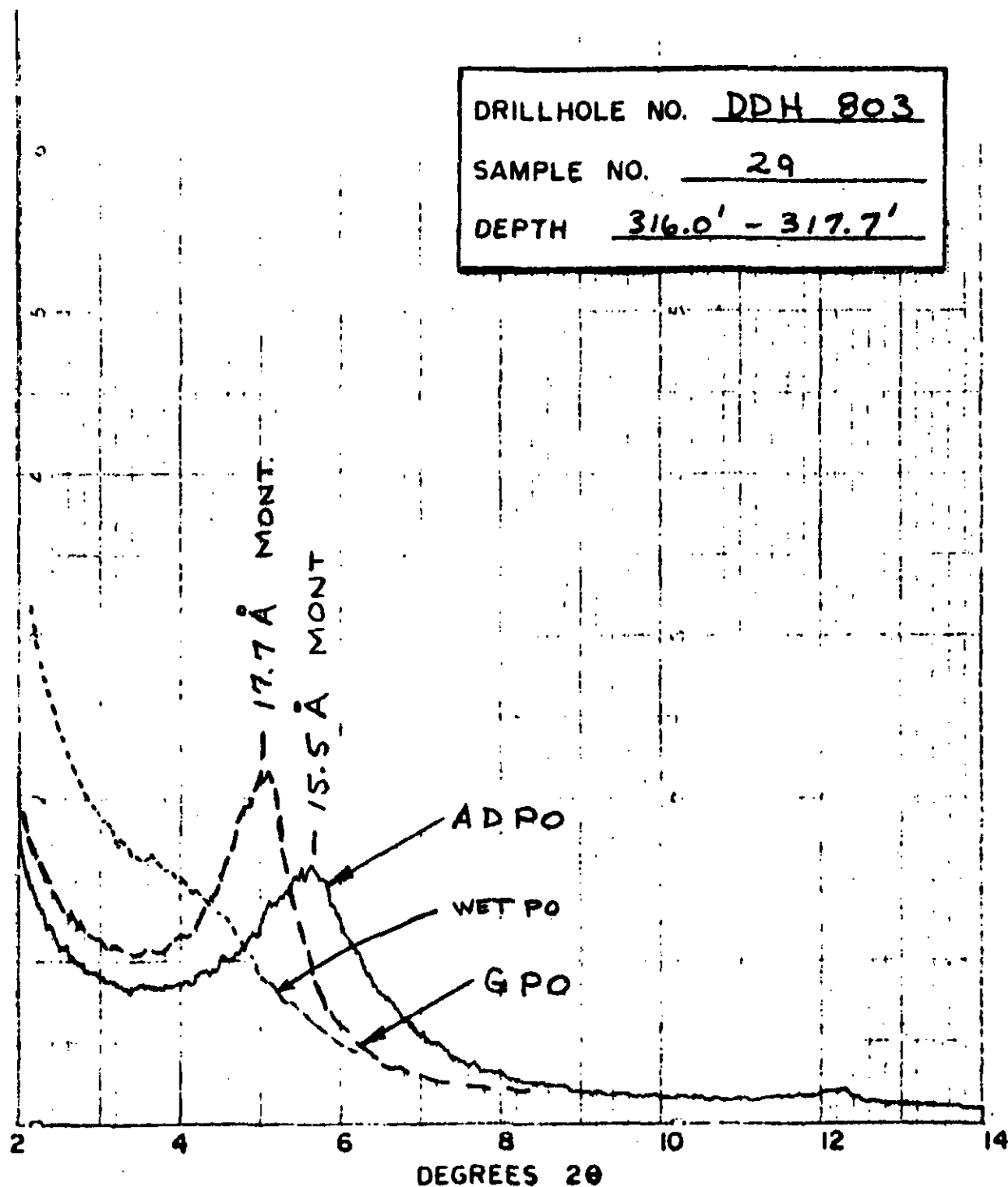


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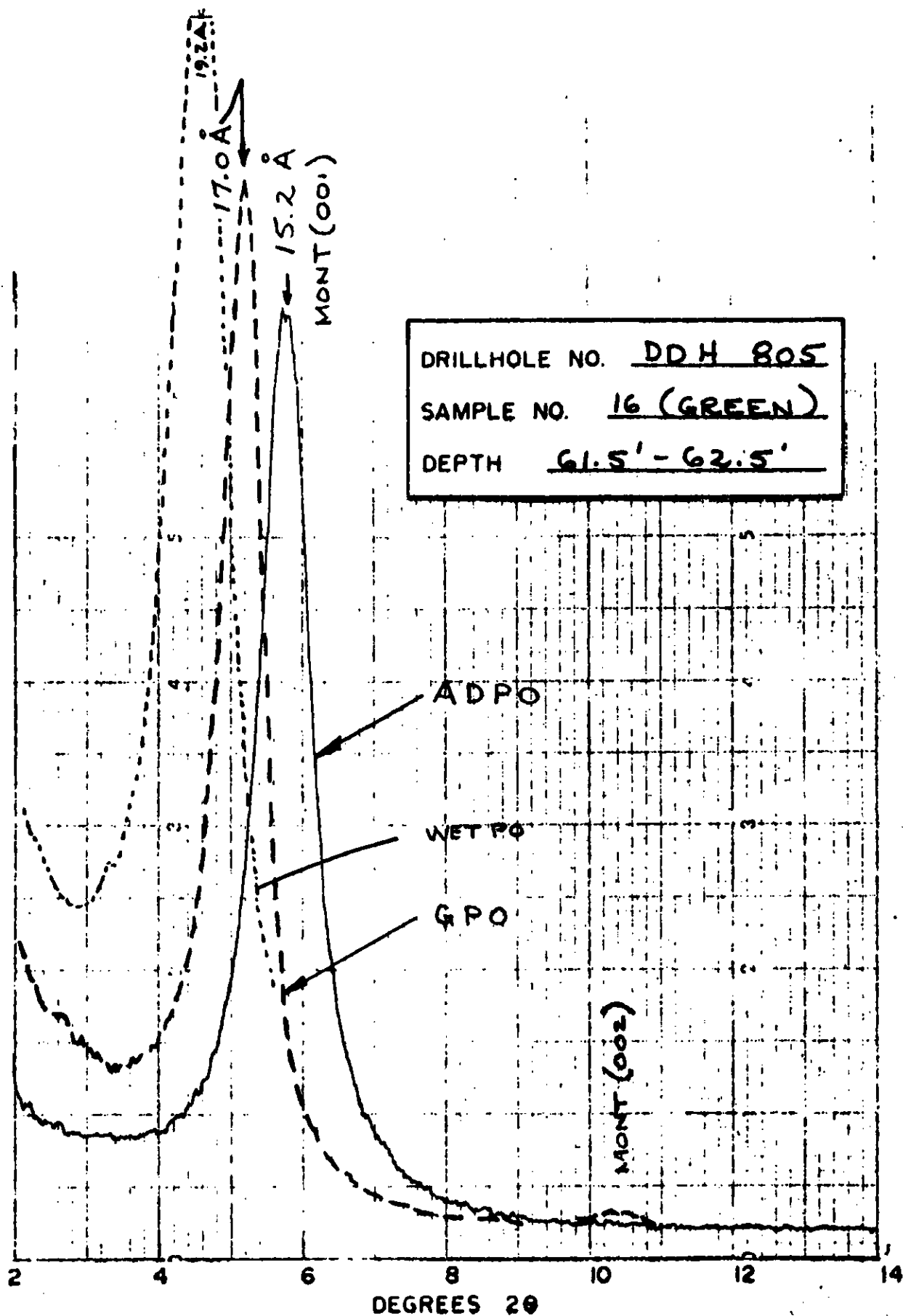
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The Univ. of Western Ontario

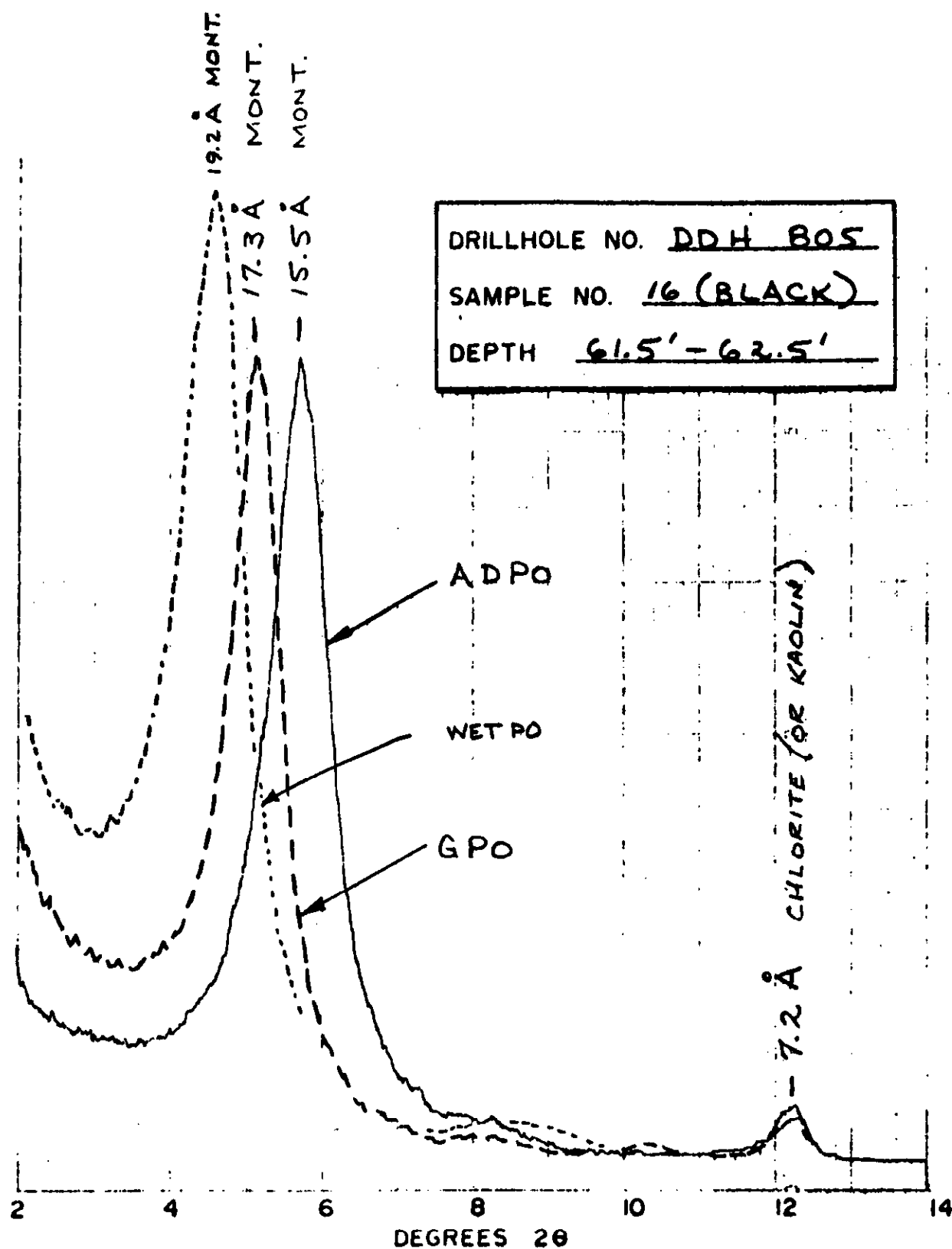


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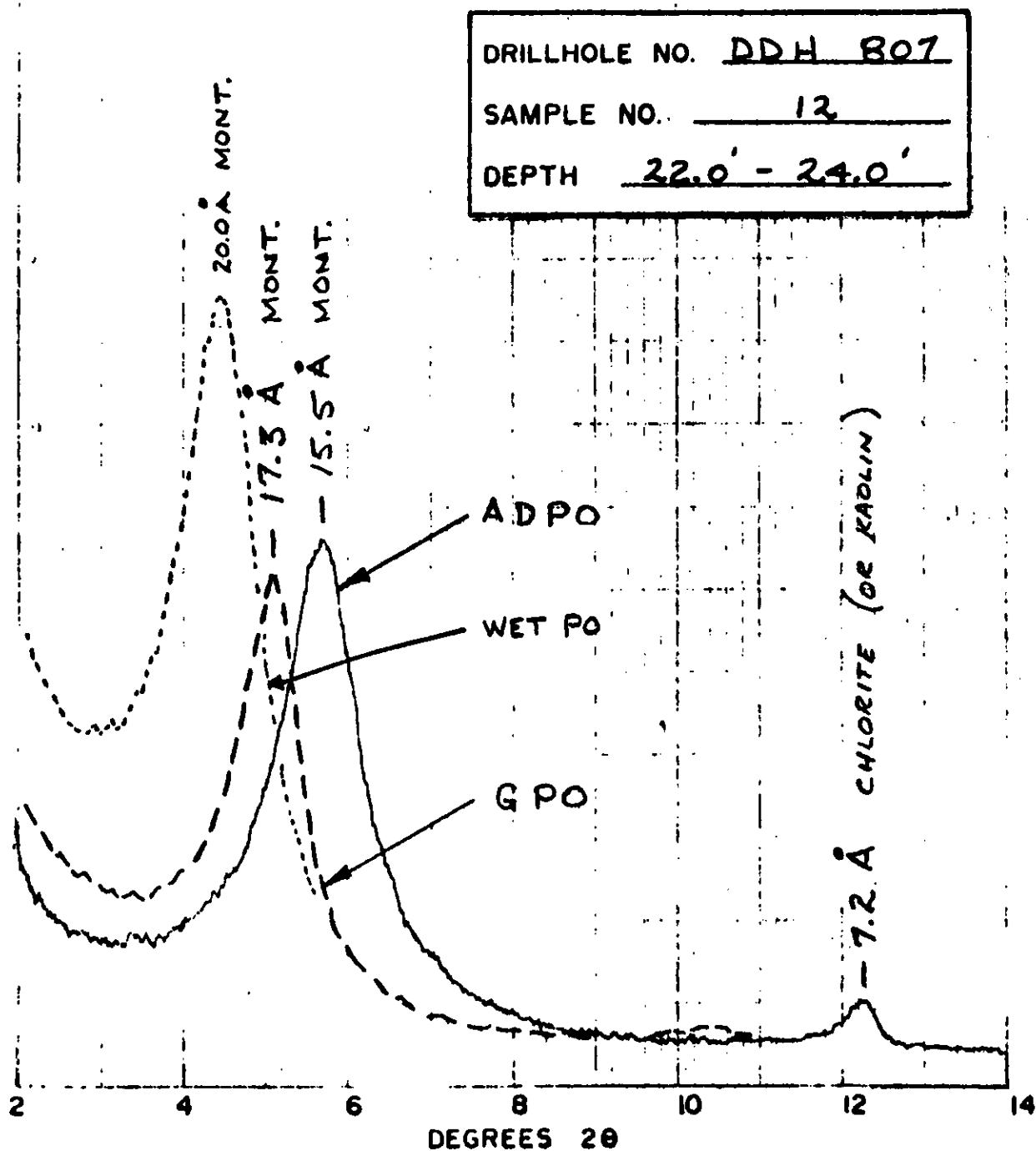


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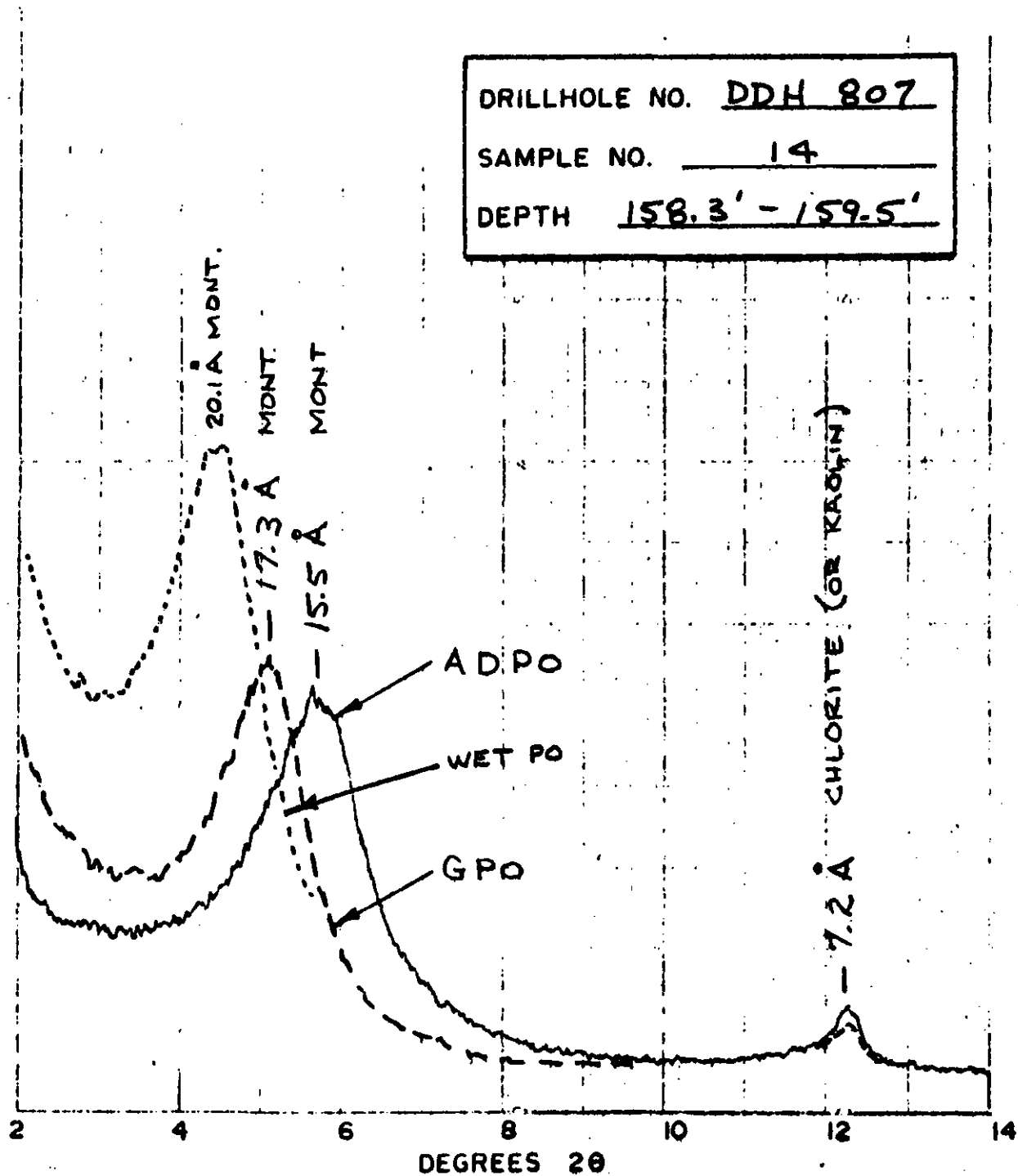
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Geotechnical Laboratory
 The Univ. of Western Ontario



X-RAY DIFFRACTION TRACES OF 2μ, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.

FEB 15 1977



FILE No.

The University of Western Ontario

Faculty of Engineering Science
London, Canada
N6A 5B9

August 13, 1976

Mr. G. Rawlings
Golder, Brawner & Associates Ltd.
224 West 8th Avenue
Vancouver, B.C.
V5Y 1N5

Dear Mr. Rawlings:

Report #2
Hat Creek Project - Mineralogical Analyses
August 13, 1976

We have completed x-ray and carbonate analyses on 9 of the 25 samples received on August 3, 1976 from Mr. H. Hawson. The results, which are all for B.H. 74-28, are reported in our Report #2 attached.

The delay in processing has been caused by the indurated nature of many of the samples making disaggregation into finer fractions very difficult.

The current suite of samples from Borehole 74-28 shows a highly variable carbonate content, most of which appears to be an impure siderite (see Table). Where siderite is of lesser importance, the silicate minerals quartz and feldspar become the dominant non-clay mineral components.

In the <2 μ fraction, montmorillonite dominates, yielding the very strong (001) peaks shown in the traces for the preferred orientation samples.

Yours sincerely,

R.M. Quigley, P.Eng.
Professor and Head
Geotechnical Section

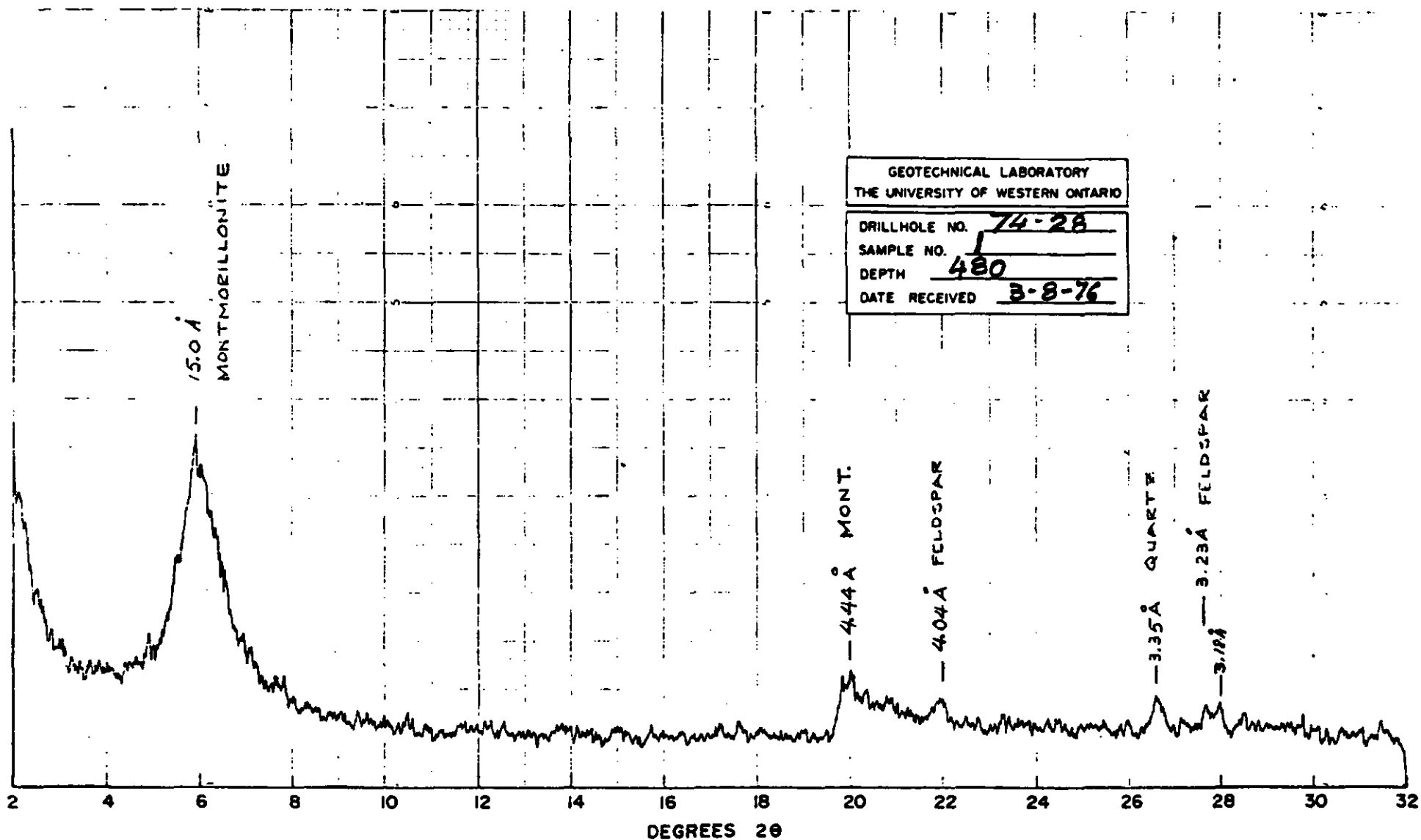
RMQ/jl
Attach.

cc. Mr. H. Hawson ✓

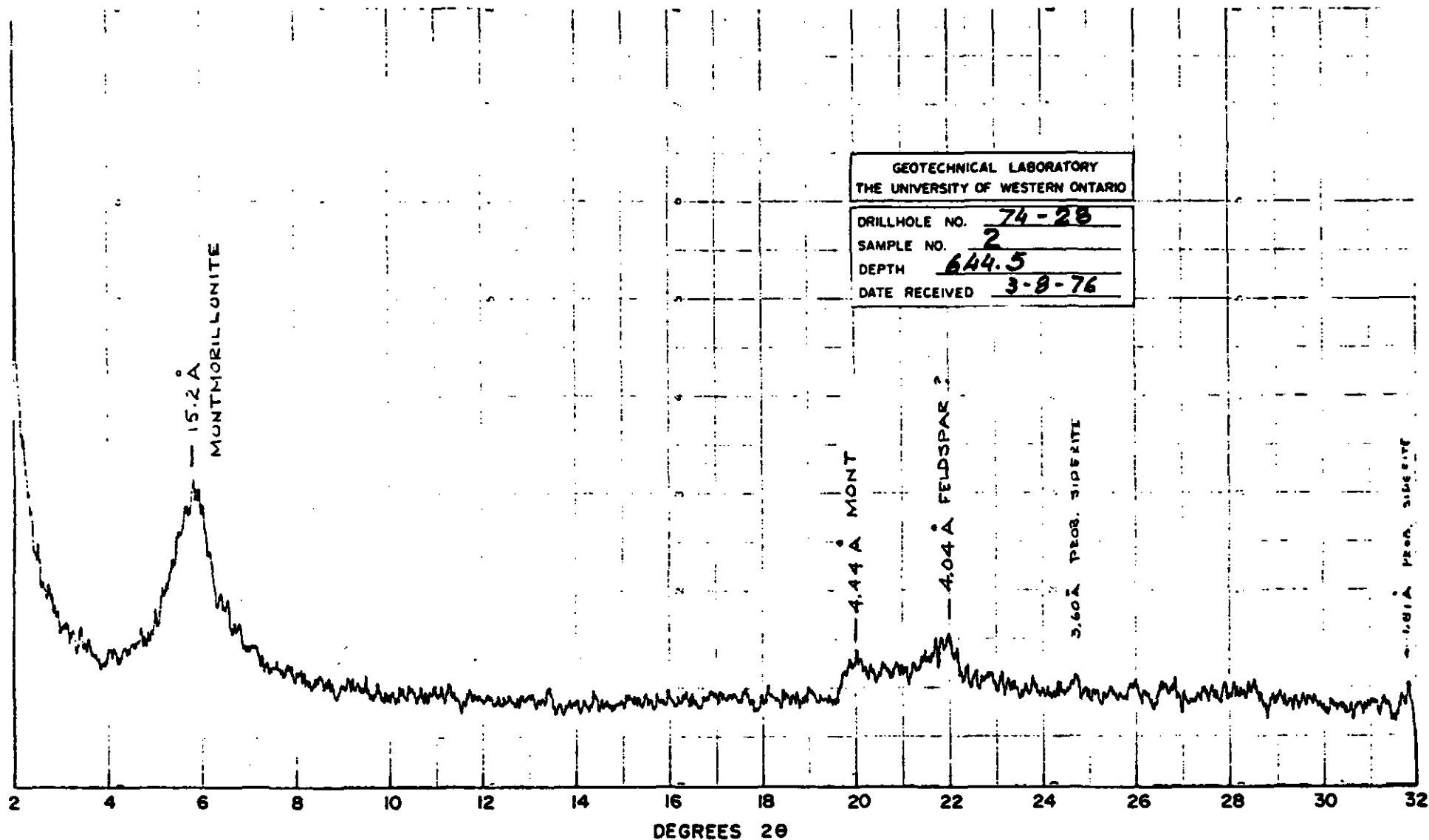
LIST OF SAMPLES RECEIVED FROM GOLDER BRAWNER & ASSOCIATES

THE UNIVERSITY OF WESTERN ONTARIO

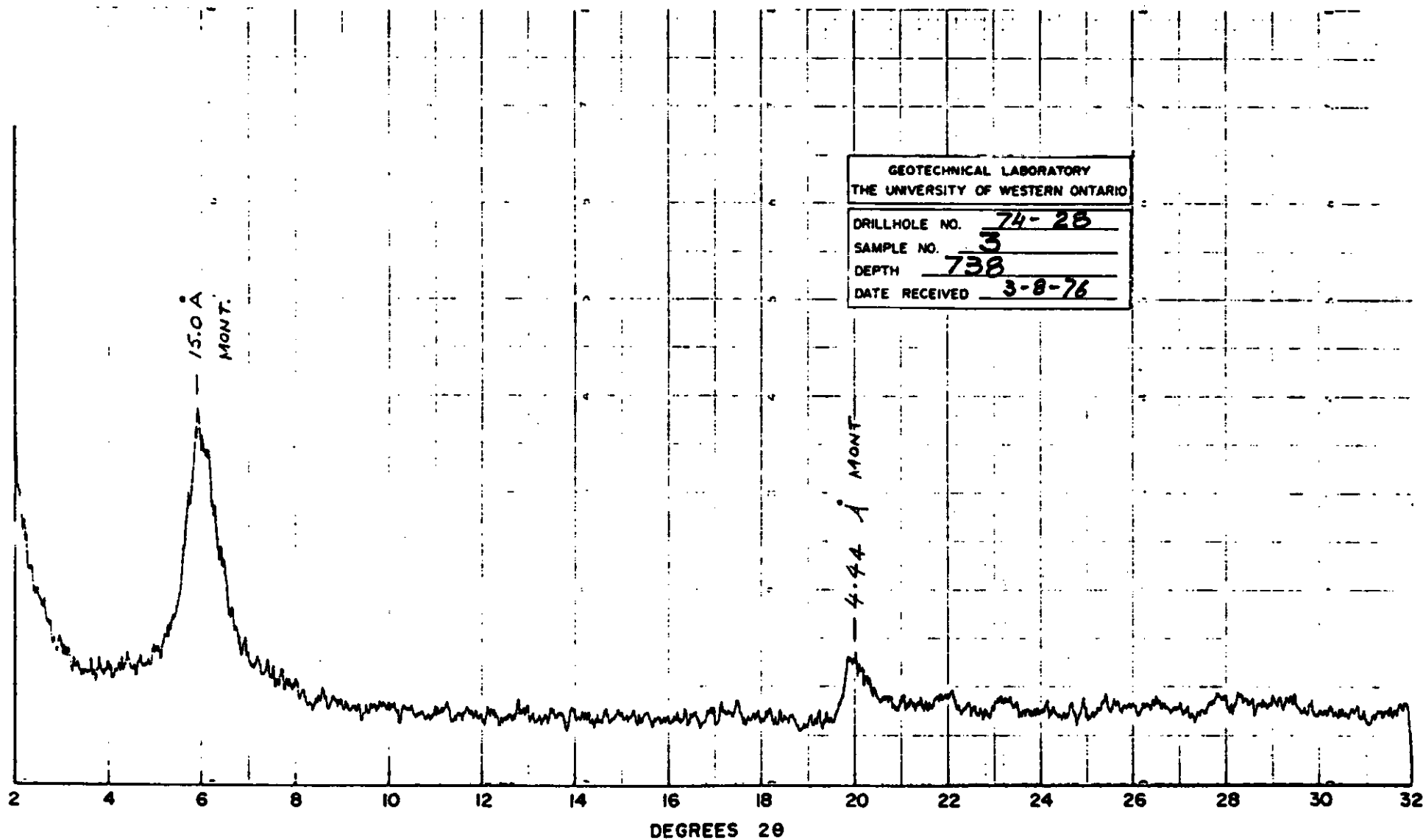
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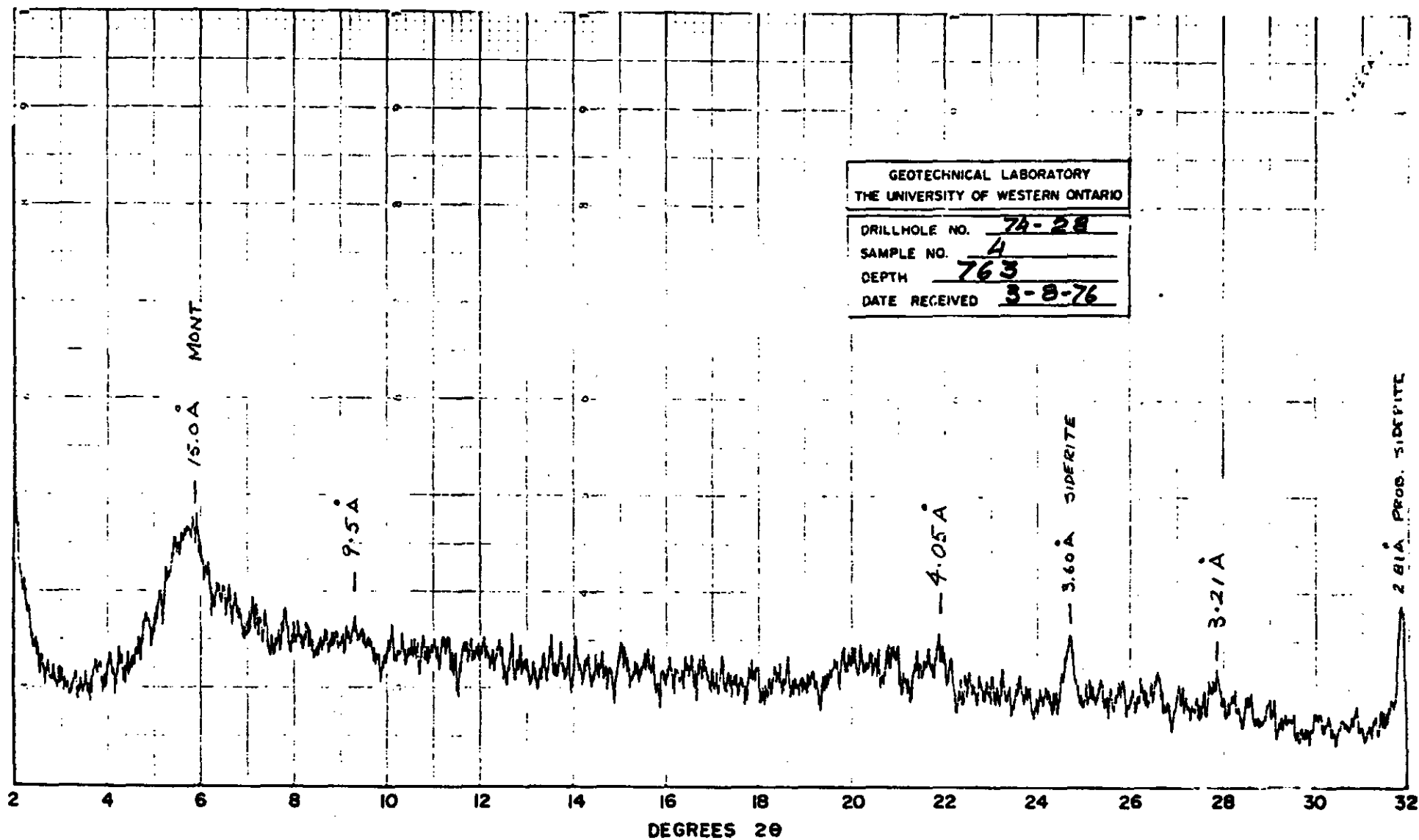
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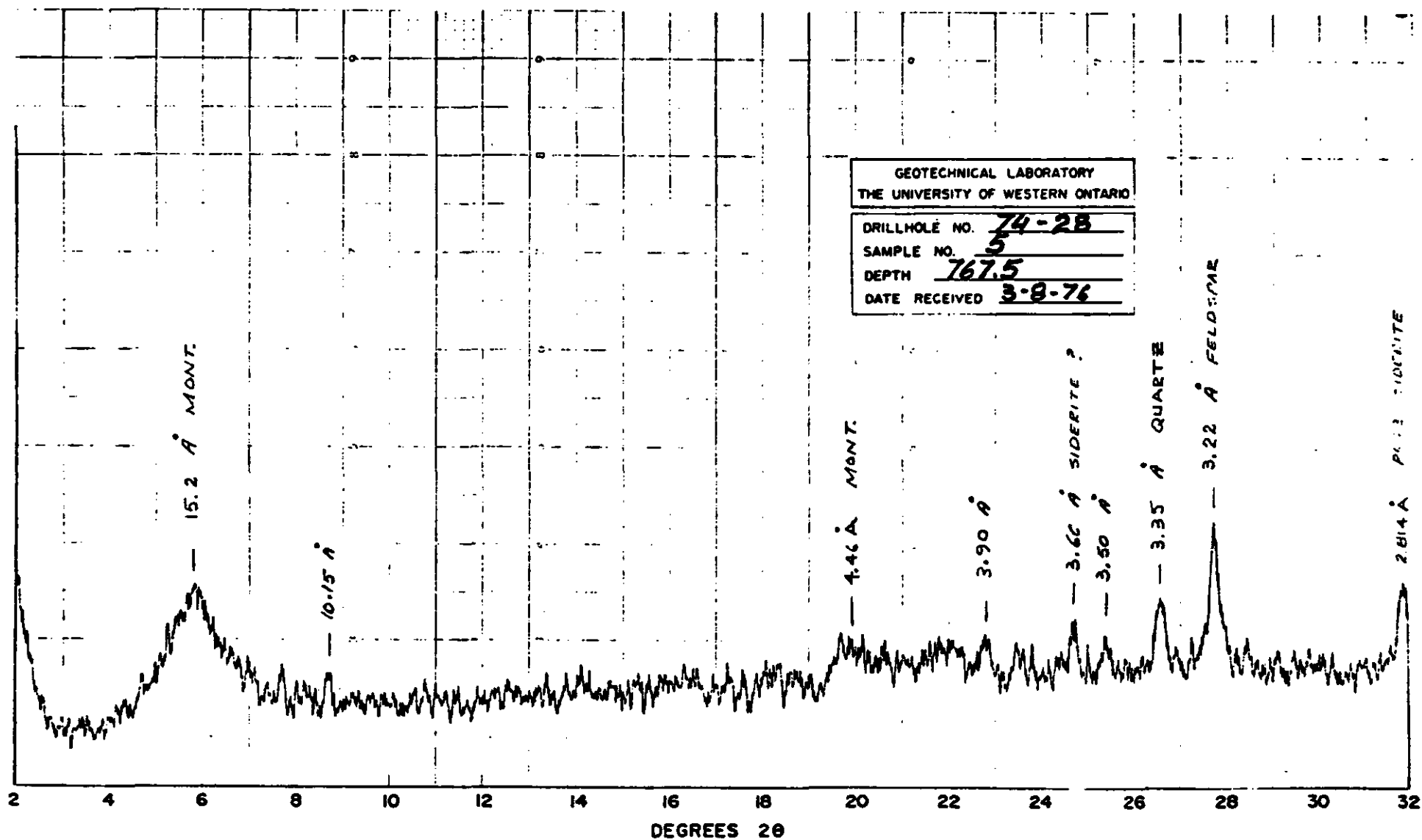
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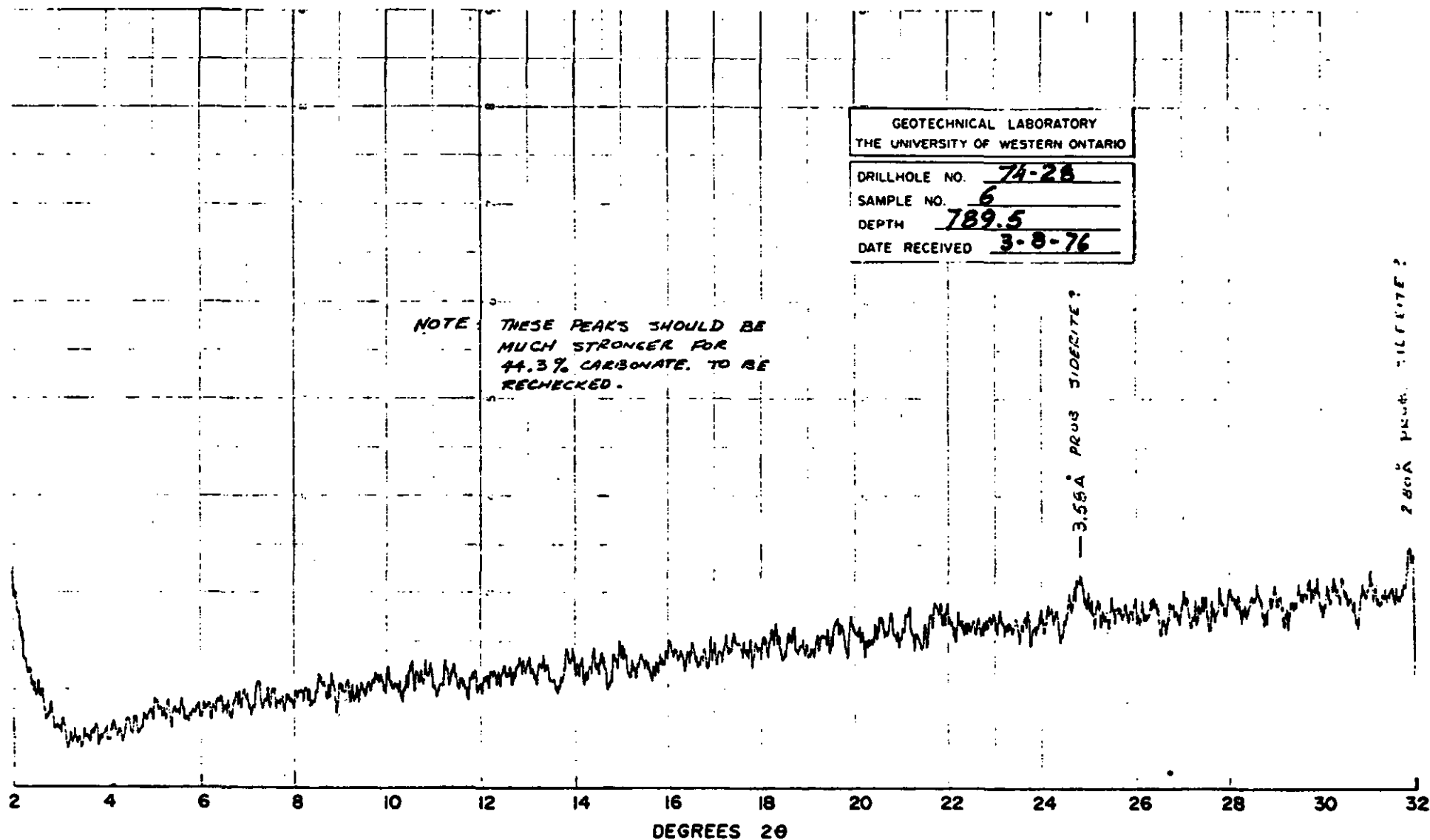
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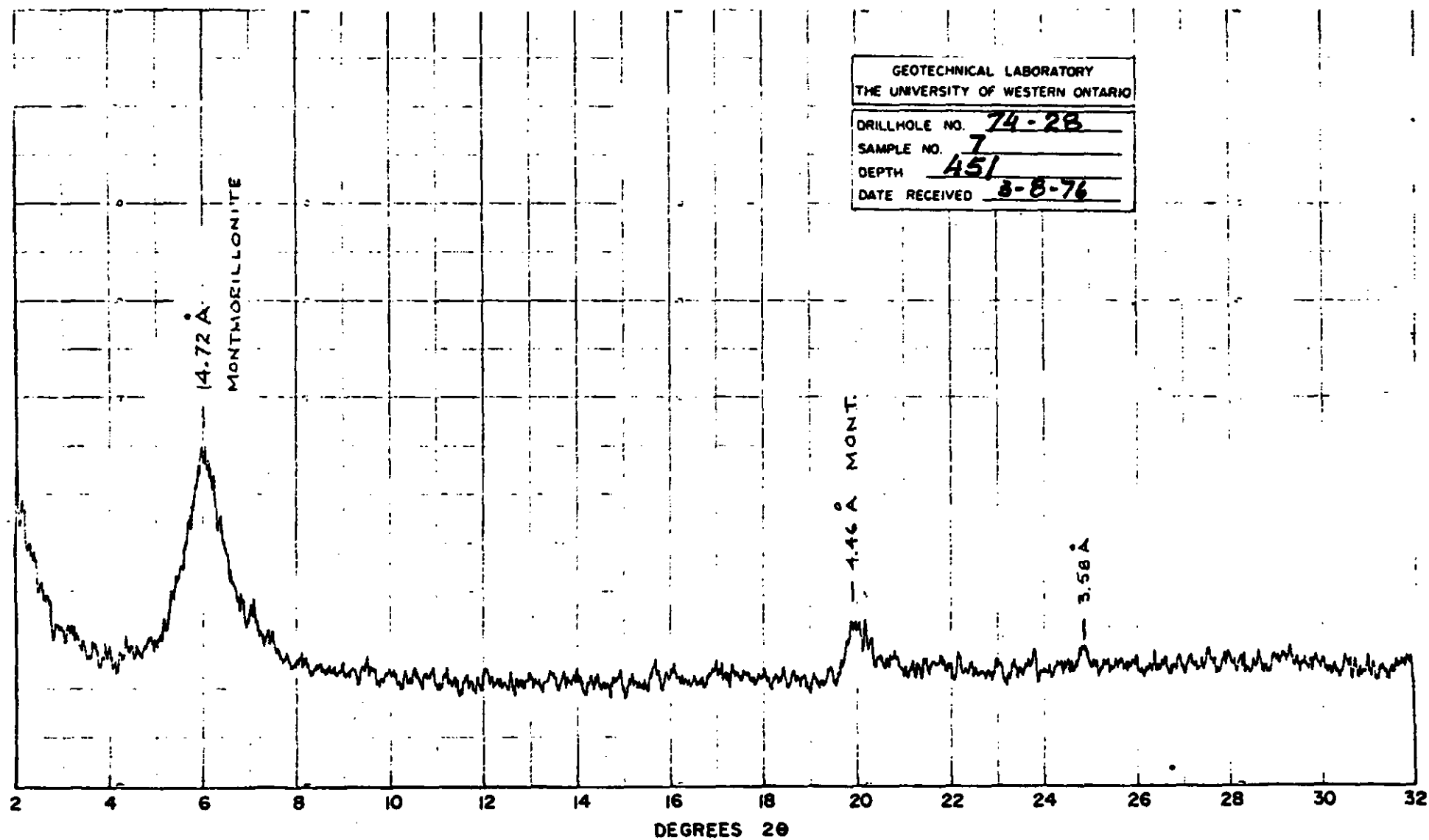
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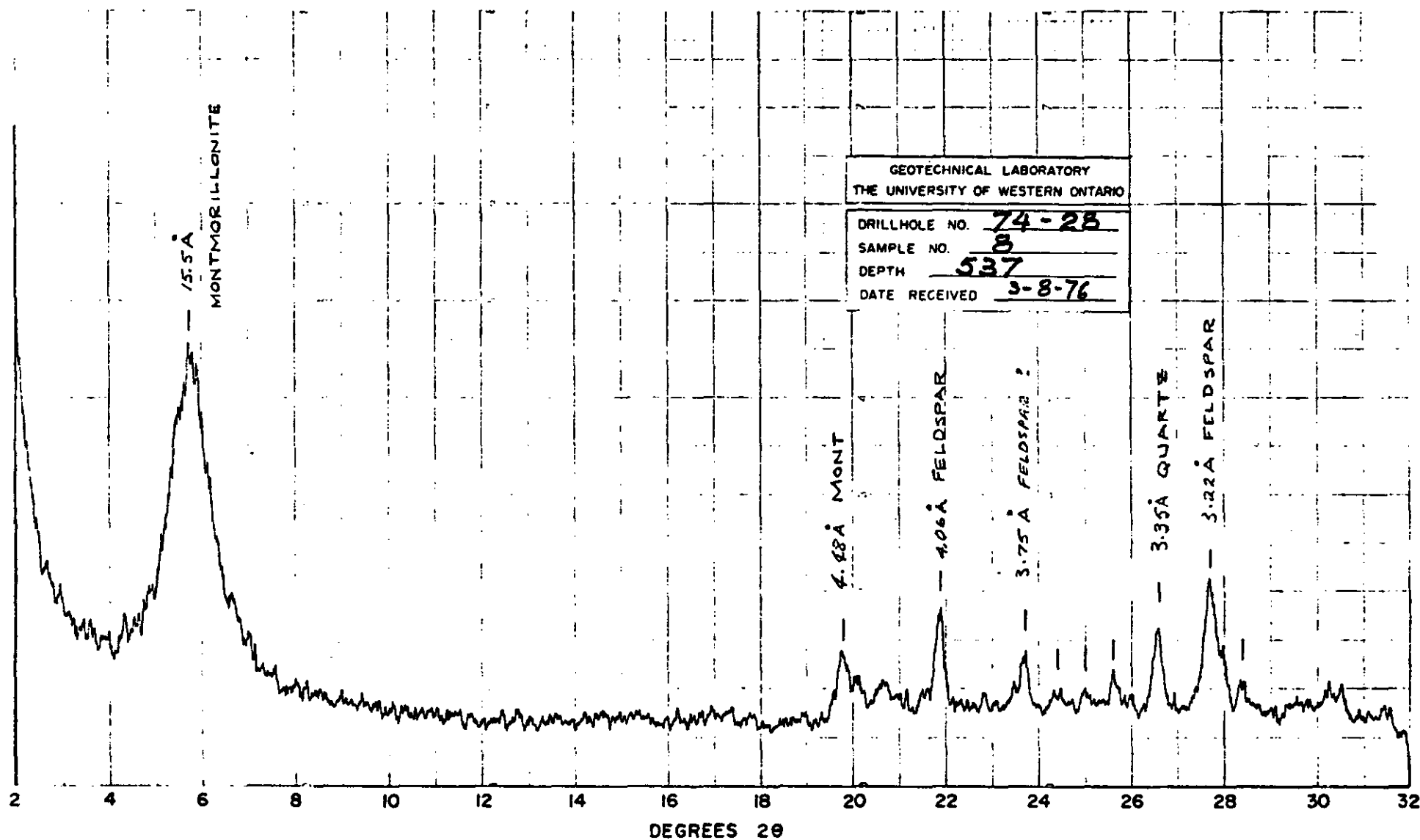
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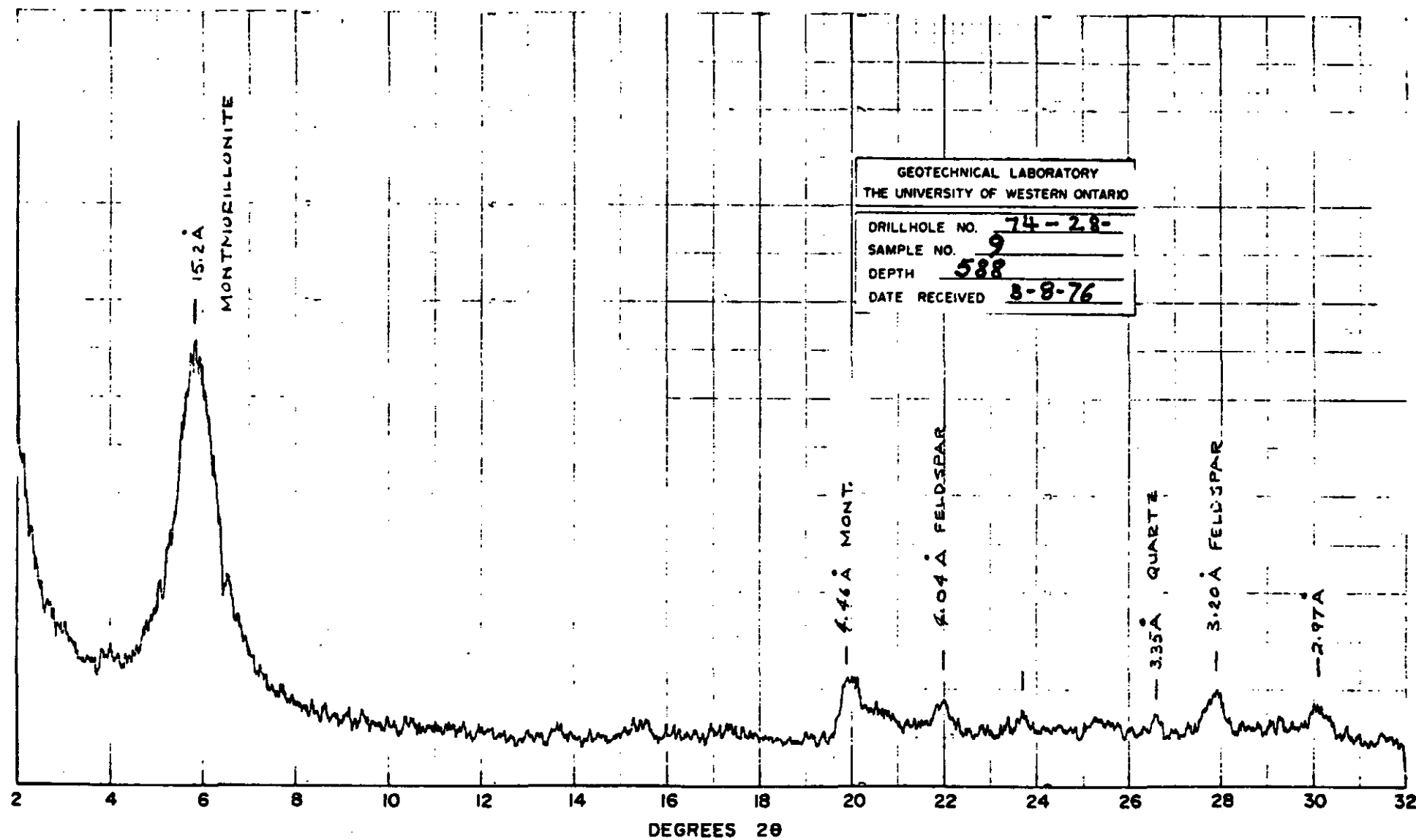
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



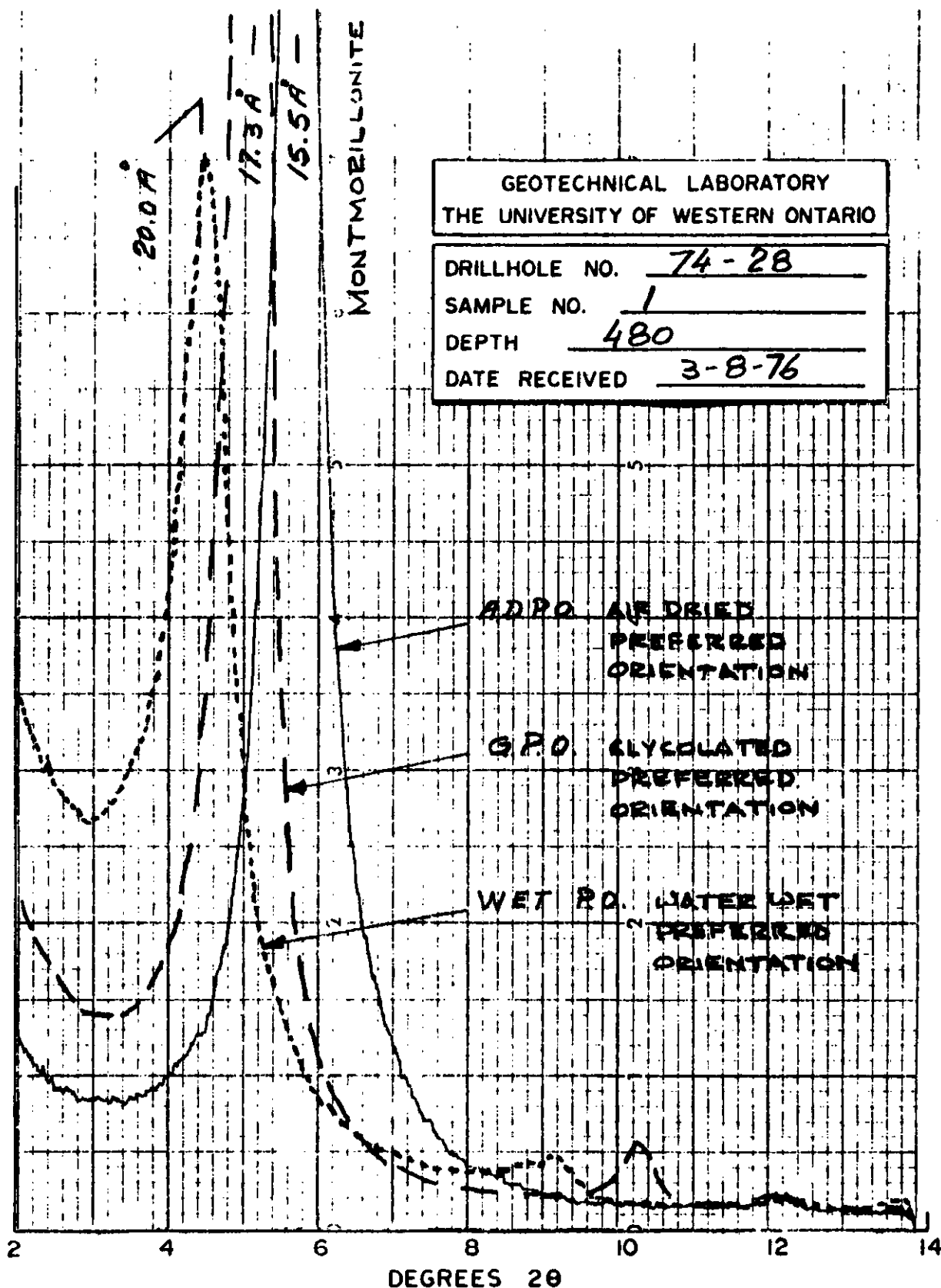
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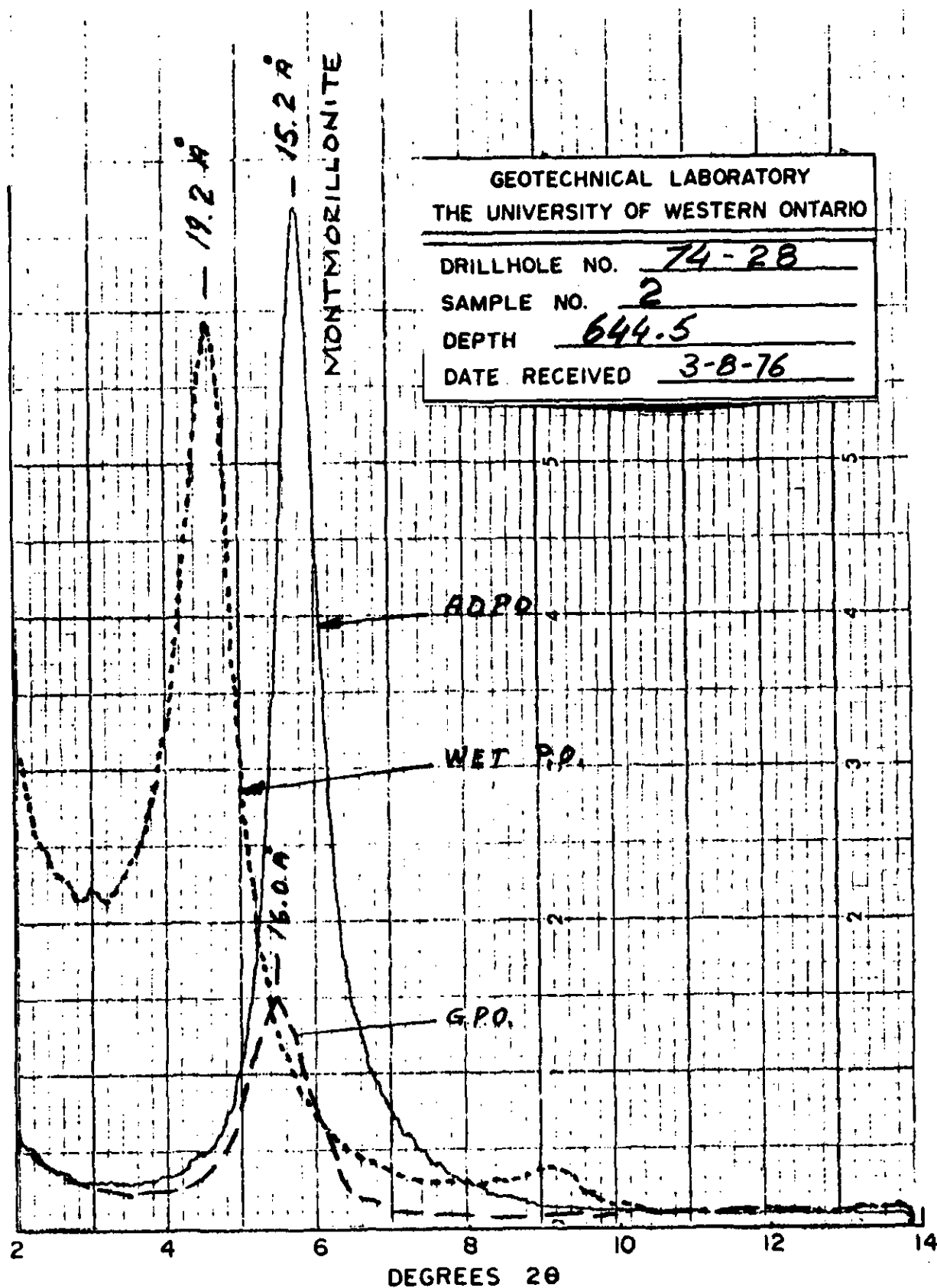
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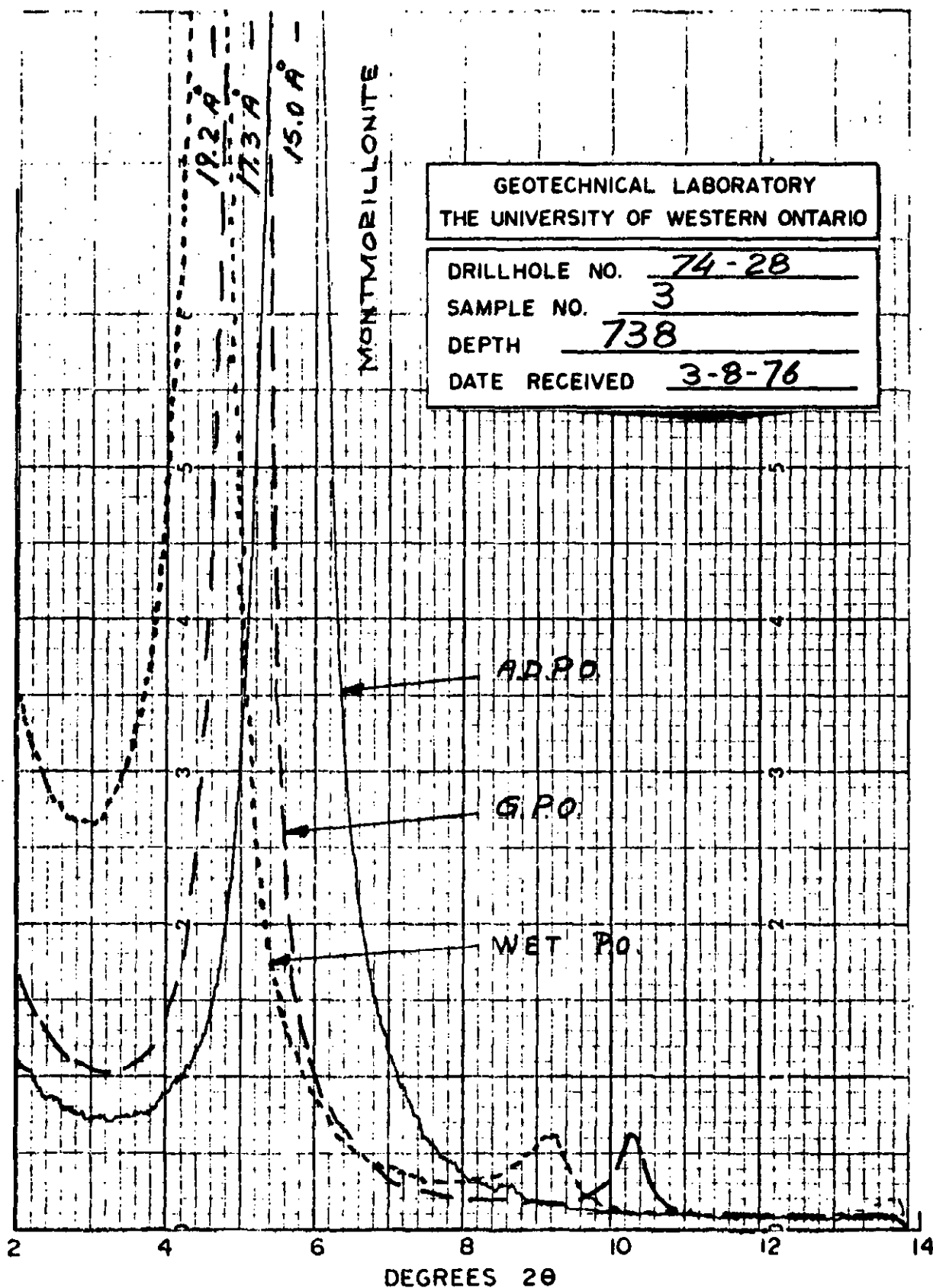
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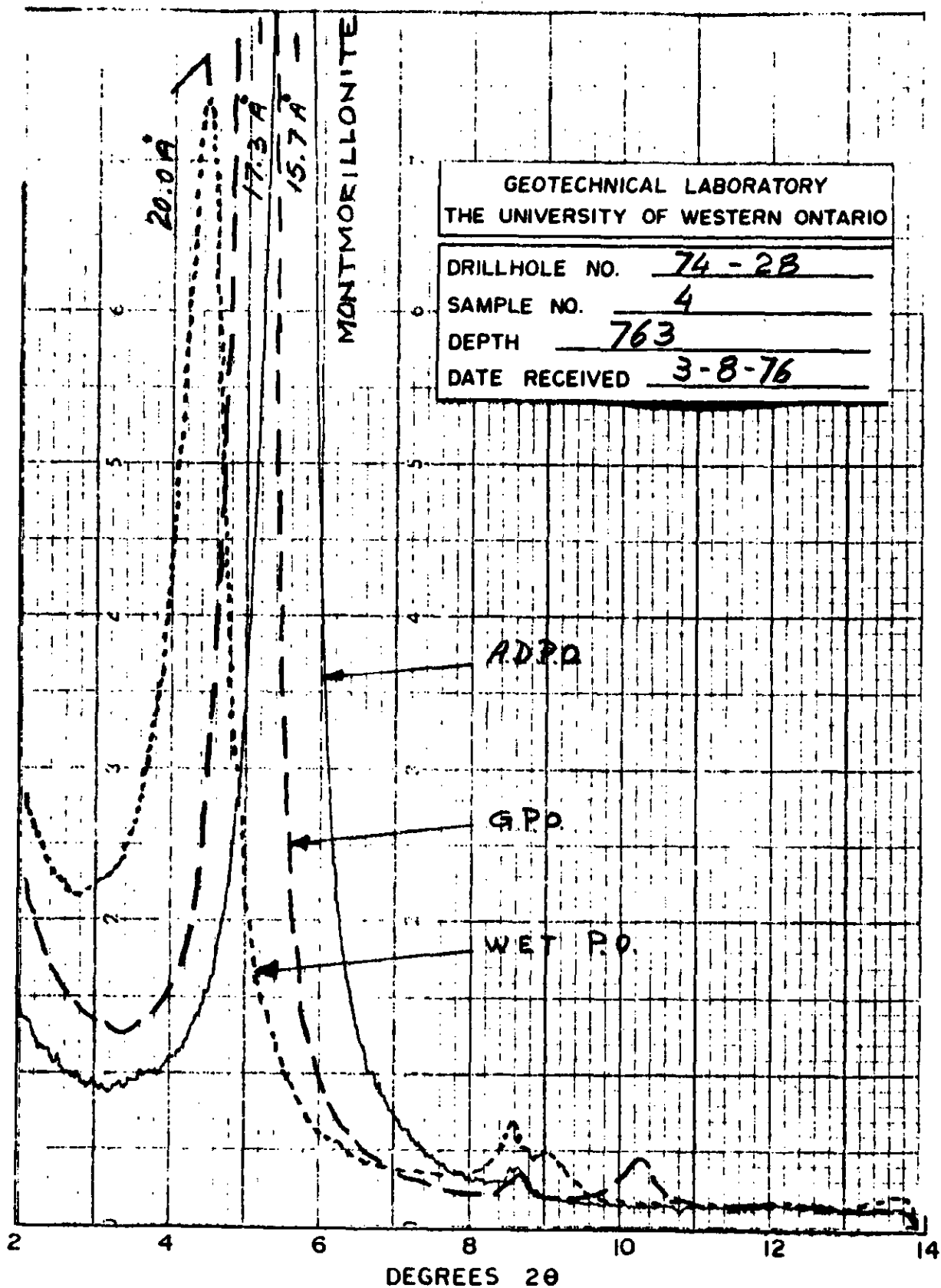
X-RAY DIFFRACTION TRACES OF 2μ , PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



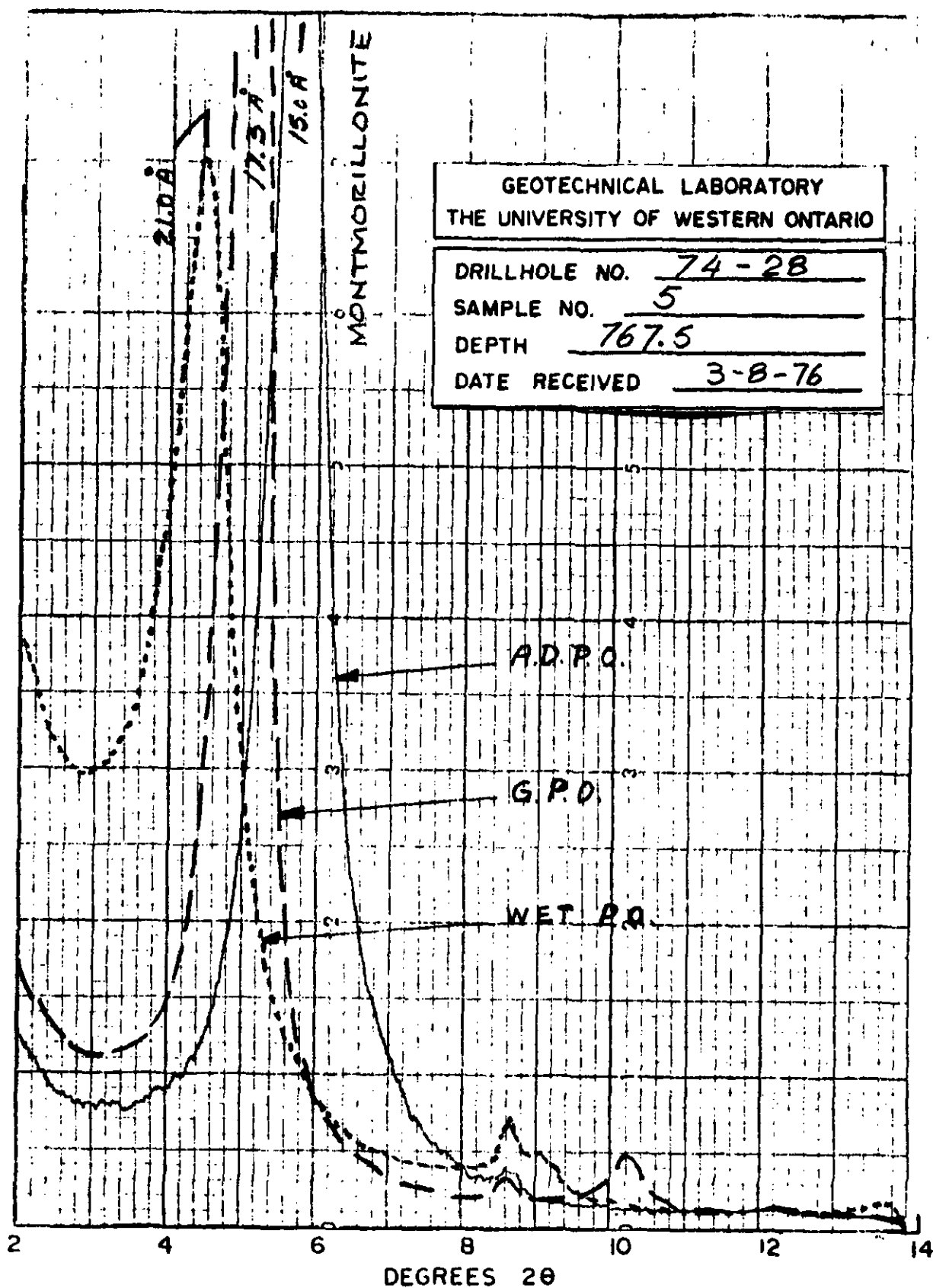
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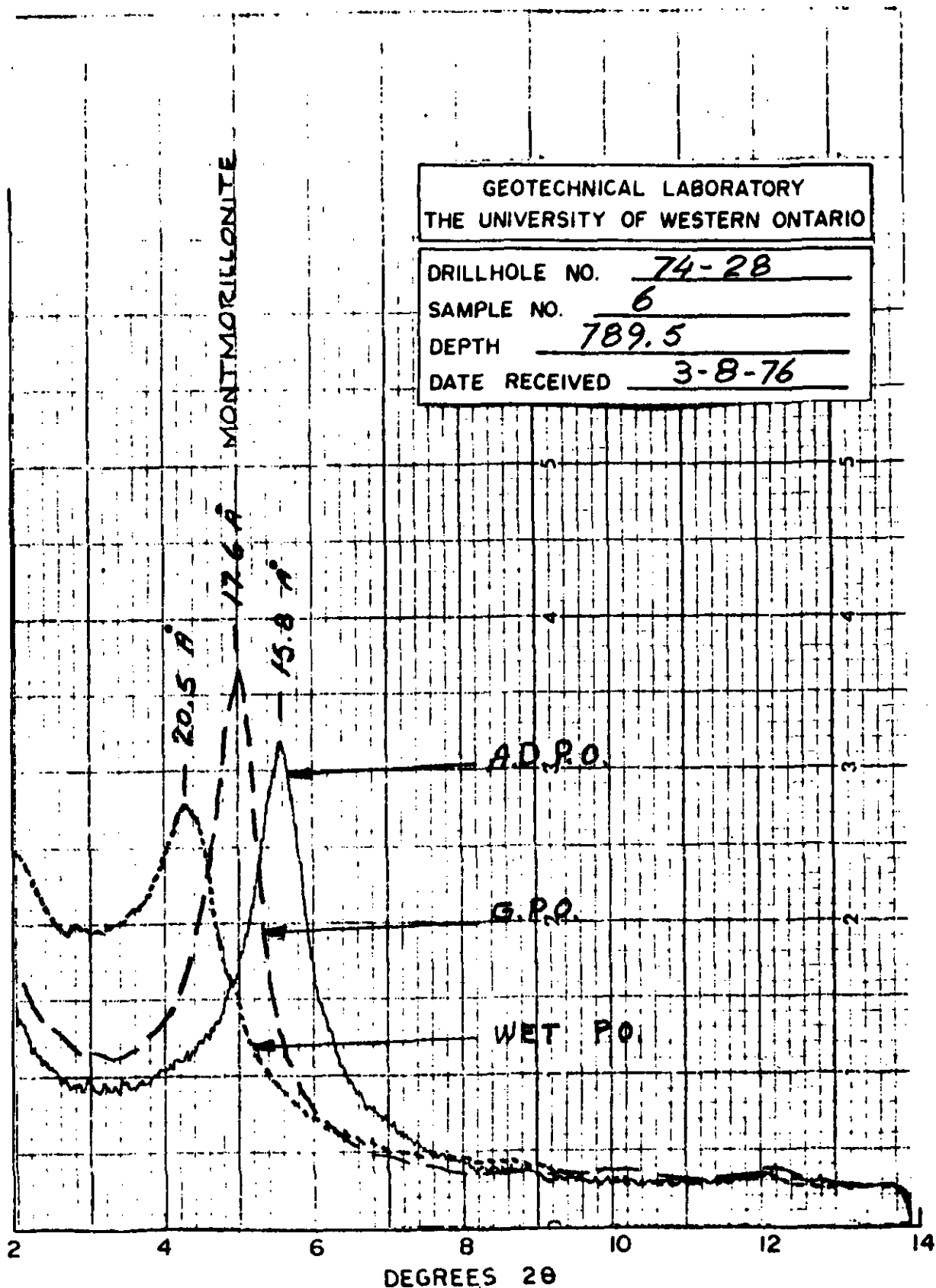
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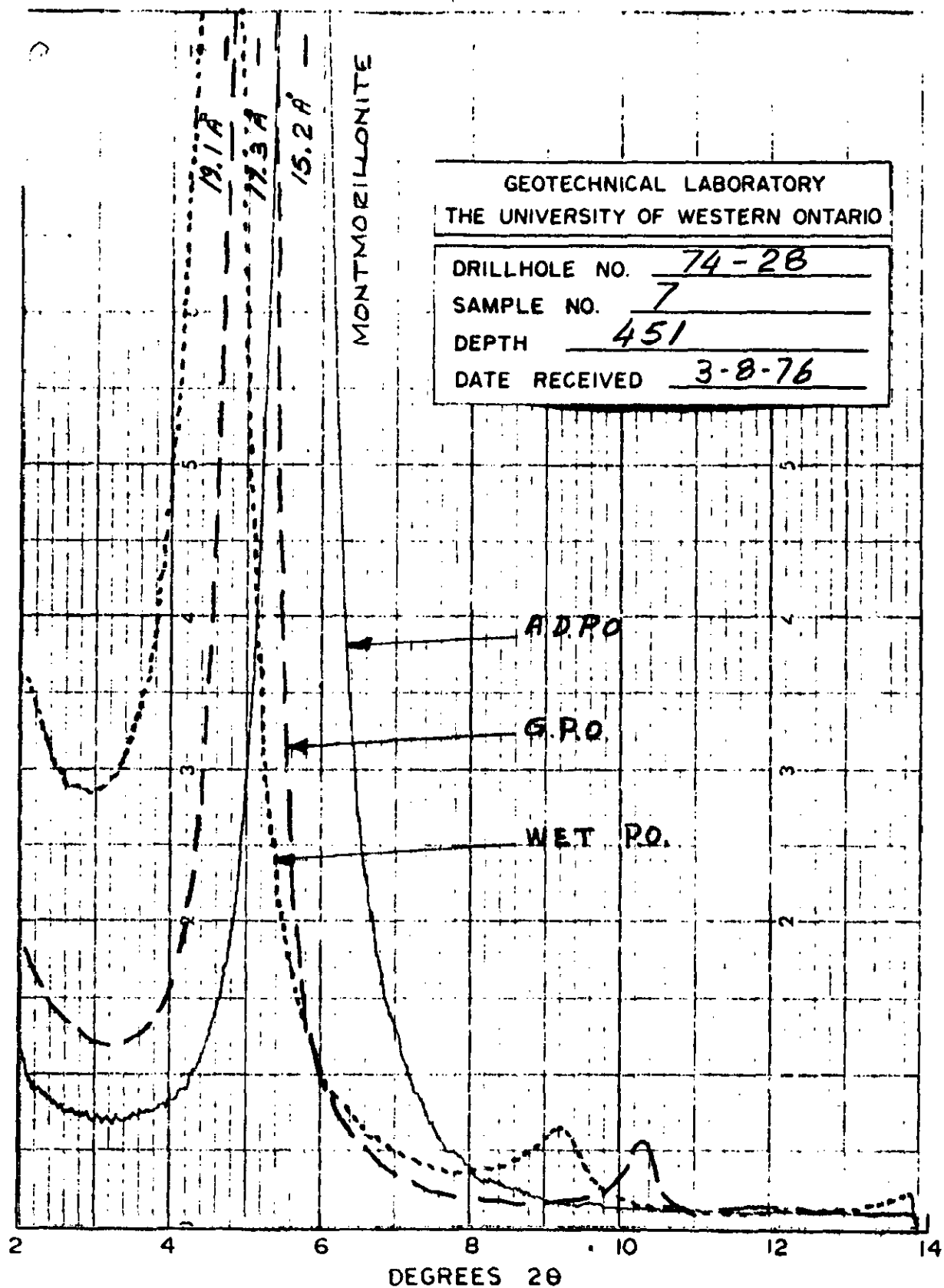
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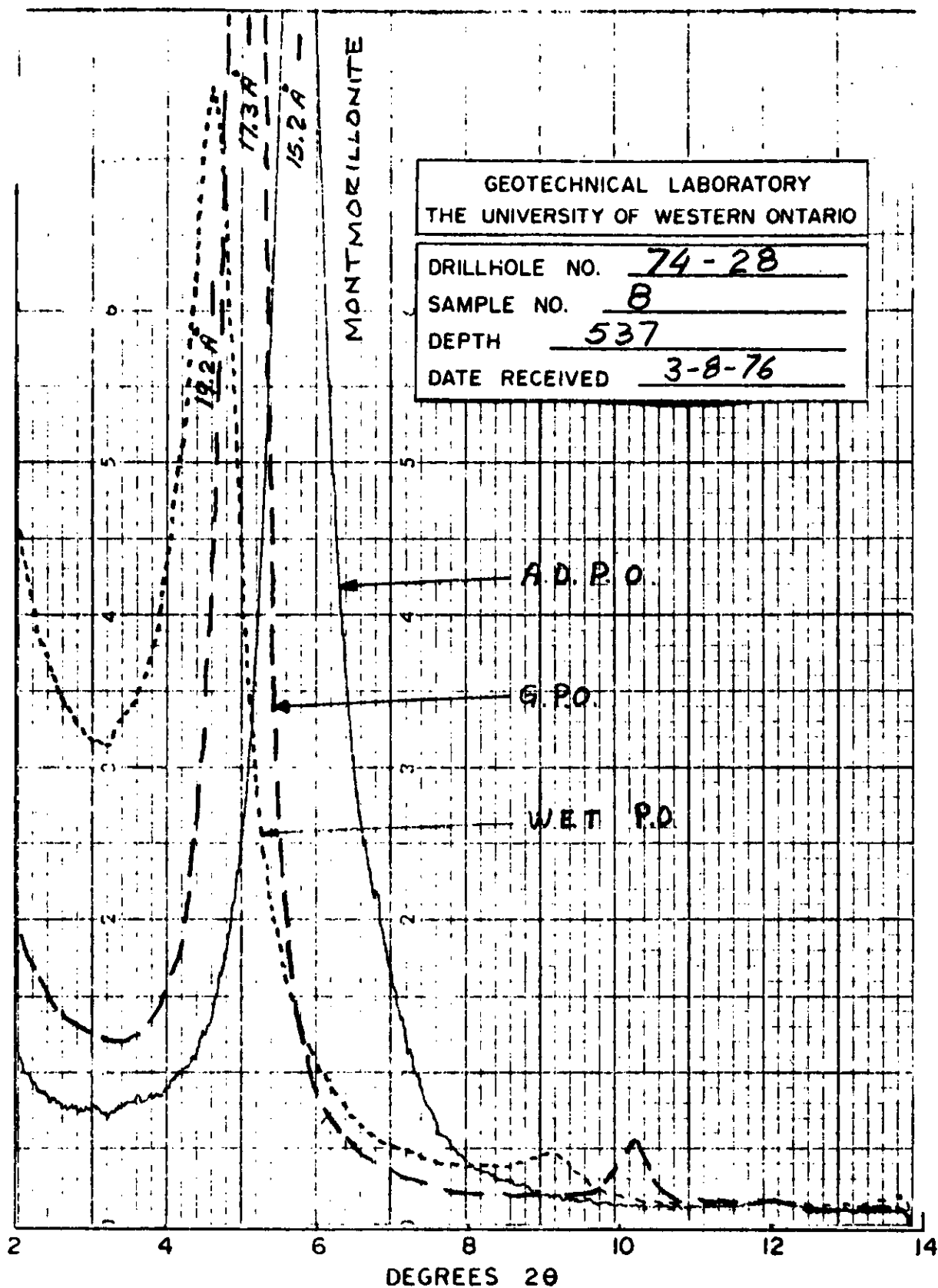
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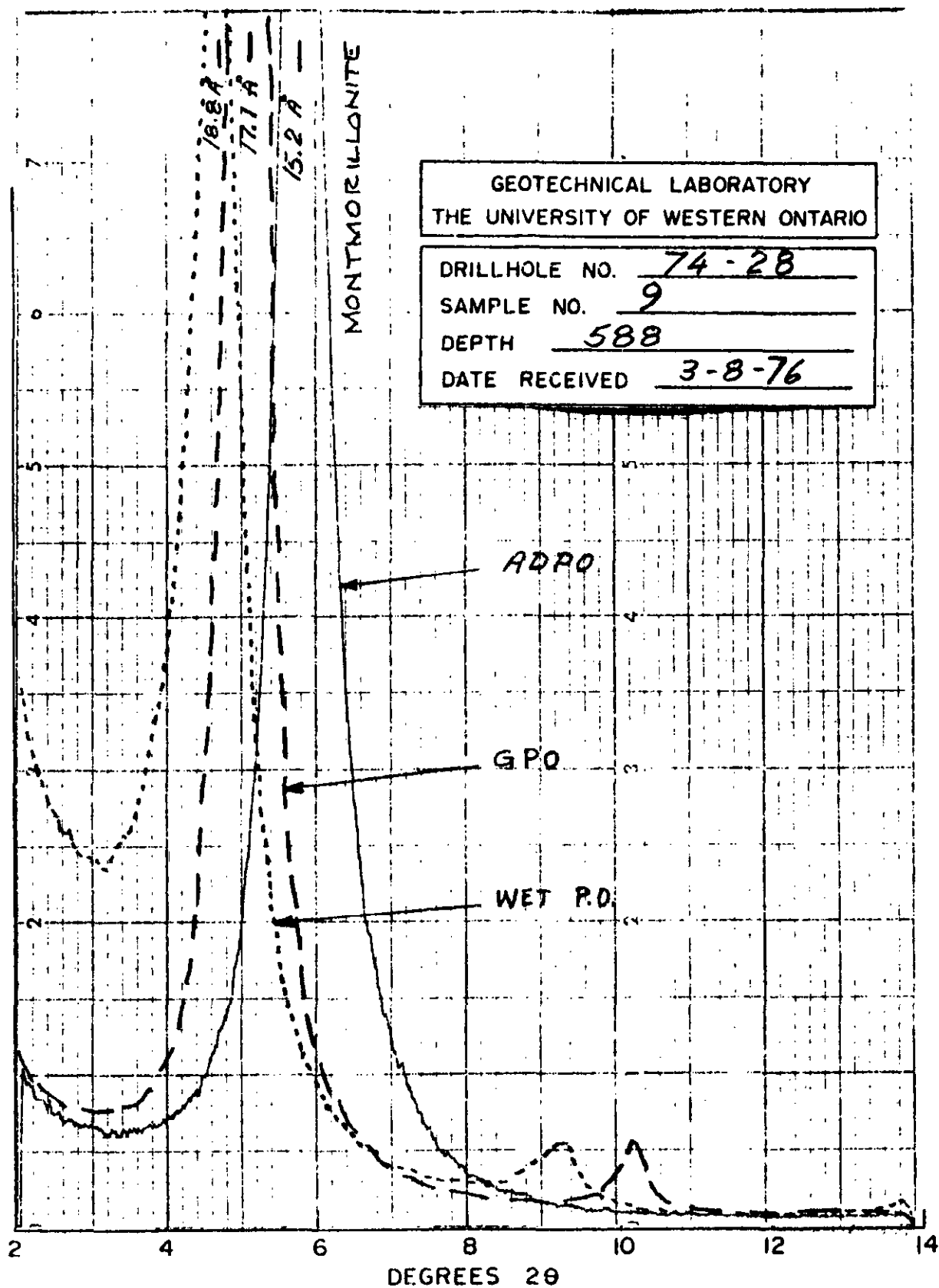
X-RAY DIFFRACTION TRACES OF 2μ , PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



X-RAY DIFFRACTION TRACES OF 2μ , PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



X-RAY DIFFRACTION TRACES OF 2μ , PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



X-RAY DIFFRACTION TRACES OF 2μ , PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



1 FEB 15 1977
FILE NO.

The University of Western Ontario

Faculty of Engineering Science
London, Canada
N6A 5B9

August 17, 1976

Mr. G. Rawlings
Golder, Brawner & Associates Ltd.
224 West 8th Avenue
Vancouver, B.C.
V5Y 1N5

Dear Mr. Rawlings:

Report #2 - Supplement
Hat Creek Project - Mineralogical Analyses
August 17, 1976

This supplement to Report #2 contains reruns of all powder x-rays on samples for B.H. #74-28. The traces were obtained on rocks more finely ground (<200 mesh) in an attempt to strengthen the x-ray peaks.

The traces are essentially as in the original report with strengthening of some of the peaks, especially those for siderite.

The most remarkable aspect of the powder patterns is the great size of the montmorillonite 15Å peak in all traces except B.H. #78-28 sample #6 where it is virtually absent. Montmorillonite is still present as shown in the preferred orientation traces for this sample in our Report #2.

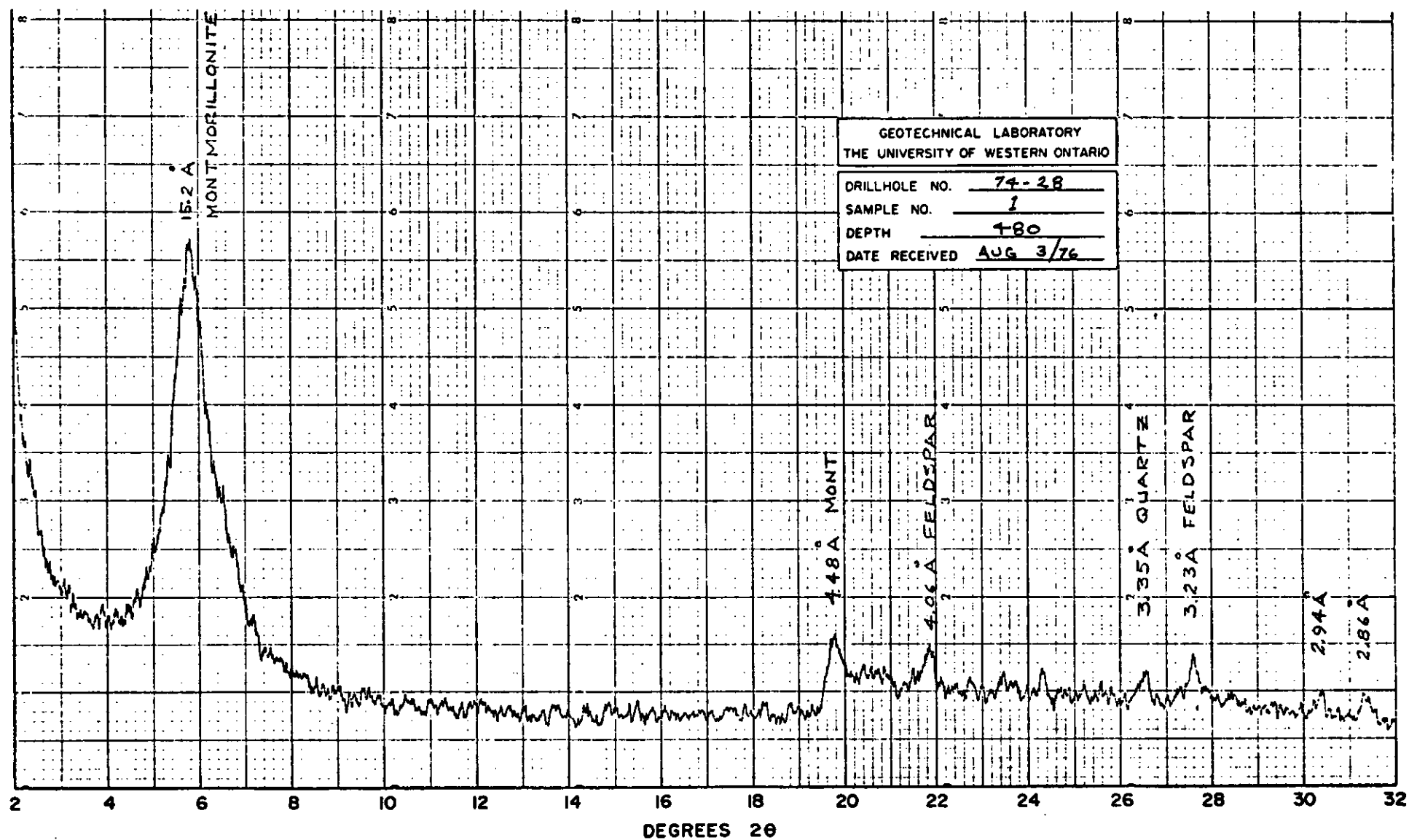
There is little evidence of cristobalite and other ash derived minerals in the rocks analyzed to date except possibly sample 74-28-2 in which a 4.06Å peak without other feldspar peaks could possibly be cristobalite.

Yours sincerely,

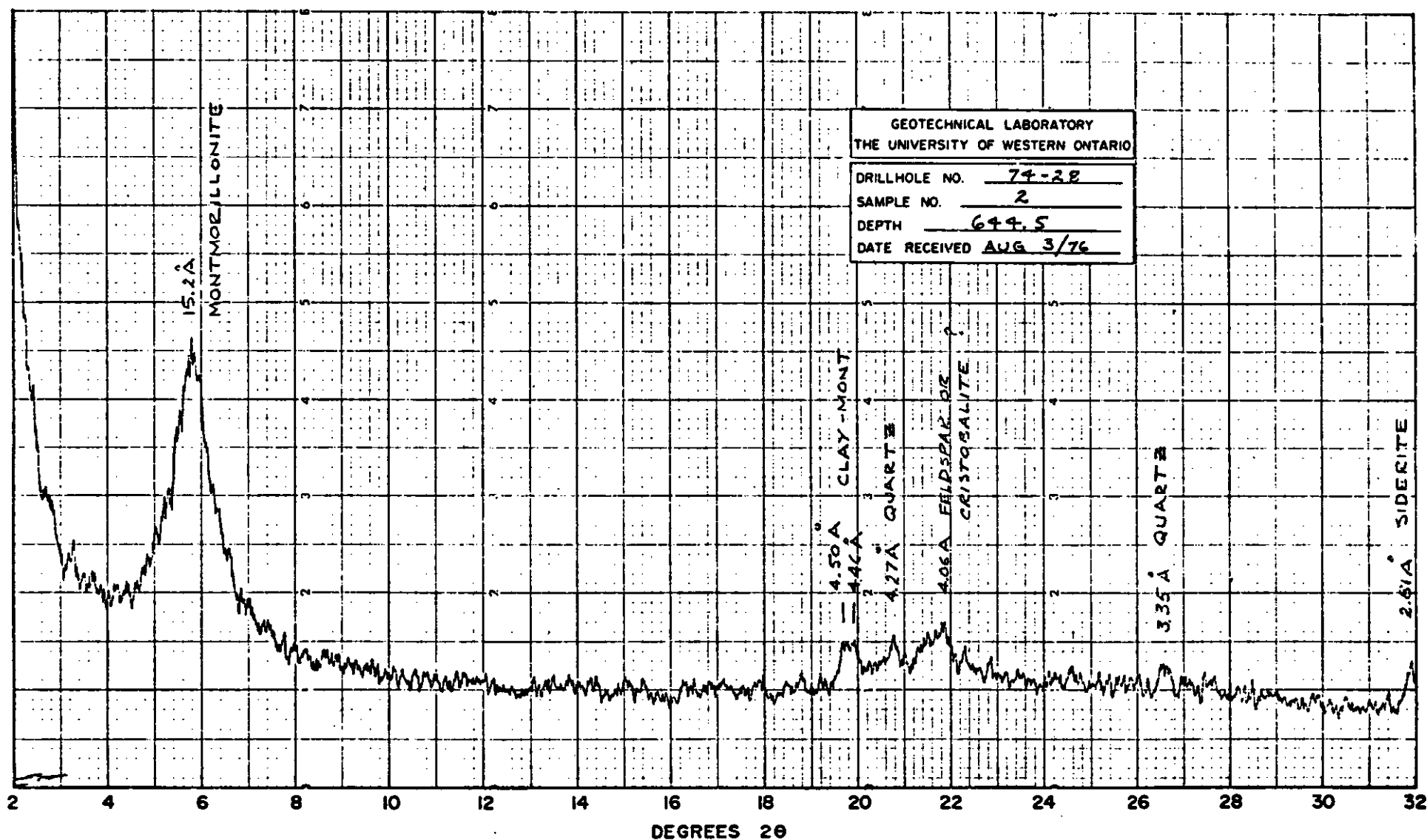
R.M. Quigley, P.Eng.
Professor of Geotechnical
Engineering

RMQ/jl
Attach.

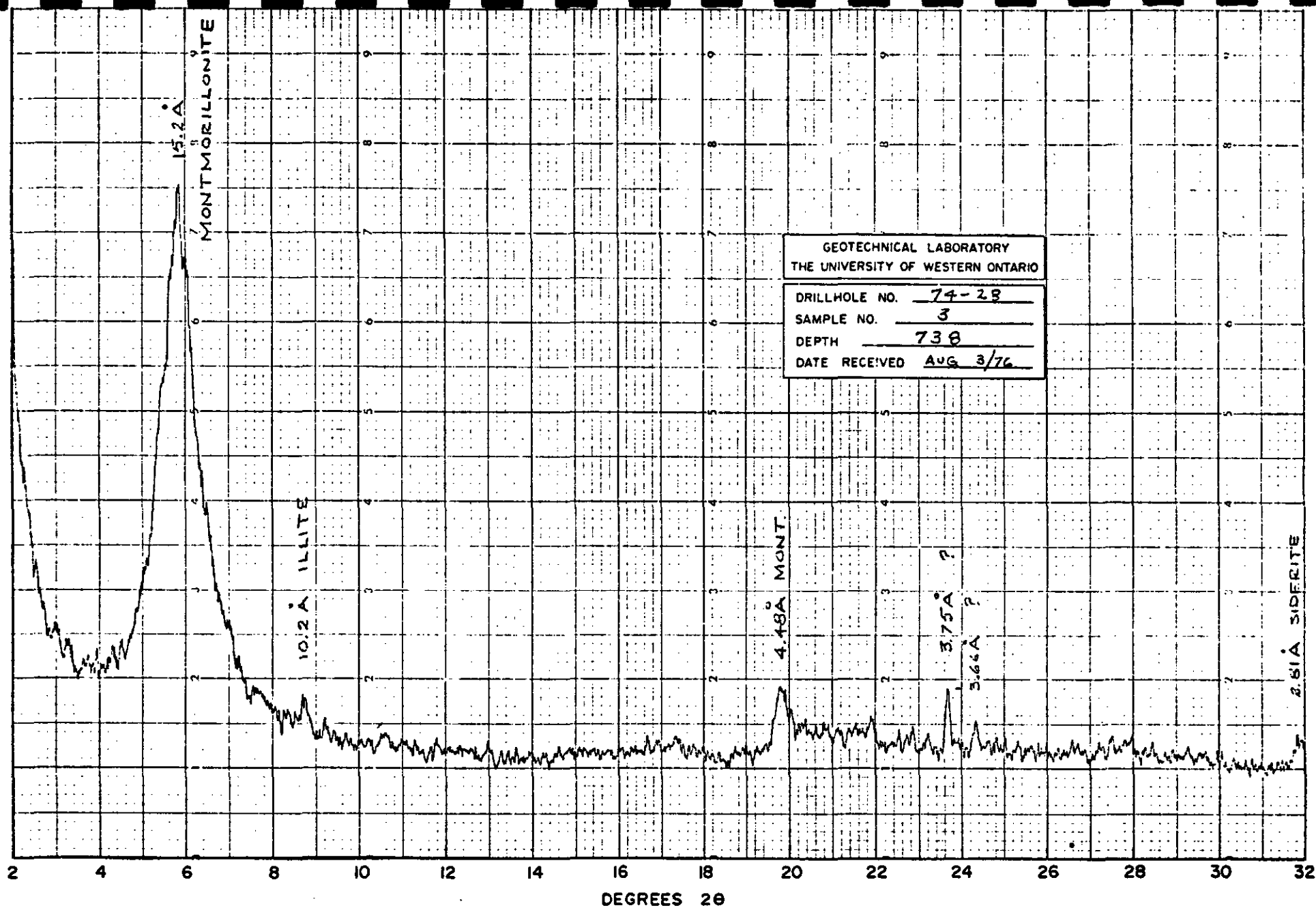
cc. Mr. H. Hawson ✓



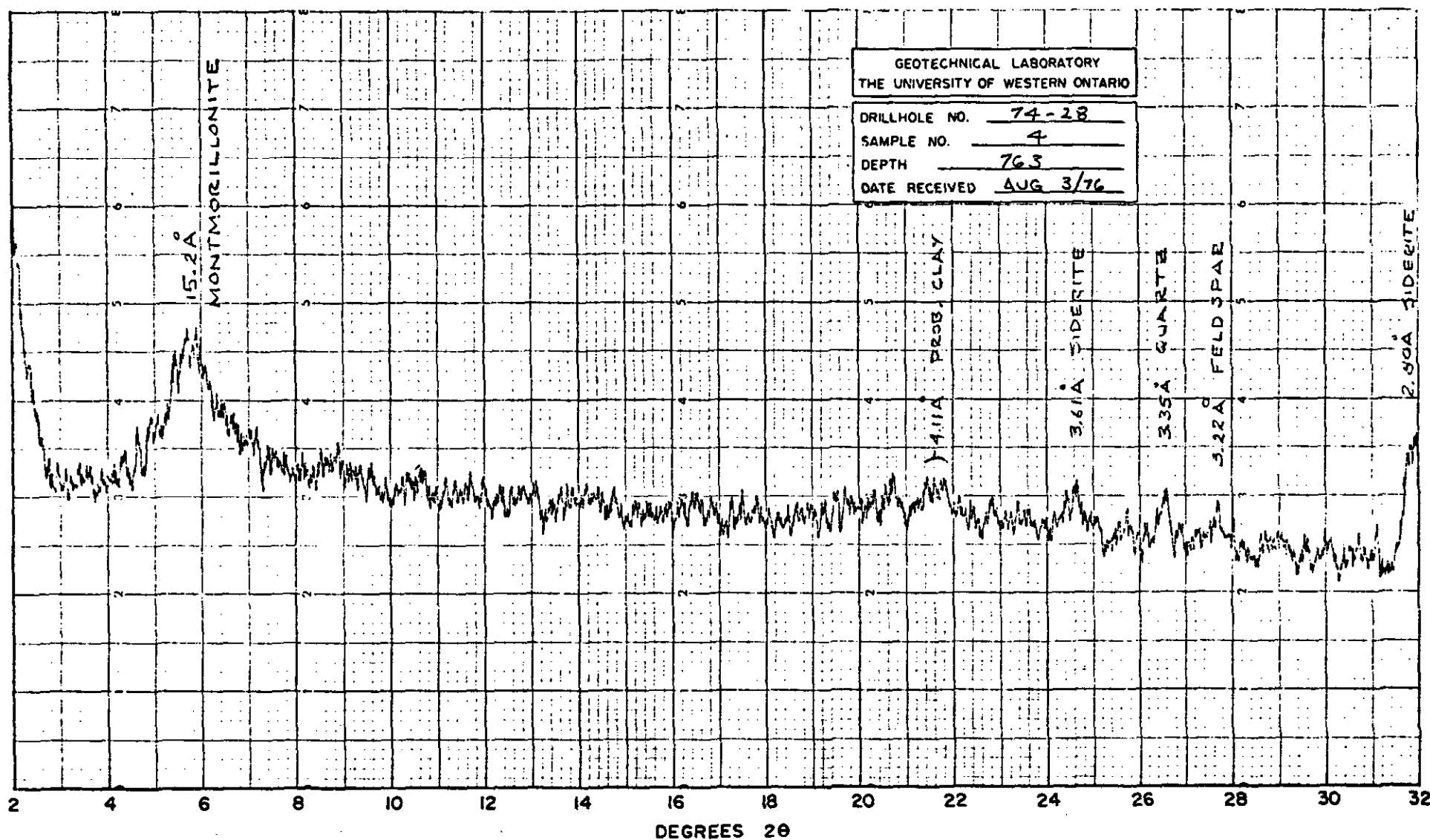
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



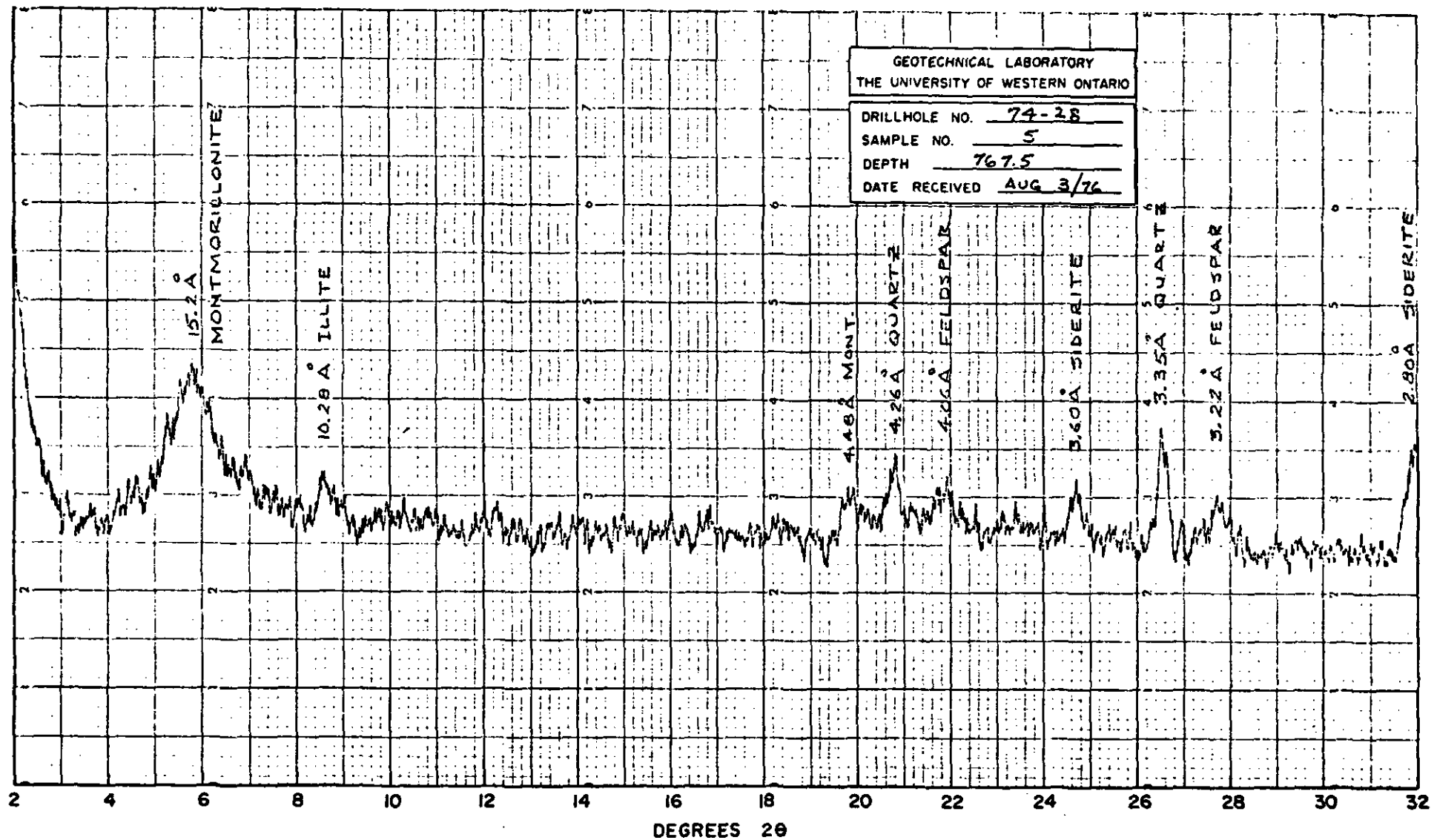
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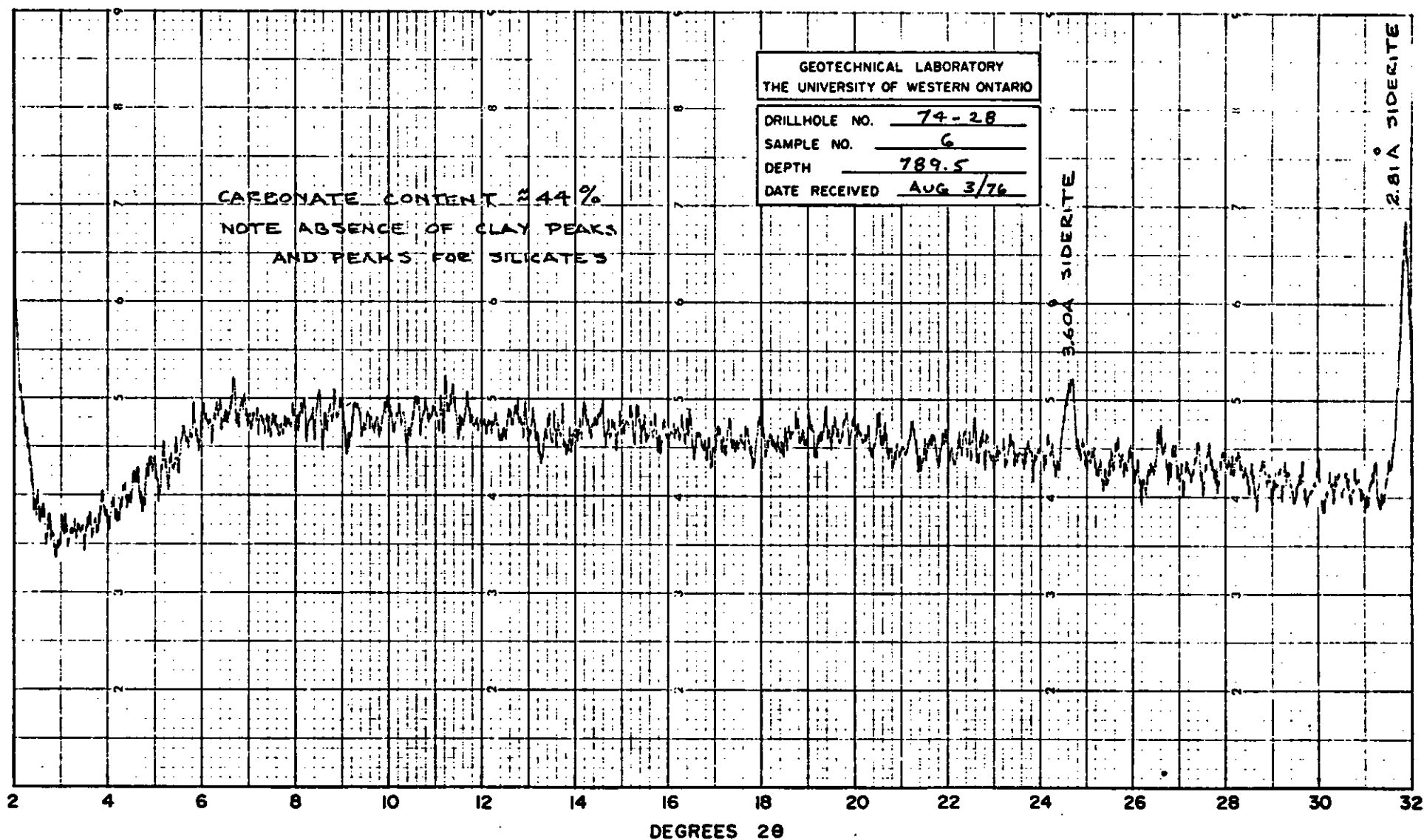
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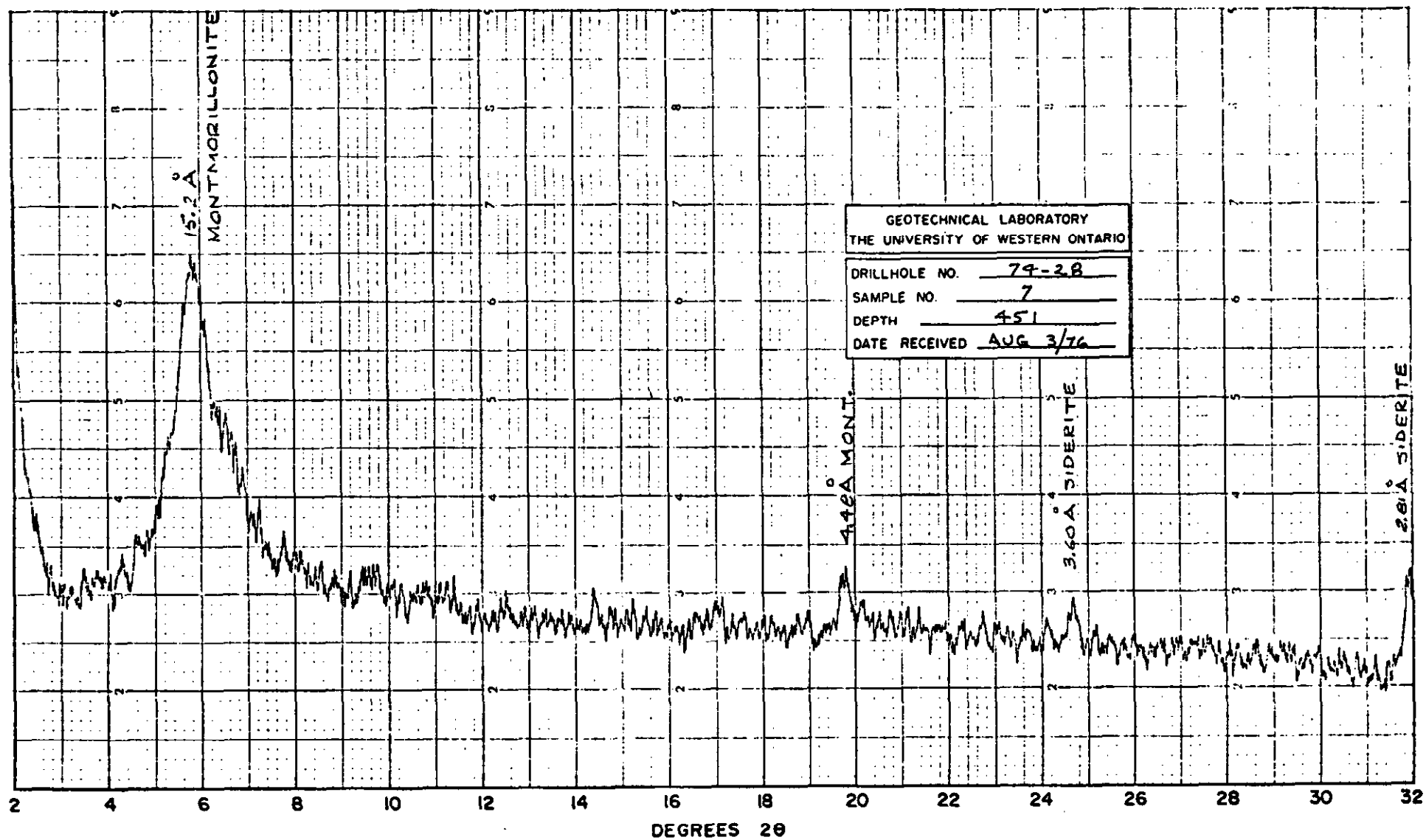
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



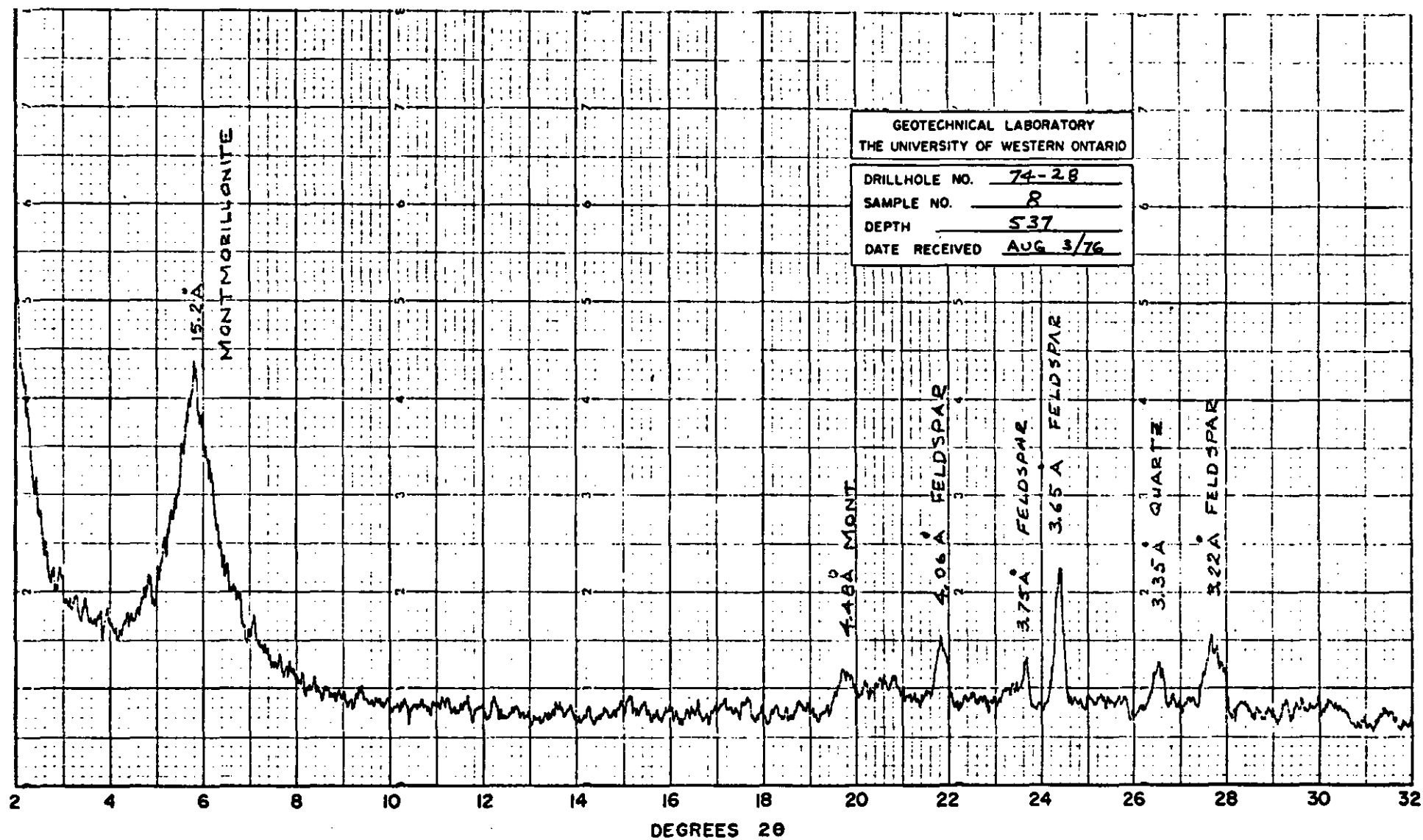
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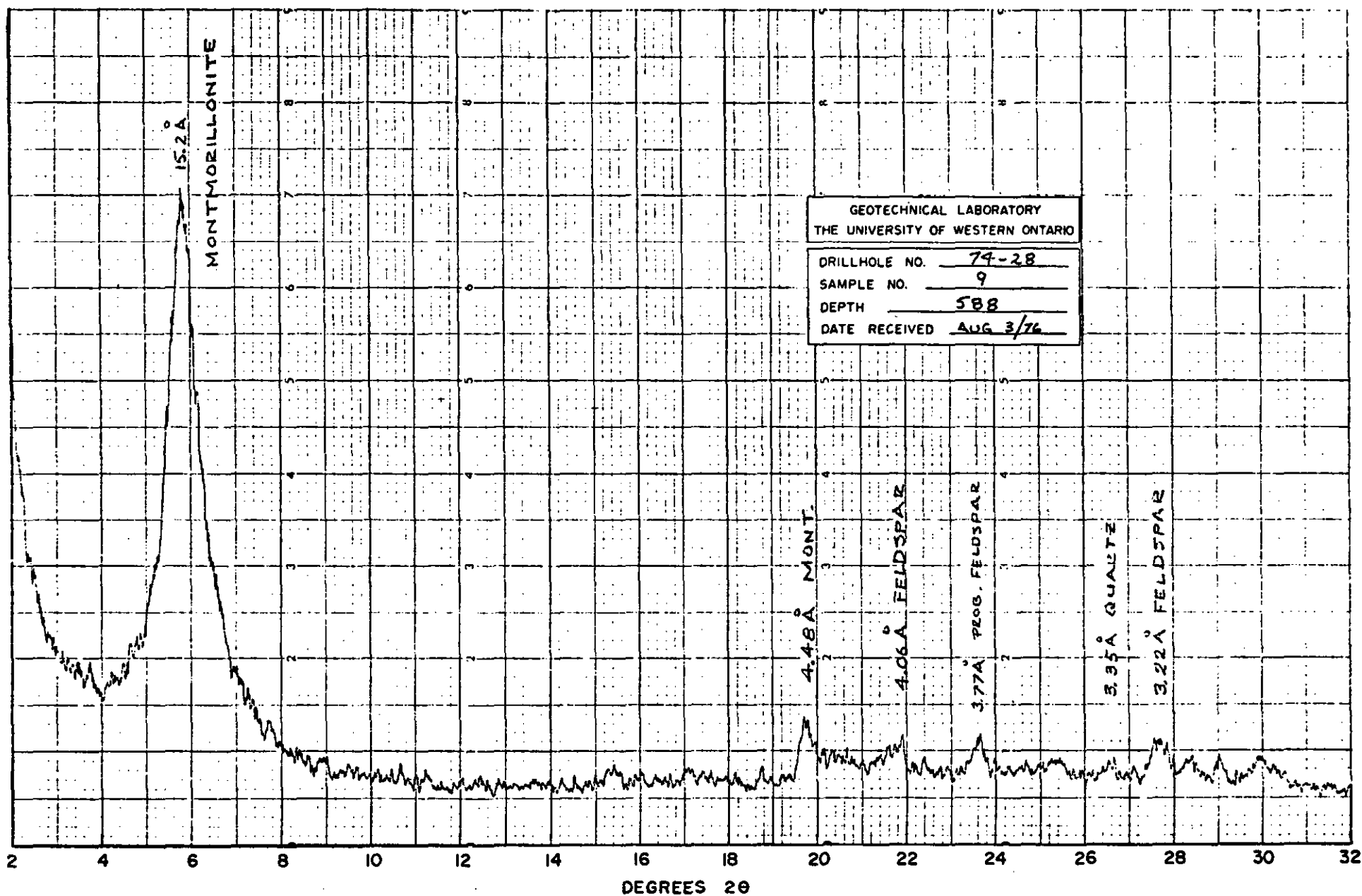
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.

15 1977

FILE No.



The University of Western Ontario, London, Canada

Faculty of Engineering Science
London, Canada
N6A 5B9

20 August 1976

Mr. G. Rawlings
Golder, Brawner & Associates Ltd.
224 West 8th Avenue
Vancouver, British Columbia
V5Y 1N5

Dear Mr. Rawlings:

Report #3 - Hat Creek Project - Mineralogical Analyses
August 20, 1976

We have completed x-ray and carbonate analyses on eight samples from borehole 76-815 received from Mr. H. Hawson on August 3, 1976. We have yet to complete the x-ray and carbonate analyses on eight further samples, however, these will be forwarded to you in early September.

During September we will also run the selected Na⁺ analyses and glycol retention values on the samples received to date.

Comments on Borehole 76-815

1. Carbonate analyses supplemented by the x-ray powder patterns showed the heavily indurated rocks to consist of 34 to 68% siderite. All rocks supplied from this hole reacted with HCl (when powdered) indicating some carbonate.
2. Where siderite was very abundant (Sa. #7, 9, 18, 22 and 29) the montmorillonite peaks were very weak or absent on the powder patterns. An absence of other peaks indicates a scarcity of silicate minerals noticed in previous rock samples.
3. Montmorillonite was confirmed to be present in the < 2 μ m fraction of all rocks as shown by the x-ray traces on oriented specimens.
4. It is concluded that the rock specimens supplied from this borehole consist dominantly of montmorillonite and siderite. Quartz and feldspar are rare (< 10%) and clearly observed only on two powder patterns for samples #12 and 20.

Yours sincerely,

R.M. Quigley, P.Eng.
Professor of Geotechnical Engineering

RMQ:em

c.e. H. Hawson ✓

LIST OF SAMPLES RECEIVED FROM GOLDER BRAWNER & ASSOCIATES

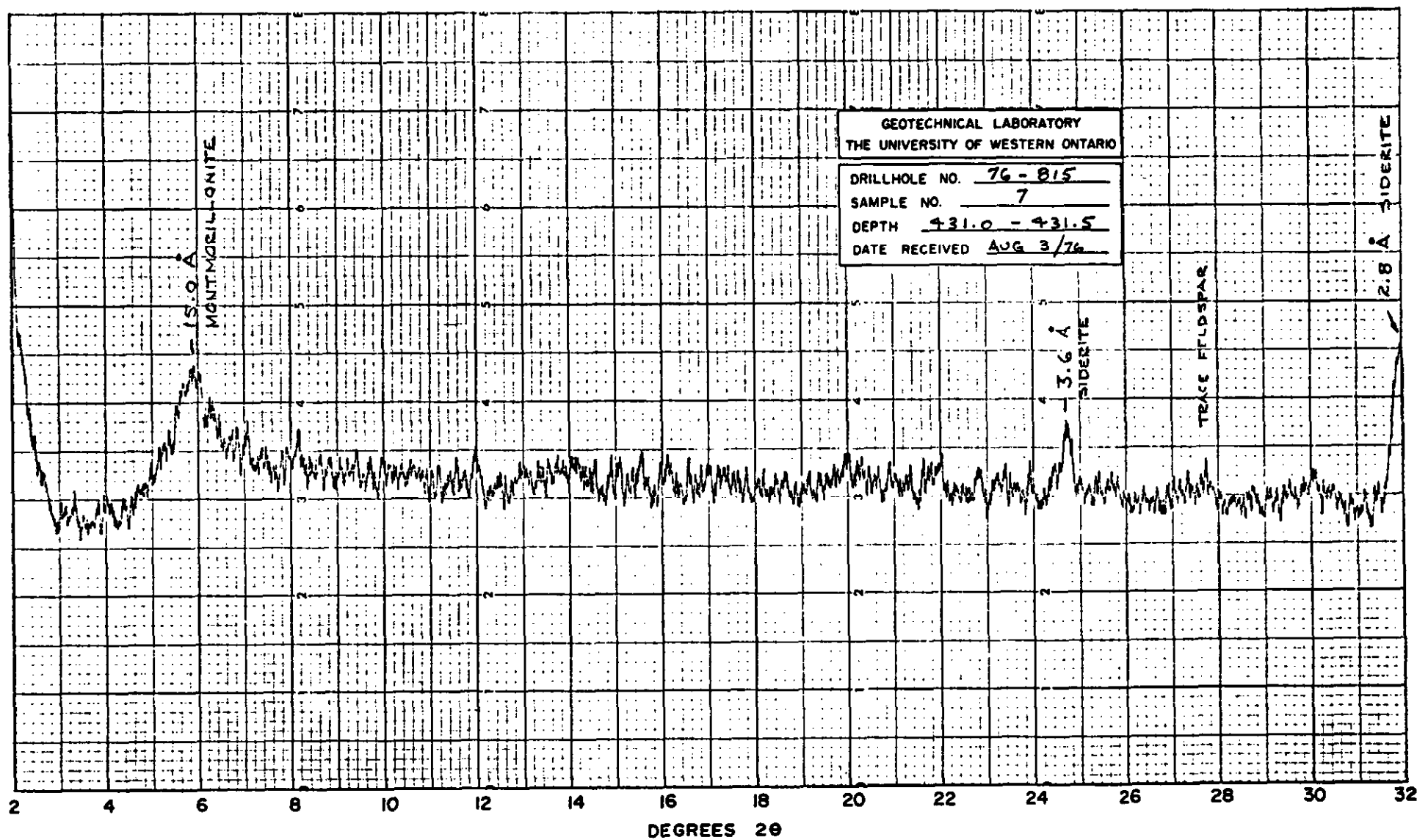
GEOTECHNICAL LABORATORY
THE UNIVERSITY OF WESTERN ONTARIO

Drill Hole No.	Sample No.	Depth (Feet)	Date Received	Testing Completed						
				X-ray				Carbonate (%)	Glycol Retention (mg/g)	Na ⁺ (PPM)
				Wet P.O.	ADPO	GPO	Powder			
76-815	7	431.0 - 431.5	AUG 3/76	✓	✓	✓	✓	34.5		
76-815	9	447.8 - 448.1	AUG 3/76	✓	✓	✓	✓	51.2		
76-815	12	482.3 - 482.6	AUG 3/76	✓	✓	✓	✓	3.5		
76-815	14	505.6 - 506.0	AUG 3/76	✓	✓	✓	✓	7.5		
76-815	18	541.5 - 542.0	AUG 3/76	✓	✓	✓	✓	34.3		
76-815	20	561.7 - 562.3	AUG 3/76	✓	✓	✓	✓	9.3		
76-815	22	582.7 - 583.2	AUG 3/76	✓	✓	✓	✓	67.6		
76-815	29	669.0 - 669.7	AUG 3/76	✓	✓	✓	✓	35.5		

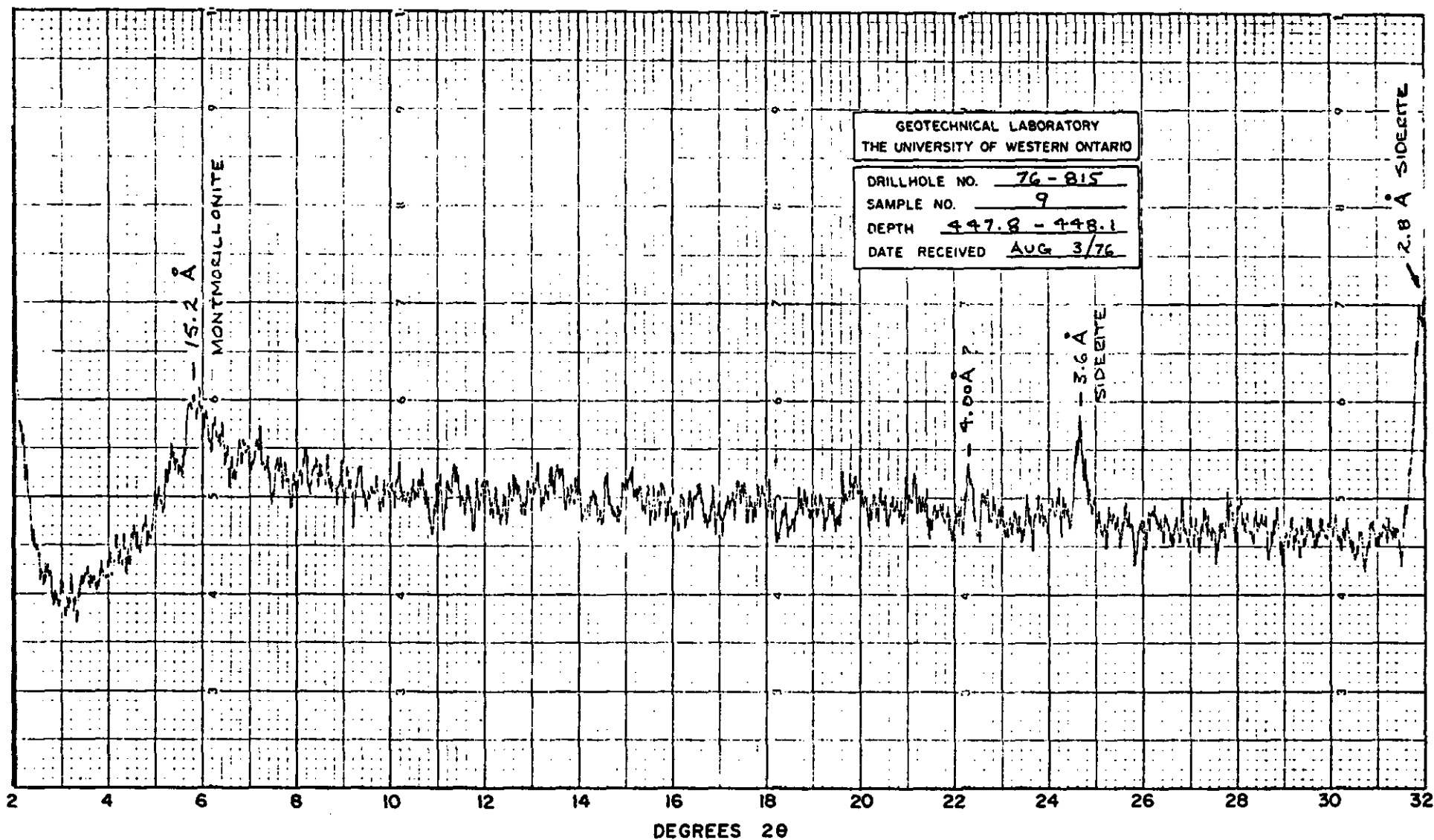
REPORT #3

K.M. Quigley

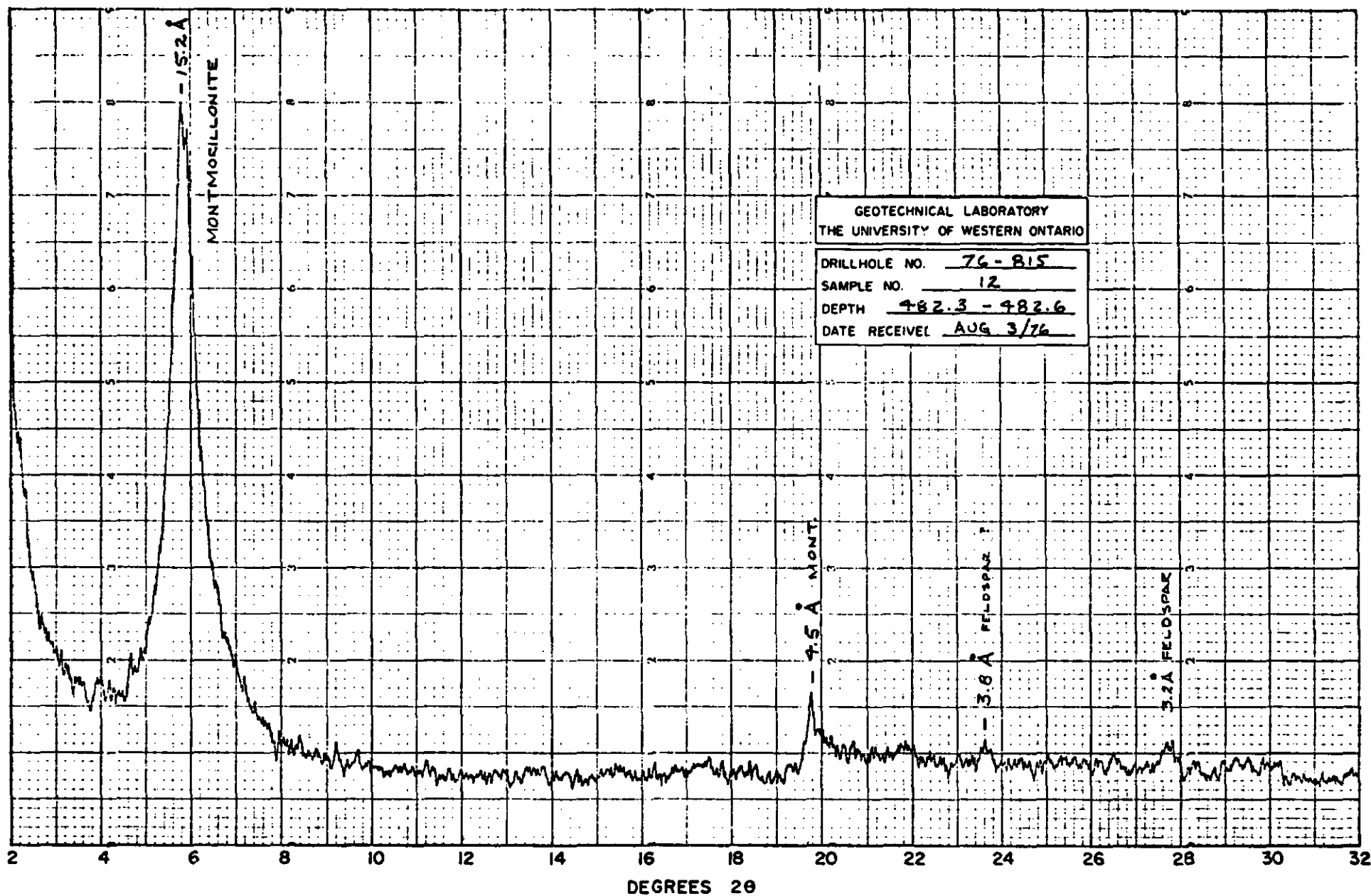
Aug. 20, 1976



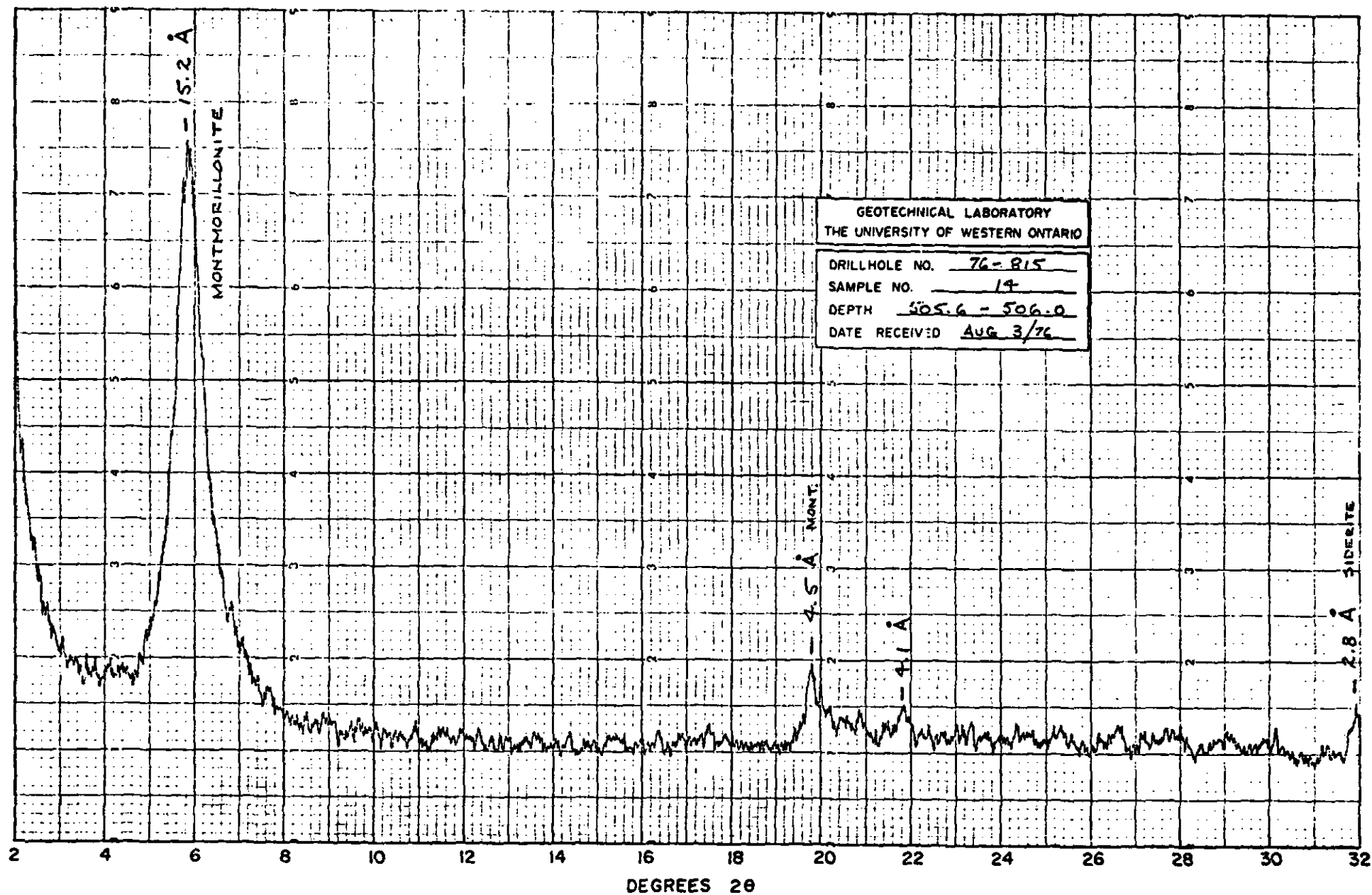
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



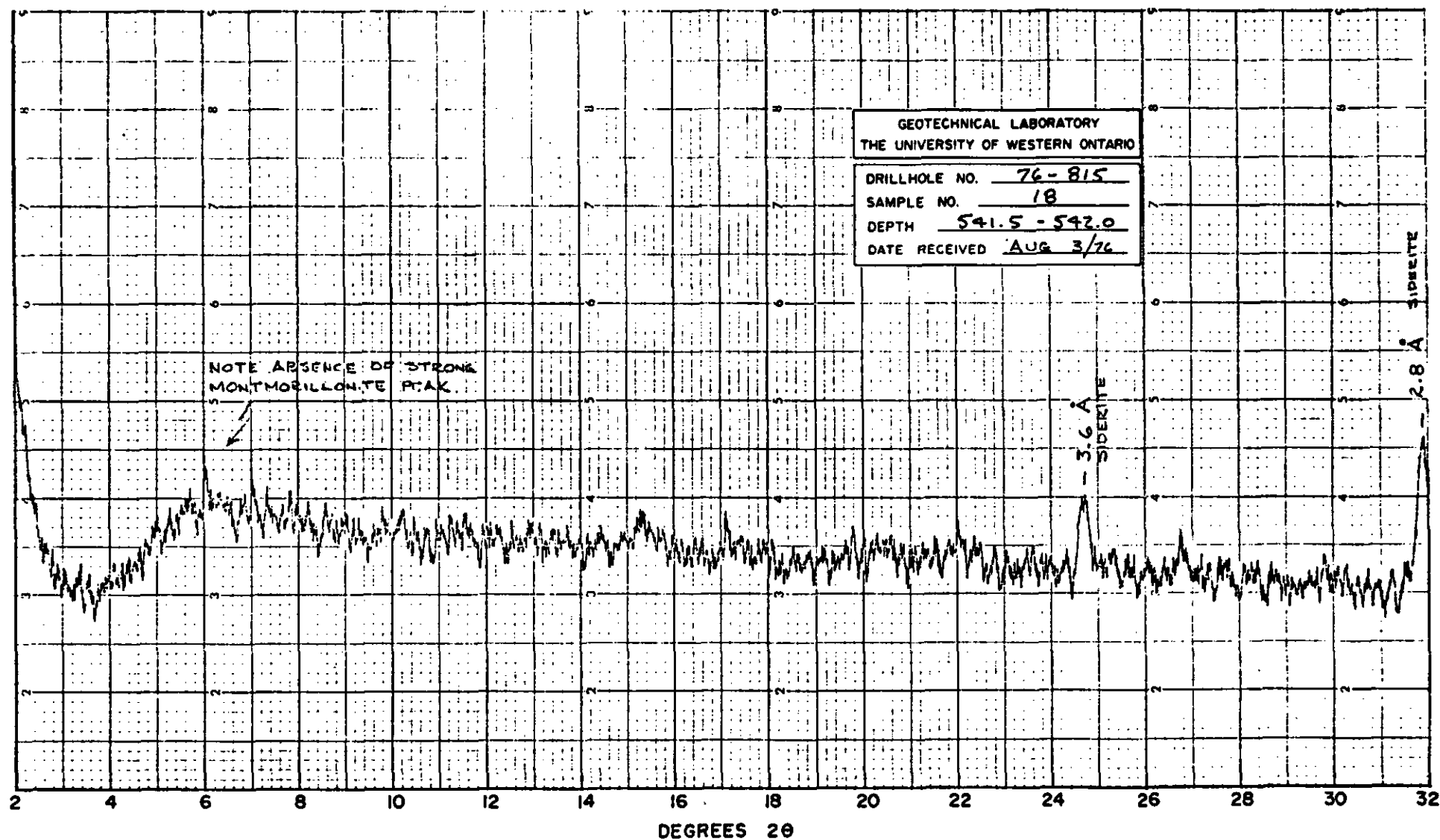
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



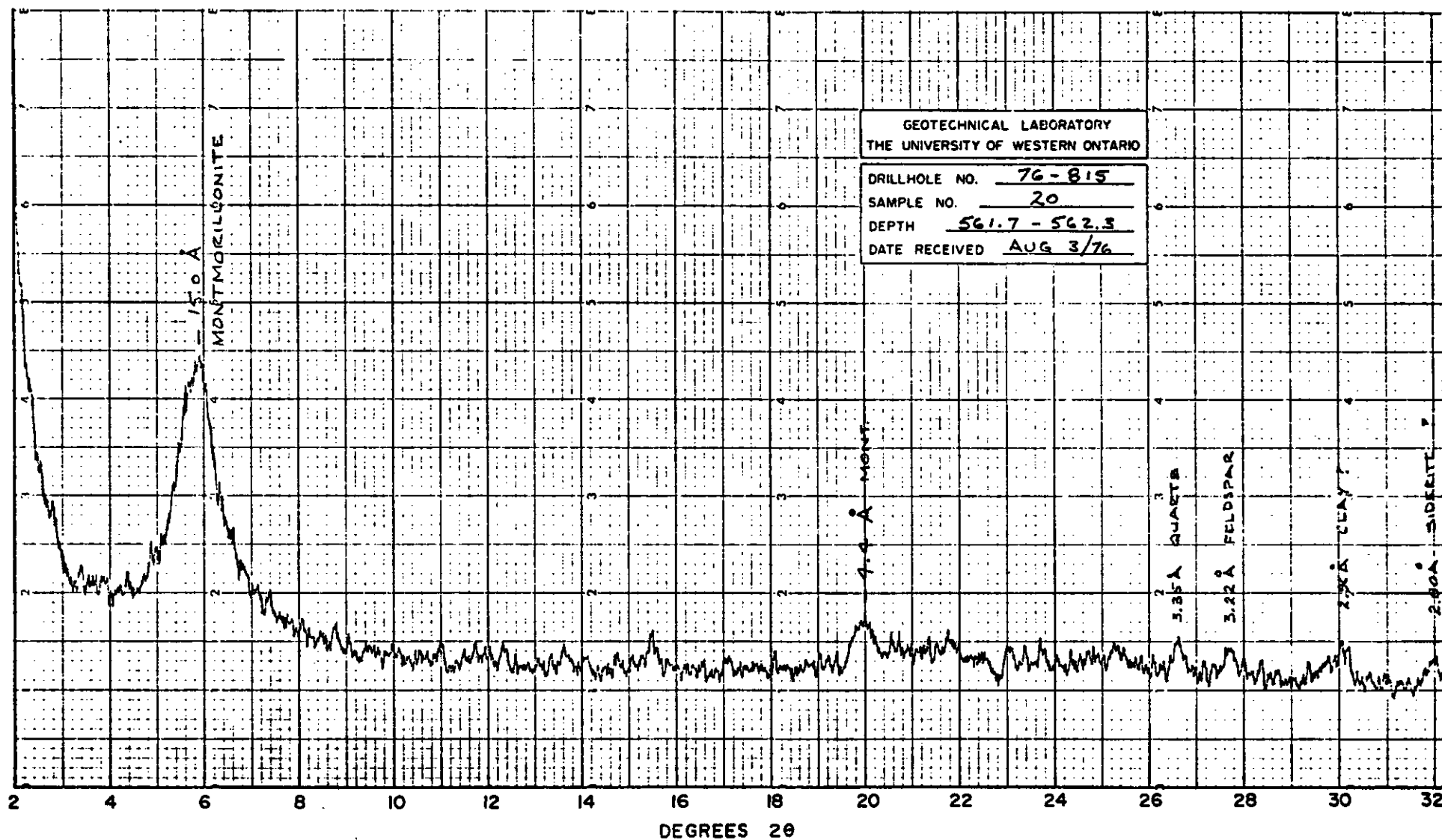
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



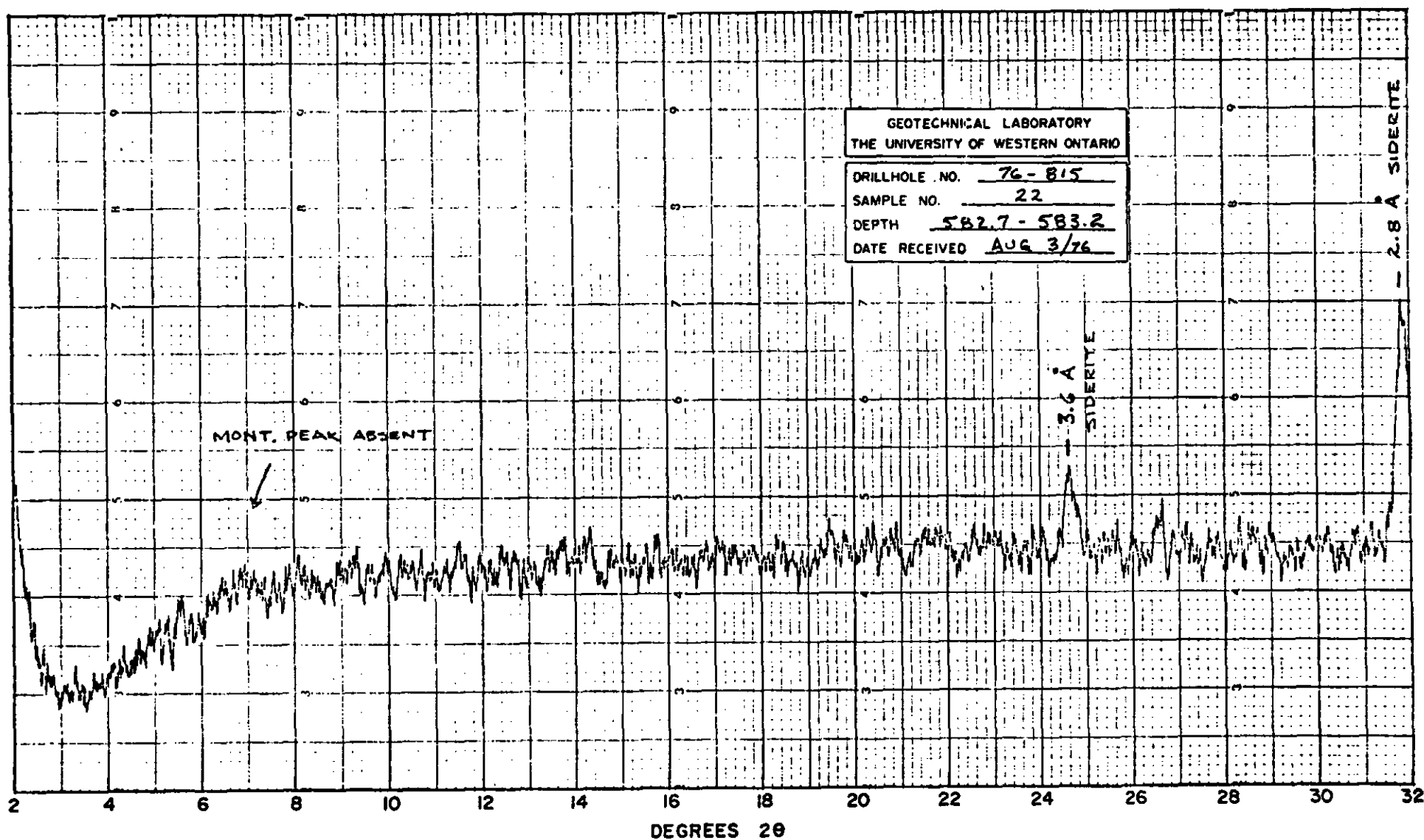
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



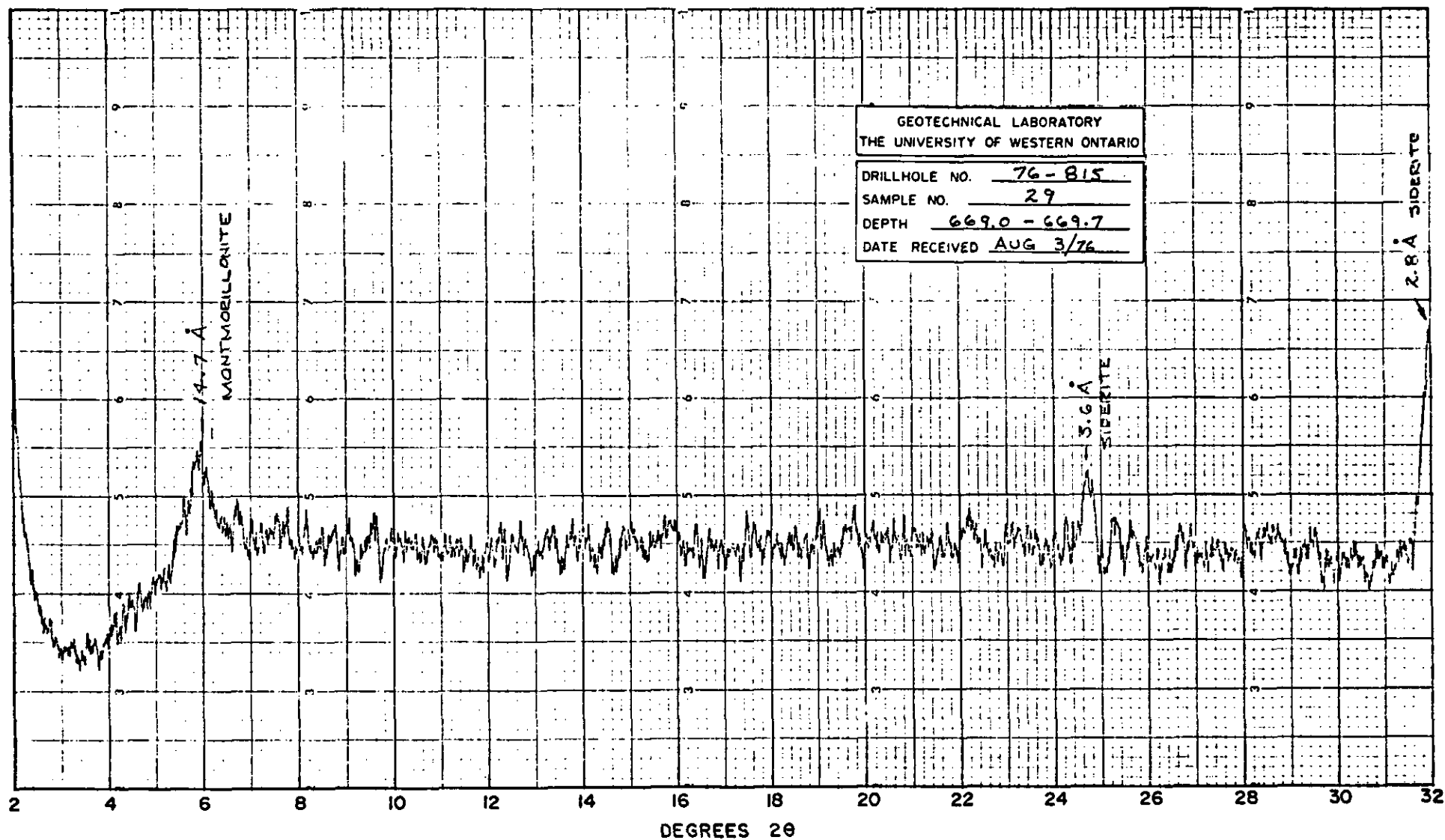
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



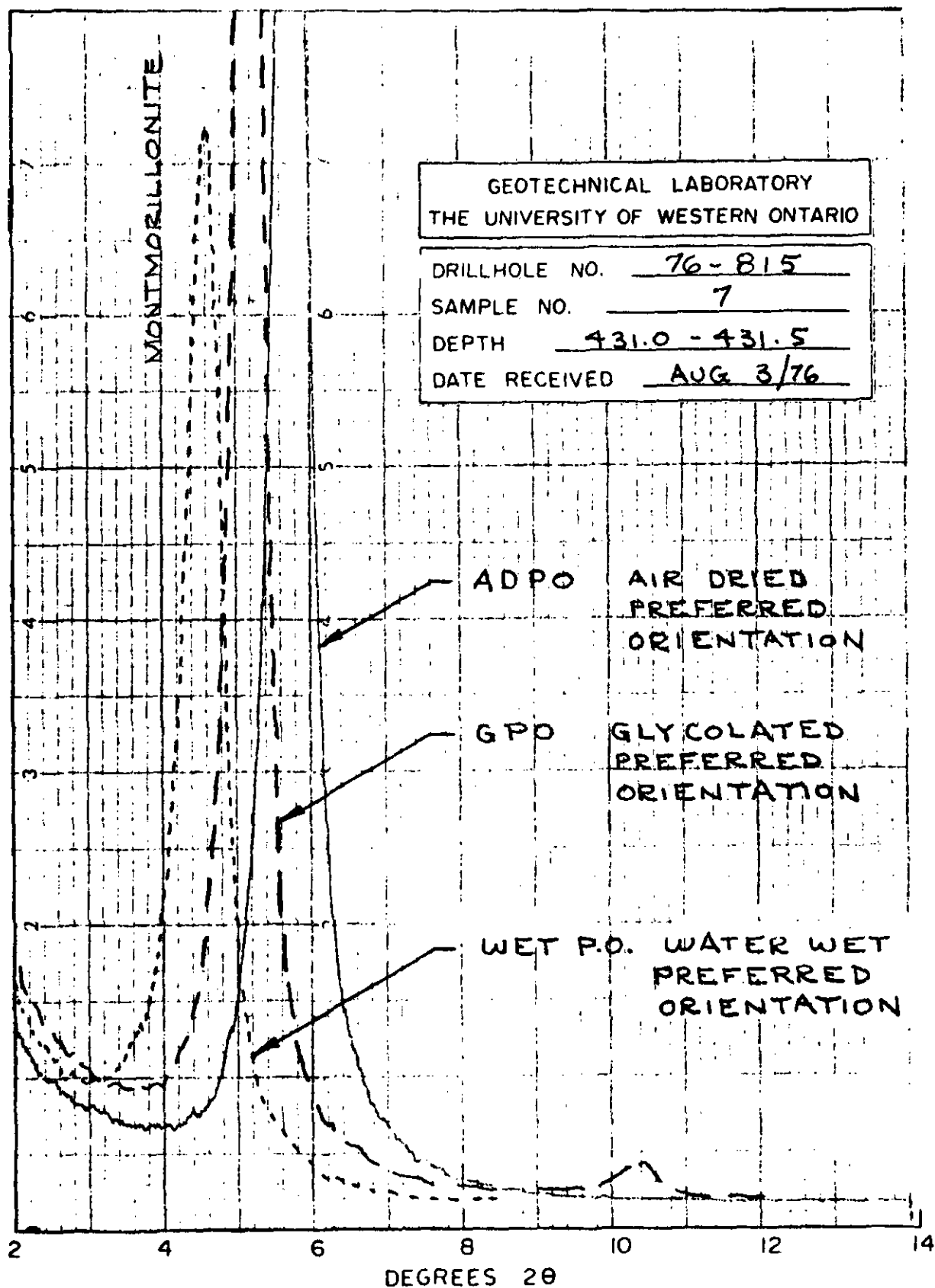
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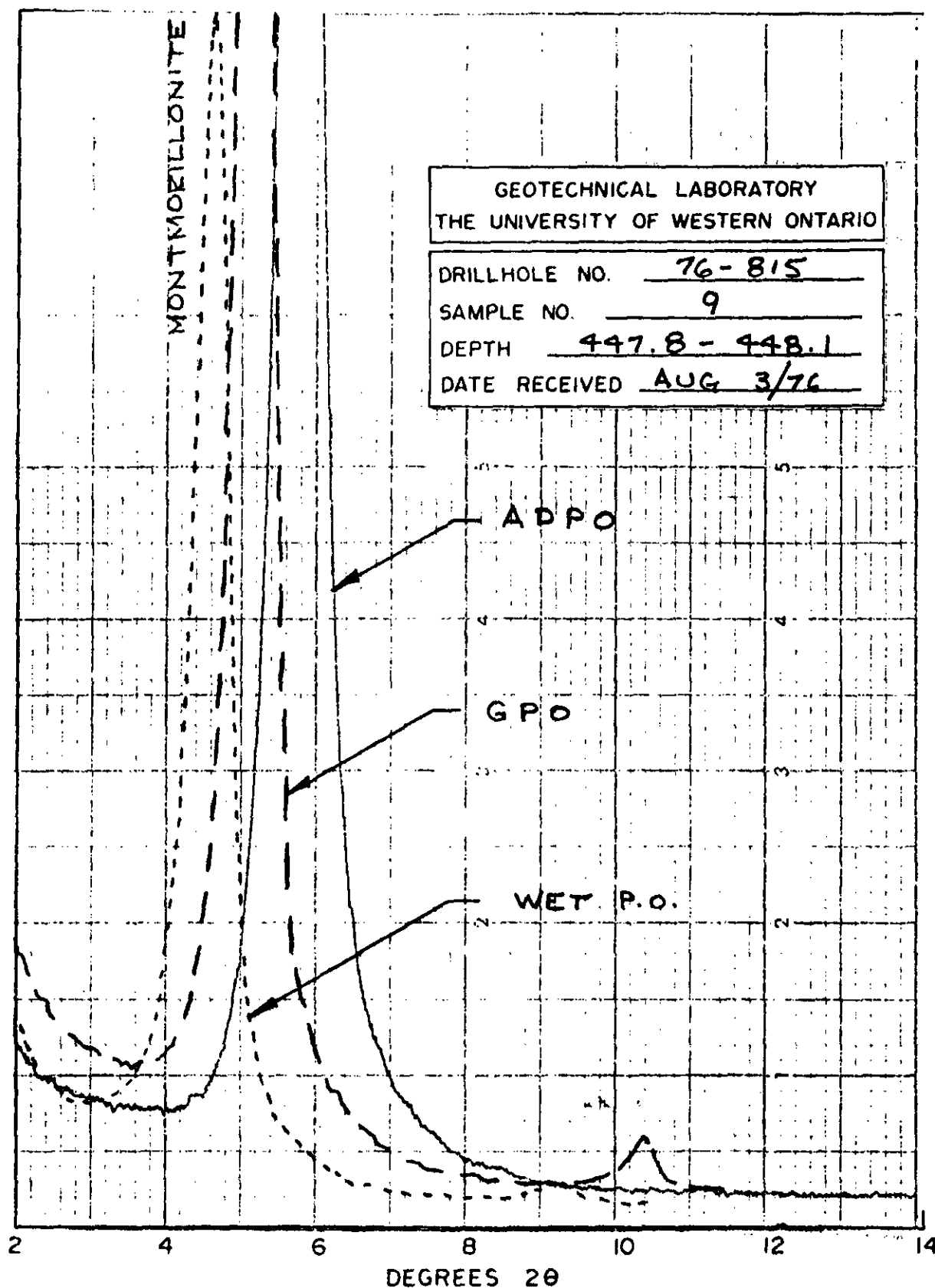
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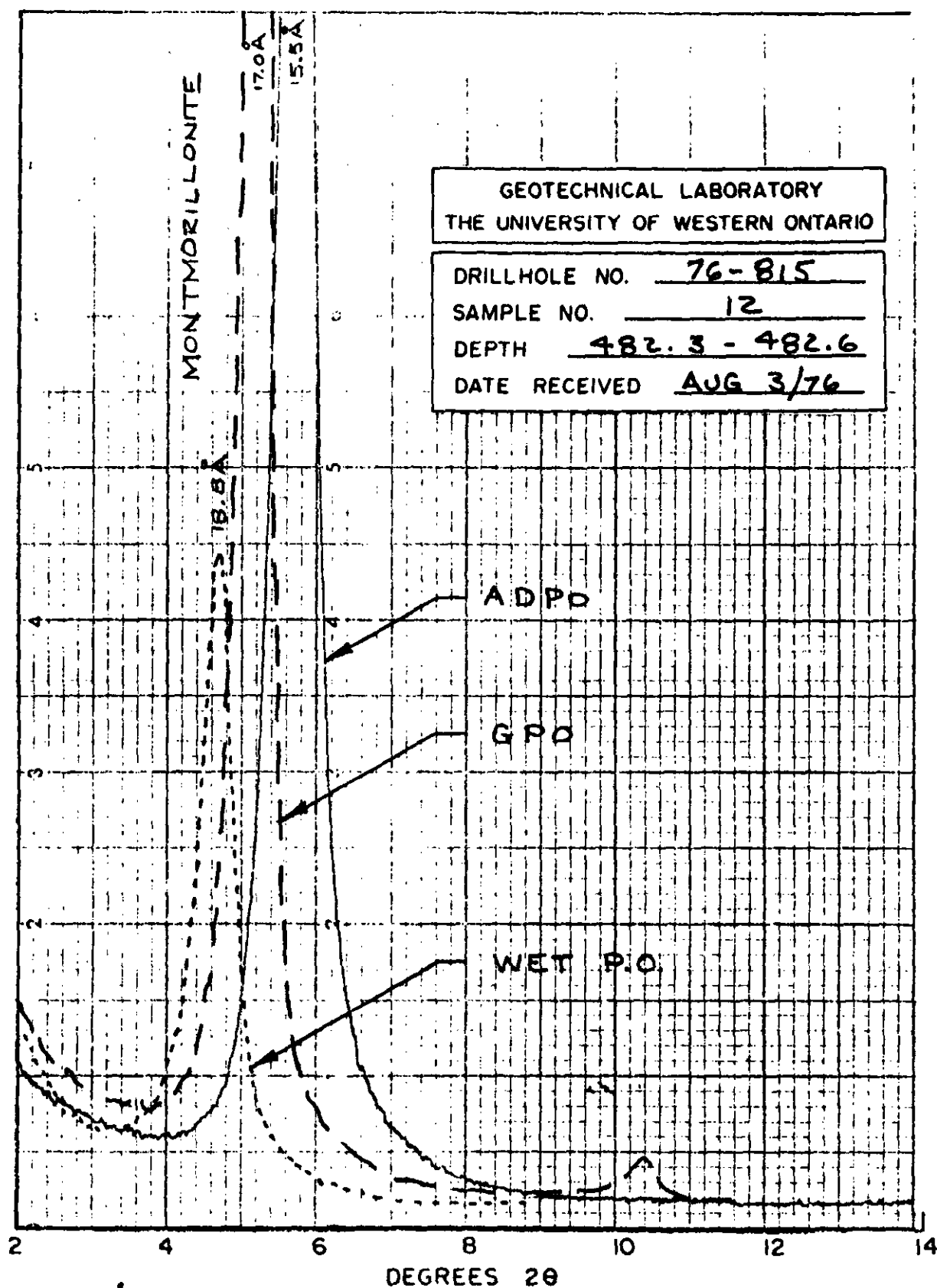
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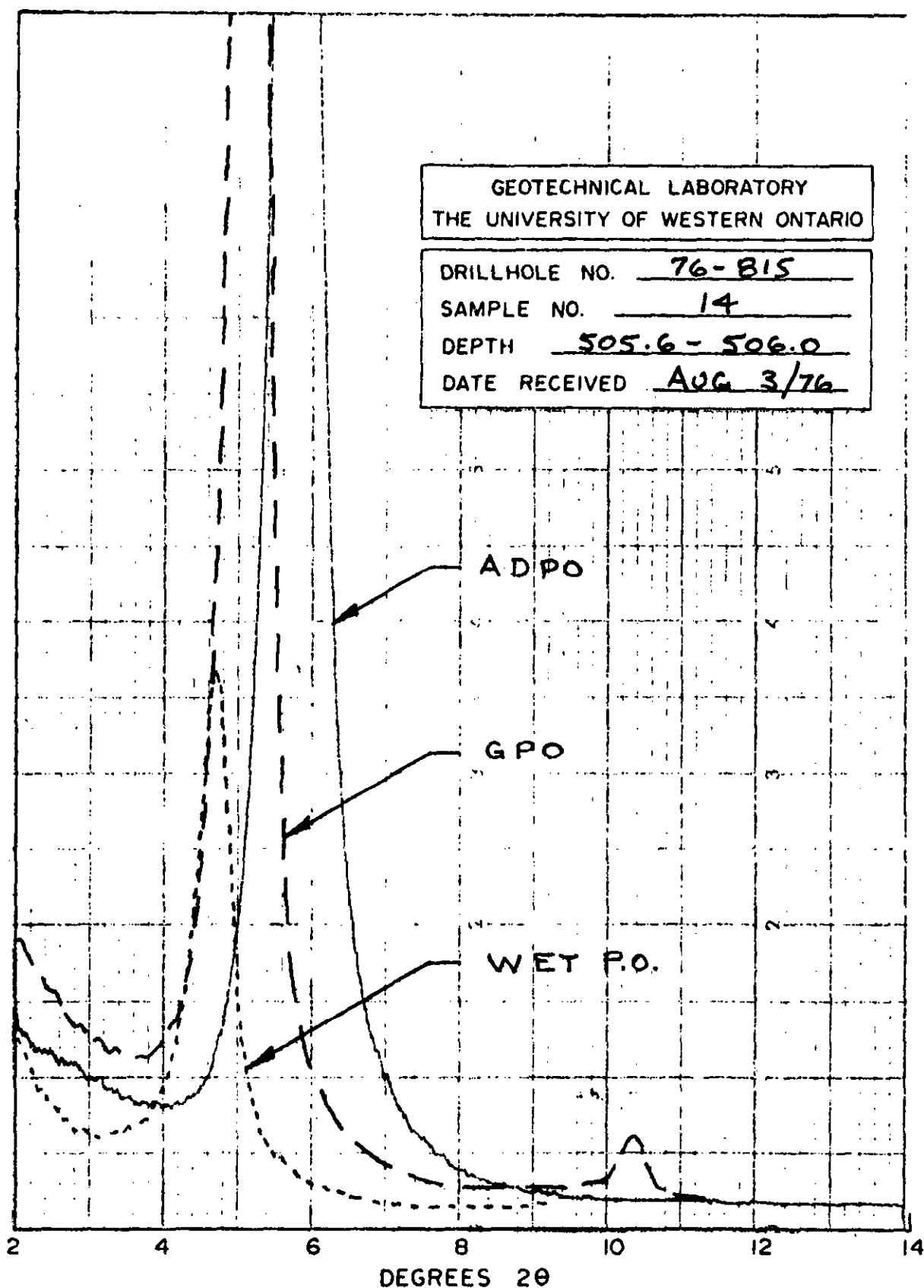
X-RAY DIFFRACTION TRACES OF 2μ , PREFERRED
ORIENTED SPECIMENS FROM HAT CREEK.



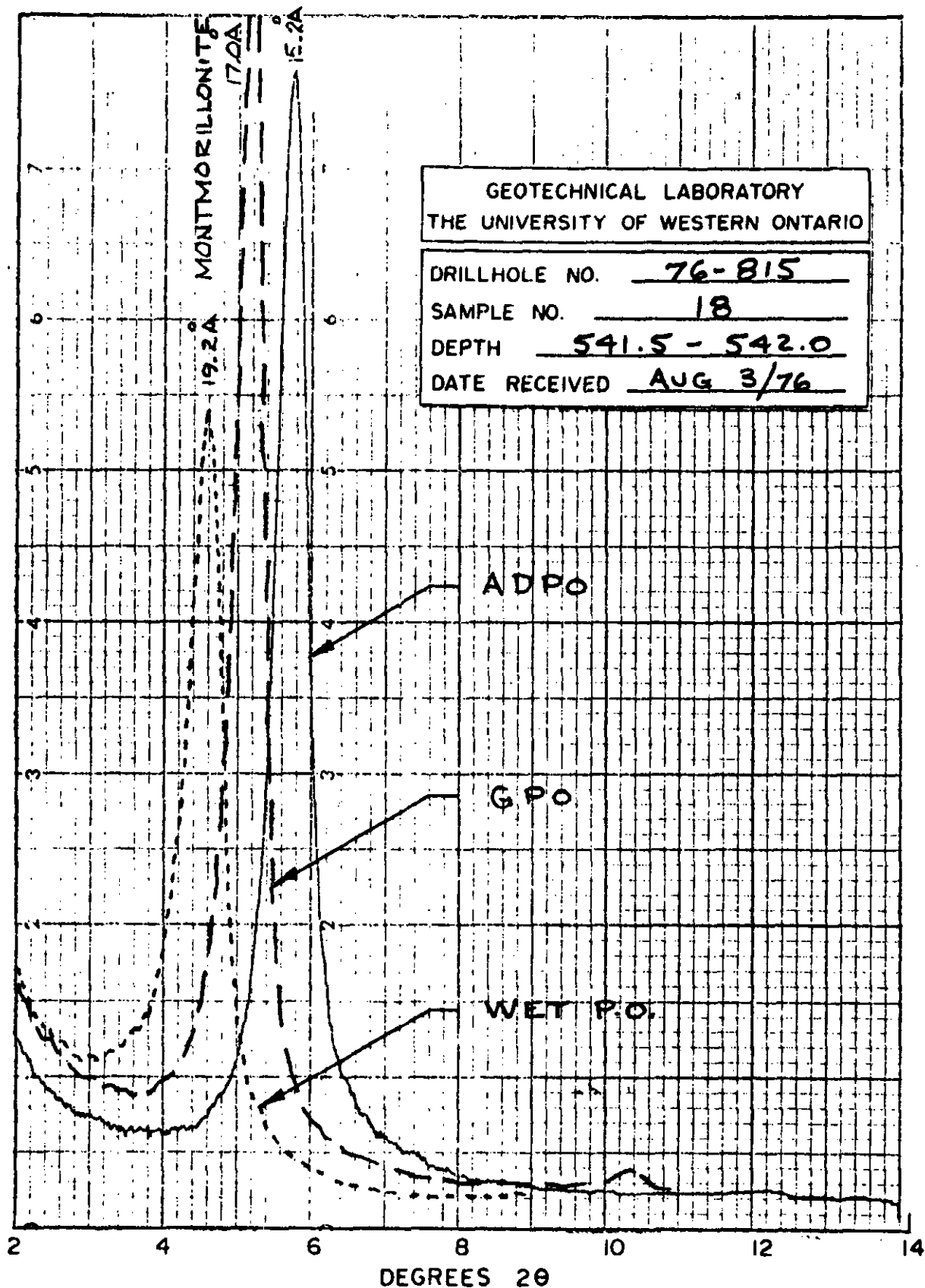
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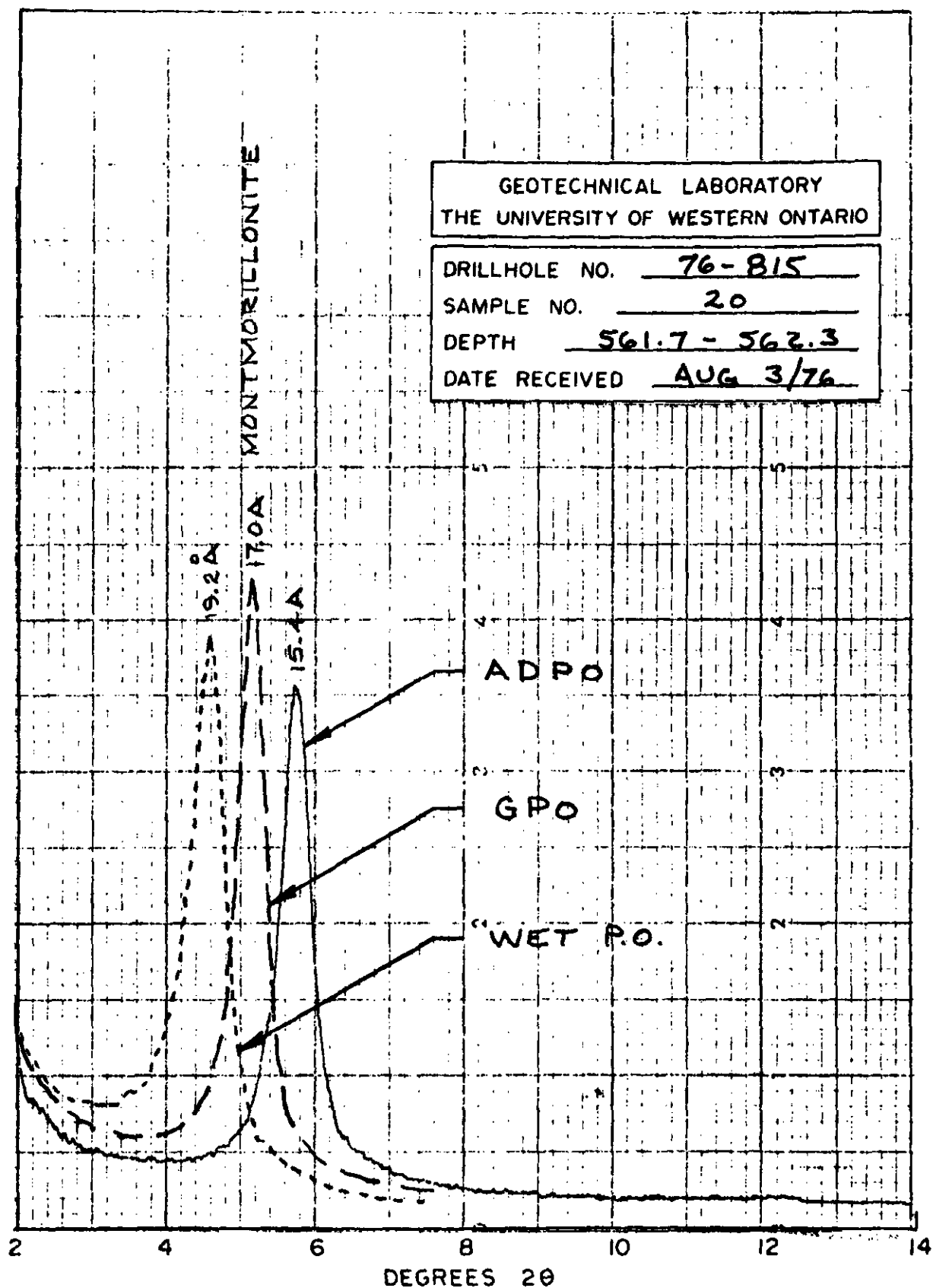
X-RAY DIFFRACTION TRACES OF 2μ , PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



X-RAY DIFFRACTION TRACES OF 2μ , PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



X-RAY DIFFRACTION TRACES OF 2μ , PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



X-RAY DIFFRACTION TRACES OF 2μ , PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.

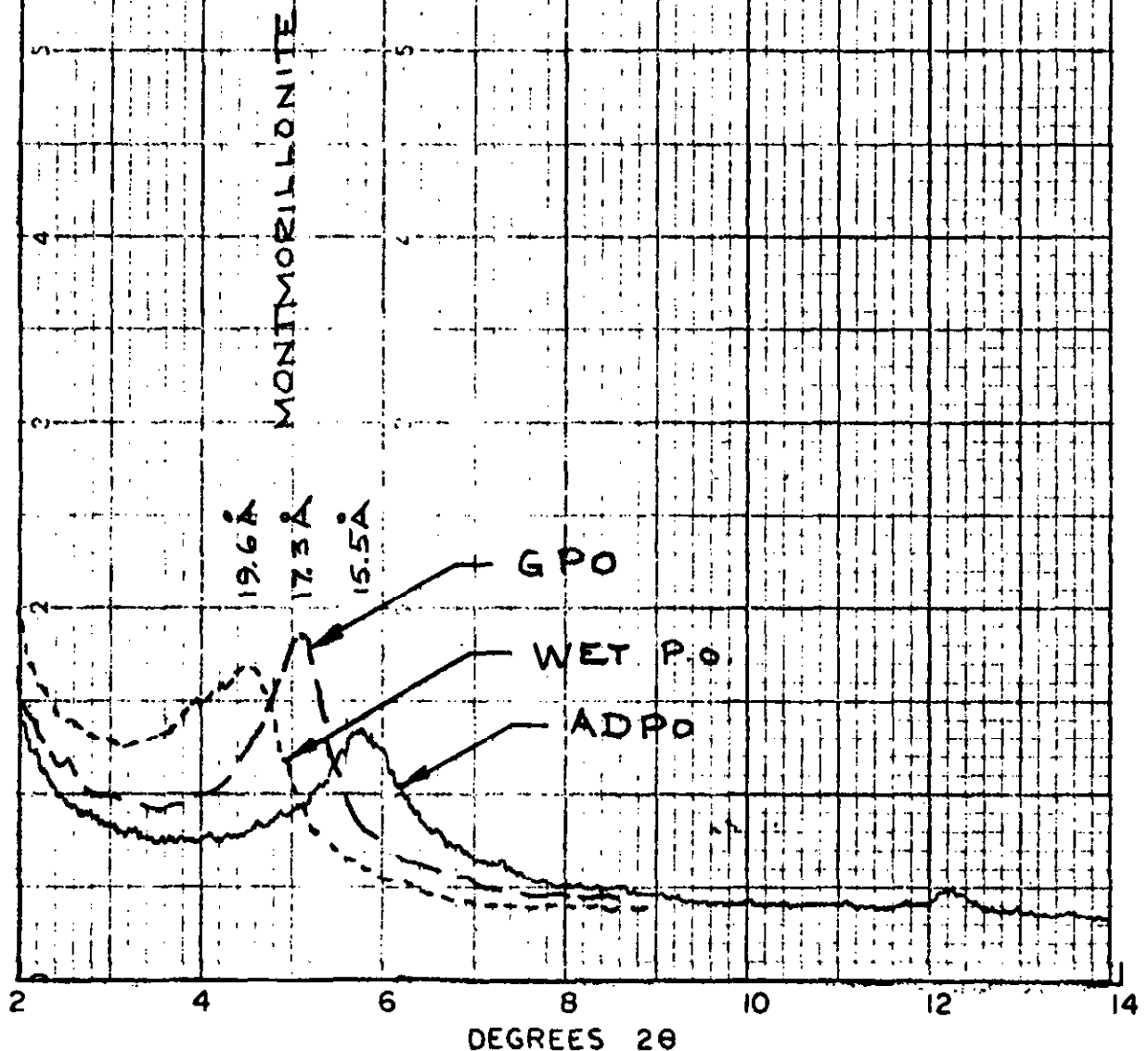
GEOTECHNICAL LABORATORY
THE UNIVERSITY OF WESTERN ONTARIO

DRILLHOLE NO. 76-815

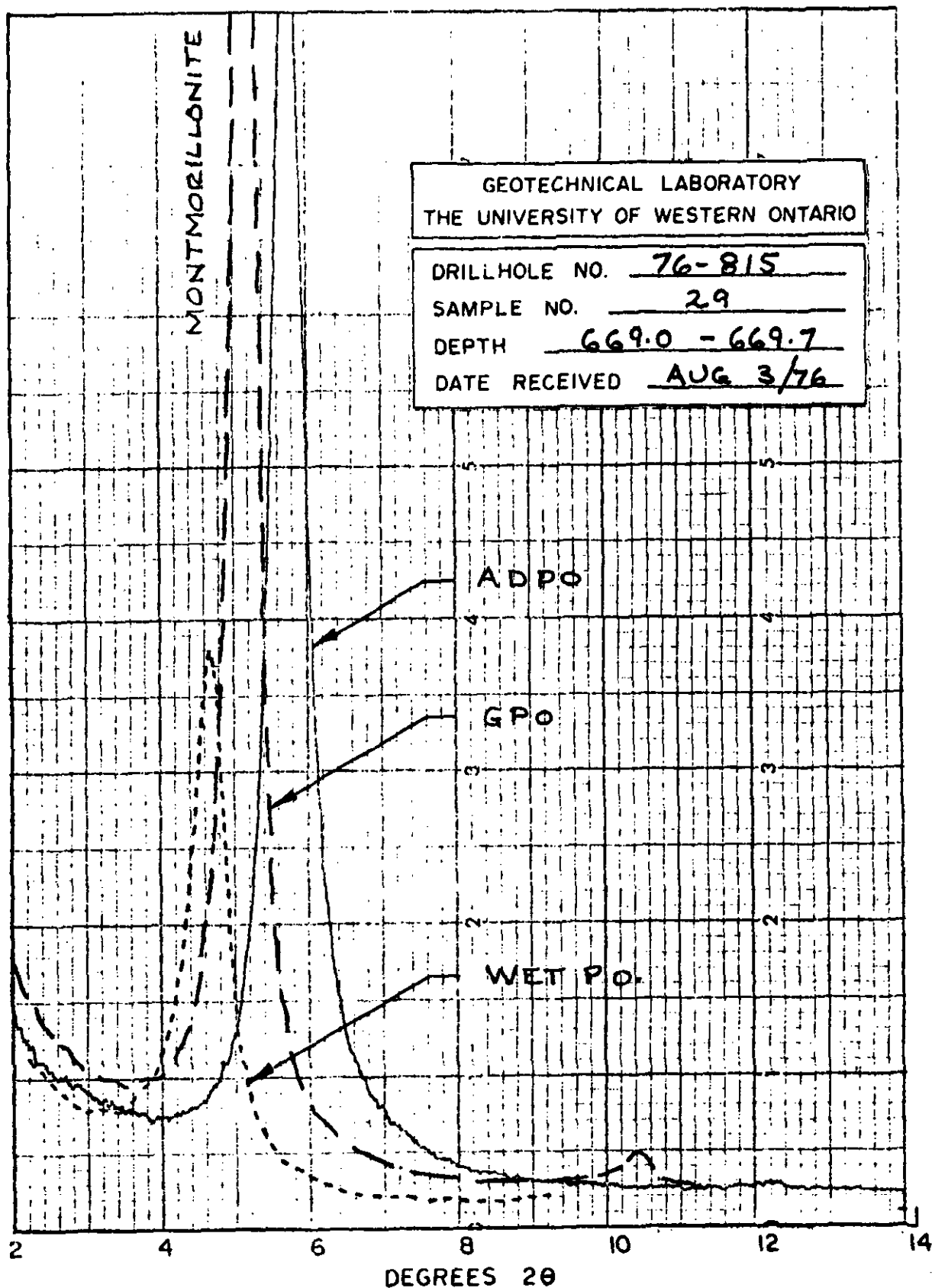
SAMPLE NO. 22

DEPTH 582.7 - 583.2

DATE RECEIVED AUG 3/76



X-RAY DIFFRACTION TRACES OF 2μ , PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



X-RAY DIFFRACTION TRACES OF 2μ , PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.

FEB 15 1977

FILE No.



Faculty of Engineering Science
London, Canada
N6A 5B9

The University of Western Ontario, London, Canada

7 September 1976

Mr. G. Rawlings
Golder, Brawner & Associates Ltd.
224 West 8th Avenue
Vancouver, British Columbia
V5Y 1N5

Dear Mr. Rawlings:

Report #4 - Hat Creek Project - Mineralogical Analyses
September 8, 1976

Enclosed are the x-ray and carbonate analyses on the last eight samples of Mr. Hawson's shipment of August 3, 1976.

On the basis of the cross-sections which you are sending to me, I will select samples for Na⁺ and glycol retentions. As we discussed by phone today, I will call you prior to commencing this last phase of the testing.

Specific Comments on Present Samples

1. Carbonate is abundant only in sample 76-816.
2. Most of the samples consist of montmorillonite and feldspar with trace amounts of quartz.
3. Sample 76-809 (#2) may contain some cristobalite.

Yours sincerely,

R.M. Quigley, P.Eng.
Professor of Geotechnical Engineering

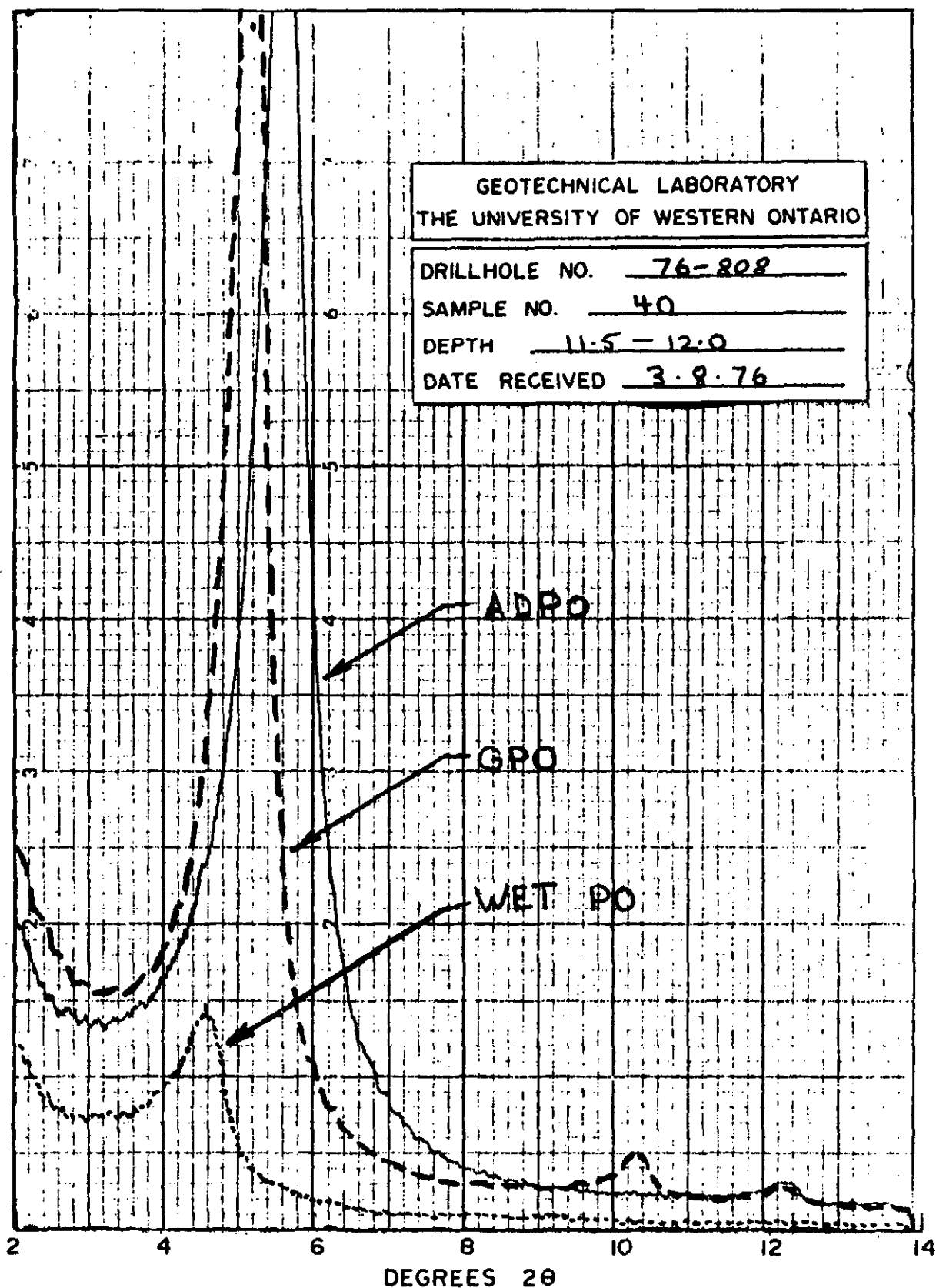
RMQ:em
Encs.

cc: Mr. H.H. Hawson, Kamloops, B.C.

LIST OF SAMPLES RECEIVED FROM GOLDER BRAWNER & ASSOCIATES

THE UNIVERSITY OF WESTERN ONTARIO

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X-RAY DIFFRACTION TRACES OF 2μ , PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.

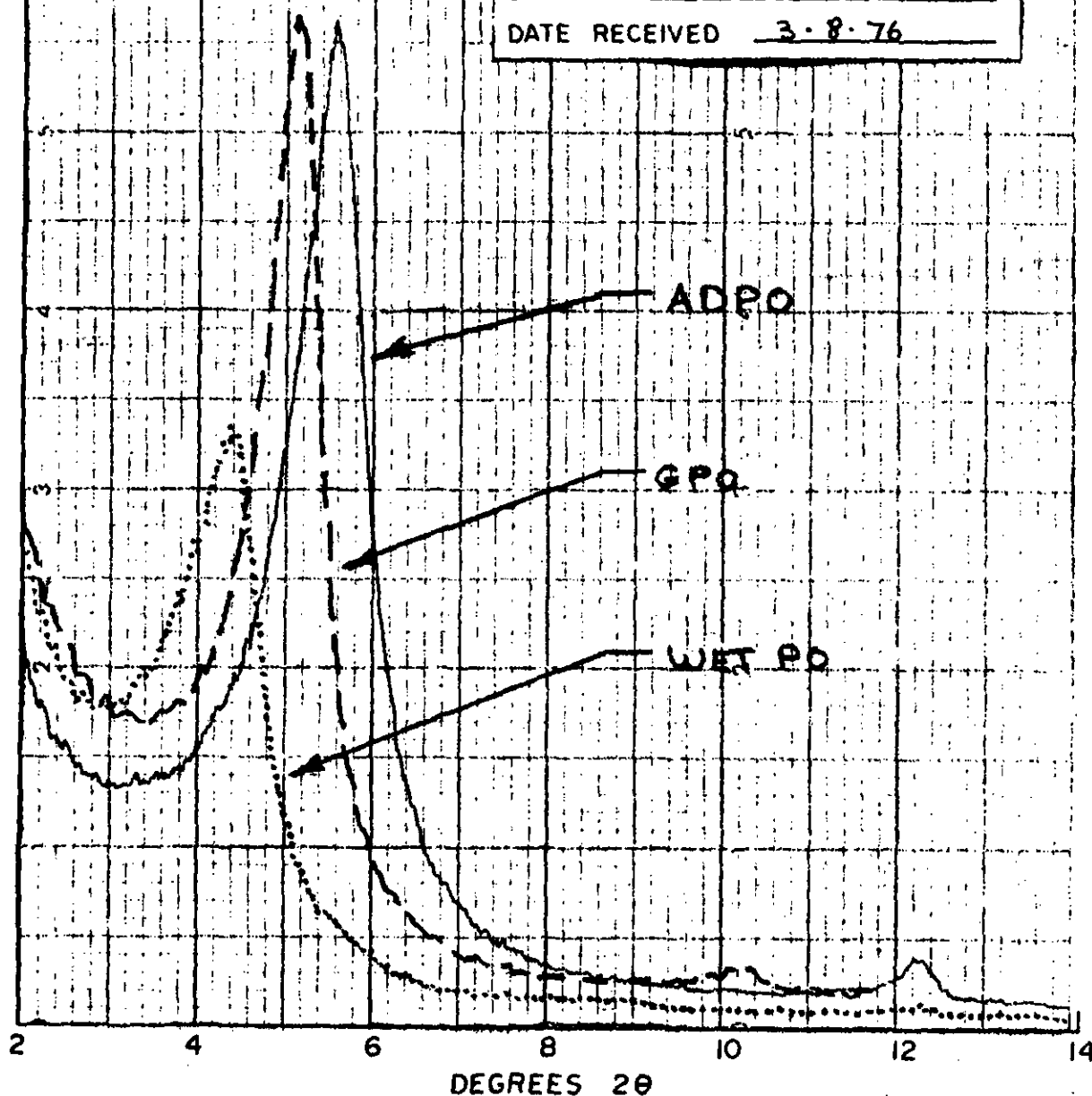
GEOTECHNICAL LABORATORY
THE UNIVERSITY OF WESTERN ONTARIO

DRILLHOLE NO. 76-808

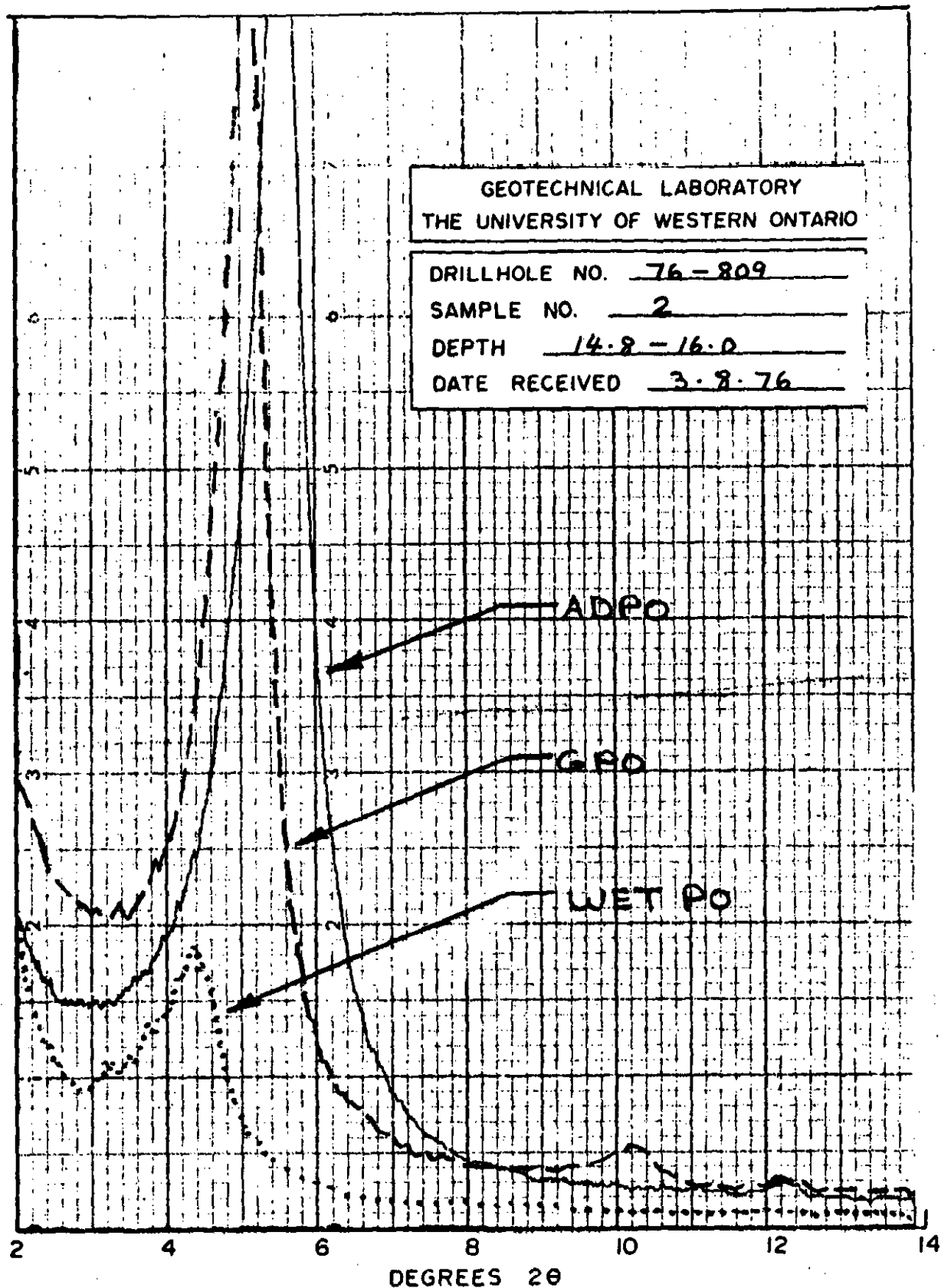
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DEPTH 30.8 - 33.3

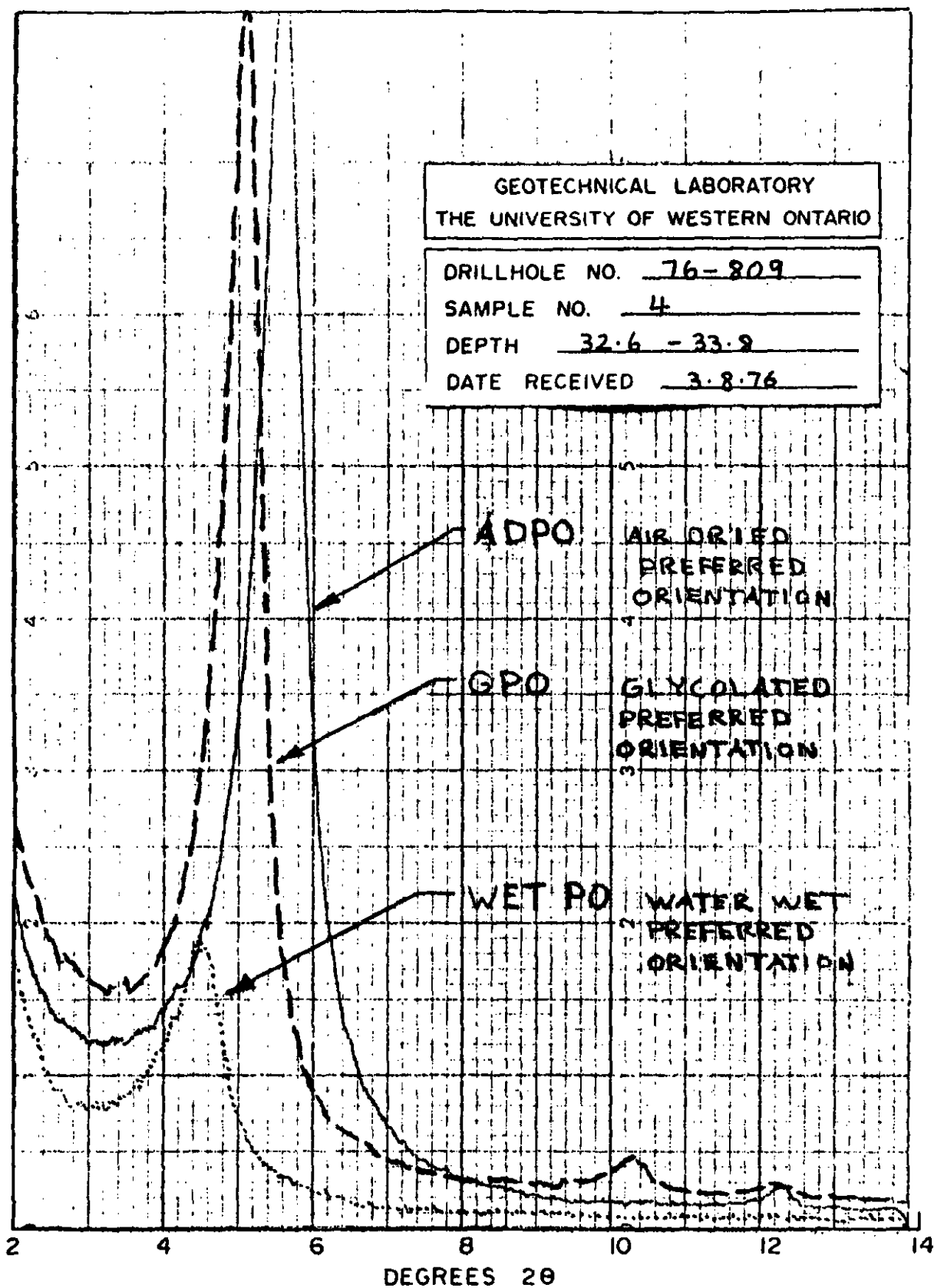
DATE RECEIVED 3.8.76



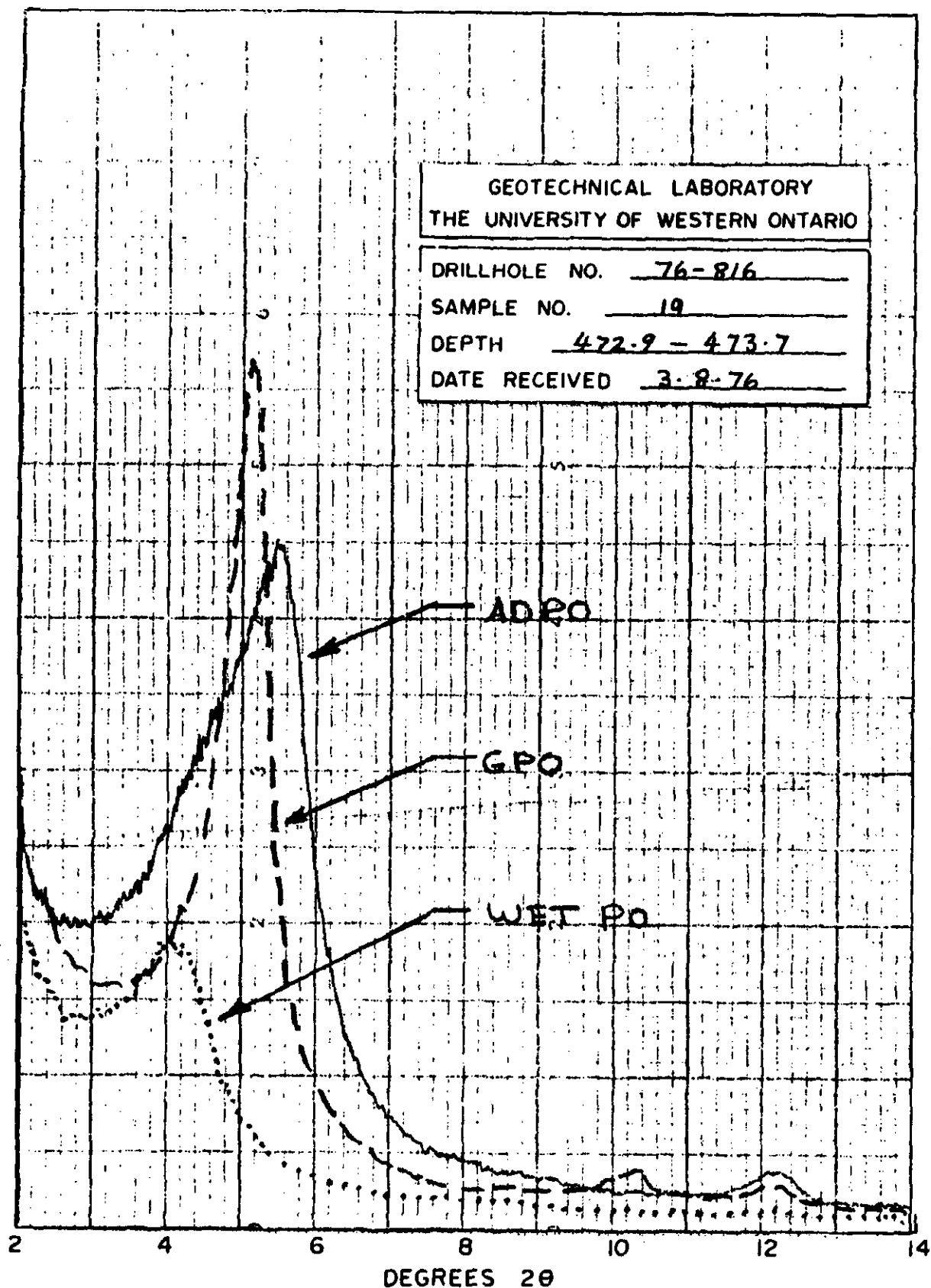
X-RAY DIFFRACTION TRACES OF 2μ , PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



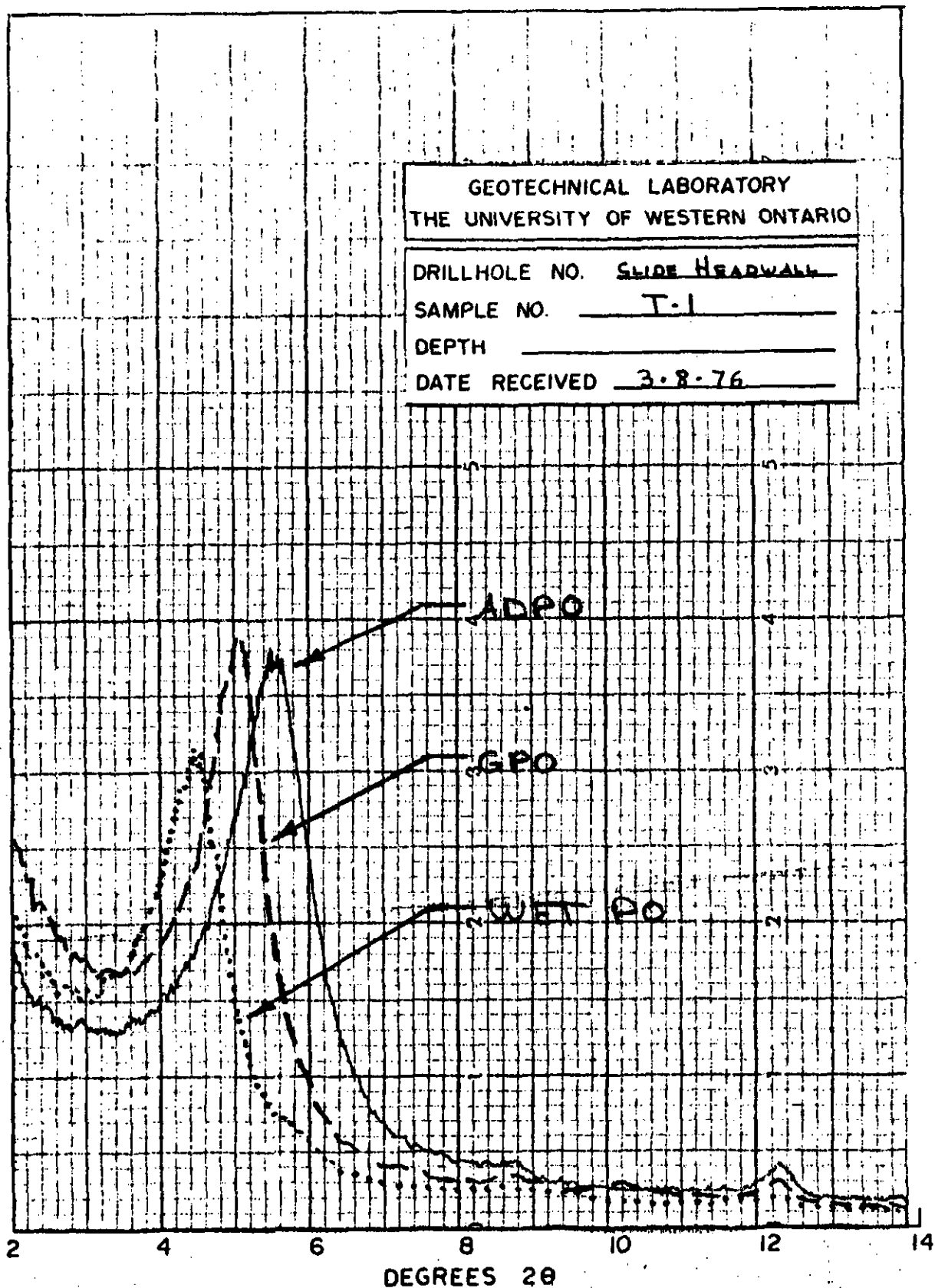
X-RAY DIFFRACTION TRACES OF 2μ , PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



X-RAY DIFFRACTION TRACES OF 2μ , PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



X-RAY DIFFRACTION TRACES OF 2μ , PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



X-RAY DIFFRACTION TRACES OF 2μ , PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.

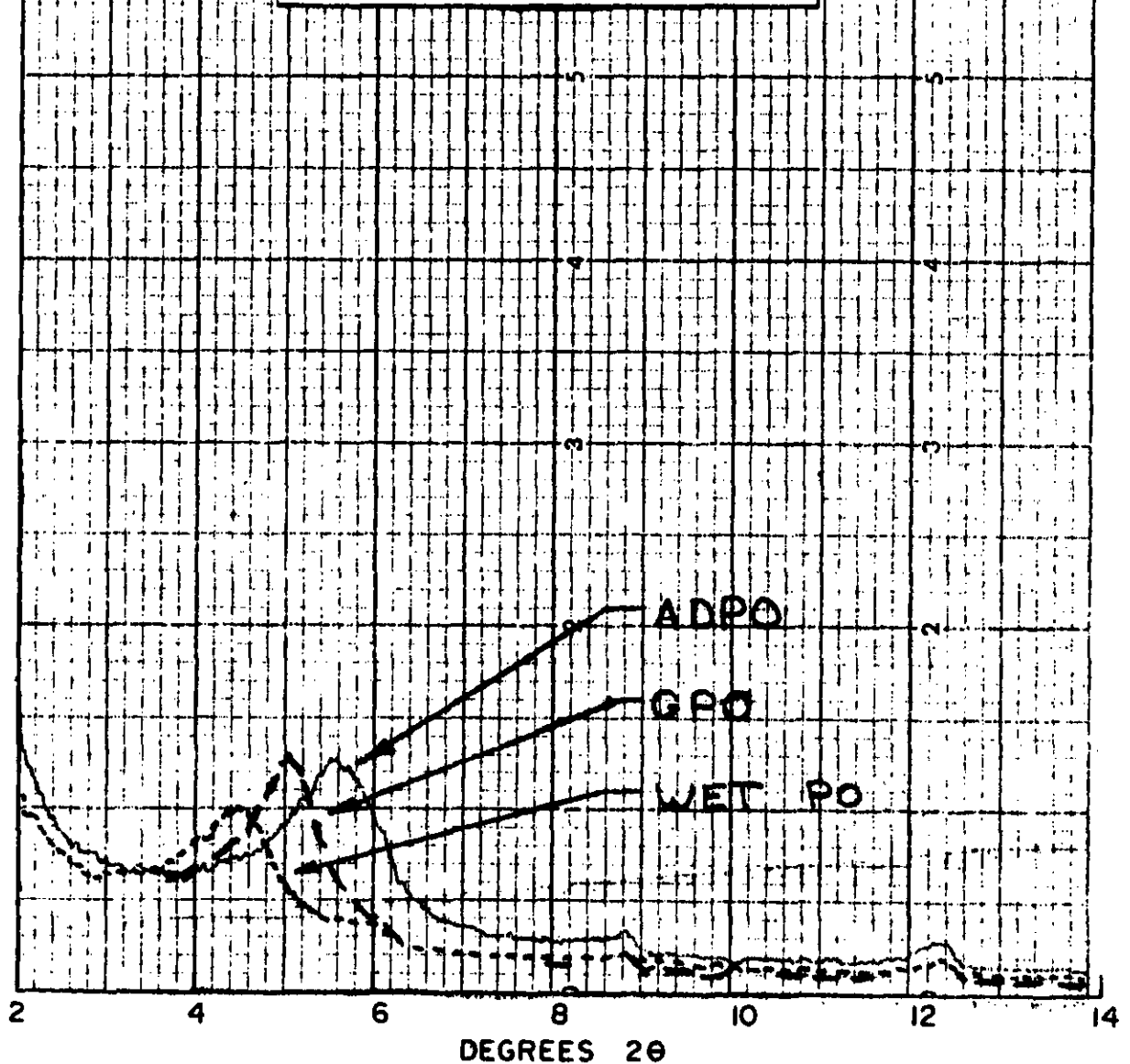
GEOTECHNICAL LABORATORY
THE UNIVERSITY OF WESTERN ONTARIO

DRILLHOLE NO. SLIDE HEADWALL

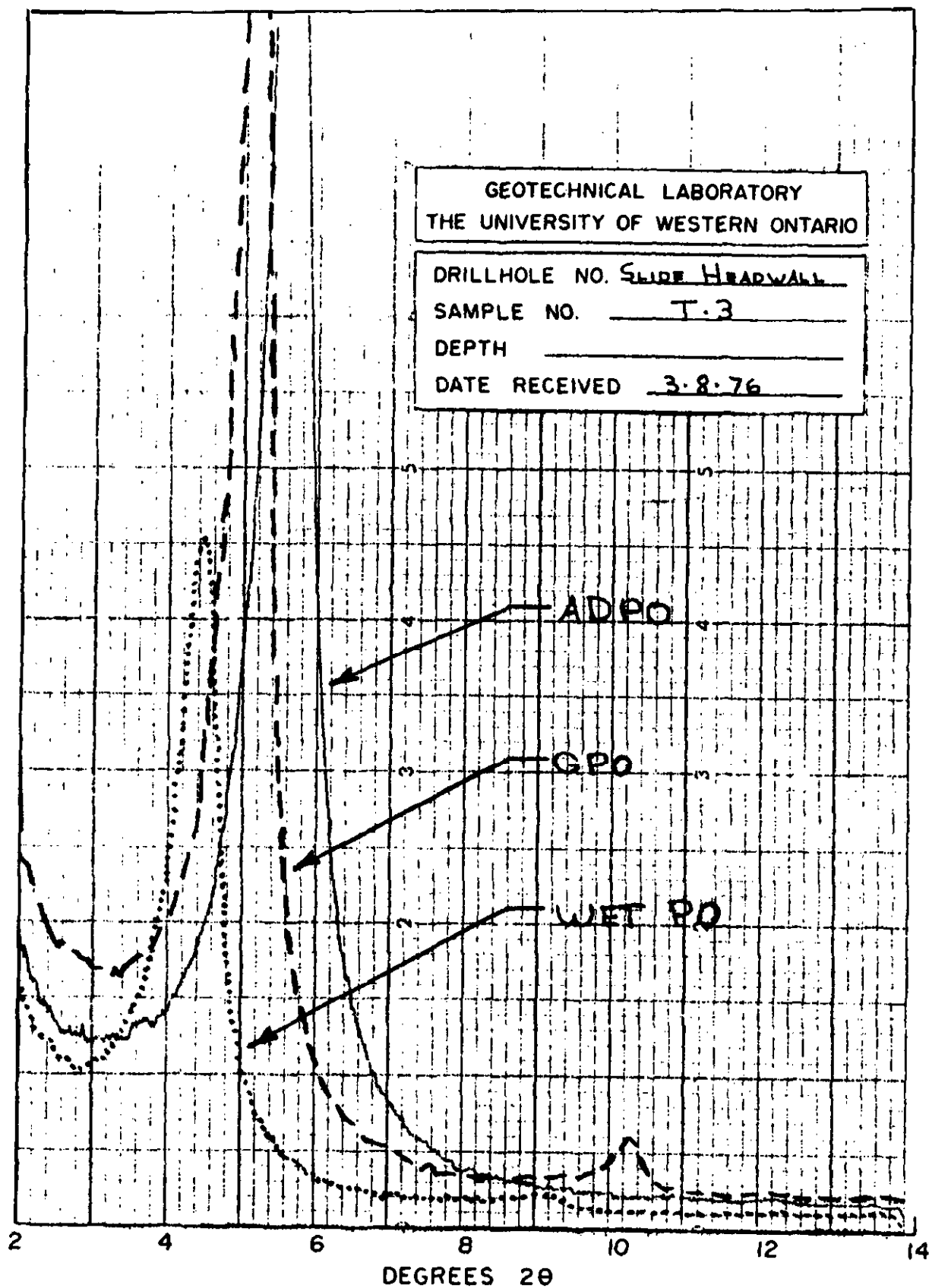
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DEPTH

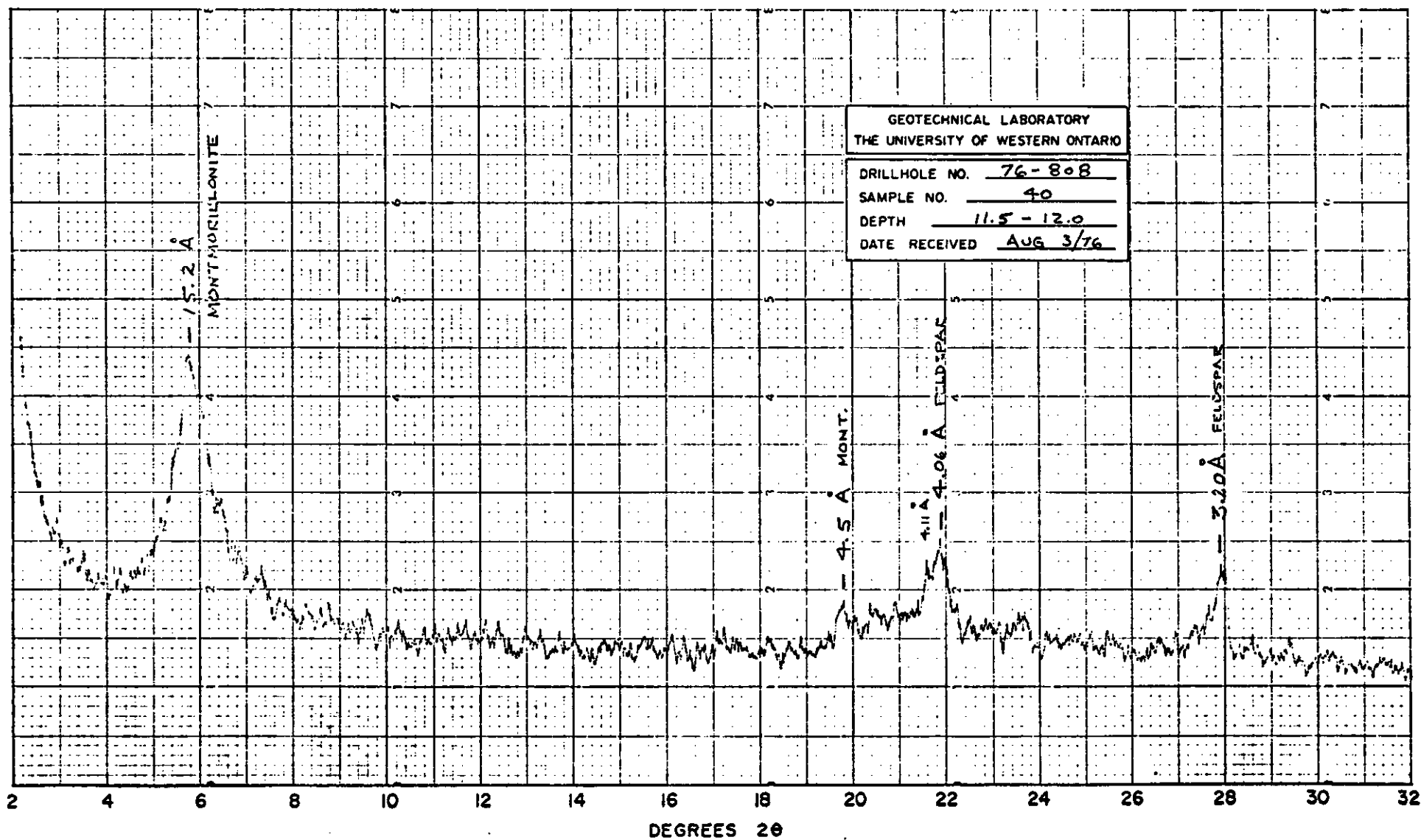
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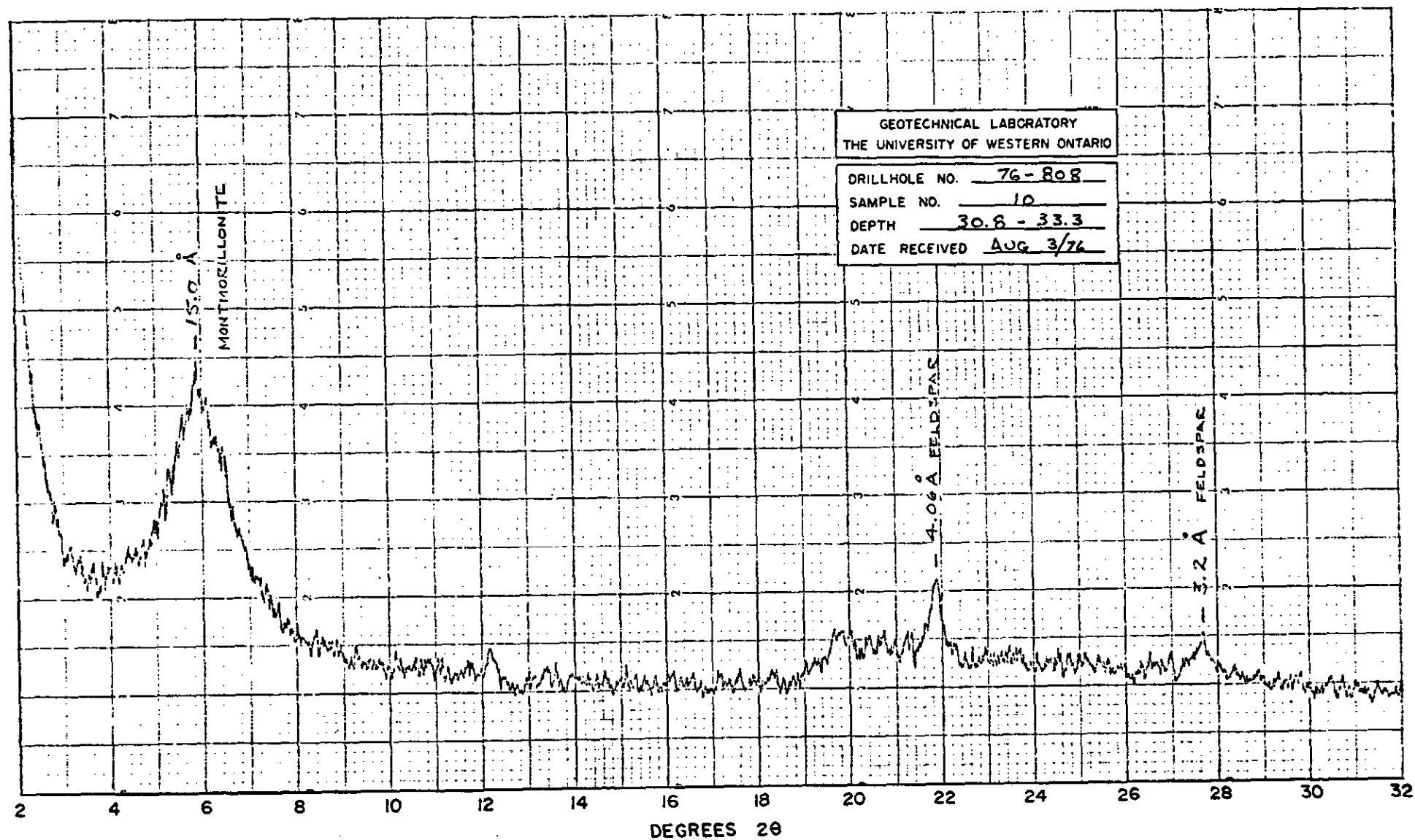
X-RAY DIFFRACTION TRACES OF 2μ , PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



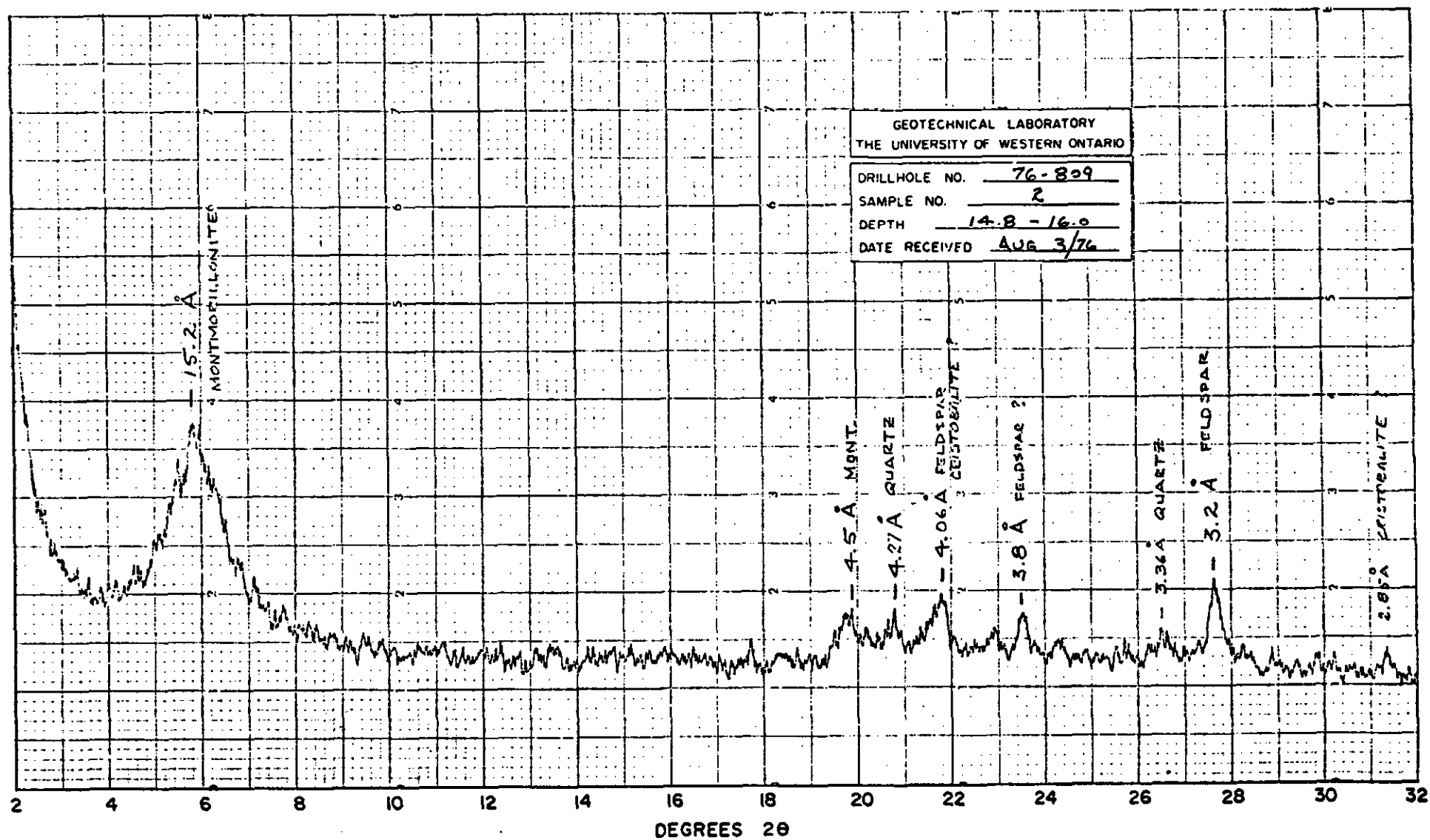
X-RAY DIFFRACTION TRACES OF 2μ , PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



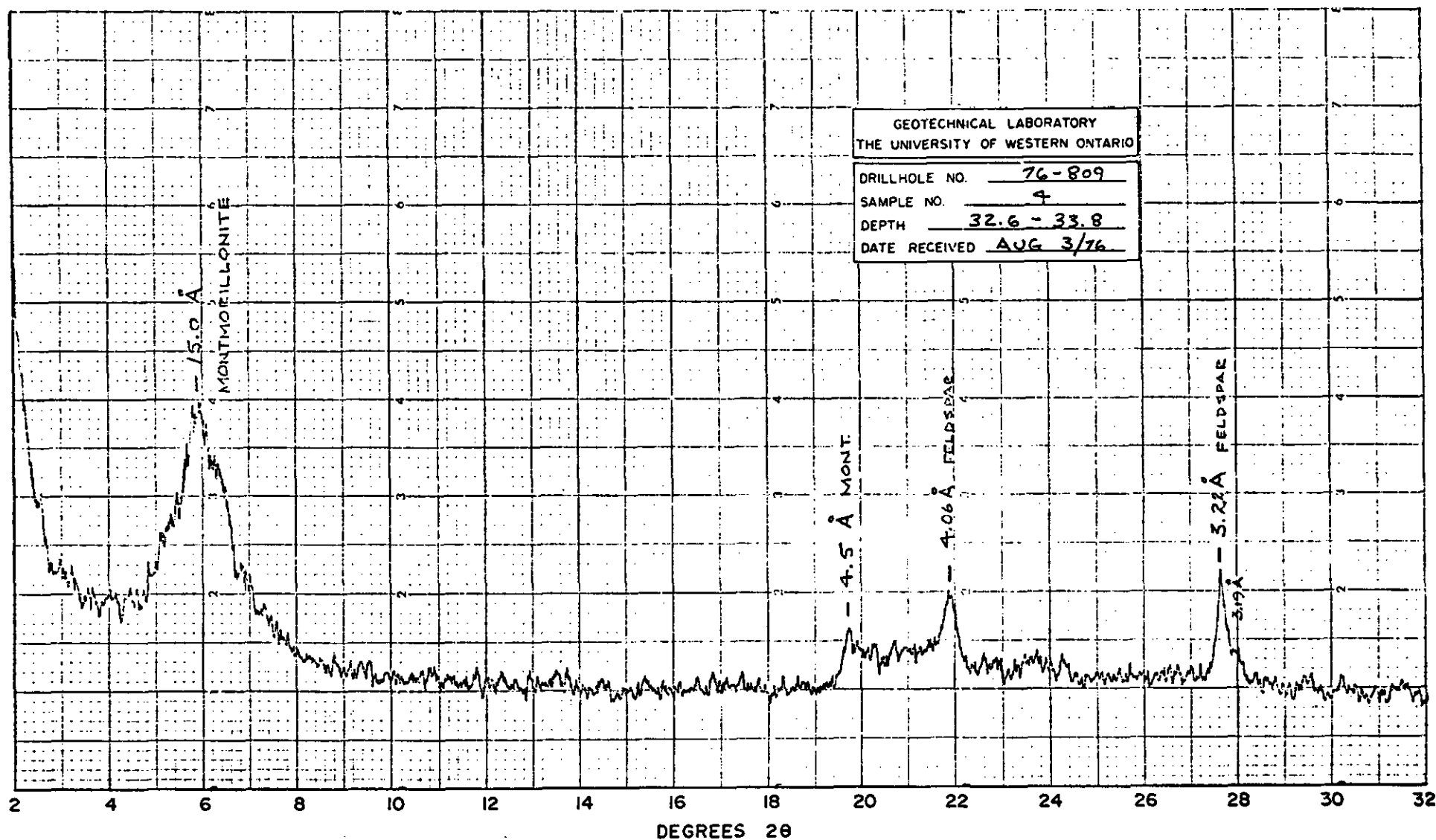
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



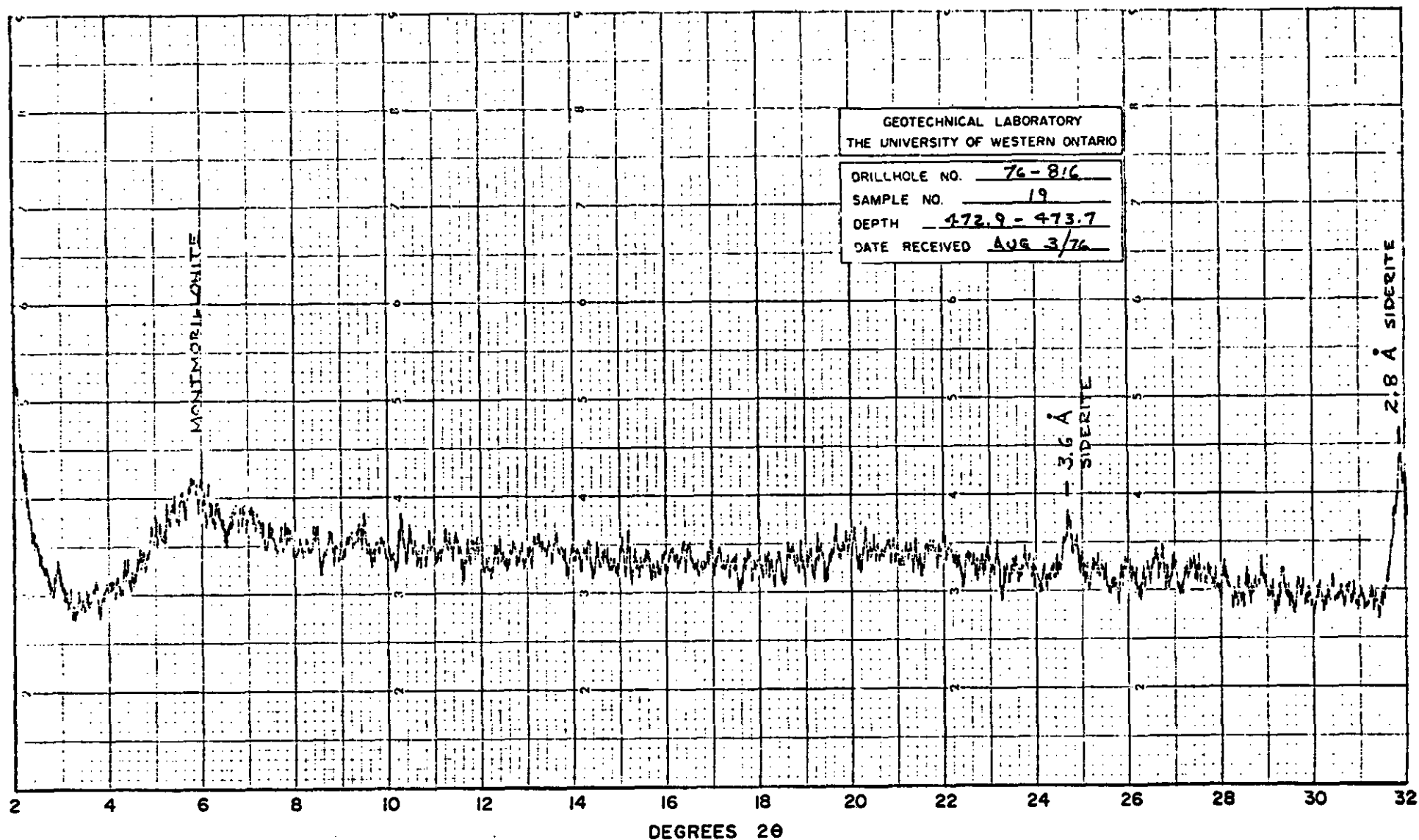
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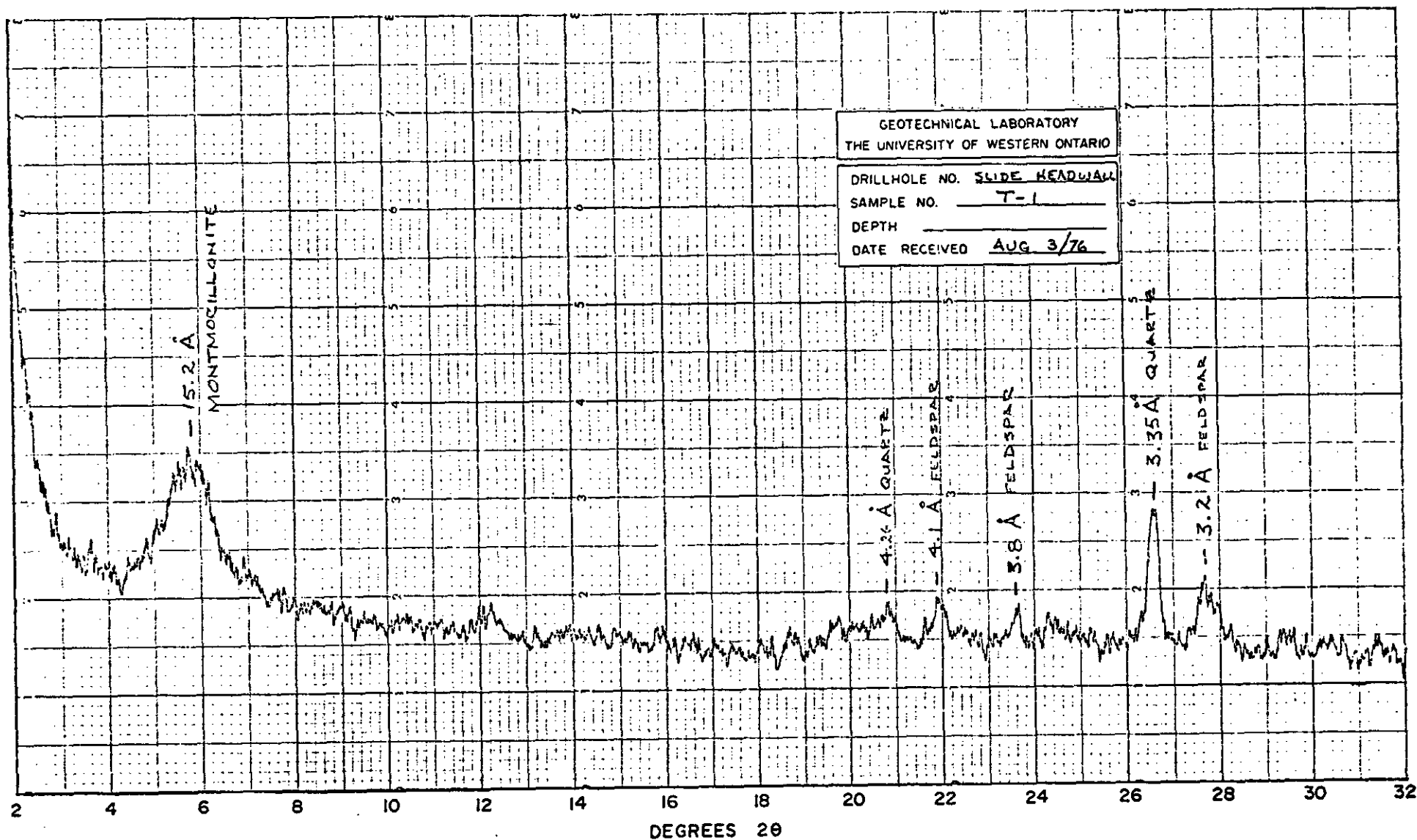
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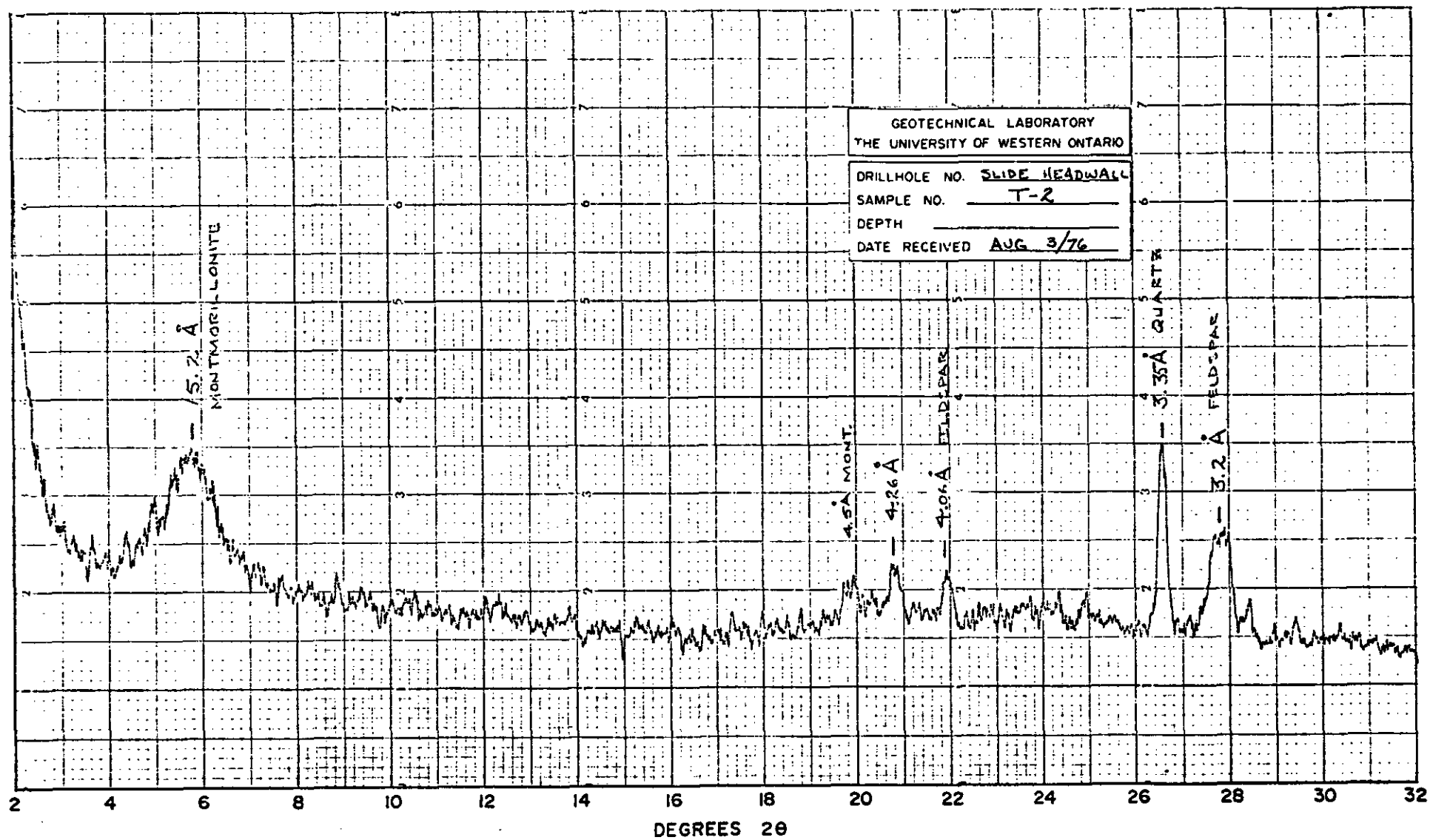
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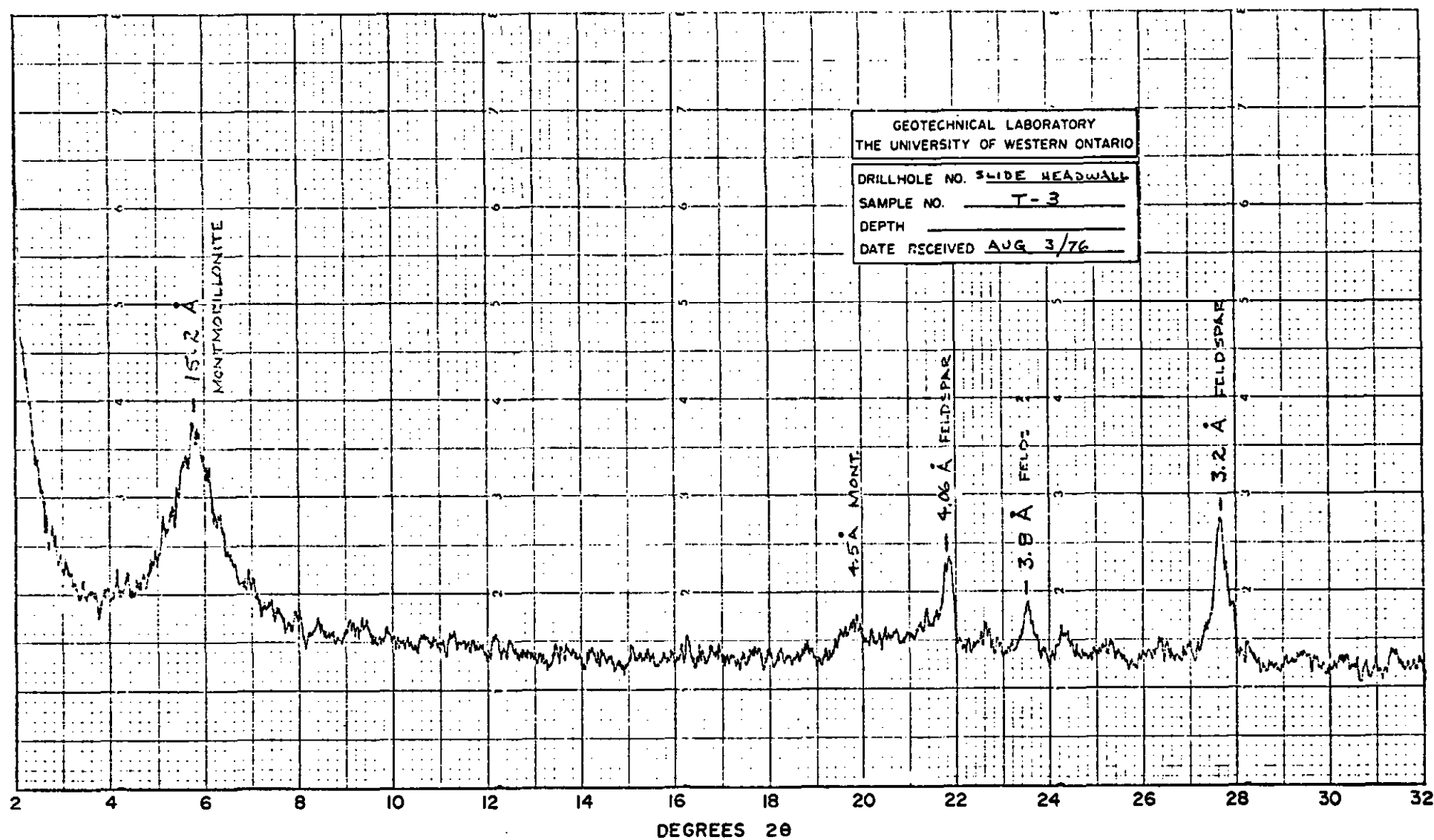
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.

FEB 15 1977



FILE No
The University of Western Ontario, London, Canada

Faculty of Engineering Science
London, Canada
N6A 5B9

8 October 1976

Mr. G. Rawlings
Golder, Brawner & Associates Ltd.
224 West 8th Avenue
Vancouver, British Columbia
V5Y 1N5

Dear Mr. Rawlings:

Report #5 - Hat Creek Project - Mineralogical Analyses
October 8, 1976

Enclosed are the x-ray and carbonate analyses on the ten samples received on September 22, 1976. These samples were generally fairly soft and waxy or soapy looking, indicating abundant contained montmorillonite.

Specific Comments on the Samples

1. Carbonate is significant only in sample 74-27-1 from 569.5 feet depth, which contained about 60.4% siderite by Chittick analysis and yielded a large 2.80 Å peak on the x-ray powder pattern.
2. The rest of the powder patterns are characterized by large (001) montmorillonite peaks and moderate to minor amounts of feldspar and quartz.
3. The x-ray traces of the oriented minus 2 µm fractions indicate montmorillonite with a degree of non-regular basal spacing not noted in previous samples. This is particularly true of the wet preferred orientation traces which show only a high background above 19.6 Å. It is probable that this represents a greater degree of hydration by water and interlayer swelling than was observed for the previous samples.

Since we have not yet received cross sections of the site upon which to base our selection of samples for the glycol retention analyses, we will defer these until after our discussions in Vancouver.

Yours sincerely,

R.M. Quigley, P.Eng.
Professor of Geotechnical Engineering

RMQ:em

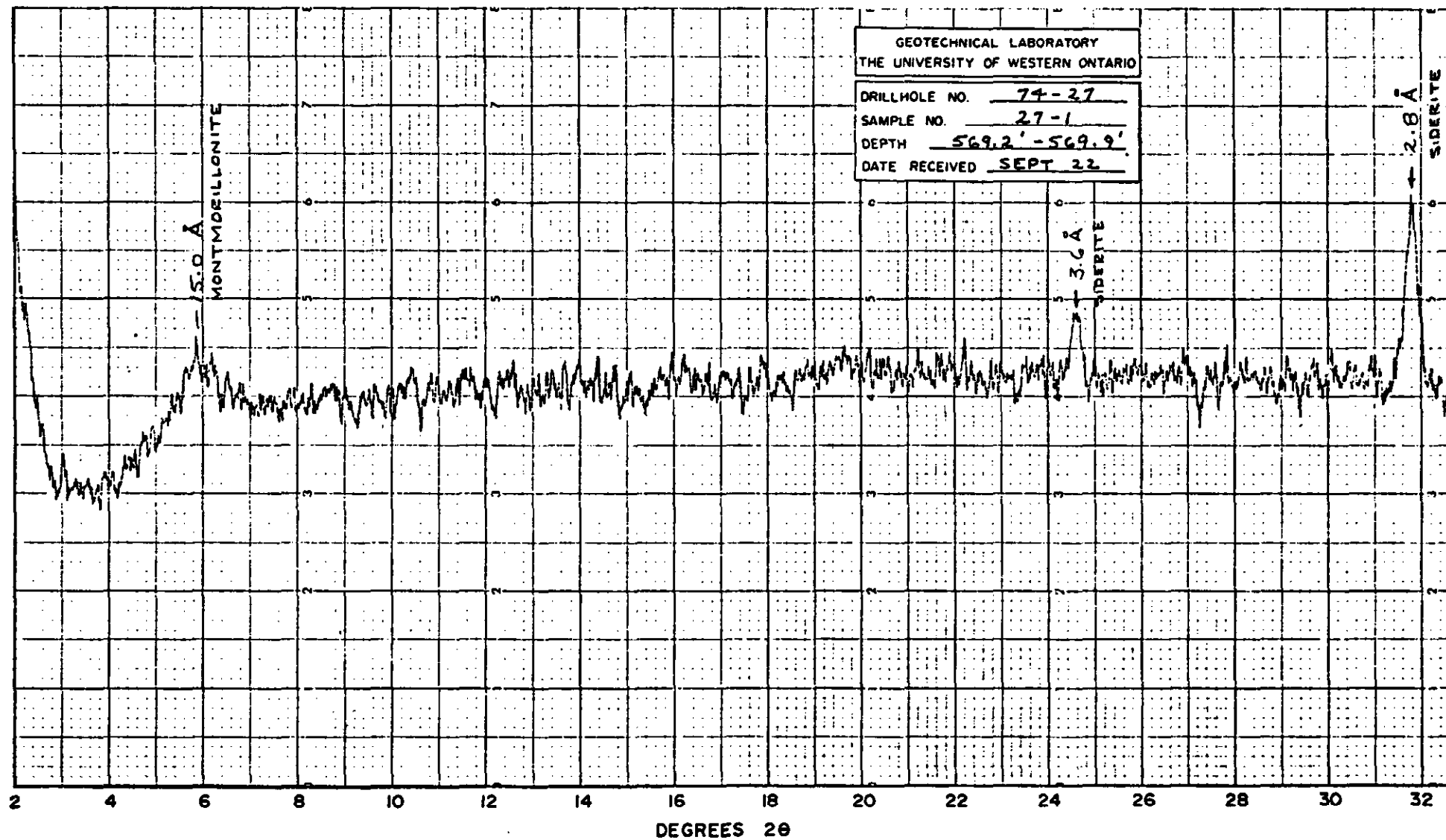
cc: Mr. H.H. Hawson
Kamloops, B.C.

LIST OF SAMPLES RECEIVED FROM GOLDER BRAWNER & ASSOCIATES

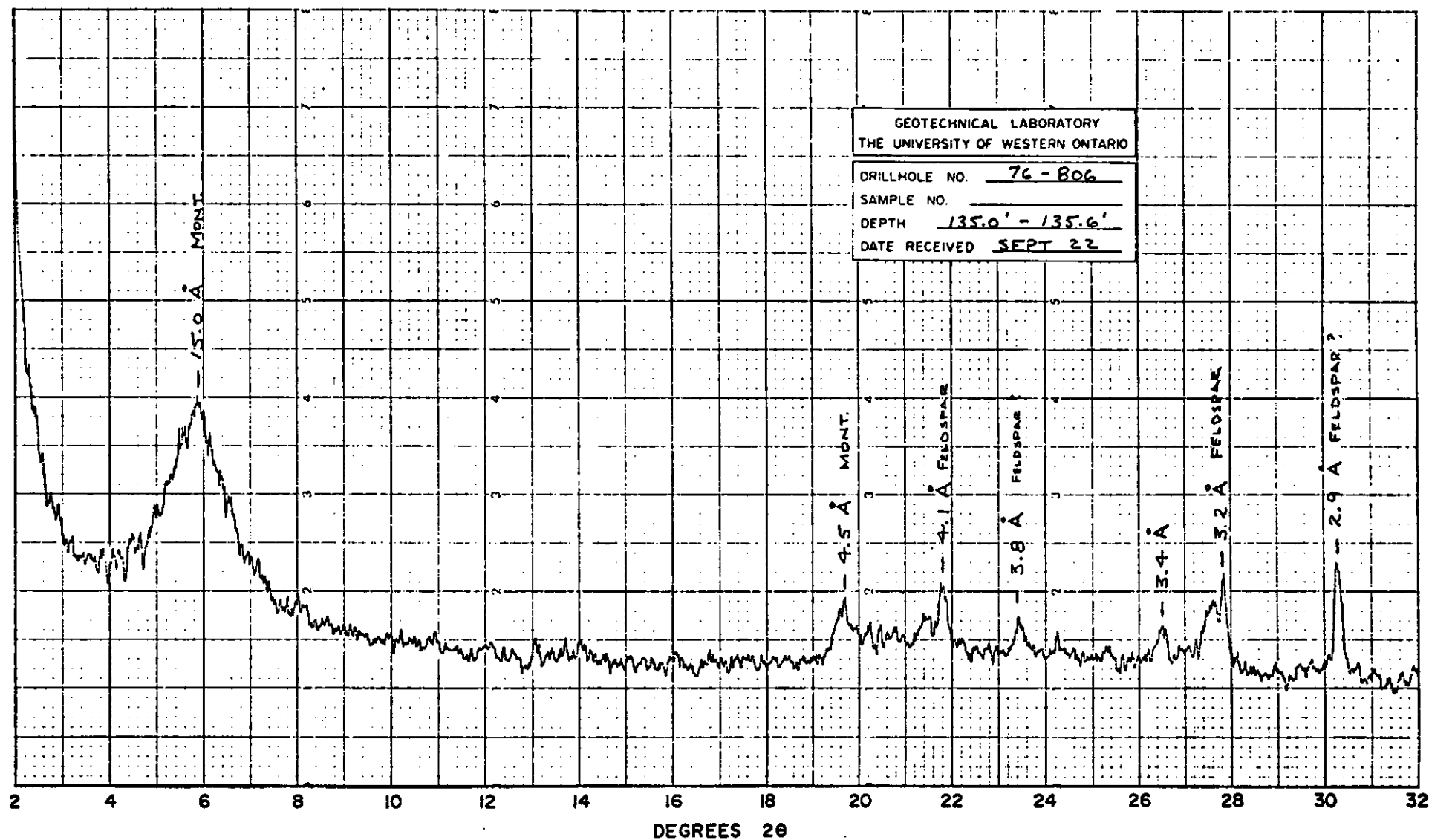
GEOTECHNICAL LABORATORY
THE UNIVERSITY OF WESTERN ONTARIO

Drill Hole No.	Sample No.	Depth (Feet)	Date Received	Testing Completed						
				X-ray				Carbonate (%)	Glycol Retention (mg/g)	Na ⁺ (PPM)
				Wet P.O.	ADPO	GPO	Powder			
74-27	27-1	569.2-569.9	SEPT 22	✓	✓	✓	✓	60.4		
76-806	-	135.0-135.6	SEPT 22	✓	✓	✓	✓	2.5		
76-806	-	325.0-325.5	SEPT 22	✓	✓	✓	✓	2.1		
76-808	-	276.0-276.5	SEPT 22	✓	✓	✓	✓	2.7		
76-808	-	392.0-392.6	SEPT 22	✓	✓	✓	✓	1.5		
76-811	5	41.5-42.5	SEPT 22	✓	✓	✓	✓	1.3		
76-811	-	112.5-113.0	SEPT 22	✓	✓	✓	✓	4.5		
76-811	-	176.5-177.0	SEPT 22	✓	✓	✓	✓	2.5		
76-812	43	157.0	SEPT 22	✓	✓	✓	✓	2.2		
76-818	4	28.3-29.6	SEPT 22	✓	✓	✓	✓	2.4		

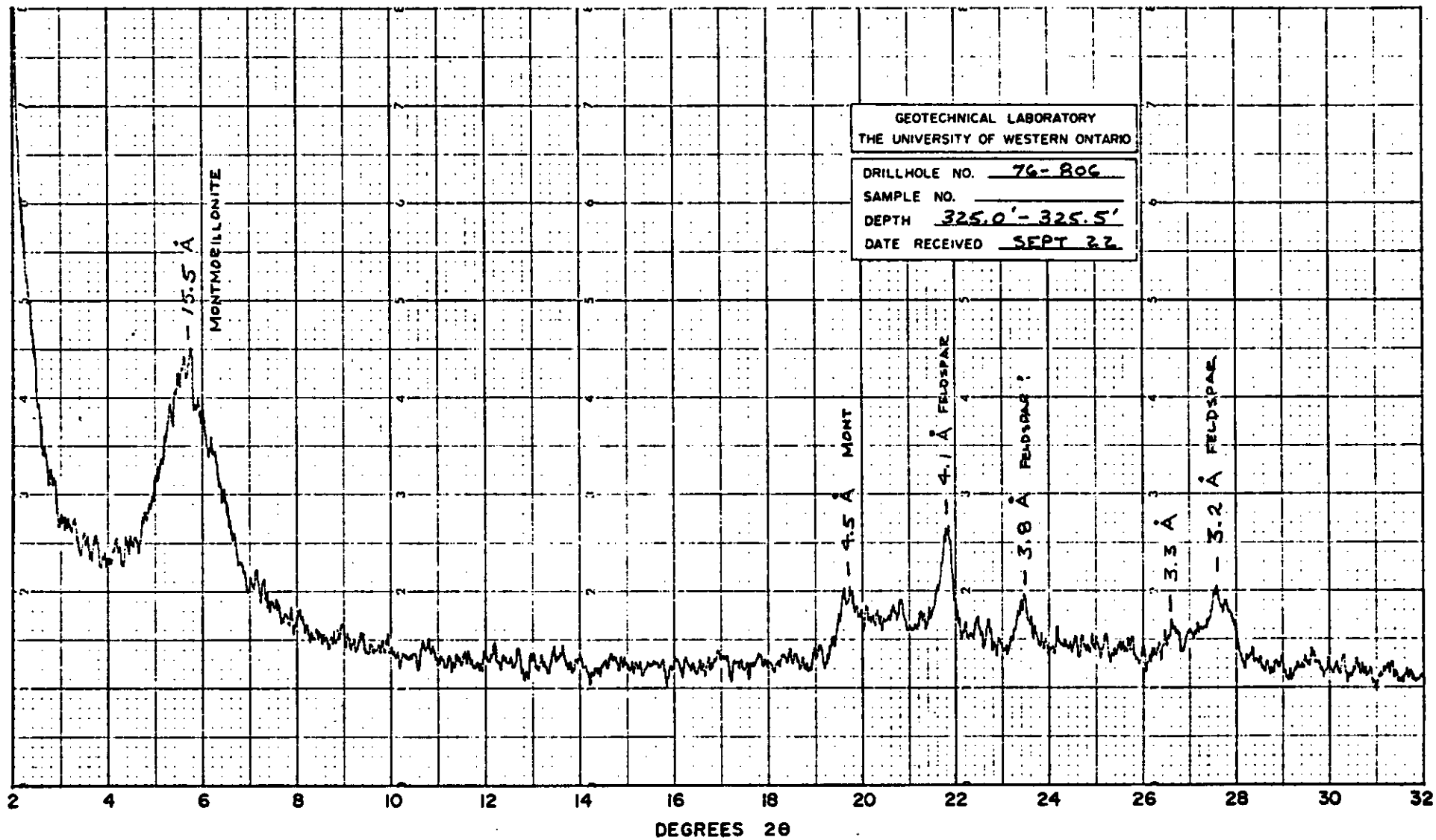
REPORT #5
K.M. Quigley
 OCT. 8/76



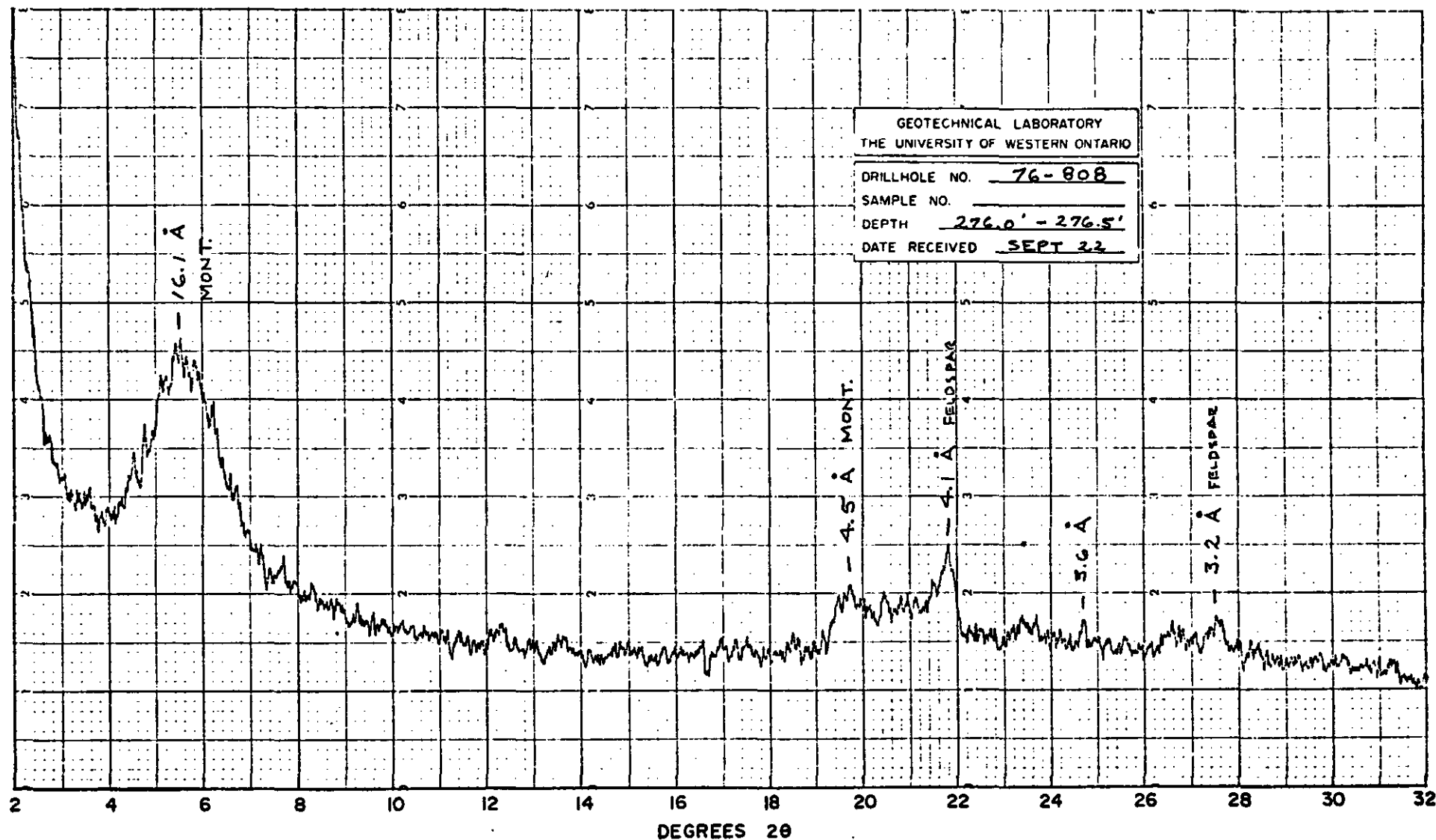
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



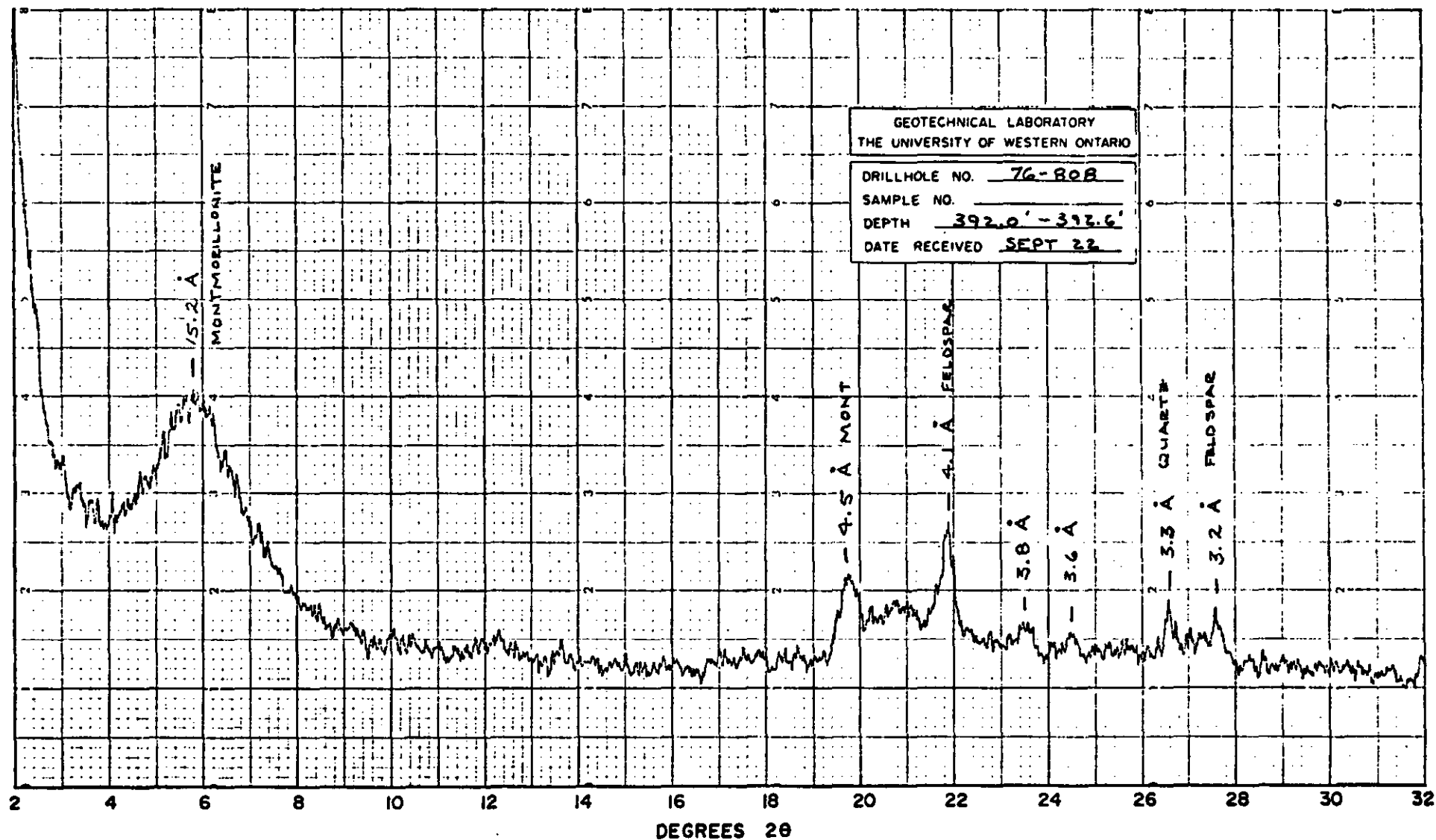
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



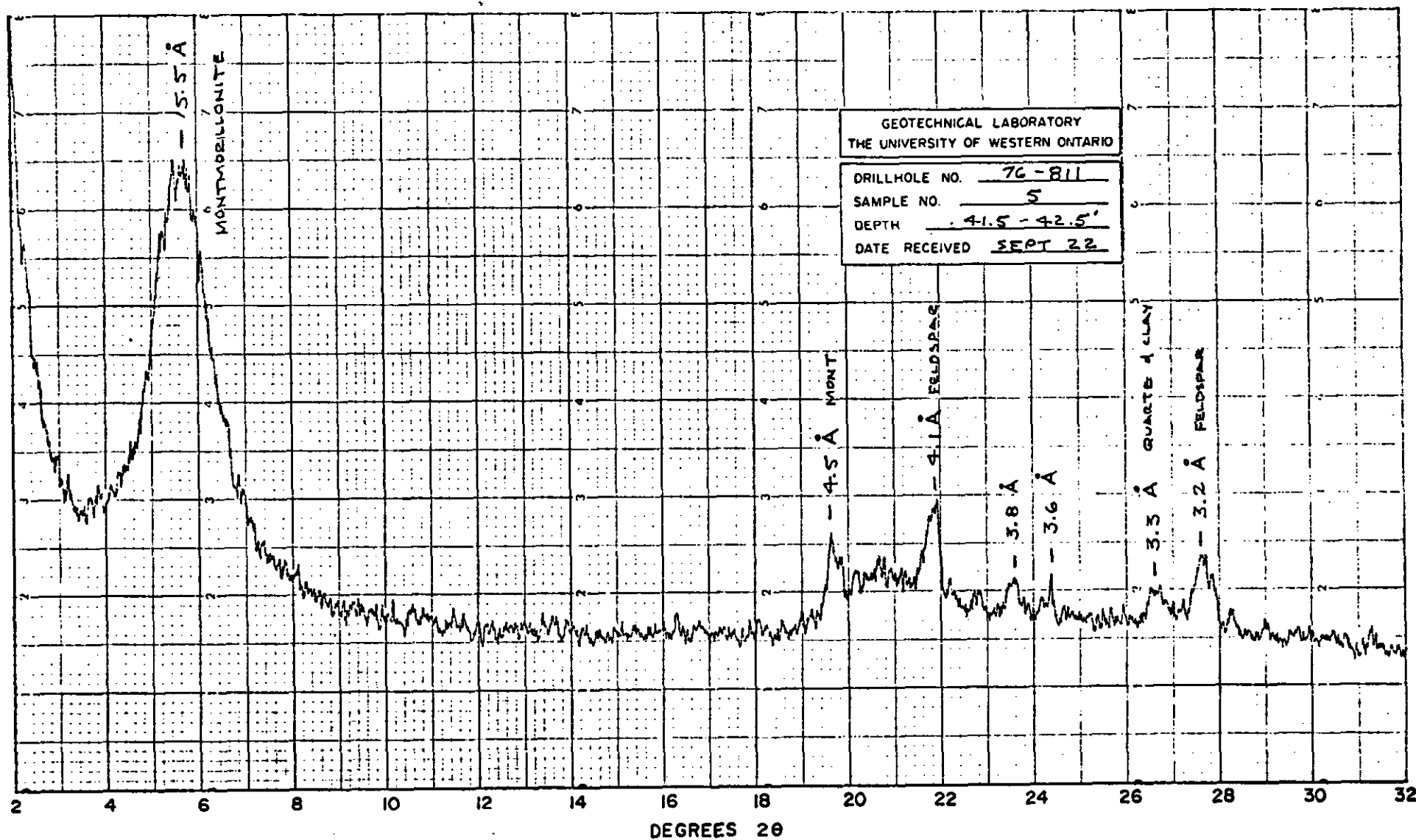
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



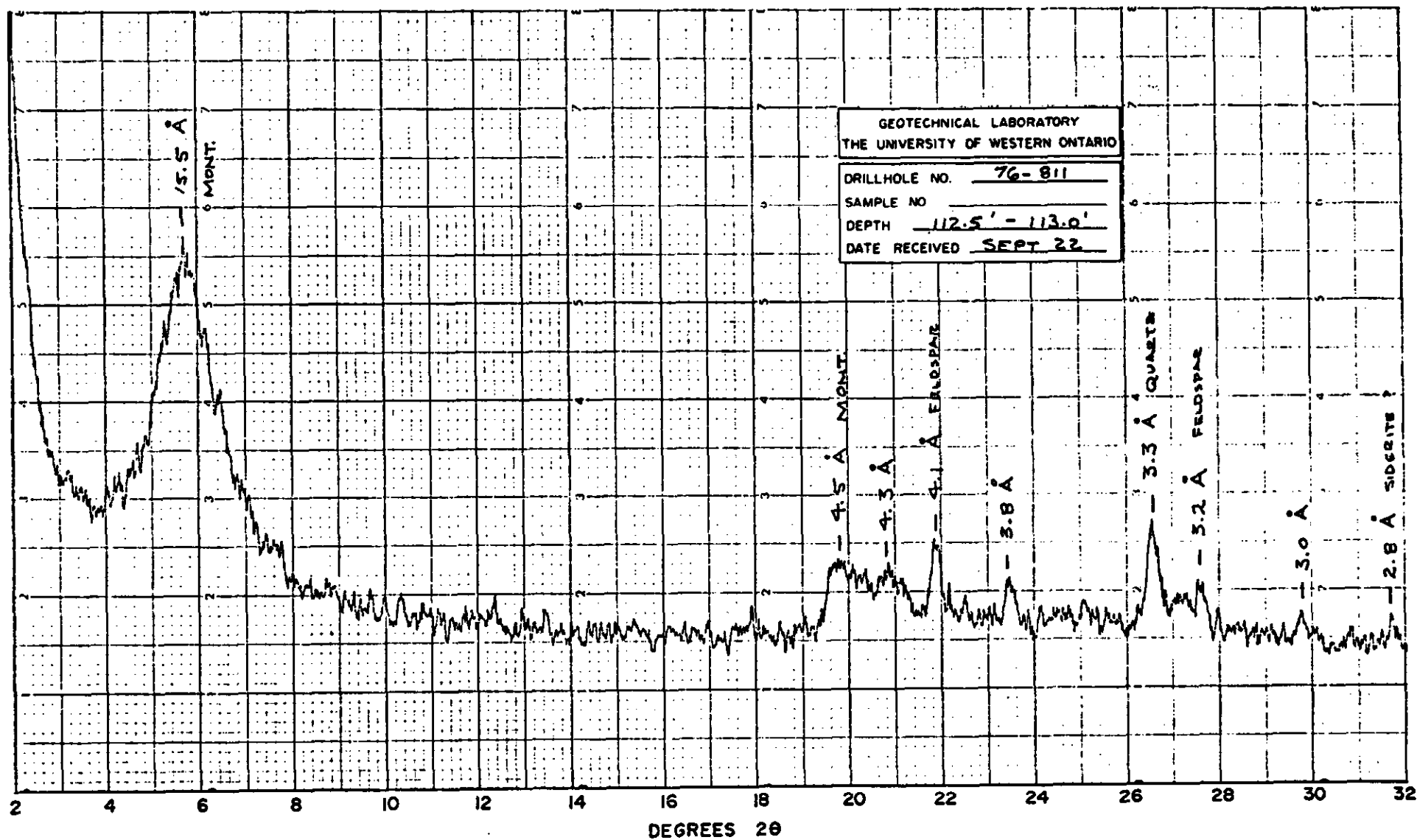
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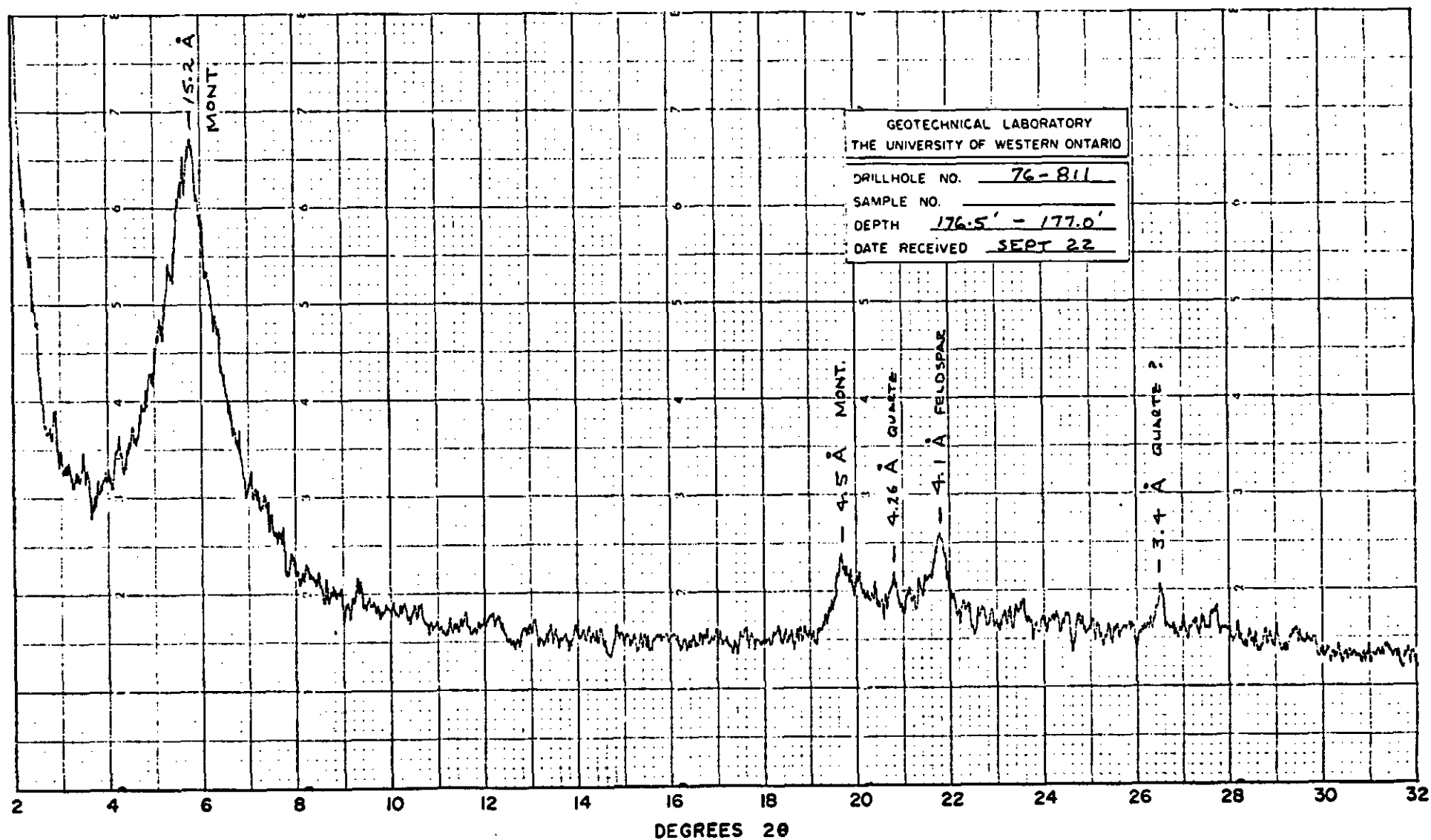
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



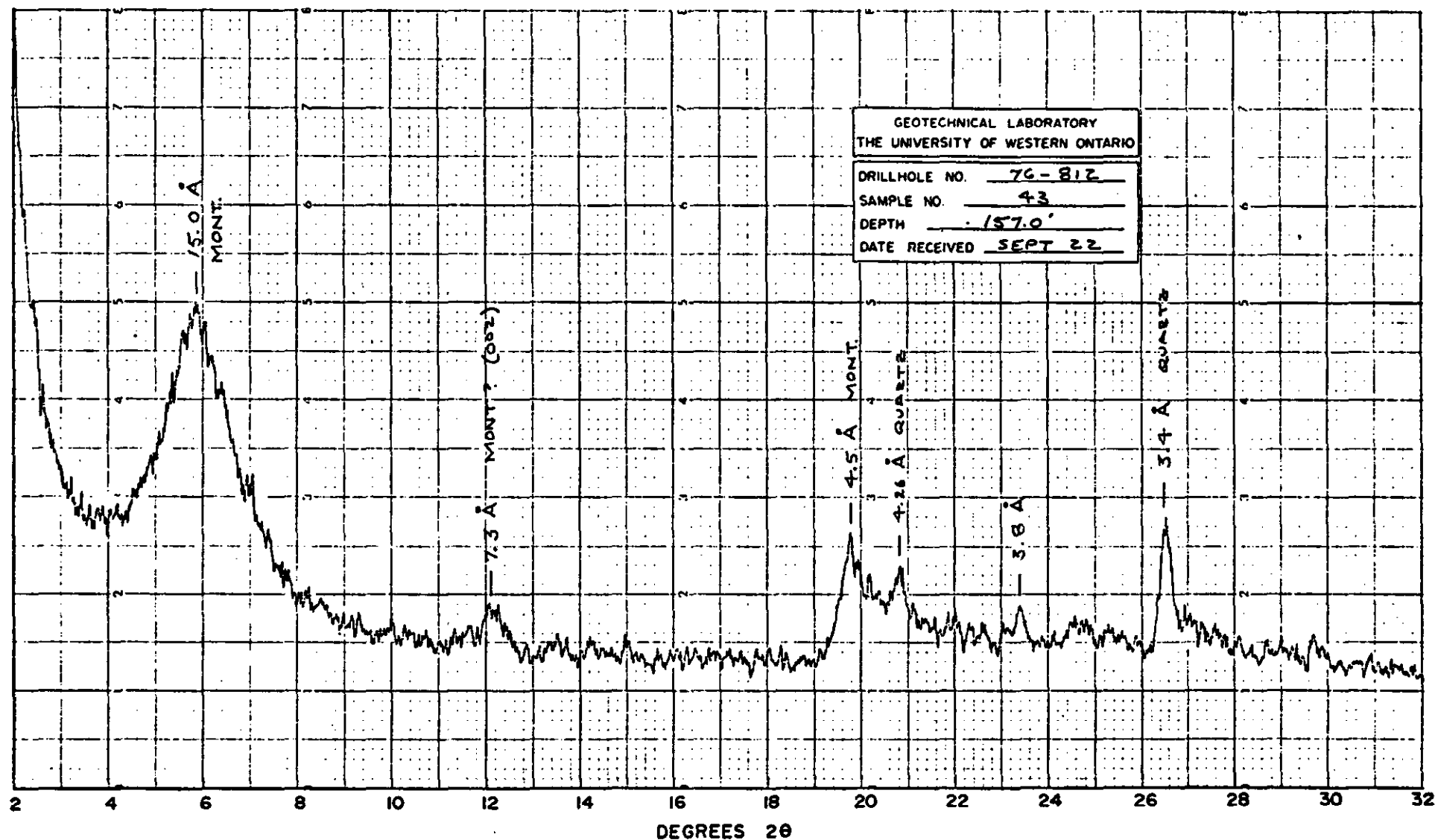
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



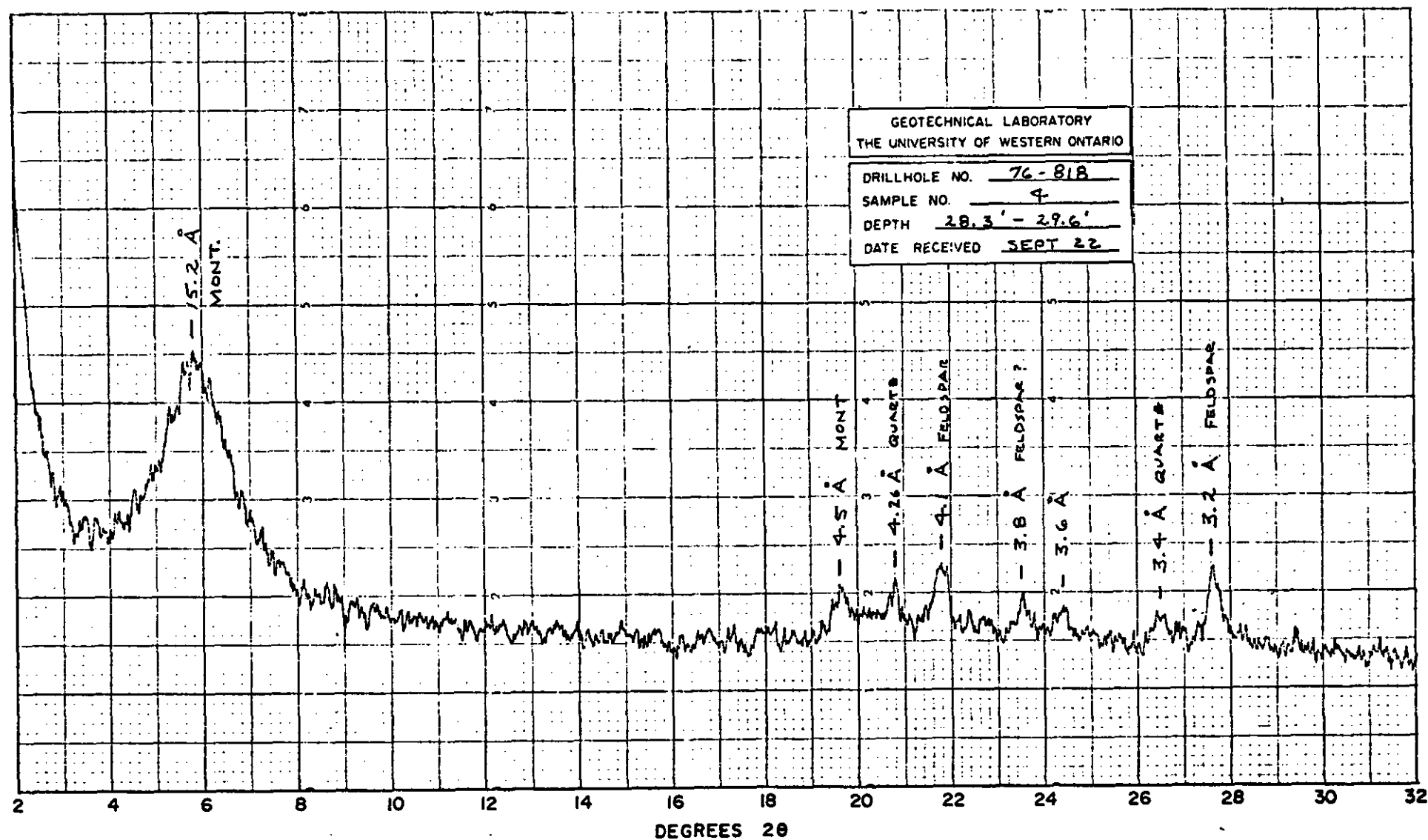
X-RAY DIFFRACTION TRACES OF WHOLE SOIL POWDERS FROM HAT CREEK.



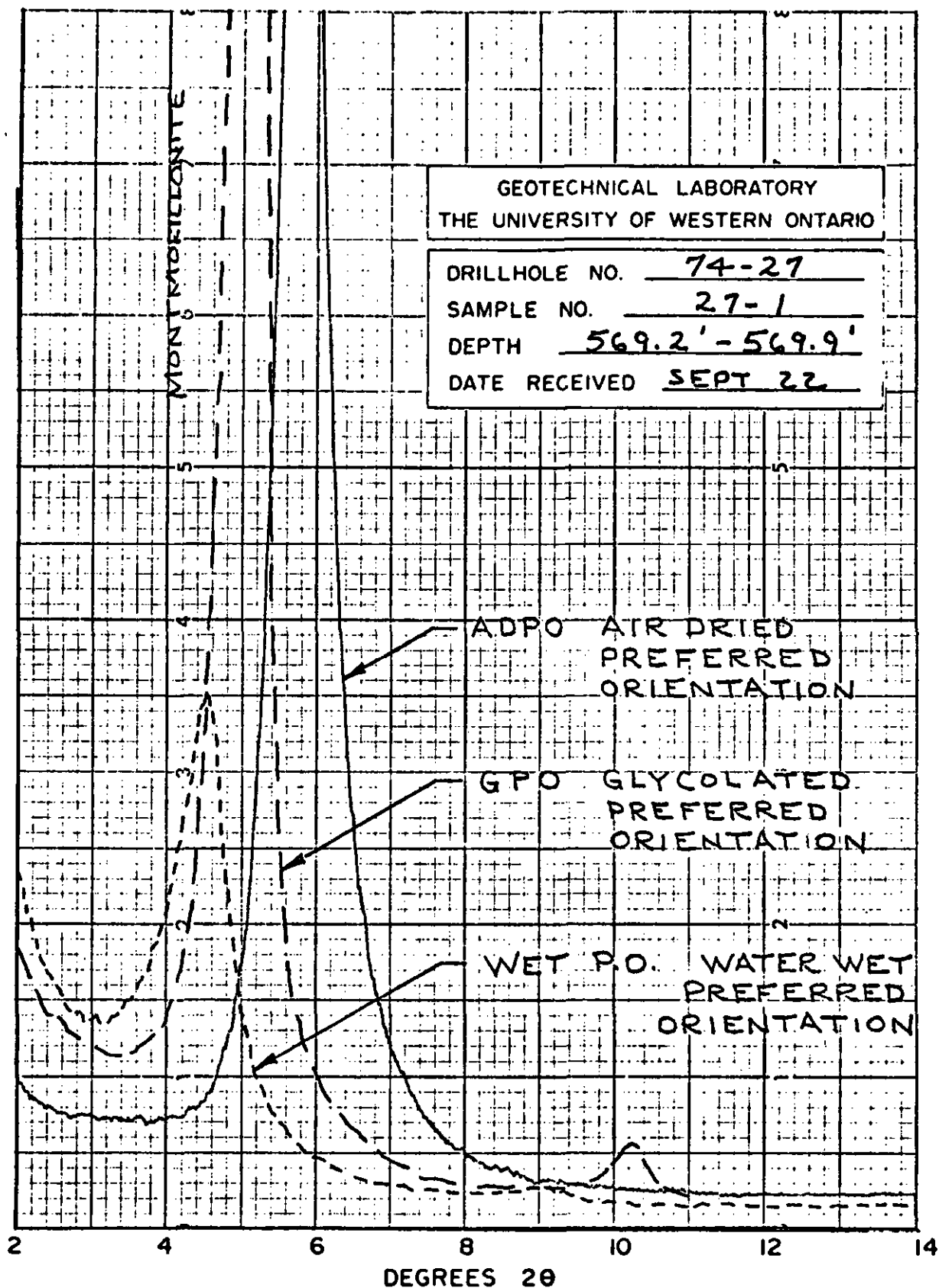
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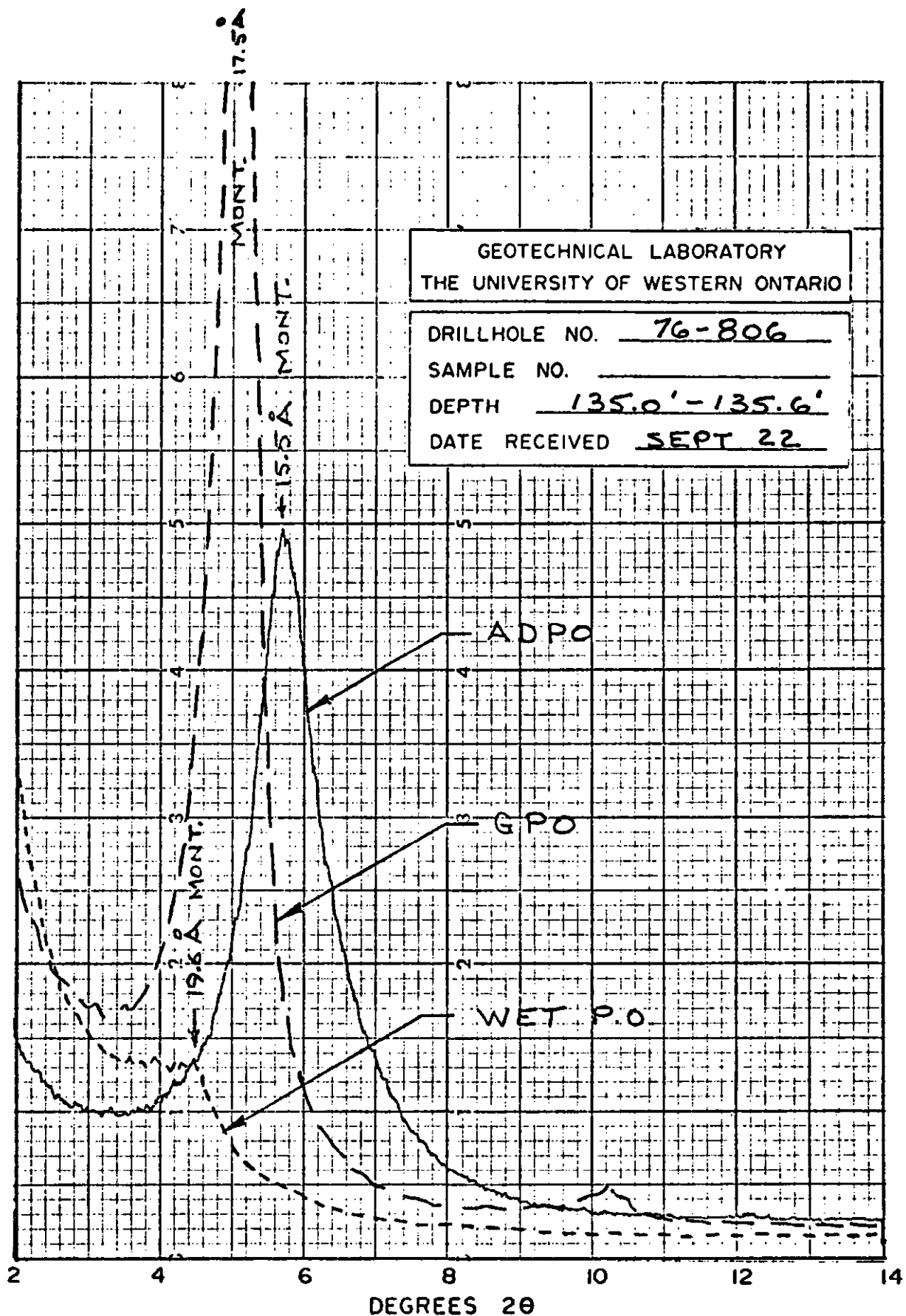
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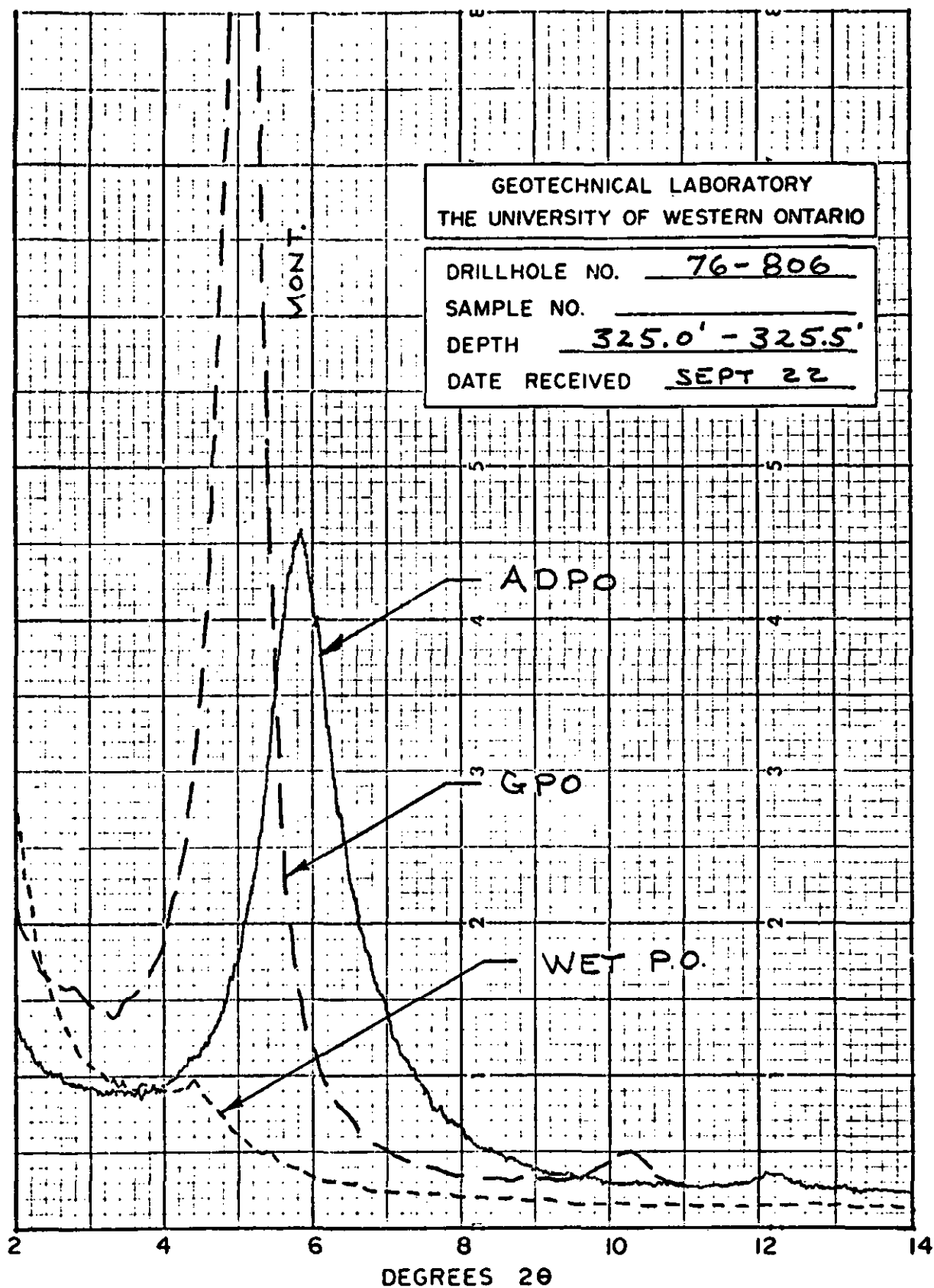
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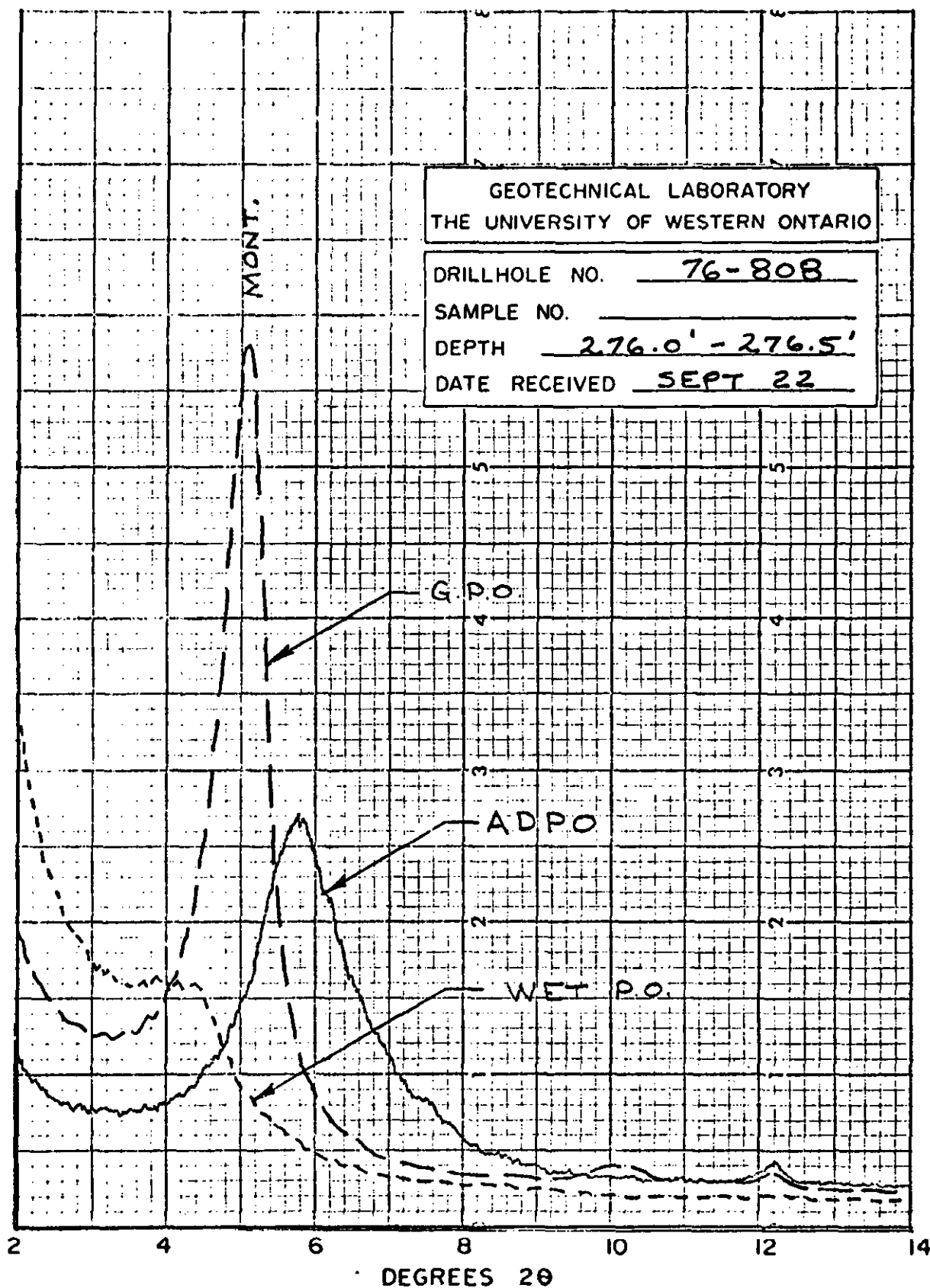
X-RAY DIFFRACTION TRACES OF 2μ , PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



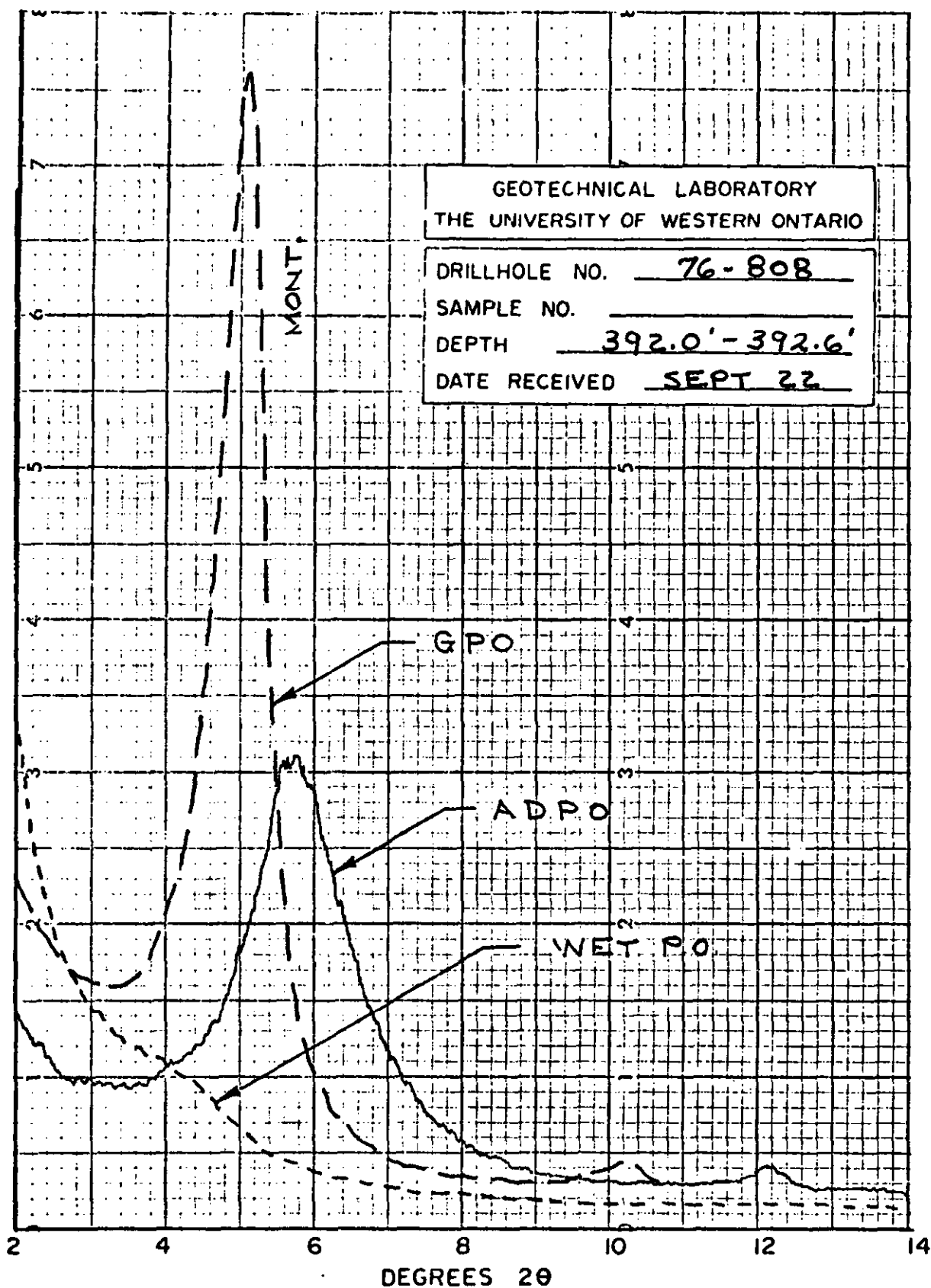
X-RAY DIFFRACTION TRACES OF 2μ , PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.



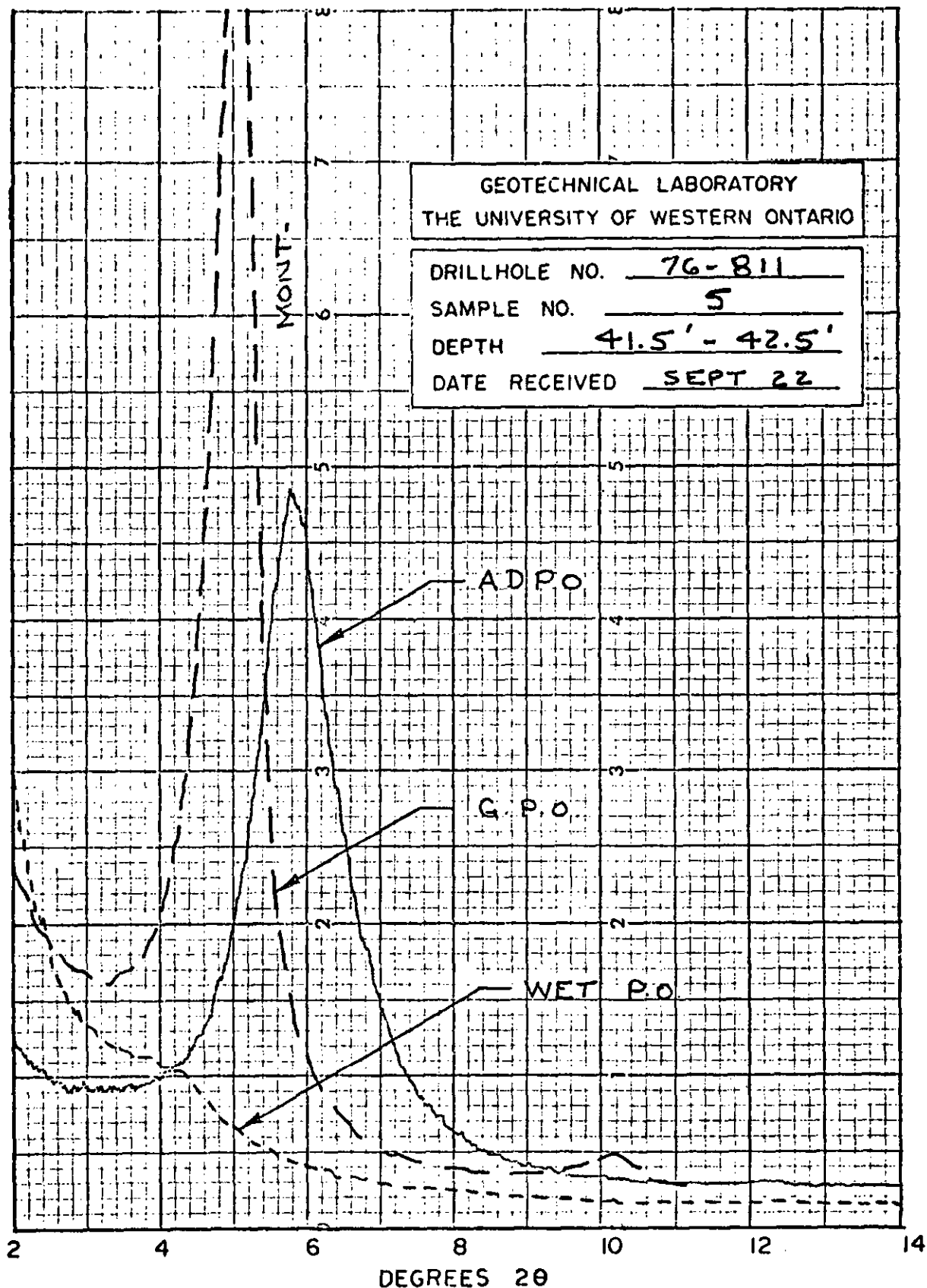
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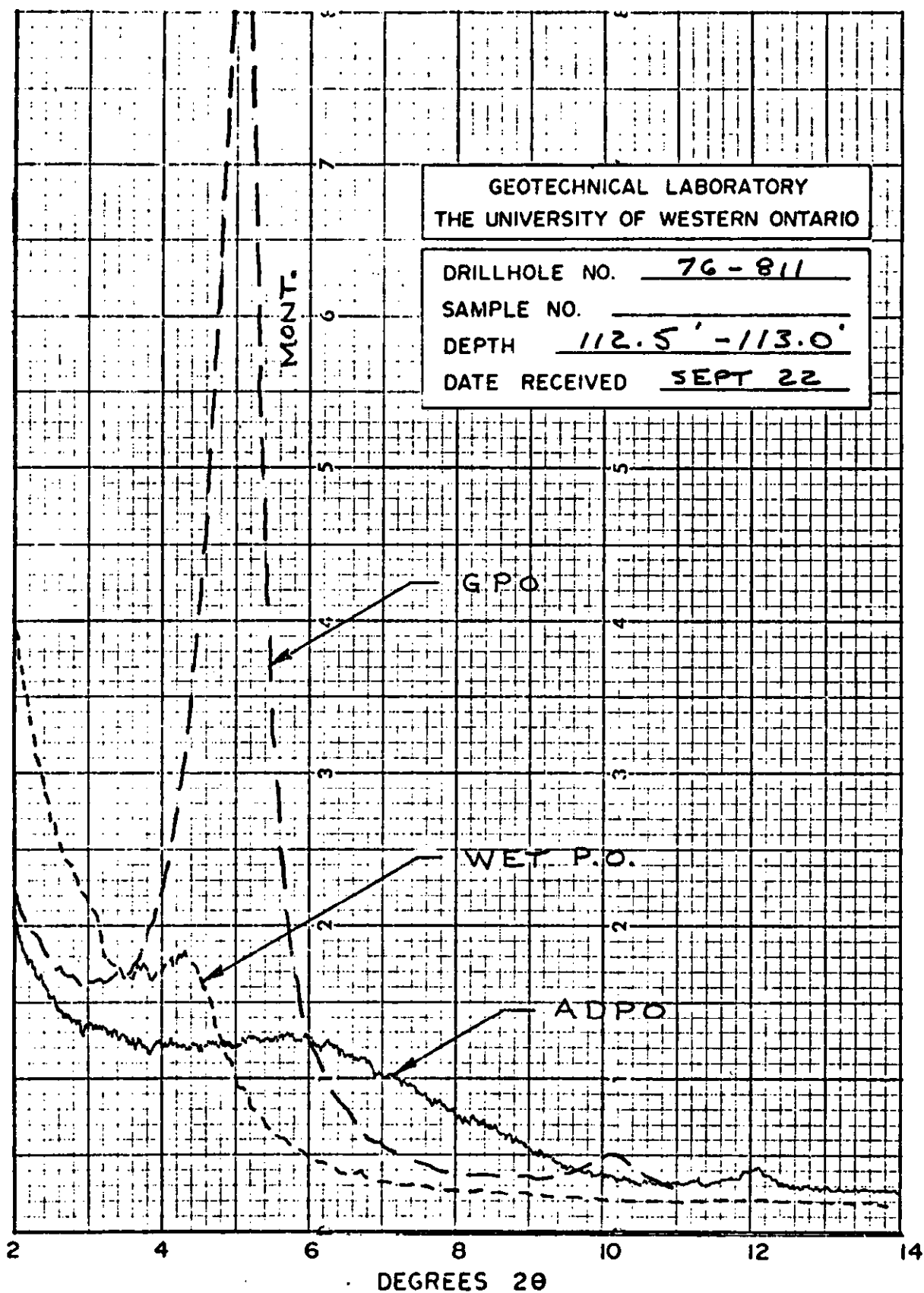
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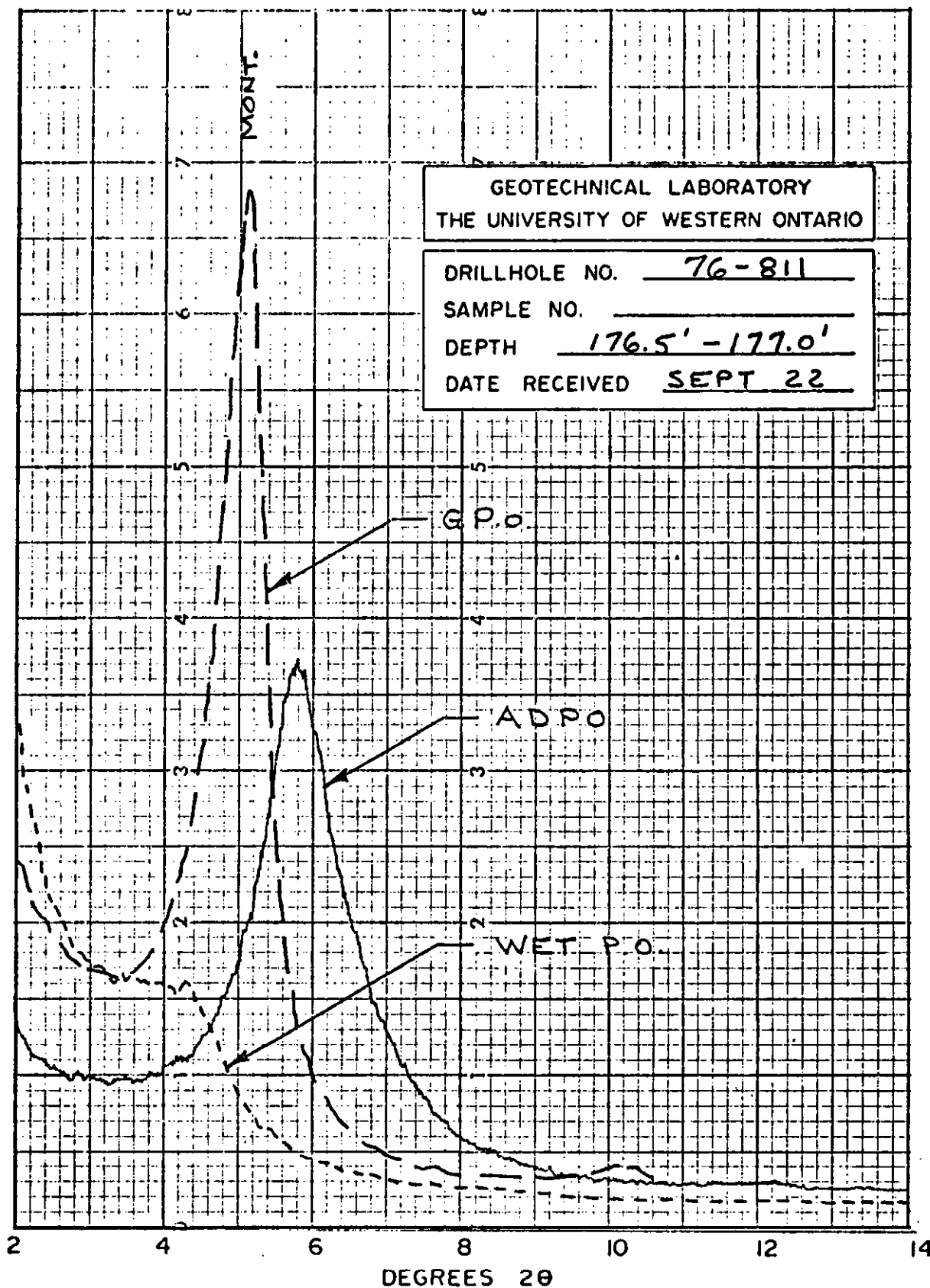
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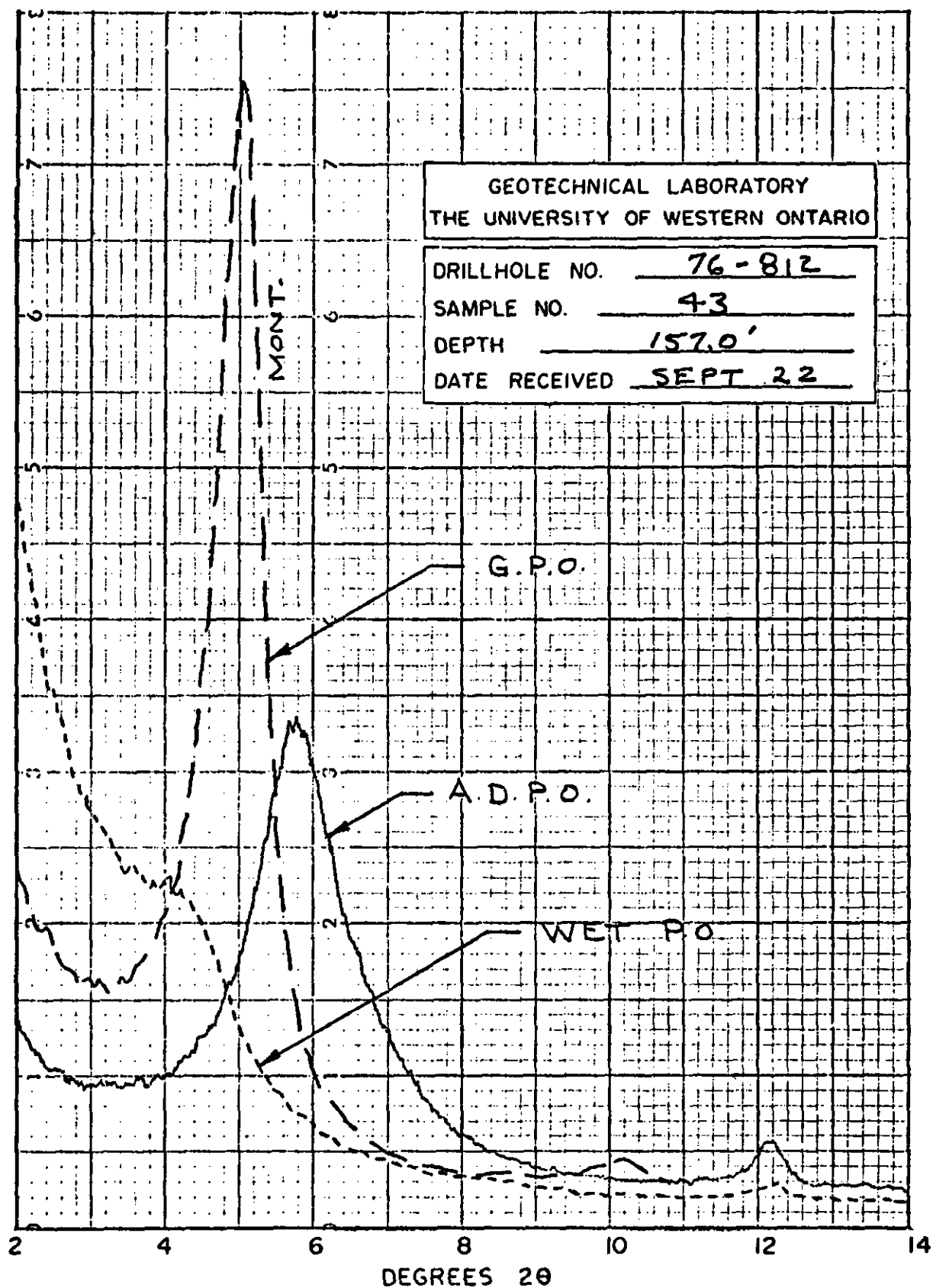
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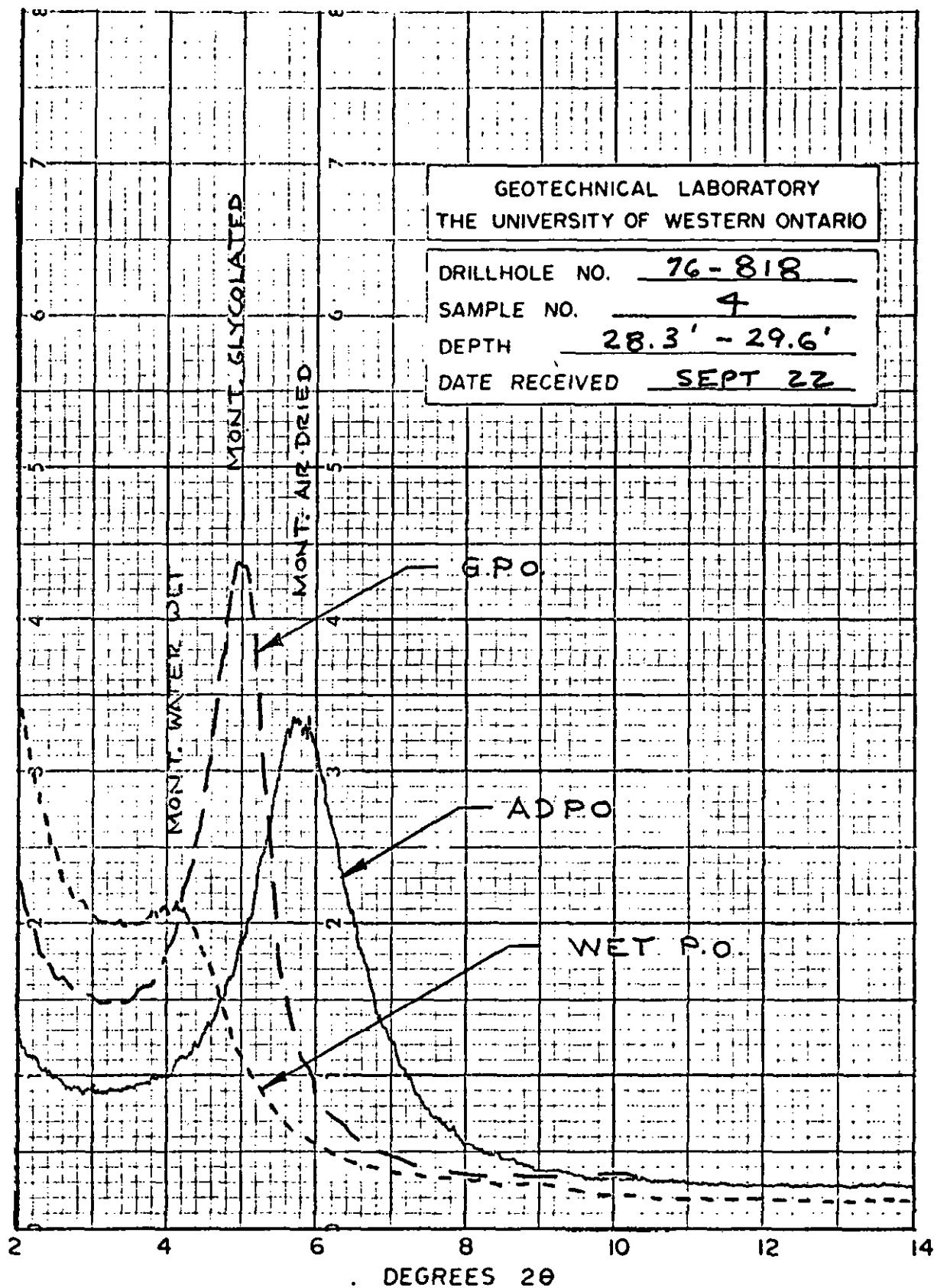
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X-RAY DIFFRACTION TRACES OF 2μ , PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.

REPORT

to

GOLDER BRAWNER & ASSOCIATES LTD.
VANCOUVER, BRITISH COLUMBIA

on

PRELIMINARY MINERALOGICAL
AND
PHYSICO-CHEMICAL ANALYSES
HAT CREEK PROJECT, BRITISH COLUMBIA

Robert M. Quigley

Faculty of Engineering Science
The University of Western Ontario
London, Ontario, Canada

November 26, 1976

TABLE OF CONTENTS

	Page
INTRODUCTION	1
PURPOSE AND SCOPE	1
X-RAY DIFFRACTION SUMMARY	2
Powder Patterns	2
X-Ray Diffraction Traces of Oriented < 2 μ m Fraction	3
CHEMICAL TESTS	4
Carbonate Analyses	4
Glycol Retentions	5
Salinity and Cation Analyses	5
Chloride Anion Measurements	7
pH Measurements	7
DISCUSSION	7
Tables I, II and III	
Figures 1 to 8	

PRELIMINARY MINERALOGICAL AND PHYSICO-CHEMICAL
ANALYSES, HAT CREEK PROJECT, B.C.

INTRODUCTION

This report presents a final summary of the results of mineralogical and chemical analyses carried out on 43 samples received from Golder Brawner Associates between June 24 and September 22, 1976.

X-ray powder patterns for whole soil samples, x-ray traces for oriented samples of $< 2 \mu\text{m}$ fractions, and carbonate analyses on all samples were presented in a series of five letter reports between July 26 and October 8, 1976. Only a brief summary of these results is contained in this report.

Recent glycol retention analyses and pore fluid chemistry studies run as a final phase of the project are detailed herein.

PURPOSE AND SCOPE

The purpose of the present study has been to define the clay mineralogy of the sedimentary strata above, below and at the flanks of the coal measures at the Hat Creek Project, B.C. Of special interest were; 1) the relationship of the

clay mineralogy to the probable engineering behaviour, and
2) the possible presence of a marker horizon.

A total of 43 samples were received from Golder Brawner & Associates Ltd. from a variety of locations defined stratigraphically on drawing V76345-3 (Golder Assoc.).

The scope of the testing has been limited to preliminary identification of the soil and rock components by x-ray diffraction and carbonate analyses. This has been supplemented by selected glycol retention analyses on 16 samples; 8 above the coal measures and 8 below. Salinity and cation analyses have been run on 8 samples; 4 above the coal measures and 4 below.

On the basis of the glycol retentions, a rough estimate can be made of the amount of montmorillonite present.

X-RAY DIFFRACTION SUMMARY

Powder Patterns

All powdered samples except those with more than about 35% carbonate yielded strong to very strong 15.2 Å montmorillonite peaks as shown in Figures 1 to 4 which contain typical powder patterns. The carbonate present appears to be an iron rich variety similar to siderite as identified on the x-ray traces. Other constituents in the samples included moderate to trace amounts of feldspar and quartz with an occasional suggestion of cristobalite.

Summaries of the soil constituents present in each sample as observed by x-ray powder diffraction are given in Tables I and II. For clarity, the carbonate contents by gasometric analysis are also given.

From an engineering point of view, the powder patterns clearly show montmorillonite to be the dominant mineral present in all samples except the indurated carbonates. Even in these samples, montmorillonite peaks were generally easily discernible on the powder patterns.

X-Ray Diffraction Traces of Oriented < 2 μ m Fraction

Typical x-ray diffraction traces of oriented specimens of the < 2 μ m fraction are given in Figures 5 to 8 inclusive. All traces are essentially similar showing strong 15.5 Å montmorillonite peaks in the air dried preferred orientation state and strong 17.0 Å peaks when glycolated. Some variation occurs in the traces for the water-wet samples, the intensity, breadth and position of the peaks varying from sample to sample. This reflects variable hydration of the clay mineral sheets and may be related in part to the quality of the distilled water used to disperse the samples as well as variable swelling characteristics of the clays.

From an engineering point of view, this tendency towards extra swell in distilled water suggests that the clays may exhibit unfavourable swelling and strength characteristics on exposure to leaching by fresh rain waters.

CHEMICAL TESTS

Chemical tests on the samples are summarized in Table III. The tests include carbonate analyses by Chittick gasometric methods, glycol retentions, pore fluid salinity and cation analyses.

Carbonate Analyses

Carbonate contents of the montmorillonite rich clays and clay-stones are generally of the order of 1 to 2%. Since the test procedure involves addition of HCl to a dried powdered sample, other gases than CO₂ from soil carbonates may occasionally be evolved. Test results of 1% carbonate, therefore, may reflect complete absence of carbonate in some of the samples.

The reaction time of the contained carbonates with HCl was delayed like dolomite, reflecting the lesser solubility of the siderite present in the rocks compared to calcite.

The x-ray traces clearly showed siderite to be the dominant carbonate. The presence of the siderite in the volcanic rich stratigraphic section would seem to reflect iron rich waters signifying volcanic activity synonymous with carbonate deposition.

Well indurated carbonate samples normally have siderite contents of about 30 to 35% with some samples containing as much as 68% carbonate. If the samples supplied to our

laboratory are fully representative of the stratigraphic section, it is very apparent from Table III that the carbonate strata seem restricted to the section above the coal measures.

Glycol Retentions

The sixteen values of glycol retention are presented in Table III. Below the coal measures, values ranging from 129 to 264 were obtained on the $< 2 \mu\text{m}$ fraction of six samples. The two high values of 243 and 264 mg/g are as high as is normally obtained on pure montmorillonite. Tests were run on two whole-soil samples (in brackets in Table III) and the results are very high (186 and 202 mg/g) indicating the great abundance of montmorillonite in the samples.

Above the coal measures, the glycol retentions varied from 136 to 265 mg/g on the $< 2 \mu\text{m}$ fractions. These values are comparable in spread to those obtained on the samples from below the coal measures.

Again, the four values above 200 mg/g are indicative of a clay fraction consisting of pure montmorillonite.

Salinity and Cation Analyses

Sample preparation for pore fluid analysis involved a single addition of distilled water to air dried soil in the ratio of 5:1 by weight. The salinities were measured by conductivity meter and are referred to NaCl standard. All

values were calculated assuming an in situ moisture content of 35% which is close to the actual average value.

Extreme difficulty was experienced in obtaining a clear liquid since the montmorillonite tended to form a very stable gel, even in dilute suspension. Eventually, all samples were split into small fractions and successfully clarified by high speed centrifugation.

The pore fluid cation analyses were run on the clear, slightly brown supernatant using a Pye Unicam atomic absorption spectrophotometer. The results only represent a guide to the pore fluid composition, since pore fluid extraction by high pressure squeezing would be required to obtain more precise values. The values of the salinity and cation measurements are presented in Table III.

The salinity values on the clay-stones tested are close to 4 g/l except for sample 74-28-1 (480 ft) which has a somewhat higher value of 6.5 g/l. The lowest salinity value of 1.9 g/l was obtained on sample 803-28 (135 ft) which is understood to be a glacio-lacustrine sediment. The lower salinity is, therefore, not surprising.

The cation analyses showed Na^+ (sodium) to be the dominant constituent of the pore fluid with values ranging from 1.15 to 2.13 g/l for the montmorillonite clay-stones. Magnesium was the next most abundant cation, ranging from 0.03 to 0.78 g/l. Iron was present in three brown coloured liquid extracts in amounts of 0.12 to 0.74 g/l and absent in

the rest of the extracts. Calcium was a negligible component of the pore fluids as extracted by the distilled water wash.

Chloride Anion Measurements

Chloride anion measurements were carried out on four selected extracts and yielded concentrations varying from 0.03 to 1.93 g/l as shown in Table III. Although the data is slim, it is speculated that high sodium values correlate with high chlorinity values in the Hat Creek deposits.

pH Measurements

The soil samples prepared for salinity analyses were also checked for pH yielding the results in Table III. The measured values range from 8.6 to 9.3 indicating a significantly alkaline environment.

DISCUSSION

The x-ray powder diffraction and carbonate data indicate that the geologic materials within the stratigraphic sequence at Hat Creek consist of:

- 1) Essentially pure montmorillonite with trace amounts of quartz and feldspar
- 2) Montmorillonite with moderate amounts of quartz and feldspar

- 3) Montmorillonite with moderate amounts of siderite
- 4) Carbonates (siderite) with moderate amounts of montmorillonite.

It appears significant that in Table I, all of the siderite rich samples occur above the coal measures.

The x-ray traces for the oriented specimens feature very strong (001) montmorillonite peaks with little or no evidence of either 10 Å illite or 7 Å kaolinite and chlorite. The very high glycol retentions of 129 to 264 reflect the abundance of montmorillonite within all < 2 µm fractions tested, including the indurated carbonates.

If pure montmorillonite is assigned its usual glycol retention of 250 mg/g, then the two whole soil samples tested (186 and 202 mg/g) contain montmorillonite contents of about 75 and 81% respectively.

The cations present in the pore fluid extracts consisted dominantly of sodium (1.2 to 2.1 g/l) with a somewhat lower value of 0.71 in the glacio-lacustrine sample 803-28 (135 ft). Magnesium was the next most abundant species with 0.03 to 0.06 g/l in the pore fluid above the coal measures and 0.14 to 0.78 g/l in the pore fluid of samples from below the coal measures. Calcium was essentially absent from the extracts, however, HCl treatment of a couple of samples suggested that some Ca^{++} may be adsorbed on the clays. Iron was detected in only the three most strongly coloured extracts.

Since magnesium (Mg^{++}) is a divalent cation it preferentially adsorbs onto the clay minerals in comparison to Na^+ , a univalent cation. Most of the cations adsorbed on the soil montmorillonites will, therefore, probably be Mg^{++} .

The total cation composition of the pore fluid extracts compares reasonably favourably with the measured salinity values. For example, the pore fluid extract from sample #74-28-1 (480 ft) has the following measured chemical constituents:

Sa #74-28-1 (480')

Salinity = 6.46 g/l

Sodium = 2.07 g/l

Magnesium = 0.03 g/l

Calcium = 0.04 g/l

Σ cations = 2.14 g/l

Chloride = 1.93 g/l

Σ cations + chloride = 4.07 g/l

Other anionic constituents such as bicarbonates and sulphates probably comprise the remainder of the soluble salts. Indeed, the very high pH values suggest the presence of soluble sulphates and it is recommended that some sulphate analyses be carried out during the next phase of the investigations.

Sodium rich montmorillonites have much higher liquid limits and activities than magnesium and calcium rich

montmorillonites. They also have correspondingly lower residual friction angles. The montmorillonites above the coal measures contain significantly less divalent cations and more Na^{++} cations in the pore fluid extracts, suggesting that they may be consistently more active and difficult to manage when exposed to atmospheric weathering than those below the coal measures.

Should strata be encountered that have significantly higher activities than the norm for surrounding strata, it is recommended that they receive special chemical testing to establish the pore fluid chemistry and adsorbed cation regime.

TABLE 1. COMPOSITION FROM X-RAY POWDER PATTERNS; BOREHOLE SAMPLES

A = Abund., Mo = Mod., Mi = Minor, T = Trace

SAMPLE			CARBONATE (Whole soil) (%)	CONSTITUENTS FROM X-RAY POWDER ANALYSES
Drill Hole	Number	Depth (ft)		
Above coal measures:				
803	28	135	1.7	Mont-A, Feldspar-A, Quartz-A
"	29	317	32.4	Mont-A, Siderite-A, Quartz-T
"	-	595	17.1	Mont-A, Felds-A, Siderite-A, Qtz-Mo (Fig.3)
815	7	431	34.5	Mont-A, Siderite-A, Felds-T
"	9	448	51.2	Mont-A, Siderite-A
"	12	482.5	3.5	Mont-A, Feldspar-Mi
"	14	506	7.5	Mont-A, Siderite-Mi, Qtz-T
"	18	542	34.3	Mont-?, Siderite-A, Qtz-T
"	20	562	9.3	Mont-A, Siderite-Mi, Qtz-Mi, Felds-Mi
"	22	583	67.6	Mont-?, Siderite-A, Qtz-T
"	29	669.5	35.5	Mont-?, Siderite-A, Qtz-T
816	19	473	30.7	Mont-?, Siderite-A, Qtz-T
74-27	1	569.5	60.4	Mont-?, Siderite-A
74-28	1	480	2.0	Mont-A, Felds-Mi, Qtz-Mi
"	2	644	6.4	Mont-A, Qtz-Mi, Siderite-Mi, Cristobalite?-Mi
"	3	738	7.5	Mont-A, Siderite-Mi, Qtz-T
"	4	763	31.6	Mont-A, Siderite-A, Qtz-Mi, Felds-Mi
"	5	767.5	26.5	Mont-A, Siderite-A, Qtz-Mo, Felds-Mi
"	6	179.5	44.3	Mont-?, Siderite-A, Qtz-T
"	7	451	12.9	Mont-A, Siderite-Mo
"	8	537	2.7	Mont-A, Felds-Mo, Qtz-Mi
"	9	588	1.5	Mont-A, Felds-Mi, Qtz-T
Below coal measures:				
804	1A	51	1.7	Mont-A, Felds-A, Qtz-Mi
805	16 Green Black	62	5.3 1.1	Mont-A, Felds-Mi, Qtz-Mi
806	7	18	1.3	Mont-A, Felds-Mo, Qtz-Mo
"	-	135	2.5	Mont-A, Felds-Mo, Qtz-Mi
"	-	325	2.1	Mont-A, Felds-Mo, Qtz-Mi
807	12	23	2.4	Mont-A, Felds-Mi, Qtz-Mi
"	14	159	1.7	Mont-A, Qtz-Mo
808	40	12	3.0	Mont-A, Felds-Mo, Qtz-T
"	10	32	1.7	Mont-A, Felds-Mo, Qtz-Mi
"	-	276	2.7	Mont-A, Felds-Mi
"	-	392	1.5	Mont-A, Felds-Mi, Qtz-Mi
809	2	15	2.6	Mont-A, Felds-Mo, Qtz-Mi, Cristob-Mi?
"	4	33	2.7	Mont-A, Felds-Mo
811	5	42	1.3	Mont-A, Felds-Mo, Qtz-Mi
"	-	113	4.5	Mont-A, Qtz-Mo, Felds-Mi, Siderite-Mi
"	-	177	2.5	Mont-A, Qtz-Mi, Felds-Mi
812	43	157	2.2	Mont-A, Qtz-Mo
818	4	29	2.4	Mont-A, Felds-Mo, Qtz-Mi

TABLE II. COMPOSITION; MUD BOIL AND SLIDE HEADWALL SAMPLES

SAMPLE		CARBONATES (Whole soil) (%)	CONSTITUENTS FROM X-RAY POWDER ANALYSES
MUD BOIL		4.0	Mont-abund. Quartz-mod. Felds-abund. Dolomite-minor
SLIDE HEADWALL	T1	2.8	Mont-abund., Quartz-abund., Feldspar-moderate
"	T2	3.8	Mont-abund., Quartz-abund., Feldspar-abund.
"	T3	4.2	Mont-abund., Feldspar-abund., Quartz-trace

TABLE III. CHEMICAL TEST RESULTS; BOREHOLE SAMPLES

SAMPLE			CARBONATE (Whole soil) %	GLYCOL RETENTION on < 2 μ m mg/g	SALINITY g/l	Na g/l	Ca g/l	Mg g/l	Fe g/l	Cl g/l	pH
Drill Hole	Number	Depth (ft)									
Above coal measures:											
803	28	135	1.7	207	1.9	0.71	0.02	0.04	-	-	8.7
"	29	317	32.4	142							
"	-	595	17.1	213							
815	7	431	34.5								
"	9	448	51.2								
"	12	482.5	3.5	233							
"	14	506	7.5								
"	18	542	34.3								
"	20	562	9.3	136	3.4	1.15	0	0.06	-	-	8.6
"	22	583	67.6								
"	29	669.5	35.5								
816	19	473	30.7								
74-27	1	569.5	60.4								
74-28	1	480	2.0		6.46	2.07	0.04	0.03	0	1.93	8.7
"	2	644	6.4	167							
"	3	738	7.5	265							
"	4	763	31.6								
"	5	767.5	26.5								
"	6	179.5	44.3								
"	7	451	12.9								
"	8	537	2.7	190	3.9	1.24	0	0.05	0	0.96	8.6
"	9	588	1.5								
Below coal measures:											
804	1A	51	1.7								
805	16 Green Black	62	5.3 1.1								
806	7	18	1.3								
"	-	135	2.5			1.96	-	0.78	-	?	-
"	-	325	2.1							0.03	
807	12	23	2.4								
"	14	159	1.7								
808	40	12	3.0								
"	10	32	1.7								
"	-	276	2.7	185	4.6	2.13	0	0.49	0.74	0.24	9.3
"	-	392	1.5	131							
809	2	15	2.6								
"	4	33	2.7								
811	5	42	1.3	(186) 180	-						
"	-	113	4.5	129							
"	-	177	2.5	(202) 243	4.2	2.10	0	0.63	0.62	-	9.3
812	43	157	2.2								
818	4	29	2.4	264	3.7	1.59	0	0.14	0.12	-	9.1

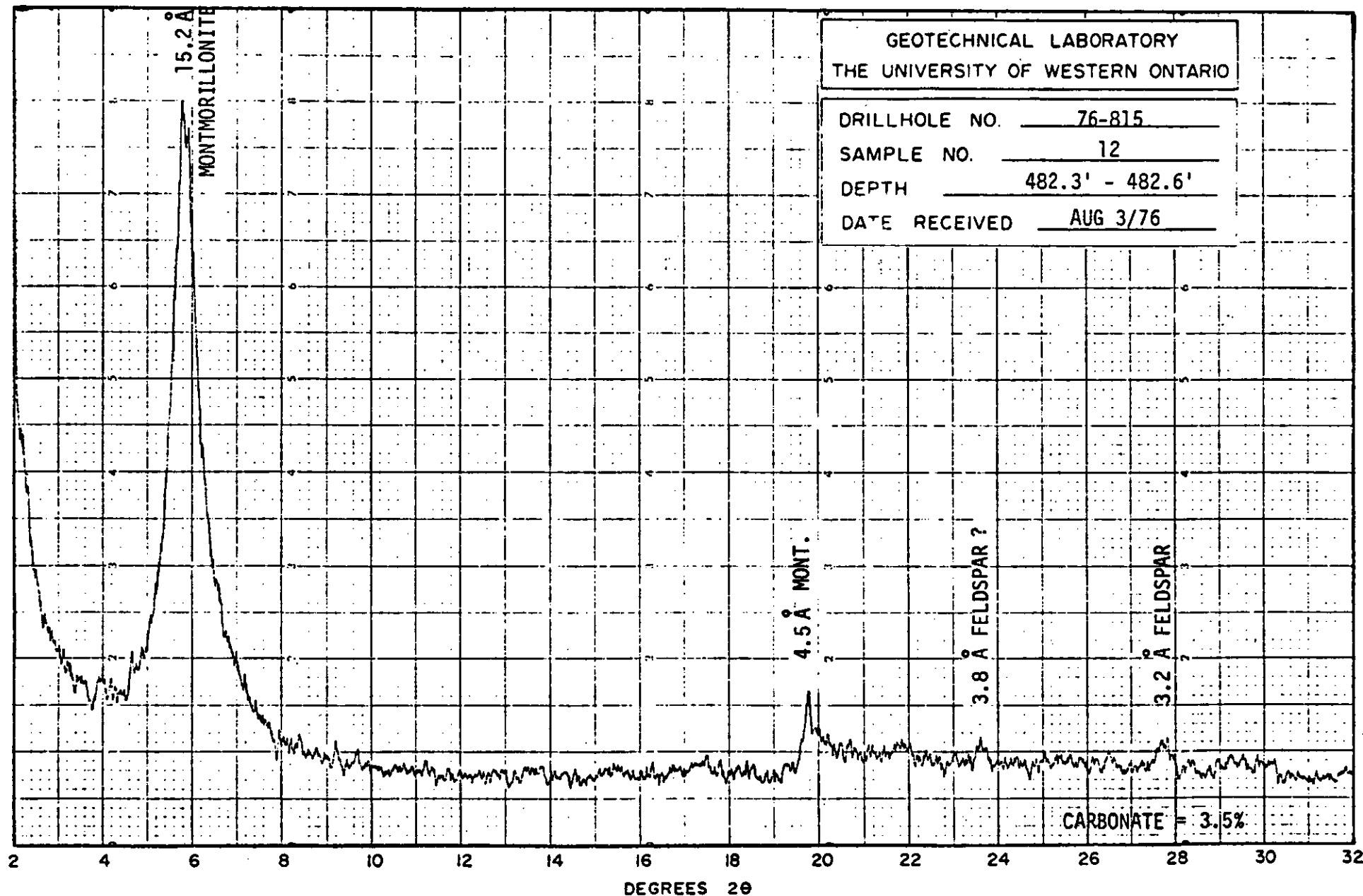


FIG. 1. X-RAY DIFFRACTION TRACE OF WHOLE SOIL POWDER FROM HAT CREEK.

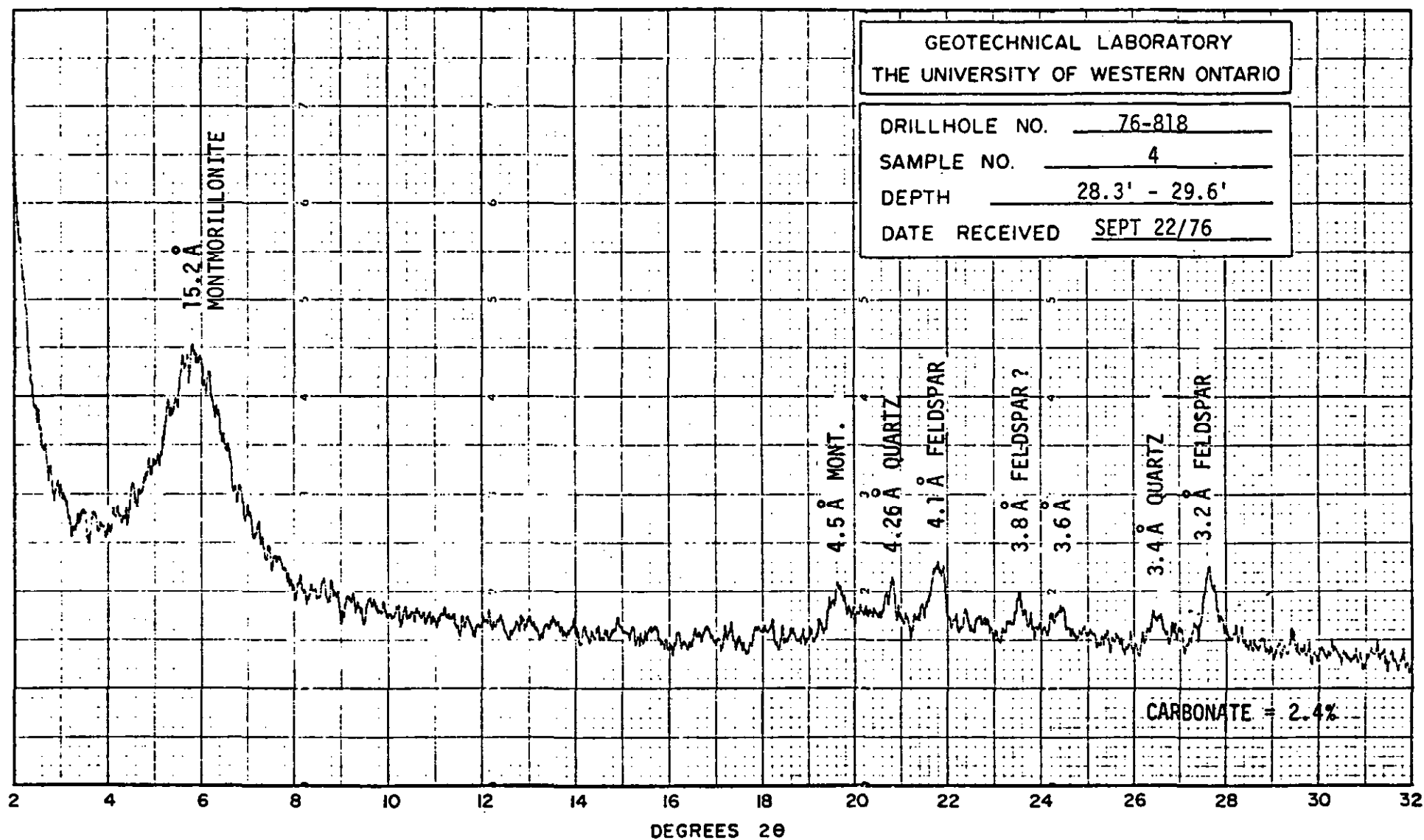


FIG. 2. X-RAY DIFFRACTION TRACE OF WHOLE SOIL POWDER FROM HAT CREEK.

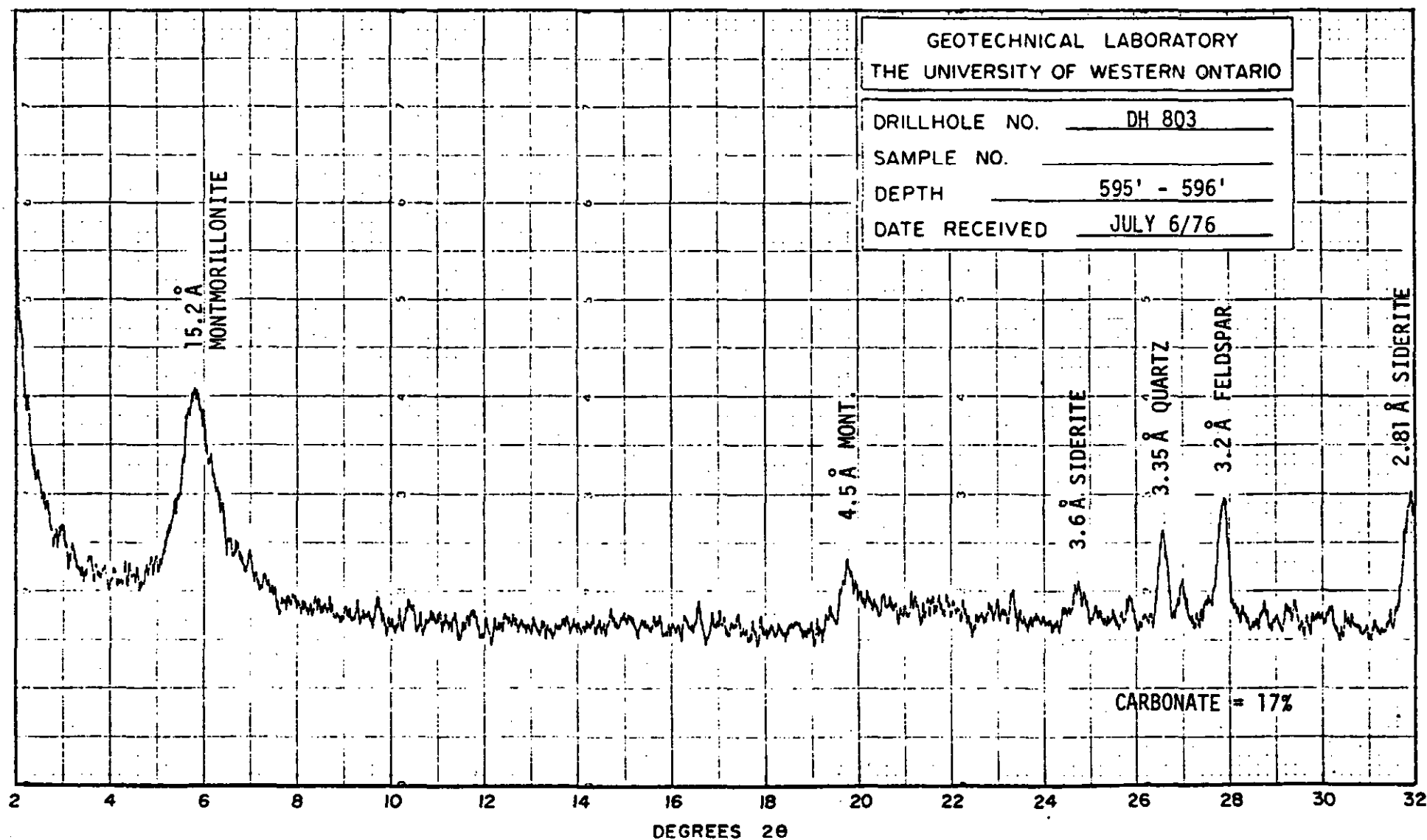


FIG. 3. X-RAY DIFFRACTION TRACE OF WHOLE SOIL POWDER FROM HAT CREEK.

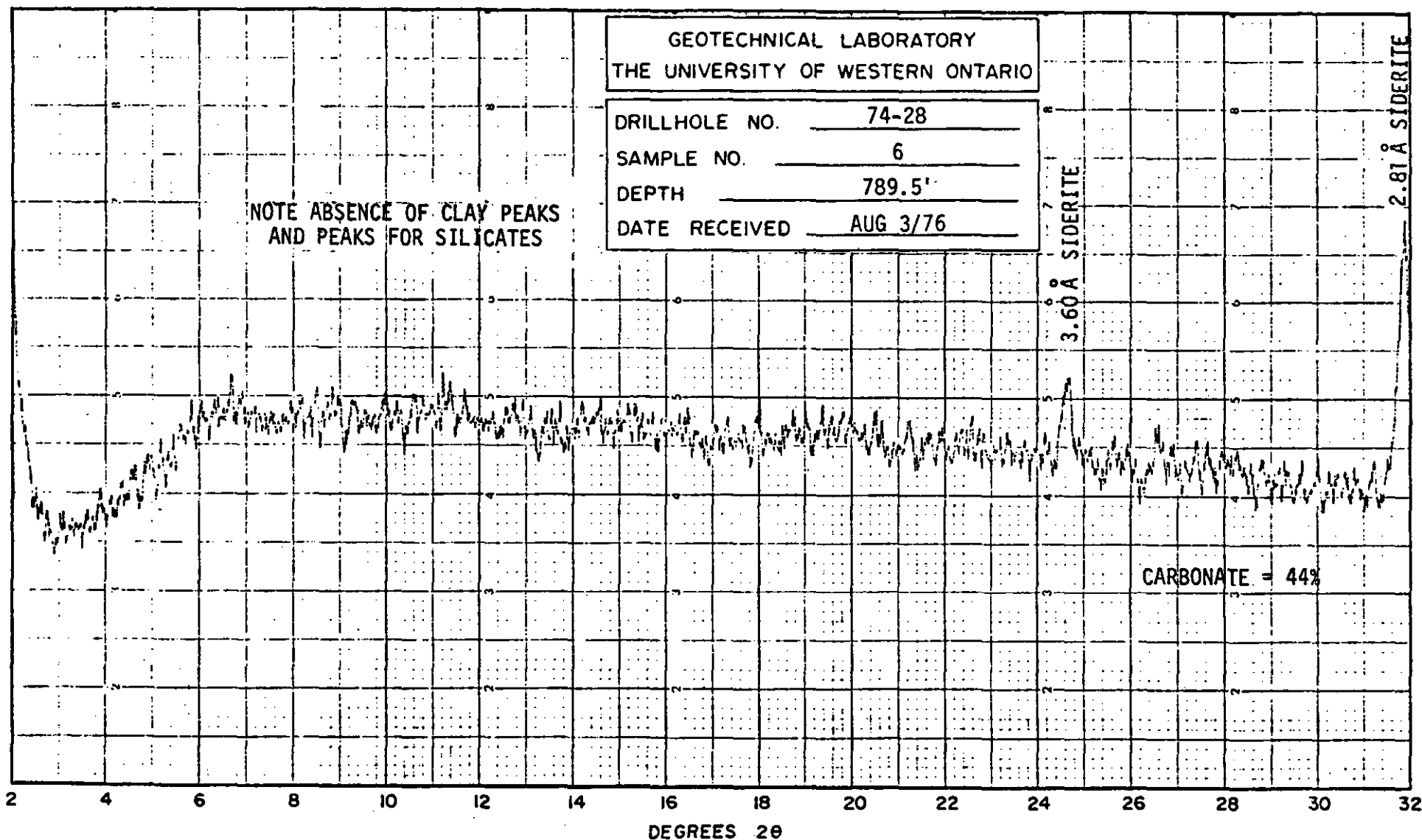
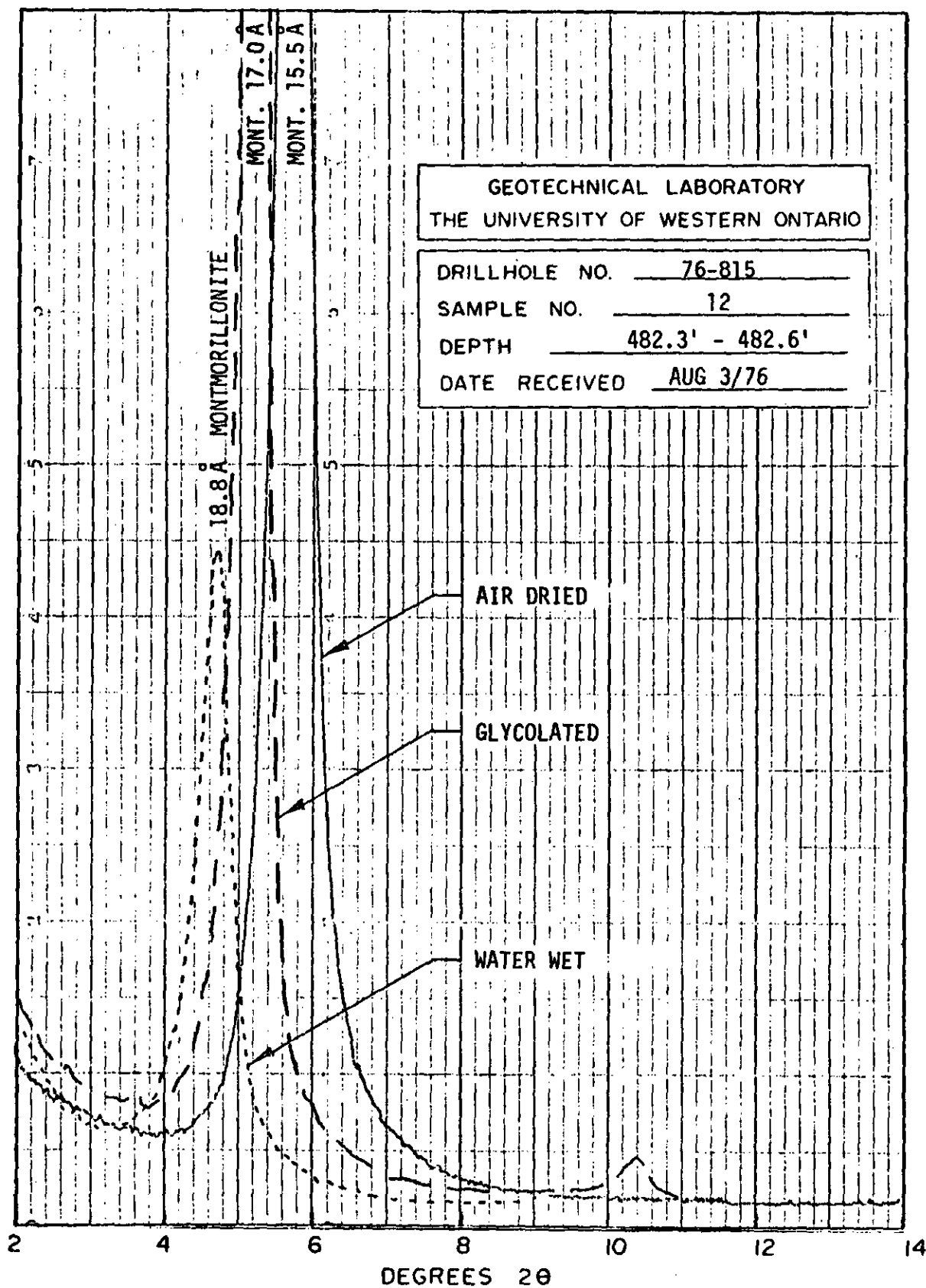
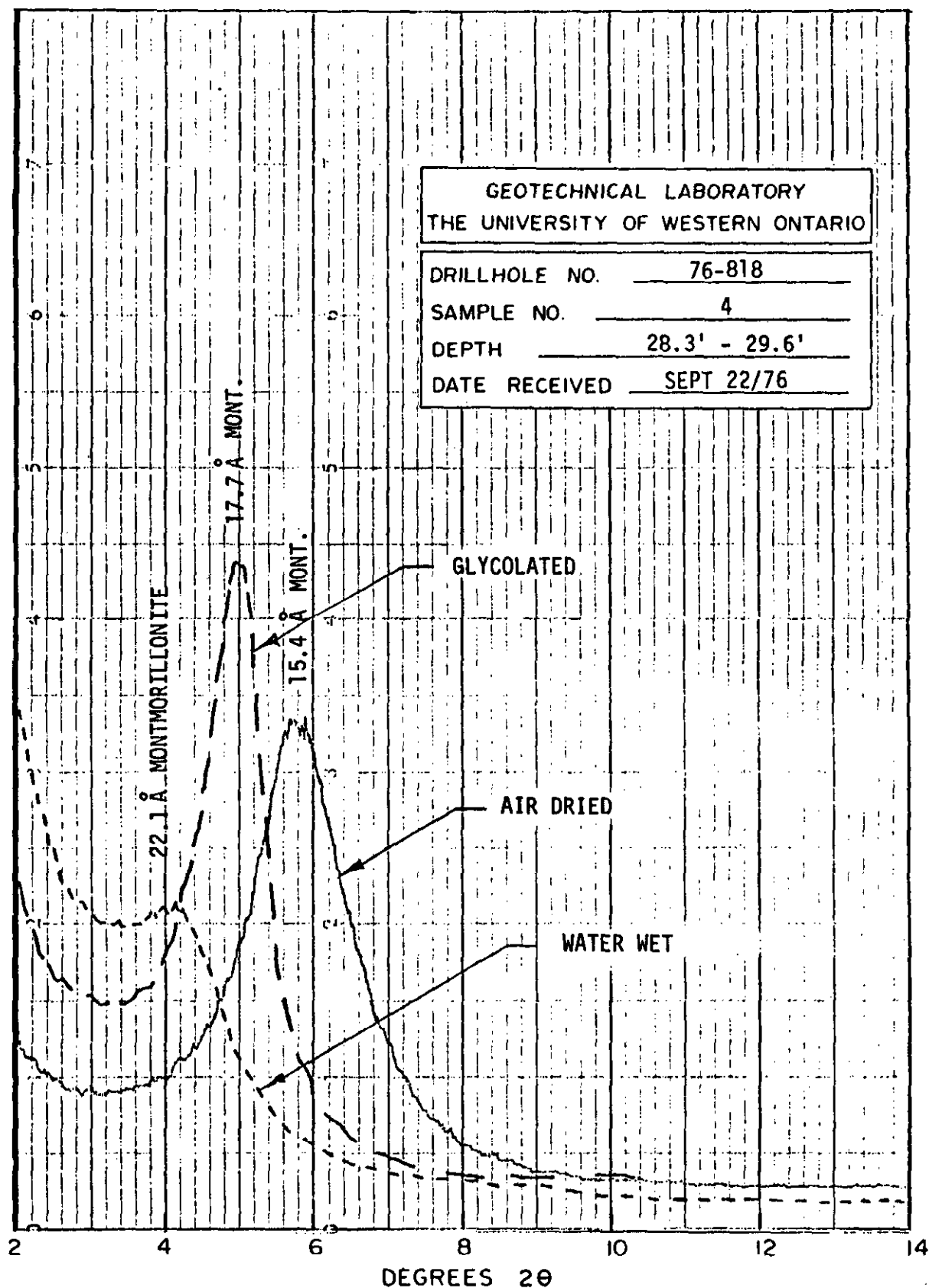


FIG. 4. X-RAY DIFFRACTION TRACE OF WHOLE SOIL POWDER FROM HAT CREEK.



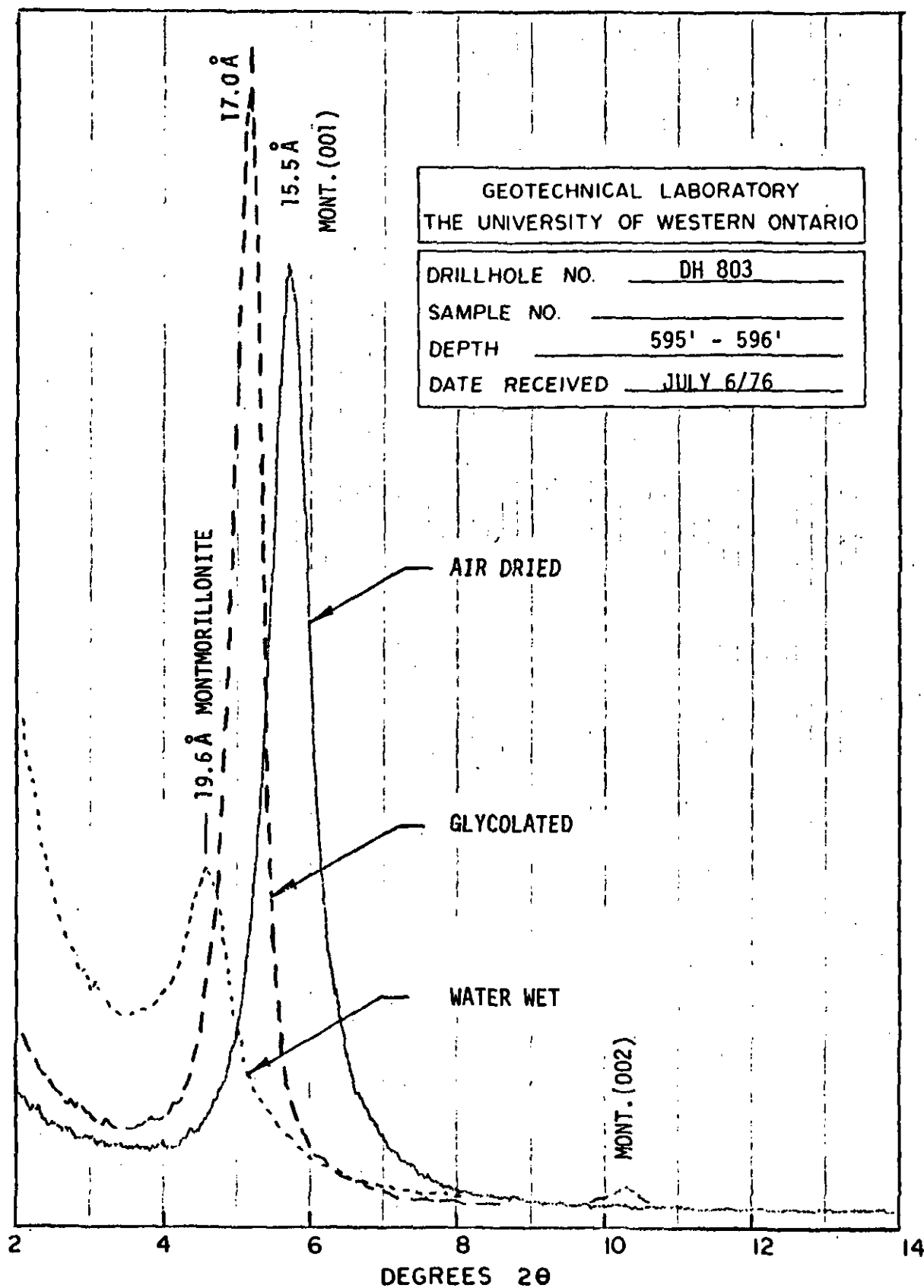
X-RAY DIFFRACTION TRACES OF $< 2 \mu\text{m}$, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.

FIG. 5.



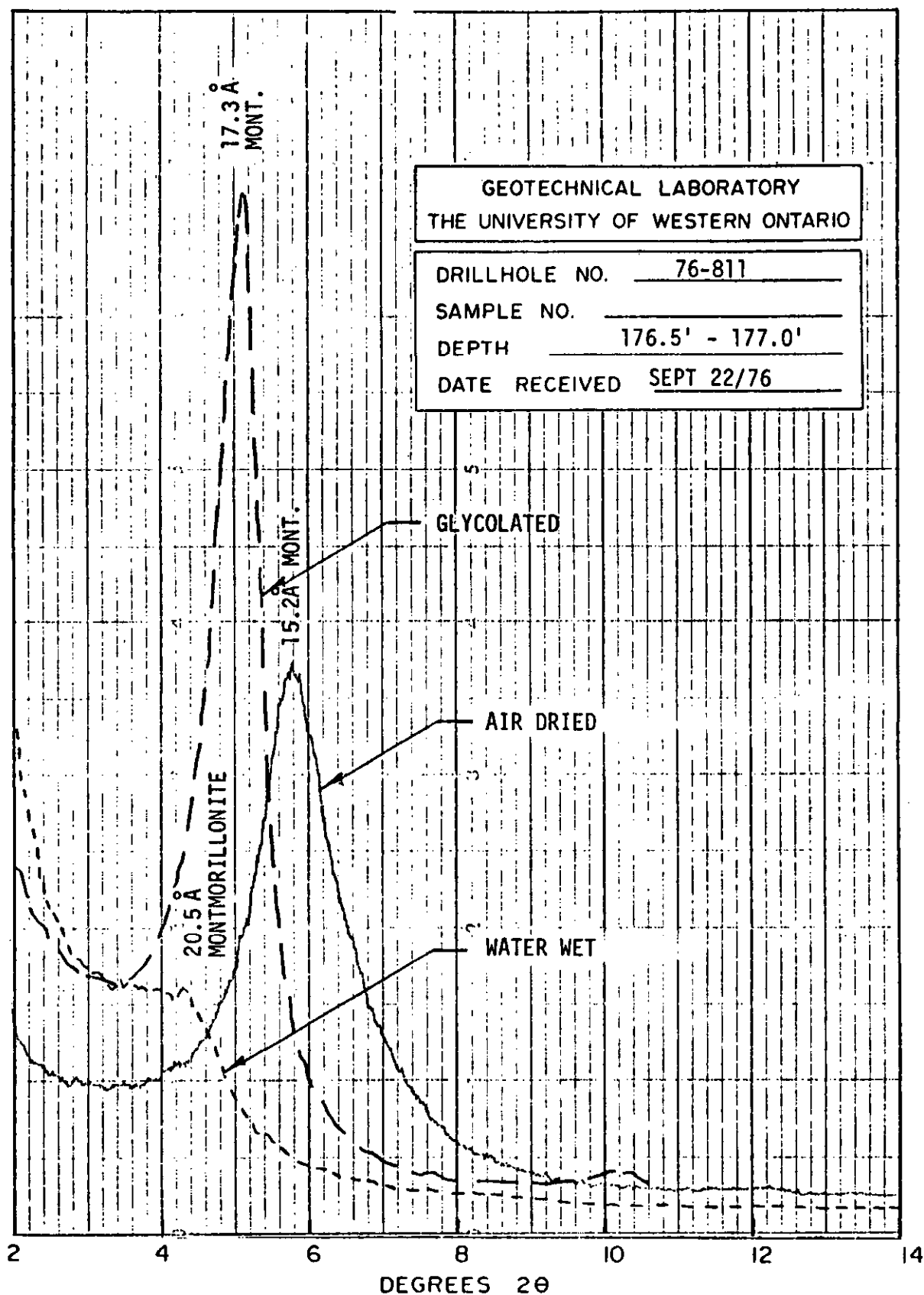
X-RAY DIFFRACTION TRACES OF $< 2 \mu\text{m}$, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.

FIG. 6.



X-RAY DIFFRACTION TRACES OF $< 2 \mu\text{m}$, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.

FIG. 7.



X-RAY DIFFRACTION TRACES OF $< 2 \mu\text{m}$, PREFERRED ORIENTED SPECIMENS FROM HAT CREEK.

FIG. 8.

R.M. QUIGLEY INC.
ROBERT M. QUIGLEY, PH.D., P.ENG.
President

1052 Kingston Avenue
London, Ontario, N6H 4C6

22 December 1976

Mr. G.E. Rawlings
Golder Brawner & Associates Ltd.
224 West 8th Avenue
Vancouver, British Columbia
V5Y 1N5

Dear Mr. Rawlings:

The Significance of Montmorillonite in
the Hat Creek Stratigraphic Section

The purpose of this letter report is to discuss the engineering characteristics of the clay mineral montmorillonite with special reference to the Hat Creek project, British Columbia. Also discussed are the significant engineering aspects of the mineralogical and physico-chemical test results contained in the University of Western Ontario research report entitled "Preliminary Mineralogical and Physico-Chemical Analyses, Hat Creek Project, British Columbia" dated November 26, 1976.

This report has been prepared in accordance with verbal arrangements made at a meeting in your Vancouver offices on October 15, 1976 and follow-up letters dated October 20 and 25, and November 2, 1976.

Crystal Structure of Montmorillonite

The clay mineral, montmorillonite, is a very fine grained, 3-layer silicate of extreme activity relative to other clays. Its crystal structure and mineralogical characteristics are illustrated in Figure 1.

As can be seen from the sketch, each 3-layer unit is comprised of a gibbsite or aluminum hydroxide sheet (G) sandwiched between two silica sheets. The gibbsite sheet carries a net negative charge of -0.3 e.s.u.

per unit cell of 10 oxygens as shown by the structural formula. This charge is balanced by adsorbed, hydrated cations that occur both between the 3-layer units and in the double layer around the entire clay particle.

The number of cations present around a clay crystal to satisfy its negative charge is normally expressed in milliequivalents/100 g of clay and for montmorillonite is of the order of 100 m.eq./100 g.

The spacing between the 3-layer units normally varies from 16 to 18 Å damp and in the natural state. If dried completely, the spacing decreases to 9.3 Å. Some expandable montmorillonites in dilute, monovalent electrolytes may swell to several tens of angstroms so that, in effect, the bulk of the crystal structure is composed of weakly adsorbed water.

The very small size of the montmorillonite particles plus the inter-layer area yield very high specific surfaces for montmorillonite (800 m²/g). Generally speaking, the smaller the particles (i.e. the greater the specific surface) the more active the clay and the lower its residual friction angle.

One measure of the specific surface is the glycol retention value expressed in mg/g. Values for montmorillonite are normally about 250 mg/g, irrespective of the cations present. The ethylene glycol used for the retention measurements is believed to adsorb on the clay in a layer 2 molecules thick.

The combination of abundant interlayer and adsorbed double layer water is responsible for the high activity, marked swelling and low strength characteristics of montmorillonites.

It is particularly significant that the type of adsorbed cations and the concentration of the pore fluid electrolyte play an important role in establishing the physical properties of this clay. For example, Na⁺-Mont swells much more than Ca⁺⁺-Mont because twice as many hydrated cations are required to satisfy the negative charges on the particles. Also, a dilute electrolyte serves to expand the double layer around the clays since there are very large concentration differences between the adsorbed cations in the double layer relative to the free water. Conversely a high electrolyte concentration (salty pore fluid) compresses the double layers, tends to cause flocculation and normally increases the strength of the soil.

If dried to fairly high temperatures ($450 \rightarrow 700^{\circ}\text{C}$), some montmorillonites become useful absorbents and decolourizing agents known as Fuller's earth.

Plasticity and Activity of Montmorillonite

Typical values for the liquid limit and activity of the most important clay minerals are tabulated as follows:

Clay Mineral	Pore Fluid Salt Conc.	ω_L (%)	Activity ($I_p \div \% < 2 \mu\text{m}$)
Kaolinite	Low \rightarrow High	30 - 60	0.2 \rightarrow 0.4
Illite & Chlorite	Low \rightarrow High	50 - 130	0.5 \rightarrow 1.0
Ca Mont	Low \rightarrow High	100 - 250	1.5 \rightarrow 1.8
Na Mont	* High	400 - 550	3.5 \rightarrow 5
Na Mont	* Low	1000 - 1300	9 \rightarrow 11

*High = 1 to 10^{-1} Normal; Low = 10^{-3} to 10^{-4} N.

The tabulation shows that montmorillonite is very active and plastic relative to the other clays. It also shows that Na montmorillonites are much more plastic and active than Ca Mg montmorillonites and that for dilute pore fluid concentrations, montmorillonite is a truly extraordinary material.

The very high liquid limit values for Na montmorillonite are caused by interlayer expansion that is inhibited by adsorption of cations such as Ca, Mg and K. Figure 2, adapted from Rosenqvist, 1957, illustrates this phenomenon for regimes of monovalent cations. The interlayer collapse caused by K^+ adsorption relative to Na^+ adsorption reduced the liquid limit of Rosenqvist's test clay from about 370 to 280. Similar collapse occurs with adsorption of Ca and Mg.

The data illustrated in Figure 3 were taken directly from Quigley et al, 1974 and serve to illustrate two points as follows:

1. The test montmorillonite, homoionic in Na^+ , has an activity of 5.5 compared to about 1.7 for the clay homoionic in Mg^{++} (Salinity $\sim 5 \text{ g/l}$).

2. The mixtures of Mg illite and Na montmorillonite produced a strong curvature in the activity curve caused by adsorption of Mg onto the montmorillonite from the illite. In other words, preferential adsorption of Mg onto the Na montmorillonite significantly reduced its activity.

Figure 3 also shows values of glycol retention obtained on the illite-montmorillonite mixtures. It is significant that for 100% montmorillonite, similar glycol retentions were obtained for the Na and Mg clay states. The glycol retentions run on the Hat Creek clays are therefore a measure of specific surface and not greatly affected by interlayer or other swelling.

Although little if any illite was observed on the x-ray traces of the Hat Creek deposits, there is enough free Mg^{++} in the pore fluid to markedly reduce the liquid limits and activity values below those for a purely Na^+ clay.

Permeability

The permeability of montmorillonite varies within the range of 10^{-9} to 10^{-8} cm/sec over a void ratio range of 2 to 10. Sodium montmorillonite is normally at least one order of magnitude less pervious than Ca Mg montmorillonites due largely to a greater proportion of the pore water being bound by adsorption around the monovalent Na cations.

For the sodium rich Hat Creek clays with a void ratio of about 1.0 (corresponding to $w_n = 35\%$), the permeability would probably be in the range of 10^{-10} cm/sec or less.

Residual Drained Strength Characteristics

The shear strength data plotted in Figure 4 were taken directly from Kenney, 1967 and serve to illustrate the residual friction angles characteristic of the main clay mineral groups. The very low values for montmorillonite are characteristic and caused by gliding along the inter-layer water between the 3-layer sheets.

The following tabulation shows the significance of both cation type and pore fluid concentration on the ϕ_{residual} :

<u>Clay</u>	<u>S (g/l)</u>	<u>ω_l</u>	<u>ω_p</u>	<u>A_c</u>	<u>ϕ_{res}</u>
Na Mont	0	~ 1500	55	~ 14	~ 4°
Na Mont	30	~ 800	45	~ 7	~ 8°
Ca Mont	0	795	47	7.4	~ 9°
Ca Mont	Ca SO ₄ sat'd	775	47	7.4	~ 10°

*Data taken from Kenney, 1967 who tested pure bentonite which may be more active than the Hat Creek clays. Valid for $\bar{\sigma}_N > 1 \text{ ton/ft}^2$.

It is apparent that both cation type and concentration play a significant role on the values obtained for ϕ_{res} , the worst combination being a very low salinity and a Na^+ cation regime.

The strength of montmorillonite at very low effective stresses is a matter of conjecture in this writer's opinion. There seems to be some evidence that ϕ_{res} actually increases at low values $\bar{\sigma}_N$. However, fabric-strength studies by the writer suggest that clay platelet orientation plays a vital role in determining ϕ_{res} . Above $\bar{\sigma}_N$ values of 1 tsf, parallelism in the shear plane is highly developed. At very low stresses and higher water contents, the natural tendency of montmorillonite to form a gel of more random fabric may become a significant factor and the apparent effective stress control on c_d and ϕ_d may be overwhelmed by long range physico-chemical bonds.

Discussion of the Hat Creek Montmorillonites

The University of Western Ontario research report dated November 26, 1976 identified montmorillonite as the dominant clay mineral within the clayey strata above and below the coal measures at Hat Creek, B.C. In some beds, montmorillonite appeared to be the only mineral present whereas in others, variable amounts of carbonate, quartz and feldspar were present.

The mineralogical compositions of typical clayey strata appear to be more or less as follows:

1. Essentially pure montmorillonite with trace amounts of quartz and feldspar (< 10% primary silicates).
2. Montmorillonite with moderate amounts of quartz, feldspar and possibly α -cristobalite (10 to 30%).

3. Montmorillonite with low to moderate amounts of carbonate (1 to 10% siderite).

The pore water composition of the clayey strata appears to be roughly as follows:

Above the coal measures:

1. Salinity = 3.5 to 6.5 g/l (less in glacio-lacustrine deposits)
2. Dominant cation is Na^+ = 1.2 to 2.1 g/l
Significant cations are Mg^{++} (+ Ca) = 0.05 to 0.07 g/l
3. Significant anions are Cl^- = 1 to 2 g/l and probably some SO_4^{--} (not determined).

Below the coal measures:

1. Salinity = 3.5 to 4.6 g/l
2. Dominant cation is Na^+ = 1.6 to 2.2 g/l
Significant cations are Mg^{++} (+ Fe) = 0.24 to 1.23 g/l
3. Significant anions are Cl^- and probably SO_4^{--} not determined.

From an engineering point of view, the "pure" or "near pure" montmorillonite beds are the most significant. The carbonate rich beds are less significant, since the carbonates act to some extent as inhibitors of swelling and produce relatively higher shear strengths. Those "near pure" montmorillonites with pore fluids of lowest salinity and highest sodium content are the most significant of all beds.

The total salinity values obtained to date (3.5 to 6.5 g/l) are high enough that extraordinary swelling is probably not a problem unless fresh water leaching somehow proceeds within the deposit. Any strata that do exist with very low pore fluid salinities must be considered as extra-significant strata requiring special attention.

Although the dominant cation is Na^+ in all pore fluid samples tested, there is enough Mg, Ca and Fe in the pore fluid to ensure a dominantly divalent regime in the double layer. This, along with the moderate salinities, should serve to effectively reduce the liquid limits and activity values of the Hat Creek clayey strata. Very approximate calculations using Gapon's exchange equation indicate that, with the pore

fluid compositions so far obtained, the cations present in the double layers around the montmorillonite consist of:

Above the coal measures:

Divalent cations	60 - 70%
Monovalent Na ⁺	40 - 30%

Below the coal measures:

Divalent cations	75 - 85%
Monovalent Na ⁺	25 - 15%

These are very approximate since the pore fluid analyses were run on a soil wash rather than squeezed out pore water and the divalent cations may be more abundant than indicated above.

Although the writer did not feel authorized to make an extensive search for geological and mineralogical references to Cordilleran bentonites, some data for Wyoming and Alberta bentonites are readily available. For example, non-marine, late Cretaceous bentonites near Edmonton (Rosalind, Alberta) are discussed by Scarfe, 1973. The major components of these bentonites are cristobalite and montmorillonite, both believed to be in situ alteration products of the glassy volcanic ash deposits. Contaminants are commonly quartz, plagioclase feldspar plus biotite and occasionally siderite. Sodium is apparently the dominant cation along with calcium and magnesium which are indicated to comprise 20 to 55% of the cation exchange capacity.

Wyoming bentonites are described by Güven and Grim, 1972, and again the dominant constituents are 70% smectite and 20% α -cristobalite in the < 5 μ m fraction. Quartz, feldspar and α -cristobalite dominate the coarse fraction (> 5 μ m).

The Hat Creek deposits are quite similar to the above bentonites although α -cristobalite having a very strong 4.04 Å peak seems to be a rather less abundant constituent.

It is understood from telephone conversations with Mr. G. Rawlings that the index properties of the Hat Creek clayey strata have been determined to be more or less as follows:

$w_n \approx 35\%$

$w_l \approx 109 \text{ to } 178\%$

$w_p \approx 34 \text{ to } 39\%$

Activity = 0.75 to 1.4 (est'd by R.M. Quigley)

The values of liquid limit seem characteristic of montmorillonite with abundant adsorbed divalent cations and are thus consistent with the physico-chemical test results. The activity values are likewise consistent with the mineralogical and physico-chemical test results although somewhat on the low side.

Conclusion

It is hoped that the previous discussions, comments and questions have satisfied the requirements expected of this letter report.

Yours truly,

R.M. QUIGLEY INC.



R.M. Quigley, P.Eng.
Designated Specialist
Civil Geotechnics
(Ontario APEO)

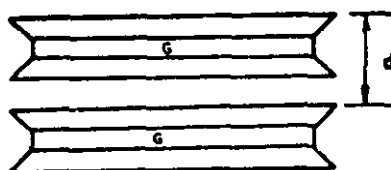
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Selected References

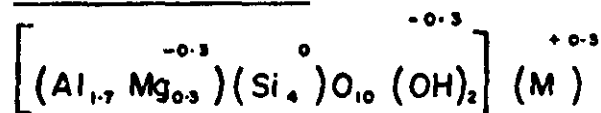
- Güven, N. and Grim, R.E., 1972. X-ray diffraction and electron optical studies on smectite and α -cristobalite associations. *Clays and Clay Minerals*, 20, 89-92.
- Kenney, T.C., 1967. The influence of mineral composition on the residual strength of natural soils. *Proc. Geotech. Conf., Oslo*, 1, 123-129.
- Quigley, R.M., Kubo, Y. and Hamilton, J.J., 1974. Activity of illite-montmorillonite mixtures. The Univ. of Western Ontario, Faculty of Engineering Science Research Report SM-3-74, 31 p.
- Rosenqvist, I.Th., 1957. Discussion. *Proc. 4th Int'l. Conf. on Soil Mechanics and Foundation Eng.*, 3, 257-258.
- Scarfe, D.W., 1973. Bentonite characteristics from deposits near Rosalind, Alberta. *Clays and Clay Minerals*, 21, 437-449.

MONTMORILLONIDS



d variable (generally 16 to 18 Å damp)

Structural Formula



Classical montmorillonite

Properties and Characteristics

C.E.C. = 100 m.eq./100 g

Glycol retention = 250 mg/g

Specific surface = 800 m²/g

Size of platy crystals:

Diameter = 0.1 to 1 μm

Thickness = $\frac{1}{100}$ diam

FIGURE 1. THE NATURE OF MONTMORILLONITE

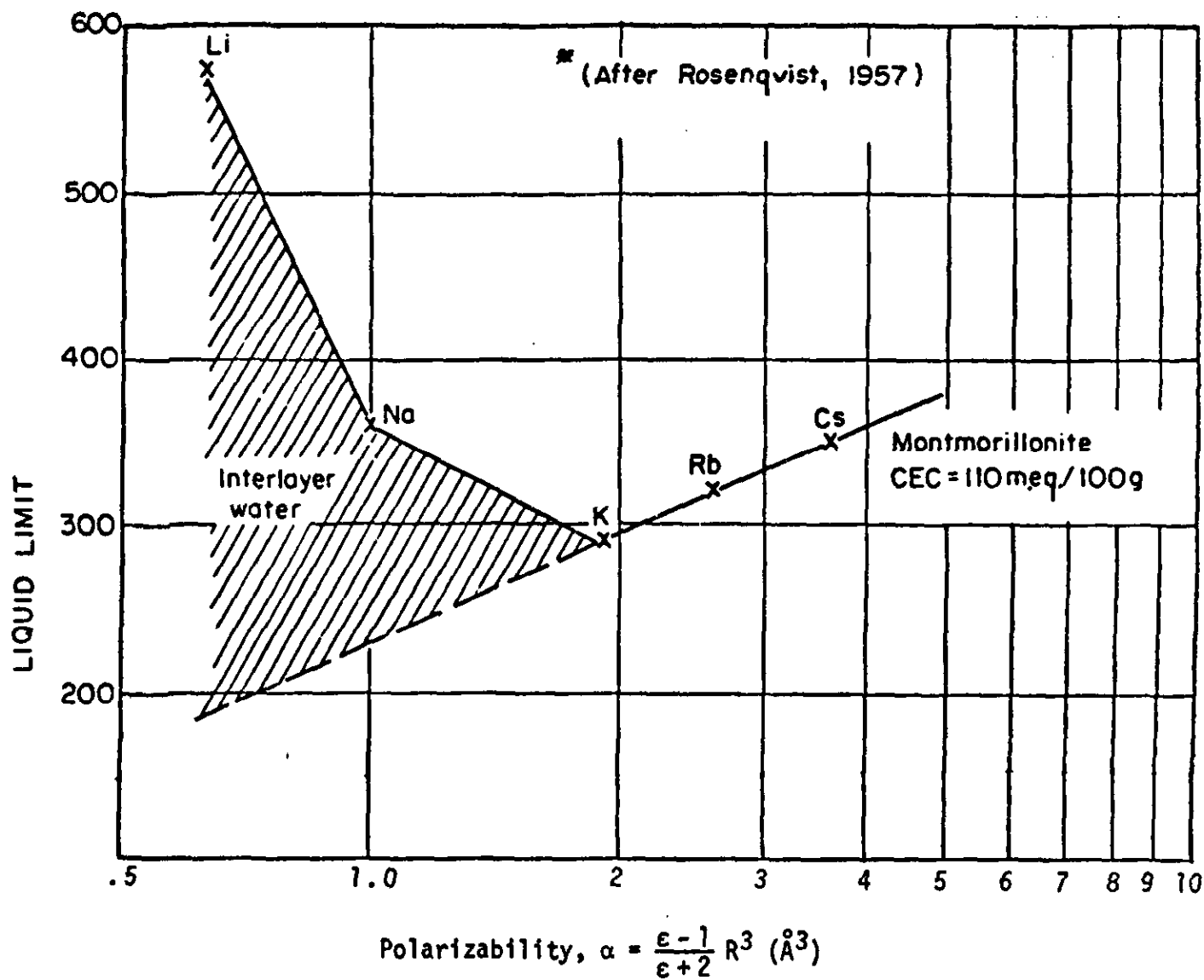


FIGURE 2. VARIATION IN LIQUID LIMIT OF MONTMORILLONITE WITH VARIOUS MONOVALENT CATIONS

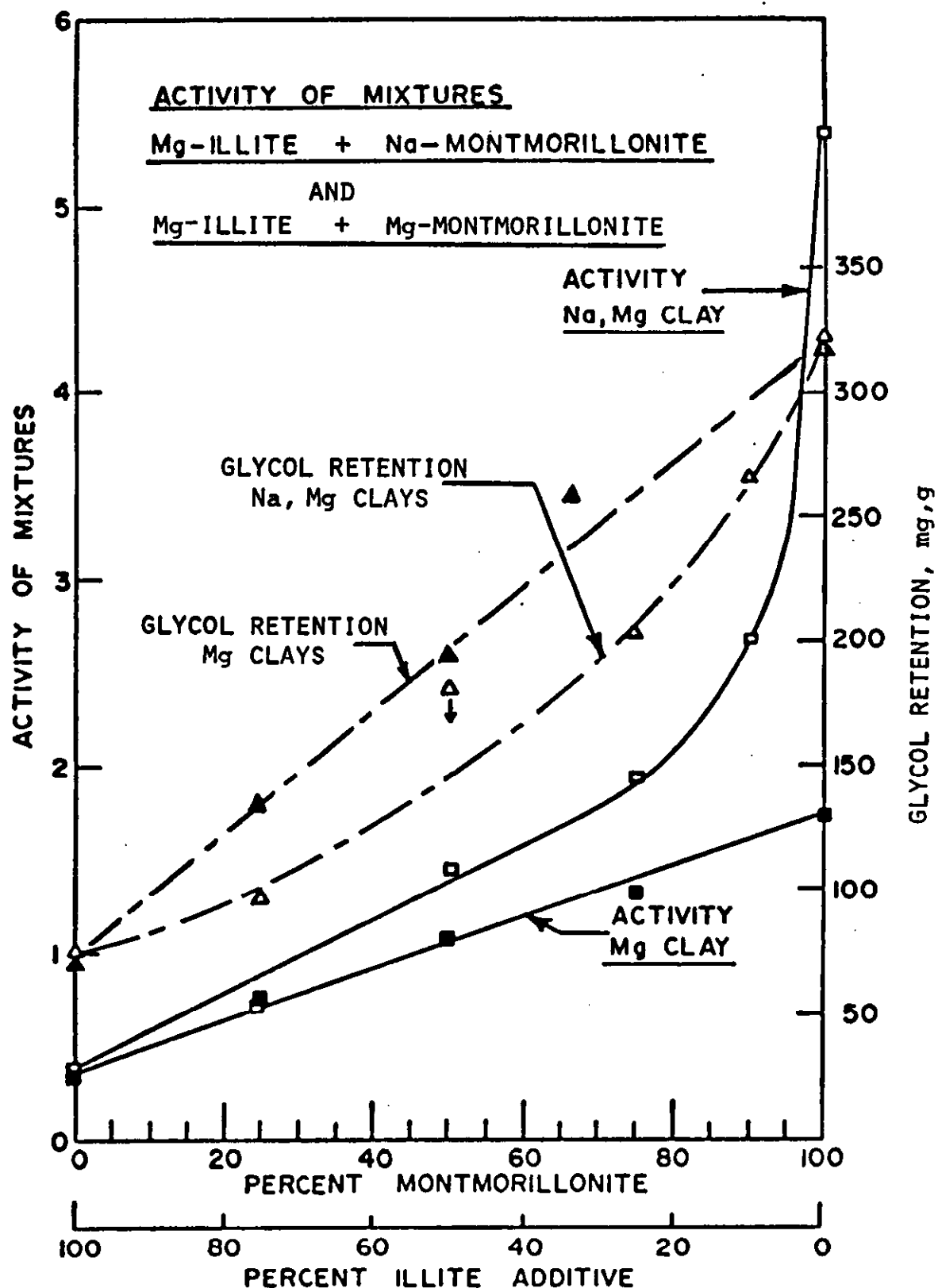


FIGURE 3. ACTIVITY AND GLYCOL RETENTION OF MIXTURES OF ILLITE AND MONTMORILLONITE (after Quigley, Kubo and Hamilton, 1974)

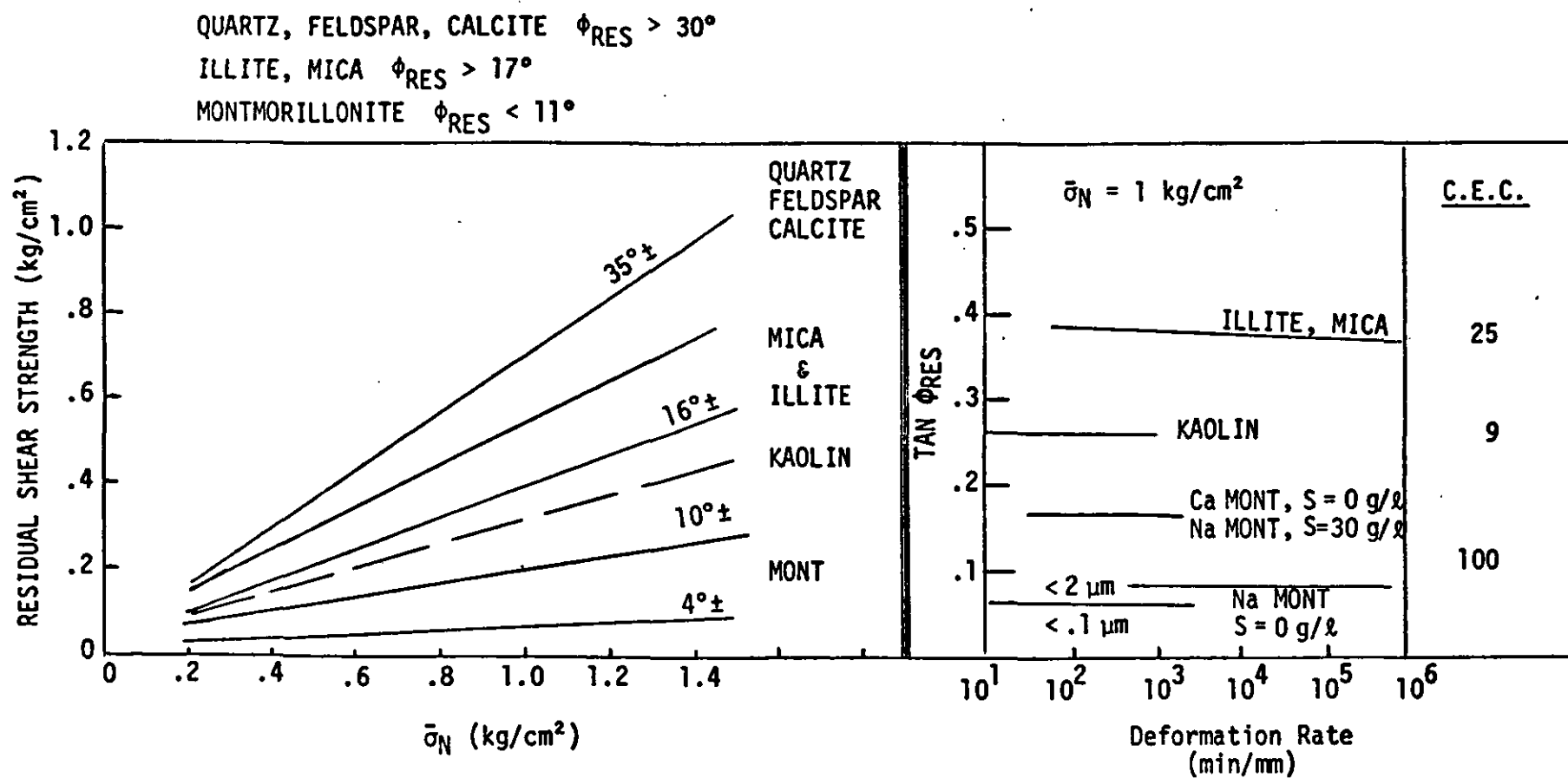


FIGURE 4. RESIDUAL DRAINED STRENGTHS OF THE CLAY MINERAL GROUPS
 (adapted from Kenney, 1967)



RECVD. AT GDA VANCOUVER
JAN 17 1977
FILE NO. 100-100000-100000

The x-ray powder pattern shows the sample to consist of the

following minerals in their approximate order of abundance:

Montmorillonite	- dominant
Feldspar and cristobalite	- moderate
Quartz	- moderate to minor

The actual x-ray trace is quite similar to that shown in Fig. 2 of our final report dated November 26, 1976. Carbonate peaks could not be identified on the trace indicating little if any siderite.

The x-ray diffraction traces on the oriented fines yielded traces similar to those shown in Fig. 7 of our November 26, 1976 report. Strong peaks at 20.1 Å (water wet), 15.2 Å (air dried) and 17.1 Å (glycolated) were obtained indicating a nearly pure montmorillonite since peaks at 10 Å and 7 Å were not present.

The pore water salinity, assuming a natural water content of 35%, is about 4.1 g/l which is similar to the salinities throughout the section as documented in Table III of our November 26, 1976 report. A measured pH of 9.6 is somewhat higher than the typical 9.3 reported on two other samples located stratigraphically below the coal measures.

The cation analyses yield values for Na, Ca and Mg as follows:

Na ⁺	= 2.1 g/l
Ca ⁺	= .016 g/l
Mg ⁺	= .014 g/l

The sodium value is close to measured values of 1.59 to 2.13 on three other samples below the coal. The values for calcium are very low as in the previous testing. The value for magnesium is much lower than the 0.5 to 0.8 g/l obtained on three other samples below the coal.

Comments

On the basis of the above analyses, it is suggested that this clay stone is essentially sodium saturated and with swelling permitted would yield a residual friction angle of not greater than 7 or 8 degrees.

Lower values would not be expected unless the salt content is reduced below its in situ value of 4.1 g/l.

The writer has reviewed the unsigned reports on the direct shear data supplied to him and concurs with their author that the undisturbed sample did not swell due to the exceptionally low permeability of the bentonitic clay stones. The writer also agrees that complete remoulding at a higher moisture content (more or less in equilibrium with the effective stress on the failure plane at failure) is the best way to establish the lower bound of the friction angle. The writer has found that removal of the grit from soft samples is often necessary to ensure that the lower bound friction values are obtained.

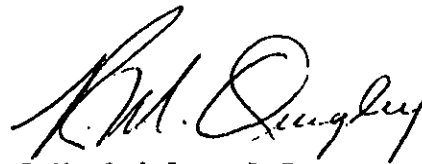
Questions which should be asked regarding direct shear procedures are as follows:

1. Did the clay actually reach residual strength in terms of both clay platelet parallelism and moisture content change?
 - (a) For hard, over consolidated clays like those from Hat Creek, the moisture content should increase greatly on the failure plane.
 - (b) For soft, normally consolidated clays rich in montmorillonite, the moisture content will decrease on the failure plane yet parallelism may cause a net loss of strength.
2. With regard to the above, an attempt should be made to obtain the moisture content on the actual failure plane and a plot of drained strength vs water content plotted as a control against plots of the strength envelope ($\bar{\sigma}_{ff}$ vs τ_{ff}).
3. Did the presence of grit rolling or grinding along between the halves of the direct shear box create an artificial ϕ ? Similarly, was there unnatural gouging by large sized particles (sand) that would create a ϕ_{res} larger than representative of the field ϕ_{res} ?

4. Was the rate of strain slow enough to ensure drainage (i.e. no excess pore pressures during shear)? Indeed, is it possible to shear a sample of hard Na bentonite by direct shear and obtain no excess pore pressures?
5. At low stress levels and very low strain rates, will the natural thixotropic properties of the bentonitic clays overwhelm the usual effective stress type of relationships commonly obtained on clayey soils?

Although these comments must necessarily be incomplete at this early phase in the study of these complex clay stones, it is hoped that they meet the present needs of the project.

Yours sincerely,

A handwritten signature in dark ink, appearing to read 'R.M. Quigley', written in a cursive style.

R.M. Quigley, P.Eng.
Professor

RMQ:em

SUMMARY OF X-RAY DIFFRACTION ANALYSES
CARRIED OUT BY THE
UNIVERSITY OF BRITISH COLUMBIA
DECEMBER, 1966

Hole No.	Depth (Ft.)	Quartz	Kaolinite	Bentonite	Siderite	Felspar	Epidote
76-123	399 -403	11	3	69	13	4	-
76-124	348 -350	9	10	71	-	10	-
76-135	296 -301	13	47	34	-	6	-
76-135	534.1-534.5	31	37	26	6	-	-
76-135	557.5-557.7	24	27	39	-	10	-
76-135	661.0-661.3	34	52	14	-	trace	-
76-136	219 -221	8	11	79	-	2	-
76-144	442	49	15	29	-	7	-
76-191	238.6-238.9	8	55	22	trace	15	-
76-191	298.2-298.5	{ 20	48	19	-	13	-
		{ 12	58	30	-	-	-
76-191	388.1-388.4	11	68	15	-	6	-
76-191	464.1-465.0	17	47	36	trace	-	-
76-191	532.8-533.1	22	29	38	-	11	-
76-191	645.0-645.5	19	51	-	19	-	11
76-191	706.2-706.5	47	53	trace	-	-	-
76-191	744.7-745.0	43	67	-	-	-	-
76-191	809.1-809.5	{ 45	51	-	4	-	-
		{ 46	44	-	-	8	-
76-191	950.2-950.8	38	62	trace	-	-	-
76-191	1285.6-1286.0	{ 35	65	-	-	-	-
		{ 43	54	-	3	-	-

Note: Accuracy for quartz, kaolinite and felspar \pm 3%,
for bentonite \pm 5%.

COPY OF ORIGINAL LETTER

CORE LABORATORIES-CANADA LTD.
Petroleum Reservoir Engineering

P.O. Box 5670, Postal Station "A"
Calgary, Alberta T2H 1Y1
Telephone: 253-3391

July 7, 1976

Birtley Engineering (Canada) Ltd.
P. O. Box 5488, Postal Station "A"
Calgary, Alberta
T2H 1X9

Attention: Mr. Don F. Symonds

Re: Analysis of Clay Samples from
B.C. Hydro Sample A-7365/66
Our File Number: 7061-6268

Gentlemen:

The analysis of the above samples showed the following.

Sample 1: Water Content 6.3%
 Mineral Content 83.3%

X-Ray Diffraction Analysis of Mineral Portion

Quartz	14
Feldspar	9
Pyrite	6
Siderite	4
Kaolinite	57
Montmorillonite	10

Sample 2: Water Content 6.3%
 Mineral Content 83.8%

X-Ray Diffraction Analysis of Mineral Portion

Quartz	18
Feldspar	9
Pyrite	5
Siderite	5
Kaolinite	50
Montmorillonite	13

....2

Birtley Engineering (Canada) Ltd.

7061-6268

Sample 3: Water Content 7.6%
 Mineral Content 80.7%

X-Ray Diffraction Analysis of Mineral Portion

Quartz	16
Feldspar	8
Pyrite	Trace
Siderite	Nil
Kaolinite	60
Montmorillonite	16

Sample 4: Water Content 4.0%
 Mineral Content 94.8%

X-Ray Diffraction Analysis of Mineral Portion

Quartz	25
Feldspar	20
Pyrite	Nil
Siderite	Nil
Kaolinite	48
Montmorillonite	7

The samples were dried in a constant humidity oven at 145°F and 50% relative humidity for four days. A Dean and Stark analysis was performed to measure the remaining water; an ash analysis to determine the mineral content and an x-ray diffraction analysis to determine the type and quantity of the clay components.

Assuming that all the water present is intramolecular (inter-layer) water associated with the montmorillonite, the ratio of water to montmorillonite is 0.756/1, 0.579/1, 0.589/1 and 0.602/1 for sample one to four, respectively. By calculating, the molecular ratio between the water and montmorillonite are 15.1, 11.6, 11.8 and 12.0 for samples one to four, respectively.

The above calculations are based on the assumption that all the water is present as intramolecular water associated with the montmorillonite. The ratio of water to montmorillonite is higher than published values (0.15 to 0.20/1) for samples dried at 145°F and 50% relative humidity. This may indicate that all the free water had not been removed or that a portion of the water had been present as intermolecular (inter-particle) being adsorbed between the montmorillonite particles rather than being adsorbed within the particles.

Yours truly,
 CORE LABORATORIES-CANADA LTD.

J. R. Jackson

APPENDIX 4

UNIAXIAL COMPRESSION TESTS

APPENDIX 4
UNIAXIAL COMPRESSION TESTS

Uniaxial compressive strength testing was carried out in conjunction with the field drilling operations in Hat Creek to assess the variation in strengths of the rock types encountered. On site testing was performed so that the prepared samples would be as fresh as possible avoiding moisture loss. The results of the testing were correlated to such factors as rock type, water content, grain size, and gross structural features. The mode of failure of each specimen was also noted.

DESCRIPTION OF TESTS

The test equipment included a manually operated hydraulic loading ram, a loading frame, a 10,000 lb. capacity proving ring and dial gauge, spherical platens to ensure that load application was perpendicular to the sample surface, and several sizes of flat platens.

The cylindrical rock specimens were cut with a length to diameter ratio of approximately 2, but not exceeding 2.5 nor less than 1.5. Careful end preparation of the sample was essential to ensure a smooth planar loading surface perpendicular to the axis of the specimen. In cases where the rock material was too weak or brittle to allow adequate end preparation, the ends of the specimen were cast in a mold of liquid sulfur, which hardened rapidly to a smooth planar surface. The effect of the sulfur was to minimize stress variations across the ends of the sample and thus ensure a uniform axial load.

Prior to testing, the initial length and average diameter of the samples were measured. Loading was applied relatively slowly to allow "seating" of the platens against the ends of the specimen. When "cracking" of the specimen

was heard the loading was slowed to allow the material time to adjust. When load drop off occurred, the load was noted and allowed to fall off to a stable value. At this point, depending on whether fracture of the specimen had occurred, the sample was reloaded until it could take no further load. The maximum load that the sample was capable of sustaining was judged to be the ultimate uniaxial compressive stress.

RESULTS

The results of the uniaxial compressive strength tests are shown in Table A4-1.

The salient features to be noted are as follows:

1. Coal strengths varied from 400 to 2,500 psi. There is no relationship between the compressive strength and depth. The strength is more related to composition, texture, water content, and orientation of discontinuities relative to the direction of loading.
2. Conglomerate varied considerably in strength depending upon the degree of cementation present. A range in uniaxial compressive strength from 60 to 560 psi was noted for badly cemented and clayey conglomerate, 560 to 1,600 psi for firmly cemented conglomerate, and 1,600 - 1,960 psi for strongly cemented conglomerate.
3. The strength of the sandstones depends largely on the nature of the cement, degree of weathering and density of packing. The strengths obtained varied from 150 to 860 psi and are low in relation to fresh unweathered sandstones measured elsewhere.
4. Siltstone strengths ranged from 80 to 520 psi. Clayey siltstone samples with clay layers failed along the layers, and gave very

low compressive strengths varying from 7 to 40 psi. No consistent relationship between unconfined compressive strength and water content was discerned.

5. Claystone strengths varied from 10 to 140 psi and results were very consistent. There is a definite tendency for strength to decrease with increasing water content. Many of these samples were highly bentonitic.

TABLE A4-1

HAT CREEK GEOTECHNICAL STUDY

UNIAXIAL COMPRESSION TEST RESULTS

Sample	Hole No.	Depth ft.	H/Ø	Co Psi	Description
1	76-809	433	1.6	447	Tuffaceous siltstone.
2	76-809	436	2.0	285	Somewhat tuffaceous, bentonitic siltstone.
3	76-809	436	1.6	383	Greenish, highly tuffaceous siltstone.
4	76-809	443	1.9	238	Greenish, highly tuffaceous w. f. grained cement.
5	76-816	752	2.1	856	M. grained, granodioritic sandstone w. coaly debris.
6	76-816	768	2.0	835	M-f grained, coaly sandstone.
7	76-816	768	2.1	766	M-f grained, coaly sandstone.
8	76-816	748	2.0	796	M. grained, grey sandstone.
9	76-816	843	2.3	J3286	Banded basalt w. chlorite amygdales.
10	76-816	?	2.0	1721	Sheared or flow banded volcanic rock.
11	76-816	783	2.0	1924	Sheared or flow banded volcanic rock.
12	76-151	789	1.8	2479	Coal
13	76-151	855	2.0	1495	Coal
14	76-149	1539	1.9	350	Siltstone?
15	76-149	1533	1.9	800	Claystone?
16	76-149	1523	2.2	807	Siltstone?
17	76-809	216	2.1	17	Possible slide plane, bentonitic gravel.
18	76-809	216	2.0	7	Bentonitic claystone w. soft layer.
19	76-809	218	2.1	35	Bentonitic claystone w. soft layer.
20	76-809	218	2.2	42	Bentonitic tuff w. bentonite seams.
21	76-809	130	1.5	114	Carbonaceous bentonitic siltstone.
22	76-809	49	2.1	42	Bentonitic siltstone w. carbonaceous partings.
23	76-809	475	2.1	703	Altered tuffaceous sandstone.
24	76-809	475	2.0	410	Altered tuffaceous sandstone.
25	76-809	462	1.9	239	Altered tuffaceous sandstone.
26	76-809	442	2.1	102	Bentonitic siltstone.
27	76-809	416	2.0	682	Gravelly sandy aggregate of volcanic debris w. zeolite.
28	76-809	401	2.2	519	Tuffaceous silty sandstone.

UNIAXIAL COMPRESSION TEST RESULTS (Continued)

Sample	Hole No.	Depth ft.	H/Ø	Co Psi	Description
29	76-809	402	2.1	466	Tuffaceous silty sandstone.
30	76-809	386	2.0	259	Tuffaceous silty sandstone.
31	76-809	395	2.0	347	Tuffaceous silty sandstone.
32	76-809	371	2.0	1454	Meta-basalt w. pyroclastic layer.
33	76-809	361	2.0	125	Coarse sandstone & bentonitic siltstone, prob. agglomeratic.
34	76-808	45	1.8	57	Carbonaceous siltstone, w. resin beads.
35	76-808	46	2.0	55	Slide debris - carbonaceous, bentonitic, tuffaceous siltstone.
36	76-808	47	2.0	90	As above with carbonaceous debris.
37	76-808	42	1.9	64	Bentonite
38	76-808	25	2.1	104	Bentonitic claystone.
39	76-808	27	2.1	83	Bentonite
40	76-810	115	2.0	57	M. grained, clayey sandstone.
41	76-810	167 ?	2.0	33	Altered tuff.
42	76-814	362	2.0	50	Bentonitic claystone.
43	76-816	641	2.0	1300	Agglomerate
44	76-816	681	2.1	708	Tuffaceous conglomerate-agglomerate.
45	76-816	718	2.1	1005	Tuff-tuffaceous sandstone.
45A	76-816	675	1.7	1952	Tuffaceous sandstone showing graded bedding.
45B	76-816	716	2.0	1036	Tuffaceous sandstone.
46	76-814	363	2.0	107	Claystone.
47	76-814	364	1.9	137	Fine grained tuff.
48	76-814	366	1.9	225	Claystone.
49	76-814	395	2.1	115	Bentonitic tuffaceous, sandy siltstone.
50	76-810	265	2.0	81	Sheared, carbonaceous, clayey siltstone.
51	76-810	218	2.1	229	Tuffaceous, coarse grained siltstone.
52	76-814	462	2.0	290	Tuffaceous, medium grained siltstone.
53	76-810	224	1.9	290	Tuffaceous, medium grained siltstone.
54	76-814	452	2.2	78	Bentonitic, silty claystone.
55	76-814	484	2.2	103	Carbonaceous, clayey siltstone.
56	76-814	596	2.1	484	Tuff w. coal partings.
57	76-814	596	2.2	492	Tuff w. coal partings.

UNIAXIAL COMPRESSION TEST RESULTS (Continued)

Sample	Hole No.	Depth ft.	H/Ø	Co Psi	Description
58	76-814	514	2.1	116	Sheared, carbonaceous siltstone.
59	76-814	555	1.9	158	Sheared, carbonaceous siltstone.
60	76-814	640	1.7	125	Silty claystone.
61	76-814	525	2.2	282	Silty coal.
62	76-814	676	1.8	445	Tuffaceous sandstone.
63	76-814	669	2.0	206	Coal - Failed on sheared bedding.
64	76-811	118	1.7	37	Bentonitic siltstone w. carbonaceous layer.
65	76-811	118 ?	2.0	59	Bentonitic siltstone (dried).
66	76-811	88	2.0	44	Bentonitic siltstone w. coaly parting.
67	76-811	118	2.2	113	Bentonitic siltstone (dried).
68	76-811	88	1.6	47	Bentonitic siltstone w. coaly parting.
69	76-811	118	1.9	80	Bentonitic siltstone (dried).
70	76-811	107	2.0	162	Interbedded, bentonitic sandstone/siltstone.
71	76-811	107	2.1	167	Interbedded, bentonitic sandstone/siltstone.
72	76-811	142	2.0	50	Disturbed bentonitic, silty gravel - slide.
73	76-811	211	2.3	235	Bentonitic, silty sandstone.
74	76-811	70	2.0	40	Bentonitic siltstone w. coaly parting.
75	76-811	265	2.2	174	M-c. grained friable sandstone.
76	76-811	230	2.0	93	Bentonitic, silty sandstone.
77	76-169	388	2.0	2496	D zone - clean durain.
78	76-168	305	2.2	706	D zone - clean durain.
79	76-169	382	1.8	998	D zone - clean durain.
80	76-168	288	2.1	589	Slightly silty coal.
81	76-813	530	2.4	8	Brecciated & sheared, bentonitic siltstone.
82	76-813	575	2.2	325	Bentonitic siltstone.
83	76-813	583	2.4	96	Bentonitic conglomerate.
84	76-813	568	2.2	70	Bentonitic conglomerate.
85	76-813	546	2.3	340	Bentonitic sandstone intact.
86	76-168	408	2.2	599	Vitrain coal sheared.
87	76-168	464	2.0	257	Durain/vitrain silty coal.
88	76-168	368	2.2	817	Silty durain coal.
89	76-169	396	2.2	847	Clairain coal intact.

UNIAXIAL COMPRESSION TEST RESULTS (Continued)

Sample	Hole No.	Depth ft.	H/Ø	Co Psi	Description
90	76-813	601	2.2	325	M. grained sandstone w. coaly parting.
91	76-813	610	2.2	359	Carbonaceous siltstone - Failed along bedding.
92	76-168	656	2.2	1557	Vitrain coal intact.
93	76-813	620	2.3	420	Slightly sheared, carbonaceous siltstone.
94	76-168	607	2.2	1780	Vitrain coal intact.
95	76-168	636	2.0	2405	Slightly silty vitrain coal.
96	76-813	590	2.3	459	Bentonitic f. grained sandstone.
97	76-817	73	2.3	1398	Clairain coal (D).
98	76-817	87	1.9	919	Silty durain coal.
99	76-171	391	2.3	442	Sheared durain & clairain coal.
100	76-168	686	2.3	1694	Vitrain, slightly sheared.
101	76-168	739	2.3	1164	Silty durain intact.
102	76-168	757	2.2	1438	Silty durain intact.
103	76-172	336	2.2	1814	Silty durain intact.
104	76-172	376	2.1	1061	Silty durain intact.
105	76-172	295	2.2	1506	Sheared durain.
106	76-812	72	2.3	53	Bentonitic, sandy siltstone.
107	76-817	201	2.2	805	Silty durain (D).
108	76-817	272	2.5	710	Durain sheared (D).
109	76-817	224	2.3	519	Silty durain & vitrain (D).
110	76-817	415	2.1	1197	Clairain (D).
111	76-812	198	2.2	66	Highly bentonitic, clayey siltstone.
112	76-817	436	2.2	707	Carbonaceous siltstone.
113	76-817	386	2.5	1028	Clairain intact.
114	76-812	123	2.2	133	Bentonitic, silty sandstone, intact.
115	76-812	157	2.0	27	Highly sheared, bentonitic, silty claystone.
116	76-812	112	2.0	38	Claystone?
117	76-812	170	2.2	29	Claystone?
118	76-812	?	2.0	18	Highly sheared, bentonitic, silty claystone.
119	76-812	243	2.1	60	Bentonitic gravel.
120	76-812	294	2.2	172	Slightly tuffaceous sandstone.
121	76-812	285	2.3	83	Bentonitic, sandy siltstone/sandstone intact.
122	76-812	328	2.3	510	Tuffaceous conglomerate.

UNIAXIAL COMPRESSION TEST RESULTS (Continued)

<u>Sample</u>	<u>Hole No.</u>	<u>Depth ft.</u>	<u>H/Ø</u>	<u>Co Psi</u>	<u>Description</u>
123	76-812	346	2.1	276	Bentonitic sandstone.
124	76-812	285	2.2	359	Bentonitic siltstone.
125	76-812	258	2.1	113	Clayey, silty sandstone.
126	76-812	346	2.2	340	Bentonitic sandstone (dried for 17-18 hrs.).
127	76-812	381	2.3	634	Bentonitic tuff.
128	76-812	361	2.2	355	M. grained bentonitic sandstone.
129	76-812	381	2.2	321	Bentonitic conglomeratic tuff.
130	76-812	389	2.2	887	Bentonitic conglomerate.
131	76-812	258	2.3	107	Bentonitic sandstone.
132	76-812	361	2.1	522	M. grained bentonitic sandstone.
133	76-812	346	2.0	738	Bentonitic sandstone (dried for 20 hrs.).
134	76-812	328	2.5	1963	Calcareous cemented.

APPENDIX 5

GEOHYDROLOGIC DATA

APPENDIX 5
GEOHYDROLOGIC DATA

Appendix 5 contains the following information:

- I) Summary hydrologic logs of all holes in which hydrologic installations and tests were made.
- II) Description of procedure used for carrying out in situ falling head permeability tests in standpipe piezometers.
- III) Installation and monitoring of piezometers.
- IV) Cantest Ltd. report on the inorganic chemical analyses of water samples.

1) Summary Hydrologic Logs

1) HYDROLOGIC LOGS

The following logs summarize hydrologic information on selected boreholes where good subsurface hydrologic data has been obtained. The abbreviated lithology is based on data supplied from drillers, core log sheets and drill logs (see Appendix 1).

In order to show all data in a compact log it was necessary to use a number of abbreviations and a symbolic notation. The following notes explain these abbreviations. The note numbers correspond to the numbers shown in parenthesis at the head of each column in the following hydrologic logs:

1. Lithology Abbreviations Used in LogsRock/Soil Type:

Slst = siltstone

Sst = sandstone

Clst = claystone





Congl = conglomerate

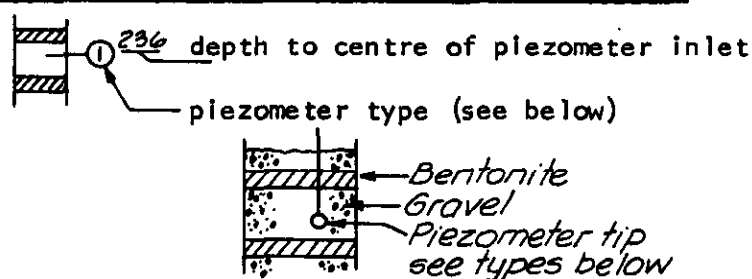
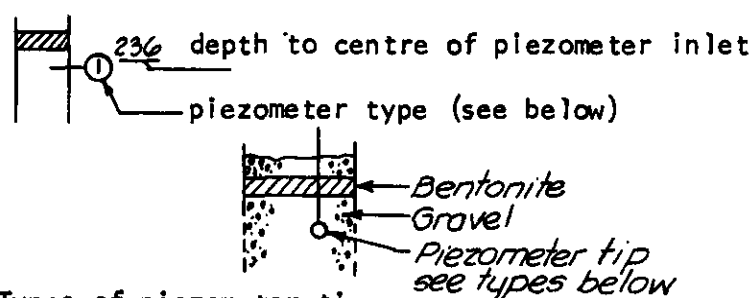
2. Datum

Unless otherwise stated all depth measurements are given in feet relative to existing ground level.

T.D. = total depth drilled.

3. Constructiona) Hole

	drilled hole casing removed
	drilled hole casing left in place
	drilled open hole
	drilled hole known to have squeezed in

Standard Double Seal Piezometer ArrangementStandard Top Seal Piezometer ArrangementTypes of piezometer tip:

- Type 1 - perforated 3/4" ϕ PVC pipe (approx. 5 ft. long)
 - wrapped with permeable fabric
- 2 - Thor pneumatic piezometer
- 3 - Slotted 1.25 in ϕ PVC pipe (approx. 2 ft. long)

b) Types of Backfill (note only fills over 5 ft. thick are shown)

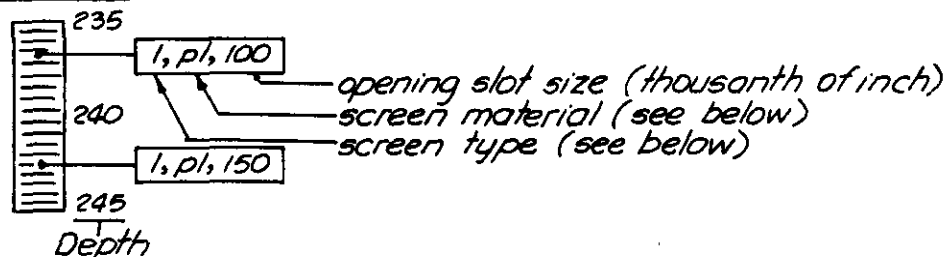
gravel

soil - local material
(undifferentiated)

sand



bentonite

cement
groutc) Well Screen

- Screen Type:
- 1) Continuous wire wound
 - 2) Slotted horizontally
 - 3) Slotted vertically
 - 4) Louvered openings

Screen Material: pl = plastic
 st = steel
 ss = stainless steel

4. WL = Water level measured when drilling had reached indicated depth.

5. WC = Water content of soil, as determined in laboratory (%).

6. Other: fl = water flowing over top of casing
Lw = losing water
Mw = making water
7. SWL = Static water level in piezometer/well after the ground water had recovered from drilling operations (October, 1976).
Positive values indicate artesian heads (i.e. above datum).
These static water levels are equivalent to total piezometric heads in all piezometers.
8. D = Depth range for permeability test
K = Average formation permeability determined (cm/sec)
M = Method used to determine permeability
p = Packer test using falling head method
f = Falling head test in piezometer
w = Pumping test
9. Elevations: are of three types:
Type 1 estimated from plan
Type 2 measured with an altimeter
Type 3 surveyed level

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-134

Sheet 1 of 1

Project Hat Creek Coal Development

Type of Drilling Rotary Core Coordinates E 17991 _____
N 75083 _____

Coordinates E - L799L - - - -

N 75987 - - - -

Rig Longyear 38 Wireline N 5987 _____

Angle from Horizontal 90°

Drilling Fluid Bentonitic Mud Angle from Horizontal 90Bearing ° AzimuthReference Elevation 3334

Type No. ⁽⁹⁾ 3

Type No. _____
_____ Centotechnical

Purpose of Hole Geotechnical

Purpose of Role - Study

[illegible]Contractor Coates Logged by DFE

Date started - 22/6/76 - Checked, by DFW -

Date completed 28/6/76 Date 14/2/77

* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale :
1 in. to 200 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-137
Sheet 1 of 1

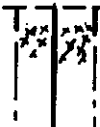


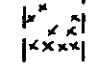

Project Hat Creek Coal Development

Type of Drilling Rotary Core
Rig Longyear 38 Wireline
Drilling Fluid Bentonitic Mud

Coordinates E 17512
N 77027
Angle from Horizontal 90
Bearing ° Azimuth

Reference Elevation 3398
Type No. 3
Purpose of Hole Geotechnical Study

Job No. 176398A

* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling			Comments	
			(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(2)(8) D	(8) K		(8) M
Gravel, Clay	0										
Slst., Sst., Congl.	43										
Grano. Breccia	168										
Slst., Sst., Congl.	198										
	238										
	260										
	320										
Mixed Coal Unit	488										
Coal	732										
	1242										
	T.D.										

↑
Caving
↓

Contractor Coates Logged by DFF
Date started 2/7/76 Checked by DFW
Date completed 9/7/76 Date 14/2/77

* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
1 in. to 300 ft.

Sheet 1 of 2

Purpose of Hole Geotechnical
Study

Caving

Vertical scale :
1 in. to 100 ft.

DRILLHOLE No. 76-138
Sheet 2 of 2

Sheet 2 of 2

Vertical scale: 1 in. to 100 ft.

Golder Associates

Sheet 1 of 1.

Study

Squeezing

Vertical scale :
1 in. to 200 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-143

Sheet 1 of 1.

Project Hat Creek Coal Development

Type of Drilling Rotary Core

Coordinates E _ _ J9028

N 82027

Rig -- Longyear 38 Wireline

Angle from Horizontal 90

Drilling Fluid Bentonitic Mud

Bearing ° Azimuth

Reference Elevation 2896

Type No. ⁽⁹⁾ _____

Purpose of Hole Geotechnical
StudyJob No. V76348-A

* (1) Lithology	(2) Depth	(2)(3) Completed Construction	(2) During Drilling				After Drilling				Comments
			(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(2)(8) D _z (8)	K (8)	M (8)	
Gravel, Clay	0 30 32										
Clst.	56 80										
Slst., Sst.	337 351 362	 ① 348 T.D.				-72					

Contractor Coates Logged by RFF

Date started 15/7/76 Checked by BEW

Date completed 18/7/76 Date 14/2/77

* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale :
1 in. to 50 ft.

Vertical scale:
1 in. to 200 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-146

Sheet 1 of 1

Project Hat Creek Coal Development

Type of Drilling Rotary Core Coordinates E 18921 ---
N 81518

Coordinates E - 1892 L - - - -

Rq Longyear 38. Wireline N-81518-2000

N 81518 7 1 1

Drilling Fluid Bentonitic Mud Angle from Horizontal 90

Angle from Horizontal 90°

Bearing ~ ~ ~ ~ ~ ° Azimuth

Reference Elevation 2857

Type No. ⁽⁹⁾ 3

Purpose of Hole Geotechnical

Study

[illegible]

Contractor Coates — — Logged by DFD —

Date started 18/7/76 Checked by DFW

Date completed 20/7/76 Date 14/2/77

* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale :
1 in. to 50 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-148

Sheet 1 of 1.

Project Hat Creek Coal DevelopmentType of Drilling Rotary CoreCoordinates E _ _ _ 17977

N 80521

Rig __ Longyear 38 Wireline

Angle from Horizontal 90°

Drilling Fluid - Bentonitic Mud

Bearing ° Azimuth

Reference Elevation 2969

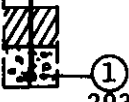
Type No. 3

Purpose of Hole Geotechnical

Purpose of Role Study

Study

Job No. Y76398-B

* (1) Lithology	(2) Depth	Completed Construction	During Drilling				After Drilling				Comments
			(3) Depth	(2)(4) W.L.	(5) W.C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(2)(8) D	(8) K	(9) M	
Gravel, Clay	0										
	57	3½"									
Clay	110										
		3"									
	231										
Clst., Sst., Congl.											
	284										
	295	T.D.					-150				

Contractor Coates Logged by DFE

Date started 21/7/76 Checked by DEF

Date completed 22/7/76 Date 14/2/77

* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale :
1 in. to 50 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-149

Sheet 1 of 1

Project -- Hat Creek Coal Development

Type of Drilling Rotary Core

Coordinates E _ _ 19003

Rig Longyear 38 Wireline

N 75981

Drilling Fluid Natural Mud

Angle from Horizontal 90

Bearing ° AzimuthReference Elevation 3267

Type No. ⁽⁹⁾ 3

Purpose of Hole _ Geotechnical

Study

Study

Job No. 176348-D

(1) Lithology	(2) Depth	(3) Completed Construction	During Drilling				After Drilling				Comments
			(2)	(2) (4)	(5)	(6)	(2) (7)	Permeability			
			Depth	W.L.	W.C.	Other	S.W.L.	D(2)(8)	K (8)	M (8)	
Gravel, Clay	0 115 177	<p>3½"</p> <p>②</p> <p>120</p>					-51				
Slst.	596	3"									
Coal	782										
Slst.	827										
Coal	1314										
Slst., Sst.	1488 T.D. 1547	<p>①</p> <p>1506</p>					-81				

Contractor Coates — Logged by DFE —

Date started 22/7/76 Checked by DFW

Date completed 28/7/76 Date 14/2/77

* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale :
1 in. to 200 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-150
Sheet 1 of 2

Project Hat Creek Coal Development

Type of Drilling Rotary Core

Rig Longyear 38 Wireline

Drilling Fluid Bentonitic Mud

Coordinates E 18517

N 81006

Angle from Horizontal 90

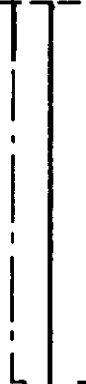

Bearing ° Azimuth

Reference Elevation 2891

Type No. 3

Purpose of Hole Geotechnical Study

Job No. V76348A

* (1) Lithology	(2) Depth	(2) (3) Completed Construction	During Drilling				After Drilling				Comments
			(2) Depth	(2) (4) W. L.	(5) W. C.	(6) Other	(2) (7) S.W.L.	Permeability			
								(2) (8) D (2) (8)	(8) K (8)	(8) M (8)	
Gravel, Clay	0										
	100										
Clst., Sst., Slst.	112										
	220										

Contractor Coates Logged by DEF

Date started 23/7/76 Checked by DEF

Date completed 24/7/76 Date 14/2/77


*NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
1 in. to 50 ft.

SUMMARY HYDROLOGIC LOG (Continued)

DRILLHOLE No. 76-150
Sheet -2- of -2-

Job No.	(1) Lithology	(2) Depth	(2) (3) Completed Construction	During Drilling				After Drilling			Comments	
				(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) SWL.	Permeability			
									(2)(8) D (2)(8)	K (8)		M (8)
	Clst., Sst., Slst.	406 414	T.D.  ① 411					-251				

Vertical scale: 1 in. to 50 ft.

Golder Associates

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-151

Sheet 1 of 1

Project Hat Creek Coal DevelopmentType of Drilling Rotary CoreCoordinates E 20996

Rig Longyear 38 Wireline

N 78484

Drilling Fluid Bentonitic Mud

Angle from Horizontal 90°

Bearing ° AzimuthReference Elevation 3019Type No. ⁽⁹⁾ 3

Geotechnical

Purpose of Hole - Study

[illegible]

Contractor Coates — Logged by DFP —

Date started 25/7/76 Checked by DFW

Date completed 28/7/76 Date 14/2/77

*NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale :
1 in. to 200 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-155

Sheet 1 of 1

Project Har Creek Coal Development

Type of Drilling Rotary Core

Coordinates E 19485

Rig Longyear 38 Wireline

N 77989

Drilling Fluid Bentonitic Mud

Angle from Horizontal 90°


Bearing --- ° Azimuth

Reference Elevation 3167

Type No. 3

Purpose of Hole Geotechnical Study

Job No. V762902

* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling			Comments	
			(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(2)(8) D	(8) K		(8) M
	0										
Sand, Gravel	82	 (1) 88 3 1/2"					-61				
	90										
	187										
	200										

Contractor Coates Logged by DFW
 Date started 30/7/76 Checked by DFW
 Date completed 4/8/76 Date 14/2/77

*NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
1 in. to 100 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-156

Sheet 1 of 2

Project Hat Creek Coal Development

Type of Drilling Rotary Core Coordinates E 21029

Rig Longyear 38 Wireline N 81484

Drilling Fluid Bentonitic Mud Angle from Horizontal 90°

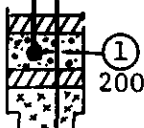
Bearing ° Azimuth

Reference Elevation 3034

Type No. 3

Purpose of Hole Geotechnical Study

Job No. Y76298A

* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling				Comments
			(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability			
								D(2)(8)	K (8)	M (8)	
Sand, Gravel, Clay	0									No water in piezometer.	
	190										
	204										
	216										
Coal											

Contractor Coates Logged by DFW

Date started 2/8/76 Checked by DFW

Date completed 4/8/76 Date 14/2/77

* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
1 in. to 50 ft.

DRILLHOLE No. 76-156
Sheet 2 of 2

DRILLHOLE No. 76-156
Sheet 2 of 2

Vertical scale: 1 in. to 50 ft.

Golder Associates

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-158

Sheet 1 of 1


Project Hat Creek Coal Development

Type of Drilling Rotary Core
Rig Longyear 38 Wireline
Drilling Fluid Bentonitic Mud

Coordinates E 17907
N 79004
Angle from Horizontal 90°
Bearing - ° Azimuth

Reference Elevation 3217
Type No. ⁽⁹⁾ 3
Purpose of Hole Geotechnical
Study

Job No. Y76348-2

* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling			Comments	
			(2) Depth	(2)(4) W.L.	(5) W.C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(2)(8) D	(8) K		(8) M
Sand, Gravel	0										
Slst.	60										
	123										
	160										
Carb. Slst.	386										
Coal	607										
Sst., Slst., Congl.	752										
	773	T.D.									
		761									

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-160

Sheet -1- of -1-.

Project Hat Creek Coal DevelopmentType of Drilling Rotary CoreCoordinates E 21022

Rig Longyear 38 Wireline

N 81999

Angle from Horizontal 90°



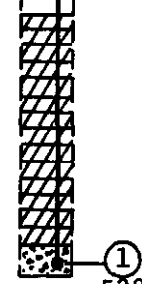

Drilling Fluid Bentonitic Muc

Bearing ° Azimuth

Reference Elevation 3035

Type No. ⁽⁹⁾ 3

Purpose of Hole GeotechnicalPurpose of Hole Study

* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling				Comments
			(2) Depth	(2)(4) W.L.	(5) W.C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(2)(8) D	(8) K	(8) M	
Sand, Gravel	0										
	195 205 238			-183							
Carb. Clst.	474 496										
Slst.	519 536			-190							

Contractor Coates — — Logged by DFP — —
Date started 9/8/76 Checked by DFW — —
Date completed 10/8/76 Date 14/2/77 — —

* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
1 in. to 200 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-161

Sheet 1 of 2

Project Hat Creek Coal Development

Type of Drilling Rotary Core Coordinates E 8526
N 80010

Coordinates E 18526

N 80012

Rlg Longyear 38 Wireline

N 80012

Angle from Horizontal 90°

Bearing _____ ° Azimuth _____

Reference Elevation 3132

Type No. ⁽⁹⁾ 3

Purpose of Hole Geotechnical

Study

[illegible]Contractor Coates — — Logged by DEF — —

Date started 10/8/76 Checked by DFW

Date completed 13/8/76 Date 14/2/77


* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale :
1 in. to 100 ft.

SUMMARY HYDROLOGIC LOG (Continued)

DRILLHOLE No. 76-161
Sheet 2 of 2

Job No.	(1) Lithology	(2) Depth	(2) (3) Completed Construction	During Drilling				After Drilling			Comments	
				(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) SWL.	Permeability			
									(2)(8) K (8)	M (8)		
	Slst., Sat., Congl., Clst.	817 853	 T.D. 842					-200				

Vertical scale: 1 in. to 100 ft.

Golder Associates

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-163
Sheet - 1 - of - 2 -

Project Hat Creek Coal Development-----

Type of Drilling Rotary Core Coordinates E 21035
N 82501

Rk Longyear 38 Wireline N 6210 90

Drilling Fluid Bentonitic Mud Angle from Horizontal 20



Bearing _____° Azimuth _____

Reference Elevation 3037 - -

Type No. ⁽⁹⁾ 3

Purpose of Hole Geotechnical

Purpose of Note = Study

(1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling				Comments
			(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(2)(8) D	(8) K	(8) M	
Sand, Clay	0										
Coal	270 276						-225				Standpipe blocked. Reading as of 31/08/76.

Contractor Coates Logged by DFP
Date started 11/8/76 Checked by DFW
Date completed 13/8/76 Date 14/2/77

* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

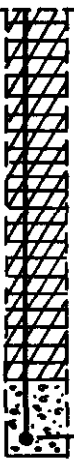
Golder Associates

Vertical scale :
1 in. to 50 ft.

SUMMARY HYDROLOGIC LOG (Continued)

DRILLHOLE No. 76-163

Sheet 2 of 2

Job No.	(1) Lithology	(2) Depth	(2) (3) Completed Construction	During Drilling				After Drilling			Comments	
				(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) SWL.	Permeability			
									(2)(8) K	(8) M		(6)
	Coal	438										
	Clst., Slst., Congl.	497										
		516		T.D.				-212				Standpipe blocked. Reading as of 31/08/76.

Vertical scale: 1 in. to 50 ft.

Golder Associates

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-168

Sheet 1 of 2

Project Hat Creek Coal Development-----

Type of Drilling Rotary Core Coordinates E 2469
N 7090

Coordinates E - 21469 - - -

Rig Longyear_38 Wireline_ N_79994 80

N 79994 - 8 - -

Angle from Horizontal 90°

Drilling Fluid Bentonitic Mud

Bearing ° AzimuthReference Elevation 2941 - -

Type No. ⁽⁹⁾ 3

Purpose of Hole Geotechnical

Purpose of Note - Study

[illegible]

Contractor Coates Logged by DFP
Date started 18/8/76 Checked by DFW
Date completed 23/8/76 Date 14/2/77

*NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale :
1 in. to 100 ft.

SUMMARY HYDROLOGIC LOG (Continued)

DRILLHOLE No. 76-168

Sheet 2 _ _ of _ 2 _

Job No.	(1) Lithology	(2) Depth	(2) (3) Completed Construction	During Drilling				After Drilling			Comments	
				(2) Depth	(2) (4) W. L.	(5) W. C.	(6) Other	(2) (7) SW.L.	Permeability			
									(2) (8) X	K (8)		M (8)
	Clst., Slst., Congl.	846	T.D. <div></div>									

Vertical scale: 1 in. to 100 ft.

Golder Associates

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-801

Sheet 1 of 2.

Project	Hat Creek Coal Development
----------------	-----------------------------------

Type of Drilling Rotary CoreCoordinates E 21326Rig Longyear 44 Wireline

N 73377

Reference Elevation 3228 - - -

Type No. ⁽⁹⁾ 3

Drilling Fluid Natural Mud__

Angle from Horizontal 90°

Purpose of Hole Geotecnica

Bearing ° Azimuth

Purpose of Visit _____
Study _____

Study

* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling				Comments
			(2) Depth	(2)(4) W.L.	(5) W.C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(2)(8) D	(8) K	(8) M	
Till	0										
	52	x x x x									
	64										
Sand, Silt					24						
					25						
	110	4 1/2"			21						
					21						
	140										
					20						
					23						
Till											
			220		10	MW					Mud being diluted.
					35						
					26						
	274	3 3/4"									
	330					MW					
Slst., Clst.											
	380				33						
		395 ①									

Contractor Tonto -- -- Logged by DFE --

Date started 4/6/76 Checked by DFW

Date completed 14/6/76 Date 14/2/77

* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale :
1 in. to 50 ft.

SUMMARY HYDROLOGIC LOG (Continued)

DRILLHOLE No. 76-801

Sheet 2 of 2

Job No.	(1) Lithology	(2) Depth	(2) (3) Completed Construction	During Drilling				After Drilling			Comments	
				(2) Depth	(2) (4) W. L.	(5) W. C.	(6) Other	(2) (7) SWL.	Permeability			
									(2) (8) X	K (8)		M (8)
	Slst., Clst.	600	T.D. <div>398 3"</div>	570	0						High water pressure.	

Vertical scale: 1 in. to 50 ft.

Golder Associates

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-802

Sheet 1 of 2

Project Hat Creek Coal Development

Type of Drilling Rotary CoreCoordinates E 15985Rig Longyear 44 Wireline

N 73261

Drilling Fluid Natural Mud

Angle from Horizontal 90°

Bearing ° AzimuthReference Elevation 3500

Type No. ^(a) 3

Purpose of Hole Getechnical

Study

[illegible]

Contractor Tonto -- -- Logged by DFW
Date started 6/6/76 -- -- Checked by DFW
Date completed 14/6/76 Date 14/2/77

* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

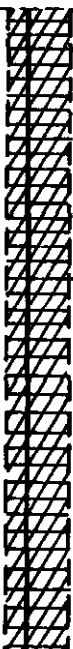


Golder Associates

Vertical scale :
1 in. to 50 ft.

SUMMARY HYDROLOGIC LOG (Continued)

DRILLHOLE No. 76-802
Sheet 2 of 2

Job No.

(1) Lithology	(2) Depth	(2) (3) Completed Construction	During Drilling				After Drilling				Comments
			(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) SWL.	Permeability			
								(2)(8) K (8)	M (8)		
Slst., Sst. Congl.			420			MW					
			465			MW					
			490			MW					
	570	 3 3/4"				MW					
	590	T.D.  578					+11				Squeezing Standpipe with pneumatic piezo- meter connected to top.

Vertical scale: 1 in. to 50 ft.

Golder Associates

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-803

Sheet 1 of 2.

Project Hat Creek Coal Development

Type of Drilling Rotary Core Coordinates E 20390
N 75100

Coordinates E 20390

Rig Longyear 44 Wireline N 5190
750

N 75190 8 1

Drilling Fluid Natural Mud Angle from Horizontal 12

Angle from Horizontal 75°

Bearing 145° Azimuth

Reference Elevation 3169

Type No. ⁽⁹⁾ 3

Purpose of Hole Geotechnical

Study

* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling				Comments
			(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(2)(8) D	(8) K	(8) M	
Till	0										
	25	x x x									
Clayey Slst.	58	①									
	68	66									
	105										
		</									

Contractor Tonto - - - - - Logged by DFP -
Date started 16/6/76 - - - - - Checked by DFW -
Date completed 23/6/76 - - - - - Date 14/2/77 -

*NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale :
1 in. to 50 ft.

DRILLHOLE No. 76-803
Sheet - 2 - of - 2 -

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-804
Sheet 1 of 2

Project Hat Creek Coal Development

Type of Drilling Rotary Core
Rig Longyear 44 Wireline
Drilling Fluid Natural Mud

Coordinates E 15097
N 75863
Angle from Horizontal 90°
Bearing - ° Azimuth

Reference Elevation 3531
Type No. 3
Purpose of Hole Geotechnical Study

Job No.

* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling				Comments
			(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(X2)(8)	K (8)	M (8)	
Till	0										
	35	①					-27				
	45	40									
Slst. Breccia			65		50	LW					Caving
	111		106			LW					Squeezing
Sst.	123										
			4½"								
	165				14						
			225		24	LW					Caving
					44						
					12						
					18						
					20						
					26						
	330				12						
			350		12						
	361				12						
					27						
	382	②			34	MW					Piezometer not operational.
		381									

Contractor Tonto
Date started 16/6/76
Date completed 23/6/76

Logged by DFF
Checked by DEW
Date 14/2/77

* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
1 in. to 50 ft.

SUMMARY HYDROLOGIC LOG (Continued)

DRILLHOLE No. 76-804

Sheet 2 of 2

Job No.	(1) Lithology	(2) Depth	(2) (3) Completed Construction	During Drilling				After Drilling				Comments
				(2) Depth	(2) (4) W. L	(5) W. C.	(6) Other	(2) (7) SWL.	Permeability			
									(2) (8) K	(8) M	(8) M	
	Slst., Sst., Congl.	437	T.D. <div style="border: 1px solid black; width: 30px; height: 30px; display: inline-block; vertical-align: middle;"></div> 3"			29 17 18	MW ↓					

Vertical scale: 1 in. to 50 ft.

Golder Associates

Sheet 1 of 1

Type of Drilling Rotary Core Coordinates E 14429
Rig Longyear 44 Wireline N 79253
Drilling Fluid Natural Mud Angle from Horizontal 75
Bearing 270 ° Azimuth

Type No. ⁽⁹⁾ 3

Purpose of Hole Geotechnical Study

Contractor Ionto -- Logged by DFF
Date started 26/6/76 -- Checked by DWF
Date completed 29/6/76 -- Date 2/14/77

* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale :
1 in. to 50 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-806

Sheet 1 of 2

Project Hat Creek Coal DevelopmentType of Drilling Rotary Core

Coordinates E__J6108

Rig Longyear 44 Wireline

N 79182

Drilling Fluid Natural Mud

Angle from Horizontal 90

Bearing ° Azimuth

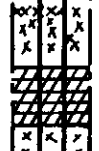
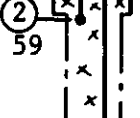
Reference Elevation 3377

Type No. ⁽⁹⁾ 3

Purpose of Hole Geotechnical Study _____

Study

Job No.

* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling			Comments	
			(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(2)(8) D	(8) K		(8) M
Till	0										
	16										
			25		31						
					52						
	60				28		-20				
					38						
					79						
					33						
					32						
					58						
							LW				
					32						
					34						
					34						
					31						
					53						
					31						
		3 3/4"	225								
					33						
					31						
					28						
					20						
	280										
					23						
					24						
					26						
					30						
					25						
					31						
					20						
		3"									
					37						
					29						
			400	0	32						

Contractor Tonto Logged by DFF

Date started 25/6/76 Checked by DEW




Date completed 6/7/76 Date 2/14/77

※ NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale :
1 in. to 50 ft.

DRILLHOLE No. 76-806
Sheet 2 of 2

Job No.	(1) Lithology	(2) Depth	(2) (3) Completed Construction	During Drilling				After Drilling				Comments
				(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) SWL.	Permeability			
									(2)(8)	K (8)	M (8)	
						30						
						26						
						27						
	Clayey Slst. (Sst., Congl.)	454				31						
		468		465	0	26		-35				
						30						
						28						
						27						
						36						
		542				35						
						</						

Vertical scale: 1 in. to 50 ft.

Golder Associates

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-807

Sheet 1 of 1

Project Hat Creek Coal Development

Type of Drilling Rotary Core

Coordinates E _ _ 12426

N 78106

Rig Longyear 44 Wireline

Angle from Horizontal 90°

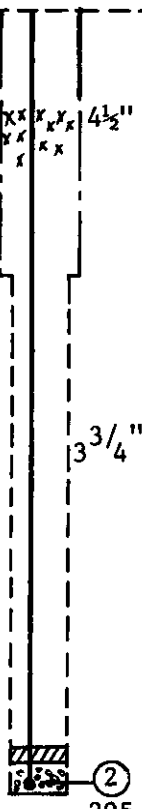

Drilling Fluid Natural MudBearing ° Azimuth Reference Elevation 3558

Type No. ⁽⁹⁾ _____ 3

Purpose of Hole Geotechnical

Purpose of this Study

Job No.

* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling				Comments	
			(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability				
								(2)(8) D	(8) K	(8) M		
Sand, Till, Sheared Material	0				20						Sheared zone 114-135.	
	27		40	-15	27	MW						
					26							
					33							
	70	70	-5		MW							
Clayey Sst., Sst.	83	80	-30									
		90	-5									
Clay, Silt, Coal	120			17								
				21								
Sst.	145			25								
				13								
				24								
				17								
	197	180	0									
	209	T.D.  ② 205				-44						

Contractor Tonto
Date started 6/7/76
Date completed 10/7/76

Logged by DFW
Checked by DFW
Date 2/14/77

*NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
1 in. to 50 ft.


Sheet 1 of 2

Study

No. of Job

Vertical scale :
1 in. to 50 ft.

DRILLHOLE No. 76-808
Sheet - 2 - of - 2 -

Sheet - 2 - of - 2 -												
Job No.	(1) Lithology	(2) Depth	(2) (3) Completed Construction	During Drilling				After Drilling			Comments	
				(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(7)(8) SWL.	Permeability			
									(2)(9) K (ft)	(3) M (ft)		(4) M (ft)
	Slst.					31						
						36						
						30						
						32						
						32						
						43						
						25						
						34						
						30						
						83						
		561 — 574 T.D.		540	-10			-186				
			① 570									

Vertical scale: 1 in. to 50 ft.

Golder Associates

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-809

Sheet 1 of 2

Project Hat Creek Coal Development

Type of Drilling Rotary Core

Coordinates E 17230

Rig Longyear 44 Wireline

N 82036

Drilling Fluid Natural Mud

Angle from Horizontal 90°

Bearing - ° Azimuth

Reference Elevation 3079

Type No. 3

Purpose of Hole Geotechnical Study

Job No.	* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling				Comments
				(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability			
									(2)(8) D (ft)	K (ft)	M (ft)	
	Sand, Gravel	0										
		15				32						
						42						
	Sheared Bentonite	35	① 33				LW	-22				
				50	0	38						
		64				27						
						31						
				95	0							
						34						
	Slst.					31						
						4 1/2"						
				160	-6	46						
						36						
						38						
		205		205	0							
						19						
						30						
						36						
						17						
				270	-11							
						25						
						31						
						24						
						30						
	Congl., (Slst., Sst.)					3 3/4"						
				330	0							
						34						
				370	0							
						30						
						20						

Contractor Tonto
 Date started 22/7/76
 Date completed 27/7/76

Logged by DFF
 Checked by DFW
 Date 2/14/77

* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

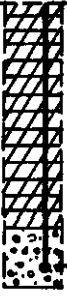
Golder Associates

Vertical scale:
 1 in. to 50 ft.

SUMMARY HYDROLOGIC LOG (Continued)

DRILLHOLE No. 76-809

Sheet 2 of 2

Job No.	(1) Lithology	(2) Depth	(2) (3) Completed Construction	During Drilling				After Drilling				Comments
				(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) SWL	Permeability			
									(2)(8) Q	(8) K	(8) M	
				406	0							
				429	0							
		459				25						
		474	T.D.			28		-62				
			① 470									

Vertical scale: lin. to 50 ft.

Golder Associates

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-810

Sheet 1 of 1

Project Hat Creek Coal Development

Type of Drilling Rotary Core

Coordinates E 16337

Reference Elevation 3024

Rig Longyear 44 Wireline

N 83287

Type No. 3

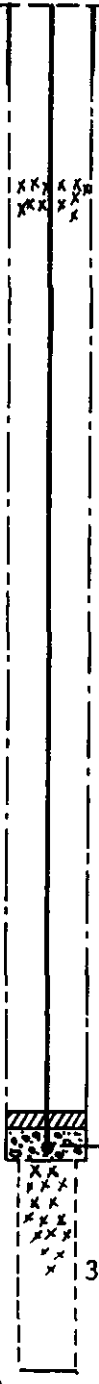

Drilling Fluid Natural Mud

Angle from Horizontal 90°

Purpose of Hole Geotechnical Study

Bearing - ° Azimuth

Job No.

(1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling				Comments
			(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(2)(8) D	(8) K	(8) M	
	0										
Sand, Gravel, Till	45		60	-12	25	LW					
			120		46	LW					
			185	-25							
	217		220	-25							
Sheared Slst.					37						
	277			-43		LW					
Congl.	292									Piezometer not operational.	
	300	299									
Sst.	314									Squeezing.	
	329	3 3/4"									
Gravel, Congl.						MW					
	354	T.D.									

Contractor Tonto
 Date started 3/8/76
 Date completed 10/8/76

Logged by DFF
 Checked by DFW
 Date 14/2/77

*NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
 1 in. to 50 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-811

Sheet 1 of 1

Project Hat Creek Coal Development

Type of Drilling Rotary Core

Coordinates E 18100

Reference Elevation 2949

Rig Longyear 44 Wireline

N 82543

Type No. 3

Drilling Fluid Natural Mud

Angle from Horizontal 90

Purpose of Hole Geotechnical Study

Bearing - ° Azimuth

Job No.

(1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling				Comments
			(3) Depth	(4) W. L.	(5) W. C.	(6) Other	(7) S.W.L.	Permeability			
								(8) D (248)	(9) K (8)	(10) M (8)	
Sand, Gravel	0	4 1/2"									
Bentonite	13										
	20				LW						
					34						
					29						
Slst.					31						
					37						
	107										
Slst., Sst.			120	0	36						
		3 3/4"									
Congl.	147										
	155										
Slst.					38						
	167										
Congl.			190	0							
	200				26						
					38						
					27						
Slst., Congl.			290	-14							
					24						
					33						
			365	0							
	381										
	398	T.D.					-31				
		①	395								

Contractor Tonto

Logged by DFW

NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Date started 16/8/76

Checked by DFW

Golder Associates

Date completed 18/8/76

Date 14/2/77

Vertical scale:
1 in. to 50 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-812

Sheet 1 of 1

Project Hat Creek Coal Development

Type of Drilling Rotary Core

Coordinates E 19028

Reference Elevation 2823

Rig Longyear 44 Wireline

N 82998

Type No. 3

Drilling Fluid Natural Mud

Angle from Horizontal 90°

Purpose of Hole Geotechnical

Bearing ° Azimuth

Study

Job No.

* (1) Lithology	(2) Depth	Completed Construction (2)(3)	During Drilling				After Drilling				Comments
			(2) Depth	(3)(4) W. L.	(5) W. C.	(6) Other	(7) S.W.L.	Permeability			
								(2)(8) D (20)	(8) K (6)	(9) M (6)	
Till	0	4 1/2"	10	0							
Slst., Sst., Congl.	46				43 34 34						
	85				29	↑ LW ↓					
Carb. Slst.					30 30 35						
	180	3 3/4"			30 31						
			215	-5	32 31						
Slst., Sst., Congl.	250			-13	33 24						
		3"	290	0	28						
	317				27						
	330	1 325			27 27		-15				
			350	-5	27 28						
	398 T.D.										

Caving

Contractor Tonto Logged by DFW
 Date started 24/8/76 Checked by DFW
 Date completed 28/8/76 Date 14/2/77

*NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
1 in. to 50 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-813

Sheet 1 of 2

Project Hat Creek Coal Development

Type of Drilling Rotary Core

Coordinates E 19058

Rig Longyear 44 Wireline

N 84552

Reference Elevation 2881

Type No. 3

Drilling Fluid Natural Mud



Angle from Horizontal 90°

Purpose of Hole Geotechnical

Bearing ° Azimuth

Study

Job No.

(1) Lithology	(2) Depth	(3) Completed Construction	During Drilling				After Drilling				Comments
			(4) Depth	(5) W. L.	(6) W. C.	(7) Other	(8) S.W.L.	Permeability			
								(9) D (10)	(11) K (12)	(13) M (14)	
T111	0 20		15	-2							
			130	0							
			235	0							
			365 367	0 -31							
	373 387		382 395	-14			-128				

Contractor Tonto
 Date started 15/8/76
 Date completed 22/8/76
 Logged by DFF
 Checked by DFW
 Date 14/2/77

*NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
 1 in. to 50 ft.

SUMMARY HYDROLOGIC LOG (Continued)

DRILLHOLE No. 76-813
Sheet 2 of 2

Job No.

(1) Lithology	(2) Depth	(2) (3) Completed Construction	During Drilling				After Drilling				Comments
			(2) Depth	(3) (4) W. L.	(5) W. C.	(6) Other	(2) (7) SWL.	Permeability			
								(2) (8) K	(8) M	(9)	
Till	518	<div>xx xx x</div>	440	-133							
			490	-3							
			520	-43	29						
Clayey Slst.	580	3"			28						
					28						
					32						
Slst., Sst., Congl.	609		585	-4	29						
					23						
Slst., (Sst.)	655	T.D.	630	0	31						
					27						
						LW					Caving Squeezing

Vertical scale: 1 in. to 50 ft.

Golder Associates

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-814
Sheet 1 of 2

Project Hat Creek Coal Development-----

Type of Drilling Rotary Core Coordinates E 20041
N 83506

Rig Longyear 44 Wireline N 05200 _____

Drilling Fluid Natural Mud --- Angle from Horizontal --90-- ---Bearing ° AzimuthReference Elevation 2970 - -

Type No. ⁽⁹⁾ 3

Purpose of Hole Geotechnical Study

No. 907

* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling				Comments
			(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(2)(8) D	(8) K	(8) M	
T111	0										
	180		125	-11							
			195	-52							
			290	-12							
	328										
Slst., Clst.	336	① 332					-176				
	341		350	-14	24						
			360	-28	33						
			370	-7	36						
	400				30						

Contractor Tonto Logged by DFF
Date started 8/8/76 Checked by DFW
Date completed 13/8/76 Date 14/2/77

* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale :
1 in. to 50 ft.

SUMMARY HYDROLOGIC LOG (Continued)

DRILLHOLE No. 76-814
Sheet 2 of 2

Job No.	(1) Lithology	(2) Depth	(2) (3) Completed Construction	During Drilling				After Drilling				Comments
				(2) Depth	(2) (4) W. L.	(5) W. C.	(6) Other	(2) (7) SWL.	Permeability			
									(2) (8) K	(9) K	(10) M	
				415	-4	26						Caving
				435		24 33 31 32						
		485		470	-8	20 32						
				500	0	26 24 25						
	Slst., Coal			550	-11	26 25 25 24						
		645		620	-6	23 23 27						
	Slst., Sst., Coal	679										
		700	T.D.		-12			-48				
			① 696									

Vertical scale: 1 in. to 50 ft.

Golder Associates

Vertical scale: lin. to 50 ft.

Golder Associates

Sheet 1 of 2

Purpose of Hole - geotechnical Study

Vertical scale :
1 in. to 50 ft.

SUMMARY HYDROLOGIC LOG (Continued)

DRILLHOLE No. 76-815

Sheet - 2 - of - 2 -

Job No.	(1) Lithology	(2) Depth	(2) (3) Completed Construction	During Drilling				After Drilling			Comments	
				(2) Depth	(2) (4) W. L.	(5) W. C.	(6) Other	(2) (7) SWL.	Permeability			
									(2) (8) D (2) (8)	K (8)		M (8)
		402			30							
					37							
					35							
					20							
					33							
					17							
				455	-63	33						
						40						
						28						
						34						
						29						
				515	-45	31						
						34						
						30						
						19						
	Clayey Slst.					30						
						35						
						29						
				585	-24	11						
		609				33	LW				Squeezing	
		624	①			33		-305				
		621				35						
				645	-20	30						
						35						
		673 T.D.				-68						

Vertical scale: 1 in. to 50 ft.

Golder Associates

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-816

Sheet 1 of 3

Project Hat Creek Coal Development

Type of Drilling Rotary Core Coordinates E 24624

Rig Longyear 44 Wireline N 78956

Drilling Fluid Natural Mud Angle from Horizontal 75°

Bearing ° Azimuth

Reference Elevation 3249

Type No. 3

Purpose of Hole Geotechnical

Study

Job No.	* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling				Comments
				(2) Depth	(2)(4) W.L.	(5) W.C.	(6) Other	(2)(7) S.W.L.	Permeability			
									Dz (8)	K (8)	M (8)	
		0										
				50	-2							
		132	x x x x x x x x x x									
	Sand, Gravel, Till		4 1/2"	155	-2							
		250			-104							
				270	-40							
				290	-20	20						
			3 3/4"			30						
		312										
		326	①			37		-152				
		338	327	340	-10	29						
						25						
						25						
						27						
						23						
	Clayey Slst.			390	-7							

Contractor Tonto Logged by DFW

Date started 18/7/76 Checked by DFW

Date completed 28/7/76 Date 14/2/77



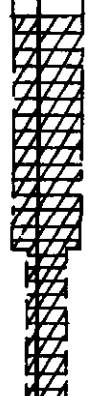

* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
1 in. to 50 ft.

DRILLHOLE No. 76-816
Sheet - 2 of 3 --

Sheet 2 of 3


Job No.	(1) Lithology	(2) Depth	(2) (3) Completed Construction	During Drilling				After Drilling				Comments	
				(2) Depth	(2) (4) W. L.	(5) W. C.	(6) Other	(2) (7) SWL.	(7) Permeability				
									(2) (8) K	(8) M	(8) M		
	Clayey Sst.					22							
						31							
				430	-136	24							
						30							
						28							
		499				32							
				500	-154								
Congl.	650		590	-158									
			650	-33									
Congl., (Sst.)	751		750	-9									
			776										
Basalt				815	-4								

Vertical scale: 1 in. to 50 ft.
Golder Associates

SUMMARY HYDROLOGIC LOG (Continued)

DRILLHOLE No. 76-816
Sheet 3 of 3

Job No.

(1) Lithology	(2) Depth	(2) (3) Completed Construction	During Drilling				After Drilling			Comments	
			(2) Depth	(3) (4) W. L.	(5) W. C.	(6) Other	(2) (7) SWL.	Permeability			
								(2) (8) D (2) (8)	K (8)		M (8)
Basalt	867 884	 T.D. 873	875	-31			-215				

Vertical scale: 1 in. to 50 ft.

Golder Associates

Sheet 1 of 2

Study

Job.

Sheet - 2 - of - 2 -

Golder Associates

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-819

Sheet 1 of 1

Project Hat Creek Coal Development

Type of Drilling Rotary Core

Coordinates E 15716

Rig Longyear 44 Wireline

N 83733

Drilling Fluid Natural Mud

Angle from Horizontal 90



Bearing ° Azimuth

Reference Elevation 2930

Type No. 3

Purpose of Hole Geotechnical Study

Job No.

* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling				Comments
			(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(2)(8) D	(8) K	(8) M	
Sand, Gravel, Till	0		35	0							Hole uncased when W.L. reading taken. High mud pressure.
	20		80	-15							
	164		150	-34							
	214		224	222							
Slst., Sst.	246		265			MW					
	319		T.D.								

Hole uncased when W.L. reading taken.

High mud pressure.

Contractor Tonto Logged by DFF
 Date started 29/8/76 Checked by DFW
 Date completed 2/9/76 Date 14/2/77

* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
1 in. to 50 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-820

Sheet 1 of 1

Project Hat Creek Coal Development

Type of Drilling Rotary Core Coordinates E 22872
 Rig Longyear 44 Wireline N 69184

Reference Elevation 3084
 Type No. 3

Drilling Fluid Natural Mud Angle from Horizontal 90
 Bearing - ° Azimuth

Purpose of Hole Geotechnical Study

Job No.	* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling				Comments
				(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability			
									(2)(8) D	(8) K	(8) M	
	Sand, Gravel	0										
		28		35	70	39						
		52				57						
		59	① 56					-8				"Sand" in hole.
						38						
						37						
						37						
						51	MW					"Sand" in hole.
						27						
	Clayey Slst.					25						
						35						
						40						
						29						
						35						
						11						
						14						
		195				27		-6				
		207	T.D. ① 202									

Contractor Tonto Logged by DFW
 Date started 10/9/76 Checked by DFW
 Date completed 13/9/76 Date 4/2/77

* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
 1 in. to 50 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-821

Sheet 1 of 1

Project Hat Creek Coal Development

Type of Drilling Rotary Core Coordinates E 22929 55507

Coordinates E 22929 75507

Rq Longyear 44 Wireline N 7550

N 7550 0 0 0

Drilling Fluid Natural Mud Angle from Horizontal 90

Angle from Horizontal 90°

Bearing ° AzimuthReference Elevation 2963

Type No. ⁽⁹⁾ 3

Purpose of Hole - Geotechnical

Purpose of Role - Researcher
Study - Study

Study

* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling				Comments
			(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(2)(8) D	(8) K	(8) M	
Sand, Gravel, Till	0										
Brecciated Slst.	65		70	-7							
			125	-2							
	227										
	239	T.D.					-8				

Contractor Tonto Logged by DFP
Date started 14/9/76 Checked by DFW
Date completed 16/9/76 Date 14/2/77

*NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale :
1 in. to 50 ft.

Sheet 1 of 1

Bearing _____° Azimuth _____

Study

Job No.

Vertical scale :
1 in. to 20 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-824

Sheet 1 of 1

Project Bat Creek Coal Development

Type of Drilling Diamond

Coordinates E 38493

Rig Longyear 44 Wireline

N 7660

Drilling Fluid Natural Mud

Angle from Horizontal 90°

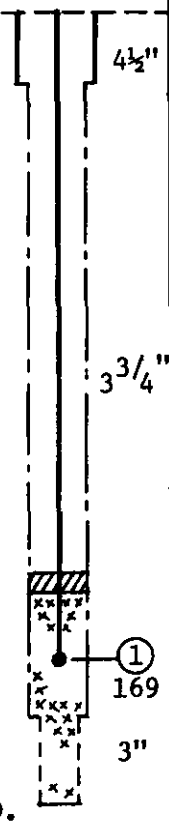
Bearing ° Azimuth

Reference Elevation 3853

Type No. 3

Purpose of Hole Geotechnical Study

Job No.

(1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling				Comments	
			(2) Depth	(2)(4) W.L.	(5) W.C.	(6) Other	(2)(7) S.W.L.	Permeability				
								(2)(8) D	(8) K	(8) M		
Till	0		75	-75							No water encountered in the till.	
			115	-115								
	150		145	-65								
Greenstone							-155	160-	3.6x			2 cave-ins - 1st to 192' 2nd to 150' after piezo installation & retrieval of HQ rods.
	182							192	10 ⁻⁸	f		
								160-	4.0x			
	205	T.D.						192	10 ⁻⁶	p		170-205' interval subsequently caved in.

Contractor Tonto
 Date started 25/9/76
 Date completed 4/10/76

Logged by DFF
 Checked by DFW
 Date 14/2/77

*NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
 1 in. to 50 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-825

Sheet 1 of 1

Project Hat Creek Coal Development

Type of Drilling Rotary Core

Coordinates E 36136
N 82508

Reference Elevation 4600

Rig Longyear 44 Wireline

Angle from Horizontal 90°

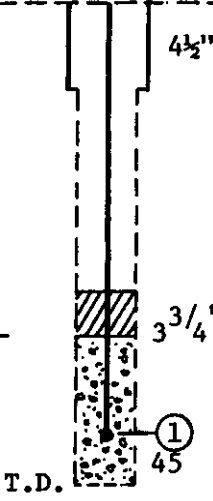
Type No. 3

Drilling Fluid Natural Mud

Bearing - ° Azimuth

Purpose of Hole Geotechnical Study

Job No.

* (1) Lithology	(2) Depth	(2) (3) Completed Construction	During Drilling				After Drilling				Comments
			(2) Depth	(2) (4) W. L.	(5) W. C.	(6) Other	(2) (7) S.W.L.	Permeability			
								(2) (8) O	(8) K	(8) M	
Sand	0										
Chert	20										
	35										
	50						-12				

Contractor Tonto
Date started 6/10/76
Date completed 7/10/76

Logged by DFF
Checked by DEW
Date 14/2/77

* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
1 in. to 20 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-826

Sheet 1 of 1

Project Hat Creek Coal Development

Type of Drilling Rotary Core

Coordinates E 36754

N 82611

Reference Elevation 4619

Type No. 3

Rig Longyear 44 Wireline

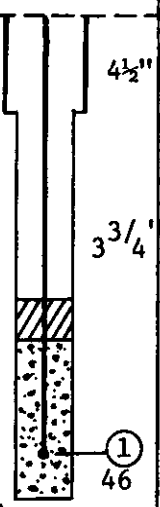
Angle from Horizontal 90

Purpose of Hole Geotechnical Study

Drilling Fluid Natural Mud

Bearing ° Azimuth

Job No. V76298A

* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling			Comments	
			(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(2)(8) D (ft)	K (ft)		M (ft)
Phyllite	0										
	10										
	34										
	50 T.D.						-13				

Contractor Tonto Logged by DFW
 Date started 8/10/76 Checked by DFW
 Date completed 8/10/76 Date 14/2/77

*NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
1 in. to 22 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. 76-827
Sheet 1 of 1

Project Har Creek Coal Development

Type of Drilling Rotary Core Coordinates E 37163
N 82798

Rig Longyear 44 Wireline Angle from Horizontal 90°

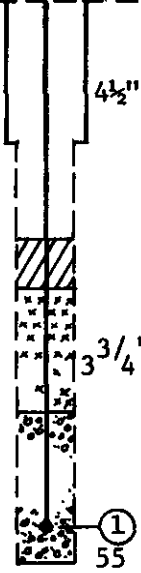
Drilling Fluid Natural Mud Bearing --- ° Azimuth

Reference Elevation 4603

Type No. 3

Purpose of Hole Geotechnical Study

Job No. Y762218-D

* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling				Comments
			(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(2)(8) D	(8) K	(8) M	
Till	0										
	15										
	24										
	30										
Phyllite	36										
	43										
	58	T.D.					-12				
	55										

Contractor Tonto Logged by DEF
Date started 9/10/76 Checked by DEF
Date completed 10/10/76 Date 14/2/77

*NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
1 in. to 20 ft.

SUMMARY HYDROLOGIC LOG

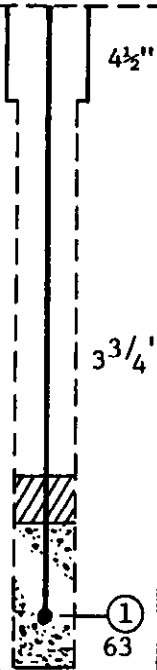
DRILLHOLE No. 76-828
Sheet 1 of 1

Project Hat Creek Coal Development

Type of Drilling Rotary Core
Rig Longyear 44 Wireline
Drilling Fluid Natural Mud
Coordinates E 3730
N 82231
Angle from Horizontal 90
Bearing Azimuth

Reference Elevation 4613
Type No. 3
Purpose of Hole Geotechnical Study

Job No. 176238-A

* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling				Comments
			(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(2)(8) D	(8) K	(8) M	
Sand, Gravel	0										
	10										
Phyllite	39										
	48										
	54										
	68	T.D.					-11				

Contractor Tonto
Date started 11/10/76
Date completed 12/10/76
Logged by DFF
Checked by DFW
Date 14/2/77

*NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
1 in. to 20 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. RH-76-10

Sheet 1 of 2

Project Hat Creek Coal Development

Type of Drilling Rotary

Coordinates E 18008

Rig Bucyrus Erie

N 76011

Drilling Fluid Air

Angle from Horizontal 90°

Bearing - ° Azimuth

Reference Elevation 3335

Type No. 3

Purpose of Hole Geotechnical Study

Job No. Y76248A

* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling				Comments
			(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(2)(8) D	K (8)	M (8)	
Sand, Gravel	0										
	81										
Clst.	110										
Carb. Clst.	119										
	130							119 -130	3.2x 10 ⁻⁹	f	
Slst., Sst.	141							141 -156	5.3x 10 ⁻⁹	f	
Slst.	154										

Contractor Tonto Logged by DFW
 Date started 7/8/76 Checked by DFW
 Date completed 8/8/76 Date 14/2/77


*NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
1 in. to 20 ft.

SUMMARY HYDROLOGIC LOG (Continued)

DRILLHOLE No. RH-76-10
Sheet 2 of 2

Job No.	(1) Lithology	(2) Depth	(2) (3) Completed Construction	During Drilling				After Drilling				Comments	
				(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) SWL.	Permeability				
									(2)(8) D	(8) K	(8) M		
		163											
	Congl.	170											
	Sst.	179											
	Sst., Sst.	182		T.D.					-26	172-182	6.0x10 ⁻⁹	f	

Vertical scale: 1 in. to 20 ft.

Golder Associates

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. RH-76-11

Sheet 1 of 1

Project Hat Creek Coal Development

Type of Drilling Rotary

Coordinates E 17528

Rig Bucyrus Erie

N 76983

Drilling Fluid Air

Angle from Horizontal 90

Bearing ° Azimuth

Reference Elevation 3397

Type No. 3

Purpose of Hole Geotechnical Study

Job No. V762282

* (1) Lithology	(2) Depth	Completed Construction (2)(3)	During Drilling				After Drilling				Comments
			(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(2)(8) D	(8) K	(8) M	
Bentonite	0										
	38										
Basalt											
	81										
	90										
Bentonite											
	110										
Sst.											
	122										
	125										
Slst., Sst.											
	134										
	148										

Contractor Tonto Logged by DFW
 Date started 9/8/76 Checked by DFW
 Date completed 10/8/76 Date 14/2/77

* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
1 in. to 20 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. RH-76-12
Sheet 1 of 2

Project Hat Creek Coal Development

Type of Drilling Rotary

Coordinates E 18450

Rig Bucyrus Erie

N 77016

Drilling Fluid Air

Angle from Horizontal 90°

Bearing ° Azimuth

Reference Elevation 3341

Type No. 3

Purpose of Hole Geotechnical Study

Job No. Y76229 B

* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling				Comments
			(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(2)(8) D(2)(8)	K (8)	M (8)	
Gravel, Till	0										
							</				

Contractor Tonto

Logged by DFF

Date started 8/8/76

Checked by DEW

Date completed 9/8/76

Date 14/2/77

*NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

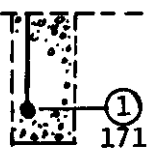
Golder Associates

Vertical scale:
1 in. to 20 ft.

SUMMARY HYDROLOGIC LOG (Continued)

DRILLHOLE No. RH-76-12

Sheet -2- of -2--

Job No.	(1) Lithology	(2) Depth	(2) (3) Completed Construction	During Drilling				After Drilling			Comments	
				(2) Depth	(2) (4) W. L.	(5) W. C.	(6) Other	(2) (7) SWL.	Permeability			
									(2) (8) D	(8) K		(8) M
	S1st.	174	T.D.  171					-139		1.2x 10 ⁻⁸	f	

Vertical scale: 1 in. to 20 ft.

Golder Associates

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. RH-76-13

Sheet 1 of 1

Project Hat Creek Coal DevelopmentType of Drilling Rotary

Coordinates E _ _ 17000

Rtg Bucyrus Erie

N 78002

Reference Elevation 3427

Type No. ⁽⁹⁾ 3

Drilling Fluid Air

Angle from Horizontal 90°

Purpose of Hole Geotechnical

Bearing _____° Azimuth _____

Purpose of Hold _____ Study

* (1) Lithology	(2) Depth	(3) Completed Construction	During Drilling				After Drilling				Comments
			(2) Depth	(4) W.L.	(5) W.C.	(6) Other	(7) S.W.L.	Permeability			
								(2)(8) K	(8) M	(9) M	
Bentonite	0	6 1/2"									
Clay, Slst.	42	6"									
Slst.	56										
	62										
	77										
	84	85	81			-71	2.1x 10 ⁻⁸	f			
	101		98			-77	9.5x 10 ⁻⁹	f			
Slst., Congl	111										
	121	T.D.	118			-75	1.4x 10 ⁻⁸	f			

Contractor Tonto Logged by DFP
Date started 11/8/76 Checked by DFW
Date completed 12/8/76 Date 14/2/77

* NOTE: Bracketed numbers refer to notes on pages A5-2
of this report.

Golder Associates

Vertical scale :
1 in. to 20 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. RH-76-14
Sheet 1 of 1

Project Hat Creek Coal Development

Type of Drilling Rotary

Coordinates E 17227

Rig Bucyrus Erie

N 82021

Drilling Fluid Air

Angle from Horizontal 90°

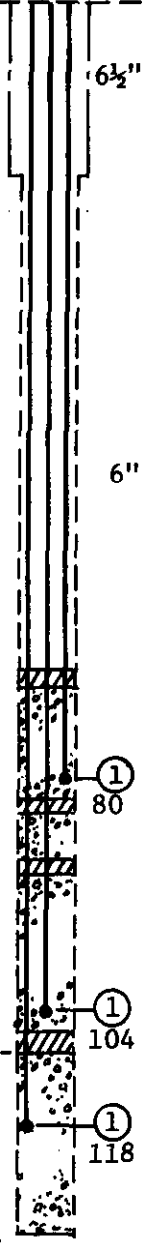
Bearing ° Azimuth

Reference Elevation 3083

Type No. 3

Purpose of Hole Geotechnical Study

Job No. 176238A

* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling				Comments	
			(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability				
								(2)(8) D	(8) K	(8) M		
Sand, Gravel	0											
Bentonite and slide material	15											
Clayey Slst.	64											
	71											
	83						-61		1.8x 10 ⁻⁹	f		
	91											
	107						-92		1.9x 10 ⁻⁹	f		
	109											
							-120		3.0x 10 ⁻⁹	f		
	128	T.D.										

Contractor Tonto
Date started 13/8/76
Date completed 13/8/76

Logged by DFF
Checked by DFW
Date 14/2/77

* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
1 in. to 20 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. RH-76-15

Sheet 1 of 2

Project Hat Creek Coal Development

Type of Drilling Rotary

Coordinates E _ _ 19755

Rtg Bucyrus Erie

N 82009

Drilling Fluid Air

Angle from Horizontal 90

Bearing ° Azimuth

Reference Elevation 2823

Type No. ⁽⁹⁾ 3

Purpose of Hole Geotechnical

Study

* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling				Comments
			(2) Depth	(2)(4) W.L.	(5) W.C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(2)(8) D _r (%)	(8) K	(9) M	
Sand, Gravel	0										
	25	6½"									
Coal		6"									
	110										
</											

Contractor Tonto Logged by DFF

Date started 18/8/76 Checked by DEW

Date completed 20/8/76 Date 14/2/77


* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale :
1 in. to 20 ft.

SUMMARY HYDROLOGIC LOG (Continued)

DRILLHOLE No. RH-76-15
Sheet 2 of 2

Job No.	(1) Lithology	(2) Depth	(2) (3) Completed Construction	During Drilling				After Drilling				Comments
				(2) Depth	(2) (4) W. L.	(5) W. C.	(6) Other	(2) (7) SWL.	Permeability			
									(2) (8) X	K (8)	M (8)	
	Coal	164						-14	164-149	7.8x10-5	f	
		175										
		191						-14	191-202	2.7x10-5	f	
		202 T.D.										

Vertical scale: 1 in. to 20 ft.

Golder Associates

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. RH-76-16

Sheet 1 of 1

Project Har Creek Coal Development

Type of Drilling Rotary

Coordinates E 19885

Rig Bucyrus Erie

N 76552

Drilling Fluid Air

Angle from Horizontal 90

Bearing ° Azimuth

Reference Elevation 3182

Type No. 3

Purpose of Hole Geotechnical Study

Job No. 176248A

* (1) Lithology	(2) Depth	(2)(3) Completed Construction	During Drilling				After Drilling				Comments
			(2) Depth	(2)(4) W.L.	(5) W.C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(2)(8) D	(8) K	(8) M	
Till	0										

Contractor Tonto Logged by DFW
 Date started 19/8/76 Checked by DFW
 Date completed 21/8/76 Date 14/2/77

*NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
1 in. to 50 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. RH-76-16A

Sheet 1 of 1

Project Hat Creek Coal Development

Type of Drilling Rotary Coordinates E 19879
N 76561

Coordinates E 19879
N 76561

Rio Bucyrus Erie N 70281

N 76561

Drilling Fluid Air Angle from Horizontal 90

Angle from Horizontal 90°

Drilling Fluid Air Angle from Horizontal 22
 Direction 0 Azimuth 0Bearing ° AzimuthReference Elevation 3182

Type No. ⁽⁹⁾ 3

Purpose of Hole **Geotechnical**

Purpose of Hole Geotechnical
Study

Study

[illegible]

Contractor Tonto Logged by DFE

Date started 21/8/76 Checked by DFW

Date completed 22/8/76 Date 14/2/77

* NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
1 in. to 50 ft.

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. RH-76-17
Sheet 1 **of** 1

Project Hat Creek Coal Development

Type of Drilling Rotary _____ Coordinates E 20145 _____
N 76312 _____

Rq Bucyrus Erie N 76512

Drilling Fluid Air _____ Angle from Horizontal 90 _____

Angle from Horizontal 90°----

Bearing ° Azimuth

Reference Elevation 3172
(9) 3

Type No. 3

Purpose of Hole Geotechnical Study _____

Job No. Y76248-B

* (1) Lithology	(2) Depth	Completed Construction (2)(3)	During Drilling				After Drilling				Comments
			(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability			
								(2)(8) D	(8) K	(8) M	
Sand	0										
	30										
Till	85										
	157										
	166						-56				Reading prior to pumping test.
	270										
Clayey Slst.	281						-42				Reading prior to pumping test.
	391										
		T.D.					-46				Reading prior to pumping test.

Contractor Tonto 404 404 Logged by DFF
Date started 23/8/76 Checked by DFW
Date completed 24/8/76 Date 14/2/77

* NOTE: Bracketed numbers refer to notes on pages A5-2
of this report.

Golder Associates

Vertical scale :
1 in. to 50 ft.

Sheet 1 of 1

Project Hat Creek Coal Development

Type of Drilling Rotary

Coordinates E 19710

Rig Bucyrus Erie

N 76733

Drilling Fluid Air

Angle from Horizontal 90°

Bearing _ _ _ _ _ ° Azimuth

Reference Elevation 3194

Type No. ^(g) 3

Purpose of Hole Geotechnical
StudyJob No. V-76348 B[illegible]

Contractor Tonto — Logged by DF

Date started 24/8/76 Checked by DFW

Date completed 25/8/76 Date 14/2/77

*NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale :
1 in. to 50 ft

Sheet 1 of 1

Project Hat Creek Coal Development

Type of Drilling Rotary

Coordinates E 19959

Rlg Bucyrus Erie

N 76477

Reference Elevation 3175

Type No. 3

Drilling Fluid Air

Angle from Horizontal 90°

Purpose of Hole Geotechnical _ _

Study

[illegible]

Contractor Tonto Logged by DFF
Date started 25/8/76 Checked by DFW
Date completed 1/9/76 Date 14/2/77

*NOTE: Bracketed numbers refer to notes on pages A5-2 of this report.

Golder Associates

Vertical scale:
1 in. to 50 ft.

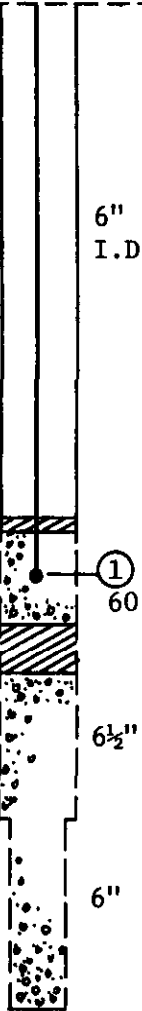
Job No. V-76348 B

SUMMARY HYDROLOGIC LOG

DRILLHOLE No. RH-76-20
Sheet 1 of 1

Project Hat Creek Coal Development
Type of Drilling Rotary Coordinates E 23211
Rig Bucyrus Erie N 75277
Drilling Fluid Air Angle from Horizontal 90°
Bearing ° Azimuth

Reference Elevation 2953
Type No. 3
Purpose of Hole Geotechnical Study

* (1) Lithology	(2) Depth m.	(2)(3) Completed Construction	During Drilling				After Drilling				Comments
			(2) Depth	(2)(4) W. L.	(5) W. C.	(6) Other	(2)(7) S.W.L.	Permeability			
								D(2)(8)	K (8)	M (8)	
Sand, Gravel, Till	0									Lithology interpreted from DDH 76-821 (RH 76-21)	
	55										
	65										
	70										
Brecciated Slst.	85										
	105	T.D.									

Contractor Tonto Logged by DFE
Date started 10/9/76 Checked by DFW
Date completed 12/9/76 Date 14/2/77

* NOTE: Bracketed numbers refer to notes on pages A5-2
of this report.

Golder Associates

Vertical scale:
1 in. to 20 ft.

II) In Situ Permeability Testing

II) IN SITU PERMEABILITY TESTING

Falling head permeability tests were performed through the standpipe piezometers installed in six of the air-flush drill holes, (RH 76 Nos. 10-15) and in three diamond drill holes located in the proposed ash dump area (76-822, 76-823 and 76-824).

1. The water in each standpipe was allowed to stabilize to a static level.
2. Water was then poured into the standpipe to impose an excess pressure head of about 30 ft. of water at the test section.
3. The water level in the tube was then monitored until it approached the original elevation.
4. From a plot of pressure head vs. time (or depth below a fixed datum vs. time) the permeability constant was calculated by means of the following equation:

$$k = \frac{r^2 \ln (L/R)}{2L (t_2 - t_1)} \ln (H_1/H_2)$$

where k = permeability constant

r = radius of standpipe

L = length of isolated borehole section

R = radius of borehole

H_1 = pressure head of water in standpipe above static level at some point during the test

H_2 = pressure head at some later time

$t_2 - t_1$ = time interval between H_2 and H_1 measurement.

The results of these tests are summarized in Table A5-1.

Piezometer No. 1⁽⁴⁾

Piezometer No. 3

5) See index to abbreviations in preamble to Appendix 1, Volume 2.

III) Installation and Monitoring
of Piezometers

III) INSTALLATION AND MONITORING OF PIEZOMETERS

Two types of piezometers were used, and were set in either cored mud-flush diamond-drill holes (3 to 4-inch diameter), or in air-flush rotary holes (6-inch diameter). A total of 74 standpipe piezometers and 19 pneumatic piezometers were installed. Details of the installations including typical designs are included in the last section and are summarized in Table A5-1.

All piezometer installations were designed as permanent installations to provide long-term monitoring of piezometric heads resulting from seasonal changes and pit excavation.

The piezometers were installed preferably in air-flush rotary holes, so that problems arising from the mudded walls of the holes were obviated. However advantage was also taken of the large number of mud-flush holes being drilled to install instruments wherever practicable. In the deeper holes, where the hole walls were difficult to stabilize, piezometer installations had to be completed through the drill rods after geophysical logging had been carried out. Piezometers were set in nests of one, two and occasionally three per hole, and only one hole had four piezometers (RH 76-15). The upper piezometers were usually set quite easily in the open hole after removal of the drill rods and before collapse of the hole.

The piezometers installed during the 1976 drilling program have been useful in providing initial piezometric head values. Many of the piezometers installed during July and August are still dropping slightly, and appear to be slowly stabilizing. The slow response in some of the standpipe piezometers is not surprising considering the low permeability of the siltstone and claystone (approx. 10^{-8} cm/sec.). Figure A5-1 shows hydrographs of piezometers in two holes, (DDH 76-801 and 76-805), which illustrate the response curves experienced in different areas with different piezometer types. The standpipe piezometer in

DDH 76-801 is located in siltstone on the southeastern pit perimeter, and the hydrograph shows a gradual decline of the water level in the standpipe. The two pneumatic piezometers in DDH 76-805 showed significant changes during the same period, thus demonstrating the sensitivity of these piezometers in low permeability sediments.

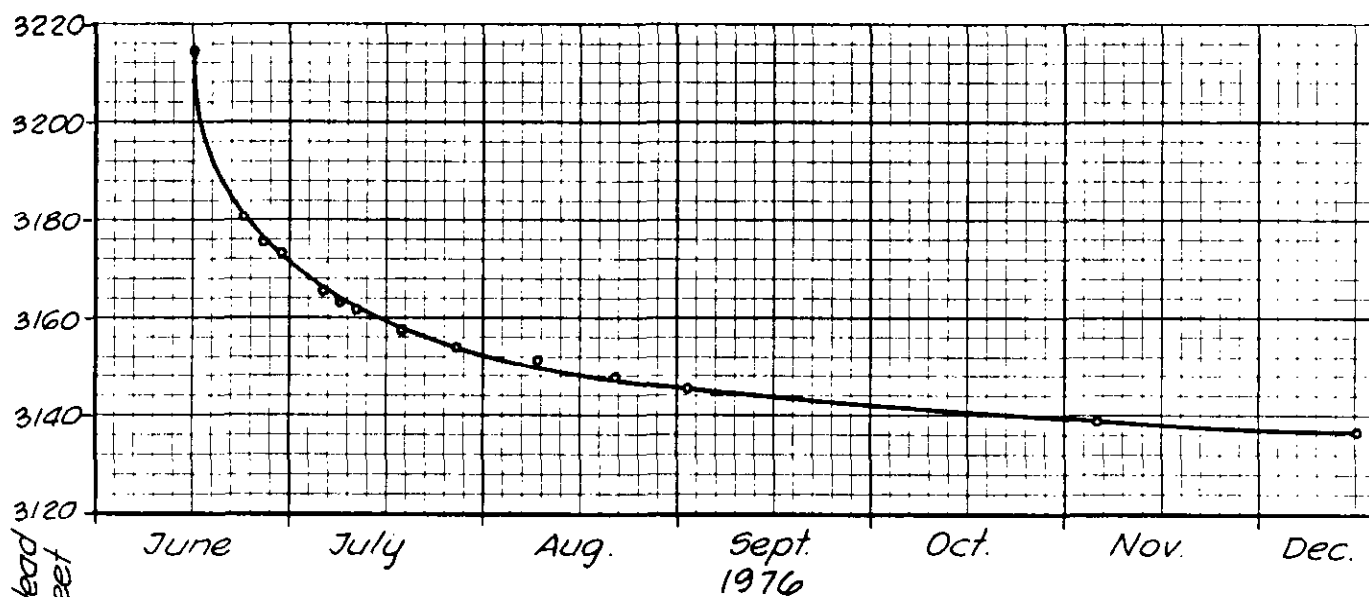
A regular monthly monitoring program for all piezometers has been recommended by GA, and it is being carried out by DCA for BCH. This program should be continued.

Project No. V-76398 B

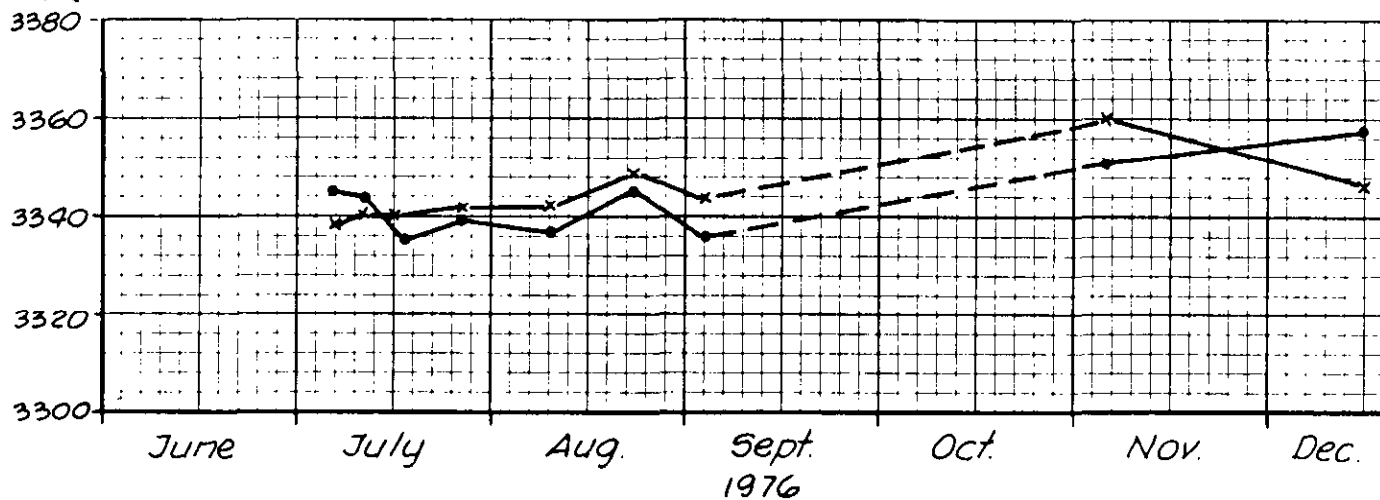
HYDROGRAPHS OF PIEZOMETERS 76-801-1, 76-805-1 AND 76-805-2

Figure A5-1

STANDPIPE PIEZOMETER IN DDH 76-801



PNEUMATIC PIEZOMETERS IN DDH 76-805



—●— Piezometer No. 1
-x- Piezometer No. 2

Golder Associates

Drawn HY
Reviewed MS
Date Mar. '77

IV) Report on Chemical Analysis
of Water Samples

IV) CANTEST LIMITED REPORT ON THE INORGANIC CHEMICAL
ANALYSIS OF WATER SAMPLES

Five water samples were collected from creeks, springs and the pump test well and were submitted to Cantest Limited for inorganic chemical analyses. Their report is attached, and the following sampling sites correspond with the sampling numbers given:

<u>GA Sample No.</u>	<u>Sample Site</u>
76-1	Aleece Creek: 2,000 ft. from lake outlet
76-2	Spring: on south shore of Aleece Lake
76-3	Aleece Lake: at 2 ft. depth near outlet
76-4	Well RH 76-19: during development
76-5	Hat Creek: near borehole RH 76-20
76-6	Well RH 76-19: at end of pump test

These data are summarized along with isotope data in Table 3 in the Main Report.



can test ltd.

1650 PANDORA STREET, VANCOUVER, B.C. V6L 1L6 • TELEPHONE 254-7278 • TELEX 04-54210

Report On Water Samples for Chemical Analysis File No. 4780 B
Reported to Golder Associates, Report No. _____
Consulting Geotechnical Engineers, Date Nov. 9, 1976
224 W. 8th Avenue, Atten: R. Allan Dakin
Vancouver, B.C. Re: Hat Creek Project

We have tested the samples of water submitted by you on October 22, 1976 and report as follows:

SAMPLE IDENTIFICATION:

The samples were submitted in plastic bottles labelled -

- Aleece Creek - 76 - 1
- 76 - 3
- 76 - 4
- 76 - 5
- 76 - 6

METHOD OF TESTING:

The samples were tested in accordance with the procedures set down in "Standard Methods for the Examination of Water and Wastewater" - 13th Edition, published by the American Public Health Association, 1975. Some of the samples were small, and for this reason Calcium, Magnesium, and Sodium were analysed by Plasma Spectroscopy rather than traditional methods.

RESULTS OF TESTING:

(on following page)

RESULTS OF TESTING:

<u>Test Parameter</u>	<u>76 - 1</u>	<u>76 - 3</u>	<u>76 - 4</u>	<u>76 - 5</u>
pH	7.85	7.60	7.60	8.0
Conductivity	508.	508.	677.	462 micromhos cm
Dissolved Cations				
Calcium	Ca ⁺⁺ 44.8	33.9	19.0	58.0 ppm
Magnesium	Mg 21.7	25.2	9.4	17.1 ppm
Sodium	Na 33.0	38.0	110.	21.3 ppm
Potassium	K 9.0	11.5	18.0	4.0 ppm
Iron	Fe -	L 0.05	-	- ppm
Dissolved Anions				
Bicarbonates	HCO ₃ -	265.	260.	- ppm
Sulfate	SO ₄ -	52.2	47.7	- ppm
Chloride	Cl ⁻ -	L 0.5	L 0.5	- ppm
Total Hardness	CaCO ₃ 201.	188.	86.0	214. ppm

(con't on following page)

RESULTS OF TESTING:

76 - 6

pH		7.60	
Conductivity		1834.	micromhos/cm
Total Hardness	CaCO ₃	208.	ppm
Dissolved Anions			
Alkalinity			
Bicarbonates	HCO ₃	1150.	ppm
Carbonates	CO ₃	NIL	ppm
Hydroxyl Ion	OH ³	NIL	ppm
Chlorides	Cl	L 0.5	ppm
Sulfates	SO ₄	17.3	ppm
Nitrates	N	L 0.10	ppm
Nitrites	N	L 0.001	ppm
Phosphates	PO ₄	L 0.01	ppm
Fluoride	F ⁴	0.067	ppm
Dissolved Cations			
Calcium	Ca	47.7	ppm
Magnesium	Mg	21.6	ppm
Potassium	K	34.0	ppm
Sodium	Na	330.	ppm
Iron	Fe	L 0.05	ppm
Aluminum	Al	0.004	ppm
Arsenic	As	L 0.005	ppm
Cadmium	Cd	L 0.001	ppm
Chromium	Cr	L 0.001	ppm
Copper	Cu	0.007	ppm
Mercury	Hg	L 0.0002	ppm
Lead	Pb	0.020	ppm
Zinc	Zn	1.97	ppm
Boron	B	L 0.1	ppm
Selenium	Se	L 0.004	ppm
Strontium	Sr	0.06	ppm
Lithium	L	L 0.05	ppm
Vanadium	V	L 0.10	ppm
Total Kjeldahl Nitrogen		22.2	ppm
Total Dissolved Solids		1500.	
Fixed		1400.	
Volatile		200.	

L - less than

CAN TEST LTD.,


A. W. Maynard, MSc
Chemist.

/dn

APPENDIX 6

PUMP TEST REPORT
FOR BOREHOLE RH 76-19

APPENDIX 6PUMP TEST REPORT
FOR BOREHOLE RH 76-19LOCATION AND CONSTRUCTION OF TEST WELL
AND OBSERVATION PIEZOMETERS

A 23-day pumping test was carried out on borehole RH 76-19 which is located slightly south of the middle of the proposed pit, see Drawing 6 (main text). The hole was constructed by first drilling and casing a 12-inch diameter hole to a depth of 145 ft. and then drilling an open hole to 400 ft. depth. The hole was drilled using a rotary drilling rig with an air-flush system. An 8-inch steel casing, which had perforations cut into the lower 255 ft., was then set into the hole and the annular space was backfilled with pea-gravel (see details in the Hydrologic Log for borehole RH 76-19 in Appendix 5). The completed hole was surged with air for about 3 days until the formation material had stabilized. Four observation holes were drilled within a radius of 360 ft. of this pump well, were completed at depths of about 400 ft. using biodegradable mud, and up to three piezometers were installed in each hole (see construction details, Appendix 5).

GEOLOGY AND HYDROLOGY OF TEST SITE

The pumped well (RH 76-19) was drilled into the upper claystone-siltstone member of the Coldwater Formation (see Drawing A6-1). The surficial deposits at the site were about 100 ft. thick and were comprised of till with minor inter-beds of sand and gravel. These surficial deposits were cased off to prevent vertical seepage into the well. The well screen (i.e. slotted portion of 8-inch casing) penetrated about half of the siltstone-claystone aquifer unit (see Section B-B, Drawing A6-1). This aquifer is not areally extensive as it is shaped like a

narrow trough approximately 1,000 ft. wide and running parallel to the axis of Hat Creek. This trough rests on top of a folded 700 ft. thick layer of coal (see Sections A-A and B-B, Drawing A6-1).

An examination of the piezometric heads in the aquifer prior to the start of the pump test show the following:

- a) the piezometric heads are generally about 50-90 ft. below ground level (i.e. in the till above the Coldwater Formation) and hence the till could be acting as a confining layer for ground water in the Coldwater Formation.
- b) the sand and gravel layer around RH 76-18 is a source of local recharge to the Coldwater Formation. This is not surprising as flows of about 60 gpm were encountered while drilling this borehole.
- c) the ground water generally flows downwards and follows the general slope of the topography, except in the area of RH 76-18 where local recharge disturbs this pattern.

PUMP TEST PROCEDURE

A small (1 h.p.) submersible pump was set in the 8-inch well to a depth of 380 ft. below ground. In order to reduce the water flows and line pressures at the ground surface, a small pipe-tee with an orifice plate was installed in the drop pipe just above the submersible pump. This allowed some water to escape back into the well, and hence reduced the line pressures. The water discharge from the well was controlled by means of a small needle valve.

In order to ensure that no water could seep back into the ground the pumped water was directed into a large mud pit. The pump test was started on

September 22, 1976 and the initial pumping rate was 1 gpm for the first three hours. The test had to be suspended for 19 hours while a malfunctioning generator was repaired and then the 1 gpm pumping rate was resumed. As very little recovery had been recorded in either the well or the observation piezometers, the effects of the suspension in pumping was small in relation to the length of the test that was carried out. After two days the pumping rate was reduced to 0.5 gpm, on the 3rd day the rate was reduced again to 0.1 gpm and this pumping rate was maintained for the remainder of the 23-day test. While the pump test was running, water levels and pneumatic pressures were read in the pumped well and in the piezometers around the well (see list of all measurements in pump test data summary in this appendix). In addition samples of the water pumped from the well were collected at the start and at the end of the pump test. These samples were sent for chemical and isotope analyses (see summary of results in Table 3 of the main report). Water temperatures and the electrical conductivity of the pumped water were measured at intermittent intervals during the pumping test (see data given in remarks column of pump test data summary in this appendix).

At the end of the test the pump was turned off and the response in the piezometers were monitored. An automatic water level recorder was installed in standpipe piezometer DDH 76-149-1.

ANALYSIS OF PUMP TEST DATA

The water level and pneumatic pressure readings were converted to piezometric elevations and drawdown, and are shown plotted in Figures A6-1 and A6-2. These figures show that the piezometric levels in the pumped well and the piezometers responded very rapidly at the start of the test, but after about 6 days of pumping most piezometers had stabilized and remained relatively stable for the remainder of the test.

Log-log graphs of drawdown versus time since pumping started were plotted for all piezometers and type curves were constructed so that hydrogeologic parameters, transmissivity and storage coefficients could be calculated. The type curves were constructed by modifying the standard Theis curve to account for the following:

- 1) partial penetration of the aquifer (Walton, 1972 p. 215);*
- 2) aquifer anisotropy: vertical permeability (k_v) to horizontal permeability k_h ratio is assumed to be 1:10 (Boulton and Streltsova, 1976);
- 3) large diameter of well relative to pumping rate (Boulton and Streltsova, 1976);
- 4) leakage of water from more permeable sand and gravel zones in the surficial till unit above the aquifer (Walton, 1972, p. 217).

Examples of plotted data and calculations using the modified type curve are given in pump test data summary sheets for piezometers RH 76-17-1, RH 76-18-2, DDH 76-149-1 and DDH 76-149-2. A summary of the results of calculations for all piezometers are given in Table A6-1. Similar type curves were used to calculate parameters from log-log distance-drawdown plots. These type curves incorporated the modifications previously described. The results of these calculations are shown in Table A6-2 for the periods 12 days and 23 days after the test started.

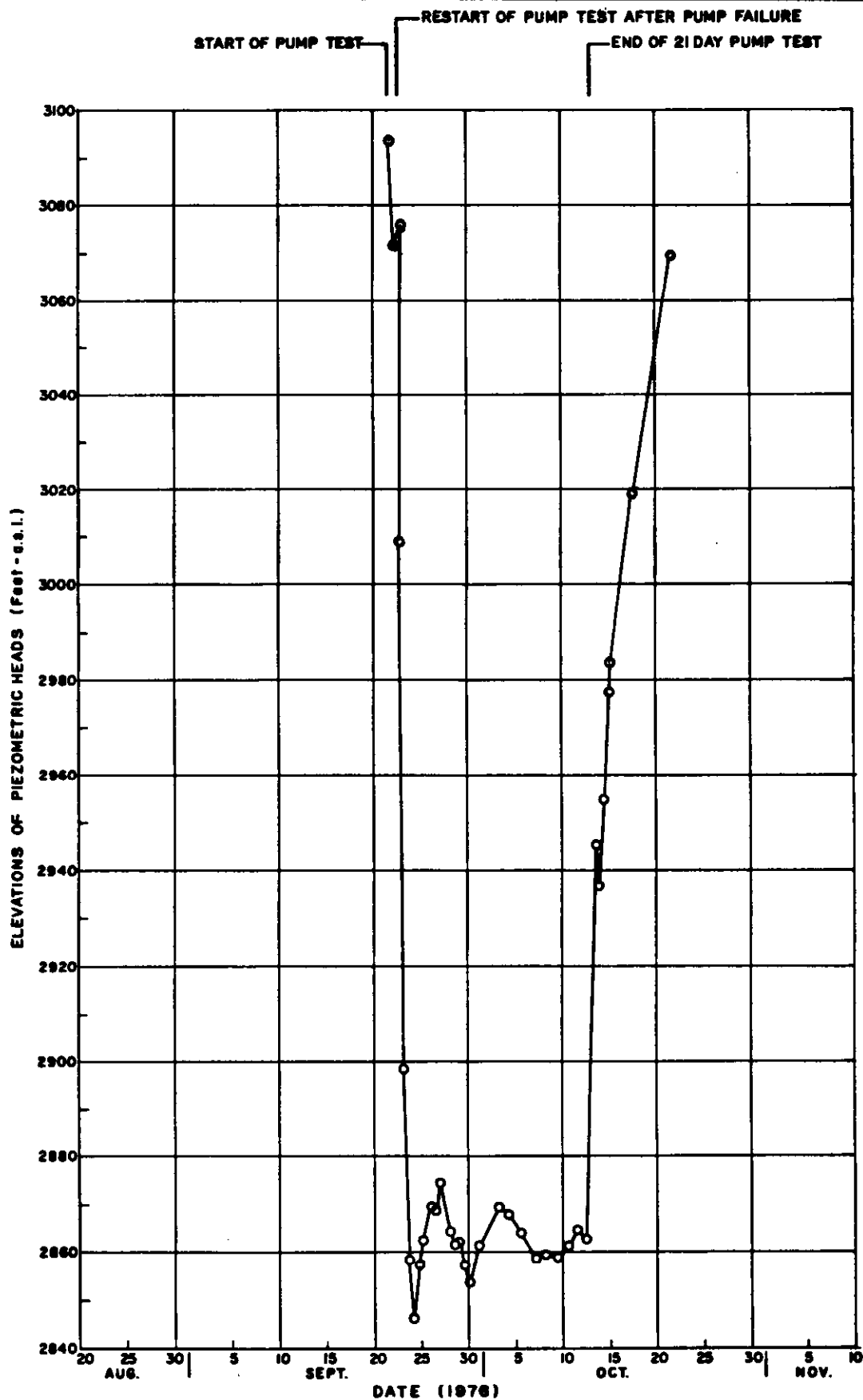
Because of the large diameter of the pumped well relative to the aquifer permeability, the recovery method of aquifer analysis (Walton, 1972) would not be easy to analyze and hence was not used.

*See List of References and Glossary in Section 9. of the main text.

ELEVATIONS OF WATER LEVELS IN PUMPED WELL RH76-19 DURING PUMP TEST.

FIGURE A6-1

Project No. Y76348B



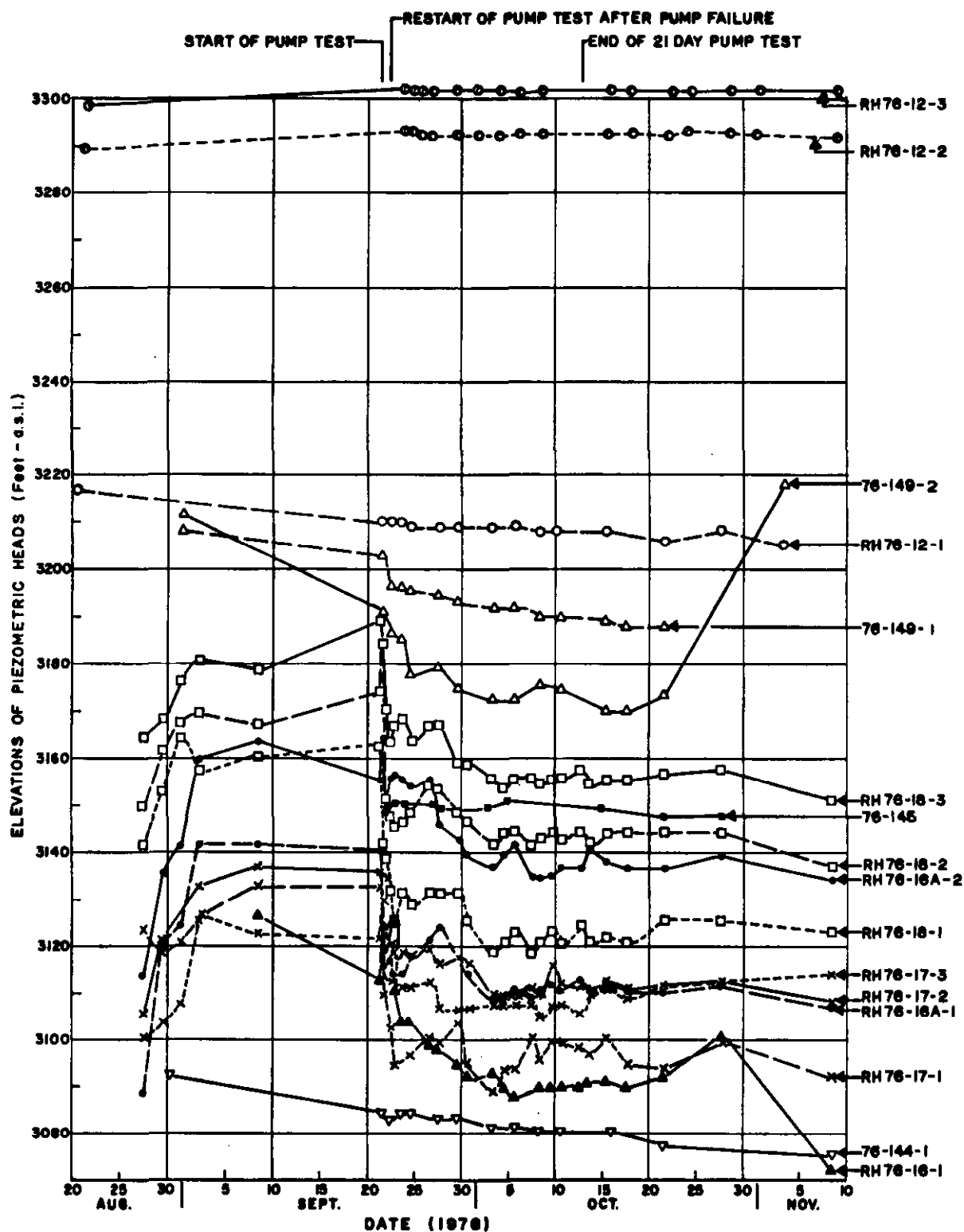
Golder Associates

Drawn *at*
App'd *226*
Date *Jan-77*

Project No. V223428

ELEVATIONS OF PIEZOMETRIC HEADS IN OBSERVATION HOLES: BEFORE, DURING AND SUBSEQUENT TO PUMPING TEST OF RH76-19.

FIGURE A6-2



Golder Associates

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App'd: *[Signature]*
Date: Jan 77

DISCUSSION OF RESULTS

- 1) The calculated aquifer transmissivity ("T") of the siltstone-claystone aquifer ranges between 0.20-1.15 gpd/ft. and averages 0.7 gpd/ft. for the piezometers around the well (Table A6-1). If we assume that the average aquifer thickness is about 600 ft., then the calculated horizontal permeability of the aquifer would be 5.3×10^{-8} cm/sec. This figure is in reasonable agreement with the permeability figures determined using the falling head method in standpipe piezometers, see Table A5-1. For example in piezometer RH 76-12-1 which is located 1,400 ft. from the pumped well the calculated permeability is $k = 1.2 \times 10^{-8}$ cm/sec.
- 2) The calculated storage coefficients (S) ranged from 0.21×10^{-7} to 9×10^{-7} and averaged 4×10^{-7} for the piezometers around the well (Table A6-1). Assuming a 600 ft. aquifer thickness the average specific storage (see Glossary) would be $4 \times 10^{-7} / 600 = 6.7 \times 10^{-10}$ $\text{ft}^{-1} = 2.2 \times 10^{-11}$ cm^{-1} .
- 3) The pump test showed that ground water in the sands and gravels in the till above the aquifer was recharging water to the siltstone-claystone aquifer. Evidence for this was observed in both the piezometric head pattern near the well (see Section A-A, Drawing A6-1) and in the response shown in piezometer DDH 76-149-2. This latter piezometer is located in the till and showed a 25-ft. decline in piezometric head during the pump test.
- 4) The pump test showed that there is a hydraulic connection between the A-zone coal, B-zone coal and sandstone-siltstone unit below. This statement is based on observations in piezometers DDH 76-149-1 and DDH 76-144-1 which both show a response as a result of pumping well RH 76-19.

- 5) The more permeable coal ($k = 10^{-4}$ cm/sec.) zones are sufficiently far from the well to have no influence on the calculations for transmissivity.

CONCLUSIONS

- 1) The pump test has shown that some depressurization had taken place in the sediments around the pump test site.
- 2) The siltstone-claystone (Coldwater Formation) sediments have a permeability of about 10^{-8} cm/sec. and specific storage of about 2×10^{-11} cm⁻¹.
- 3) The test demonstrated that the surficial deposits are recharging the Coldwater Formation and that it will be essential to dewater these surficial deposits before the siltstone can be effectively depressurized.

TABLE A6-1**HYDROGEOLOGIC PARAMETERS CALCULATED FROM
TIME-DRAWDOWN CURVES**

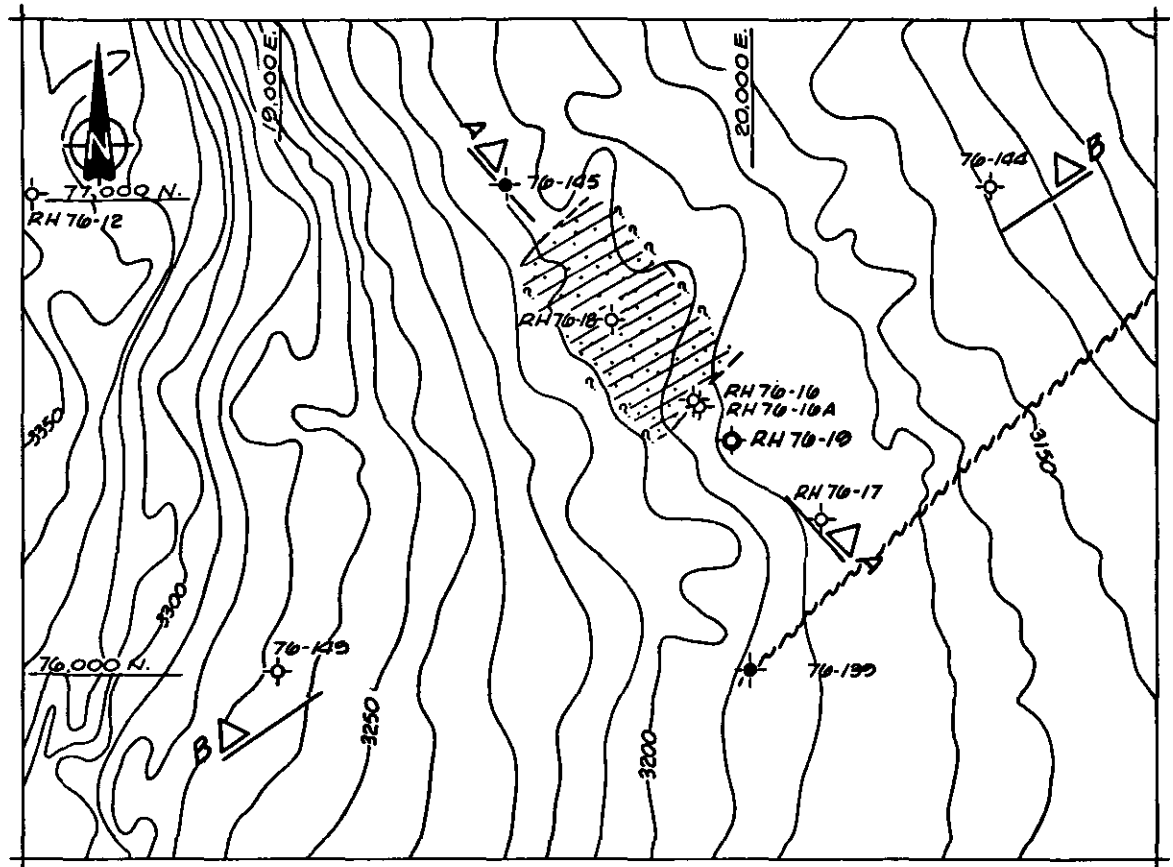
Observation Point	Distance From Pumped Well (ft)	Aquifer Parameter	
		Transmissivity T (gpd/ft)	Storage Coefficient S x 10 ⁻⁷
RH 16A-1	105	0.21	5.3
RH 16A-2	105	0.20	6
RH 16-1	115	0.7	2
RH 17-1	249	0.64	0.35
RH 17-2	249	1.04	1.13
RH 17-3	249	0.76	9
RH 18-1	357	0.76	0.21
RH 18-2	357	0.96	0.28
RH 18-3	357	1.15	0.67
Average		0.71	4.1
DDH 144-1	760	1.15	0.66
DDH 149-1	1080	0.5	0.52
DDH 149-1	1080	0.5	0.52
DDH 149-2	1080	0.29	0.91

TABLE A6-2**HYDROGEOLOGIC PARAMETERS CALCULATED
FROM DISTANCE-DRAWDOWN CURVES**

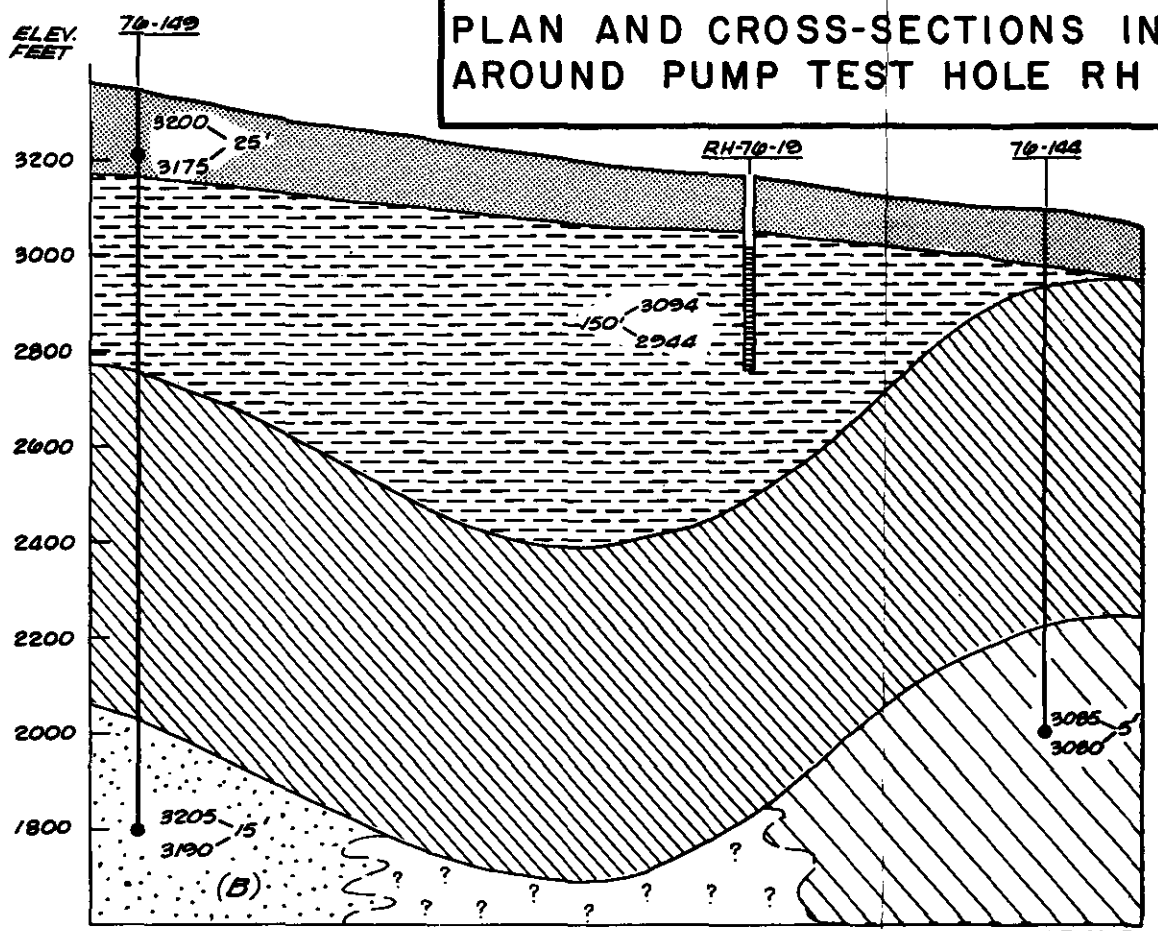
Time Since Pumping Started (days)	Aquifer Parameter	
	Transmissivity T gpd/ft.	Storage Coefficient S
12	0.2	2x10 ⁻⁵
23	0.13	7.8x10 ⁻⁶

PLAN AND CROSS-SECTIONS IN AREA
 AROUND PUMP TEST HOLE RH 76-19

DRAWING A6-1

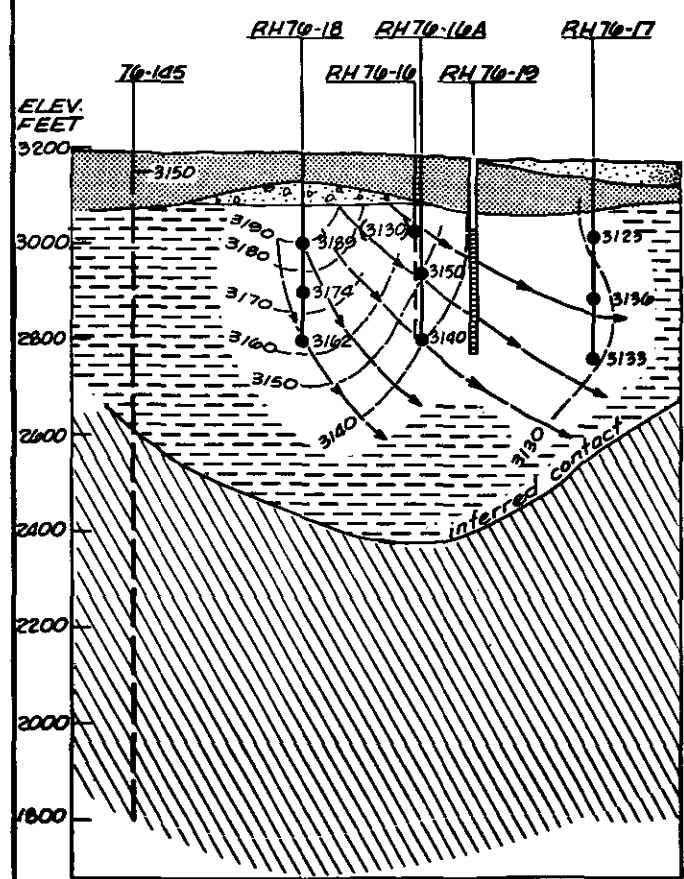


PLAN

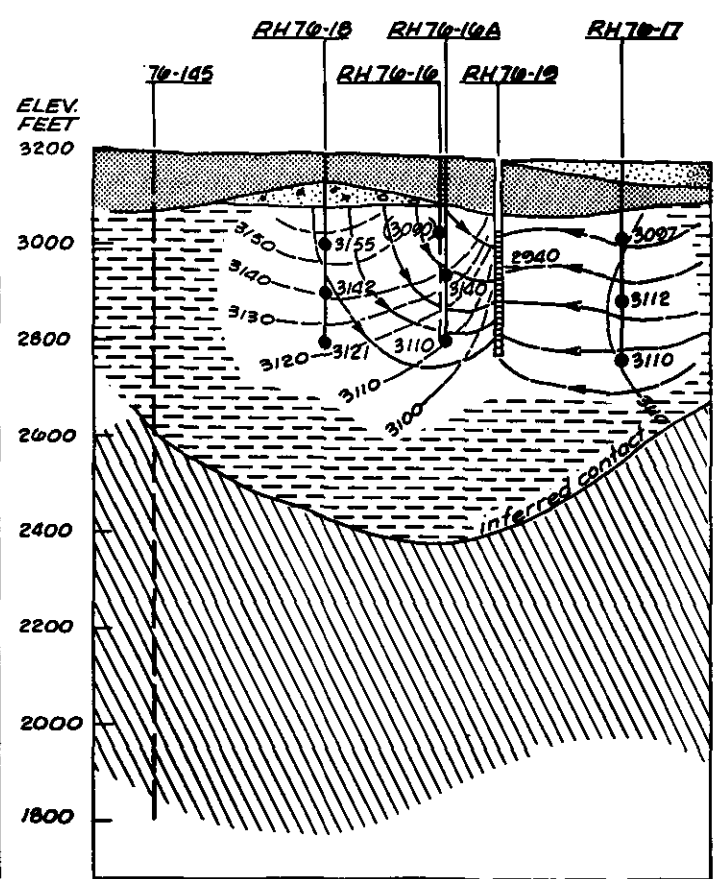


SECTION B-B

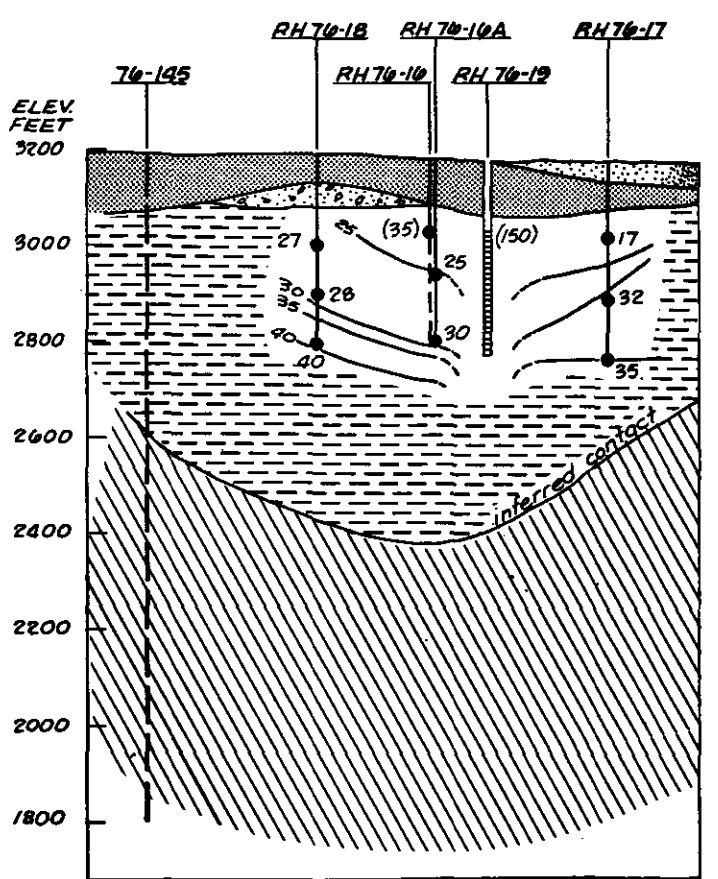
NOTATION: INITIAL PIEZOMETRIC HEAD = 3085
 FINAL PIEZOMETRIC HEAD = 3080



a) Piezometric head distribution before pump test started.



b) Piezometric head distribution at end of pump test.



c) Lines of equal drawdown at end of pump test.

LEGEND

~~~~~ Approx. location of fault.  
 3250 Ground contours (feet asl) contour interval 10 ft.  
 + Active observation hole with piezometers used for pump test.  
 • Observation hole not used because of lack of response.  
 • Pumped well.  
 [Hatched] Area of significant sand and gravel lenses in surficial till deposits. (see plan)  
 3150 Equipotential lines.  
 — Groundwater flow lines.  
 25 Lines of equal drawdown at end of pump test. (feet)  
 [Vertical line] Well screen.  
 [Dot] Location of piezometer.  
 [Stippled] Sand and silt.  
 [Dotted] Gravel and sand.  
 [Horizontal lines] Till + undifferentiated sand and gravel.  
 [Wavy lines] Claystone and siltstone. (upper Coldwater Fm.)  
 [Diagonal lines] Coal (A zone)  
 [Cross-hatched] Coal (B zone) with facies change to interbedded siltstone and sandstone in region of 76-149.

400 0 400 800  
 SCALE - FEET

Golder Associates

DRAWN \_\_\_\_\_  
 REVIEWED \_\_\_\_\_  
 DATE Feb. 77

**Project No. Y76342B-**

DATE: Start Sept. 22, 1976  
Finish Oct. 14, 1976

Type: ☐ Screened well ☐ Pneumatic piezo.  
☐ Unscreened well ☒ Standpipe piezo.  
Datum elevation 3346 FT. a. s. l.  
Elevation static water level 3210 FT. a. s. l.  
Elevation of screened interval            to            a. s. l.

**DATA ON PUMPED WELL AND AQUIFER:**

Aquifer Conditions: ☒ confined  
☐ unconfined

Aquifer description Coldwater Fm (Siltstone)

Aquifer thickness 800 feet

Depth to pump suction 370 feet

Type of test : ☒ constant rate  
☐ step drawdown

Well depth \_\_\_\_\_ 400 feet  
Well diameter \_\_\_\_\_ 8 inches  
Pump type \_\_\_\_\_ Electric Submersible  
Final pumping rate \_\_\_\_\_ 0.1 gpm

Logged by RAO

## Project No. Y763428-

Observations in RH 76-12-2  
Sheet 1 of 1  
DATE: Start Sept. 22, 1976  
Finish Oct. 14, 1976

☐ Screened well                      ☐ Pneumatic piezo.  
 Type: ☐ Unscreened well            ☒ Standpipe piezo.  
 Datum elevation 3346 FT. \_\_\_\_\_ a. s. l.  
 Elevation static water level 3291 FT. \_\_\_\_\_ a. s. l.  
 Elevation of screened interval \_\_\_\_\_ to \_\_\_\_\_ a. s. l.

Aquifer Conditions: ☒ confined  
☐ unconfined

Aquifer description Coldwater Fm (Siltstone)

Aquifer thickness 800 feet

Depth to pump suction 370 feet

Type of test : ☒ constant rate  
☐ step drawdown

## Golder Associates

Logged by—     L.D.

## Project No. Y763402-

Observations in RH 76-12-3  
Sheet 1 of 1  
DATE: Start Sept. 22, 1976  
Finish Oct. 14, 1976

☐ Screened well      ☐ Pneumatic piezo.  
 Type: ☐ Unscreened well      ☒ Standpipe piezo.  
 Datum elevation 3346 FT. \_\_\_\_\_ a. s. l.  
 Elevation static water level 3300 FT. \_\_\_\_\_ a. s. l.  
 Elevation of screened interval \_\_\_\_\_ to \_\_\_\_\_ a. s. l.

**Aquifer Conditions:** ☒ confined  
☐ unconfined

**Aquifer description:** Coldwater Fm (Siltstone)

**Aquifer thickness:** 800 feet

**Depth to pump suction:** 370 feet

**Type of test:** ☒ constant rate  
☐ step drawdown

## Golder Associates

Logged by-- RAJ

Project No. Y163402

**PUMP TEST DATA SUMMARY**

PROJECT Hat Creek Coal  
 Location Cache Creek, B.C.  
 Pumped Well RH 76-19

Observations in RH 76-16  
 Sheet 1 of 2  
 DATE: Start Sept. 22, 1976  
 Finish Oct. 14, 1976

**DATA ON OBSERVATION POINT:**

Datum point Top of tube  
 Depth to static water level             
 Screened/open hole interval            to           

Type: ☐ Screened well ☒ Pneumatic piezo.  
☐ Unscreened well ☐ Standpipe piezo.  
 Datum elevation 3182.1 ft. a.s.l.  
 Elevation static water level            a.s.l.  
 Elevation of screened interval            to            a.s.l.

**DATA ON PUMPED WELL AND AQUIFER:**

Well depth 400 feet  
 Well diameter 8 inches  
 Pump type Electric Submersible  
 Final pumping rate 0.1 gpm

Aquifer Conditions: ☒ confined ☐ unconfined  
 Aquifer description Coldwater Fm (Siltstone)  
 Aquifer thickness 800 feet  
 Depth to pump suction 370 feet  
 Type of test: ☒ constant rate ☐ step drawdown

| Time |     |      | Elapsed Time<br>"t"<br>(mins.) | Depth to Water<br>(ft.) | Pressure<br>(Pneumatic<br>piezometers<br>only)<br>(p.s.i.) | Elevation<br>of Water<br>(ft.)<br>a.s.l. | Drawdown<br>(ft.) | Pump Rate<br>Q<br>(l.g.p.m.) | Remarks                 |
|------|-----|------|--------------------------------|-------------------------|------------------------------------------------------------|------------------------------------------|-------------------|------------------------------|-------------------------|
| Dy.  | Hr. | Min. |                                |                         |                                                            |                                          |                   |                              |                         |
| 22   | 9   | 00   |                                |                         | 38                                                         |                                          | -                 |                              |                         |
|      |     | 160  | 0                              |                         | -                                                          | 3126.1                                   | -                 |                              | Pumping started         |
|      |     | 1630 | 30                             | 48.4                    | 47                                                         | 3133.7                                   | -                 |                              |                         |
|      |     | 1900 | 180                            | 60.0                    | 42                                                         | 3122.1                                   | 4.0               |                              |                         |
| 23   | 11  | 30   | 1170                           | 57.7                    | 43                                                         | 3124.4                                   | 1.7               |                              |                         |
|      |     | 1930 | 1650                           | 71.5                    | 37                                                         | 3110.6                                   | 15.5              |                              |                         |
| 24   | 15  | 30   | 2850                           | 78.5                    | 34                                                         | 3103.6                                   | 22.5              |                              |                         |
| 25   | 13  | 30   | 4170                           | 78.5                    | 34                                                         | 3103.6                                   | 22.5              |                              |                         |
| 27   | 14  | 00   | 7080                           | 83.1                    | 32                                                         | 3099.0                                   | 27.1              |                              |                         |
| 28   | 14  | 30   | 8550                           | 89.2                    | 31.5                                                       | 2097.9                                   | 28.2              |                              |                         |
| 30   | 14  | 00   | 11400                          | 87.7                    | 30                                                         | 3094.4                                   | 31.7              |                              |                         |
| 1    | 15  | 45   | 12945                          | 90.0                    | 29                                                         | 3092.1                                   | 34.0              |                              |                         |
| 4    | 9   | 30   | 16890                          | 90.0                    | 29                                                         | 3092.1                                   | 34.0              |                              |                         |
| 5    | 13  | 00   | 18540                          | 92.3                    | 28                                                         | 3089.8                                   | 36.3              |                              |                         |
| 6    | 17  | 00   | 20220                          | 94.6                    | 27                                                         | 3087.5                                   | 38.6              |                              |                         |
| 8    | 11  | 00   | 22840                          | -                       | -                                                          | -                                        | -                 |                              |                         |
| 9    | 9   | 00   | 24060                          | 92.3                    | 28                                                         | 3089.8                                   | 36.3              |                              |                         |
| 10   | 15  | 30   | 25890                          | 92.3                    | 28                                                         | 3089.8                                   | 36.3              |                              |                         |
| 11   | 15  | 00   | 27300                          | 92.3                    | 28                                                         | 3089.8                                   | 36.3              |                              |                         |
| 13   | 14  | 00   | 30120                          | 92.3                    | 28                                                         | 3089.8                                   | 36.3              |                              |                         |
| 14   | 17  | 30   | 31770                          | 91.2                    | 28.5                                                       | 3090.9                                   | 35.2              |                              | Pumping stopped (19:11) |
| 16   | 11  | 15   |                                | 91.2                    | 28.5                                                       | 3090.9                                   | 35.2              |                              |                         |
| 18   | 16  | 00   |                                | 92.3                    | 28                                                         | 3089.8                                   | 36.3              |                              |                         |
| 22   | 15  | 30   |                                | 90.0                    | 29                                                         | 3092.1                                   | 34.0              |                              |                         |
| 28   | 15  | 30   |                                | 80.8                    | 33                                                         | 3101.3                                   | 24.8              |                              |                         |





Project No. Y763008

**PUMP TEST DATA SUMMARY**

PROJECT Hot Creek Coal  
 Location Cache Creek, B.C.  
 Pumped Well RH 76-19

Observations in RH 76-16A-1  
 Sheet 1 of 2

DATE: Start Sept. 22, 1976  
 Finish Oct. 14, 1976

**DATA ON OBSERVATION POINT:**

Datum point Top of tube  
 Depth to static water level 40.6 FT.  
 Screened/open hole interval to

Type: ☐ Screened well ☒ Pneumatic piezo.  
☐ Unscreened well ☐ Standpipe piezo.  
 Datum elevation 3182.1 FT. a. s. l.  
 Elevation static water level 3141.5 a. s. l.  
 Elevation of screened interval to a. s. l.

**DATA ON PUMPED WELL AND AQUIFER:**

Well depth 400 feet  
 Well diameter 8 inches  
 Pump type Electric Submersible  
 Final pumping rate 0.1 gpm

Aquifer Conditions: ☒ confined ☐ unconfined  
 Aquifer description Coldwater Fm (Siltstone)  
 Aquifer thickness 800 feet  
 Depth to pump suction 370 feet  
 Type of test: ☒ constant rate ☐ step drawdown

| Time |     |      | Elapsed Time<br>"t"<br>(mins.) | Depth to Water<br>(ft.) | Pressure<br>(Pneumatic<br>piezometers<br>only)<br>(p.s.i.) | Elevation<br>of Water<br>(ft.)<br>a.s.l. | Drawdown<br>(ft.) | Pump Rate<br>Q<br>(l.g.p.m.) | Remarks              |
|------|-----|------|--------------------------------|-------------------------|------------------------------------------------------------|------------------------------------------|-------------------|------------------------------|----------------------|
| Dy.  | Hr. | Min. |                                |                         |                                                            |                                          |                   |                              |                      |
| 22   | 9   | 00   | 0                              | 41.5                    | 150                                                        | 3140.6                                   |                   |                              |                      |
|      |     | 1600 | 0                              |                         | -                                                          | -                                        | -                 |                              | Pumping started.     |
|      |     | 1630 | 30                             | 40.3                    | 150.5                                                      | 3141.8                                   | 0                 |                              |                      |
|      |     | 1900 | 180                            | 66.9                    | 139                                                        | 3115.2                                   | 26.3              |                              |                      |
| 23   | 11  | 30   | 1180                           | 64.6                    | 140                                                        | 3117.5                                   | 24.0              |                              |                      |
|      |     | 1930 | 1650                           | 68.1                    | 138.5                                                      | 3114.0                                   | 27.5              |                              |                      |
| 24   | 15  | 30   | 2850                           | 68.1                    | 138.5                                                      | 3114.0                                   | 27.5              |                              |                      |
| 25   | 13  | 30   | 4170                           | 64.6                    | 140                                                        | 3117.5                                   | 24.0              |                              |                      |
| 27   | 14  | 00   | 7080                           | 61.1                    | 141.5                                                      | 3121.0                                   | 20.5              |                              |                      |
| 28   | 14  | 30   | 8550                           | 58.8                    | 142.5                                                      | 3123.3                                   | 18.2              |                              |                      |
| 30   | 14  | 00   | 11400                          | 64.6                    | 140                                                        | 3117.5                                   | 24.0              |                              |                      |
| 1    | 15  | 45   | 12945                          | 68.1                    | 138.5                                                      | 3114.0                                   | 27.5              |                              |                      |
| 4    | 9   | 30   | 16890                          | 73.8                    | 136                                                        | 3108.3                                   | 33.2              |                              |                      |
| 5    | 13  | 00   | 18540                          | 73.8                    | 136                                                        | 3108.3                                   | 33.2              |                              |                      |
| 6    | 17  | 00   | 20220                          | 71.5                    | 137                                                        | 3110.6                                   | 30.9              |                              |                      |
| 8    | 11  | 00   | 22740                          | 73.8                    | 136                                                        | 3108.3                                   | 33.2              |                              |                      |
| 9    | 9   | 00   | 24060                          | 71.5                    | 137                                                        | 3110.6                                   | 30.9              |                              |                      |
| 10   | 15  | 30   | 25890                          | 70.4                    | 137.5                                                      | 3111.7                                   | 29.8              |                              |                      |
| 11   | 15  | 00   | 27300                          | 71.5                    | 137                                                        | 3110.6                                   | 30.9              |                              |                      |
| 13   | 14  | 00   | 30120                          | 69.2                    | 138                                                        | 3112.9                                   | 28.6              |                              |                      |
| 14   | 17  | 30   | 31770                          | 71.5                    | 137                                                        | 3110.6                                   | 30.9              |                              | Pump stopped (19:11) |
| 16   | 11  | 15   |                                | 70.4                    | 137.5                                                      | 3111.7                                   | 29.8              |                              |                      |
| 18   | 16  | 00   |                                | 71.5                    | 137                                                        | 3110.6                                   | 30.9              |                              |                      |
| 22   | 15  | 30   |                                | 71.5                    | 137                                                        | 3110.6                                   | 30.9              |                              |                      |
| 28   | 15  | 30   |                                | 70.4                    | 137.5                                                      | 3111.7                                   | 29.8              |                              |                      |

## Project No. V76348B

Observations in RH 76-16A-1  
Sheet 2 of 2  
DATE: Start Sept. 22, 1976  
Finish Oct. 14, 1976

Logged by -     fag

Project No. Y763008

## PUMP TEST DATA SUMMARY

PROJECT Hot Creek Coal  
 Location Cache Creek, B.C.  
 Pumped Well RH 76-19

Observations in RH 76-19A-2  
 Sheet 1 of 2  
 DATE: Start Sept. 22, 1976  
 Finish Oct. 14, 1976

## DATA ON OBSERVATION POINT:

Datum point Top of tube  
 Depth to static water level 19.6 FT.  
 Screened/open hole interval to

Type: ☐ Screened well ☒ Pneumatic piezo.  
☐ Unscreened well ☐ Standpipe piezo.  
 Datum elevation 3182.1 FT. a. s. l.  
 Elevation static water level 3163.5 FT. a. s. l.  
 Elevation of screened interval to a. s. l.

## DATA ON PUMPED WELL AND AQUIFER:

Well depth 400 feet  
 Well diameter 8 inches  
 Pump type Electric Submersible  
 Final pumping rate 0.1 gpm

Aquifer Conditions: ☒ confined ☐ unconfined  
 Aquifer description Coldwater Fm (Siltstone)  
 Aquifer thickness 800 feet  
 Depth to pump suction 370 feet  
 Type of test: ☒ constant rate ☐ step drawdown

| Time  | Elapsed Time "t" (mins.) |          | Depth to Water (ft.) | Pressure (Pneumatic piezometers only) (p.s.i.) | Elevation of Water (ft.) a.s.l. | Drawdown (ft.) | Pump Rate Q (l.g.p.m.) | Remarks                 |
|-------|--------------------------|----------|----------------------|------------------------------------------------|---------------------------------|----------------|------------------------|-------------------------|
|       | Dy.                      | Hr. Min. |                      |                                                |                                 |                |                        |                         |
| 22 9  | 00                       | 0        | 26.9                 | 94                                             | 3155.2                          |                |                        |                         |
|       | 16                       | 00       | -                    | -                                              | -                               | -              |                        | Pumping started         |
|       | 16                       | 30       | 30                   | 98                                             | 3164.5                          | -              |                        |                         |
|       | 19                       | 00       | 180                  | 91                                             | 3148.3                          | 15.2           |                        |                         |
| 23 11 | 30                       | 1170     | 26.9                 | 94                                             | 3155.2                          | 8.3            |                        |                         |
|       | 19                       | 30       | 1650                 | 25.7                                           | 3156.4                          | 7.1            |                        |                         |
| 24 15 | 30                       | 2850     | 26.9                 | 94                                             | 3155.2                          | 8.3            |                        |                         |
| 25 13 | 30                       | 4170     | 28.0                 | 93.5                                           | 3154.1                          | 9.4            |                        |                         |
| 27 14 | 00                       | 7080     | 26.9                 | 94                                             | 3155.2                          | 8.3            |                        |                         |
| 28 14 | 30                       | 8550     | 36.1                 | 90                                             | 3146.0                          | 17.5           |                        |                         |
| 30 14 | 00                       | 11400    | 39.6                 | 88.5                                           | 3142.5                          | 21.0           |                        |                         |
| 1 15  | 45                       | 12945    | 43.0                 | 87                                             | 3139.1                          | 24.4           |                        |                         |
| 4 9   | 30                       | 16890    | 45.3                 | 86                                             | 3136.8                          | 26.7           |                        |                         |
| 5 13  | 00                       | 18540    | 43.0                 | 87                                             | 3139.1                          | 24.4           |                        |                         |
| 6 17  | 00                       | 20220    | 40.7                 | 88                                             | 3141.4                          | 22.1           |                        |                         |
| 8 11  | 00                       | 22740    | 47.6                 | 85                                             | 3134.5                          | 29.0           |                        |                         |
| 9 9   | 00                       | 24060    | 47.6                 | 85                                             | 3134.5                          | 29.0           |                        |                         |
| 10 15 | 30                       | 25890    | 47.6                 | 85                                             | 3134.5                          | 29.0           |                        |                         |
| 11 15 | 00                       | 27300    | 45.3                 | 86                                             | 3136.8                          | 26.7           |                        |                         |
| 13 14 | 00                       | 30120    | 45.3                 | 86                                             | 3136.8                          | 26.7           |                        |                         |
| 14 17 | 30                       | 31770    | 41.9                 | 87.5                                           | 3140.2                          | 23.3           |                        | Pumping stopped (19:11) |
| 16 11 | 15                       |          | 44.2                 | 86.5                                           | 3137.9                          | 25.6           |                        |                         |
| 18 16 | 00                       |          | 45.3                 | 86                                             | 3136.8                          | 26.7           |                        |                         |
| 22 15 | 30                       |          | 45.3                 | 86                                             | 3136.8                          | 26.7           |                        |                         |
| 28 15 | 30                       |          | 43.0                 | 87                                             | 3139.1                          | 24.4           |                        |                         |

Project No. V76348B

Observations in RH 76-16A-2  
Sheet 2 of 2  
DATE: Start Sept. 22, 1976  
Finish Oct. 14, 1976

[illegible]

Project No. Y263422

**PUMP TEST DATA SUMMARY**

PROJECT Hot Creek Coal  
 Location Cache Creek, B.C.  
 Pumped Well RH 76-19

Observations in RH 17-1  
 Sheet 1 of 8  
 DATE: Start Sept. 22, 1976  
 Finish Oct. 14, 1976

**DATA ON OBSERVATION POINT:**

Datum point Top of tube  
 Depth to static water level 46.5 FT.  
 Screened/open hole interval to

Type: ☐ Screened well ☒ Pneumatic piezo.  
☐ Unscreened well ☐ Standpipe piezo.  
 Datum elevation 3179 FT. a.s.l.  
 Elevation static water level 3132.5 FT. a.s.l.  
 Elevation of screened interval to a.s.l.

**DATA ON PUMPED WELL AND AQUIFER:**

Well depth 400 feet  
 Well diameter 8 inches  
 Pump type Electric Submersible  
 Final pumping rate 0.1 gpm

Aquifer Conditions: ☒ confined ☐ unconfined  
 Aquifer description Coldwater Fm (Siltstone)  
 Aquifer thickness 800 feet  
 Depth to pump suction 370 feet  
 Type of test: ☒ constant rate ☐ step drawdown

| Time |     |      | Elapsed Time<br>"t"<br>(mins.) | Depth to Water<br>(ft.) | Pressure<br>(Pneumatic<br>piezometers<br>only)<br>(p.s.i.) | Elevation<br>of Water<br>(ft.)<br>a.s.l. | Drawdown<br>(ft.) | Pump Rate<br>Q<br>(l.g.p.m.) | Remarks                  |
|------|-----|------|--------------------------------|-------------------------|------------------------------------------------------------|------------------------------------------|-------------------|------------------------------|--------------------------|
| Dy.  | Hr. | Min. |                                |                         |                                                            |                                          |                   |                              |                          |
| 22   | 9   | 00   | 0                              | 46.3                    | 154                                                        | 3132.7                                   |                   |                              |                          |
|      | 16  | 00   | 0                              |                         | -                                                          |                                          | -                 |                              | Pump started             |
|      | 16  | 30   | 30                             | 55.5                    | 150                                                        | 3123.5                                   | 0                 |                              |                          |
|      | 19  | 00   | 180                            | 69.4                    | 144                                                        | 3109.6                                   | 22.9              |                              | Pump stopped @ 150 mins. |
| 23   | 11  | 30   | 1170                           | 76.3                    | 141                                                        | 3102.7                                   | 29.8              |                              |                          |
|      | 19  | 30   | 1650                           | 84.4                    | 137.5                                                      | 2094.6                                   | 37.9              |                              | Pump restarted @ 1290    |
| 24   | 15  | 30   | 2850                           | 75.1                    | 141.5                                                      | 3103.9                                   | 28.6              |                              |                          |
| 25   | 13  | 30   | 4170                           | 82.1                    | 138.5                                                      | 3096.9                                   | 35.6              |                              |                          |
| 27   | 14  | 00   | 7080                           | 78.6                    | 140                                                        | 3100.4                                   | 32.1              |                              |                          |
| 28   | 14  | 30   | 8550                           | 79.8                    | 139.5                                                      | 3099.2                                   | 33.3              |                              |                          |
| 30   | 14  | 00   | 11400                          | 75.1                    | 141.5                                                      | 3103.9                                   | 28.6              |                              |                          |
| 1    | 15  | 45   | 12945                          | 84.4                    | 137.5                                                      | 3094.6                                   | 37.9              |                              |                          |
| 4    | 9   | 30   | 16890                          | 90.1                    | 135                                                        | 3088.9                                   | 43.6              |                              |                          |
| 5    | 13  | 00   | 18540                          | 85.5                    | 137                                                        | 3093.5                                   | 39.0              |                              |                          |
| 6    | 17  | 00   | 20220                          | 85.5                    | 137                                                        | 3093.5                                   | 39.0              |                              |                          |
| 8    | 11  | 00   | 22740                          | 78.6                    | 140                                                        | 3100.4                                   | 32.1              |                              |                          |
| 9    | 9   | 00   | 24060                          | 83.2                    | 138                                                        | 3095.8                                   | 36.7              |                              |                          |
| 10   | 15  | 30   | 25890                          | 79.8                    | 139.5                                                      | 3099.2                                   | 33.3              |                              |                          |
| 11   | 15  | 00   | 27300                          | 79.8                    | 139.5                                                      | 3099.2                                   | 33.3              |                              |                          |
| 13   | 14  | 00   | 30120                          | 80.9                    | 139                                                        | 3098.1                                   | 34.4              |                              |                          |
| 14   | 17  | 30   | 31770                          | 82.1                    | 138.5                                                      | 3096.9                                   | 35.6              |                              | Pump stopped (19:11)     |
| 16   | 11  | 15   |                                | 88.6                    | 140                                                        | 3100.4                                   | 32.1              |                              |                          |
| 18   | 16  | 00   |                                | 84.4                    | 137.5                                                      | 3094.6                                   | 37.9              |                              |                          |
| 22   | 15  | 30   |                                | 85.5                    | 137                                                        | 3093.5                                   | 39.0              |                              |                          |
| 28   | 15  | 30   |                                | 79.8                    | 139.5                                                      | 3099.2                                   | 33.3              |                              |                          |

**Project No. V763480**

Sheet 2 of 3

Pumped Well RH 76-19

DATE: Finish Oct. 14, 1976

[illegible]

## PUMP TEST DATA SUMMARY

PROJECT Hat Creek Coal  
 Location Cache Creek, B.C.  
 Pumped Well RH 76-19

Observations in RH76-17-1  
 Sheet 3 of 3

DATE: Start Sept. 22, 1976  
 Finish Oct. 14, 1976

## DATA ON OBSERVATION POINT:

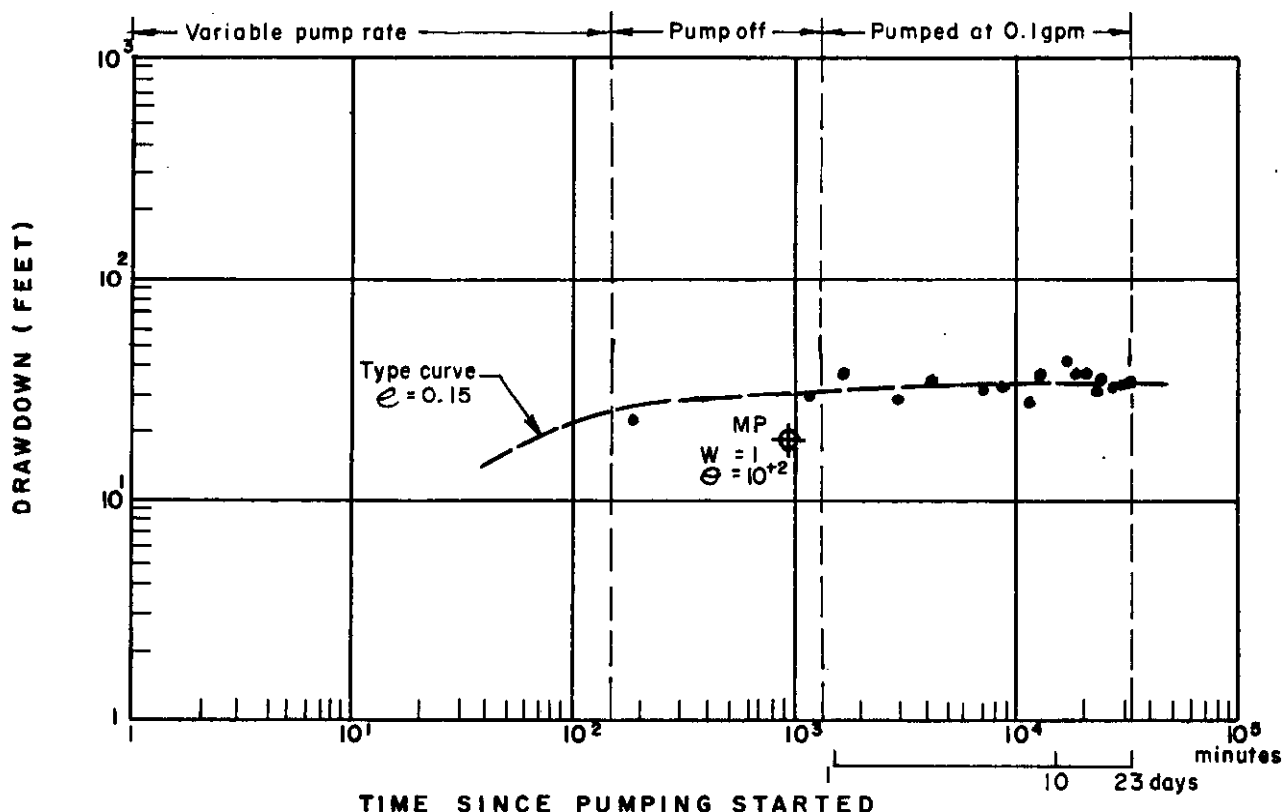
Datum point Top of tube  
 Depth to static water level 46 ft.  
 Screened/open hole interval 391 to 404

Type: ☐ Screened well ☒ Pneumatic piezo.  
☐ Unscreened well ☐ Standpipe piezo.  
 Datum elevation 3179 a. s. l.  
 Elevation static water level 3133 a. s. l.  
 Elevation of screened interval 2788 to 2775 a. s. l.

## DATA ON PUMPED WELL AND AQUIFER:

Well depth 400 feet  
 Well diameter 8 inches  
 Pump type Electric Submersible  
 Final pumping rate 0.1 gpm

Aquifer Conditions: ☒ confined ☐ unconfined  
 Aquifer description Coldwater Fm (Siltstone)  
 Aquifer thickness 800 feet  
 Depth to pump suction 370 feet  
 Type of test: ☒ constant rate ☐ step drawdown



Calculations:  $T = \frac{114.6 QW}{S} = \frac{114.6 \times 0.1 \times 1}{19} = 0.64 \text{ gpd/ft.}$

$S = \frac{Tt}{2693(r^2)\Theta} = \frac{0.64 \times 920}{2693(249)^2 \times 100} = 3.5 \times 10^{-8}$

Where:  $W$  and  $\Theta$  are constant values for a given match point.

$e = \frac{r}{h} \left[ \frac{k_y}{k_h} \right]^{1/2}$

$h$  = thickness of aquifer.

$Q$  = Average pumping rate (gpm)  
 $S$  = Drawdown (feet)  
 $r$  = Radius from pumped well (feet)  
 $t$  = Time (minutes)  
 $S$  = Storage coefficient  
 $T$  = Transmissivity (gpd/ft.)



## PUMP TEST DATA SUMMARY

PROJECT Hot Creek Coal  
 Location Cache Creek, B.C.  
 Pumped Well RH 76-19

Observations in RH 17-2  
 Sheet 1 of 2  
 DATE: Start Sept. 22, 1976  
 Finish Oct. 14, 1976

## DATA ON OBSERVATION POINT:

Datum point Top of tube  
 Depth to static water level 43 FT.  
 Screened/open hole interval to

Type: ☐ Screened well ☒ Pneumatic piezo.  
☐ Unscreened well ☐ Standpipe piezo.  
 Datum elevation 3179 FT. a.s.l.  
 Elevation static water level 3136 FT. a.s.l.  
 Elevation of screened interval to a.s.l.

## DATA ON PUMPED WELL AND AQUIFER:

Well depth 400 feet  
 Well diameter 8 inches  
 Pump type Electric Submersible  
 Final pumping rate 0.1 gpm

Aquifer Conditions: ☒ confined ☐ unconfined  
 Aquifer description Coldwater Fm (Siltstone)  
 Aquifer thickness 800 feet  
 Depth to pump suction 370 feet  
 Type of test: ☒ constant rate ☐ step drawdown

| Time |     |      | Elapsed Time<br>"t"<br>(mins.) | Depth to Water<br>(ft.) | Pressure<br>(Pneumatic piezometers only)<br>(p.s.i.) | Elevation of Water<br>(ft.)<br>a.s.l. | Drawdown<br>(ft.) | Pump Rate<br>Q<br>(l.g.p.m.) | Remarks              |
|------|-----|------|--------------------------------|-------------------------|------------------------------------------------------|---------------------------------------|-------------------|------------------------------|----------------------|
| Dy.  | Hr. | Min. |                                |                         |                                                      |                                       |                   |                              |                      |
| 22   | 9   | 00   | 0                              | 43.2                    | 102.5                                                | 3135.8                                |                   |                              |                      |
|      | 16  | 00   | 0                              | -                       | -                                                    | -                                     |                   |                              | Pump started         |
|      | 16  | 30   | 30                             | 44.4                    | 102                                                  | 3134.6                                | 8.4               |                              |                      |
|      | 19  | 00   | 180                            | 60.5                    | 95                                                   | 3118.5                                | 24.5              |                              |                      |
| 23   | 11  | 30   | 1170                           | 58.2                    | 96                                                   | 3120.8                                | 22.2              |                              |                      |
|      | 19  | 30   | 1650                           | 60.5                    | 95                                                   | 3118.5                                | 24.5              |                              |                      |
| 24   | 15  | 30   | 2850                           | 60.5                    | 95                                                   | 3118.5                                | 24.5              |                              |                      |
| 25   | 13  | 30   | 4170                           | 61.7                    | 94.5                                                 | 3117.3                                | 25.7              |                              |                      |
| 27   | 14  | 00   | 7080                           | 59.4                    | 95.5                                                 | 3119.6                                | 23.4              |                              |                      |
| 28   | 14  | 30   | 8550                           | 62.9                    | 94                                                   | 3116.1                                | 26.9              |                              |                      |
| 30   | 14  | 00   | 11400                          | 61.7                    | 94.5                                                 | 3117.3                                | 25.7              |                              |                      |
| 1    | 15  | 45   | 12945                          | 62.9                    | 94                                                   | 3116.1                                | 26.9              |                              |                      |
| 4    | 9   | 30   | 16890                          | 69.8                    | 91                                                   | 3109.2                                | 33.8              |                              |                      |
| 5    | 13  | 00   | 18540                          | 69.8                    | 91                                                   | 3109.2                                | 33.8              |                              |                      |
| 6    | 17  | 00   | 20220                          | 69.8                    | 91                                                   | 3109.2                                | 33.8              |                              |                      |
| 8    | 11  | 00   | 22740                          | 67.5                    | 92                                                   | 3111.5                                | 31.5              |                              |                      |
| 9    | 9   | 00   | 24060                          | 69.8                    | 91                                                   | 3109.2                                | 33.8              |                              |                      |
| 10   | 15  | 30   | 25890                          | 62.9                    | 94                                                   | 3116.1                                | 26.9              |                              |                      |
| 11   | 15  | 00   | 27300                          | 67.5                    | 92                                                   | 3111.5                                | 31.5              |                              |                      |
| 13   | 14  | 00   | 30120                          | 67.5                    | 92                                                   | 3111.5                                | 31.5              |                              |                      |
| 14   | 17  | 30   | 31770                          | 67.5                    | 92                                                   | 3111.5                                | 31.5              |                              | Pump stopped (19:11) |
| 16   | 11  | 15   |                                | 66.3                    | 92.5                                                 | 3112.7                                | 30.3              |                              |                      |
| 18   | 16  | 00   |                                | 68.6                    | 91.5                                                 | 3110.4                                | 32.6              |                              |                      |
| 22   | 15  | 30   |                                | 67.5                    | 92                                                   | 3111.5                                | 31.5              |                              |                      |
| 28   | 15  | 30   |                                | 66.3                    | 92.5                                                 | 3112.7                                | 30.3              |                              |                      |

Project No. V76348B

Sheet 2 of 2

Location Cache Creek, B.C.

DATE: Start Sept. 22, 1976 - - -

Finish Oct. 14, 1976

## Golder Associates

Logged by - RRB - - - - -

## PUMP TEST DATA SUMMARY

PROJECT Hot Creek Coal  
 Location Cache Creek, B.C.  
 Pumped Well RH 76-19

Observations in RH 76-17-3  
 Sheet 1 of 2

DATE: Start Sept. 22, 1976  
 Finish Oct. 14, 1976

## DATA ON OBSERVATION POINT:

Datum point Top of tube  
 Depth to static water level 56.5 FT.  
 Screened/open hole interval to

Type: ☐ Screened well ☒ Pneumatic piezo.  
☐ Unscreened well ☐ Standpipe piezo.  
 Datum elevation 3179 FT. a. s. l.  
 Elevation static water level 3122.5 FT. a. s. l.  
 Elevation of screened interval to a. s. l.

## DATA ON PUMPED WELL AND AQUIFER:

Well depth 400 feet  
 Well diameter 8 inches  
 Pump type Electric Submersible  
 Final pumping rate 0.1 gpm

Aquifer Conditions: ☒ confined ☐ unconfined  
 Aquifer description Coldwater Fm (Siltstone)  
 Aquifer thickness 800 feet  
 Depth to pump suction 370 feet  
 Type of test: ☒ constant rate ☐ step drawdown

| Time |     |      | Elapsed Time<br>"t"<br>(mins.) | Depth to Water<br>(ft.) | Pressure<br>(Pneumatic<br>piezometers<br>only)<br>(p.s.i.) | Elevation of Water<br>(ft.)<br>a.s.l. | Drawdown<br>(ft.) | Pump Rate<br>Q<br>(g.p.m.) | Remarks              |
|------|-----|------|--------------------------------|-------------------------|------------------------------------------------------------|---------------------------------------|-------------------|----------------------------|----------------------|
| Dy.  | Hr. | Mln. |                                |                         |                                                            |                                       |                   |                            |                      |
| 22   | 9   | 00   | 0                              | 57.4                    | 47                                                         | 3121.6                                |                   |                            |                      |
|      | 16  | 00   | 0                              | -                       | -                                                          | -                                     | -                 |                            | Pump started         |
|      | 16  | 30   | 30                             | 49.3                    | 50.5                                                       | 3129.7                                | -                 |                            |                      |
|      | 19  | 00   | 180                            | 66.7                    | 43                                                         | 3112.3                                | 10.2              |                            |                      |
| 23   | 11  | 30   | 1170                           | 66.7                    | 43                                                         | 3112.3                                | 10.2              |                            |                      |
|      | 19  | 30   | 1650                           | 66.7                    | 43                                                         | 3112.3                                | 10.2              |                            |                      |
| 24   | 15  | 30   | 2850                           | 67.8                    | 42.5                                                       | 3111.2                                | 11.3              |                            |                      |
| 25   | 13  | 30   | 4170                           | 67.8                    | 42.5                                                       | 3111.2                                | 11.3              |                            |                      |
| 27   | 14  | 00   | 7080                           | 66.7                    | 43                                                         | 3112.3                                | 10.2              |                            |                      |
| 28   | 14  | 30   | 8550                           | 72.4                    | 40.5                                                       | 3106.6                                | 15.9              |                            |                      |
| 30   | 14  | 00   | 11400                          | 72.4                    | 40.5                                                       | 3106.6                                | 15.9              |                            |                      |
| 1    | 15  | 45   | 12945                          | 72.4                    | 40.5                                                       | 3106.6                                | 15.9              |                            |                      |
| 4    | 9   | 30   | 16890                          | 71.3                    | 41                                                         | 3107.7                                | 14.8              |                            |                      |
| 5    | 13  | 00   | 18540                          | 71.3                    | 41                                                         | 3107.7                                | 14.8              |                            |                      |
| 6    | 17  | 00   | 20220                          | 71.3                    | 41                                                         | 3107.7                                | 14.8              |                            |                      |
| 8    | 11  | 00   | 22740                          | 71.3                    | 41                                                         | 3107.7                                | 14.8              |                            |                      |
| 9    | 9   | 00   | 24060                          | 74.8                    | 39.5                                                       | 3104.2                                | 18.3              |                            |                      |
| 10   | 15  | 30   | 25890                          | 71.3                    | 41                                                         | 3107.7                                | 14.8              |                            |                      |
| 11   | 15  | 00   | 27300                          | 71.3                    | 41                                                         | 3107.7                                | 14.8              |                            |                      |
| 13   | 14  | 00   | 30120                          | 73.6                    | 40                                                         | 3105.4                                | 17.1              |                            |                      |
| 14   | 17  | 30   | 31770                          | 69.0                    | 42                                                         | 3110.0                                | 12.5              |                            | Pump stopped (19:11) |
| 16   | 11  | 15   |                                | 67.8                    | 42.5                                                       | 3111.2                                | 11.3              |                            |                      |
| 18   | 16  | 00   |                                | 70.1                    | 41.5                                                       | 3108.9                                | 13.6              |                            |                      |
| 22   | 15  | 30   |                                | 67.8                    | 42.5                                                       | 3111.2                                | 11.3              |                            |                      |
| 28   | 15  | 30   |                                | 66.7                    | 43                                                         | 3112.3                                | 10.2              |                            |                      |

Project No. V76348B

Sheet 2 of 2

Pumped Well RH 76-19 - - - - -

DATE: Finish Oct. 14, 1976

[illegible]

Project No. Y263402

# PUMP TEST DATA SUMMARY

PROJECT Hot Creek Coal  
 Location Cache Creek, B.C.  
 Pumped Well RH 76-19

Observations in RH 76-18-1  
 Sheet 1 of 2  
 DATE: Start Sept. 22, 1976  
 Finish Oct. 14, 1976

## DATA ON OBSERVATION POINT:

Datum point Top of tube  
 Depth to static water level 34.7 FT.  
 Screened/open hole interval to

Type: ☐ Screened well ☒ Pneumatic piezo.  
☐ Unscreened well ☐ Standpipe piezo.  
 Datum elevation 3195 FT. a.s.l.  
 Elevation static water level 3160.3 FT. a.s.l.  
 Elevation of screened interval to a.s.l.

## DATA ON PUMPED WELL AND AQUIFER:

Well depth 400 feet  
 Well diameter 8 inches  
 Pump type Electric Submersible  
 Final pumping rate 0.1 gpm

Aquifer Conditions: ☒ confined ☐ unconfined  
 Aquifer description Coldwater Fm (Siltstone)  
 Aquifer thickness 800 feet  
 Depth to pump suction 370 feet  
 Type of test: ☒ constant rate ☐ step drawdown

| Time |     |      | Elapsed Time<br>"t"<br>(mins.) | Depth to Water<br>(ft.) | Pressure<br>(Pneumatic<br>piezometers<br>only)<br>(p.s.i.) | Elevation of Water<br>(ft.)<br>a.s.l. | Drawdown<br>(ft.) | Pump Rate<br>Q<br>(l.g.p.m.) | Remarks              |
|------|-----|------|--------------------------------|-------------------------|------------------------------------------------------------|---------------------------------------|-------------------|------------------------------|----------------------|
| Dy.  | Hr. | Min. |                                |                         |                                                            |                                       |                   |                              |                      |
| 22   | 9   | 00   | 0                              | 32.6                    | 156                                                        | 3162.4                                |                   |                              |                      |
|      | 16  | 00   | 0                              | -                       | -                                                          | -                                     | -                 |                              | Pump started         |
|      | 16  | 30   | 30                             | 46.5                    | 150                                                        | 3198.5                                | 11.8              |                              |                      |
|      | 19  | 00   | 180                            | 56.9                    | 145.5                                                      | 3138.1                                | 22.2              |                              |                      |
| 23   | 11  | 30   | 1170                           | 63.8                    | 142.5                                                      | 3131.2                                | 29.1              |                              |                      |
|      | 19  | 30   | 1650                           | 69.6                    | 140                                                        | 3125.4                                | 34.9              |                              |                      |
| 24   | 15  | 30   | 2850                           | 63.8                    | 142.5                                                      | 3131.2                                | 29.1              |                              |                      |
| 25   | 13  | 30   | 4170                           | 66.1                    | 141.5                                                      | 3128.9                                | 31.4              |                              |                      |
| 27   | 14  | 00   | 7080                           | 62.7                    | 143                                                        | 3132.3                                | 28.0              |                              |                      |
| 28   | 14  | 30   | 8550                           | 62.7                    | 143                                                        | 3132.3                                | 28.0              |                              |                      |
| 30   | 14  | 00   | 11400                          | 62.7                    | 143                                                        | 3132.3                                | 28.0              |                              |                      |
| 1    | 15  | 45   | 12945                          | 69.6                    | 140                                                        | 3125.4                                | 34.9              |                              |                      |
| 4    | 9   | 30   | 16890                          | 76.5                    | 137                                                        | 3118.5                                | 41.8              |                              |                      |
| 5    | 13  | 00   | 18540                          | 74.2                    | 138                                                        | 3120.8                                | 39.5              |                              |                      |
| 6    | 17  | 00   | 20220                          | 71.9                    | 139                                                        | 3123.1                                | 37.2              |                              |                      |
| 8    | 11  | 00   | 22740                          | 76.5                    | 137                                                        | 3118.5                                | 41.8              |                              |                      |
| 9    | 9   | 00   | 24060                          | 74.2                    | 138                                                        | 3120.8                                | 39.5              |                              |                      |
| 10   | 15  | 30   | 25890                          | 71.9                    | 139                                                        | 3123.1                                | 37.2              |                              |                      |
| 11   | 15  | 00   | 27300                          | 74.2                    | 138                                                        | 3120.8                                | 39.5              |                              |                      |
| 13   | 14  | 00   | 30120                          | 70.8                    | 139.5                                                      | 3124.2                                | 36.1              |                              |                      |
| 14   | 17  | 30   | 31770                          | 74.2                    | 138                                                        | 3120.8                                | 39.5              |                              | Pump stopped (19:11) |
| 16   | 11  | 15   |                                | 73.1                    | 138.5                                                      | 3121.9                                | 38.4              |                              |                      |
| 18   | 16  | 00   |                                | 74.2                    | 138                                                        | 3120.8                                | 39.5              |                              |                      |
| 22   | 15  | 30   |                                | 69.6                    | 140                                                        | 3125.4                                | 34.9              |                              |                      |
| 28   | 15  | 30   |                                | 69.6                    | 140                                                        | 3125.4                                | 34.9              |                              |                      |

Project No. V76348B-

Sheet 2 of 2

Pumped Well   RH 76-19   - - - - -

DATE. Finish Oct. 14, 1976 \_ \_ \_

[illegible]

## PUMP TEST DATA SUMMARY

PROJECT Hot Creek Coal  
 Location Cache Creek, B.C.  
 Pumped Well RH 76-19

Observations in RH 76-18-2  
 Sheet 1 of 3

DATE: Start Sept. 22, 1976  
 Finish Oct. 14, 1976

## DATA ON OBSERVATION POINT:

Datum point Top of tube  
 Depth to static water level 25.5 FT.  
 Screened/open hole interval      to     

Type: ☐ Screened well ☒ Pneumatic piezo.  
☐ Unscreened well ☐ Standpipe piezo.  
 Datum elevation 3195 FT. a.s.l.  
 Elevation static water level 3169.5 FT. a.s.l.  
 Elevation of screened interval      to      a.s.l.

## DATA ON PUMPED WELL AND AQUIFER:

Well depth 400 feet  
 Well diameter 8 inches  
 Pump type Electric Submersible  
 Final pumping rate 0.1 gpm

Aquifer Conditions: ☒ confined ☐ unconfined  
 Aquifer description Coldwater Fm (Siltstone)  
 Aquifer thickness 800 feet  
 Depth to pump suction 370 feet  
 Type of test: ☒ constant rate ☐ step drawdown

| Time |     |      | Elapsed Time<br>" "<br>(mins.) | Depth to Water<br>(ft.) | Pressure<br>(Pneumatic<br>piezometers<br>only)<br>(p.s.i.) | Elevation<br>of Water<br>(ft.)<br>a.s.l. | Drawdown<br>(ft.) | Pump Rate<br>Q<br>(l.g.p.m.) | Remarks              |
|------|-----|------|--------------------------------|-------------------------|------------------------------------------------------------|------------------------------------------|-------------------|------------------------------|----------------------|
| Dy.  | Hr. | Min. |                                |                         |                                                            |                                          |                   |                              |                      |
| 22   | 9   | 00   | 0                              | 20.9                    | 118                                                        | 3174.1                                   |                   |                              |                      |
|      | 16  | 00   | 0                              | -                       | -                                                          | -                                        | -                 |                              | Pump started         |
|      | 16  | 30   | 30                             | 10.5                    | 122.5                                                      | 3184.5                                   | -                 |                              |                      |
|      | 19  | 00   | 180                            | 44.0                    | 108                                                        | 3151.0                                   | 18.5              |                              |                      |
| 23   | 11  | 30   | 1170                           | 47.5                    | 106.5                                                      | 3147.5                                   | 22                |                              |                      |
|      | 19  | 30   | 1650                           | 49.8                    | 105.5                                                      | 3145.2                                   | 24.3              |                              |                      |
| 24   | 15  | 30   | 2850                           | 48.4                    | 110                                                        | 3146.6                                   | 22.9              |                              |                      |
| 25   | 13  | 30   | 4170                           | 46.3                    | 107                                                        | 3148.7                                   | 20.8              |                              |                      |
| 27   | 14  | 00   | 7080                           | 40.6                    | 109.5                                                      | 3154.4                                   | 15.1              |                              |                      |
| 28   | 14  | 30   | 8550                           | 41.7                    | 109                                                        | 3153.3                                   | 16.2              |                              |                      |
| 30   | 14  | 00   | 11400                          | 46.3                    | 107                                                        | 3148.7                                   | 20.8              |                              |                      |
| 1    | 15  | 45   | 12945                          | 48.4                    | 106                                                        | 3146.4                                   | 23.1              |                              |                      |
| 4    | 9   | 30   | 16890                          | 53.3                    | 104                                                        | 3141.7                                   | 27.8              |                              |                      |
| 5    | 13  | 00   | 18540                          | 50.9                    | 105                                                        | 3144.1                                   | 25.4              |                              |                      |
| 6    | 17  | 00   | 20220                          | 50.9                    | 105                                                        | 3144.1                                   | 25.4              |                              |                      |
| 8    | 11  | 00   | 22740                          | 53.3                    | 104                                                        | 3141.7                                   | 27.8              |                              |                      |
| 9    | 9   | 00   | 24060                          | 52.1                    | 104.5                                                      | 3142.9                                   | 26.6              |                              |                      |
| 10   | 15  | 30   | 25890                          | 50.9                    | 105                                                        | 3144.1                                   | 25.4              |                              |                      |
| 11   | 15  | 00   | 27300                          | 52.1                    | 104.5                                                      | 3142.9                                   | 26.6              |                              |                      |
| 13   | 14  | 00   | 30120                          | 50.9                    | 105                                                        | 3144.1                                   | 25.4              |                              |                      |
| 14   | 17  | 30   | 31770                          | 53.3                    | 104                                                        | 3141.7                                   | 27.8              |                              | Pump stopped (19:11) |
| 16   | 11  | 15   |                                | 50.9                    | 105                                                        | 3144.1                                   | 25.4              |                              |                      |
| 18   | 16  | 00   |                                | 50.9                    | 105                                                        | 3144.1                                   | 25.4              |                              |                      |
| 22   | 15  | 30   |                                | 50.9                    | 105                                                        | 3144.1                                   | 25.4              |                              |                      |
| 28   | 15  | 30   |                                | 50.9                    | 105                                                        | 3144.1                                   | 25.4              |                              |                      |





Project No. 1763002

# PUMP TEST DATA SUMMARY

PROJECT Hot Creek Coal  
 Location Cache Creek, B.C.  
 Pumped Well RH 76-19

Observations in RH 76-18-2  
 Sheet 3 of 3  
 DATE: Start Sept. 22, 1976  
 Finish Oct. 14, 1976

## DATA ON OBSERVATION POINT:

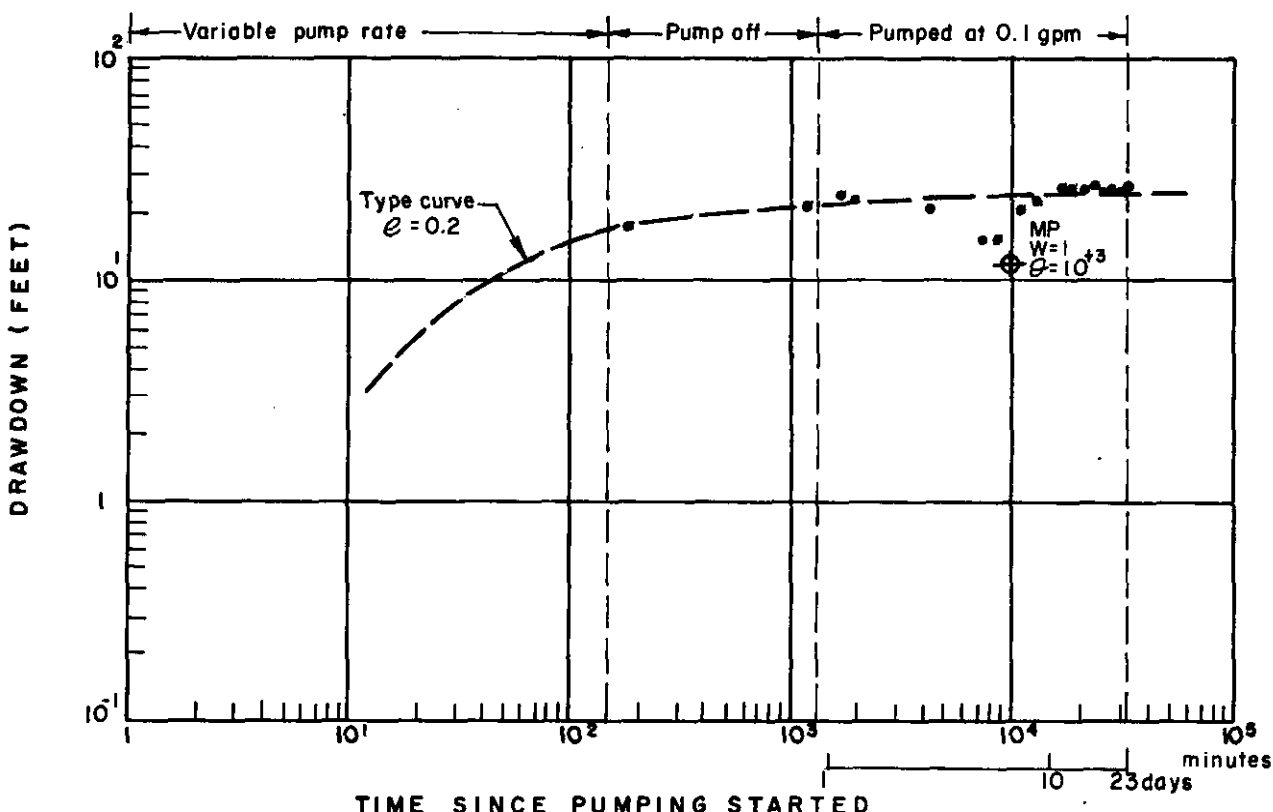
Datum point Top of tube  
 Depth to static water level 21 ft.  
 Screened/open hole interval 282 to 285 ft.

Type: ☒ Screened well ☒ Pneumatic piezo.  
☐ Unscreened well ☐ Standpipe piezo.  
 Datum elevation 3195 a.s.l.  
 Elevation static water level 3174 a.s.l.  
 Elevation of screened interval 2913 to 2910 a.s.l.

## DATA ON PUMPED WELL AND AQUIFER:

Well depth 400 feet  
 Well diameter 8 inches  
 Pump type Electric Submersible  
 Final pumping rate 0.1 gpm

Aquifer Conditions: ☒ confined ☐ unconfined  
 Aquifer description Coldwater Fm (Siltstone)  
 Aquifer thickness 800 feet  
 Depth to pump suction 370 feet  
 Type of test: ☒ constant rate ☐ step drawdown



Calculations:  $T = \frac{114.6 QW}{S} = \frac{114.6 \times 0.1 \times 1}{12} = 0.96 \text{ gpd/ft.}$

$S = \frac{Tt}{2693(r^2)\theta} = \frac{0.96 \times 10^4}{2693(357)^2 \times 10^{-3}} = 2.8 \times 10^{-8}$

Where:  $W$  and  $\theta$  are constant values for a given match point.  
 $e = \frac{r}{h} \left[ \frac{k_v}{k_h} \right]^{1/2}$   
 $h$  = thickness of aquifer.

$Q$  = Average pumping rate (gpm)  
 $S$  = Drawdown (feet)  
 $r$  = Radius from pumped well (feet)  
 $t$  = Time (minutes)  
 $S$  = Storage coefficient  
 $T$  = Transmissivity (gpd/ft.)

Project No. Y26340A**PUMP TEST DATA SUMMARY**

PROJECT Hot Creek Coal  
 Location Cache Creek, B.C.  
 Pumped Well RH 76-19

Observations in RH 76-19-3  
 Sheet 1 of 2

DATE: Start Sept. 22, 1976  
 Finish Oct. 14, 1976

**DATA ON OBSERVATION POINT:**

Datum point Top of tube  
 Depth to static water level 14 FT.  
 Screened/open hole interval to

Type: ☐ Screened well ☒ Pneumatic piezo.  
☐ Unscreened well ☐ Standpipe piezo.  
 Datum elevation 3195 FT. a.s.l.  
 Elevation static water level 3181 FT. a.s.l.  
 Elevation of screened interval to a.s.l.

**DATA ON PUMPED WELL AND AQUIFER:**

Well depth 400 feet  
 Well diameter 8 inches  
 Pump type Electric Submersible  
 Final pumping rate 0.1 gpm

Aquifer Conditions: ☒ confined ☐ unconfined  
 Aquifer description Coldwater Fm (Siltstone)  
 Aquifer thickness 800 feet  
 Depth to pump suction 370 feet  
 Type of test: ☒ constant rate ☐ step drawdown

| Time |     |      | Elapsed Time<br>"t"<br>(mins.) | Depth to Water<br>(ft.) | Pressure<br>(Pneumatic<br>piezometers<br>only)<br>(p.s.f.) | Elevation of Water<br>(ft.)<br>a.s.l. | Drawdown<br>(ft.) | Pump Rate<br>Q<br>(l.g.p.m.) | Remarks              |
|------|-----|------|--------------------------------|-------------------------|------------------------------------------------------------|---------------------------------------|-------------------|------------------------------|----------------------|
| Dy.  | Hr. | Min. |                                |                         |                                                            |                                       |                   |                              |                      |
| 22   | 9   | 00   | 0                              | 6.0                     | 80.5                                                       | 3189                                  | -                 |                              |                      |
|      | 16  | 00   | 0                              |                         | -                                                          | -                                     | -                 |                              | Pump started         |
|      | 16  | 30   | 30                             | 14.1                    | 77                                                         | 3180.9                                | .1                |                              |                      |
|      | 19  | 00   | 180                            | 24.5                    | 72.5                                                       | 3170.5                                | 10.5              |                              |                      |
| 23   | 11  | 30   | 1170                           | 31.5                    | 69.5                                                       | 3163.5                                | 17.5              |                              |                      |
|      | 19  | 30   | 1650                           | 28                      | 71                                                         | 3167.0                                | 14.0              |                              |                      |
| 24   | 15  | 30   | 2850                           | 26.8                    | 71.5                                                       | 3168.2                                | 12.8              |                              |                      |
| 25   | 13  | 30   | 4170                           | 31.5                    | 69.5                                                       | 3163.5                                | 17.5              |                              |                      |
| 27   | 14  | 00   | 7080                           | 28                      | 71                                                         | 3167.0                                | 14.0              |                              |                      |
| 28   | 14  | 30   | 8550                           | 28                      | 71                                                         | 3167.0                                | 14.0              |                              |                      |
| 30   | 14  | 00   | 11400                          | 36.1                    | 67.5                                                       | 3158.9                                | 22.1              |                              |                      |
| 1    | 15  | 45   | 12945                          | 36.1                    | 67.5                                                       | 3158.9                                | 22.1              |                              |                      |
| 4    | 9   | 30   | 16890                          | 39.5                    | 66                                                         | 3155.5                                | 25.5              |                              |                      |
| 5    | 13  | 00   | 18540                          | 41.8                    | 65                                                         | 3153.2                                | 27.8              |                              |                      |
| 6    | 17  | 00   | 20220                          | 39.5                    | 66                                                         | 3155.5                                | 25.5              |                              |                      |
| 8    | 11  | 00   | 22740                          | 39.5                    | 66                                                         | 3155.5                                | 25.5              |                              |                      |
| 9    | 9   | 00   | 24060                          | 40.3                    | 65.5                                                       | 3154.7                                | 26.3              |                              |                      |
| 10   | 15  | 30   | 25890                          | 39.5                    | 66                                                         | 3155.5                                | 25.5              |                              |                      |
| 11   | 15  | 00   | 27300                          | 39.5                    | 66                                                         | 3155.5                                | 25.5              |                              |                      |
| 13   | 14  | 00   | 30120                          | 37.2                    | 67                                                         | 3157.8                                | 23.2              |                              |                      |
| 14   | 17  | 30   | 31770                          | 40.3                    | 65.5                                                       | 3154.3                                | 26.7              |                              | Pump stopped (19:11) |
| 16   | 11  | 15   |                                | 39.5                    | 66                                                         | 3155.5                                | 25.5              |                              |                      |
| 18   | 16  | 00   |                                | 39.5                    | 66                                                         | 3155.5                                | 25.5              |                              |                      |
| 22   | 15  | 30   |                                | 38.4                    | 66.5                                                       | 3156.6                                | 24.4              |                              |                      |
| 28   | 15  | 30   |                                | 37.2                    | 67                                                         | 3157.8                                | 23.2              |                              |                      |

Project No. V76348B

Sheet 2 of 2

Location CACHE CREEK, B.C.

DATE: Start SEPT, 22, 1976

Finish OCT. 14, 1976

Logged by     Pao

## PUMP TEST DATA SUMMARY

PROJECT Hot Creek Coal  
 Location Cache Creek, B.C.  
 Pumped Well RH 76-19

Observations in RH 76-19  
 Sheet 1 of 6  
 DATE: Start Sept. 22, 1976  
 Finish Oct. 14, 1976

## DATA ON OBSERVATION POINT:

Datum point Top of tube  
 Depth to static water level 89.3 FT.  
 Screened/open hole interval to

Type: ☒ Screened well ☐ Pneumatic piezo.  
☐ Unscreened well ☐ Standpipe piezo.  
 Datum elevation 3183.5 FT. a.s.l.  
 Elevation static water level 3094.2 FT. a.s.l.  
 Elevation of screened interval to a.s.l.

## DATA ON PUMPED WELL AND AQUIFER:

Well depth 400 feet  
 Well diameter 8 inches  
 Pump type Electric Submersible  
 Final pumping rate 0.1 gpm

Aquifer Conditions: ☒ confined ☐ unconfined  
 Aquifer description Coldwater Fm (Siltstone)  
 Aquifer thickness 800 feet  
 Depth to pump suction 370 feet  
 Type of test: ☒ constant rate ☐ step drawdown

| Time     | Elapsed Time "t" (mins.) |     |      | Depth to Water (ft.) | Pressure (Pneumatic piezometers only) (p.s.i.) | Elevation of Water (ft.) a.s.l. | Drawdown (ft.) | Pump Rate Q (l.g.p.m.) | Remarks                   |
|----------|--------------------------|-----|------|----------------------|------------------------------------------------|---------------------------------|----------------|------------------------|---------------------------|
|          | Dy.                      | Hr. | Min. |                      |                                                |                                 |                |                        |                           |
| 22 16 00 |                          |     | 0    | 89.3                 |                                                | 3094.2                          | 0              | 1.0                    | W.L. probe on the blink   |
|          |                          |     | ½    | -                    |                                                | -                               | -              | 1.0                    | W.L. probe on the blink   |
|          |                          |     | 1    | -                    |                                                | -                               | -              | 1.0                    |                           |
|          |                          |     | 1½   | 93.4                 |                                                | 3090.1                          | 4.1            | 1.0                    |                           |
|          |                          |     | 2    | 90.2                 |                                                | 3093.3                          | 0.9            | 1.0                    |                           |
|          |                          |     | 2½   | 90.3                 |                                                | 3093.2                          | 1.0            | 1.0                    |                           |
|          |                          |     | 3    | 90.4                 |                                                | 3093.1                          | 1.1            | 1.0                    |                           |
|          |                          |     | 3½   | 90.5                 |                                                | 3093.0                          | 1.2            | 1.0                    |                           |
|          |                          |     | 4    | 90.7                 |                                                | 3092.8                          | 1.4            | 1.0                    | Q varied from 0.9-1.1     |
|          |                          |     | 4½   | 90.9                 |                                                | 3092.6                          | 1.6            | 1.0                    | due to siltation in valve |
|          |                          |     | 5    | 91.0                 |                                                | 3092.5                          | 1.7            | 1.0                    |                           |
|          |                          |     | 6    | 91.3                 |                                                | 3092.2                          | 2.0            | 1.0                    |                           |
|          |                          |     | 7    | 91.5                 |                                                | 3092.0                          | 2.2            | 1.0                    |                           |
|          |                          |     | 8    | -                    |                                                | -                               | -              | 1.0                    | W.L. probe problems       |
|          |                          |     | 9    | 92.3                 |                                                | 3091.2                          | 3.0            | 1.0                    |                           |
|          |                          |     | 10   | 92.5                 |                                                | 3091.0                          | 3.2            | 1.0                    |                           |
|          |                          |     | 12   | 93.2                 |                                                | 3090.3                          | 3.9            | 1.0                    |                           |
|          |                          |     | 14   | 93.7                 |                                                | 3089.8                          | 4.4            | 1.0                    |                           |
|          |                          |     | 16   | 94.2                 |                                                | 3089.3                          | 4.9            | 1.0                    | Water temp = 9.5°C        |
|          |                          |     | 18   | 94.7                 |                                                | 3088.8                          | 5.4            | 1.0                    |                           |
|          |                          |     | 20   | 95.2                 |                                                | 3088.3                          | 5.9            | 1.0                    |                           |
|          |                          |     | 25   | 96.7                 |                                                | 3086.8                          | 7.4            | 1.0                    |                           |
|          |                          |     | 30   | 98.4                 |                                                | 3085.1                          | 9.1            | 1.0                    |                           |
|          |                          |     | 45   | 102.6                |                                                | 3080.9                          | 13.3           | 1.0                    |                           |
| 22 17 00 |                          |     | 60   | -                    |                                                | -                               | -              | 1.0                    | Generator problems        |

Project No. V76348A

## PUMP TEST DATA SUMMARY

PROJECT HAT CREEK COAL  
 Location CACHE CREEK, B.C.  
 Pumped Well RH 76-19

Observations in RH 76-19  
 Sheet 2 of 6  
 DATE: Start SEPT. 22/76  
 Finish OCT. 14/76

| Time |     |      | Elapsed Time<br>"t"<br>(mins.) | Depth to<br>Water<br>(ft.) | Pressure<br>(Pneumatic<br>piezometers<br>only)<br>(p.s.i.) | Elevation<br>of<br>Water<br>(ft.)<br>a.s.l. | Drawdown<br>(ft.) | Pump<br>Rate<br>Q<br>(g.p.m.) | Remarks                    |
|------|-----|------|--------------------------------|----------------------------|------------------------------------------------------------|---------------------------------------------|-------------------|-------------------------------|----------------------------|
| Dy.  | Hr. | Min. |                                |                            |                                                            |                                             |                   |                               |                            |
| 22   | 17  | 30   | 90                             | 105.8                      |                                                            | 3077.7                                      | 16.5              | 1.0                           | Conductivity = 1300 micro- |
|      | 18  | 0    | 120                            | 111.2                      |                                                            | 3072.3                                      | 21.9              | 1.0                           | mhos/cm.                   |
|      | 18  | 30   | 150                            | 113.9                      |                                                            | 3069.6                                      | 24.6              | 1.0                           |                            |
|      | 19  | 00   | 180                            | -                          |                                                            | -                                           | -                 | 1.0                           | Test discontinued due to   |
|      |     |      |                                |                            |                                                            |                                             |                   |                               | generator problems         |
| 23   | 13  | 30½  | 1290½                          | 105.1                      |                                                            | 3078.4                                      | 15.8              | 1.0                           | Pumping resumed.           |
|      |     | 31   | 1291                           | 105.3                      |                                                            | 3078.2                                      | 16.0              | 1.0                           | Water - creamy, silty      |
|      |     | 31½  | 1291½                          | 105.4                      |                                                            | 3078.1                                      | 16.1              | 1.0                           |                            |
|      |     | 32   | 1292                           | 105.6                      |                                                            | 3077.9                                      | 16.3              | 1.0                           |                            |
|      |     | 32½  | 1292½                          | 105.6                      |                                                            | 3077.9                                      | 16.3              | 1.0                           |                            |
|      |     | 33   | 1293                           | 105.7                      |                                                            | 3077.8                                      | 16.4              | 1.0                           |                            |
|      |     | 33½  | 1293½                          | 105.8                      |                                                            | 3077.7                                      | 16.5              | 1.0                           |                            |
|      |     | 34   | 1294                           | 105.9                      |                                                            | 3077.6                                      | 16.6              | 1.0                           |                            |
|      |     | 34½  | 1294½                          | 106.0                      |                                                            | 3077.5                                      | 16.7              | 1.0                           |                            |
|      |     | 35   | 1295                           | 106.1                      |                                                            | 3077.4                                      | 16.8              | 1.0                           |                            |
|      |     | 36   | 1296                           | 106.3                      |                                                            | 3077.2                                      | 17.0              | 1.0                           |                            |
|      |     | 37   | 1297                           | 106.5                      |                                                            | 3077.0                                      | 17.2              | 1.0                           |                            |
|      |     | 38   | 1298                           | 106.7                      |                                                            | 3076.8                                      | 17.4              | 1.0                           |                            |
|      |     | 39   | 1299                           | 106.9                      |                                                            | 3076.6                                      | 17.6              | 1.0                           |                            |
|      |     | 40   | 1300                           | 107.2                      |                                                            | 3076.3                                      | 17.9              | 1.0                           |                            |
|      |     | 42   | 1302                           | 107.7                      |                                                            | 3075.8                                      | 18.4              | 1.0                           |                            |
|      |     | 44   | 1304                           | 108.0                      |                                                            | 3075.5                                      | 18.7              | 1.0                           |                            |
|      |     | 46   | 1306                           | 108.4                      |                                                            | 3075.1                                      | 19.1              | 1.0                           |                            |
|      |     | 48   | 1308                           | 108.8                      |                                                            | 3074.7                                      | 19.5              | 1.0                           |                            |
|      |     | 50   | 1310                           | 109.4                      |                                                            | 3074.1                                      | 20.1              | 1.0                           |                            |
|      |     | 55   | 1315                           | 110.5                      |                                                            | 3073.0                                      | 21.2              | 1.0                           |                            |
|      | 14  | 0    | 1320                           | 112.1                      |                                                            | 3071.4                                      | 22.8              | 1.0                           |                            |
|      |     | 10   | 1330                           | 114.2                      |                                                            | 3069.3                                      | 24.9              | 1.0                           |                            |
|      |     | 20   | 1340                           | 116.9                      |                                                            | 3066.6                                      | 27.6              | 1.0                           |                            |
|      |     | 30   | 1350                           | -                          |                                                            | -                                           | -                 | 1.0                           |                            |
|      |     | 50   | 1370                           | 120.0                      |                                                            | 3063.5                                      | 30.7              | 1.0                           |                            |
|      | 15  | 10   | 1390                           | 122.5                      |                                                            | 3061.0                                      | 33.2              | 1.0                           |                            |
| 23   |     | 35   | 1415                           | 128.2                      |                                                            | 3055.3                                      | 38.9              | 1.0                           |                            |

Project No. Y76348B

## PUMP TEST DATA SUMMARY

PROJECT HAT CREEK COAL  
 Location CACHE CREEK, B.C.  
 Pumped Well RH 76-19

Observations in RH 76-19  
 Sheet 3 of 6  
 DATE: Start SEPT. 22/76  
 Finish OCT. 14/76

| Time |     |     | Elapsed Time<br>"t"<br>(mins.) | Depth to<br>Water<br>(ft.) | Pressure<br>(Pneumatic<br>plezometers<br>only)<br>(p.s.i.) | Elevation<br>of<br>Water<br>(ft.)<br>a.s.l. | Drawdown<br>(ft.) | Pump<br>Rate<br>Q<br>(g.p.m.) | Remarks                             |
|------|-----|-----|--------------------------------|----------------------------|------------------------------------------------------------|---------------------------------------------|-------------------|-------------------------------|-------------------------------------|
| Dy.  | Hr. | Mn. |                                |                            |                                                            |                                             |                   |                               |                                     |
| 23   | 16  | 0   | 1440                           | 131.5                      |                                                            | 3052.0                                      | 42.2              | 1.0                           | Water colour - very silty           |
|      |     | 40  | 1480                           | 137.4                      |                                                            | 3046.1                                      | 48.1              | 1.0                           | dirty appearance                    |
|      | 17  | 30  | 1530                           | 143.4                      |                                                            | 3040.1                                      | 54.1              | 1.0                           |                                     |
|      | 18  | 20  | 1580                           | 145.3                      |                                                            | 3038.2                                      | 56.0              | 1.0                           |                                     |
|      | 19  | 10  | 1630                           | 147.2                      |                                                            | 3036.3                                      | 57.9              | 1.0                           |                                     |
|      | 20  | 0   | 1680                           | 154.3                      |                                                            | 3029.2                                      | 65.0              | 1.0                           |                                     |
|      | 20  | 50  | 1730                           | -                          |                                                            | -                                           | -                 | 1.0                           |                                     |
|      | 21  | 40  | 1780                           | 159.9                      |                                                            | 3023.6                                      | 70.6              | 1.0                           |                                     |
|      | 22  | 30  | 1830                           | 163.2                      |                                                            | 3020.3                                      | 73.9              | 1.0                           |                                     |
|      | 23  | 20  | 1880                           | 168.2                      |                                                            | 3015.3                                      | 78.9              | 1.0                           |                                     |
| 24   | 0   | 10  | 1930                           | 176.7                      |                                                            | 3006.8                                      | 87.4              | 1.0                           |                                     |
|      | 1   | 0   | 1980                           | 182.5                      |                                                            | 3001.0                                      | 93.2              | 1.0                           |                                     |
|      | 1   | 50  | 2030                           | 189.6                      |                                                            | 2993.9                                      | 100.3             | 1.0                           |                                     |
|      | 4   | 30  | 2190                           | -                          |                                                            | -                                           | -                 | 1.0                           |                                     |
|      | 5   | 20  | 2240                           | 214.6                      |                                                            | 2968.9                                      | 125.3             | 1.0                           |                                     |
|      | 7   | 50  | 2390                           | 242.8                      |                                                            | 2940.7                                      | 153.5             | 1.0                           |                                     |
|      | 8   | 40  | 2440                           | 253.6                      |                                                            | 2929.9                                      | 164.3             | 1.0                           |                                     |
|      | 9   | 30  | 2490                           | 260.3                      |                                                            | 2923.2                                      | 171.0             | 1.0                           |                                     |
|      | 10  | 20  | 2540                           | 269.8                      |                                                            | 2913.7                                      | 180.5             | 1.0                           |                                     |
|      | 11  | 10  | 2590                           | 278.7                      |                                                            | 2904.8                                      | 189.4             | 1.0                           |                                     |
|      | 12  | 0   | 2640                           | 284.3                      |                                                            | 2899.2                                      | 195.0             | 1.0                           |                                     |
|      | 12  | 50  | 2690                           | 290.2                      |                                                            | 2893.3                                      | 200.9             | 1.0                           |                                     |
|      | 13  | 40  | 2740                           | 298.4                      |                                                            | 2885.1                                      | 209.1             | 1.0                           |                                     |
|      | 14  | 30  | 2790                           | 302.9                      |                                                            | 2880.6                                      | 213.6             | 1.0                           |                                     |
|      | 15  | 20  | 2840                           | 307.8                      |                                                            | 2875.7                                      | 218.5             | 1.0                           |                                     |
|      | 16  | 10  | 2890                           | 310.8                      |                                                            | 2872.7                                      | 221.5             | $\frac{1}{2}$                 | Flow adjusted to $\frac{1}{2}$ gpm. |
|      | 17  | 0   | 2940                           | 312.4                      |                                                            | 2871.1                                      | 223.1             | $\frac{1}{2}$                 |                                     |
|      | 17  | 50  | 2990                           | 317.4                      |                                                            | 2866.1                                      | 228.1             | $\frac{1}{2}$                 |                                     |
|      | 18  | 40  | 3040                           | -                          |                                                            | -                                           | -                 | $\frac{1}{2}$                 | Adjustment to flow                  |
|      | 19  | 30  | 3090                           | 317.2                      |                                                            | 2866.3                                      | 227.9             | $\frac{1}{2}$                 |                                     |
|      | 20  | 20  | 3140                           | 318.8                      |                                                            | 2864.7                                      | 229.5             | $\frac{1}{2}$                 |                                     |
|      | 21  | 10  | 3190                           | 320.6                      |                                                            | 2862.9                                      | 231.3             | $\frac{1}{2}$                 |                                     |
| 24   | 22  | 00  | 3240                           | 321.9                      |                                                            | 2861.6                                      | 232.6             | $\frac{1}{2}$                 |                                     |

Project No. 176348B

## PUMP TEST DATA SUMMARY

PROJECT HAT CREEK COAL  
 Location CACHE CREEK, B.C.  
 Pumped Well RH 76-19

Observations in RH 76-19

Sheet 4 of 6

DATE: Start SEPT. 22/76  
 Finish OCT. 14/76

| Time |     |      | Elapsed Time<br>"t"<br>(mins.) | Depth to Water<br>(ft.) | Pressure<br>(Pneumatic<br>piezometers<br>only)<br>(p.s.i.) | Elevation of Water<br>(ft.)<br>a.s.l. | Drawdown<br>(ft.) | Pump Rate<br>Q<br>(i.g.p.m.) | Remarks                     |
|------|-----|------|--------------------------------|-------------------------|------------------------------------------------------------|---------------------------------------|-------------------|------------------------------|-----------------------------|
| Dy.  | Hr. | Min. |                                |                         |                                                            |                                       |                   |                              |                             |
| 24   | 22  | 50   | 3290                           | 322.9                   |                                                            | 2860.6                                | 233.6             | 1/2                          |                             |
|      | 23  | 40   | 3340                           | 324.5                   |                                                            | 2859.0                                | 235.2             | 1/2                          |                             |
| 25   | 0   | 30   | 3390                           | 326.0                   |                                                            | 2857.5                                | 236.7             | 1/2                          |                             |
|      | 1   | 20   | 3440                           | 327.2                   |                                                            | 2856.3                                | 237.9             | 1/2                          |                             |
|      | 2   | 10   | 3490                           | 329.5                   |                                                            | 2854.0                                | 240.2             | 1/2                          |                             |
|      | 3   | 00   | 3540                           | 330.4                   |                                                            | 2853.1                                | 241.1             | 1/2                          |                             |
|      | 3   | 50   | 3590                           | 331.4                   |                                                            | 2852.1                                | 242.1             | 1/2                          |                             |
|      | 4   | 40   | 3640                           | 331.4                   |                                                            | 2852.1                                | 242.1             | 1/2                          |                             |
|      | 5   | 30   | 3690                           | 332.6                   |                                                            | 2850.9                                | 243.3             | 1/2                          |                             |
|      | 6   | 20   | 3740                           | 334.3                   |                                                            | 2849.2                                | 245.0             | 1/2                          | Adjustment of flow          |
|      | 7   | 10   | 3790                           | 336.0                   |                                                            | 2847.5                                | 246.7             | 1/2                          |                             |
|      | 8   | 00   | 3840                           | 338.0                   |                                                            | 2845.5                                | 248.7             | 1/2                          |                             |
|      | 10  | 0    | 3960                           | 335.4                   |                                                            | 2848.1                                | 246.1             | 1/2                          |                             |
|      | 11  | 0    | 4020                           | 336.7                   |                                                            | 2846.8                                | 247.4             | 1/2                          | Water clearing; still silty |
|      | 11  | 50   | 4070                           | 336.5                   |                                                            | 2847.0                                | 247.2             | 1/2                          |                             |
|      | 15  | 00   | 4260                           | 337.3                   |                                                            | 2846.2                                | 248.0             | 20 oz/m.                     | Flow adjusted to 20 oz/min. |
|      | 17  | 00   | 4380                           | 339.0                   |                                                            | 2844.5                                | 249.7             | 20 oz/m.                     |                             |
|      | 18  | 00   | 4440                           | 337.5                   |                                                            | 2846.0                                | 248.2             | 4 oz/m.                      |                             |
| 25   | 21  | 00   | 4620                           | 334.5                   |                                                            | 2849.0                                | 245.2             | 10 oz/m.                     | Flow adjusted to 10 oz/min. |
| 26   | 2   | 00   | 4920                           | 325.3                   |                                                            | 2858.2                                | 236.0             | 10 oz/m.                     |                             |
|      | 6   | 00   | 5160                           | 326.1                   |                                                            | 2857.4                                | 236.8             | -                            | Difficult to keep valve     |
|      | 12  | 00   | 5520                           | 320.2                   |                                                            | 2863.3                                | 230.9             | 20 oz/m.                     | unsilted, therefore causing |
|      | 16  | 00   | 5760                           | 315.7                   |                                                            | 2867.8                                | 226.4             | 15 oz/m.                     | uneven Q rates              |
| 27   | 8   | 00   | 6720                           | 313.0                   |                                                            | 2870.5                                | 223.7             | 15 oz/m.                     |                             |
|      | 14  | 00   | 7080                           | 313.8                   |                                                            | 2869.7                                | 224.5             | 15 oz/m.                     | Water clearer, less silty   |
|      | 19  | 00   | 7280                           | 314.0                   |                                                            | 2869.5                                | 224.7             | 15 oz/m.                     |                             |
| 28   | 8   | 30   | 8190                           | 307.9                   |                                                            | 2875.6                                | 218.6             | 10 oz/m.                     | Temp. = 13°C, Cond. = 1670  |
|      | 14  | 00   | 8520                           | 316.3                   |                                                            | 2867.2                                | 227.0             | 20 oz/m.                     | Water - light grey, br.     |
| 29   | 8   | 30   | 9630                           | 318.7                   |                                                            | 2864.8                                | 229.4             | 15 oz/m.                     |                             |
|      | 19  | 00   | 10260                          | 320.9                   |                                                            | 2862.6                                | 231.6             | 15 oz/m.                     |                             |
| 30   | 8   | 30   | 11070                          | 320.7                   |                                                            | 2862.8                                | 231.4             | 15 oz/m.                     |                             |
|      | 18  | 30   | 11670                          | 325.7                   |                                                            | 2857.8                                | 236.4             | 15 oz/m.                     |                             |
| 1    | 8   | 30   | 12510                          | 329.3                   |                                                            | 2854.2                                | 240.0             | 15 oz/m.                     | Water fairly clear          |

Project No. Y76348B**PUMP TEST DATA SUMMARY**

PROJECT HAT CREEK COAL  
 Location CACHE CREEK, B.C.  
 Pumped Well RH 76-19

Observations in RH 76-19Sheet 5 of 6

DATE: Start SEPT. 22/76  
 Finish OCT. 14/76

| Time |     |     | Elapsed Time<br>"1"<br>(mins.) | Depth to Water<br>(ft.) | Pressure<br>(Pneumatic<br>piezometers<br>only)<br>(p.s.i.) | Elevation of Water<br>(ft.)<br>a.s.l. | Drawdown<br>(ft.) | Pump Rate<br>Q<br>(i.g.p.m.) | Remarks                                              |
|------|-----|-----|--------------------------------|-------------------------|------------------------------------------------------------|---------------------------------------|-------------------|------------------------------|------------------------------------------------------|
| Dy.  | Hr. | Mn. |                                |                         |                                                            |                                       |                   |                              |                                                      |
| 1    | 15  | 45  | 12945                          | 327.7                   |                                                            | 2855.8                                | 238.4             | 10 oz/m.                     | Rained at night                                      |
| 2    | 8   | 30  | 13950                          | 321.7                   |                                                            | 2861.8                                | 232.4             | 7 oz/m.                      | When first meas. = 7 oz/m. Valve shaken-Q inc. to 15 |
| 4    | 10  | 00  | 16920                          | 313.3                   |                                                            | 2870.2                                | 224.0             | 12 oz/m.                     | Rained at night                                      |
| 5    | 13  | 00  | 18540                          | 314.9                   |                                                            | 2868.6                                | 225.6             | 10 oz/m.                     |                                                      |
| 6    | 17  | 30  | 20250                          | 318.8                   |                                                            | 2864.7                                | 229.5             | 11 oz/m.                     | Water fairly clear                                   |
| 8    | 10  | 00  | 22680                          | 324.0                   |                                                            | 2859.5                                | 234.7             | 10 oz/m.                     |                                                      |
| 9    | 10  | 00  | 24120                          | 323.0                   |                                                            | 2860.5                                | 233.7             | 10 oz/m.                     |                                                      |
| 10   | 5   | 00  | 25860                          | 324.0                   |                                                            | 2859.5                                | 234.7             | 10 oz/m.                     |                                                      |
| 11   | 5   | 00  | 27300                          | 322.0                   |                                                            | 2861.5                                | 232.7             | 10 oz/m.                     |                                                      |
| 12   | 4   | 30  | 28710                          | 318.0                   |                                                            | 2865.5                                | 228.7             | 9 oz/m.                      |                                                      |
| 13   | 4   | 00  | 30120                          | 320.0                   |                                                            | 2863.5                                | 230.7             | 10 oz/m.                     |                                                      |
| 14   | 8   | 00  | 31800                          | 237.4                   |                                                            | 2946.1                                | 148.1             | 4 oz/m.                      | Low Q, due to silting                                |
| 14   | 9   | 11  | 31871                          | 246.5                   |                                                            | 2937.0                                | 157.2             | 1 GPM                        | PUMP SHUT OFF                                        |
|      |     |     | t' (min)                       |                         |                                                            |                                       |                   |                              |                                                      |
| 14   | 9   | 11½ | ½                              | -                       |                                                            | -                                     | -                 |                              | RECOVERY                                             |
|      | 19  | 12  | 1                              | 246.4                   |                                                            | 2937.1                                | 157.1             |                              |                                                      |
|      |     | 12½ | 1½                             | 246.3                   |                                                            | 2937.2                                | 157.0             |                              |                                                      |
|      |     | 13  | 2                              | 246.3                   |                                                            | 2937.2                                | 157.0             |                              |                                                      |
|      |     | 13½ | 2½                             | 246.3                   |                                                            | 2937.2                                | 157.0             |                              |                                                      |
|      |     | 14  | 3                              | 246.2                   |                                                            | 2937.3                                | 156.9             |                              |                                                      |
|      |     | 14½ | 3½                             | 246.2                   |                                                            | 2937.3                                | 156.9             |                              |                                                      |
|      |     | 15  | 4                              | 246.2                   |                                                            | 2937.3                                | 156.9             |                              |                                                      |
|      |     | 15½ | 4½                             | 246.2                   |                                                            | 2937.3                                | 156.9             |                              |                                                      |
|      |     | 16  | 5                              | 246.2                   |                                                            | 2937.3                                | 156.9             |                              |                                                      |
|      |     | 17  | 6                              | -                       |                                                            | -                                     | -                 |                              |                                                      |
|      |     | 18  | 7                              | 246.1                   |                                                            | 2937.4                                | 156.8             |                              |                                                      |
|      |     | 19  | 8                              | 246.1                   |                                                            | 2937.4                                | 156.8             |                              |                                                      |
|      |     | 20  | 9                              | 246.1                   |                                                            | 2937.4                                | 156.8             |                              |                                                      |
|      |     | 21  | 10                             | 246.1                   |                                                            | 2937.4                                | 156.8             |                              |                                                      |
|      |     | 23  | 12                             | 246.0                   |                                                            | 2937.5                                | 156.7             |                              |                                                      |
|      |     | 25  | 14                             | 246.0                   |                                                            | 2937.5                                | 156.7             |                              |                                                      |
|      |     | 27  | 16                             | 245.9                   |                                                            | 2937.6                                | 156.6             |                              |                                                      |
|      |     | 29  | 18                             | 245.9                   |                                                            | 2937.6                                | 156.6             |                              |                                                      |



Project No. V76248B

Sheet 6 of 6

DATE: Start SEPT. 22/76  
Finish OCT. 14/76

## Golder Associates

Logged by -     Rao

**Project No. Y2K3402 -**

Sheet 1 of 1

DATE: Start Sept. 22, 1976  
Finish Oct. 14, 1976

☐ Screened well                      ☐ Pneumatic piezo.  
 Type: ☐ Unscreened well                      ☒ Standpipe piezo.  
 Datum elevation ----- 3137.1 FT. ----- a. s. l.  
 Elevation static water level ----- 3085 FT. ----- a. s. l.  
 Elevation of screened interval ----- to ----- a. s. l.

Aquifer Conditions: ☒ confined  
☐ unconfined

Aquifer description Coldwater Fm (Siltstone)

Aquifer thickness 800 feet

Depth to pump suction 370 feet

Type of test: ☒ constant rate  
☐ step drawdown

SON

Project No. Y76348B

Sheet 1 of 1

DATE: Start Sept. 22, 1976  
Finish Oct. 14, 1976

☐ Screened well      ☐ Pneumatic piezo.  
 Type: ☒ Unscreened well      ☐ Standpipe piezo.  
 Datum elevation — 3196.5 FT. ——— a. s. l.  
 Elevation static water level — 3151 FT. ——— a. s. l.  
 Elevation of screened interval — ——— to ——— a. s. l.

Datum elevation 3196.5 FT. \_\_\_\_\_ a. s. l.  
Elevation static water level 3151 FT. \_\_\_\_\_ a. s. l.  
Elevation of screened interval \_\_\_\_\_ to \_\_\_\_\_ a. s. l.

Aquifer Conditions: ☒ confined  
☐ unconfined

Aquifer description Coldwater Fm (Siltstone)

Aquifer thickness 800 feet

Depth to pump suction 370 feet

Type of test: ☒ constant rate  
☐ step drawdown

Type of test: ☒ constant rate  
☐ step drawdown

## Golder Associates

Logged by RAO

## Project No. Y763488-

Sheet 1 of 2

DATE: Start... Sept. 22, 1976  
Finish... Oct. 14, 1976

☐ Screened well                      ☐ Pneumatic piezo.  
 Type: ☐ Unscreened well            ☒ Standpipe piezo.  
 Datum elevation 3270 FT. \_\_\_\_\_ a. s. l.  
 Elevation static water level 3205 FT. \_\_\_\_\_ a. s. l.  
 Elevation of screened interval \_\_\_\_\_ to \_\_\_\_\_ a. s. l.

Aquifer Conditions: ☒ confined  
☐ unconfined

Aquifer description Coldwater Fm (Siltstone)

Aquifer thickness 800 feet

Depth to pump suction 370 feet

Type of test: ☒ constant rate  
☐ step drawdown

## Golder Associates

Logged by RAE

Project No. 1763402

# PUMP TEST DATA SUMMARY

Observations in DDH 76-149-1

Sheet 2 of 2

PROJECT: Hot Creek Coal  
Location: Cache Creek, B.C.  
Pumped Well: RH 76-19

DATE: Start Sept. 22, 1976  
Finish Oct. 14, 1976

## DATA ON OBSERVATION POINT:

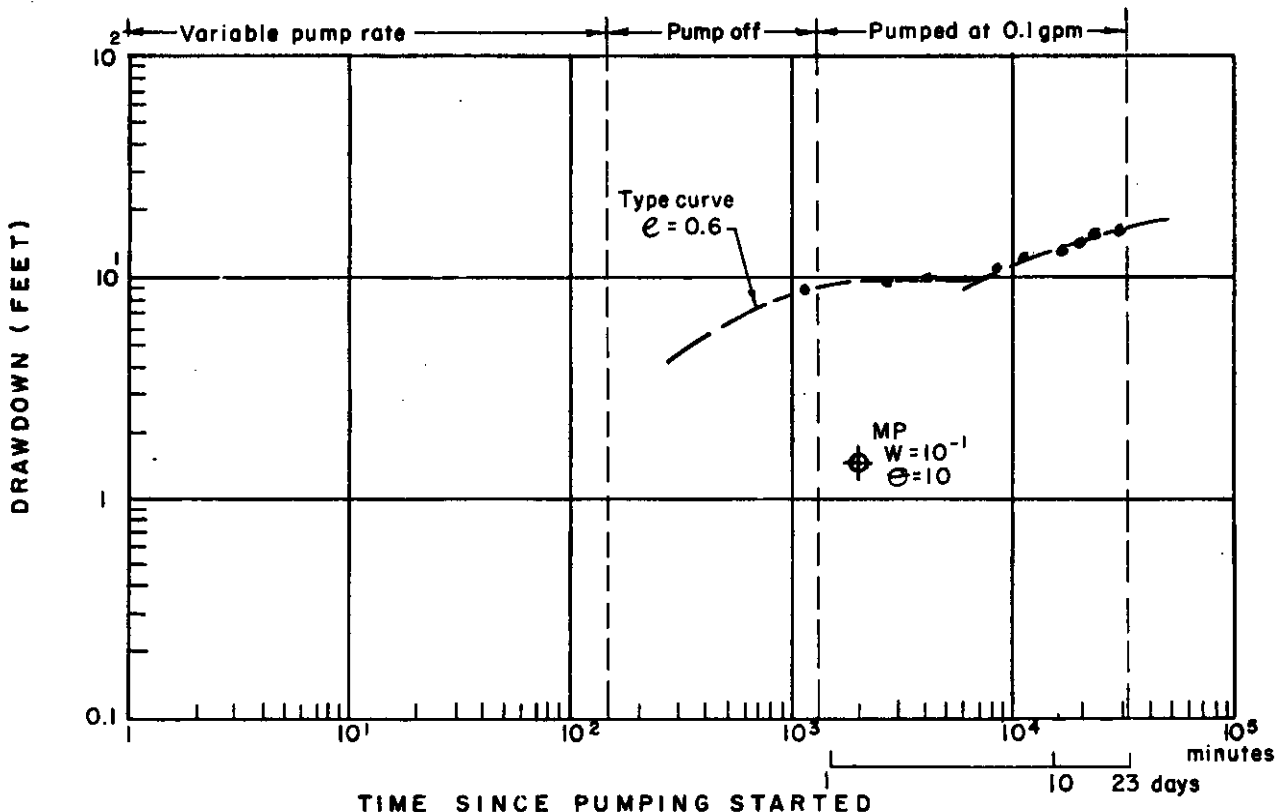
Datum point: Top of tube  
Depth to static water level: 65 ft.  
Screened/open hole interval: 115 to 120

Type: ☐ Screened well ☐ Pneumatic piezo.  
☐ Unscreened well ☒ Standpipe piezo.  
Datum elevation: 3270 ft a. s. l.  
Elevation static water level: 3205 a. s. l.  
Elevation of screened interval: 3155 to 3150 a. s. l.

## DATA ON PUMPED WELL AND AQUIFER:

Well depth: 400 feet  
Well diameter: 8 inches  
Pump type: Electric Submersible  
Final pumping rate: 0.1 gpm

Aquifer Conditions: ☒ confined ☐ unconfined  
Aquifer description: Coldwater Fm (Siltstone)  
Aquifer thickness: 800 feet  
Depth to pump suction: 370 feet  
Type of test: ☒ constant rate ☐ step drawdown



Calculations:  $T = \frac{114.6 QW}{S} = \frac{114.6 \times 0.1 \times 0.1}{2.2} = 0.5 \text{ gpd/ft.}$

$S = \frac{Tt}{2693(r^2)\theta} = \frac{0.5 \times 2.7 \times 10^4}{2693(1080)^2 \times 10} = 4.3 \times 10^{-7}$

Where:

W and  $\theta$  are constant values for a given match point.

$e = \frac{r}{h} \left[ \frac{k_y}{k_h} \right]^{1/2}$

h = thickness of aquifer.

Q = Average pumping rate (gpm)  
S = Drawdown (feet)  
r = Radius from pumped well (feet)  
t = Time (minutes)  
S = Storage coefficient  
T = Transmissivity (gpd/ft.)



## PUMP TEST DATA SUMMARY

PROJECT Hat Creek Coal  
 Location Cache Creek, B.C.  
 Pumped Well RH 76-19

Observations in DDH 76-149-2  
 Sheet 2 of 2

DATE: Start Sept. 22, 1976  
 Finish Oct. 14, 1976

## DATA ON OBSERVATION POINT:

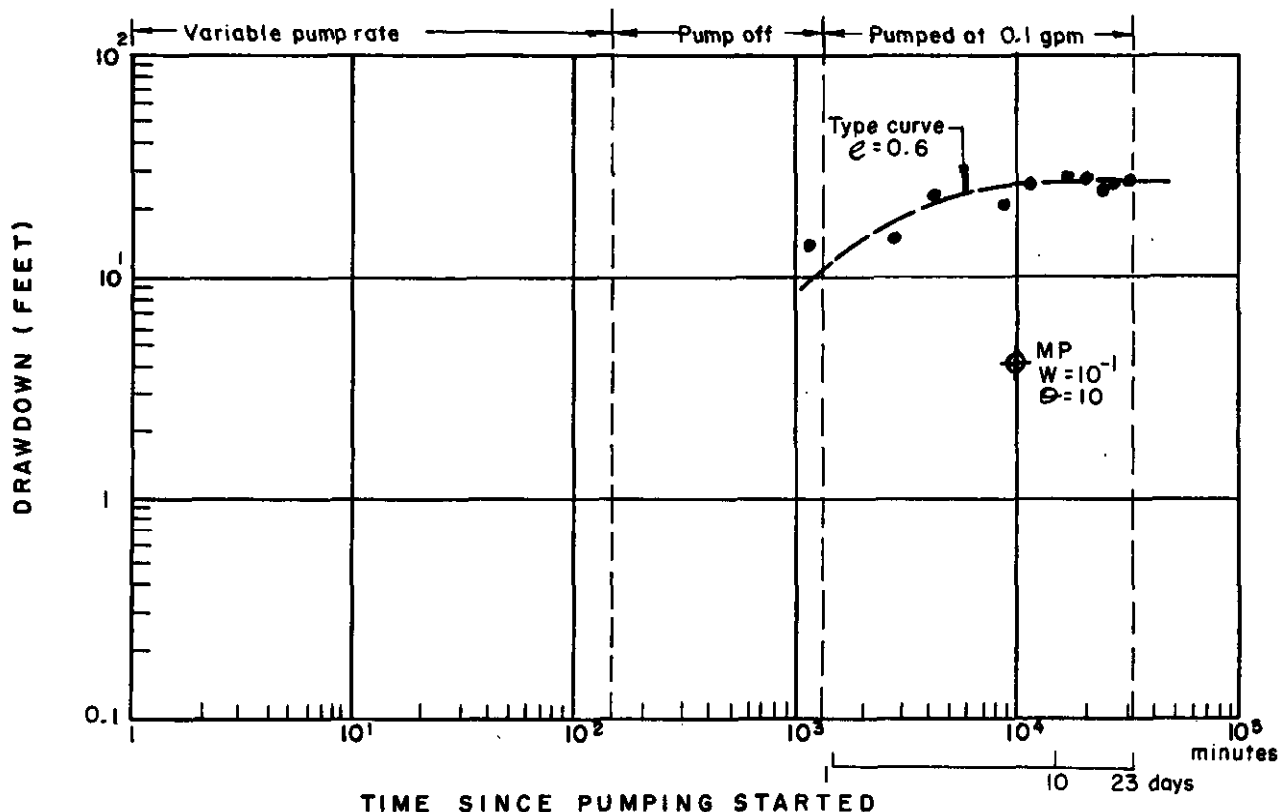
Datum point Top of tube  
 Depth to static water level 70  
 Screened/open hole interval 115 to 120

Type: ☐ Screened well ☒ Pneumatic piezo.  
☐ Unscreened well ☐ Standpipe piezo.  
 Datum elevation 3270 a. s. l.  
 Elevation static water level 3200 a. s. l.  
 Elevation of screened interval 3155 to 3150 a. s. l.

## DATA ON PUMPED WELL AND AQUIFER:

Well depth 400 feet  
 Well diameter 8 inches  
 Pump type Electric Submersible  
 Final pumping rate 0.1 gpm

Aquifer Conditions: ☒ confined ☐ unconfined  
 Aquifer description Coldwater Fm (Siltstone)  
 Aquifer thickness 800 feet  
 Depth to pump suction 370 feet  
 Type of test: ☒ constant rate ☐ step drawdown



Calculations:  $T = \frac{114.6 QW}{S} = \frac{114.6 \times 0.1 \times 0.1}{4} = 0.29 \text{ gpd/ft.}$

$$S = \frac{Tt}{2693(r^2)\theta} = \frac{x}{2693(1080)^2 \times 10} = 9.1 \times 10^{-8}$$

Where:

W and  $\theta$  are constant values for a given match point.

$$e = \frac{r}{h} \left[ \frac{k_y}{k_h} \right]^{1/2}$$

h = thickness of aquifer.

Q = Average pumping rate (gpm)

S = Drawdown (feet)

r = Radius from pumped well (feet)

t = Time (minutes)

S = Storage coefficient

T = Transmissivity (gpd/ft.)