BRITISH COLUMBIA PROSPECTORS ASSISTANCE PROGRAM MINISTRY OF ENERGY AND MINES GEOLOGICAL SURVEY BRANCH

PROGRAM YEAR:1994/95REPORT #:PAP 94-13NAME:ERIK OSTENSOE

GEOCHEMICAL AND GEOPHYSICAL

REPORT

ON THE

RAINBOW 2 AND 3 MINERAL CLAIMS

Tulameen District - Similkameen Mining Division British Columbia 49°34′ → 120°50′

NTS 92H/10W

Field Work Performed: October 16, 1994 to November 16, 1994.

Office Work Performed:

November 17, 1994 to January 15, 1995.

by

T.E. Lisle, P. Eng. and E. A. Ostensoe, P. Geo.

January 15, 1995.

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CONTENTS

page

1. INTRODUCTION	1
2. LOCATION AND ACCESS	2
3. PROPERTY	2
4. CLIMATE, TOPOGRAPHY AND VEGETATION	2
5. HISTORY	5
6. 1994 WORK PROGRAM	5
7. REGIONAL SETTING	6
8. GEOLOGY OF THE RAINBOW CLAIMS	8
9. MAGNETIC SURVEY	9
10. VLF-EM SURVEY	10
11. GEOCHEMISTRY	11
12. CONCLUSIONS	13
13. RECOMMENDATIONS	13
14. REFERENCES	14
 15. PERSONNEL (a) T. E. Lisle, P. Eng. (b) E. A. Ostensoe, P. Geo. 	15
16. STATEMENT OF EXPENDITURES	16
17. APPENDICES	17

ILLUSTRATIONS

	page
FIGURE 1. Location Map - Rainbow Claims	3
FIGURE 2. Claim Map	4
FIGURE 3. Regional Geology	7
FIGURE 4 (a) Ground Magnetometer Survey - Profile Map (b) - Contour Map	in pocket "
FIGURE 5. VLF-EM Survey - Fraser Filtered Tilt Angle Data	н
FIGURE 6. Geochemical Survey	**

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TABLES

TABLE 1.	Rainbow Claims	2
TABLE 2.	Work - Proposed and Completed	6

1. INTRODUCTION

The authors submitted, in May, 1994, a proposal to the Prospectors Assistance Program, British Columbia Ministry of Energy, Mines and Petroleum Resources, for partial funding of a limited exploration program of the Rainbow claims, Tulameen district, Similkameen Mining Division, B.C.

The proposal included preparation of 23.3 kilometres of grid lines, 32 line kilometres of geological, magnetic and electromagnetic surveys, and the collection and analysis of 640 soil samples and 100 rock samples. The estimated cost of the combined program was \$27,679.20. The authors wish to acknowledge with thanks the assistance of grants received that funded a significant part of the cost of their work.

The authors, in the period October 16, 1994 to November 16, 1994, completed a large part of the proposed program of work. Unusually early and heavy snowfalls in the project area, combined with time and budget constraints, frustrated geological mapping and caused elimination of parts of the electromagnetic survey.

This report describes exploration work completed with the help of the 1994 Prospectors Assistance Program funding. All technical observations are presented and are discussed in the report Several maps have been prepared and various appendices contain the basic data. Some interpretation has been attempted and suggestions for additional work are included.

2. LOCATION AND ACCESS

The Rainbow claims lie on the north slope of the Tulameen River valley six to ten kilometres west and northwest of the village of Tulameen in southcentral British Columbia (Figures 1 and 2). Geographic coordinates are 49° 43' north and 120°50' west and NTS sheet is 92H/10W.

Elevations are between 840 metres asl at Tulameen River and 1646 metres asl in the central part of Rainbow 3 claim. Terrain is relatively subdued but near Lawless Creek and its tributary streams, slopes are steep.

Access to the claims is by the Lawless Creek Forest Service road that passes from the Coquihalla Highway easterly toTulameen and by the Princeton to Tulameen paved road. A logging road along the north side of Tulameen River west of the town gives access to the south part of the Rainbow 4 claim. Roads have gravelled, all weather surfaces and are maintained throughout much of the year. The common claim line of the Rainbow 2 and Rainbow 3 claims crosses the Lawless Creek Forest Road about 8.1 km northwest of Tulameen.

3. PROPERTY

The Rainbow property comprises three claims with a total of 46 units (Table 1). They are located within the Similkameen Mining Division and are owned jointly by T. Lisle and E. Ostensoe (Figure 2).

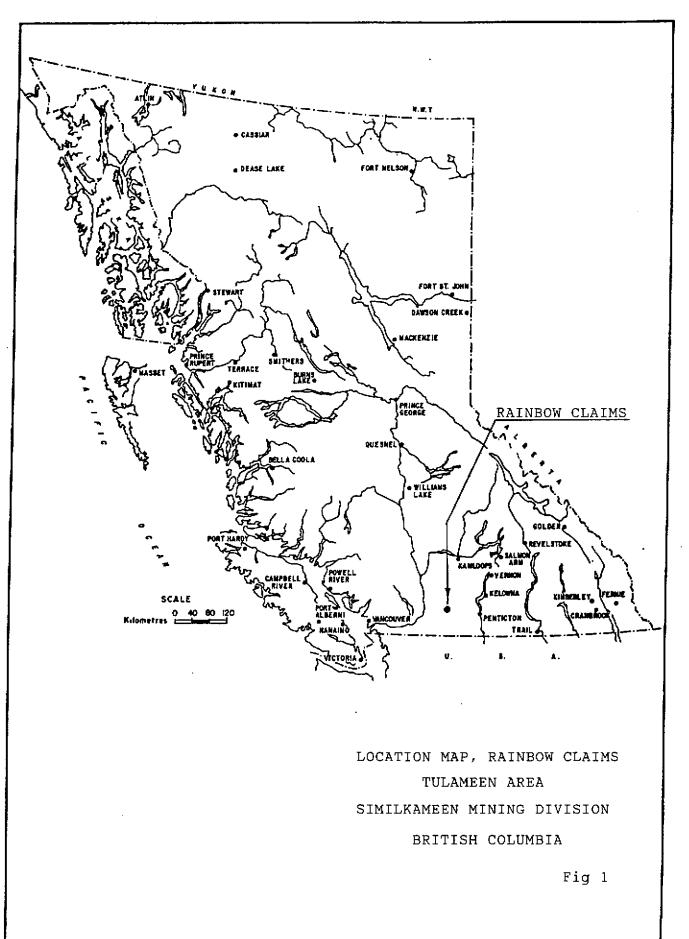
Claim Name	Units	Record No. Located Expi		
Rainbow 2	20	309158	May 6, 1992	May 6, 1995
Rainbow 3	16	309159	May 7, 1992	May 7, 1995
Rainbow 4	10	323956	March 1, 1994	March 1, 1995

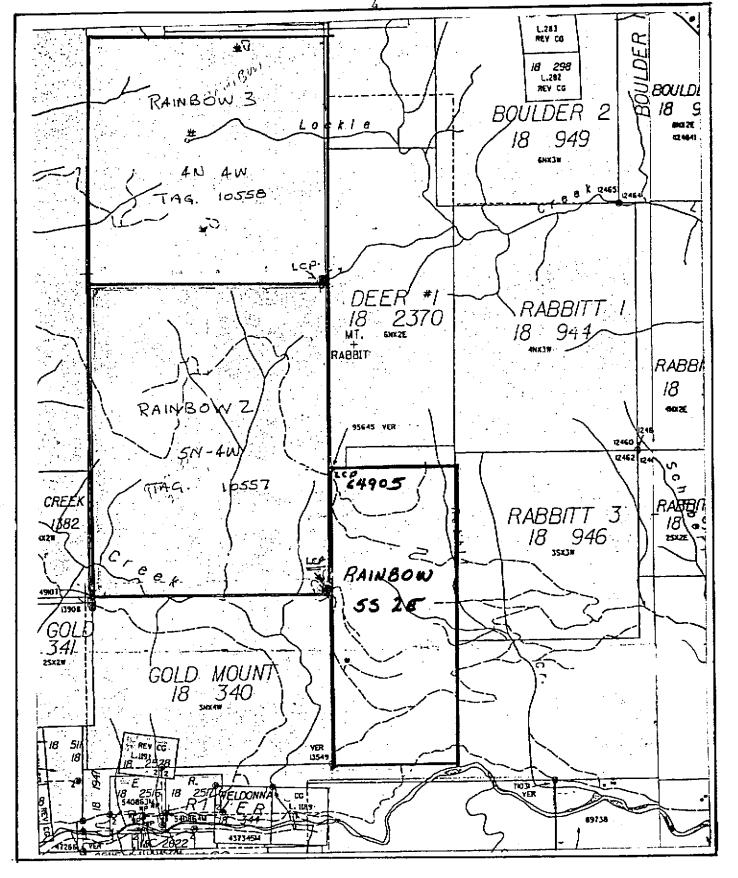
Table 1. Rainbow Claims.

4. CLIMATE, TOPOGRAPHY AND VEGETATION

The climate in the Rainbow claims area is transitional between dry conditions of the southern Interior Plateau and wetter conditions of the Cascade Mountains. Summers are hot and dry and winters are cold with substantial snowfalls. More than one metre of snow fell in the project area in the period October 16 through November 16, 1994.

The Rainbow claims span elevations from the Tulameen River, about 900 metres asl, and the top of Boulder Mountain, about 1675 metres asl. North of the Lawless Creek forest road, the terrain is forested and topography is mostly gentle; the lower portion, south of that road, is steep and





RAINBOW PROJECT, CLAIM MAP. BRITISH COLUMBIA CLAIM MAP 92 H 056

Figure 2.

characterized by bluffs and canyons. Several small streams originate on Boulder Mountain and flow either southerly to Lawless Creek or easterly to Boulder Creek.

The upper parts of the area are forested with thick stands of spruce, fir, and balsam, and a few red cedar trees. Large yellow pine trees are present but not numerous on south facing parts of upper slopes. Large parts of the area north of the Lawless Creek forest road have been logged in recent years.

5. HISTORY

The mining history of the Tulameen area is documented in numerous government publications and in more than 120 technical reports that have been filed as assessment work on mineral prospects in a 300 square kilometre area approximately centred on Tulameen.

The first comprehensive geological map of the Tulameen area was included in GSC Memoir 26, authored by Charles Camsell and issued in 1913. Camsell showed a small granitic stock intrusive into Nicola Group and dioritic rocks at Boulder Mountain.

Early prospectors were undoubtedly attracted to the Tulameen area by placer mining possibilities, particularly by discoveries of platinum in nearby streams and by production of large nuggets from Lawless and Boulder Creeks. A large gossaned alteration zone, now exposed by sidecuts along the Lawless Creek forest road, occurs along a substantial creek valley that passes through Rainbow 2 claim. Several small bedrock pits located north of the road were excavated many decades ago and expose local concentrations of pyrite and magnetite within the zone.

Geological and geochemical assessment work reports numbered 16016 and 17271 apply to parts of the Rainbow claims. A preliminary prospecting report by Lisle and Ostensoe in 1993 presents some information concerning the geology of the claims. Important background information may be obtained from these and other sources.

6. 1994 WORK PROGRAM

The following work was completed on the Rainbow claim between October 16 and November 16, 1994:

	Rain	bow 2	Rain	bow 3		
	Proposed	Completed	Proposed	Completed		
Linecutting (100 m lines - 25 m spacing)	11.3 km	11.3 km	12.0 km	11.0 km		

Soil Geochemistry 340 359 * - 412 of 608 soil samples have been ana		359* n analysed.	300`	249*
Rock Geochemistry	50	6	50	0
Magnetic Survey	17.0 km	17.0 km	15.0 km	10.0 km
VLF-EM Survey	17.0 km	10.0 km	15.0 km	7.0 km
Geological Survey	17.0 km	0	15.0 km	0

Table 2. Work - Proposed and Completed

7. REGIONAL SETTING

The Nicola Group in southern British Columbia is part of a linear northwesterly Cordilleran belt of volcanic and sedimentary rocks developed in an Upper Triassic island arc environment. The Groups is, at least in the Princeton-Merritt area, a westward younging assemblage comprising

a) an eastern belt of alkalic and calc-alkalic submarine volcanic rocks, lahar deposits, basaltic flows, and high-level syenitic stocks,

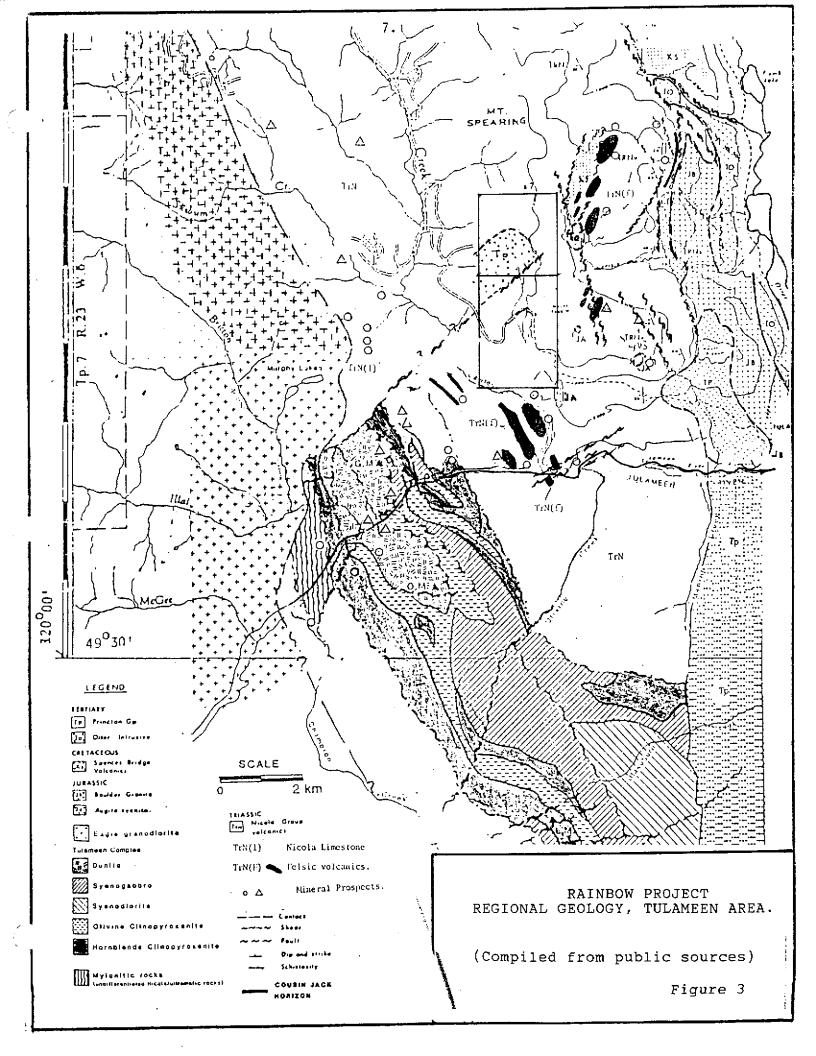
b) a central belt of alkalic and calc-alkalic subaerial and submarine assemblages of andesite, basalt and co-magmatic intrusions of diorite and syenite, and breccia, conglomerate and lahar deposits,

c) a western belt of calc-alkalic flow and pyroclastic rocks ranging in composition from andesite to rhyolite, with minor interbedded limestone, volcanic conglomerate, sandstone and argillite. This assemblage underlies much of the Tulameen area.

The Nicola Group rocks, west of Tulameen, are bounded on the west by the Eagle Granodiorite, a syntectonic intrusion of apparent Upper Jurassic age. The contact area is marked by an amphibolitic zone. Both the Nicola and Eagle rocks dip westerly along a regionally developed northwest foliation. Figure 3 illustrates some features of the regional geology near the Lawless Creek area.

Several small intrusions are present in the Tulameen area, including Late Traissic to Early Jurassic granites and the Tulameen ultramatic complex of apparent Late Triassic age (Nixon, 1988). Tertiary-age granite stocks, particularly the Otter Granite, are important relatively young plutons.

All of the older rock units are disrupted by northeast faults of mid-Tertiary age that mark significant right-lateral and vertical displacement. One such fault is believed to form the northern



boundary of the Tulameen ultramafic complex at Grasshopper Mountain a few kilometres southwest of the Rainbow claims and to trend northeasterly through the Rainbow. Regional evidence suggests that rocks on the north side of the fault are offset four kilometres northeasterly.

Nicola Group volcanic rocks and related intrusions are hosts to world-class copper-gold porphyry deposits at Kamloops and Princeton, and copper-molybdenum porphyry deposits at Highland Valley, north of Merritt, and elsewhere in the Cordillera. The western belt of the Nicola Group embraces many mineral prospects in addition to the large Craigmont copper-iron deposit.

8. GEOLOGY OF THE RAINBOW CLAIMS

The geology of the Tulameen area was described by C. Camsell in 1913 in GSC Memoir 26. He identified, within the current Rainbow 3 claim, a stock of Otter Granite intrusive into Nicola Group rocks, and to the south, a smaller augite syncite pluton.

The Otter Granite stock is of Early Tertiary age and is commonly medium grained and pink coloured. Composition varies from granite to, in a border phase, quartz diorite. Prospecting by the writers during 1992 (assessment report, 1993) revealed that it may have dimensions about 1.5 by 2.0 kilometres, that it is elongate northwesterly, and it is possibly truncated on its south side by a northeast fault. Enclosing rocks have been to variable degrees altered by siliceous potassic feldspar metasomatism.

Camsell noted the presence of a small elongated intrusion of augite syenite south of the Otter Granite. Rice (GSC Memoir 243, 1947) determined that this intrusion is of Late Triassic to Early Jurassic age, and that it includes some peridotite, pyroxenite and gabbroic phases. Details of the dimensions and composition of this body on the Rainbow claims have not been determined. It is known however to be dark grey-green, fine to medium grained, and dioritic and has been observed to be magnetically distinct from neighboring rock types.

East of the Otter Granite-type stock, a formation previously described as a breccia forms a persistent belt that trends north-northwesterly through much of the eastern part of the Rainbow survey grid. This unit is tuffaceous, locally cherty, and includes sections that contain beige to pink coloured fine-grained clasts up to 40 cms in diameter, as well as subordinate amounts of small mafic clasts. At 27+00N, 5+00W, it is well-bedded, strikes northwest and dips $-72^{(-)}$ west. The writers believe that this breccia is similar to, possibly part of, a formation known to be present near sulphide mineral occurrences elsewhere on Boulder Mountain. Copper mineralization was noted near the east boundary of Rainbow 2 claim.

Prospecting by the writers during 1992 investigated a large pale coloured alteration zone situated between the Otter Granite-type complex on the west and the above-described breccia on the east. The zone is siliceous, weakly porphyritic, and exhibits strongly developed argillic (clay-sericite-pyrite) alteration. It is well exposed along the Lawless Creek Forest road at 19+50N, 3+50 to 5+50 W and in a logging slash at 25+00N, 5+00 to 6+00W. The presence of finely disseminated

sulphide grains, localized concentrations of coarse grained sulphides, and the weakly to vaguely expressed porphyritic textures are similar to, and suggest an affinity to, a series of mineralized porphyry dykes that is exposed elsewhere in the Princeton-Tulameen district. Old prospector's workings found at 20+00N, 3+50W and 22+00N, 5+00W explored limonitic, very highly altered zones with 10% pyrite and up to 5% magnetite. These workings occur within a distinct magnetic trend that is described in the following section of this report.

Parts of the Rainbow claims are underlain by andesitic to dacitic flows and fragmental rocks of the Nicola Group. A distinctive coarsely porphyritic andesite rock type also occurs in other parts of the Boulder Mountain-Rabbitt Mountain area.

A satisfactory more comprehensive discussion of the petrology, structure, alteration and mineralization of the Rainbow property cannot yet be presented. Detailed geological mapping was planned as part of the 1994 work program but was precluded by onset of winter conditions.

9. MAGNETIC SURVEY

A magnetic survey was conducted over the Rainbow claim grid in the fall of 1994 using two GSM-19 (19-T) high sensitivity proton magnetometer/gradiometers equipped with inbuilt microprocessors and memory. The field instrument was synchronized with a similar unit that was set up in Tulameen as a base station.

The magnetometers were initially tuned to a total magnetic field intensity of 58,000 nT, appropriate for the survey area. Observations were taken at 12.5 metre intervals on all 100 metre spaced grid lines with the exception of lines 35+00N and 36+00N. Steve Lowe, geophysical technician, data processor and auto-cad operator, was given the Rainbow grid data and executed corrections and procedures to produce computer generated plan and profile presentations (Figures 4(a) and (b).

Technical data and specifications of the GSM-19 and 19T magnetometer systems are included in Appendix 2(a) of this report.

The results of the magnetic survey are summarized as follows:

1) Magnetic relief in the survey areas low and commonly within a range of 300 nT near 58,000 nT

- 2) Magnetic values tend to be slightly higher in the north and east parts of the grid relative to values observed elsewhere
- 3) The southwest corner of the grid, in particular lines 8+00N through 14+00N from about 5+00W to 10+00W, exhibits high magnetic relief (up to about 1100 nT) and is magnetically distinct from the balance of the grid
- 4) A series of narrow magnetic "highs", up to about 500 nT, form a conspicuous, but locally broken, north-northwesterly linear trend from the southeast to northwest corners of the grid.

This linear trend is locally flanked at distance about 200 metres to the east by a series of magnetic highs that are either isolated or are part of a weaker north-northeasterly linear trend.5) An overall northerly to northwesterly magnetic grain to the grid is emphasized by a small number of line to line responses of small amplitude, both positive and negative.

Preliminary interpretation of the magnetic data relative to 1992 prospecting and mapping, indicates that the magnetic response noted in 3) above is a reflection of the underlying dioritic unit. The cause of the north northwest linear magnetic texture is more obscure. That part of the grid between 20+00N and 24+00N may reflect pyrite-magnetite accumulations between the large felsic alteration zone to the west and the bedded clastic unit to the east A secondary linear magnetic feature between lines 28+00N and 34+00N is at least in part coincident with an eastern section of the Otter Granite member.

10. VLF-EM SURVEY

A very low frequency electromagnetic survey was conducted over about two-thirds of the Rainbow property grid using a Sabre model 27 VLF-EM receiver.

The VLF-EM technique measures the field-strength of signals that are generated by distant very powerful radio transmitters. Variations in dip angle and field strength are recorded in the field, processed using the Fraser Filter method, plotted, and then interpreted in terms of conductivity contrasts. Conductive areas can be identified and related to geological features including structures and, possibly, mineralization. Results can be confused by conductive clay layers and by terrain effects. Faults and shear zones may produce anomalous data but only if conductivity is associated with them.

The Sabre model 27 VLF-EM instrument is a sensitive precise radio signal receiver. For purposes of the Rainbow grid survey the 18.6 Khz signal generated by a station near Seattle, Washington, was employed. The ideal station should be located so that the direction of the signal is approximately perpendicular to the direction of the grid lines. The Cutler, Maine and Annapolis, Maryland stations would also have been appropriate signal sources.

Two measurements were recorded in the field:

- 1) tilt angle of the resultant field, measured in degrees of tilt
- 2) field strength of the horizontal component of the VLF field

Tilt angle measurements were "Fraser Filtered", a process that enables data to be presented on a plan map and contoured. Instrument specifications and detailed field procedures are described in Appendix 2(b) of this report.

Figure 5 displays Fraser filtered tilt angle observations. Data have been extended between grid lines where appropriate and have been contoured where sufficient information is available. No overall electromagnetic pattern has been recognized but several trends have been identified. Better interpretation of data will be possible when the remaining grid lines have been surveyed.

11. GEOCHEMISTRY

Bedrock exposure in the Rainbow claims area varies greatly but, in general, outcrop distribution suggests that parts of the property have only shallow overburden cover, in the order of a metre or less. The east part of Rainbow 3 claim has few outcrops and along parts of the Lawless Creek Forest road some till deposits are obviously several metres deep.

Juvenile podzolic soils that prevail in most of the Rainbow area are developed on tills and colluvium deposits. Southwest of the Rainbow property, eutric bronisols are dominant in a plateau-like area and on gentle westerly slopes but both eutric bronisols and humo-ferric podsols are present on steep southerly slopes (Cook, Fletcher, 1994).

Soil samples were taken from the Rainbow claim grid as a means of investigating the distribution of metal values in the underlying bedrock. The samplers recorded the soil characteristics at the time of sample collection (Appendix 1). Where topography is subdued, soil horizons are well developed in the till and the depth of overlying 'A' horizon soils varies from about 10 cm to in excess of one metre. 'B' horizon soils are generally less than 40 cms deep, are reddish brown coloured, and include 10 to 20% gravel-sized fragments and a few cobble-sized clasts. 'B' soils may rest directly on bedrock but more commonly overlie 'C' soils that are pale to yellow-brown with highly variable amounts of clay, silt, sand and clast content. Soil horizon development is rudimentary on steeper terrain where active colluvium or till and colluvium deposits prevail.

The intent of the soil sampling program was to sample the lower 'C' horizon. The practical limit of our sampling tools and methods was about 1 metre and if the 'C' was not encountered then the deepest available soil was sampled. Samples were taken from pits (average depth about 0.5 m) that were dug at 50 metre intervals along the grid lines. Soils were placed in standard kraft soil envelopes. Details of colour, depth, horizon were recorded, along with estimates of clay, silt, sand and fragment contents on sample sheets that comprise Appendix 1(a).

All soil samples were air dried and then transported to Vancouver, B. C. Four hundred and twelve soil samples, up to the time of this report, were submitted to Acme Analytical Laboratories Ltd. for drying and screening, followed by geochemical analysis for gold by acid leach and atomic absorption methods and for 30 other elements by induced coupled plasma determination. Five rock samples, collected from old prospecting workings on lines 20+00N and 22+00N, were analyzed for the same elements plus platinum and palladium. One rock sample was analysed by whole rock ICP methods. Analytical data is contained in Appendix 1(b) of this report. One

hundred and ninety-eight soil samples have been placed in temporary storage and will be analysed when funds are available for that purpose.

The results of the analyses for five of the elements of particular interest to us, gold, silver, copper, lead and zinc, are summarized herewith:

Element	No. of Samples	Range of Contents	Remarks
Gold	412	≤ 1 to 290 ppb	44 samples ≥ 10 ppb
Silver	412	≤0.1 <i>to</i> 0.70 <i>ppm</i>	17 samples≥ 0.30 ppm
Copper	412	≤1 <i>to</i> 466 <i>ppm</i>	15 samples \geq 100 ppm
Lead	412	≤ 2 <i>to</i> 270 <i>ppm</i>	5 samples≥ 20 <i>ppm</i>
Zinc	412	6 to 517 ppm	8 samples≥ 200 <i>ppm</i>

Contouring, due to wide line spacing and gaps in analytical information, is not practical. The data does not permit much line to line correlation of possibly anomalous metal values but does indicate that some areas of the grid are anomalous.

The strongest clustering of anomalous gold-copper-zinc values occurs in the southeast section of the grid from about 10+00N to 20+00N. The higher responses are located near north to northwest trending magnetic features. The grid section 24+00N, 4+00W to 34+00N, 0+00W contains several soils anomalous in copper and gold and increasingly to the northeast, zinc. Anomalous copper and zinc analyses appear to be related to eastern parts of the grid that are thought to be underlain by a clastic sedimentary unit.

Anomalous gold analyses are to some extent clustered along the western side of the Rainbow grid, an area that is underlain by Otter Granite in the north, a mafic diorite complex in the south, and by Nicola volcanic rocks in the central portion. Some possible zones appear to trend westerly off the grid.

A few, generally isolated, anomalous gold analyses occur within or near the large alteration zone that occupies central parts of the grid. The more easterly section of this zone is partly marked by strong magnetic patterns and old trenches expose significant pyrite-magnetite mineralization. Five rock samples from the alteration zone did not generate analyses of interest but the wide scattering of anomalous gold in soil values suggest that further examination is warranted.

12. CONCLUSIONS

The writers have completed programs of geophysical surveys and geochemical soil sampling on the Rainbow 2 and 3 mineral claims. Data have been plotted and evaluated. Approximately 198 soil samples remain to be analysed. Geological mapping and additional geophysical work are required in order to provide complete coverage of the existing grid. Approximately one half of the property remains to be explored by prospecting and surveys.

The Rainbow claims are located in an area of Nicola Group volcanic and sedimentary rocks that have been intruded by granitic rocks of Jurassic age and by dioritic rocks of Early Tertiary age. One major zone of intense argillic alteration is exposed on Rainbow 3 claim. Geochemically anomalous metal values are present in some areas of magnetic and electromagnetic activity.

It is concluded that the Rainbow claims exhibit geological characteristics favourable for the location of worthwhile deposits of massive sulphide and precious metals.

13. RECOMMENDATIONS

- 1) Analyse remaining soil samples and complete in-fill soil sampling at 25 metre spacing in areas of continuing interest
- 2) Map geologically all of the existing grid
- 3) Extend grid to northwest to provide coverage in the area of the apparent geophysical/ geochemical trend along the Otter Granite contact. Complete soil sampling, geological mapping, and magnetic and VLF-EM surveys of the grid extension
- 4) Extend grid to southeast onto Rainbow 4 claim to cover anticipated geophysical/geochemical trend in that direction
- 5) Methodically prospect remaining areas of the Rainbow claims
- 6) Compile and correlate Rainbow project data with detailed exploration data from claims that adjoin to the east and compile available data, geology, magnetics, electromagnetics and geochemistry, at suitable scale onto a single map.
- 7) Investigate other possible contouring configurations of VLF-EM data



14. REFERENCES

1) Lord, T. and Green, A.	Soils and Surficial Geology of the Tulameen Area, Agriculture Canada, 1974
2) Cook, S.J. and Fletcher, W. K.	Platinum Distribution in Soil Profiles of the Tulameen Ultramafic Complex, Souther British Columbia, Journ. Geochem. Expl., July, 1994
3) Camsell, C.	Geology and Mineral Deposits of the Tulameen District, British Columbia, Geol. Surv. Canada Memoir 26, 1913
4) Monger, J.W.H.	Geology of the Hope and Ashcroft Map Areas, British Columbia, Maps 41-1989, 42-1989, Geol. Surv. Canada
5) Preto, V. A.	Geology of the Nicola Group between Merritt and Princeton, Bulletin 69, B.C. Ministry of Energy, Mines and Petr. Resources, 1979
6) Rice, H.M.A.	Geology and Mineral Deposits of the Princeton Map Area, Geol. Surv. Canada, Memoir 243, 1947
7) Nixon, G. T.	Geology of the Tulameen Ultramafic Complex, Open File 1988-25, BC Ministry of Energy, Mines and Petr. Resourses, 1988
7) Lisle, T. E. and Ostensoe, E.	Prospecting Report on the Rainbow 2 and 3 Mineral Claims, Tulameen Area, Similkameen Mining Division, B. C., January 15, 1993.

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15. PERSONNEL

The following persons carried out the field work and prepared the accompanying report:

1) T. E. LISLE, P. Eng. - geologist, (UBC, 1964)

- more than thirty years experience in mineral exploration, principally in western and northern North America
- member of APEGBC, Geol. Assoc. Canada, CIMM
- performed field work as described in this report in the period October 16 through November 16, 1994

2) E. A. OSTENSOE, P. Geo. - geologist, (UBC, 1960)

- more than thirty years experience in mineral exploration, principally in western North America
- member of APEGBC
- performed field work as described in this report in the period October 16 through November 16, 1994.

17. APPENDICES

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APPENDIX 1. (a) GEOCHEMICAL DATA SHEETS (b) Certificates of Analysis

APPENDIX 2. GEOPHYSICAL INSTRUMENTS

- (a) Instruction Manual GSM-19T Magnetometer
- (b) Specifications and Instructions Sabre Model 27 VLF-EM Receiver

APPENDIX 1

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GEOCHEMICAL DATA

Abbreviations used on data sheets.

Type of survey	:	S = soil; SS = Silt; R = Rock
Depth	:	Recorded in meters.
Material	:	T = Till; Co = Colluvium; A = Alluvial; GF = Glaciofluvial. F = Fluvial; O = Organic
% Organic	:	L = Low; M = Moderate; H = High
Colour	:	<pre>Br. = Brown; (L = Light; P = Pale; Y = Yellow; R = Red; G = Grey, Dk = Dark) Bl= Black. G = Grey. O = Orange</pre>
% Gravel	:	Estimated % of gravel sized fragments.* Till commonly contains up to 10% cobble-sized fragments.
Horizon.	:	 A. Commonly black organic-rich surface material. B. Commonly Brown to red-brown. C. Commonly pale to yellow brown occurring at a depth of 0.5 meters or deeper.
Clay	:	L = Low; M = Moderate; H = High.
Clay Silt		L = Low; M = Moderate; H = High. L = Low; M = Moderate; H = High.

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4	7.+00, 8+00		•30	TLP,	Be 15-20	C MTH	m m	Steep Scope
5	7,7,50 8,4,0,0		- 50	TLP	<u>Be</u> 20	C M	M	
6 <u>, i , i , i , i</u> ,	8,700 8+00] < G\$7.	.20	GI!L	R + 30	C? 4	M MHH	
7	8+50,8+0,0	G GST	· 2 5	۲. L E	3R +35	Ç ? 4	MH	Laure Tree of the State of the
B 5	9+00, 8+0,0	5 GS7 + Die	·25	CIIL B	R 30	C K		Bonne in the test of a traffer Alogfer
9	Q1750 B+00		.15	TLE	ba ~ 15	G H	MM	
	1,0,+,0,0 , 8,+,90	, s <u>r</u>	.50	7 L Y	Ba 15-20	C M-H		New BALL warden in SAL GLAYS
		······································						

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PROJECT K	AINBOW		L9N	PLOTTED	ALR PHOTO		
-	LOVEMBER 4, 1				MAP		
LOCALITY LA	WLESS CR., Tur	AMEEN, B.C.		SAMPLER	ERIK	OSTENSO	ε
	ALLON $-(GRU)$ SI	YPE DR MRY ADRK PT.S	material Depth : organ	colour 1. ;% G	ravel Horizon	n Clay Silt San	a. REMARKS
	ZAST NORTH	22 23124 25 26	5127.28 27 30 • 6 -	31,32 <u>33</u>	1.35 36.37 //	30139 40 4	
2	0+1510		,2,5 [Er [56		
3	1.+.ad		.4,0		50	H.	
	1+50		·50 [] []		÷ <	H	- Charlowsky Kyme - Liensger Gage - m
5	2,+,0,0		·4.0		10 [M M C	- Probably award B+C Large Broght - Court
٥ (()	2+50		· <u>50</u>		<u>2</u> C] d lay +."
	3,+,0,0		•70	Vet 0	55	HMW] Softer till
	3,+,50		4.0	Vet []	S C	MM	Hard till Hard till
	A,+,00		50 []		04	FI M	Till Have, Tray
	4+50		50 🗌	Br	2 B <u>/</u>	MM	1 Sort. Logged ion ago
		· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·				

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		_		19	N			
	PROJECT	RAINBOW			PLOTTI	D AIR PHOT	<u></u>	
	DATE	,	1994.			MA		
	LOCALITY	LAWLESS CR., To	LAMEEN, B.C.		SAMPL	ER Erik	Ostensor	
	SAMPLE	LOCATION GRID	TYPE DR SURV BDRK PT.S	o Depth materia	rganic 1 colcar	% Gravel Hori	zon Clay Silt Sand	R EM A RK S
۱	<u>1,2,3,4</u> <u>5,6,7,8</u>	$\begin{array}{c c c c c c c c c c c c c c c c c c c $		26127128 29 •50	30 31,32 33 DK Vor	34.35 36.37 3 B/C	38139 40 41 H M M	Soil not till. Rocky. Flat ground.
<u>.</u>		, 5,+,5,0 , , , , , , ,		160		2 1/2	HMM	Aboue till. Also took à Record spliform B horizon at depti 40cm
3		16,+00		:40		56	HML	Flatter terrain than the W.
4		6+50		·30	l Gr			Clay till V.haro. Slope 25' 1.
5		17,+00		50				As below.
6		7.+50		·50	br [H M L	Modified till.
7		8,+,0,0		•40	Red hv] [] []	M M L	Wear top of STeepest terraid. Good visterial
8		8,+50		· 1 4.5	Lt lar] रिइ ि		Tree moto car 21 Por Mill 2009, AT Bar Mill 2009, AT Bar Ast Cr. at 8+60W
9		9+00		:35	Land Land] <u>7</u> 5 B e		light soil is call in
10		9.+50 10+00		30	Lt br] [3] [B] 5. C	H M M	
					<i>p D</i> ,			_ Near top of Slope. Side hill drove off Stamply to East

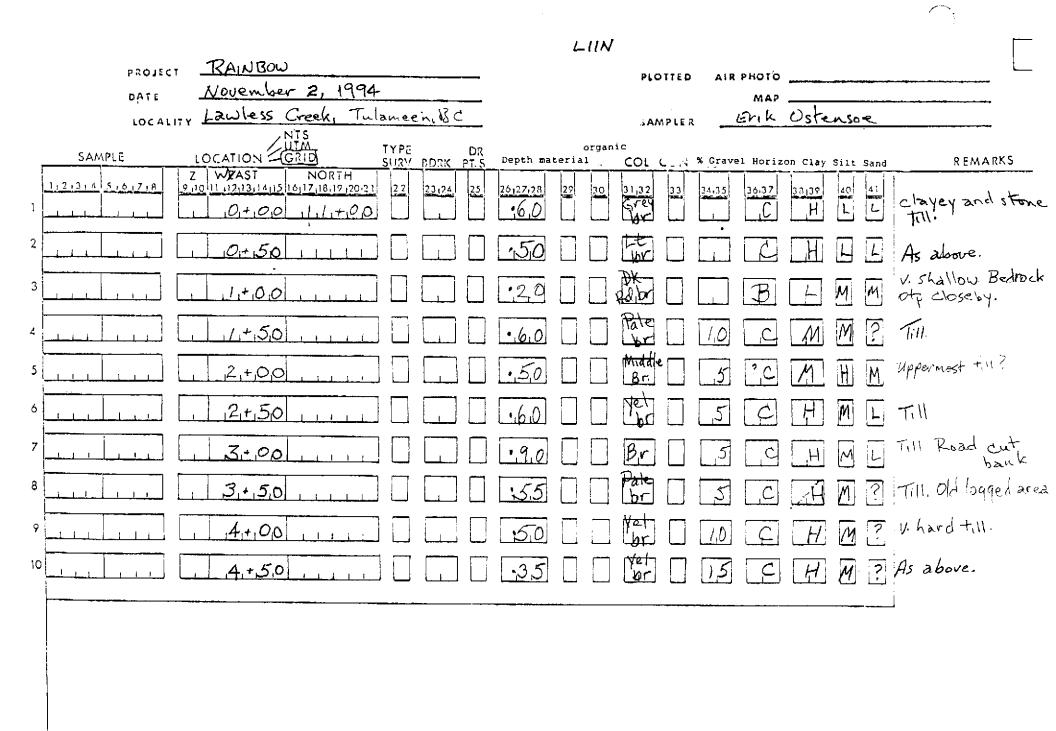
 $i \in \mathbb{N}$

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	PROJECT	RAINBOL						F	LOTTED	A 1 P 3	отон					
	DATE	Novemb	er 3,199	4				•			MAP					
	LOCALIT	, LAWLESS C	REEK, Tu	-AMET	EN, BC			\$	AMPLER						TE	LISLE
	SAMPLE			TYPE	 D3	. Depth ma		anic colo				n Clay S				
	1,2,3,4 5,6,7,A	Z WEAST I	NORTH			1				iavel	HOFIZO	n Clay :	Silt Sa	and.		REMARKS
1		<u>10,11,12,13,14,15</u>	$\frac{1}{100} + \frac{1}{100} = \frac{1}{100} + \frac{1}{100} = \frac{1}$	22 2 5	23124 25	• 45		10 31,3 BrP		4,35 5-20	36,37 C	38139 M	40 ₩	4 	1 24	top man have
2		10+50	1/19+100	5		125	7	L PB	d []≠[5	c	Н	L	L-14	ة رمينو، م	•••
3		,1,+,0,0	1/10++1010	<u>s</u> [-35	7	PB		15	C	M	M	3		
4		1+50	LIQAOO	5		.60	7	PB		20	C	4	Μ	н		.•.
5		,2,+,0,0	110400	5		•40	7	B		5	ß	μ	Μ	Ŀ	1	• .
6		2+50	1/10/100	<u></u>		$\cdot 7 \rho$?	PB		5-20	C?	<u>L</u>		H		
7		,3,+,0,0	1/10+100	5		.70	7	L PB		5-20	ç		ЬМ	н		
8		,3,+,5,0	1/10+010	5		.60		L XB		5-20	C	ĿM	M	ᡔᢇᡰ	,	e
9		A 4,40,0		5		·55	T	PB		5-20	Ç	L-M	ĻΜ	M		
10		4,+,5,0	1.0+00	5		·45	6	L YB	g. 🗌 🛛	5-20	Ç	L-14		1-13	Sandy	4.11
		4+00W	10400	5		.15	T.	L RB	2. ±1	5	в	M-H	ruj [rM.	· · ·	· A

	LION	
	PROJECT RAINBOW PLOTTED AIR PHOTO	L
	DATE November 3, 1994	
	LOCALITY LAWLESS CREEK, TULAMEEN, B.C. SAMPLER, ERIK OSTENSOE	
•	NTS UIM TYPE DR organic SAMPLE LOCATION GRID SURV BDRK PT.S Ver of material colour % Gravel Horizon Clay Silt Sand REMAR	RK S
1	$\frac{1}{1,2},\frac{1}{3},\frac{1}{4},\frac{5}{5},\frac{6}{6},\frac{7}{1,8}$ $\frac{2}{9,10}$ $\frac{1}{1,12},\frac{1}{3},\frac{1}{4},\frac{15}{16},\frac{1}{1,0},\frac{1}{1,0},\frac{1}{2,0,021}$ $\frac{22}{23,24}$ $\frac{23}{25}$ $\frac{26}{27,28}$ $\frac{27}{30}$ $\frac{31}{32}$ $\frac{34}{35}$ $\frac{36}{37}$ $\frac{38}{38}$ $\frac{40}{41}$ $\frac{41}{41}$ $\frac{5}{1,0}$ $$	TE-1.
2	I J.F.F.S.O IIII S I O ED A L ME I E MA MAN	<i>TC</i> 1.
3	Libition II. On ridge	: Facing
4	HARDPAN TI	<u>L.L.</u>
5		
6	111 1714510 111 5 . CAO Br 10 FM H M As above. So	me stps
7		and tran
8	1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.	112 due 70 15 8+ 35W 1711.
9	19+00	
10		al 100 00 15
	10+00 .50 Red br 5 B L M M sandy, rusty, L	<i>B</i> .

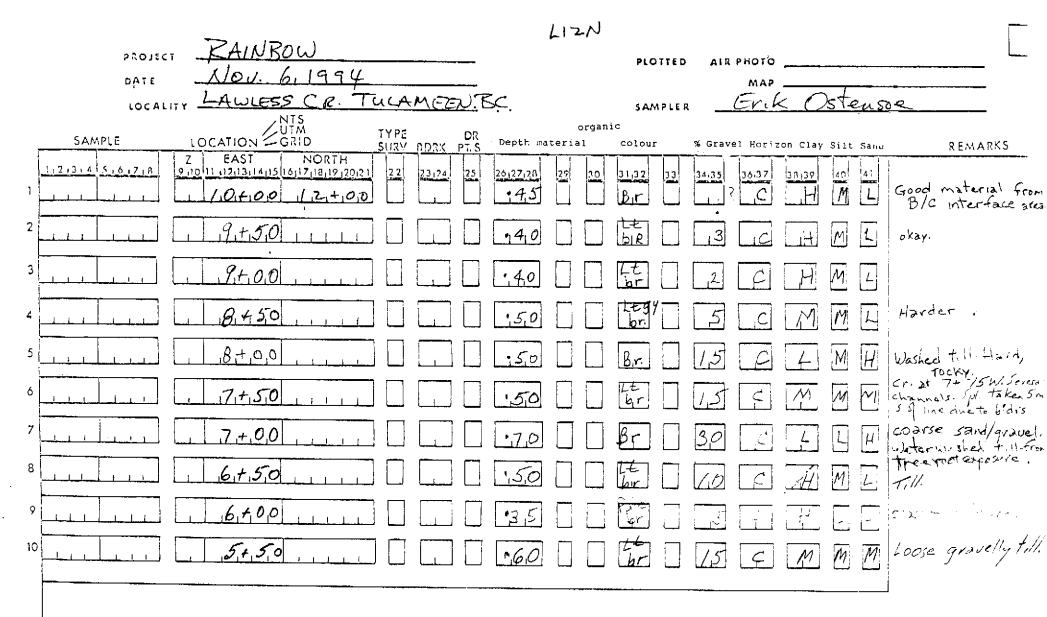


	PROJECT	RAINBOW			. IIN	PLOTTED	AIR PHOTO				
	DATE LOCALITY	November 2/3, LAWLESS CREEK.		<u>3</u> .C.		SAMPLER	MAP ERIK		TENSO	E	
p	SAMPLE	LOCATION CRID	TYPE SURM BORK P	DR TS Depth mate	organi d Fial		% Gravel Hori:	on Clay :	Silt Sand	R	EMARKS
	<u>.2.3.4 5.6.7.8</u>	Z W EAST NORTH 101111211311411511611711811212 15+10.01111111111	0121 22 23,24			31,32 Yez	34,35 36.37 (10 0	<u>эпізу</u> Н	40 41 M ?	Till	
2		151+1510		•4.0		AT .	20 30	M	MM	Mixed Elc. 1 V. Lard C.	steep
3		. 6.+0.0		•4,0		ay lar		H	ML	V. hardt	
4		6,+50		•60		Et]	25 C	M	M	Hart	sney tu and mail.
5		,7,+,0,0		4.0		ter [15 C	H		T.II. V.Steer	
- ا		, 1,+,5,0		50		Dkr 🗌	60 ? 0	1	ΜH	Poorsan	
7		, <u>8,+,00</u> , , , , , ,		150			20 C	Н	ML	Hard Car St at 7-	1-17 75707+85 J.
8		B+,50		150			25 [0		MH	Water Wa	the defines.
9		, 9,+0,0					S C	H	M	Till. 11	: 10.
10		9,+,5,0 10+00		·50 •65		Lyr IKgybr	5 C 2 C	H	ML	Stoney cle rocks: Clay u	y. Rounded with cobbles lacuetrine
						U1				May be	acustrine.

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PROJEC				PLOTTED	AIR PHOTO	e	
DATE	November 6, 1994 IT LAWLESS CR. TULAM	man Re			MAP	Ostensoe	12N.
LOCAL	ITY HADLESS CK. TUCAM	EENINC	org	SAMPLER anic	Crik	<u>Uniterise</u>	
SAMPLE	LOCATION GRID SURV	DR <u>DDRK PT.S</u>	Depth material	colour %	Gravel Horiz	on Clay Silt Sand	REMARKS
1,2,3,4 5,6,7,8	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	<u>23124</u> 25	26127128 29 30 •5-5	31,32 33	34.35 36.37 B	3.7.139 40 41 M M L	Т.11
	4+50		.6.0] Lebr	10 IC	MML	T.11
	4,+,0,0		.50] 🚰 🗌 [_ح [c	HML	Road cut. East side of road is at 4+04 w. w side thout 4+12 m
	3+50		•4.5	LE br	,5 C	HMZ	Till
5	, ,3,+,0,0		:50		_3 _C	H H L	Till-c'aley.
	1 21+1510		.35	Reder.	BB	MML	1
, , , , , , , , , , , , , , , , , , , ,	, ,Z,+,0,0 , , , , , , , , , , , , , , , , ,		13.0	Drewn	B	MM	Virocky Colluvium + soi
	/,4,5,0		-3.5	Br		H M L	
9			<u>·2.5</u>	Pele Yellew Br	BC	H H O	
0	0 + 00		•25	Graybr	5 C High B/C	H H L H M L	Much outcrop. old
				·			Much outcrop. old trenches. Angular large rock frags wi Clay infilling.

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	PROJECT RAINBOW DATE NOVEMBER 1/2, 1994	-	L13N	PLOTTED	AIR PHOTO		/3N
	IDEALITY LAWLESS CR. TULAMEEN, B			SAMPLER		OSTENSOE	
,	SAMPLE LOCATION GRID SURV BOOK PT	R D	organi Depth material		Gravel Horiz	on Clay Silt Sand	R EMARKS
J	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		<u>6127128</u> 22 30 1710	31,32 DX EDX	34.35 50 B	38139 40 41 L L M	much talks fones. Angular fongs.
2			.60	Val.Br	73 R	MMM	Til Da sore 20050-5
3			.70			MMM	? Det used the
4			.7.0	lyet	R C	MML	Π.Π.
5	<u>, z, t, 0, 0</u>		·60				Not it is to be
6	····		.50			H M M	
7			.50	grey [13 C	HMM	Hard till.
8	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		140	Gray	20 5	FI	
. 9	4400		:50	br [15 5	HMM	TillROAD
10	4,4,5,0		50 [br	1,0 C	H M	Tī11.
					<u> </u>		<u>.</u>

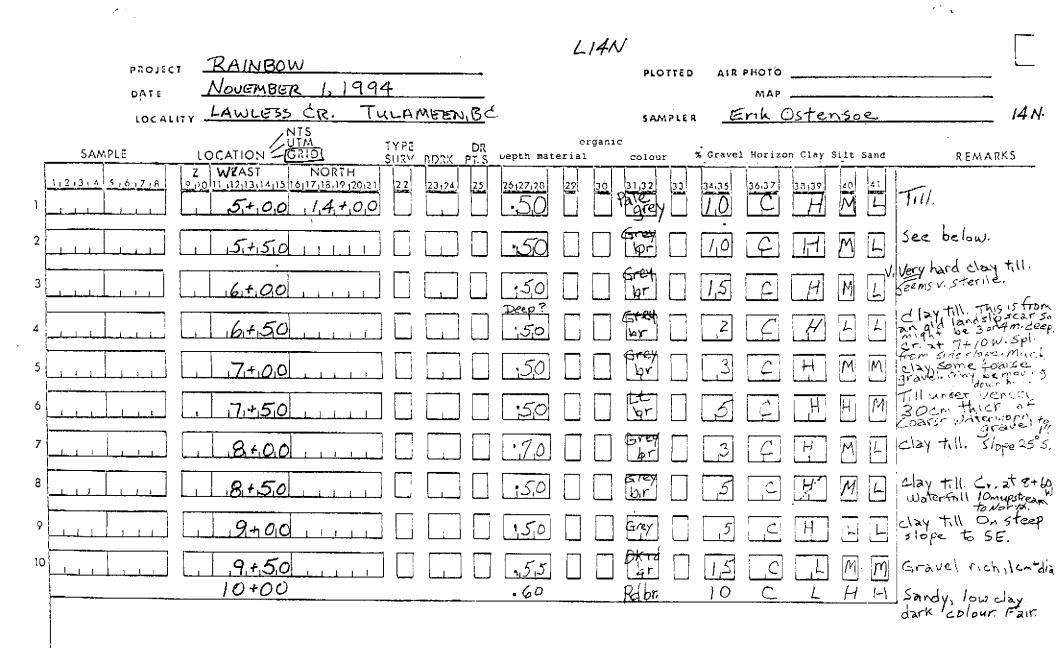
	PROJECT RAINBOW PLOTTED AIR PHOTO	
	DATE November 2, 1994 MAP	 /3N
	IOCALITY Lawless Cr. Tulanieen, B.C. SAMPLER Erik OSTENSOE	
-		REMARKS
1	$\frac{1}{12}, 3, 4, 5, 6, 7, 8 = \frac{2}{9}, \frac{10}{11}, \frac{12}{13}, \frac{14}{15}, \frac{15}{16}, \frac{17}{18}, \frac{19}{20021} = \frac{22}{23}, \frac{23}{24} = \frac{25}{25}, \frac{26}{27}, \frac{29}{30} = \frac{30}{31, 32} = \frac{34}{33} = \frac{36}{34, 35} = \frac{36}{27}, \frac{36}{31, 39} = \frac{40}{41} = \frac{41}{21}$	
2	LILLI I SHISOLILI I I I I I I I I I I I I I I I I I	hard till.
3		+111. 6+25W
4	LI LE SOLITION CONSIGNATION CALLANEY	till. Spl is
5	HMM TILlow	t <i>loosened</i> ait
6	I I I I I I I I I I I I I I I I I I I	
7		eep Stope to S. 8+7 5W
8		ceps/speto
9	HILL 19, +, 0,0	L till from L tree root.
10		
	10+00 .45 GreyBr C H M L TIll. Ha	ard, stoney.

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× 1			Ž,				۲. او ۱۰	
			L14N	/				
PROJECT	RAINBOW	·····			AIR PHOTO	•		
DATE	OCT 31, Nov. 1,			,	MAP	· · · · · ·		- 14N
LOCALITY	LAWLESS CR. T	ULAMBEN, BC		SAMPLER	ERIK	OSTENS	TOE	_
	LOCATION GRID	TYPE DR SURV ADAK PT.S	organ •Depth material	_	ravel Horizo	n Clay Silt Sar	nd REM	ARKS
1 <u>1121314</u> <u>5161718</u>	Z WEAST NORTH 10 11 12 13 14 15 161 7 18,17 20 1 D + 00 1 Arto		26127128 29 30 • S O	14005	.35 36.37 3 C	37,139 40 4 H		
2	19+50 111			Bre.	5 C	HAP	Maybe ti likely or	н Ъ.
3	1.4.90		50 🛛	Br. []	0 C	MH		
4	1,1,1,5,0		.50		0 C	MMF		+11
5	12-ti010		.50		5 <u>c</u>	MM M	Also took Sample for	B-horijon Comparison
6	121450		17.0		3 ØC	H H	5012.1/0+	-T11/ +
7	, 3, 40,0 , , , ,		-50		হ	HM		
8	3,+50		.53 🗌 🗌	br [2 7	HM	Clayey. Da	rk soil.
9	4,4010		-5.5		3 98	MM	Clayey. Da Fair to good Road E side	at 4+ 08W
	. 4.4.5.0		- <u>5</u> 5 [] [5 B/C	MM	M. Flatter gri to the west	Not till.

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		T a.			L	15N						
	PROJEC		711000				PLOTTED	AIR PI	ното	· · · · · · · · · · · · · · · · · · ·		
	DATE	October							MAP			
	LOCAL	ITY LAWLESS CREE	K, LULAME	<u>en, U.C</u> .			SAMPLES	a <u>Eri</u>	K OSTER	1506		
-	SAMPLE	LOCATION - GRID	D TYPE SURV	DR BD3K P7.S	Depun maler	organic 1al	colour	% Gravel	Horizon Clay	Silt Sand	REMARKS	
1	1,2,3,4 5,6,7,8	Z WE ST N 21011.1213.141516117		23124 25	26127128 - 5-9	30	31,32 31,32 33	34.35 25	16.37 38139 C O		Washed gravel. Like'y of ngalie	
2		4,+,50			িন্দ্রন		br [15	CL	MM	Fair to good in ."	
3		4+00	3_4		·35		BR	70	<u>C</u> H	[4] M	not till	
4		3+50			·45		BE		СН	HL	B ALL ALL ALL	
5		3,+00			.5,0			20		ME.		
6		, 2,+,5,0	1		<u>.</u> 55		YB4		CM	M	······································	
7		,2,+,00,			• 25		6. B	5	CM	M M		
8		1+50			.50		BR.		C M	MM		
9		1,1,+,0,0			•20		ER []		E M		er en en en la fertil. F	
10		0+00			:50 35			5 5	C 114 C H	M L	Tree 1 15th Rock;	1-

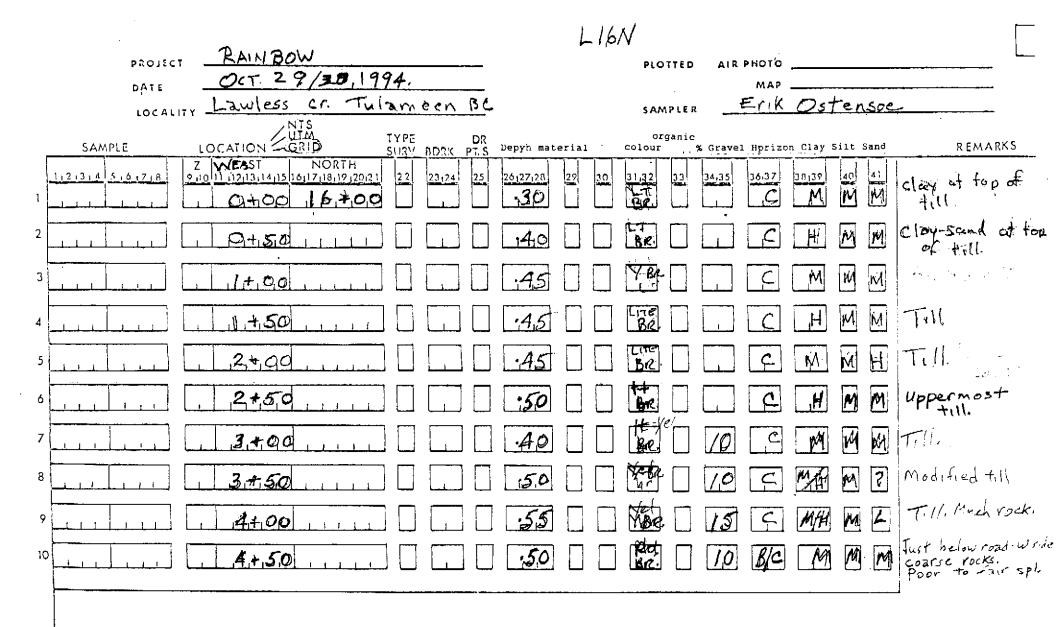
						L15N						
	· •	RAINBOW					PLOTTED	AIR PHOT	°			 _
		OCTOBER						MA	P			15N
	LOCALITY -		R. TULAMER	N. BC			SAMPLES	ERII	c Os-	TENSOE	, 	
	SAMPLE LO			DR BD3K PT.S	Depth mate	organ: rial	ic colour	% Gravel Ho	rizon Cla	y Silt Sand	REMARK5	
	Z 13 14 5 16 17 18 0 10	11,12,13,14,15[16]1	NORTH 7 <u>113117,20121</u> 22 7 .5.+ 100	23,24 25,	26127128 •55	27 30	31, <u>32</u> Kar but	34,35 10		40 41 M H	Sandy. Not Dkreddlsh, till.	
2		9,+,5,0			•1710		Greek [S C	ЭН	MM	Till Taken at 1-	+≶SW
3		9,+00			.50		Kar [ID B	1 D		Sandy Sol'. Real to 1k -	
4		8+50			•50		Ra Vor	12 (MM	Nepermast till	L
5		8,+,0,0			•60		िल्ला 🗌				的建立的	
6		7,+50	+ ī _ ↓		.50		Br []	20 3			May include topmost tr	11.
7		.7+00			•70		lar D	15 B/		M	Chorizon ?No	<i>t 1</i> ,
8		6+50			•.5,0		Pate [Washed to	e'
9		6+00			•70			20			reck = and	
10		5,4,5,0			•55		lare [2 4	M: F		÷.,
F											4	

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	LIEN											
	PROJECT RAINBOW PLOTTED AIR PHOT	٥٢٥										
		NAP IK OSTERUSOE										
	NTS UIM TYPE DR organic	Horizon Clay Silt Sand REMAR	KS									
1	Z EAST NORTH 1121314 5161718 21011 12131415161171819 20121 22 23174 25 26127128 27 30 31,22 33 34.35 36.31											
2		ZA LA M H Not till Road	inded evel									
3	3 1 6 7 6 7 6 7 1 1 1 1 1 1 1 1 1 1	C M M M TILL Stol take	00W Seren Ceren									
4		E I II II //₀+ till										
5	5											
6		EMMETIN										
7	7 []	C L H Gravely, roc	. ky.									
. 8	8	C Z M H Sandy/gravelly Daridge, Creek	cat 1, flows,									
9	° · · · · · · · · · · · · · · · · · · ·	CHEM?										
10		BLAM Mor bearock or BCLHHGravelly. 20	1									
		of small cr. (flo	WS SEly									

	PROJECT		k	AINGUN	-										17N
	DATE		Ct7	29/9					PLC	DITED AIS	MAP	9	2 11 03	6	
	LOCALI	TY		AM 5 87	<u>v • </u>				5 A.M	APLER		T.B.L		•••••	
SAMPL			NTS UTM GRIDI	SI	YPE 13V DD3K	DR PT, S	Depth mate	organ '	nic Colour	% Grav	el Horiz	on Clay :	Silt Sand	β	REMARKS
	6 17 18	2 5AS 2,1011,12,13 0,+		הדאכ 🗌	22 23124	25	26127128 • 445	20 T L	31,32 PBR	33 34,35 ZQ	36.37 4	эл <u>і</u> зу М	40 41 M M		
2		O,+	50 11	71+1010			.30	7	BR	+25	<u>ح</u> ۲	<u></u> н_м,	M M	Bediocle Loc ATIO	· · Approx
3		1+	00 1	7,+00	< 7		.55	7 4	P.Ba	20	Ç	M	m M		
4		/ _+	50 J	7+00			.45	T L	P .Y Ba	+ 15	Ç	M	M M-M		
5		2,7	00 1	7+ 00			.40	- L	PBr.	15-20	Ç	м,	MM		
6		, 27	50 1	7+00	5		.55	74	P-Y BR	-+ 15	C	M 1	M M4	H. Top	of C
7		3+	00 ,/	7,+,00			-50	TIM	DK-B-	0	B	M-H	M [L]	Low Di	aw.
8		37.	50 J	7+,00	3 7		.50	7 L	P,Br.	5	<u>C</u> ?	M	M.M.		
9	<u>1</u> <u>1</u>	4+	00 1	7+100			.45	22	PBA	+15	Ę	M.	MM	- - -	
10	i nin	4,+	50 1	7+00			-25	7	P.B.	-20	4	Н	m m	Lower BANK	Roan by ditch-
		<u> </u>		· · · · · · · · · · · · · · · · · · ·								<u>. </u>			

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				L171	v			
	PROJECT	TRAINBOW	(5 Q <i>A</i>		PLOTTED A1	R PHOTO		-
	DATE	OCTOBER 30	<u>(174)</u>	• •		MAP		
	LOCALITY	LAWLESS CR.	TULAMEEN,	2.C.	SAMPLER	ERIK OS	1 E N20E	-
_	SAMPLE	LOCATION - GRID	TYPE DR SURY BDRK PT.S	organi Depth material		vel Horizon Clay Si	It Sand REM.	ARKS
	121314 5161718	Z W#AST NORTH		26127,28 2610 2610 27,28 29 30 30	31,32 33 34,35 24,35 70 10	36.37 <u>7</u> <u>7</u> <u>7</u>	M M Till-border	therial.
2		15450 1111		-50			M M T.I.	
3		16,+,0,0		35	Ter 20		E E Colimz 1	i y i v jus Si je je je je
4		6+150		40			M I Much so	
5		7,40,0		•4.5	br 20		M H Correr	5 hy
6		7,+,570		50] [] [] [] []	M M 521-19 900	;
7		, 8,4,0,0		:40			H M By rocks	
8		,8,+,5,0		50			M M Not +:	
9		. 9,+00		<u>.20</u>			M H Sand	. avel
ן סנ ן		9 , + , 5 , 0 (0+00		50 [] 145	Rusty 20		M. H. Sandy M. H. Sandy	G + (
					red		1	

	PROJECT	RAINBOW						
	DATE	Oct. 29, 190	14 (SAT.)		PLOTTED	MAP _		IBN-
	LOCALITY	LAWLESS CR.	TULAMEEN	B.C.	SAMPLER	Erik O		
1	SAMPLE		TYPE DR SURY DDRK PT.S	organ: Depth material		% Gravel Horizo	on Clay Silt Sand	REMARKS
1	<u>1,2,3,4</u> 5,6,7,8 <u>2,1</u>	₩₩7AST NORTH 011_1213,14,15 16117,18,19,20 1,0,4,0,0 1/,8,+,0		26127,28 29 30 •45		34,35 <u>36,37</u> <u></u>	38.139 40 41 M M M	Sandy restant
2		9+5P		.4.5		10 10	LHH	Similar to 1001
3		9.+00		·45 [Bren [5 0	HML	the second second
4		8+50		.50	Bra	10 C	M H M	•
5		8, 4,0,0		.6.0		10 C	HML	port a constant
6		7, +50] [.6.6] [Bre	15 C	MHM	ar a practic
7		.7.+0.0		.4.5	हित्		MHH	State which we have
8		6+50		.50	Be	10 C (M H H	Rockey and the
9		6190] .75 [] [MHH	on since the creat 54 90 his creat spin
10		5,4,5,0		50	Bre -	5 C	HHL	Start Resty.
		· · · · · · · · · · · · · · · · · · ·			· · · · · · · · · · · · · · · · · · ·			·

 $\gamma = N_{1}$

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PROJECT	RAINBOW			PLOTT	D AIR PHOTO		
DATE	OCT. 29, 1994			<u> </u>			
LOCALITY	LAWLESS CR. THI	AMEENBO					
SAMPLE		TYPE DR SURV DDRK PT.S	or Depth material	ganic colour	% Gravel Horizo	n Clay Silt S	and REMARKS
	5400 13141516117181970121	22 23124 25	26127128 29 1 510	30 31,32 3: 30 31,32 3:	34,35 36,37	30130 40 H	Cr. + 5+20416 5+254.
2	4+50		<u>,5</u> 0			H H	M Road 1 +104 14
3	A.+0,0		50	Vet Bre		MM	
4	3,+50		·A.0	Be C		M	
s	, 3,+,0,0		35			M M	
6	12,+,5,0		:7.0			MW	
7	,2,+,0,0		.45			HM	M Strong Hundhich
8	1+50		;4,0	20 Bre		MM	M Till V. S. staston
9			<u>120</u>				
	0+09		· <u>3</u> 5	Red Br		MM	M FALL M V. Focky grow
							Pear Pr

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2001501	RAINBON	ر.			2		PHOTO			L
DATE .	OCT	1994	_				MAP	92	4056	
LOCALITY	TULAMET		`		57	AMPLER		T. B. LISL	. ඌ	
SAMPLE L	OCATION - GRID	- TYPE SUBY	DR BDRK PT.S	c Depth materia	rganie 1 colo	ur %Grav	el Horiz	on Clay Sil	t Sand	REMARKS
	EAST W NO	RTH	23,74 25	26127,28 29 -40 TF?	30 31,32 L RG	33 34.35	36.37 B ⁷ ,	38139 4	2 41	
2	4+00 119	1400		·120 TF	L RIB] [] + <u>50</u>	C^{3}	4		
3	3+50 19	17 pc		.55 T	LPB	20	C 2	M		
	3+00 12	R+,00		.45 7	L P.B.	, 25	<u>ر</u> ۲	L-M. M	у м-н,	
5	1217,50 1	7,4,0,0 5		.45 T	L P.B.	2 5	<i>C</i>	M. A	M	
	121+100 119	7,7,00		.50	L P.B	g. 5	5	M-H	M	
	1,450 19	400 5	Classe	·125 T	L DK	3. 10-15	Ę	MTH.	4 M	
8	1+00 19	100	?	·40 T	L P.B		G	M		
9 *	0+50 1	9.+00	?	·45 T	L P.B	d. +15	<u>,</u>	M	1	
	,0+00 ,1,	9,7.90		· 40 7	L P.E	4-15		<u>M</u> .	M. M. C.	
C, e										

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	PROJECT .	RAINTSOUL			PLOTTED	AIR PHOTO		[9,4
	DATE -	007 .20/94 TULAMOON	· · · ·			MAP		
	LOCALITY	, NTS		org	\$AMPLER manic			
1	······		TYPE DR SURY DORK PT.S	Depth material	colour %	Gravel Horizon Cl	ay Silt Sand R	EMARKS
1	1,2,3,4 5,6,7,8 2,13 -1,-1 -1 -1	$\frac{2}{10} + 0.0 + 1.9 + 0.0$	2 2 23,724 2.5		30 31,32 33 34, L Be. 15-			T. (1
2		1917150 111914019		807	Br Z	0 C H	ML EAD SZM	Playey till.
3		9700 19400		-50 7	L Pale 1	s C M		
4		18,7,50 ,1,9,7,00		·40 7		5 C M+		
5		BTOP 1.9.1.00		· <i>55</i> 7	4 RB +2	p 32, M	MM	
6		17,+,50 1,9,+,00		- 60 7	L YB Z	0 G M-H	M m-44	
7		7,7,00 ,1,9,2,00		.65 7	L YB ±2	р <u>С</u> м-н	+ m m	
8		6750 19200		.60 7			M M IOM W	of CK.
9		6400 19.400		1.5e 7		<i>.</i>	m m-4.	Ango lev
10		5+50 19+00 5+00 19+00		-65 T -55 T	L 13 1 2 L 995. 15	5 C ² t=n 20 C t-m	M M Rocker	ing o lar.
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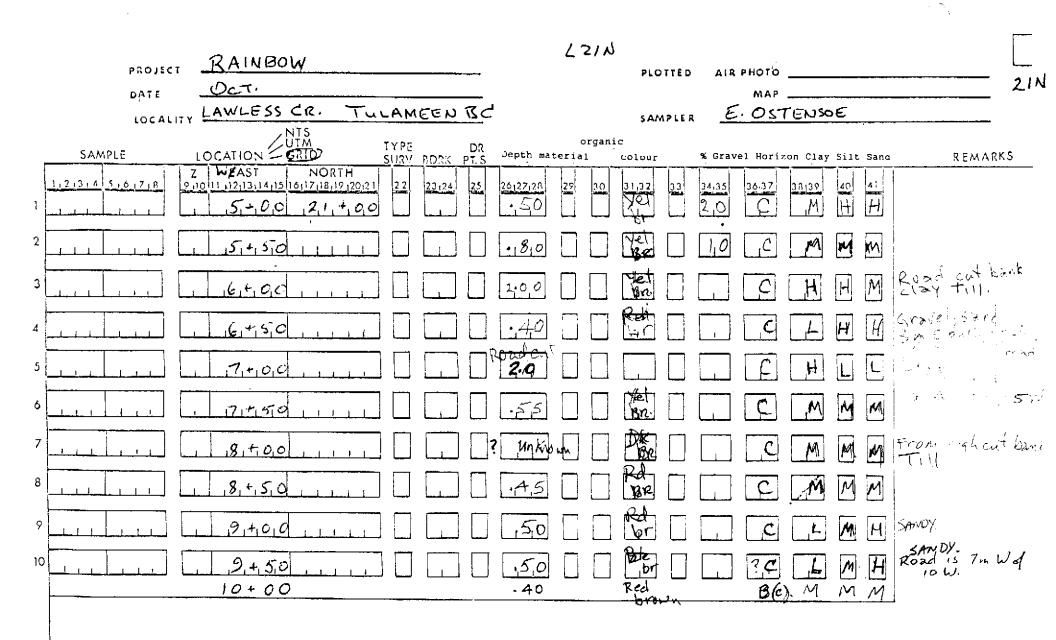
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PROJECT -	KAINBOW.	2			P. OTTED	AIR F	ното					
DATE -	OCT. 27 (94	· · · · · · · · · · · · · · · · · · ·					MAP		1240			
LOCALITY	TULAMUTEN.				SAMPLE			<u> ب</u>	USLE			
SAMPLE L	OCATION STA	TYPE DR SURY BORK PLS	Depth mater	organic rial	colour	% Grave	1 Horiz	on Clay	Silt Sand		REMARKS	
7	DIT 12131415 161718.19120121 DIT 12131415 161718.19120121 DIT 101 12 12 10 10	22 23174 25 5 ?	26 <u>127128</u> • 6 0		31,32 33 P1Be	34.35 Zp	36:37 C	3 <u>8139</u> M.	40 41 M M			
2	101+1510 12101+1010	570	•40		Pibe.	+15	¢ ?	M				
3	11+00 20+00		.50		Y.Ba	15	C	M	M H			
	11+150 12101000		.45	TL	Y.B.	15	Ģ	M	MM			
5	121+1010 ,219+100		.60		RBe 🗌	15	<u>B?</u>	M	MM			
6	121+159 1210+100		•,6,0		Þ.Ba	15	B ² ₁ C ²	M	MM			
	31,00 ,20,400		.30	7	BR	20	B	M	M			
8	3+159 120+100		• 70		YBe	+15	C	κή.	MM	Near	ord Pi	45
9	HHUN JUHAC		•40		P.B.	20	C	M	MM			
	A.+50 120+00		·50 ·65		7 8 2. BR	20 20	ß	M-H M	M M M N	Near	Bedroc	216-

20N

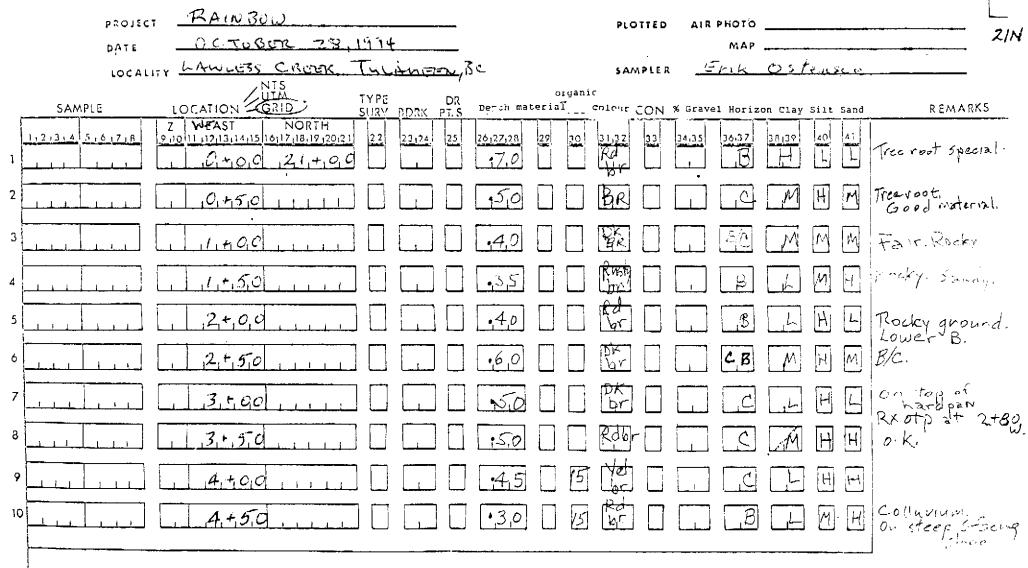
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	21039	RAINE	ാധ 2.								ρκοτό						20N.
	DATE		27 194			-		PL	OTTED	дік	мар	•	9214	056			
	LOCAL	ITY TOLAM	1 5 B W		•	_		5 A	MPLER		·	- (- E - ,	۲.				
	SAMPLE	LOCATION	NTS UTM GRID	TYPE Sury	D <u>2038 PT</u>	R S Depth m	or naterial	ganic colo	ve %	Gravel	Norizo	n Clay	Silt 5	and		REMAR	K\$
1	1,2,3,4 5,6,7,R	Z WSAST 0.10 11.02030405 1.51+5 P		22	23124 2	s <u>26127128</u> •1 25		0 31,32 L YBR		34.35	36.37 Ç	38139 H	40		t. Serve		•
2		161400	1210+1010			·150	7	PiBa		20	Ę	MTH	Μ	M-L			
3		6_+_S p	20,400			-6.0		BI		-5	A	4'	2				· .
4		17,+00	1201+,00			.50		GR		15	<i>C</i> ?	M	Μ	M	1997 - 19 19 - 19 - 19		
5		, ,7,+,S,O	120,+,00			•60] 7 [L YBA		15	C 2	M	Μ	M			
6		, <u>181400</u>	201+190] [3]		.65		4 X-9 X-8		20	C?	M	Μ	M			
7		8+,5P	20,400			.70		L RB		20	<u>c</u> ?	M	М	M			
8		, 9rt pp	20,100] []		.60] 🖻 (L YBA BR] []-/	15	C	M	M	MA. T	ίορ	of C'	
9		9,450	12101+160] []		·6 ₀		L BR		15720	٢?	Н	Μ	L			
10		, 1,0,+, o,c		, []		.59] - []		å.	20	٢,2	M	М	M			
			<u>+</u>							····			••••				



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	project		RAINBOW						PLOT	TED	AIR	рното						H.
	DATE LOCAL		OCTORES LAWLESS			MAR BC	_		SAM?	LER	H	MAP Erik (<u>92</u> 2: Ken			6		22N
SAMPLE		L	OCATION H	NTS JTM SRIDJ		DR DDRK PT.S		organ material	_			Horiz					, R E M A	RKS
2+314 510	61718	Z	WEAST	NORTH	1 22	23.74 25 Schist	26127128 •14,0	29 30	31,32 Red hr	33	34,35 1_0	36:37 C	20139 L	40 M	A1 M	Rocky Splist	1 x6 x BR of e. Rus st fm	to adjoins by sericit cy sericit SW. moti
			4,+,5,0				• 70		lar [10		M	M	M	-to Not	5+2: tilli	S WE PROVE
i	1 1		4-00				150		<u>ак</u> 'яу [1,0	<u> </u>	M	M	М	Till		
			3+50				•50		hind br		5	LC	Щ	Μ	M	From		l ately mer
			13,-10,0				•6,0		Mor A		10		M	نبيت	فببيا	<i>+-</i> : -		
			121+150				·3.0		DK br		5	C/.B?	M	M	M	1200 28 A	т. С. Т. С.	
	1		,2,+0,0				.30		Br		[/]0]	В	M	1	M	Colly and	reddis y. soil	a-br.
1.4			1, +, 5,0				:4.0		br		10	<u> </u>	M	1	H	V.rock Not =	y. 5017	,

:40

:6,0

·50

1.1.2

1

2

3

4

5

6

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1+00

0+50

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Grey br DKGrey

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H Sandy , tocky 7.11.

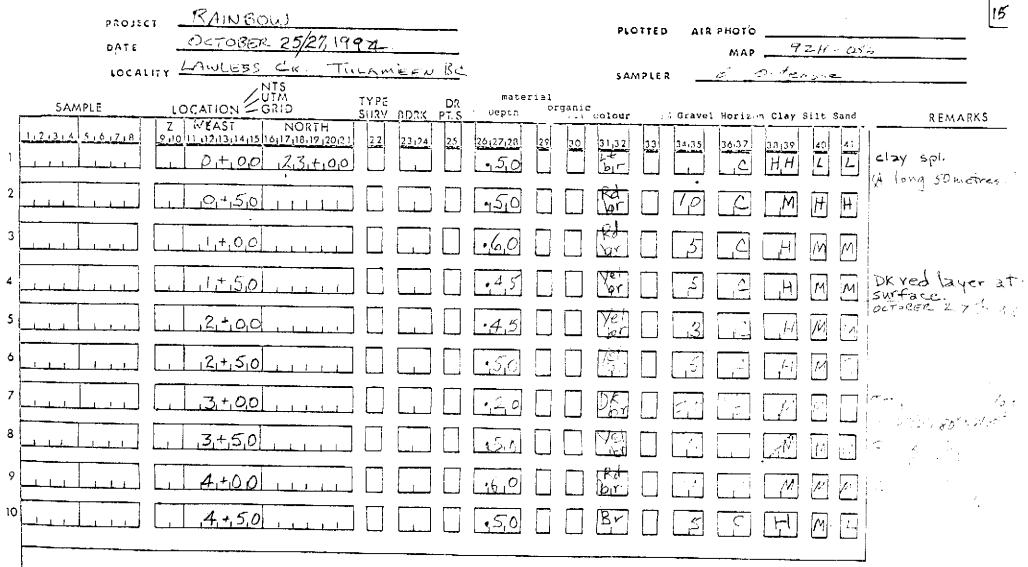
Muchy till-clay Would busty B'be better? Tree root. All clay.

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	PROJECT	RAINBOW OCT. 25 194	ef.				PLOTI	TED AIR	PHOTO				- 22N
	•	LANGESS CR NIS		<u>Re</u> 1			\$AMP	1 E R	MAP Erik		H - D.	··· (,,	
	SAMPLE		TYPE <u>Surv Dork F</u>	DR 9 <u>7. S</u>	Dopth materi	organ al	ic ^{Colour}	% Grav	ei Horiz	on Clay	Silt Sand	B REA	A A RKS
1	<u>12,314</u> 5,617,8	10111203040508012080	2 120:21 2.2 23:24	25	26127.28 •50	<u>30</u>	31,32 Dir	13 34.35 1,5	36:37 C	37,39 M	40 41 M M	Topmost 12 till?	iver of
2		9,+,5,0			1.810		br [ĹĈ	Ч	ML	Soil Hake	A 25
3		9,4,0,0			.60					M	HM	Not the use	Good spin
4		.3,+,≞,o			•,4,0		dk bir	5	C	M	MM	Deep soil Dirt mon. till laye	1. Top of
5		18,-10,0			· 8p		ler [C	М	MM	Till	r
6		17141510 111			.9.0		le br	[70]	C	,H		Corgeks at 7. Sp Aron or Rocky HIN Forest Fast	1) 7-165W COU LOANY DAVER
7		,7,+,0,0 , , ,			.8.0		tt br] []0]	C	,H		Forest Fast	JA 7+50×
8		6-50			.6.5				<u>د</u>	M			
9		1611010 111			150		br [1.5	F			Pale brown Hard stone	to grey
10		5,1,5,0			·20		LE bir	10		M		Stoney t. 1 slope W'ly +	From o creek
												1 24 5+541	~

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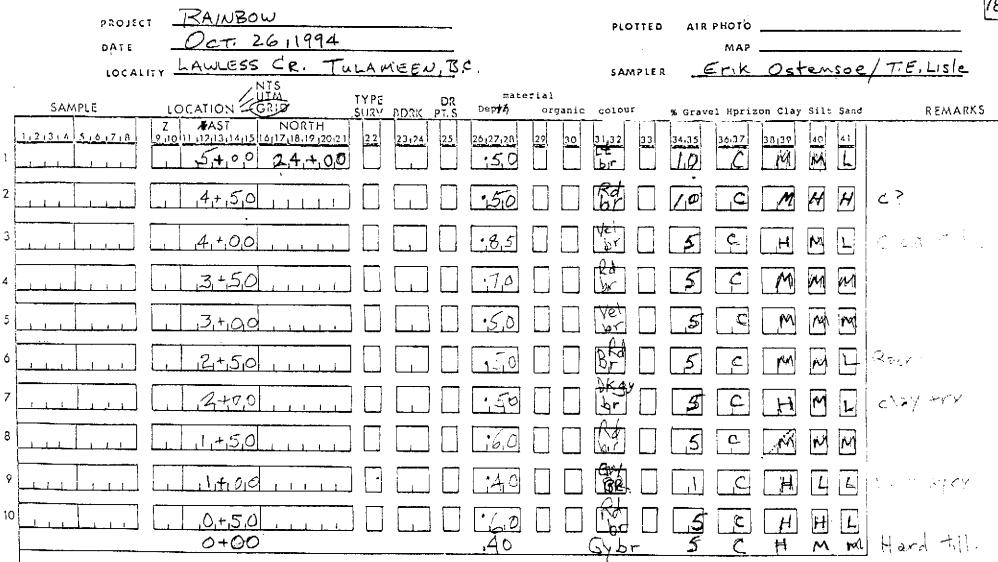


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	PROJECT	RAINBOW		_				16
	DATE	OCTOBER	27, 1994	-	PLOTTED	аі г рното Мар		
	LOCALITY	LAWLESS CR.	TULAMEEN,	BC	SAMPLER		Ostensoe	
	SAMPLE (OCATION SRID	TYPE D	R organ	nic			
1	Z	EAST NORT			colour % G	ravel Horigon	Clay Silt Sand	REMARKS
1		<u>11 (12)3(14)15 16)17(18)15</u> 5+00 2.3,4	الافا المستعين المستحي	5 <u>26127,28</u> <u>29</u> <u>30</u>	31,32 33 DVK Ba	34.35 36.37 3 B/C	30,39 40 41 H	Rocky Collovium?
2		5,+50		35	LBe [10 C	LHH	on Bedrock.
3		16,+,0,0		55 🛛	LBR,	ρÇ	M M.	
4		161+50		.4,5		5 [C	HML	
5		77.00] ·A.5		5 C	H L L	-++ 11.
6		7,+,50				5 C		
7		8, -, 0, 0		50		10 C		Till slash sty Cresh at 8+10 W.
8		,8,+,50,,,,		-5,0	Br	3		Cred at 8+10 ~. Road el 8+60-70
9		9,+0,0				3 C	HML	Clay Till W
10		9+50 10+00] [53]		S C	HMM	711
					Yet's	<u>/ 0 </u>	MMH	Sandy +,11

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				LZ4N			10
	PROJECT	RAINBOW		PLOTTE			17
	DATE	Oct. 26, 1994			MAP	······································	
	LOCALITY	Lawless Creek. T.	limeer, B.C	SAMPLE	R ERKO	STENSOE	
-	SAMPLE		PE DR RV NDRK PT.S Depth ma	organic terial colcur	% Gravel Horizon Cl	ay Silt Sand REMAR	KS
1	1,2,3,4 5,6,7,β 2,1 -1,2,3,4 5,6,7,β 2,1	WZAST NORTH 0 11 112113114115 16117 18,19,20,21 1 10,7 10,0 12,4,+10,0	22 23,24 25 26127,28 15,0	29 <u>30</u> <u>31,32</u> <u>33</u> Br	34.35 36.37 30.37 30.39 10 10 10		ccial
2		9,+,5,0,,,,,,	-1415	Pate	5 C M	M M Possible Till,	
3		, 3, +, 0, 0		Grey br	10 [] [M	M M Till Dense B RODA From 8+	72 +
4		13,+15,0,	<u> </u>		M. 2 0.1	U II II Till On stop	inii. Nair Aran ann
5		8,+;0,0		br		M L slash e 20 to	0₩1 7+75 W.
6		17,+,5,0					
7		.7.+.0.0					
8		6, +, 5, 0					, Ν
9 10							
		5,+,5,0					

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	PROJECT	RAINBOW	PLOTTED AIR PHOTO	
	DATE	October 24, 1994	MAP 924-056	
	LOCALITY		SAMPLER Erik Ostensoe	
	SAMPLE	LOCATION GRID SURV BORK PT.S	organic Depth material Colour %Gravel Horizon Clay Silt Sand R	
1	<u>1,2,3,14</u> 5,16,17,8 9,	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
2				- 4
3				
4				
5			LEO Br 3 C H U M Upper til	
6				
7			. 90 DET I SCHEL Motored the	
8		3,+,5,0	B. B. C. C. M. H. Stratter	
9			550 CEEEEEEEEEEEEEEEEEEEEEE	1
10		<u>4, +, 50</u>	3.5 Br 20 B/C 1 M M Hoorly developed horizon: Edge & forest at 4+3	J.
			Otps an aroun	d.

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L 25N

	PROJEC	r												12
	DATE					-		PLOT	TED AIR	рното Мар				
	LOCALI	7.7			•	-		SAMP	LER					
	SAMPLE	LOCATION	NTS UTM GRID	Ť Y PE SU 2V	D. BD3K PT.		organi terial	c Colour	% Grave	≥l Horiz	on Clay	Silt Sand	r R	EMARKS
1	1,2,3,4,5,6,7,B	Z //EA5T 9.10111.12,13,11 5.4	NORTH 4115(16)17,18,19,20 29 2.5.5.10	21 22	23124		29 30	31,32 Rd	1,5	36.37	38138 M	40 41 M M	What is	rock at
2			1			130					H		c1211501	soil. the black the brown
3						•4,5		Rea Jori		3	Ц			Sate Sate - S
4						•4 ×] [/,0]		M			
5		17,*.	20			<u>;</u> 30		Por [H	MM		
6	· · · · · · · · · · · · · · · · · · ·	7.4	50			· <u>5</u> 0		Mid		Ĺ	H		1.7	
7		. jô, 4	0.0 Oct. 25/94			.40		l'ar	1,5	C	M	MM	TIL RO	ocky!
8						16,0		yei br	1,0	2	[M Z	Tilli Fin	re of woods 175 W. Cr. 27 8 + 70W.
9		19 ,+,,	0011			:50		V pale brown grey	[10]		[H]			
10		(0+c				·55		bir [[H] M	M M M M	T.II.	ave post
										<u> </u>		1*1 1*1	<u></u>	* 9+ 75W

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	PROJEC DATE	0 CT 24, 199					PLOTTED	AIR	рното мар	92 4	1 05	6
		ITY TULAMOUN					SAMPLER			E. LISUS		_ , , _
-	SAMPLE	LOCATION GRIDE	TY PE SURM	ם <u>הסגר את סק</u>	epth materi	organi c c ial	colour	% Grav	vel Hori	zon Clay 5	ilt San	a REMARKS
1	1,2,3,4,5,6,7,8	Z EAST NOF 9,1011,12,13,14,15 1.0,17,18, 1.0,14,10,026,17	19 12012 1 2.2	23,24 25	26127128	27 <u>30</u> 51 6 2 L	31,32 33 BR.	34.35 ZO	36.37 B	30139 40 H M	K	CRBEIL BOB - Clay-Si Poise Squepler + Grove 1-
2		1 01 1+1510 2141	+1010 S		70	74	y Br	153	4	M-IH M	L	ISM to SE of Star
3		1 de +1 +100 Z 161 1	+ 90 \$.65	74	P BR Y Be	15-22	G	<u>w</u> w	\$9	Top se'c'
4		1 + 50 26	HOC S		.50	74	YIB	10115	¢	M [14]		TPEE Proving
5		21110026	+ 00 5		.70	74	XB]	15	C	MM		
6		1 21 171510 2161	+190 5		. 60		Bfe	15	<u> </u>	M M		THE CONTRACTOR
7		3. 17.00 2.6	+190		.50	7 2	RBe -	15-20	C ⁻ ?	1 P		Bistoner 15'
8		3 1+ 1510 ZG	+1010		.50	72	YB2.	20	C]	thender service
9		4 1 10024	+ 90 5		. 60	Ŧ 4	Per -	- 15	<u>c</u> ?			
10		4 + 50 26			• 4.5		Be	20	<u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>			suberap- angular Frags
		5+00 26	+06 5		.55	+	PBR.	15	C.	~ ,	u m	

26 N.

PROJECT DATE				PLOTTED A	MA2	92H 056	
•	TULAMEEN'			SAMPLER	م. مربق <u>مربق میں میں میں میں میں میں میں میں م</u>	TC LISIE	<u></u>
SAMPLE	LOCATION - GRID	TYPE DR SURY BORK PT.S	Depth material	nic colour % Grav	el Horizon Cl a	Y Silt Sand	REMARKS
1,2,3,4,5,6,7,8	Z EAST NORTH 9 110111 1211311411516117118119120121 1 51 1+1515 ZIG 14 190	22 23124 25	26127178 29 3	0 31,32 33 34,3 A ic 4/15			
2	6 1+1010 ZIG 1+1010		.40 7	Pale Ise			
3	6, + 50 26+00		.15 7	Pare +15			Brocoric?
	7 +10,02,61+1010		.55 7	Pole YBA	e 4-	MMH	Edge of NK brank.
5	7, +5026 +100		2.40 7	4 YBe 25		M M-H	· · ·
6	1 8 1+ 00 2 6 1+ 1010	⊈ <u> </u>	•30 F	(- 7,BR - 2,0			
7	8 +50 Z 6 + 1010			- YiBe, Ze		A M M	
8	9 + 00 2 6 + 00		1.2:0 77	4 BR 24			ON Strong ?
9 	4 +150 ZG1 +190			L BR 29			Poss ć
	1,0,1,00 Z.G. 1,00			G Be 1+2	0 <u>B</u> ⁷ N	1. m. mt	
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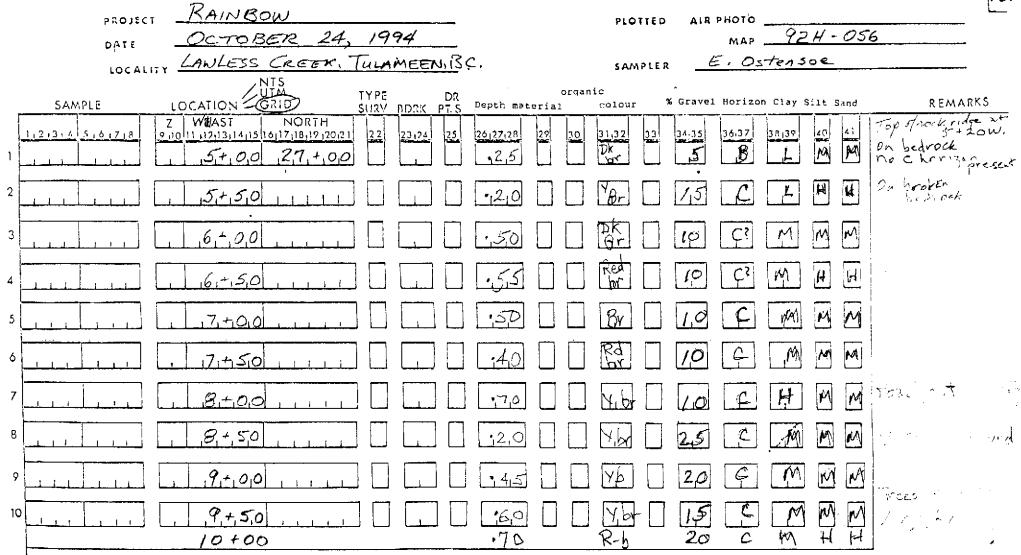
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	PROJECT DATE	RAINBOW October 23	,1994				PLOT	TED		MAP		2H-	056
	LOCALITY	Lawless Creek.	Talameen Ba				S AM	PLER	<u> </u>	<u>ak O</u>)stens	50- 2	,
	SAMPLE	OCATION CRID	TYPE Sury Bork	DR PT. S	Depth mate	% organie rial (colour	%	Gravel	Horizo	n Clay S	ilt_sam	-R-EMARKS
1	Z 1, 2, 3, 4 5, 6, 7, 8 0, 1	011.121314115 1611711819 011.121314115 1611711819 01+1010 12.7.4	H 120121 22 23124	25	26127128 15D	27 30	31,32 7 br	33	14,35	36.37 _C	30136 H	40 A: M IM	Hard packed till
2		10,450			45		Br		0	<u>"C</u>	H	MM] May not be hardp
3.					.50	5	Grey		0		H		1 production Section 2000 production and Section 2000 production and Section 2000
* 4		11+150											Ny service services
5		12,+,0,0			·60		cr cr		/,C	 		H] Rocky
6		21510			·5-0		br		_5-				Hardpan
7		,3,+,0,0			·35		<u>Br</u>		- É	<u>[</u> 2]	M		_ ក្រុងស្ទុង ហ
8		3,+,5,0			16,5				5	62	Ń	<u>m</u>	
9		A+0,0			•,570				: 5			<u></u>	į
10		4,+5,0			•.6.0		Br		< 10			<i>#</i> - 7	Poorly dev. horizon I class of forest a 4+30w
		· · · · · · · · · · · · · · · · · · ·				•							

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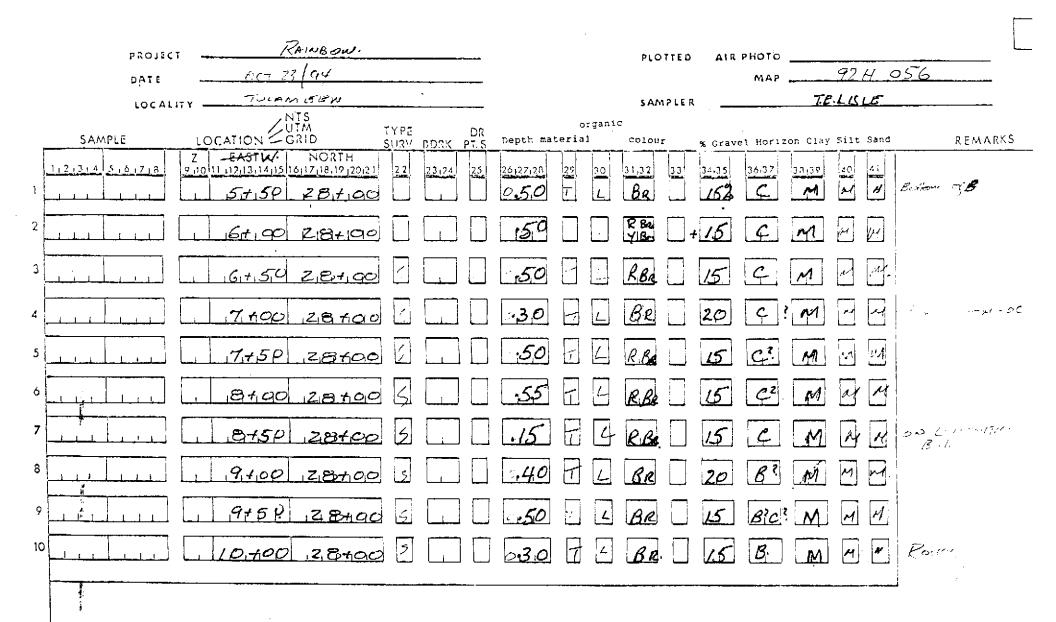


	PROJECT .	RAIWBOW				PLOTTED	AIR PHOTO			
	DATE	OCT 24, 1994					MAP		056	
	LOCALITY	TULAMEEN	•			SAMPLER		7.E ()	SLE	
F	SAMPLE L		TYPE DR SURY RDRK PT.S	Depth mater	organic isl		6 Gravel Horiz	on Clay Si	lt Sand	REMARKS
1	Z 1121314 5161718 910	- EAST W NORTH 11.12,13,14,15,16,17,18,19,20,21 10,17,10,0 12,18,400	22 23124 25	25127128 0,40	2 <u>30</u> T	31,32 33 YBR	34,35 7,5 26,37	30,39		
2		0,7,50 121871010	2	.55 7	M	BR.	15 B	11	4 14	
3		1+100 28+90	5	-50	70	YBR [wist G	M .	1 M.	
4		11+50 28+00		.60	7 4	BR	+10 B?	M -		
5		2,+10,0 28,+,00	9	.50	76	Be	15 4		4 M	TOP OF C
6		121+519 128+00	8	·16 P -	7	YR [+15 4	MIH		we z
7		3+00 28+00		· ,6 ,0 7	- 4	Y ₁ B	+1 E C	Mitt		TREE ROOT ANS. NBT
8		3+50 28+00	3	165		B.e.	-15 4?	M		4.0 Motris Noilly St.
9		EHOID 28+ 90	§	.30	7 [_	YBe [15° G	MTH		TRUE ROOT
10		4+50 28+00 5+00 28+00		-70	T T L	Br	10715 B 15 C	M-H	M . M.	e Below Tree Coot
			5= 81			-				

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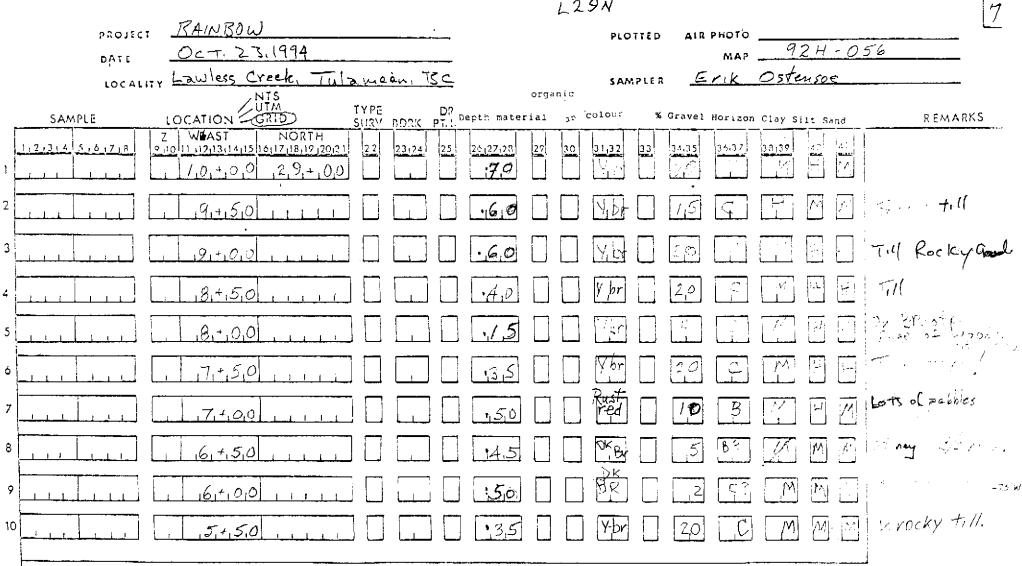
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PROJECT RAINBOW	L2911 8
DATE Detober 23,195	PLOTTED AIR PHOTO 24 MAP 92H-055
LOCALITY Lawless Creek, T	ulameen. B.C. SAMPLER Erit Mostensore
SAMPLE LOCATION GRID	Organic YPE DR Depth material epicur % Gravel Horizon Clay Silt Sand REMARKS
Z MEAST NORTH	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
3	
4	
5 3 5 0 2	
6 1 12 + 50	$\square \square $
7	1
8	
9	I I I I I I I I I I I I I I I I I I I
$10 \begin{array}{c c} & & & \\ & & & & \\ & & & \\ & & & \\ & & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & $	<u>Go</u> <u>Bir</u> <u>J</u>
	CM hole. OT of stope.

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30 N'

	PROJEC	т <u>Rains</u> Ост	23/84 ·				PLOTTED	AIR PH	-	924/	256	
	DATE	TILA	NEEN	•			SAMPLER		MAP	T.E.C.ISL		
	SAMPLE		TS TM TYP RID		. Depth mat	organı erial	_	% Gravel H	orizon Clay	Silt Sand		REMARKS
1	1121314 5161718	Z EAST V 9,10 11,12,13,14,151. St. 0,0		23,24 25	26127128 2	2 30 T	31,32 33 BR	24.35 15	25155 75.0 M	40 41 M M		
2		14.4.50	30141010 2	2	0150		Be.	15	f? M	k m.		
3		.4,+,00	30,400	?	0,50		Pole	15%	E M	MM	:	
4		3+50	30+100 9		o,S,O		Pale BR	15,72	1	7		
5		3,+,0,0	30100	AP	0.15	í 🖌	RBe	5-10	g 1' <u>2</u> m	~ 4	on entr	gr + follow
6		12+50	30,400 4		0150	7	Pula R.P.	15%	g []		:	
7		12.t O Q	30+00		.67	7 [H]	<u>B1.</u>	~ 5	A? H.	<u> </u>	Poor	Somple.
8		1:+50	30+00 6		·65	1 4	RB	+15%	3'c' H	M 4		
9		1400	30+00 5] []	.60	T M	Be	15%	3 ⁷ H	~ 4	0.5 K.#	Black - Mar
10		0+50 0+00	30+00 S		•#5 •#5	7 E 7	BR. Pale	10-15 [150	C? L-M C M	M.L.	, -	

	,				30N;			
	PROJECT DATE LOCALIT	·			PLÖTTED SAMPLET	MAP	92 H T.E. HISLE	/056
	SAMPLE	LOCATION - GRID	TYPE DR SUBV_BDRK_PT.S	Depth material	organic Colour	% Gravel Horiz	on Clay Silt Sand	REMARKS
1	1,21314 5161718	Z 2.10 11.12,13,1415 16,17,18,19,20,2 10,709 30,700	21 22 23124 25	26127,28 29 1 85	30 31,32 33 Q	34,35 -5 A 38?	38139 40 41 M-1+ M' L	BOG. Cfto 7+50 W ORANGE Feat? OBANGE Feat? below OBANCHI Black 'A!
2		12+150 1310+1010	o S	.45	PiBe -	615 4	MMM	Bo Hom of B'?
3		19,400 30,4,90	a s 🗔 🗌	0.55	Be	10 C?	MMM	Good sample at edge of bog.
4		1 1814150 319+101	0 2 [] []					Bog. Decempton weber 3 55024.
· 5	11.5	B1+10P ,319,+10.0	0200					Bog 11 and
6		171+15P 13101+190		050 ?	0	45 A B?	# # ?	BOG - Thin orange layer, below Black cloyey A' He igun
7		7+00 3,0+100		0.50 7	L BR	±15 B?C?	MMM	
8		6,+50 3,9+00		0 .40 7	L Pule BR	15 C?		Subcrop- Service schust 3 M- from OC
9		6+00 30+00	23 🗌 🗌	2:55 7	LBR	1015 e?	MMM	
10		5,+50 3,0+,04	0 8 7]40 7	L R.B.	15 B?	M M M	¢
-		<u></u>						
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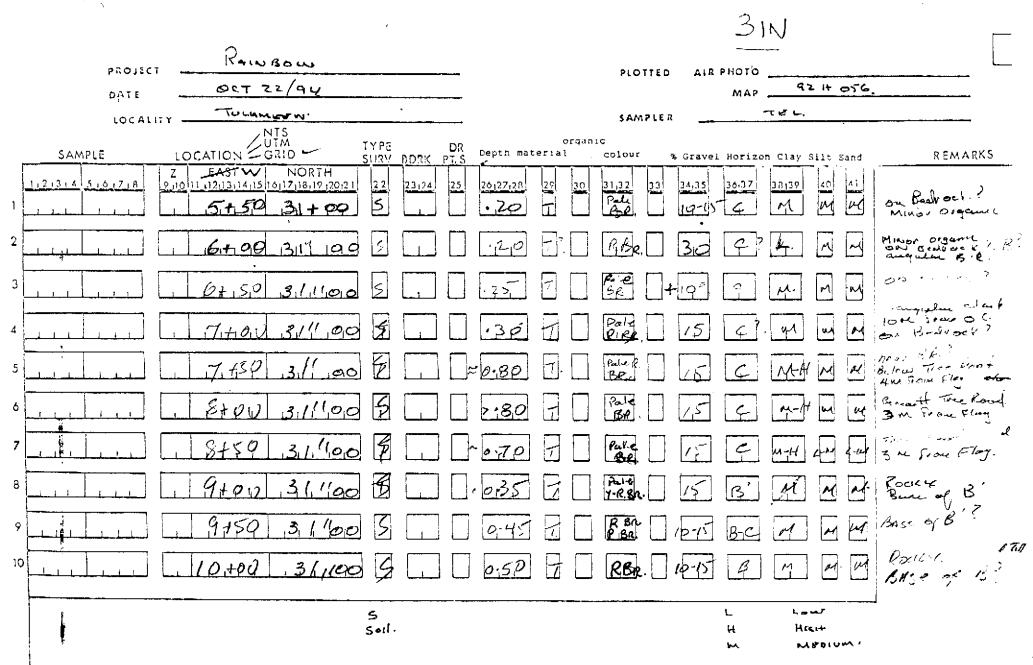
		_	,						3(N	[
	PROJECT	RAINBOW.	·····			PLOTTED	AIR PHOT				L
	DATE	OCT 22 (94					MA	·	14056		
	LOCALIT	TULAMEENI	·		organ	SAMPLER	<u> </u>	E. LISUE			
	SAMPLE	LOCATION - GRID -	TYPE DR SURY_DDRK_PT.S	Depth mat			% Gravel Ho	rizon Clay	Silt Sand	REMAR	<s< th=""></s<>
	121314 5 6 7 8	Z EAST NORTH NORTH 12/13/14/15/16/17/18/19/20/21	2 2 23.24 25	2612712B	29 30	31,32 33	34.35 36.37	38138	40 41		<u>.</u>
1		1 19400 31 400	\$?	0:40	7	B _l e.	153 B		~ ~5		
2		0+150 1311+1010	57.	01710	-	RB	152 B	M		RAHTWOER B	s in almost
3		1+00 311+0P	8	050		XA RIBE	15% C	M		минь, 'В'	. 1
4		11,+15,0 ,3,VA-100		0:65	90	RIBE	15 4	4	21	Den hargen 1	E 1, 58 -54
5		12,+10,0 ,3,1"+,00		0.67		YB .	152 CAB		a a	Tour of Car	af an e
6		121+1510 13 (+ 0P	3	0,25	70	Poste +	157- 9	4	a) 21	TALOS +5% Storf store	±5см Стані
7		13,+10,0,31/FOP	3	0:50	50	R.BR	15% C?	M		At when any any any any any any any any any an	
8		3+50 31+00	S Nº	0;20	50	ÅR.	152 C] In	11 14	ion actional	Nucla
9		41100 3400	3	0:45	30	Pale BR	10 A C	<u>M</u>		SN Firm OC	
10		4+50,31/+00 5+00W 31+00	5	0:50		1.15R.	10:15 C	? <u>m</u>		- ige in vision	
					·		1	<u>ل ب ب ا</u>			
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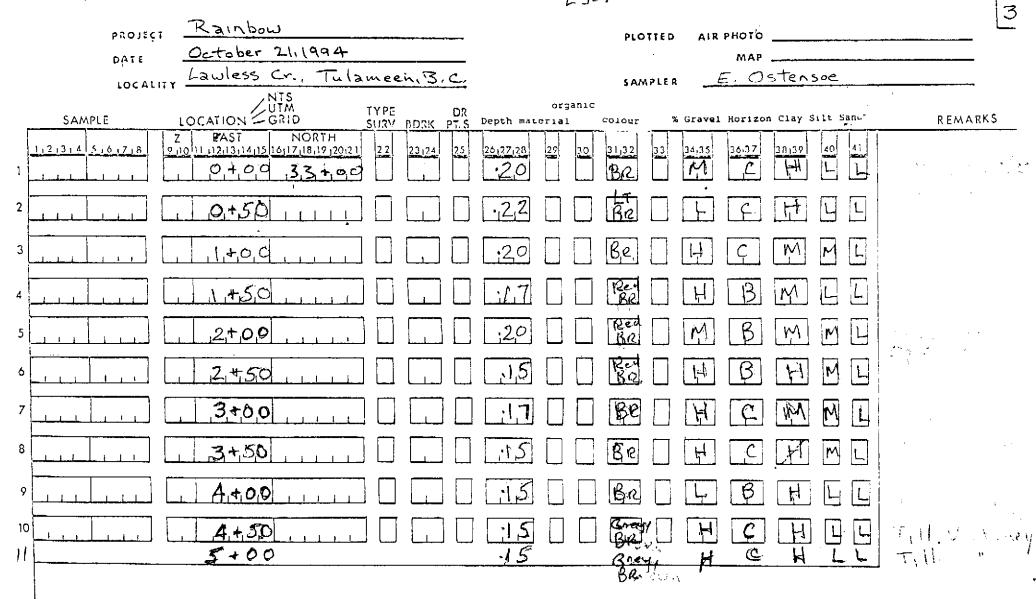
		<i>,</i>	
	PROJECT	RANKED	- PLOTTED AIR PHOTO
	DATE	<u> </u>	MAP
	LOCALITY	the second state of the second s	SAMPLER <u>E Ostensoe</u>
	SAMPLE	OCATION GRID SURM DOAK PT	organiv R Depth material Colour % Gravel Horizon Clay Silt Sand REMARKS
1	<u>1,2,3,4</u> 5,6,7,8	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
2			14.0 Bed 25 B H L Fair Spl. Much
3			1.60 D R. D TO C H M C Possible deep B-
4		1,1,+5,0	I I I I I I I I I I I I I I I I I I I
5		2,+,0,0	
6			25 BE 35 CM MM KANA
7		3,+,0,0	14.0 Mild 3.5 S M H H bass to Ker
8		3,+,5,0	16,5 MAR 35 C M F M back work with bir 35 C M F M more pale colored
9		4,+,0,0	40 G G G M M M Hall save frage
10		4 + 5,0	4.5 Br 35 C H M L barrer + cobbiles
		5+00	50 Redbr: 20 B/C L M M Drainage. Likely B. Denser practiced gravel augular fragments

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		L 32N	5
	PROJECT	RAINBOW PLOTTED AIR PHOTO	Ľ
	DATE	October 22, 1994	
	LOCALITY	Y Lawless Creek, Tulaincen.BC SAMPLER E. Ostensoe.	
-	SAMPLE L	NTS UIM TYPE DR Depth material colour: % Gravel Horizon Clay Silt Sand REMARI LOCATION - GRID SURV BDDK PT.S	RK S
- ۱	1,2,3,4 5,6,7,8 0,10		d +(1).
2		Lieutione IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	e 14 B
3		Librison III III III 20 III Realist	Are as
4		1,7,+,a0,,,,, IIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	ник страни.
5		I T, + 15,0	an a
6			t de la
7		13+50,	6 .
8		19, top III IIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	
9			·,
10		1.0,+0,0	Ι.

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				23	30			6
	PROJECT	RAINTOW			PLOTTED	AIR PHOTO		
	DATE	Oct. 22, 1994		· ·		MAP_		
	LOCALI	TY Lawless Creek, Tula	meen, B.C.		SAMPLER	<u>E</u> Dete		
	SAMPLE	LOCATION -GRID	TYPE DR SURY BORK PT.S	%Organic depth material	colaur	% Gravel Horiz	on Clay Silt Sa	nd REMARKS
1	1121314 5161718	Z NEAST NORTH 9,10011,12,13,14,15,16,17,18,12,20,21 1,0,4,0,0 ,3,3,40,0	⊐ {""! "" "\	26127128 29 30 15	31,32 33 Dige	34.35 36.37 Hit B	38139 40 41 M M L	V shallow soil over rock. Poor spi.
2				.40	BR [20 B/C	MHM	Good soil but not a good c horizon
3		<u> </u>		.30	Black.			BADE Som - edge of small wraw dark
4		1 2 m ()		.50	BR	10 C	HML	
5		1,2,+,0P] [50] []	Vellen BR	25 C	H M L	Fair bocky one
6		17,4,50] 35 🛛 🖓	Kellow BF	20 C	HHL	
7		μ, τ, f, θ, θ, μ,		25	BRUM	30 C	M H	Shallon Indi
8		6,+57] ·,Z,Ø	BiR,	30 C		
9		6,40,0		·60		75 C	MM	good spl. (TUL)
10		5,+,5,0] :15	Rβ.β₽	B ² C ³		Mon otp. Downslope from bodrock - 2M. (TEL)
				· -		· · · · · · · · · · · · · · · · · · ·		×

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	PROJECI		RAINB									PLO.	TTED	AIR	ркотю					-
	DATE		<u>017 21</u>												MAP		920	4 0	56	
	LOCALI	τ¥		2-4-N 115	Tout	me	870-					5 AM	PLER		7.	<u>e. 213</u>	s L C			
SAMI	PLE	The second se	ION ZO		T 5	7 PE 187	<u>ndak</u>	DR <u>P7</u>	Depth ma	org teria	anic 1	colour	,	6 Grave.	. Horizo	n Clay	silt	Sand		REMAR
<u>1,2,3,4</u>	5 <u>161718</u>	1000	AST WI 2131141151 2499	NORT 6;17;18;17 1 3:4 -4	H 12013 1		23174) 2,	25	26127128	29 7	30	31,32 D,BR	32	34.15 2.5	36.37 3	38139 H	40	41	c. 1 quan	iel și S
<u> </u>	- 1 4 - 1 -		<u>14 při</u>	13141	1010	5	7		- 10	F		Y-R Be	[] I	0-15	BAC	LJM	M		. I can't	Mary - I
			100	,3,4:'	00	5	7		.50	7		Phit RBR		10:15	BC?	L	Μ	Μ	وم م ² 2 2 2 روا م مارو	Paleer.
	· · · · · · · · · · · · · · · · · · ·		459	34	00				که،			P Be Y Be		10^	B+C	L.	M	M	Seal -	
			<u>+ PY </u>	3.4	00				.50	2		KBR LCGY.		10	Bt C	M	LT M	1- 14	1 1 1	? 1
	· · · · · · · · · · · · · · · · · · ·	[1 22	3.4		5			.50			RBR		10-15	<u>B</u> ?	M	M	2	kali a sul a	
				314.11	······				.45			YiBe	∐ ≁	10	C	M	M	M	TELC 25MC	Batter.
<u>+ + 1</u>	<u></u>	[1 2 2 4	3.4/1		R	.		<u>.50</u>			Y 82 R 80		15	B+C				- 190	
			1+15P	341	,	2			2.45	17 Fr		YBR		10				M	Tor of Noan	
			+ 00	34		s S			-50	<u>1</u>		BR	نيا	U.V. 5	B			₩1 ·	Bodere	

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			,				34N.)	[
	PROJECT	RAINBOW-				PLOTTED			
	DATE	TULAMEEN, BC		•				<u>92 H</u>	1056
	LOCALITY	ZNIS	· · · · · · · · · · · · · · · · · · ·	-		SAMPLER	1, 5	LISLE	
		OCATION - GRID - SI	YPE DA JRY DDRK PT.:	S Depth mater	organic ial	colour	% Gravel Hori	zon Clay Silt :	sand REMARKS
. 1	1121314 5161718 21 1121314 5161718 21 1121314 5161718		22 23174 <u>75</u> S 3	2 <u>0127128</u> 01• 50	29 <u>30</u> 7	31,32 2BA RIGR	34.35 36.37 107 C. ⁷ .		1 995W
2		191+1510 13141 1010	5 7	0,40	7	Riber 🗌	ε.γοβ β?		grading for Y-R. Brown
3		1911 PP 341 OP	5 4 [30	7	P.Be	10 1	·· ·· [34 Stor 0 B. R
4		18-1-1-2 34 00	G M C	.29	50	PiBe	10 8.2		it ous Bedrocit.
5		B1+1010 341 00		40.45	- I	R Be	10 Btc	M	Base of B'
6		171+150 341,00		125	77	X BR	10 (1)	m M	- on Bedrock 1.0 M
7		7+09 3411,00	3	+0.50	20	Br	15	M M	Bedrock
8		67 50 341.00		+ 0,50	20	RBE.	19-15 B+C		
9		6+00 34100	3	0.20		DBR Ribe	15 Btc	M- M-	4 CA BE Sample .
10		5+50 3400	\$ [] [0.45	7	YBa.	15 (+13	Al. M	Top of C
			. <u> </u>	<u> </u>				• • • • • • • • • • • • •]

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	PROJECT	RAINBO						PLO	TTED A	IR PHOTO				
	DATE	OCT 21	194							MAP		92H0	56	
	LOCALITY	TOLAN	MEENS: B.	<u>c.</u>				S AA	12 L E R		TEL	ISLE		
		LOCATION S	- S				% orga	niç					*	
-	SAMPLE			YPE <u>Nav be</u>	DR. <u>DRK <u>P</u>1.5_</u>	Depts mate	rial	' colour	%	Gravel Ho	izon Cl	ay Silt Sa	na	REMARKS
	<u>1,2,3,4,5,6,7,8</u> Z	545TW	NORTH 17,18,19,20,21	2 2 2 2 3	3124 2.5	26127128	27 30	31,32	33 34.3	5 36.37	38139	40 41		
1			35+109			.4.0		Barker			Ļ	MH	-, · , .	15 cm FRAGE.
2		14+1510	13157+1010	5		<u>،ح</u> ام	TL	RIBR,	[] [0]	s <u>B</u> ?	LM	MM	St M	● 公式1 ()
3		4,4,0,0	361+1010	5		.50		R.B.	5-1	a B?	<u> </u>	M m-1		
4		3450	13:51+100	2		1.45		P.B.		- <u>B</u> !	L_	M		
5		3,4,00	3.57.00			·5 O		R.B.		B?	<u> </u>	M		
6		RH510	13:57+100	5		.35		RBh		β?	LiM	MM	;	
7		12+00	3.5+00	5		.40	T	Rele Ble		B ² C ²	LiM	MM		
8		1+50	35+00	2		.50		BR.	#[[دع	LM	MM	₹54 ÷	
9		1.1.100	35+P,0			ە ك.	Ī	R Ba		0 B5	L-M	MM		
10		0+50	35,4,00 35+00			. 40 .50	<u>ר ו</u>	RBa YBe	<u>-</u>	5 B ² C	4 LM		2215-14 Decision 1200-1	 The second second

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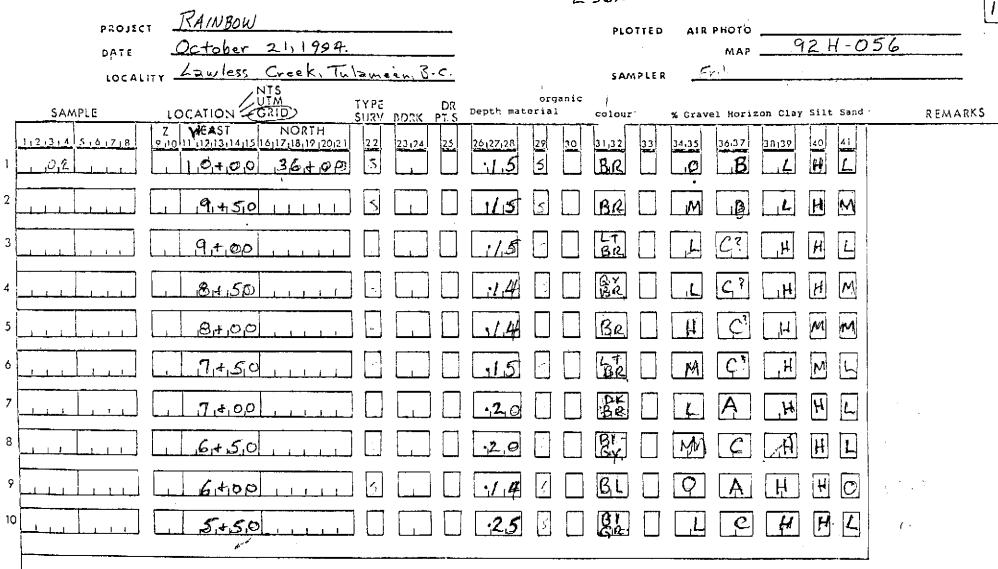
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	PROJEC DATE		· 21/94.	,				PLO	TTED	AIR PHO	ото ПарЯ	A OSE	÷	
	LOCAL			. <u>c</u> .				\$ AM	PLER		· < 1.56			
	SAMPLE	· · · / /		TYPE SURV_DDR		.Depth ma	%organ teria]	re Colour	9	6 Gravel H	orizon Clay	Silt San	d RF	MARKS
ך ו ו	1 2 3 4 5 6 7 8	Z EAST-W 9,1011,12,13,14,15 1,01+,00	NORTH 16117,18,19,20,21	22 231		26127,28 016,D	27 30 67?	31,32 RBA		34.35 36. 10% [40 41 M 4	1Frags 5-2	e sus -
2		9+50	13151+1010	3		0.50	a T.	R-Y BR:	<u>+</u>	10% B1	C M+H	u m	DIL Brown degs	'B' to 0-35*
3		19t,00	35,+0,0		2	0,30	7	R-Y BR	1	-15 B B+	c M	4 14		. 6 f
4		8750	35+00	5		0.60	7 .	R-Y Ba		10% 8+	C M	MM		
5		BTPQ	35+00	5		0:5,0	7	R.Y Be		10% B+	C M	M 4		o cut
6		1 4+50	35+00	2 [0:55		RB		5-8% B	2 41	~ ~	3% clasts 5% q1 - 001	Lo IDEM. La ISMI.
7		7+00	35+00	5		0.50	7.	RB		COYS BA	c M	N M	Guyolar k frays - 10	- Suf Kour 5.15 %
8		6+59	3570P	5		a-40		YBO		10-15%	- 4	M		
9		6700	35+00			0.35	z 🗌	YB		5-10%	2 4-41-	nd M		
10		5+50	35,+00	3		0.40	A7 🗌	BR.		5-10%		44 - A4	Hard Co Baral	Till-
										<u></u>	L LO M NO H HE	س ۵ ان علم جالم -		

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	PROJECT	RAINBOW		2
	DATE	OCTOBER 21, 1994	PLOTTED AIR PHOTO	<u> </u>
		Lawless Cr., Tulameen, BC	MAP	
	LOCALITY	NIS	SAMPLER <u>E. Ostensoe</u>	
r	SAMPLE L	OCATION - GRID TYPE DR	organic Depth material / colour % Gravel Horizon Clay Silt Sand REMAR	KS
1		$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
2				
3		4,4,0,0		
4		3+50	20 I II M B M H M	
5		3,+00	20 I I I M G M M L	
6		,2,+5,0	IS C M C M M C	
7		2+00		
8		1+50		
9		1,400,		
10 {{		0+00	20 BR. MCHML 20 BR. LCHLL	

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1	3	6	N



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							Tor	<u>a L</u>	<u>isl</u>	≥ <u>P</u>] 145	ROJE W. Ro	CT klan	R- Roa	L 1 d, No	?il€ rth V	2 # ancour	94- ver Bi	-419 : V7N) 3 2V8	Pa	ige	1								L	
AMPLE#	Мо ррпп	Cu ppm	Pb ppm		Ag ppm	Ni ppm			Fe X		U ppm						Bi ppm		Ca X		La ppm			Ba ppm		8 ppm	Al X	Na X	к Х	¥ ppm	Au* ppt
36N 10+00W 36N 9+50W E L36N 9+50W 36N 9+00W 36N 8+50W		44 32 30 - 29 - 42		53 50 58	~<.1 ~<.1 ~<.1 ~<.1 ~<.1	18 22 20 15 21	14 11 13	1047 1033 723	4.49 4.30 4.19 4.60 4.84	4 4 5 2 2	১ ১ ১ ১ ১ ১	<2 <2 <2 <2 <2 <2 <2 <2 <2 <2		26	.3 <.2 <.2 <.2 <.2 <.2		<2 2 4 <2 11	68 72	.31 .30 .40	.106 .071 .069 .062 .088		33 32 30	1.05 .95 .93 .97 1.16	148 141 229	.08	4 <2 Z	3.45	.02 .01 .02	.10 .10	<1 <1 <1 <1	2 1 1 1 3
36n 8+00w 36n 7+50w 36n 7+00w 36n 6+50w 36n 6+50w	5	57	6	66 109 76	<.1 - <.1 3 5	25 21 17 12 25	14 20 10	786 5266 2690	4.69 4.65 5.18 3.56 5.20	<2 <2 4 3	10 13		2 3	25 81	<.2 <.2 .4 .6 .9	<2 <2	<2 5 <2 6 4	75 66 59	.26 1.10 1.13	.069 .062 .152 .084 .075		34 30	1.20 1.06 .77 .87 .92	157 329 190	.08 .05	<2 < <2 < <2 :	2.88	.03 .02	.08 .08	<1 <1 <1 <1 <1	
36n 5+50w 36n 5+00w 36n 4+50w 36n 4+00w 36n 3+50w	2 1 <1 <1	28	× 8 5 7	93 150 114	.2 .3 ~.1 .2 .1	22 18 16 17 15	12 13 10	951 715 487	4.35 4.16 4.08 3.49 4.28	9 <2 <2 2 3	<5 <5 <5		<2 2 <2	24			<2 <2 <2 <2 <2	62 67 64	.97 .29 .36	.059 .067 .084 .043 .089	21 28 9 10 12	30 32 29	1.04 .94 .83 .73 .75	214 131	.06 .05 .09 .08 .08	5 <2 <2	4.27 2.95	.01 .02	.08 .07	<1 <1 <1 <1 <1	:
36N 3+00W 36N 2+50W 36N 2+00W 36N 1+50W 36N 1+50W 36N 1+00W	<1 1 1 <1 1		6 10 6 10 10	89 82 109	<.1 <.1 <.1 <.1	18 12 12 15 11	11 10 13	418 593 672	4.03 3.88 3.46 3.89 4.44	4 3 <2 6 10	<5 <5 <5	<2		25 29 23	<.2 <.2 <.2 <.2 <.2 <.2	Ŝĸĉĉ		61 57 59	.27 .33 .26	.051 .088 .043 .078 .080	13 8 11 10 13		.83 .69 .81 .72 1.10	114		<2 <2 <2	2.37	.02 .01	.06 .06 .06 .07 .09	<1 <1 <1 <1 <1	
36n 0+50w 36n 0+00w 34n 10+00w 34n 9+50w 34n 9+50w	<1 1 2 2 1	× 23	17 10	118 51 57	, 1 , 1 , 1 , 1 , 1 , 1 , 1 , 1 , 1 , 1	10 19 14	12 16 13	600 462 512	4.10 4.17 4.53 3.86 4.27	3 <2 2 <2 <2 <2 <2	<5 <5 <5	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	2 2 5 3 3	28 18 17	<.2 <.2 <.2 <.2 <.2	4 3 5 2 2 2	4 <2 <2 <2 9	63 66	.23 .13 .16	.092 .080 .054 .054 .054	11 11 14 11 10	26 32 26	.91 1.04 1.19 .68 1.04	83	.06 .06 .06 .10 .07	<2 <2 <2		.01 .01 .01	.09 .07 .09 .08 .09	<1 <1 <1 <1	2
34n 8+50w 34n 8+00w 34n 7+50w 34n 7+00w 34n 6+50w	1 7 1 1 3	53 38 58	/ 14 / 13 / 15 / 3 / 4	89 101 93	- <.1 1 - <.1 - <.1 - <.1	24 16 26	11 15 16	517 891 1010	4.27 3.91 4.39 4.98 4.10	7 4 2 4 2	<5 <5 <5	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	3 3 3 5	38 17	.7 <.2 <.2	4 5 2 6	< < < < < < < < < < < < < < < < < <> </td <td>62 71 74</td> <td>.47 .15 .16</td> <td>.075 .046 .112 .100 .049</td> <td>13 26 11 11 17</td> <td>37 33</td> <td>.83 .99 .94 1.43 .90</td> <td>100 111</td> <td>.08</td> <td><2 5 <2</td> <td></td> <td>.01</td> <td>.09 .09 .13</td> <td><1 <1 <1 <1 <1</td> <td></td>	62 71 74	.47 .15 .16	.075 .046 .112 .100 .049	13 26 11 11 17	37 33	.83 .99 .94 1.43 .90	100 111	.08	<2 5 <2		.01	.09 .09 .13	<1 <1 <1 <1 <1	
34N 6+00W 34N 5+50W 34N 5+00W 34N 4+50W 34N 4+50W	2 2 2 1	31 44 34	/ 9 / 7 / 11	109 118 95	<.1 <.1 < .1		10 14 13	708 755 685	3.89 4.21 3.94	5 5	<5 <5 <5	<2 <2	2 <2	51 54 38	.4 .4 .2	<2 <2 2		63 69 62	.58 .63 .49	.101 .045 .046 .056 .047		32 36 27		168 161 104	.08 .08 .06	<2 <2 <2	3.60 2.75 2.82 2.55 2.58	.01 .02 .01	.06 .08 .08	<1 <1	
STANDARD C/AU-S	19	ICP THIS ASS - S	5 5 LEA AY RE AMPLE	DO GR CH IS Comme Type	AM SA PART NDED : P1-		SDI WRMN NCKA	GESTE FE S ND CO 11-P1	D WITI R CA I RE SAI 2 ROCI	1 3ML 2 LA (1PLES	3-1-2 CR MG IF CU AU* A	HCL- BA TI PB Z	HNO3- BW NAS	H2O A AND L > 1%,	T 95 IMITE	DEG. D FOR	CFOR NAK	ONE AND AU >	HOUR AL. 1000									. 06	. 15	9	5

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Tom Lisle PROJECT R-1 FILE # 94-4193



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ACHE ANALYTICAL																															
SAMPLE#	Mo ppm	Çu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Min ppm	fe X	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppn	Şb ppm	Bi ppm	V PPM	Ca %	P X	La ppm	Cr ppn	Mg X	Ba ppm	ті Х	B ppm	AL X	Na X	K X	W ppm	Au* ppb
L34N 3+50W L34N 3+00W L34N 2+50W L34N 2+50W L34N 2+00W L34N 1+50W	1 1 2 1	35 - 39 - 25 -	 13 13 18 19 10 	142 148 132	~<.1 *<.1 *<.1	18 17 14 11 13	13 18 13	821 4 751 4 1053 5 615 3 613 4	4.03 5.03 5.46	5 <2 3 <2 2 <2	ও ও ও ও	~~~~~ ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	4 <2 <2 <2 3	28 36 27 41 20	.3 .6 .9 .4 .6	₹ ₹ ₹ ₹ ₹ ₹ ₹	2 3 2 2 2 2 2 2 2	67 64 83 59 61	.40 .30 .60	.087 .051 .111 .035 .075	15 15 11 15 14	32 30 23 21 23	.85 .84	149 142 155 205 123	.06 .08 .07 .05 .06	3 4 2	3.72 2.60 3.32 3.45 3.40	.02 .02 .03	-08 -07	1 <1 <1 <1 2	3 3 1 2
L34N 1+00W L34N 0+50W L34N 0+00W L32N 10+00W L32N 9+50W	1 <1 1 2	49 94 29		141 198 79	1 2 1	13 14 22 23 23	12 13 15	844 / 472 / 1196 / 930 / 820 /	4.28 4.97 4.30	3 3 3 2 2 2	ৎ ও ও ও ও	<2 <2 <2 <2 <2 <2 <2 <2 <2	3 2 3 2 3	29 32 49 38 40	.6 .3 1.0 .3 1.0	<2 4 2 2 2 2	~~~~ ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	62 69	.63 .46	.052 .072	16 18 42 14 19	23 31 37	.98 .89 1.08 1.33 1.09	161 234 101	.05 .05 .05 .09 .10	<2 7 3	3.37 3.06 4.71 2.65 2.86	.03 .03 .03	.12 .10 .16 .12 .11	1 <1 <1 <1 1	2 2 4 3 11
L32N 9+00W L32N 8+50W L32N 8+00W L32N 7+50W L32N 7+00W	2 3 2 5 2	41 - 17 - 34 - 46 - 40	-		1 .1 .2	15 9 16 24 21	11 15 15	874 522 5 819 938 815	5.35 4.51 4.85	3 2 4 2 5	ও ও ও ও ও	~~~~~~ ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	3 5 3 3 2	32 14 27 48 45	1.0 .4 .4 .3 .9	<2 3 2 2 2 2 2	<2 <2 <2 5 2	63 84 68 75 65	.11 .24 .58	.084 .219 .066 .031 .062	33 10 18 42 16	20 30 38	1.09 .82 1.08 1.12 1.01	76 113	.05 .05 .08 .06 .07	7 7 6	3.99 3.38 2.69 3.88 3.02	.03	.14 .08 .11 .11 .11	1 <1 <1 <1 <1	11 22 6 2 1
L32N 6+50W L32N 6+00W L32N 5+50W L32N 5+00W RE L32N 5+00W	3 2 1 5 5	55 39	10 16 15	75 121 176	<.1 <.1 < .1	23 23 16 24 23	24 11 31	818 559 979 2424 2390	6.23 4.73 6.11	2 6 2 9 6	<5 <5 <5 <5 <5	<2 <2 <2 <2 <2 <2 <2	<2 4 2 4 5	16	1.2 .9 1.0 1.3 1.1	<2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <	<2 <2 <2 5 <2	68 103 72 80 81	. 14 . 23 . 49	.050 .206 .170 .108 .107	20 11 9 42 42	24 28 35	1.16 1.12 .97 .94 .95	103	.08 .06 .06 .08 .08	6 3 <2	2.99 3.40 3.58 3.96 3.98	.02 .01 .02 .01 .01	.11 .07 .12 .09 .09	1 <1 <1 <1	2 2 1 3 3
L32N 4+50W L32N 4+00W L32N 3+50W L32N 3+00W L32N 3+00W	1 2 1 1	112 321 66	12 16 17 17 14 20	99 85 122	1 2 - <.1 1 3	21 22 20 20 15	24 19 21	680 1015 830 902 1101	4.78 4.43 4.74	7 6 2 10 7	৩ ৩ ৩ ৩ ৩ ৩ ৩	<2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <	3 4 3 2 3	26 21 31 21 20	1.0 .7 1.0 .5 .8	2 2 2 2 2 2 5	<2 <2 <2 <2 <2 <2 <2 <2 <2 <2	63 74 68 82 72	.20 .40 .22	.052 .088 .042 .068 .084	13 15 29 11 11	27 34		117 134 167 171 141	.07 .07 .07 .08 .07	4 3 3	2.44 3.82 3.09 3.95 3.60	.03 .02 .03 .01 .01	.09 .08 .10 .09 .09	<1 1 2 <1	2 2 1 3
L32N 2+00W L32N 1+50W L32N 1+00W L32N 0+50W L32N 0+00W	2 1 2 3 2	51 · 49 64	v 23	156 183 172	- . i - 1	16 14 15 18 19	17 13 12	618 796 841 1035 825	4.71 4.24 4.44	<2 5 3 6 3	<5 <5 <5 <5	<2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <	2 2 2 2 2	46	.5 7 1.0 1.2 .9	< 2 3 2 2 2 2 2 2	<2 10 <2 5 <2	73 65 62 62 59	.17 .51 .74	.059 .063 .072 .056 .053	10 14 27 35 22	23 25 24 25 26	.74 .98 .87 .90 .89	170 209 207 288 161	.11 .06 .06 .07 .07	3 3 <2	3.51 3.92 3.32 3.83 2.55	.01	.09 .13 .12 .12 .11	<1 <1 <1 <1 <1	4 2 3 4 3
L30N 10+00W L30N 9+50W L30N 9+00W L30N 7+50W STANDARD C/AU-S	6 1 1 1 19	30	_	89 84 6	- <.1 - <.1 1 - <.1 - <.1	5 15 18 4 72	1	490 331	3.62	≪2 9 8 5 43		<2 <2 <2 <2 <2 7	- 3	28	.4 .7 .6 <.2 19.3	6 <2 <2 9 13	<2 <2 <2 <2 18	8 71 65 13 60	.24 .29 .21	.056 .059 .041 .059 .095	10 11 19 56 40	29 7	1.05	46 1 3 9 139 89 185	.11 .08 .08 .10 .08	2 3 2	2.28 3.11 3.52 2.64 1.88	.05 .02 .02 .04 .06	.01 .08 .08 .02 .16	<1 <1 <1 <1 13	1 2 <1 48

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Tom Lisle PROJECT R-1 FILE # 94-4193



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ACHE ANALYTICAL																														CRE ANA	LYTICAL
SAMPLE#	Мо ррпя	Cu ppm		2n ppm	Ag ppm	Ni ppm	Со ррт	Mn ppm	Fe X	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca X	р Х	La ppm	Cr ppm	Mg X	Ba ppm	τi X	8 ppm	Al X	Na X	K X	V ppm	Au* ppb
L30N 7+00W L30N 6+50W L30N 6+00W L30N 5+50W L30N 5+50W	3 4 2 4 2		- 13 - 11 - 8	73 - 68 - 46-	1 - <.1 - <.1 - <.1	13 17 23 22 21	17 21 20	358 5 637 4 1082 4 889 4 850 4	4.94 4.67 4.89	7 <2 <2 <2 2 2	ও ও ও ও ও ও ও ও ও ও ও ও ও ও ও ও ও ও ও	< < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 < 2 <	8 5 3 2 4	16 28 23 25 27	.2 .7 <.2 .7 .7	10 2 7 7 7	3 5 4 2 2		.25		16 19 12 9 23	26 29	.88 .95 1.06 1.23 1.41	92 110 138 131 113	.05 .10 .06 .08	<2 <2 <2	3,92 3,50 3,18 3,58 3,92	.02 .02 .01 .01 .02	.07 .09 .09 .09 .09	ণ <1 <1 <1 <1	1 4 4 1 2
L30N 4+50W L30N 4+00W L30N 3+50W L30N 3+00W L30N 3+00W L30N 2+50W	1 1 1 1	71 - 67 81			1 -<.1 -<.1	21 22 17 21 21	18 20 27	1061 909 1107 1413 811	4.56 4.61 5.02	2 6 6 2 5	জ জ জ জ জ জ জ জ জ জ জ জ জ জ জ জ জ জ	<2 <2 <2 <2 <2 <2 <2	3 3 2 3 3	27 33 28 30 25	.8 .8 .5 .6	6 5 2 5 4	11 8 <2 <2 <2	72 69 66 80 66	.30 .29 .33	.096 .061 .081 .144 .087	15 13 15 12 14	27 25 26	1.57 1.36 1.24 1.38 .86	141 126 202 155 164	.05 .06 .06 .06 .09	<2 <2 2	3.26 3.10 3.39 3.77 3.35	.01 .01 .01 .01 .01	. 12 . 12 . 14 . 13 . 09	<1 <1 1 <1	1 1 2 4
L30N 2+00W L30N 1+50W L30N 1+00W L30N 0+50W L30N 0+00W	8 4 5 2 1	75 \ 62 53 \	4 31 15 12 12	135 ⁻ 99 -	.2 1	15 19 21 23 18	21 10 10	553 1117 1442 802 521	5.33 5.78 4.09	<2 6 <2 <2 3	9 <5 <5 <5	<2 <2 <2 <2 <2 <2	<2 <2 <2 <2 <2 <2	90 64 69 69 43	.2 1.2 .6 .8 .4	<2 <2 <2 <2 7	5 7 3 2 4	72 50	2.60 1.32 1.39 1.43 .67	.099 .063	12 21 19 24 18	13 27 21 24 25	1.02 .90 .62 .82 .88	106 204 177 212 169	.02 .05 .05 .06 .08	<2 : 4 : <2 :	1.77 3.91 2.51 3.29 2.90	.02 .03 .02	.07 .07 .06 .08 .08	<1 <1 <1 <1 <1	2 14 12 3 2
L28N 10+00W RE L28N 10+00W L28N 9+50W L28N 9+00W L28N 8+50W	4	27 27 25 26 20	10 10 10 9	105 104 55	.1 .1 <.1 <.1 <.1	19 21 20 20 15	13 15 18	470	4.19 4.30 5.11	<2 <2 <2 4 9	<5 <5 7 <5 <5	<2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <	2 3 4 5	33 33 26 31 18	.3 .6 .2 .2	6 4 <2 3 3	6 3 4 ~2 ~2	68 68 69 64 66	.45 .25 .36	.087 .089 .093 .077 .116	11 11 16 36 14	24	.91 .91 .72 .97 .74	169 165 107 161 104	.09 .09 .10 .07 .07	3 5 3	3.37 3.26	<.01 .02 .01 <.01 .01	.08 .08 .07 .08 .07	<1 <1 <1 <1	2 1 3 4 6
L28N 8+00W L28N 7+50W L28N 7+00W L28N 6+50W L28N 6+00W	4 5 3 2	47	8 12	56		18 15 19 14 20	14 19 20	652 305 822 576 491	4.79 5.18 4.98	2 4 2 2 5	৩ ৩ ৩ ৩ ৩ ৩ ৩	< < < < < < < < < < < < < < < <> </td <td>5 8 5 6 6</td> <td>23 18 25 18 26</td> <td>.6 <.2 <.2 <.2</td> <td><2 <2 3 <2 7</td> <td><2 5 8 5 8</td> <td>65 68 78 66 72</td> <td>.18 .23 .14</td> <td>.085 .098 .158 .184 .091</td> <td>41 78 15 16 19</td> <td>22</td> <td>.90 .81 1.20 .89 1.14</td> <td>111 65 86 54 89</td> <td>.08 .08 .05 .08 .06</td> <td><2 4 <2</td> <td>3.31</td> <td>.02 .01 <.01 .01 .01</td> <td>.09 .05 .08 .07 .08</td> <td>1 <1 <1 <1 <1</td> <td>3 6 1 6 2</td>	5 8 5 6 6	23 18 25 18 26	.6 <.2 <.2 <.2	<2 <2 3 <2 7	<2 5 8 5 8	65 68 78 66 72	.18 .23 .14	.085 .098 .158 .184 .091	41 78 15 16 19	22	.90 .81 1.20 .89 1.14	111 65 86 54 89	.08 .08 .05 .08 .06	<2 4 <2	3.31	.02 .01 <.01 .01 .01	.09 .05 .08 .07 .08	1 <1 <1 <1 <1	3 6 1 6 2
L28N 5+50W L28N 5+00W L28N 4+50W L28N 4+00W L28N 3+50W	2 1 2 4 2	84 60	- 14	49 82 81	<.1 <.1 <.1 .2	28 49 36 25 16	24 23 17	771 824 1161 950 648	5.40 4.73 4.38	<2 <2 <2 3 <2	ও ও ও ও ও ও ও ও ও ও ও ও ও ও ও ও ও ও	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	2 5 3 2 2	53	.3 .2	4 ~2 ~2 ~2 ~2	4 3 <2 11 4	75 93 82 67 64	.26 .18 .65	.059 .108 .114 .047 .101	18 14 13 24 17	68 3 36 26	1.38 3.00 1.24 1.27 .89	156 109 115 116 118	.07 .04 .10 .07 .07	<2 <2 <2		.01 <.01 .01 .02 .01	.09 .09 .07 .09 .10	<1 <1 <1 <1 <1	1 1 2 2 2
L28N 3+00W L28N 2+50W L28N 2+00W L28N 1+50W L28N 1+50W	1 2 3 2	84 65	√ 13 < 13	101- 92. 102	. <.1	20 17 16 18 17	21 20 12	610 839 925 920 743	4.93 5.08 3.98	7 8 2 2 4	<5 <5 <5 <5	<2 <2 <2 <2 <2 <2 <2	2 5 2 2 2	32 46 55 85 46	<.2 .2 .3 .7 <.2	< < < < < < < < < < < < < < < < < <> </td <td><2 10 10 8 9</td> <td>67 77 68 60 59</td> <td>.55 .86</td> <td>.062 .073 .072 .040 .037</td> <td>16 25 20 18 20</td> <td>28 25 24</td> <td>1.20 1.06 1.02 .75 .90</td> <td>87 90 97 131 116</td> <td>.06 .06 .05 .06 .05</td> <td>2 <2 <2</td> <td>2.85 2.94 2.87 3.04 2.56</td> <td>.01 .02 .01 .01 <.01</td> <td>.09 .08 .07 .07 .07</td> <td><1 <1 <1 <1 <1</td> <td>5 7 47 2 4</td>	<2 10 10 8 9	67 77 68 60 59	.55 .86	.062 .073 .072 .040 .037	16 25 20 18 20	28 25 24	1.20 1.06 1.02 .75 .90	87 90 97 131 116	.06 .06 .05 .06 .05	2 <2 <2	2.85 2.94 2.87 3.04 2.56	.01 .02 .01 .01 <.01	.09 .08 .07 .07 .07	<1 <1 <1 <1 <1	5 7 47 2 4
STANDARD C/AU-S	20	56	43	134	6.9	74	33	1048	3.96	39	22	6	38	52	19.1	13	22	60	.52	.094	40	61	.93	190	.08	34	1.88	.06	<u>. 16</u>	10	49

44

Tom Lisle PROJECT R-1 FILE # 94-4193



ppm p L28N 0+50W 1 L28N 0+00W <1 L26N 10+00W 2 L26N 9+50W 1 L26N 9+50W 3 L26N 9+00W 3 L26N 8+50W <1 L26N 8+00W <1	Cu ppm p 55 - 38 - 43 - 22 - 13 - 31 - 28 - 27 -	14 12 8 13 5 10 9 7	n Ag m ppm 33 03 02 82 9 - <.1	ррт 16 22	10 12 11	1018 4 819 3	. 19	7	U ppmr <5	Au ppm <2		Sr ppm	Cd PPM	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg X	8а ррл	Ti X	B ppm	Al X	Na X	К %	¥ ppm	Au* ppb
L28N 0+00W <1 L26N 10+00W 2 L26N 9+50W 1 L26N 9+00W 3 L26N 8+50W <1 L26N 8+50W <1	38- 43-7 22-7 13-7 31-7 28-	8 13 5 10 9 7 6 5	03 02 82	22 12 8	12 11	819 3		7	<5		_																		
L28N 0+00W <1 L26N 10+00W 2 L26N 9+50W 1 L26N 9+00W 3 L26N 8+50W <1 L26N 8+50W <1	38- 43-7 22-7 13-7 31-7 28-	8 13 5 10 9 7 6 5	03 02 82	22 12 8	12 11	819 3		•			2	80	.5	<2	3	51 1	.25	077	14	26	.73	141	.07	<2 ·	3.17	.03	.08	<1	<1
L26N 10+00W 2 L26N 9+50W 1 × L26N 9+00W 3 × L26N 8+50W <1 L26N 8+50W <1	43 × 22 × 13 × 31 × 28 ×	5 10 9 7 6 5	0~ .2 82	12 8	11			3	<5	<2	3	45	.4	6	<2		.56		16	33		165	.06		2.65		.10	<1	
.26N 9+50W 1 ≤ .26N 9+00W 3 ≤ .26N 8+50W <1 .26N 8+00W <1	 22 ✓ 13 ✓ 31 ✓ 28 ✓ 	97 65	82	8		761 4		5	<5	<2	ž	31	<.2	<2	2		.54		40	25		244	.07		3.10	.02	.09	<1	4- 3-
26N 9+00W 3 x 26N 8+50W <1 26N 8+00W <1	13 < 31 √ 28 ↓	65		-	15	476 3		ŝ	<5	<2	4	24	<.2	2	<2		.34		17	21		200	.05		2.50		.08	<1	2
L26N 8+00W <1	28 🗸	67		J.		854 4		4	<5	<2	3	37	<.2	<2	<2		.35	•	11	11		438	.02		2.55		.11	<1	1
.26N 8+00W <1	28 🗸		5 - <.1	14	17	560 4	. 19	<2	<5	<2	5	25	<.2	<2	4	58	.22	082	15	23	1.11	116	.06	<2	2.82	.01	.09	<1	2
-		5 4	7~ .2	12		650 3		5	<5	<2	4	27	<.2	2	<ż		.29		11		1.19	95	.05		2.23		.07	<1	1
			7 ~ < 1	21		580 4		ź	<5	<2	3	20	<.2	<2	<2		.20		11		1.05	94	.04				.08	<1	<1
	17/		3 - < 1	13		406 3		6	<5	<2	3	22	<.2	<2	3		.21		25		.84	82	.05		2.28		.05	<1	1
	30		72			778 4		<2	<5	<2	2	26	<.2	<2	<2		.27		11			107	.05		3.08	.01	.09	<1	ż
26N 6+00W <1	47 × 1	17 0	7 ~ .1	15	20	1021 4	77	7	<5	<2	3	28	.4	<2	<2	70	.27	173	11	26	1.13	150	.06	2	3.35	.02	.11	<1	4
1		14 14		33		856 4		3	<\$	<2	5	60	<.2	<2	5	62	.80		37			129	.09		3.93	.02	.08	<1	6
			82	19		742 4		5	<5	<2	2	23	.4	2	<2		.23		13		1.00		.05		2.82		.08	<1	2
	41 \	6 17				2292 4		<2	<5	<2	3	26	.5	<2	<2		.29		13		•								3
			4-<.1			1122 4			<5	<2	2	26										157	.07		3.28		.09	<1	
	207	(9	4 ~ 4.1	13	21	1122 4	.14	2	<>	<2	2	20	<.2	<2	2	70	.27	.095	16	25	1.12	105	.06	<2 .	3.50	.01	.09	<1	2
	55 /		41	21	-	858 5		<2	<5	<2	3	26	.3	<2	<2		.24		14		1.32	90	.05		3.51	.02	.09	<1	2
	84 🗸		9 - 1	21		1110 4		<2	<5	<2	<2	27	.5	<2	2		.25		13			104	.06		3.21	.01	.08	<1	2
	87			19		1129 4		<2	<5	<2	3	26	.5	<2	<2		. 25		13			110	,06		3.27	.01	.08	<1	5
	72 - ′		5 .4	23		1011 4		4	<5	<2	4	22	.7	<2	<2		.20		16			107	.07	4	3.32	.02	.10	<1	5
6N 2+00W . 2	75 _K	10 10	04	14	18	688 4	.71	<2	<5	<2	4	28	<.2	3	<2	76	.27	.069	17	23	1.07	123	.08	<2	2.83	.01	.06	<1	3
26N 1+50W 1	36 🗸	98	43	19		687 4		3	<5	<2	3	44	.4	z	<2	60	.56	.047	18	29	.89	141	.07	<2	2.38	.01	.07	<1	3
6N 1+00W 1	49 V	13 8	41	14	9	946 3	.91	<2	<5	<2	2	54	.2	-2	<2		. 92		17	27	.75	121	.07		2.54	.03	.05	<1	2
:6N 0+50W 1	55 🗸	8 9	4 2	17		1302 3		<2	<5	<2	3	60	.3	<2	<2		.77		19			149	.06		2.21	.03	.08	<1	
6N 0+00W 2	79 ¥	12 12	4~ .4	29	11	852 4	.77	<2	<5	<2	2	68	1.1	<2	<2	61 1			30	34		210	.04		3.68		.10	<	
4N 10+00W 1	33 🗸	12 8	01	15	14	442 4	.09	<2	<5	<2	3	26	.4	<2	<2	57			19	23		113	.06		2.58		.08	<1	24
4N 9+50W 1	40 -	47	9~ <.1	13	13	471 4	.04	<2	<5	<2	3	29	.6	<2	<2	60	.28	051	16	74	1.11	100	.05	-2	2.47	.01	.06	<1	ź
	29 🗸		1.3	17		636 3		<2	<5	<2	4	25	.3	<2	5	56	.27		12		1.02	83	.05		2.26		.09	<1	2
			3~ .2			716 4		<2	<5	<2	<2	27	.4	<2	7		.29		13			119	.05		2.73		.11	<1	
	50 2		01	16		656 4		<2	<5	<2	3	26	.8	~2	<2		.25		14				.05		3.49				3
	58		3			749 3		4	<5	<2	2	28	.0	ž	<2		.25		16								.11	<1	
	20,	7 0	J~ .C	10	10	147 3	.07	4	• • •	~2	2	20	- 2	2	×2	22	.51	.020	10	20	.81	90	.05	<2	1.79	.01	.10	<1	17
	41 🗸		2 - <.1	17		640 4		<2	<5	<2	3	34	.3	2	<2	62	.39		19		1.09	96	. 05		2.12		.10	<1	9
	- 36 🏹		1~.1	14		1026 4		<2	<5	<2	4	24	.2	<2	<2		.22		19	20		142	.06	<2	2.85	.01	.11	<1	9
	32 🗸		11	14		750 4		<2	<5	<2	7	27	.6	4	<2		.20		21	19	.81	151	.05	<2	3,11	.01	.10	<1	
	33 🗸	27	2 <.1	16	21	955 4	.73	<2	<5	<2	8	35	.5	<2	5	65	.33	.087	40	18	.84	96	.06	<z (<="" td=""><td>2.66</td><td>.02</td><td>.07</td><td><1</td><td>1:</td></z>	2.66	.02	.07	<1	1:
24N 5+00W <1	43 ¥	12 9	21	14	15	754 4	.34	<2	<5	<2	<2	29	1.0	<2	<2	63	.30	.084	14	21	1.27	86	.05		2.57		.11	<1	6
ANDARD C/AU-S 19	58	38 12	4 6.7	70	31	1048 3	.96	40	14	6	36	51	18.9	14	22	63	.51	.093	40	60	.92	186	.08	7.9	1 88	.06	16	9	49

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Tom Lisle PROJECT R-1 FILE # 94-4193



i i i i i i i i i i i i i i i i i i i																													NCHE ANA	1111046
SAMPLE#	Mo ppm		Pb ppm		Ag ppr		Co ppm			As ppm		Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P X	La ppm	Cr Mg ppm X	Ba ppm	ті Х	B ppm	AL X	Na X	K X		Au* ppb
L24N 4+50W L24N 4+00W L24N 3+50W L24N 3+00W RE L24N 3+00W	2 2 1 <1	69 48 44	✓ 14 v 10 ✓ 16 ✓ 15 v 15	96 97 136		24 20 25	27 25 17	898	5.08 4.63 4.10	9 9 3 5 11	ৎ ৎ ৩ ৩ ৩ ৩	< < < < < < < < < < < < < < < < <> </td <td>7 5 4 4 4</td> <td>30 29 24 25 25</td> <td>.6 <.2 <.2 .5 .2</td> <td><2 4 <2 <2 4</td> <td><2 4 2 3 <2</td> <td>77 66 66 58 60</td> <td>.23 .1 .26 .1 .20 .0 .23 .0 .24 .0</td> <td>05)95)85</td> <td>16 21 16 13 14</td> <td>19 1.16 23 1.05 23 1.08 23 .96 23 1.00</td> <td>87 134 148</td> <td>.05 .06 .08 .06 .06</td> <td><2 <2 <2</td> <td>2.84 3.00 3.11 2.92 3.01</td> <td>.02 <.01 .01</td> <td>.10 .09 .09 .10 .10</td> <td>া <া <া <া</td> <td>23 3 11 3</td>	7 5 4 4 4	30 29 24 25 25	.6 <.2 <.2 .5 .2	<2 4 <2 <2 4	<2 4 2 3 <2	77 66 66 58 60	.23 .1 .26 .1 .20 .0 .23 .0 .24 .0	05)95)85	16 21 16 13 14	19 1.16 23 1.05 23 1.08 23 .96 23 1.00	87 134 148	.05 .06 .08 .06 .06	<2 <2 <2	2.84 3.00 3.11 2.92 3.01	.02 <.01 .01	.10 .09 .09 .10 .10	া <া <া <া	23 3 11 3
L24N 2+50W L24N 2+00W L24N 1+50W L24N 1+50W L24N 1+00W L24N 0+50W	1 1 1 <1	65 47 41 33	√ 15 √ 20 √ 17	134 165 132 80		2 17 1 15 3 12	14 15 12	628 687	4.58 4.08 4.15 3.70 3.76	5 5 10 8 5	ৎ ৎ ৎ ও	∾ ∾ ∾ ∾ ∾	4 2 3 4 2	47 30 23 62 29	.2 .6 .2 .6 <.2	3 4 3 5 3	10 7 <2 2 3	66 66 64 64	.51 .0 .33 .0 .22 .0 .49 .0 .27 .0	097 068 023	17 15 12 17 14	33 1.17 26 .86 25 .76 27 1.03 26 .76	155 148 148	.06 .06 .10	<2 <2 <2	3.39 3.01 3.06 2.35 3.25	.01 .01	.09 .09 .08 .09 .07	ব ব ব ব ব	
L24N 0+00W L22N 10+00W L22N 9+50W L22N 9+00W L22N 9+00W L22N 8+50W	1 1 1 1	41 81 49		9 12 21		1 22 1 19 1 18	14 20 17	511 633 11 78 1557 900	4.02 5.32 4.40	10 7 13 6 7	ৎ ১ ২ ১ ১ ১	<2 <2 <2 <2 <2 <2 <2	3 3 6 2 4	36 38 48 28 33	.6 .5 .4 .9	7 <2 3 <2 3	4 8 2 5 4	60 60 67 67 64	.41 .0 .40 .0 .61 . .27 . .30 .0	049 103 118	12 22 28 18 27	23 .77 24 1.04 28 1.29 30 .91 27 .88	96 151 163	.06 .05 .06	<2 <2 <2	2.66 2.22 2.27 3.73 3.14	.01 .01 .01	.08 .07 .11 .14 .11	<1 <1 <1 <1 <1	2
L22N 8+00W L22N 7+50W L22N 7+00W L22N 6+50W L22N 6+50W	1 1 1 1	30 57 42	16 17 12 17 12 14 14 17 9	6 8 11	1 9 ~ < 8 - < 0 - 9 - <	1 10 1 23 2 10	5 14 2 18 3 17	s 637 7 540	4.11 3.92 4.94 3.97 3.95	6 6	<5	<2 <2 <2 <2 <2 <2 <2 <2 <2	4 2 4 3 2	41 26	.2 2.> 2.	5 <2 4 5 3	9 ~2 ~2 ~2 ~2 ~2 ~2	59 60 65 57 55	.38 .0 .38 .1 .41 .1 .24 .1 .34 .1	059 094 089	15 20 23 15 24	26 1.2 24 1.0 23 1.3 19 .9 18 .9	i 84 9 96 2 111	.05 .06 .06	<2 <2 <2	2.08	<.01 .02	.08 .09 .08 .08 .07	<1 <1 <1 <1 <1	
L22N 5+50W L22N 5+00W L22N 4+50W L22N 4+00W L22N 3+50W	2 7 2 1 1	31 44 58	i√ 11 √ 15 √ 12 √ 11 ↓ 16	26	8 - <. 7 - <. 9 - <. 2	1 1 1 1 1 2	3 10 2 20 2 2	5 326) 511 7 554	3.94 9.90 5.46 5.26 4.49	<2 5 <2	<5 <5 <5	< < < < < < < < < < < < < < < <> </td <td>4 5 5 4 5</td> <td>150 63 42</td> <td>.6 <.2 .5</td> <td>2 <2 6 9 7</td> <td><2 <2 3 5 <2</td> <td>144 83 88</td> <td>.37 . .29 . .31 . .41 . .28 .</td> <td>275 123 131</td> <td>22 25 20 22 13</td> <td>16 1.0 13 1.4 20 1.1 18 1.0 23 1.0</td> <td>5 208 8 157 5 228</td> <td>.10</td> <td><2 <2 3</td> <td>1.75 2.72 2.95 3.03 3.07</td> <td>.05 .02 .02</td> <td>.11 .11 .10</td> <td></td> <td></td>	4 5 5 4 5	150 63 42	.6 <.2 .5	2 <2 6 9 7	<2 <2 3 5 <2	144 83 88	.37 . .29 . .31 . .41 . .28 .	275 123 131	22 25 20 22 13	16 1.0 13 1.4 20 1.1 18 1.0 23 1.0	5 208 8 157 5 228	.10	<2 <2 3	1.75 2.72 2.95 3.03 3.07	.05 .02 .02	.11 .11 .10		
L22N 3+00W L22N 2+50W L22N 2+00W L22N 1+50W L22N 1+00W	1 1 8 3 1	62 460 44	2 × 17 2 × 17 5 × 12 5 × 14	7 11 2 7 5 6	3 ~ . 0 ~ < . 9 ~ . 9 ~ .	1 2 2 1 1 7	1 1 B 3 7 2	8 813 4 577 6 660	4.15 4.33 7 8.02 5.47 9 4.08	7 8 	<5 <5 <5	<2 <2	4 7 3	29 21 45	.4 <.2 <.2	2 <2 <2 3 5	3 3 2	73 86 87	.29 . .14 . .44 .	140 332 056	14 19 18 29 11	25 .9 22 .8 16 .9 75 1.5 32 1.2	4 81 8 137	.12 .12 .07	<2 <2 <2		. 02	.06 .06	<1 <1	
L22N 0+50W L22N 0+00W L20N 10+00W L20N 9+50W L20N 9+00W	211111111111111111111111111111111111111	6 4: 4	2 √ 2 1 √ 1 2 ← 1 0 √ 1 0 √ 1	8 12 7 1 9		.1 2 .1 1 .1 1	0 1 6 1 6 1	4 84 4 82 3 79	4 4.31 6 4.26 3 4.00 9 3.70 8 3.87) 7) 3) <2	<5 <5 <5 <5	<2 <2 <2	4 3 3	27 30 40) <.2) .3	5 <2 8 5 3	3 9 7	60 60 64	.30 .40	.054 .080 .057	27 18 20 26 15	25 .9 25 1.1 25 .9 27 .8 22 .9	Z 100 1 140 5 104) .05) .07 , 08	<2 <2 <2	2.43 2.35 2.73 2.14 2.10	.01 .02	.09 .10 .08	1	1 1 1
STANDARD C/AU-S	19	5	93	7 1	32 6	.9 7	2 3	1 104	2 3.9	5 39	2 15	; 7	37	<u> </u>	2 19.3	15	15	60	.51	.095	40	63 .9	2 184	02	3 34	1.88	. 06	.16	12	2

ACHE ANALYTICAL

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Tom Lisle PROJECT R-1 FILE # 94-4193

Page 6

CHE ANALITICAL

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ACHE ANALYTICAL	Mo	Cu ppm			-	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	8i ppm	V ppm	Ca X	P X	La ppm	Cr ppm	Mg X	Ba ppnt	Ti X	8 ppn	Al X	Na X	K X	¥ ppm	Au* ppb
L20N 8+50W L20N 8+00W L20N 7+50W L20N 7+00W L20N 6+50W	1 1 2 5	40 43 43	 15 10 10 11 5 	76 67 70	1 1 1 1 1	7 11 11 12 21	16 14 10	770 506 458 621 157	4.07 4.04 2.97	<2 ~2 ~2 ~3 ~2 ~2 ~2 ~2 ~2 ~2 ~2 ~2 ~2 ~2 ~2 ~2 ~2	ও ও ও ও ও	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	5 5 4 3 2	18 20 15 34 55	<.2 <.2 <.2 .3 <.2	<2 <2 <2 3 3	<2 3 <2 5 <2	54 49 49 42 46	.21 .18 .43	.102 .063 .076 .029 .069	12 13 8 37 77	19 19 17 21 13	.67 .71 .66 .81 .52	94 120 93 128 85	.07 .06 .05 .04 .01	<2 4 <2	2.32 1.68 1.87 1.90 2.25	<.01 <.01 .01	-07 -05 -05 -07 -06	<1 <1 <1 <1	2 3 3 3 2
120N 6+00W L20N 5+50W L20N 5+00W L20N 5+00W L20N 4+50W L20N 4+00W	1 3 1 <1 5	30 29 35 36 ~ 24	5 16 8	60 132 98	-<.1 -<.1 -<.1 -<.1	13 6 23 10 12	24 23 14		4.59	<2 <2 <2 3 <2		<2 <2 <2 <2 <2 <2	2 14 4 3	24 25 21 30 36	<.2 .4 .4 .4 .2	<2 <2 2 4 3	~ 4 ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	53 42 56 58 56	,37 ,24 ,32	.167 .128 .094 .074 .082	11 92 29 14 10	17		78 56 79 81 87	.06 .02 .07 .08 .06	<2 <2 <2	2.02 1.94 2.37 1.78 2.10	<.01 .01 <.01	.05 .07 .08 .07 .11	ব ব ব ব ব	2 6 2 2 <1
L20N 3+50W L20N 3+00W L20N 2+50W L20N 2+50W L20N 2+00W L20N 1+50W	3 <1 1 20	°23 35 35		107 120	<.1 '1 '1 '- <.1	15 17 8 8 12	14 16 10	1293 435	4.81 3.57 3.97 8.03 3.95	< < < < < < < < < < < < < < < < < < <		<2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <	4 2 3 4 2	20 37	.7 .2 .3 .4	<2	< < < < < < < < < < < < < < <> <> <> <><> </td <td>55 60 59</td> <td>.38 .23 .19</td> <td>.117 .102 .116 .098 .062</td> <td>14 7 12 10 12</td> <td>20 23 24 24 23</td> <td>1.03 .90 .74 .86 .92</td> <td>116 99 139 137 103</td> <td>.05 .05 .07 .04 .05</td> <td><2 2 <2</td> <td>2.71 2.35 2.80 2.10 2.23</td> <td>.01 .01</td> <td>.08 .09 .09 .09</td> <td><1 1 <1 <1 <1</td> <td>1 1 3 1 3</td>	55 60 59	.38 .23 .19	.117 .102 .116 .098 .062	14 7 12 10 12	20 23 24 24 23	1.03 .90 .74 .86 .92	116 99 139 137 103	.05 .05 .07 .04 .05	<2 2 <2	2.71 2.35 2.80 2.10 2.23	.01 .01	.08 .09 .09 .09	<1 1 <1 <1 <1	1 1 3 1 3
L20N 1+00W RE L20N 1+00W L20N 0+50W L20N 0+00W L18N 10+00W	1 1 <1	37 52 43	7 11 2 m 13		, - < 1 - < 1 - < 1 - < 1 - < 1	13 12 13	12 12 14	680 952 711	3.59 3.66 3.98 4.02 3.63	2 2 5	<5 <5 <5	<2 <2 <2 <2 <2 <2 <2	2 3 3	21 15 15	.7 1.0 .6 .4	<2 <2 2	~ ~ ~ ~ ~ ~ ~ ~	55 61 62	.30 .20 .14	.042 .043 .072 .064 .060	13 13 12 14 19	22 24 24 23 20	.88 .89 .82 .81 .78	114 119 120 122 128	.05 .05 .06 .06 .06	<2 <2 2	3.44		.07 .07 .08 .07 .07	<1 <1 <1 <1 <1	2 17 1 <u>3</u> 5
L18N 9+50W L18N 9+00W L18N 8+50W L18N 8+50W L18N 8+00W L18N 7+50W	1	34 43	5 e 4 e	7 10		20 15 15	13 14 14	514 658 1019	4.27 3.40 3.98 3.63 3.42	√2 2 2	<5 <5 <5	<2 <2 <2 <2 <2	2 4 2	31 22 27	.5	3 <2 <2	5 <2	52 58 54	.34 .20 .28	.089 .082 .095 .085 .083	13 15 10	20 20 22 18 17	.74 .76 .71 .84 .70	114 90 112 110 103	.05 .07 .05	<2 <2 3		.01 .01 01	. 08 . 08 . 09	1 <1 <1	2 1 1
L18N 7+00W L18N 6+50W L18N 6+00W L18N 5+50W L18N 5+50W		3 3 4 3	2 1 3 1 1 1 5 1	8 10 1 11 5 11 8 11	2 - 1 2 - 1 1 1 5 1 5 1	1 18 1 13 1 16	3 14 2 17 5 16	630 530 734	3.76 3.83 4.24 4.06 4.22	<2 4 7	<5 <5 <5	<2 <2 <2	3	19 25 23	.2 .7 .6	2 <2 2	<2 <2 4	54 56 55	.18 .25 .21	.108 .103 .108 .106 .106 .058	9 16 10		.68 .63 .75 .75 .99	108 101 103 88 120	.07 .07 .06	<2 <2 2	2 2.41 2 2.24 2 2.24 2 2.24 2 1.95 2 2.22	.01 .02 5 .01	.06 .06 .07	<1 <1 <1	16 14
L18N 4+50W L18N 4+00W L18N 3+50W L18N 3+50W L18N 2+50W	ĺ	1 3 1 5 1 4 1 6		8 7 3 12 0 10 1 16	9 <_'	1 1 1 1 1 2 2 2	3 18 1 14 3 10	3 725 6 64 9 96) 3.91 5 4.46 1 3.73 1 4.44 3 3.66	5 4 5 4 4 10	<5 <5) <5			24 2 29 5 45	.3 .7 1.1	5 7 8 <2	<2 <2 <2	2 62 2 58 2 58	.29 .42 .94	5 .074 7 .099 2 .061 4 .044 5 .055) 13 14 26	22 25 26	.90 .75	117 97 195	.06 .06 .07		2 1.82 2 2.44 2 2.14 2 2.14 2 2.8 2 2.8	4 .01 4 .01 8 .01	0. 0.		
STANDARD C/AU-S		-	-	-		•		3 104	2 3.9	<u>6 4</u>	1 18		7 37	7 52	18.6	5 15	5 17	7 60) .5	1.094	40	62	.92	182	.08	3 3	3 1.8	8 .07	7.1	5 1!	5 48

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Tom Lisle PROJECT R-1 FILE # 94-4193



ACHE ANALYTICAL																														CINE ANAL	TICAL
SAMPLE#	Mo ppm	Cu ppm	Pb ppm	2n ppm	Ag ppm	Ni ppm	Co ppnt	Mn ppn		As ppm	U PPM			Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca X	P X	La ppm	Cr ppm	Mg %	Ba ppm	Ti X	B ppm	Al X	Na X	к Х	W ppm	Au* ppb
L18N 2+00W L18N 1+50W L18N 1+00W L18N 0+50W L18N 0+50W	1 1 1 2 1	79 v 59 - 103 -	16 20	99 - 517 245 * 134 - 123 -	<.1 <.1 <.1	12 15 15 15 13	14 23 35	917 881 1615 1142 1107	4.34 4.33 4.97	5 ~ ~ ~ ~ ~ ~ ~	ও ও ও ও ও ও ও ও ও ও	° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° °	4 3 3 4 3	50 32 25 26 30	1.4 3.5 .8 .5 .8	<2 <2 <2 <2 <2 <2 <2	<2 <2 <2 5 <2 5 <2	66 64 66 70 77	.27 .30	.087 .051 .114 .085 .067	20 21 14 15 13	26 21	1.12 .93 .99 1.19 .84	114 120 154 137 154	.05 .08 .06 .05 .06	<2 2 <2 <2	3.31 3.26 3.62 3.62 3.81	.01 .01	.09 .12 .10 .11 .09	1 1 1 1 1 1 1 1	2 4 30 4 2
L16N 10+00W L16N 9+50W L16N 9+00W L16N 8+50W L16N 8+50W	1 1 1 1 2	47 35 -	14 8 15		2 <.1	9 10 11 17 9	9 14 20	1010 936 798 499 714	3.84 4.02 5.44	8 <2 8 3 <2		<2 <2 <2 <2 <2 <2 <2 <2	<2 3 2 5	27 44 32 45 52	.8 .7 .4 .4 1.0	3 5 3 2 2	5 3 2 9 2	56 61 58 60 59	.25		10 28 14 13 17	23 22 19	.70 .74 1.03 .92 .64	116 147 62 157 215	.06 .07 .06 .06 .09	5 <2 3	2.25 2.47 2.02 2.33 2.13	.02 .01	.07 .09 .09 .09 .09	<1 <1 <1 <1	1 4 25 16 4
L16N 7+50W L16N 7+00W L16N 6+50W L16N 6+00W L16N 5+50W	1 3 3 7 2	42 45 44 66 81	9 10	94 113 104 51 141	.1 .1 - .1	17 16 21 8 19	18 23 20	635 574 575 623 940	5.65 6.15 7.26	4 3 2 5 2	<5 <5 <5 <5 <5	<2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <	5 8 6 11 4	38 22 27 36 38	.7 .3 .2 .3	<2 <2 <2 <2 <2 <2	2 3 2 2 2 2 2 2	63 64 68 69 60	.20 .27 .39	.087 .137 .157 .166 .083	16 19 16 67 53	18 22	1.10 .69 .97 1.17 .78	98 99 106 72 174	.08 .11 .06 .05 .07	<2 <2 2	2.26 2.93 2.80 2.11 3.32	.01 .01 .01 .01 .02	.07 .07 .07 .08 .09	<1 <1 <1 <1 <1	2 5 - 8 3
L16N 5+00W L16N 4+50W L16N 4+00W L16N 3+50W CL16N 3+00W	1 1 1 1 1 1	50 45 43 27 58	15 10	169 - 126 - 118 128 136 -	1 1 1	16 20 17 14 11	20 15 13	747 690 713 702 696	4.60 4.00 3.47	7 6 5 6 <2	ৎ ১ ৩ ৩ ৩	<2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <	3 2 2 2 3	32 36 33 28 36	.7 .9 .5 .5	<2 <2 3 5 2	<2 3 <2 5 2	66 68 62 59 65	.38 .37 .33	.121 .121 .120 .081 .055	14 14 11 10 13	21 22 22 22 23	-86 -93	130 123 102 116 126	.08 .07	<2 <2 3	2.62 2.57 2.24 2.47 2.50	.02 .01 .01 .01 <.01	.07 .09 .10 .10 .09	<1 <1 2 <1 1	3 1 6 <1 9
RE LIGN 3+00W LIGN 2+50W LIGN 2+00W LIGN 1+50W LIGN 1+00W	. 1 <1 1 1	51 53	- 14 - 10 + 16	138 135 126 166 170	- <.1 1 1	13 12 15 19 16	14 16 15	711 694 656 998 996	3.90 4.02 4.27	4 2 7 7 2	৩ ৩ ৩ ৩ ৩ ৩	< < < < < < < < < < < < < < < < < < < <	<2 <2	36 33 36 30 27	<.2 .5 .6 .4 .3	<2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <	<2 <2 3 <2 3 <2 3	68 64 64 66	.41 .43 .36	.056 .064 .044 .087 .079	14 13 13 17 15		.98 .97	115 88 122	.08 .07 .06	<2 <2 <2	2.53 2.58 2.05 2.74 2.73	.01 .01 .01	.08 .09 .07 .12 .10	1 <1 <1 <1	8 10 10 2 1
L16N 0+50W L16N 0+00W L14N 10+00W L14N 9+50W L14N 9+00W	<1 <1 1 1 <1	29	/ 11 / 10 / 7		- <.1	16 14 15 12 11	12 13 16	806 775 570 561 578	3.61 3.59 4.67	10 6 8 5 3	<5 <5 <5 <5	< < < < < < < < < < < < < < < <> </td <td><2 3 4</td> <td>29 24 24</td> <td>.2 .3 .4 <.2 <.2</td> <td><2 5 <2</td> <td><2 <2 <2 7 <2</td> <td>63 61 55 60 63</td> <td>.37 .25 .24</td> <td>.067 .076 .056 .071 .033</td> <td>14 11 9 17 10</td> <td>24 18 22</td> <td>.88</td> <td>108 119</td> <td>.07 .08 .10</td> <td>2 <2 <2</td> <td></td> <td></td> <td>.08 .08 .07 .09 .10</td> <td><1 <1 <1 <1</td> <td>4 10 3 6 2</td>	<2 3 4	29 24 24	.2 .3 .4 <.2 <.2	<2 5 <2	<2 <2 <2 7 <2	63 61 55 60 63	.37 .25 .24	.067 .076 .056 .071 .033	14 11 9 17 10	24 18 22	.88	108 119	.07 .08 .10	2 <2 <2			.08 .08 .07 .09 .10	<1 <1 <1 <1	4 10 3 6 2
L14N 8+50W L14N 8+00W L14N 7+50W L14N 7+00W L14N 6+50W	<1 <1 <1 <1 <1 1	39 `24 55	13		3	16 14 13	15 12 12	965 648 647 778 953	3.79 3.32 3.99		5 <5	<2 <2 <2 <2 <2 <2	3 2 3	34 29	.7 <.2 <.2	9 4 <2	10 3 9 7 <2	72 60 55 60 64	.34 .32 .59	.091 .087 .124 .095 .091	19 13 9 17 20	23 19 26	.60 1.20	170	.09 .07	2 2 4	2.90 2.71 2.36 2.00 2.13	.02	. 13 . 14 . 10 . 15 . 13	ব ব ব ব	5 3 2 5 8
STANDARD C/AU-S	19	59	39	123	6.8	72	32	1037	3.96	39	22	6	37	52	18.4	14	22	60	.51	. 095	40	62	.91	183	.08	33	1.88	.07	. 16	14	50

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Tom Lisle PROJECT R-1 FILE # 94-4193

ACHE AMALTTICAL				_																									v		Au*
SAMPLE#	Mo	Cu ppm			in Ag xa ppan					As ppm	ป ppm	Au ppm	ĩh ppm	Sr ppn	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca X	P X	La ppm	Сг ррт	Mg X	Ba ppm	Ti X	ppm	Al %	Na X		ppa	ppb
L14N 6+00W L14N 5+50W L14N 5+00W L14N 5+00W L14N 4+50W L34N 4+00W	1 1 1 2 1		57	1 1 1	151 101 182 33 - <.1	12 14 18	12 12 19	586 691 569 830 814	3.36 3.52 4.83	3 5 5 4 2	ৎ ১ ১ ১ ১ ১ ১ ১ ১	<2 <2 <2 <2 <2 <2 <2	4 3 2 4 <2	33 28 33 31 34	.3 <.2 .3 .2	<2 <2 <2 <2 <2 <2 <2 <2	<2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <	55 57 65	.35 .35 .31	.043 .116 .050 .114 .079	15 10 13 13 16	22 23 24 23 21	1.01 .76 .85 .86 .83	67 124 89 147 163	.07 .08 .09 .10 .08	4 <2 <2	1.66 2.08 1.89 2.97 2.61	.01 .03 .01 .02 .01	.10 .10 .14 .10 .10	1 <1 <1 <1	4 / 3 - 4 - 21 - 7 -
L14N 3+50W L14N 3+00W L14N 2+50W L14N 2+00W A L14N 2+00W B	1 1 1 <1 <1	41 55 39	- 13 - 6 - 10	5 1 5 2) 1	454 23 .3 194 13 .4 864	13 14 11	12 13 12	604 662 908 606 781	3.58 3.90	<2 5 4 <2 5		< < < < < < < < < < < < < < < < < < <	<2 2 3 4 2	32 31 27 28 27	.2 .2 .5 .4	<2 <2 <2 2 <2	<2	57 60 61 56 55	.33 .28 .32	.041 .044 .113 .084 .139	16 11 13 11 12	21 22 23 22 20	.71 .89 .81 .81 .69	109 89 169 92 115	.08 .08 .07 .07 .07	<2 <2 3	1.95 1.86 3.11 1.76 2.17	.02 .01 .02 .01 .01	.08 .10 .14 .08 .10	<1 <1 <1 <1 <1	4- 7. 3. 14. 5.
L14N 1+50W L14N 1+00W L14N 0+50W L14N 0+00W L14N 0+00W	1 1 1 1 1 1 1 1 1 1 1	52 39 48) - 11 2 - 9 2 - 4 3 - 9 2 - 10	71 41 7	183 27 .2 25 .3 923 80 - <.1	2 15 5 14 5 14	i 15 11 11	850 813 545	3.72 4.30 4.12 3.77 3.55	5 9 7 6 2	<5 <5 <5	<2 <2 <2 <2 <2 <2	2 2 2 2 2 2 2	30 24 32		<2 <2 <2	8 <2 <2	65 63	.37 .28 .39	.074 .129 .154 .052 .047	11 12 17 12 11	22 21 19 26 21	.90 .83 .66 1.03 .93	92 159 121 44 54	.07 .09 .05 .07	2 <2 <2	1.91 2.19 2.09 1.74 1.70	.01 .01 .01 .01 .01	.08 .10 .10 .12 .11	<1 <1 <1 <1	2 - 10- 8 - - - - - - - - - - - - - - - - - -
- RE L12N 10+00W L12N 9+50W L12N 9+00W L12N 9+00W L12N 8+50W L12N 8+00W	<pre>- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1</pre>	3	3 / 1: 7 / <} 0 / _ / 7 / <	2 4	74 74 70 ~ <. 04 . 74 - <.	1 16 1 12 2 13	5 13 2 13 3 11	609 540 540	3.55 3.65 3.55 3.23 2.88	5 <2 <2	<5 <5 <5	<2 <2 <2 <2 <2 <2	<2 2 2 2 2 2 2 2	35 34 29	×.2 2.	<2 3 <2	<2 <2 <2	61 64 55	.39 .39 .33	.047 .058 .044 .046 .078	10 11 9 9 9	20 26 26 24 23	1.01 .98 .94	58 74 57 88 101	.06 .08 .10 .07 .07	<2 <2 <2	1.69 1.87 1.77 1.92 1.77	.01 .01 .01	. 13 . 10 . 13	ং1 ং1 ং1 ং1	4 1 2 4 3
L12N 7+50W L12N 7+00W L12N 6+50W L12N 6+00W L12N 5+50W	1 2	4 4 3	5 1 1 4 1	7 2	109 70 117 76	1 1: 2 1: 1 1	2 13 0 1 1 10	5 857 641 547	3.89 4.11 3.40 3.37 5.3.87	6 3 <2	<5 <5 <5	<2 <2 <2	2 3 2 <2 <2	39 35 37	<.2 <.2	<2 5 <2	<2 <2 <2	63 51 54	.57 .41 .38	.091 .087 .077 .058 .060	18 17 14 13 12	25 22 24	.83	94 74 84 40 134	.07 .07 .08	<2 <2 <2	1.86 1.73 1.61 1.56 2.30	.02 .01 .01	.10 .13	<1 <1 <1	5 23 3
L12N 5+00W L12N 5+50W L12N 4+50W L12N 4+00W L12N 3+50W L12N 3+50W	1	64	8 / 7 / 1 0 / 1 3 /	7 1 1 2	192 201 121 101	5 1 3 1 2 1 2 1	7 14 4 1 6 1 7 1	5 88 0 1 760 6 653	1 4.26 0 3.68 9 4.09 3 4.19 1 3.76	3 6 2 13 2 6	<5 <5 <5	<2 <2 <2		27 49 34	.5 .2 .7	4 2 5	<2 4 <2	58 74 71	.3(.51	090. 084 068 0.058 0.058 0.112	11 16 13	22 26 35	.71	151 127 103	.08 11 201	3 <2 1 <2 9 <2	2.66 2.2.28 2.2.41 2.41 2.1.97 2.1.88	.02 .02 .01	. 10 . 12 . 12	<1 <1 <1	12 6 10
L12N 2+50W L12N 2+50W L12N 2+00W L12N 1+50W L12N 1+50W L12N 0+50W	<	1 5 1 3 1 6 1 7	2 / 1 6 / 61 / 1	12 9 <2	199 118	2 1 3 .2 1 .3 1	9 1 8 1 5 1	3 79 3 101 3 62 9 70	1 3.90 6 4.07 4 3.79 5 3.00 0 3.80	5 10 7 6 9 1 ⁴ 6 1	5 <5 1 <5 5 <5	<2 <2 <2		5 42 2 36 4 16	2 .4 5 <.2 5 .3		s 2 s ≺2	57 63 51	4	7 .220 0 .136 2 .133 4 .089 6 .164	14 11	19 21 20	.71 .88		00. (00. (0. (6 < 6 < 7 <	2 2.41 2 2.14 2 1.94 2 3.04 2 2.85	.03 .01 .02	i .10 .10 2 .07) <1) <1 7 <1	i 5 1 48 1 26
STANDARD C/AU-	s <u>1</u>				136 7		74 3	3 104	3 3.9	6 4	1 15	56	37	7 57	2 18.9	2 14	4 21	60).4	9 .094	40	62	.92	188	3.0	8 3	5 1,88	3 .07	.16	5 13	3 53

ACHE ANALYTICAL

Tom Lisle PROJECT R-1 FILE # 94-4193

																												-	AC	HE ANALY	ЛІСА
ACHE ANALYTICAL SAMPLE#	Mo	Cu ppm	Pb ppm	Zn ppm	-	Ni	Co ppm	Mn ppm	Fe %	As ppm	U ppm		Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca X	P X	La ppm	Cr ppm	Mg X	8a ppm	Ti X	8 ppm	A1 %	Na X	K X		Au* ppb
L12N 0+00W L10N 10+00W L10N 9+50W L10N 9+00W L10N 8+50W	1 1 1 <1 <1	152 33 36 28 30	* 8 * 4 * 5	167 76 103	* < 1 * < 1 * < 1 * < 1 * < 1	8 8 10 10 5	11 10 10	644 695 640 586 496	3.67 3.31 3.71 3.47	5 4 2 4 6	<5 <5 <5 <5 6	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	4 3 3 2	27 28 44 37 30	<.2 .3 <.2 <.2 <.2	7 3 2 2 2	9 2 8 4 3	69 54 68 60 61	.35 .64 .48	.079 .124 .091 .057 .040	13 11 12 10 8	21 20 35 25 24	.93 .63 1.08 .92 .90	185 140 73 74 68	.06 .09 .10 .10 .08	2 7 4 <2	2.26 1.86	.02 .02 .01	.10 .09 .13 .11 .07	<1 2 <1 <1 <1	5 1, 3, 1, 5
LION 8+00W RE LION 8+00W LION 7+50W LION 7+00W LION 6+50W	<1 _1 <1 1 1	26 37 33	/ <2 9 3	- 51 105 107	<.1 <1 1 - <1 - <1	10 10 14 18 9	13 13 8	547 550 738 457 589	3.52 4.11 3.30	5 5 2 2 5	5 5 6 5 5 5 5	<2 <2 <2 <2 <2 <2 <2 <2	5 5 3 2 2	66 66 44 36 41	<.2 <.2 <.2 <.2 <.2	4 <2 <2 <2 <2	7 <2 4 <2 5	69 70 73 55 58	.61 .49 .37	.053 .051 .059 .053 .045	11 11 13 12 10	16 34 29	1.07 1.07 1.25 .85 1.08	74 72 86 87 53	.14 .14 .09 .10 .10	2 3 <2	2.31	.01 .01 .01 .01 .01	.10 .10 .14 .12 .12	<1 <1 <1 <1 <1	<1 <1 2 88
LION 6+00W LION 5+50W LION 5+00W LION 5+00W LION 4+50W LION 4+00W A	1 <1 <1 <1	42	8 8 5	122 135 129			11 11 12	569 650 603 612 776	4.08 4.01 3.74	4 3 5 4	<5 <5	<2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <	3 3 4 <2 <2	45 37 35 32 32	<.2	3 <2 5 4 2	<2 <2 5 3	71 68 64 61 61	.46 .37 .38	.056 .088 .051 .101 .086	20 13 15 11 12	29	1.26 1.08 .97 .91 .92	49 93 92 103 119	.07 .09 .08 .07 .08	4 <2 4	1.99 2.07 2.02 1.96 2.10	.01 .01 .01	.09 .11 .09 .10 .10	<1 <1 <1 <1	1 3 7 5 9 4
L10N 4+00W B L10N 3+50W L10N 3+00W L10N 2+50W L10N 2+00W	<1 1 1 1	36 42 66	. 8	122 15 12	5 / .3 21 11 51 2 - <.1	12 15 15	11 15 14	1368 606 740 847 1494	3.67 4.04 4.11	5 6 5 6 3	<5 5	<2 <2 <2 <2 <2	3 3 4 <2	26	<.2 <.2 <.2	3 3 7 3 5	3 <2 2 7	56 61 66 65 60	.35 .38 .31	. 148 . 063 . 091 . 054 . 192	10 10 12 15 12	21 24 28 25 22	.85 .86	118 113	.07 .08 .08 .08 .08	4 5 <2	2.26 1.75 2.00 1.89 2.22	.02 .02 .01 .02 .02	. 11 . 09 . 08 . 08 . 14	<1 <1 <1 <1 <1	1 2 4 1
L10N 1+50W L10N 1+00W L10N 0+50W L10N 0+50W L10N 0+00W		32	· 3	8 7 11 5 11	7 ~ <.1 9 / .1 4 ^ <.1 2 ^ .2 7 - <.1	14 19 14	14 18 13	590 637 1393 705 615	4.05	7 2	5 <5	<2 <2 <2 <2 <2 <2	3	34 47 33	<.2 <.2 <.2	2 3	<2 3	93 66 81 68 71	.41 .80 .44	.100 .066 .118 .076 .066		30	.91 1.36 .84	106	.07 .07 .09	2 9 4	1.73 1.62 2.36 1.76 2.46	.02 .01 .03 .02 .01	.12 .15 .17 .19 .11	<1 1 <1 <1	290 4 4 <u>3</u> 1
L8N 9+50W L8N 9+00W L8N 8+50W L8N 8+00W L8N 7+50W	<	1 37 1 62 1 45		2 34 7 6 5 6	71 52 71 2 .1 92	2 14 24 9	16 31 13	694 887 1108 511 385	3.85 5.46 3.60	8 5 <2	6 <5 7	<2 <2	3 6 3	42 52 48	<.2 <.2 <.2	2 <2 3	12 <2 <2	89 75	.45 .60 .42	.045 .076 .065 .042 .042	20 11	21 60 20		144 154 84	.08 .07 .11	3 3 <2	2.36 2.45 2.99 1.88 1.60	.01 .01 .01 .02 .01	.12 .12 .16 .13 .11	<1 <1 <1 <1	1 24 2
L8N 7+00W L8N 6+50W L8N 6+00W L8N 5+50W L8N 5+50W	<	1 22 1 30 1 4 1 4 1 2	2 / 1) / 1) / 1	6 6 3 7 9 10 3 5	2 8 6	1 5 2 1 ⁻¹ 2 14 2 15	1 10 4 17 2 10	9 412 9 510 7 759 9 373 9 473	3.21 4.40 3.00	15) 8) 8)	5 6 5 7 5 <5		2 3 2 5 2 4	36 30 35	5 .2) <.2 5 <.2	5 <2	8 <2 4	59 63 48	.3	5 .041 4 .055 5 .134 6 .058 9 .065	12 22 13	29 21 19	5 .77 1 .94 5 .64	72 157 61	.08 .07 .08	3 2 7 <2 3 2	1.34 1.64 2.19 1.42 1.78	.01 .01 .02	.10 .09 .08	<1 <1	1 2 3
STANDARD C/AU-S					1 6.		-	2 1032			2 16	5 (5 34	5	1 18.0) 14	. 19	62	.5	1 .094	40	6	.91	190	.08	3 33	5 1.88	.07	. 15	12	53

Tom Lisle PROJECT R-1 FILE # 94-4193



ACHE ANALTITCA	L																													ALME	ANALTI
SAMPLE#	Mio ppm	Cu ppm	Pb ppm		Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sp ppn	8i ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg X	8a ppm	Ti %	B ppm	Al %	Na X	K %	₩ ppm	Au* ppb
L8N 4+50W	1	47 -	13	103	´ <.1	19	15	1011	3.86	9	<5	<2	3	34	.5	<2	3	66	.41	.126	16	29	.92	119	.10	4	2.19	.01	.11	1	2
L8N 4+00W	<1	46	/ 8	99	<.1	12	13		3.92	6	<5	<2	2	33	.4	<2	7	63	.39	.062	18	29	.98	96	.09	2	1.95	<.01	.13	<1	3
L8N 3+50W	2	26	6	56	· <.1	5	12	494	3.02	4	<5	<2	5	43	<.2	5	<2	50	.34	.051	17	14	.73	69	.03	3	1.63	<.01	.10	<1	57
L8N 3+00W	1	33	10	98	1	13	13	703	3.70	7	<5	<2	3	35	.3	3	2	66	.44	.071	11	31	1.07	96	.09	2	1.83	.01	. 13	<1	4
L8N 2+50W	2	33	9	141	4	15	12	895	3.50	3	<5	<2	3	54	.4	8	3	53	.74	.041	13	25	.85	150	.10	3	2.48	.03	.10	<1	2
RE L8N 2+50W	2	3 3 -	- 13.	136	.2	17	12	888	3.58	2	<5	<2	<2	53	.7	4	<2	53	.74	.040	13	26	.86	138	. 10	5	2.52	.02	.10	<1	7
18N 2+00W	1	29	13	75	.1	12	12	564	3.75	7	<5	<2	2	38	.4	7	3	74	.49	.067	10	34	.84	53	.10	2	1.68	.02	.10	2	3
L8N 1+50W	3	63	17	96	.3	14	13	881	4.28	<2	<5	<2	2	61	.3	<2	<2	65	.83	.039	23	32	1.00	184	.08	<2	2.62	.02	.11	<1	4
L8N 1+00W	2	40	12	79	<.1	16	15	938	3.94	11	<5	<2	<2	54	.6	5	10	65	.74	.034	18	32	.96	150	.09	2	2.23	.01	.17	<1	3
L8N 0+50W	2	29	10	71	<.1	15	14	636	3.83	3	<5	<2	2	51	.5	<2	9	66	.70	.017	19	30	.98	161	.09	2	2.21	.02	.13	<1	6
18N 0+00W	1	27	10	102	1	16	15	672	3.70	8	<5	<2	2	29	.3	2	3	57	.39	.072	14	27	.92	118	.06	3	1.81	.01	. 16	<1	1
STANDARD C/AU-S	22	62	42	128	7.5	72	32	1078	4.09	41	24	7	41	53	19.1	14	22	62	.51	.095	42	62	.92	190	.09	34	1.94	.07	.17	14	49

Sample type: SOIL. Samples beginning 'RE' are duplicate samples.

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44



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Tom Lisle PROJECT R-1 FILE # 94-4193



ACRE MALITICAL

SAMPLE#	Mo ppm						Co Co	Mn ppm		As ppm	ų Ppm	Au ppm (Sr ppm	Cd ppm	Sb ppm		V ppm	Ca X		La ppm			Ba ppm	ті % р	B pm	Al %	Na X	К ⊾ %µрп		Pt** ppb	Pd** ppb
91618 91619 91620 91621 91622	<1 1 4 1 1	157 8 4 7	16 <2 2 5 <2	6 9 <1 5	<.1 <.1 <.1 <.1	7 1a 25 9 3	57 9 3 7	434 84 114	17.19 3.99 1.41 3.85 3.76	6 2 8	<5 <5 <5	<2	3 7 4	73 6 45	.7 <.2 .3	<2 2	<2 <2 <2	65 9 62	.74 1.10 .04 .73 .72	.154 .023 .157	10 21 8	8 71	2.96 .46 1.49	7 10<.	. 18 . 01 . 28	<2 2 <2 <2 1	2.56 .57 1.18	.03 .06 .05	.01 <1 .03 <1 .10 <1 .10 <1 .09 <1	15 <1 <1	<3 3	5
RE 91622 Standard C/Fa-100S	1 1	-	<2 38	-	<.1 7.0	8 71	12 31 1	1 12 1052	3.80 3.96	_	<5 18	<2 7		41 53	.3 19.4	<2 14		57 60	.71 .49	.159 .096	7 40		t.55 .93		.26 .08				.10 <1 .16 15			<3 51

Sample type: ROCK. Samples beginning 'RE' are duplicate samples. AU** PT** & PD** ANALYSIS BY FA/ICP FROM 10 GM SAMPLE.

		T	om Lisl	e PROJECT	ROCK	File #	94-41	93	Page	a 12				4
	· · · · · · · · · · · · · · · · · · ·		······································	145 W. Rocklar	nd Road, No	rth Vancou	wer BC V7	N 2V8						
	SAMPLE#	SiO2 Al 203		CaO Na20 K20 1 2 X X X	1102 P205 1 % %	4n0 Cr203 % %	Ba Ni ppm ppm	Sr ppm	Zr 1 ppm ppm		Sc LC ppm)I SUM % %		
	91623 RE 91623	69.83 16.32 69.37 16.24	2.13 .69 2.11 .70	.42 5.79 2.01 .40 5.67 2.10	.67 .16 .67 .15	.02 <.002 .01 <.002	273 <10 271 11	206 204	248 19 251 20	2 10 11		9 100.05 0 99.53		
			GRAM OF LI	BOZ AND ARE DIS	SOLVED IN 1	00 MLS 5%	HNO3. 8a	IS SUM	AS Baso4	AND	DTKER MET	TALS ARE SU	M AS OXIDES.	
		SOIL P11-P12 F		<u>ples beginning (</u> /	1		\cap	l						
DATE RECEIVED:	NOV 18 199	74 DATE R	EPORT MAI	(LED: $N_0 \sqrt{2}$	25/94.	SIGNE	D BY	· [~	··].D.	TOYE,	C.LEONG,	J.WANG; C	ERTIFIED 8.C. AS	SAYER
					1				J					
				. ·										
·														

ACME AF	YTIC/	L L	ABOI	RATO	RIES	LTI).			Е. Н					- de sér						PI	IONE	(604	1)25	3-31	58 FAX	(61	25	3-17	16
AA									0.588	EOCH n Lj 145 (lsle	<u>)</u>	?il€	e #	94 94 Inth V	-45(52	Pa	age										Av L	
AMPLE#	Mo ppm	Cu ppm	РЬ ppm	Zn ppm	Ag ppm	Nī ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cđ ppm	Sb ppm	Bi ppm	V ppm	Св %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	BAL ppm %	Na %	K %	¥ ppm	Au* ppb
35N 10+00W 35N 9+50W 35N 9+00W 35N 8+50W 33N 10+00W	15 3 1 2 <1	40 39 31 35 37	9 8 6 11 10	73 63 88 86 67	.2 .2 .2 .1 <.1	22 26 23 23 23 22	13		4.42	<2 3 <2 3 7	6 <5 <5 <5	< < < < < < < < < < < < < < < < < < <	3 2 2 2 2 2	23 46 64 25 18	<.2 .2 .2 .2 <.2	3 <2 2 2 4	<2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <	81 77 74 83 83	.53 .72 .20	.079 .046 .043 .037 .092	39 20 18 19 13	40 38 32	1.06 1.29 1.10 1.13 1.25	132 200 281 187 99	.07 .08 .07 .07 .05	2 3.34 <2 2.86 2 3.12 3 3.51 <2 3.54	.01 .02 .02 .02 .02	.09 .08 .08 .09 .10	1 1 2 2 1	4 2 1 5 6
33N 9+50W 33N 9+00W 33N 8+50W 33N 8+00W 33N 1+50W	1 5 <1 2 1	47 58 27 34 53	11 12 13 9 15	106 70 74 67 147	.2 .4 .1 <.1 .4	24 25 17 22 19	15 18 11 14 14	703 312	4.28	8 4 <2 5	<5 8 5 <5 <5	<> < < < < < < < < < < < < < < < < < <	2 3 3 3 2	25 45 19 20 30	.2 .2 <.2 <.2	4 3 3 4 3	<2 <2 <2 <2 <2 <2	86 80 77 81 76	.48 .18 .17	.059 .041 .048 .057 .073	20 56 28 10 19	38 37 30 28 30	.86 1.02 .87 .86 .91	177 199 100 115 271	.08 ,05 .06 .10 .05	<2 4.04 4 3.93 3 3.81 3 3.81 2 3.30	.02 .02 .01 .02 .02	.09 .09 .06 .11 .09	1 1 2 3	3 4 2 1 4
L33N 1+00W L33N 0+50W L33N 0+00W L31N 10+00W L31N 9+50W	<1 <1 1 2 3	45 37 40 37 37	19 12 11 11 12	187 1 32 116 92 82	.2 .1 .3 .1	17 16 16 22 20	14 12 12 17 16	786 720 747	4.35 4.06 4.02 4.55 4.72	9 7 <2 7 4	<5 <5 <5 <5	<2 <2 <2 <2 <2 <2	2 2 3 2	24 32 35 29 37	.3 .2 .2 <.2 <.2	3 <2 <2 3 3	<2 <2 <2 <2 <2 <2 <2	75 69 72 83 80	.41 .40 .27	.127 .069 .048 .069 .073	13 17 19 19 20	19 30	.77 1.04 .97 1.07 1.22	180 114 135 145 137	.06 .06 .06 .08 .05	2 3.26 3 2.40 2 2.43 2 3.52 <2 3.05	.02 .01 .02 .01 .01	.10 .09 .08 .10 .10	2 2 1 1	3 7 3 2 1
L31N 9+00W L31N 8+50W L31N 8+00W L31N 1+50W L31N 1+50W	1 1 <1 2 2	34 36 35 121 44	9 13 16 15	101 78 64 95 107	.2 .2 .1 .3 .3	20 24 20 18 18		749		<2 9 3 8 13	<5 <5 <5 <5	<2 <2 <2 <2 <2 <2 <2	2 2 3 2	30 38 35 28 32	<.2 <.2 .2 <.2	<2 <2 <2 3 <2	<2 <2 <2 <2 <2 <2	79 83 77 74 74	.41 .40 .46	.064 .063 .051 .046 .034	17 16 17 35 17	42 34	1.05 1.41 1.01 1.00 .94	128 108 77 190 246	.05 .07 .09 .07 .05	3 3.10 2 2.63 3 1.91 2 3.88 2 2.88	.01 .01 .02 .02 .02	.10 .11 .07 .08 .08	2 1 1 2	4 2 6 2 5
L31N 0+50W RE L31N 0+50W L31N 0+00W L29N 7+50W L29N 7+00W	<1 <1 <1 2 4	50 48 38 42 19	8 9 11 11 10	106	.1 <.1 .2 <.1	21 20 18 22 22	14 14 11 19 22	566 703 736	4.52 4.46 3.87 5.02 7.34	7 7 8 8	<5 <5 <5 <5	<2 <2 <2 <2 <2 <2	2 2 2 4 6	32 31 33 21 57	<.2 .2 <.2	4 <2 2 <2	<2 <2 <2 <2 <2 <2	72 71 73 75 88	.44 .46 .20	.051 .051 .054 .118 .101	15 15 17 13 25	26 28 21 21 26	.85 .84 .83 1.09 .82	188 186 159 98 138	.05 .05 .06 .06 .07	3 2.57 <2 2.53 2 2.91 3 3.29 2 3.23	.02 .02 .02 .01 .02	.08 .08 .08 .09 .07	2 1 2 <1 1	8 5 2 5 3
L29N 6+50W L29N 2+50W L29N 2+00W L29N 1+50W L29N 1+00W	1 6 2 4 3	28 67 69 280 96	12 16 14 12 14	88	.1 .6 .2 .7	19 18 14 24 19		760 367 463	4.89 4.72 2.68 3.86 3.45	6 7 5 <2 6	5 <5 <5 5 5 5	<2 <2 <2 <2 <2 <2	5 2 <2 <2 2 2	15 54 53 62 55	.4 .5 .3	<2 <2 <2 <2 <2	< < < < < < < < < < < < < < < < < < <		.95 1.15 1.25	.143 .031 .059 .056 .043	21 30 15 23 25	21 25 23 26 26	.90 .72 .87 .69 .68	85 223 96 109 128	.07 .05 .05 .07 .08	2 3.51 3 3.48 <2 2.12 3 2.87 2 2.93	.01 .02 .02 .02 .02	.07 .08 .06 .05 .06	1 2 1 1 ∢1	4 7 5 6 2
L27N 3+00W L27N 2+50W L27N 2+00W L25N 7+00W L25N 6+50W	1 <1 2 1 2	59 108 53 35 33	12 12 13 10 7	80 100	.3 .4 .5 .1 .1	33 21 19 16 18	24 16 13	677 796 652	4.87 4.77 4.46 3.67 3. 93	5 5 12 <2 4	<5 <5 <5 <5	<2 <2 <2 <2 <2		32 30 33	<.2 <.2 <.2 <.2 <.2	3 <2 <2	<2	73 67	.34 .37 .36	.110 .080 .087 .066 .093	16 12 18 21 19	25 20 23	.84	112 114 113	.07 .06 .06	2 3.52 3 3.29 <2 2.73 2 2.52 4 3.05	.02 .02	.08	2 <1 1 1 <1	2 1 13 4 1
STANDARD C/AU-S	17	56	38	126	6.6	74	31	1031	3.96	44	18	7	35	49	17.2	14	18	60	.50	.093	40	61	.90	188	.08	33 1.88	.06	. 15	10	47
		THIS	LEA	CH IS	M SAM PARTI SOIL	AL FO	DR MN	FE S	R CA P	H 3ML P LA C Y Acid	RMG	BA T	(B W	AND	LIMIT	ED FOF	L NA K	AND	AL.							NATER.				
DATE REC	EIVE	D:	DEC	29 19	94]	DATE	REI	PORT	MAI	LED		Jan	. 9/	95	S	IGNE	D BY	<u>.</u> C.	:L.	·*••	0.T	OYE,	C.LEC	DNG, J	I.WANG	; CERTIFIE	D 8.C	:. ASS	AYERS	

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Tom Lisle FILE # 94-4562

ACHE ANALYTICAL																													A	CHE ANAL	TT LCAL
SAMPLE#	Мо ррпа	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Min ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	₩ ppm	Au* ppb
L25N 6+00W L25N 5+50W L25N 5+00W L25N 4+50W L25N 4+00W	1 2 2 1 5	38 26 35 139 44	10 2 9 14 11	100 48 67 92 69	<.1 <.1 .2 .1 .1	15 10 15 32 25	20 12	1389 667 518 594 645	4.87 5.02 5.62	<2 4 3 <2 <2	ৎ ২ ২ ২ ২ ১ ২ ১	~~~~~~ ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	2 6 5 4 4	30 40 49 25 36	.4 <.2 <.2 <.2 <.2	<2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <2 <	2 7 <2 3 6	76 65 93		. 125	13 75 18 16 20		.89 .99 .90 .98 1.38	157 97 102 113 132	.06 .01 .04 .09 .13	5 7 7 3 8 4	3.39 2.17 3.22 4.48 3.86	.02 .01 .02 .01 .02	.13 .10 .09 .07 .08	1 <1 <1 1 <1	2 3 2 1 59
E L25N 4+00W 23N 10+00W 23N 9+50W 23N 6+50W 23N 6+50W 23N 6+00W	5 1 2 1 2	45 44 53 35 54	9 4 6 13	68 85 76 80 106	<.1 .1 .2 .2 <.1	26 17 20 13 18	18 17 17	649 669 618 602 934	4.36 4.26 4.23	2 5 <2 11	<5 <5 <5 <5	~~~ ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	3 3 3 4	36 30 32 33 29	<.2 <.2 .4 <.2 <.2	<> < < < < < < < < < < < < < < < < < <> <>	<2 <2 3 2 2	112 66 68 64 73	.31 .33 .35	. 133 . 096 . 081 . 101 . 150	20 20 17 21 25	24 26 20	1.40 1.16 1.28 1.02 1.10	140 101 95 70 119	.13 .06 .06 .05 .07	6 3 3	3.86 2.65 2.62 2.21 3.20	.02 .01 .01 .01 .01	.07 .08 .08 .08 .12	1 <1 <1 <1 <1	45 3 8 4 2
23N 5+50W 23N 5+00W 23N 4+50W 23N 4+50W 23N 4+00W 21N 4+50W	2 2 1 2 1	14 61 38 54 35	13 14 9 4 7	40 99 85 96 98	<.1 .2 <.1 <.1 .2	8 25 18 17 16	21 18 23	354	5.58 5.85 5.07	2 5 <2 3 10	<5 <5 <5 <5 <5	< < < < < < < < < < < < < < < < < < < <	9 4 2 3 4	60 30 49 28 35	<.2 <.2 <.2 .2 <.2	<2 <2 <2 <2 <2 <2	<2 4 <2 2 3	64 72 130 79 80	.23 .42 .20	.178 .182 .143 .150 .151	61 19 28 18 13	23 20 21	1.27 1.15 1.30 1.08 .91	108 148 129 138 129	.01 .06 .03 .11 .08	6 5 <2	2.51 3.48 3.84 3.22 3.33	.04 .02 .02 .01 .01	.11 .10 .09 .09 .12	<1 <1 <1 <1 <1	1 2 3 27
21N 4+00W 21N 3+50W 19N 4+00W 19N 3+50W 19N 3+00W	2 2 13 2 2	50 66 45 45 232	4 7 9 11 8	90 92 21 92 57	<.1 <.1 .1 <.1	19 11 7 17 20	24 22 21 23 18		5.42 7.24 4.49	5 7 <2 3 5	<5 <5 <5 <5	<2 <2 <2 <2 <2 <2	2 2 5 2 2	49 41 72 38 100	<.2 <.2 <.2 .3 <.2	<2 3 <2 2 <2 <2	5 <2 7 <2 5	85 86 89 84 133	.36 .37 .33	. 134 . 135 . 184 . 129 . 108	17 18 27 15 14	21 9 23	1.17 1.13 1.07 .90 1.47	129 133 76 106 70	.13 .10 .02 .11 .06	44	2.95 2.81 2.04 2.85 2.70	.01 .01 .01 .02 .01	.11 .10 .09 .09 .11	<1 <1 <1 <1 <1	4 10 11 2 1
19N 2+50W 19N 2+00W 19N 1+50W 19N 1+00W 19N 0+50W	1 3 1 2 1	49 50 55 208 84	14 12 15 6 16	93 118 124 104 1 32	.3 <.1 .2 <.1 .1	16 16 17 16 20	22 17 16	704 912 1095 853 943	4.57 4.21 4.41	4 10 <2 9 5	<5 <5 <5 <5 <5	<2 <2 <2 <2 <2 <2	2 2 2 2 2 2	34 44 30 34 32	<.2 <.2 .3	2 <2 <2 <2 <2 <2	2 <2 7 4	63 70 70 69 72	.34 .39 .58	.060 .095 .082 .041 .061	15 17 12 22 18		.98 .90 .87 1.08 1.10	124	.07 .08 .07 .06 .07	3 <2 6	1.97 3.11 3.33 2.89 2.83	.01 .01 .01 .02 .01	.08 .13 .11 .09 .13	<1 <1 <1 <1 <1	2 1 3 2 2
.19N 0+00W .17N 10+00W .17N 9+50W .17N 9+00W .17N 9+00W	2 1 1 1	109 31 43 38 34	270 6 9 11 7	347 103 127 99 162	.1 .1 .3 .1	24 17 13 11 15		582	3.71 3.90 4.01	<2 10 7 4 6	<5 <5 <5 <5	<2 <2 <2 <2 <2 <2	2 <2 2 3 2	24 27 31 30 22	<.2 .4 <.2	<2 3 5 <2 3	3 <2 4 <2 <2	70 61 61 59 6 3	.29 .33 .29	.121 .058 .049 .067 .114	24 11 18 15 9	20	.66 .75 .79	111	.05 .08 .08 .07 .07	<2 <2 3	4.09 2.44 2.18 1.92 2.87	.01 .01 .02 .01 .02	. 15 .06 .06 .07 .08	<1 <1 <1 <1	1 1 8 2 3
L17N 8+00W L17N 7+50W L17N 7+00W L17N 7+00W L17N 4+00W L17N 3+50W	1 2 3 1 2	39 45 39 39 42	10	116 125 103	.2 .2 .1 <.1	20 15 17 14 16	19 13	777	5.13 3.73	11 12 6 10 4	<5 <5 <5 <5	<2 <2 <2 <2 <2	2 2 4 2 2 2	30 36 21 38 37	<.2 <.2 .6	3 4 2 2 2 2	2 3 <2 3	65	.30 .18 .52	.087 .107 .163 .045 .067	12 13 13 16 13	27 23 19 23 26	.69 .85 .56 .83 .84	153 136	.11 .10 .12 .08 .09	4 5 5	2.97 2.85 2.87 2.28 2.38	.02 .01 .02 .02 .02	.08 .09 .07 .09 .09	<1 <1 <1 <1 <1	1 18 240 2
STANDARD C/AU-S	19	62	40	128	7.0	71	31	1049	3.96	42	19	6	36	51	18.6	15	22	60	.51	.093	40	59	.91	190	.08	33	1.88	.06	. 15	11	47

Tom Lisle FILE # 94-4562

Page	3
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SAMPLE#	Mo ppm	Cu ppm	РЬ ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	sb ppm	8i ppm	V mqq	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	τi %	B PPM	Al %	Na %	K %	W ppm	Au* ppt
17N 3+00W	1	95	10	115	.5	22	14	1062 4	. 19	<2	<5	<2	2	49	.5	<2	<2	67	1.09	.046	31	34	1.02	163	.05	18	3.12	.02	.13	z	3
17N 2+50W	1	69	12	126	.2	18		712 4		4	<5	<2	3	35	.2	2	<2	75			18	27	.95	143	.08	3	2.68	.02	.09	2	4
17N 2+00W	2	49	11	134	.1	18				<2	<5	<2	2	39	.2	4	<2	78		.053	17		.91	141	.08	2	3.09	.02	.10	2	1
17N 1+50W	2	60	12	160	<.1	18		932 4		<2	<5	<2	2	35	.2	4	<2	76		.080	14		1.30	108	.06		2.62	.01		2	1
L17N 1+00W	2	122	13		.3	21		869 5		2	<5	<2	3	30	< .Z	5	<2	90		.089	22		1.13	186	.05		3.10	.01		1	15
		122	1.5	122		21	20	007 -		-	~	~		50			~~	/0			÷	20		100		•				•	•
17N 0+50W	1	63	13	118	<.1	41	20	731 4	.77	7	<5	<2	2	27	<.2	2	<2	90	.27	.089	10	74	1.34	149	.06	2	3.45	.01	.11	1	
17N 0+00W	1	77	15	113	.2	17	15	726 4	1.53	<2	<5	<2	2	30	<.2	2	<2	85	.53	.066	22	35	.88	142	.04	3	2.60	.01	.09	2	
L11N 10+00W	z	46	10	75	<.1	15	12	668 3	3.88	4	<5	<2	2	38	<.2	3	<2	67	.48	.043	21	30	1.07	55	.07	<2	1.84	.01	.10	1	
RE LITN 10+00W	3	45	12	69	.1	15	12	637 3	3.69	7	<5	<2	z	36	<.2	3	<2	63	.46	.042	20	28	1.02	53	.06	2	1.73	.01	.10	1	
L11N 9+50W	1	41	10	97	.1	16		719 3		ż	<5	<2	<2	32	<.2	3	<2	66	.39	.078	21	29	.89	95	.07	<2	2.23	.02	.10	1	
										_		-																			
L11N 9+00W	: 1	26	8	83	.1	13	10	580 3	3.41	<2	<5	<2	Z	37	.2	<2	<2	69	.48	.070	t 1	28	.85	85	.10	2	1.82	.02	.11	1	
L11N 8+50W	2	36	17	55	<.1	15	14	519 4	4.26	5	<5	<2	2	32	<.2	2	<2	85	41	.052	10	31	.97	55	.08	2	1.98	.01	.08	<1	
L11N 8+00W	1	53	13	74	.1	15	15	959 3	3.92	4	<5	<2	2	41	<.2	2	<2	70	.53	,083	18	30	1.18	55	.07	3	1.94	.01	.12	1	
L11N 7+50W	1	28	6	42	<.1	11	13	461	5.34	3	<5	<2	3	42	<.2	2	<2	62	.47	.054	15	21	.80	67	.06	2	1.52	.01	.09	<1	
L11N 7+00W	1	55	19	130	.1	16	12	630 3	3.92	3	<5	<2	2	34	<.2	3	<2	64	.37	.079	18	27	.83	107	.07	3	2.08	.01	. 14	1	
					-																										
L11N 6+50W	1	34	4	86	.1	15	11	745	3.54	<2	<5	<2	4	36	<.2	2	<2	61		.065	18		1.03		.06	_			. 13	1	
L11N 6+00W	1	45	10	67	<.1	16	11	527 3	3.67	<2	5	<2	2	36	.2	2	<2	70	.40	.043	14	31	.89	52	.09		1.58	.01	.12	1	
L11N 5+50W	! 1	38	10	85	<.1	14	12	5Z0 3	3.65	2	<5	<2	2	30	<.2	2	<2	70		.038	10	27	.86	79	-09	_	1,75	.01	.08	1	
L11N 5+00W	<1	44	11	98	<.1	16	12	545 3	3.77	8	<5	<2	2	33	<.2	2	<2	71	.33	.047	13	27	.90	83	. 09		1.92	.01	.09	1	
L11N 4+50W	1	45	10	127	.1	17	14	667 3	3.94	<2	<5	<2	<2	36	.2	2	<2	74	.39	.059	12	29	1.04	99	.08	<2	2.05	.01	.10	2	
	1	E.	10	111		17	• /	700		,	-5	<2	<2	36	<.2	2	<2	74	7.1	.070	13	70	1.08	90	.08	-2	2.00	.01	.10	1	2
L11N 4+00W		54 41	10	123	<.1	17 18	14	788 4 608 3		4 <2	<5 <5	<2	2	33	.3	<u>د</u>	<2	73		.061	12	30		110	.09		1.97	.01	.09	ź	¢
L11N 3+50W					-1		. –			~2						3	<2	80		.097	25		1.19	89	.07		2.21		.12	1	
L11N 3+00W	<1	94	11	101	.2	18		1059 4 748 3		, ×	<5 .r	<2	2	43	<.2		-	67		.097		24	.69	122	.08		1.97		.11	2	
L11N 2+50W	<1	39	11	134	.2	16				6	<5	<2	2	30	.2	<2	<2				12	22	.68	161	.08		2.64	.02	.09	2	
L11N 2+00W	; <1	48	14	181	.1	19	12	1138 :	5.55	4	<5	<2	z	21	.3	Z	<2	66	. 25	.216	12	22	•00	101	.09	2	2.04	.02	.09	2	
L11N 1+50W	1	69	9	64	<.1	16	12	537 3	3.99	5	<5	<2	Z	32	<,2	z	<2	76	.43	.093	13	27	.97	69	.08	<2	1.72	.01	.09	1	
L11N 1+00W	1	34	9	159	<.1	14		1066		8	<5	<2	<2	23	.2	<2	<2	59	.31	.311	8	14	.53	209	.08	Z	2.29	.02	.08	2	12
L11N 0+50W	<1	81	11	108	1	17		642		11	<5	<2	2	30	<.2	3	<2	74		.063	18		1.04	102	.07		2.24		11	1	
L11N 0+00W	i	62	13		< 1	19		808		10	<5	<2	2	28	<.2	2	<2	77		.083	13		1.09	118	.08		2.12	-	.11	1	
STANDARD C/AU-S	17			128		75		1031		42	18	7	36		17.4	15	18	60		.094	39		.91		.08		1.88	.06		10	5

Sample type: SOIL. Samples beginning 'RE' are duplicate samples.

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GSM-19T

Instruction Manual



teorophus

TERRAPLUS INC., 52 West Beaver Creek Road, Unit 14, Richmond Hill, Ontario 448 119 (Canada)

Telephone: (416) 764-5505 Fax: (416) 764-9329

GEM Systems Inc.

52 West Beaver Creek Rd. Unit 14 Richmond Hill, Ontario Canada L4B 1L9

Phone: (905) 764-8008 Fax: (905) 764-9329

1. THEORETICAL DESCRIPTION

1.1 Introduction

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The GSM-19T is a portable standard proton magnetometer/gradiometer designed for handheld or base station use for geophysical, geotechnical, or archaeological exploration, long term magnetic field monitoring at Magnetic Observatories, volcanological and seismic research, etc. The GSM-19T is a secondary standard for measurement of the Earth's magnetic field, having O.2 nT resolution, and 1 nT absolute accuracy over its full temperature range.

The GSM-19T is a microprocessor based instrument with storing capabilities. Large memory storage is available (up to 2 Mbytes). Synchronized operation between hand held and base station units is possible, and the corrections for diurnal variations of magnetic field are done automatically. The results of measurement are made available in serial form (RS-232-C interface) for collection by data acquisition systems, terminals or computers. Both on-line and post-operation transfers are possible.

The measurement of two magnetic fields for determination of gradient is done concurrently with strict control of measuring intervals. The result is a high quality gradient reading, independent of diurnal variations of magnetic field.

Optionally the addition of a VLF sensor for combined magnetometer/gradiometer-VLF measurement is available.

1.2 Magnetic Field Measurement

The magnetic field measuring process consists of the following steps:

- a) **Polarization.** A strong DC current is passed through the sensor creating polarization of a proton-rich fluid in the sensor.
- b) Deflection. A short pulse deflects the proton magnetization into the plane of precession.
- c) **Pause.** The pause allows the electrical transients to die off, leaving a slowly decaying proton precession signal above the noise level.
- d) **Counting.** The proton Precession frequency is measured and converted into magnetic field units.
- e) **Storage.** The results are stored in memory together with date, time, and coordinates of measurement. In base station mode, only the time and total field are stored.

1.3 Earth's Magnetic Field

Appendix B shows the nominal distribution of the Earth's magnetic field, with dotted lines separating the equatorial and polar regions. In polar regions the inclination of the magnetic field vector is approximately vertical, while in equatorial regions it is horizontal. To obtain the best precession signal the sensor must be aligned with the magnetic field. In polar regions the sensor axis must be horizontal, in equatorial vertical. Horizontal orientation of the sensor can be universal if the operator keeps the sensor oriented in an East-West direction (important only in equatorial regions).

Initially, the tuning of the instrument should agree with the nominal value of the magnetic field shown for the particular region in Appendix

Magnetic field direction should ideally be perpendicular to sensor axis

B. After each reading the instrument will tune itself automatically. If large changes in magnetic field are encountered between successive readings, a warning will be given to the operator and it may be necessary to repeat the reading to obtain an accurate result.

Local ferromagnetic objects like screws, pocket knives, wristwatches, tools etc. may impair the quality of measurement or in drastic cases even destroy the proton precession signal by creating excessive gradients. For best results, **ferromagnetic objects should be kept away from the sensor.** In normal applications, the magnetometer console does not produce appreciable effects on measurements provided that the sensor is installed on the staff and kept at least at arms length from the operator and the console.

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2. INSTRUMENT SPECIFICATIONS

2.1 Magnetometer / Gradiometer

Zinnaghoronn									
Sensitivity:	+/- 0.2 nT (gamma), magnetic field and gradient.								
Accuracy:	+/- 1 nT over operating range.								
Range:	18,000 to 120,000 nT, automatic tuning requiring initial set-up.								
Gradient Tolerance:	Over 7,000 nT/m								
Operating interval:	3 seconds minimum. Readings initiated from keyboard, external trigger, or carriage return via RS-232-C.								
Input/Output:	6 pin weatherproof connector, RS-232C, and (optional) analog output.								
Power Requirements:	12 V, 730 mA peak (during polarization), 30 mA standby, 1500mA peak in gradiometer mode.								
Power Source:	Internal 12 V, 1.9 Ah sealed lead-acid battery standard, others op- tional. An External 12V power source can also be used.								
Battery Charger:	Input: 110/220 VAC, 50/60 Hz and/or 12 VDC (optional). Output: 12V dual level charging.								
Operating Ranges:	Temperature: -40 °C to +60 °C. Battery Voltage: 10.0 V minimum to 15V maximum. Humidity: up to 90% relative, non condensing.								
Storage Temperature:	-70°C to +65°C								
Dimensions:	Console: 223 x 69 x 240mm. Sensor staff: 4 x 450mm sections. Sensor: 170 x 71mm dia. Weight: Console 2.1kg, Staff 0.9kg, Sensors 1.1kg each.								
2.2 VLF									
Frequency Range:	15 - 30.0 kHz.								
Parameters Measured:	Vertical In-phase and Out-of-phase components as percentage of total field. 2 components of horizontal field. Absolute amplitude of total field.								
Resolution:	0.1%.								
Number of Stations:	Up to 3 at a time.								
Storage:	Automatic with: time, coordinates, magnetic field/gradient, slope, EM field, frequency, in- and out-of-phase vertical, and both horizon- tal components for each selected station.								
Terrain Slope Range	$\Omega^{\circ} = 9\Omega^{\circ}$ (entered manually)								

Terrain Slope Range:0° - 90° (entered manually).Sensor Dimensions:14 x 15 x 9 cm. (5.5 x 6 x 3 inches).

1.0 kg (2.2 lb).

Sensor Dimensions: Sensor Weight:

Page 3

3. INSTRUMENT DESCRIPTION

3.1 Physical Overview

The parts of the GSM-19T magnetometer/gradiometer are as follows.

- The sensor is a dual coil type designed to reduce noise and improve gradient tolerance. The coils are electrostatically shielded and contain a proton rich liquid in a pyrex bottle.
- The sensor cable is coaxial, typically RG-58/U, up to 100m long.
- The staff is made of strong aluminum tubing sections (plastic staff optional). This construction allows for a selection of sensor elevations above ground during surveys. For best precision the full staff length should be used. Recommended sensor separation in gradiometer mode is one staff section (56cm from sensor axis to sensor axis), although two or more sections are sometimes used for maximum sensitivity.
- The console contains all the electronic circuitry. It has a 16 key keyboard, a 4 x 20 character alphanumeric display, and sensor and power/input/output connectors. The keyboard also serves as an ON-OFF switch.
- The power/input/output connector also serves as RS232C input/output and optionally as analog output and/or contact closure triggering input.
- The keyboard, front panel, and connectors are sealed i. e. the instrument can operate under rainy conditions.
- The charger has 2 levels of charging, full and trickle, switching automatically from one to another. Input is normally 110V 50/60Hz. Optionally, 12 VDC input can be provided.
- The all-metal housing of the console guarantees excellent EMI protection.

3.2 Software Version 4.0

There are several major versions of software for the GSM-19. As of August 92, GEM Systems added a major software upgrade to its GSM-19 family, enhancing its capabilities. This new generation of software (version 4.0) has the following advantages.

- 1. Diurnal correction (reduction) with interpolation can be used in conjunction with other GSM-19 models with software version 4.0. This allows the base mag to run with longer cycle time. Previous software could do interpolation only with fast GSM-19 types.
- 2. Memory filing system. Now 50 files can be stored in a directory, and mode of operation can be changed without erasing memory. With the software previous to version 4.0, only 1 file could be retained in memory, and this would be lost when modes of operation were switched.
- 3. Line and station numbers have been enlarged. Lines can now be 5 digits as opposed to 4 digits in previous software. Station numbers are now 7 digits as opposed to 6 in the previous software.
- 4. Transmission time has been significantly shortened.

Determining your instrument's software version

There are several visible indications that can be checked to determine if the GSM-19 has Version 4.0 software installed. Upon turning on the unit, if Version 4.0 software is present the third line of the display will indicate v4.0. Otherwise just the date of the software will be shown. Furthermore, from the main menu, **B-diurn.cor** is displayed in version 4.0 units. **B-reduction** is displayed in previous software version units. Finally, the header for every RS-232C transmission will have a v4.0 indicator and a file name.

Files

A new file will be opened in the following cases:

- 1. New file programmed by user.
- 2. Survey on a new day will automatically create a new file.
- 3. A base restart will automatically create a new file.
- 4. After the erase function is performed.

Note: The walking mag or grad has further modifications. See section 4.5 under the Walking Mag Mode subheading.

SABRE ELECTRONIC INSTRUMENTS LTD.

4245 EAST HASTINGS STREET . BURNABY, B.C. V5C 2J5

SABRE MODEL 27 VLF-EM RECEIVER

The Model 27 EM unit was designed originally for a large Canadian mining company to overcome the deficiencies inherent in existing units.

The instrument is so stable and selective that completely reliable measurements can be made on distant stations without interference from nearby powerful transmitters. Stability and selectivity are especially important when making field-strength measurements, which are now being emphasized as a means of locating conductors.

This EM receiver is very compact, requires no earphones or loudspeakers and is housed in a heavy scotch saddle leather case. All of these features add up to make an ideal one-man EM unit of unexcelled electrical performance and mechanical ruggedness.

SPECIFICATIONS

<u>Source of Primary Field</u> - VLF radio stations (12 to 24 KHz.) <u>Number of Stations</u> - 4, selected by switch; Cutler, Maine on 17.8 KHz. and Seattle, Washington on 18.6 KHz. are standard, leaving 2 other stations that can be selected by the user.

Types of Measurement

- 1. Dip angle in degrees, read on a meter-type inclinometer with a range of $\frac{+}{60^{\circ}}$ and an accuracy of $\frac{+}{15^{\circ}}$.
- Field strength, read on a meter and a precision digital dial with an accuracy exceeding 1%.
- 3. Out of phase component, read on the field strength meter as a residual reading when measuring the dip angle.

Dimensions and Weight

Approximately $9\frac{1}{2}$ " x $2\frac{1}{2}$ " x $8\frac{1}{2}$ "; Weighs 5 lbs.

Batteries

8 alkaline penlite cells. The instrument will run continuously on 1 set of batteries for over 200 hours; so that in normal on-off use, the batteries will last all season. The battery condition under load is shown by pushing a button and reading voltage on the field strength meter.

VLF-EM OPERATING INSTRUCTIONS

The equipment is operated in the usual way as follows:

- With the instrument held horizontal in front of you, turn around until a null appears on the field strength meter. You should now be facing the station.
- 2) With the receiver still facing the station, lift it to the vertical position and rotate it slightly in the vertical plane to your right or left until the best null appears on the field strength meter. Record the angle on the inclinometer at which the null appears. This is the DIP ANGLE (Positive or Negative).
- 3) Return the instrument to the horizontal plane and turn around until the field strength meter is at its maximum reading. Set this maximum reading at 100 on the meter and record the reading on the gain control dial. This is the Field Strength Reading.
- 4. Repeat steps 1, 2, and 3 at each station.
- 5) To test the batteries turn the power switch on and push the test button. The field strength meter should read above the red mark. Battery life is approximately 200 hours and if the instrument is turned off between readings, the batteries should last for an entire season.
- NOTE: An alternative way of measuring field strength is as follows: Proceed as in step 3, setting the meter to 100. Now push the field strength button (marked FS) and the meter will read 50. (If it doesn't, adjust the gain control slightly). Leave the Gain Control setting where it is and take comparative Field Strength readings at each station by pressing the Field Strength button and recording the meter reading, which will vary from its Base Station Reading as you pass over the conductive zones.

This is the method used in Part 2 of this book entitled: "DETAILED FIELD PROCEDURE".

SELECTION OF STATIONS:

The stations are selected by the switch on the control panel, with the following abbreviations being used:

C = Cutler, Maine	Frequency = 17.8 Khz.
S = Seattle, Wash.	Frequency = 18.6 Khz.
A = Annapolis, Md.	Frequency = 21.4 Khz.
H = Hawaii	Frequency = 23.4 Khz.

The two most useful stations are Cutler and Seattle and these will be used almost exclusively. Note that Seattle is off the air for several hours on Thursday for maintenance (between 10 A.M. and 2 P.M. usually). Cutler is off the air for the same length of time every Friday.

If Equipment fails to operate:

- (a) Check that station is transmitting (see above). If one station appears to be dead, check another one to see if it is operating normally.
- (b) Check batteries. If they are low or the reading begins to drop after the test button is held down for a few seconds, replace them. Note also that there are 8 batteries in the instrument and they cannot be individually checked by the test button. If the batteries have been in the unit for a long time it is possible that one is dead or very weak but that the total voltage indicated by the test button is near normal. It is cheap insurance to instal new batteries before starting a big survey.
- (c) If unit still fails to operate check that battery connectors are tight, then check wiring of battery connectors for breaks or damage.

PART 2: DETAILED FIELD PROCEDURE

OPERATING INSTRUCTIONS

SABRE VLF-EM RECEIVER

INTRODUCTION:

The VLF-EM method utilizes electromagnetic fields transmitted from radio stations in the 15-25 KHz range. The signals are propagated with the magnetic component of the field being horizontal in undisturbed areas.

Conductivity contrasts in the earth create secondary fields, producing a vertical component and changes in the field strength or amplitude. These conductive areas may be located, and to a degree, evaluated by measuring the various parameters of this electromagnetic field.

The Sabre VLF-EM receiver is tuned to receive any 4 transmitter stations: usually C - Cutler, Maine; S - Seattle; H - Hawaii; and A - Annapolis.

The station used in the survey should be selected so that the direction of the signal is roughly perpendicular to the direction of the grid lines which, in turn, should be laid out perpendicular to the regional strike.

MEASUREMENTS :

The Sabre VLF-EM receiver can be used to measure the following characteristics of the VLF field:

(a) Tilt angle of resultant field;

(b) Field strength of (a) horizontal component of field;

(b) vertical component of field.

Field Procedure

The following procedure should be followed to measure the dip angle of null and the field strength of the horizontal component of the VLF field.

Initial Field Strength Adjustment

Adjust the gain control to provide a suitable relative field strength measurement, as follows:-

(a) hold receiver in horizontal position (meter faces horizontal) and rotate in a horizontal plane until a null is indicated on the F.S. meter; rotate 90° in this horizontal plane (F.S. meter reads maximum)

(b) adjust gain control so that the F.S. meter reads 100

(c) record gain control setting (000 to 999), and do not readjust unless a major field strength occurs.

The above procedure should be carried out at the beginning of each day's survey and checked during the day.

Dip Angle Measurement Procedure

1. Hold receiver in horizontal position and rotate in the horizontal plane until a null is observed. This aligns receiver in the field and the operator should be facing southerly or easterly depending on transmitter location.

2. Bring receiver up to the vertical positon (meter faces vertical) and rotate the receiver in the vertical plane perpendicular to the transmitter direction until a null or minimum reading is observed on the field strength meter.

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3. Hold the receiver in this field strength null position and read the inclinometer in degrees. Record this dip angle of null along with sign (+ or -).

Horizontal Field Strength Measurement Procedure

1. Return receiver to the horizontal position.

2. Re-establish null bearing in horizontal plane.

3. Rotate receiver 90° in the horizontal plane.

4. Depress F.S. push button switch and observe field strength meter reading for sufficient time to obtain an average F.S. meter reading. (Depressed F.S. switch slows needle action and reduces meter reading

by half. The reading will normally range around 50).

5. Record F.S. reading.

Filtering Technique For VLF-EM Dip Angle Data

The standard profile method of presenting dip angle data may be difficult to interpret. A filtering technique, described by D.C. Fraser, 1969 (Geophysics, Vol. 34, No. 6, p. 958-967) enables the data to be presented on a plan map with conductive areas defined by contours.

The following explains the calculation:-

<u>Line</u>	Station	<u>Nu11</u>	<u>Fil</u>	<u>te</u> r
8N	0 E	+3		
	1 E	+4	+3+4= +7	
	2 E	+4	+4+4= +8 +7-(+10)=	-3
	3 E	+6	+4+6= +10 +8-(+13)=	-5
	4 E	+7	+13 +10-(+16)=	-6
	5 E	+9	+16	-8
	6 E	+12	+21	-12
			+28	+3
	7 E	+16	+18	+30
	8 E	+2		
	9 E	-4	-2	+32
	10 E	-10	-14	+14
	11 E	-6		-7
	12 E	-1->	-6-1= -7	

Figure 1 is an example of a field sheet showing null angle reading, filtered reading and relative field strength. Figure 2 shows the field sheet with filter card overlaid. The small window in the side of the card shows the four readings used to calculate the filtered reading, and an arrow showing that the filter reading is to be plotted between Station 8E and 9E as indicated in Figure 1. The card is moved down the field sheet, one reading at a time as a guide while carrying out the filter procedure. Throughout the survey care must be taken to ensure that the filtered data has the correct sign. The positive values only are plotted and contoured while for negative values, only the negative sign is plotted. Crone suggests in instructions for the Radem VLF-EM, the use of N-S or E-W notation instead of (+ or -) signs, however, for filtering a sign must be substituted.

The following convention may be used to ensure the correct sign of filtered data and provide a consistent cross-over pattern when studying the profiled null angle data.

1. When taking a reading, <u>always</u> face southerly, on east-west lines, and always face easterly on north-south lines.

2. Record data on field sheets (top to bottom) as follows:

on N-S lines record from south to north

on E-W lines record from west to east.

3. Plot and profile dip angle data on plan maps facing map north or map west.

The above convention will provide correct data regardless of the property location relative to the transmitter being used.

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Line	Stn.	Hull	Filter	Landard Contraction Contractio	
	OE	+3		50	
	IE	+4		50	
	2.E	+4.	3	52	
	35	+6	+=5	52	
	4E	+7		52	
_(56	+9		52	-1
	<u>6 E</u>	+12	+3	53	
	<u>7</u> €	+16	+30-	60	1
	<u>8E</u>	+2	-+ 32-	65	Xoral
	9E	-4	+ 14	6Z	
	10 E	-/0		50	
	IIE	-6	18	48	
	12E	-/		48	
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	145	+4		52	
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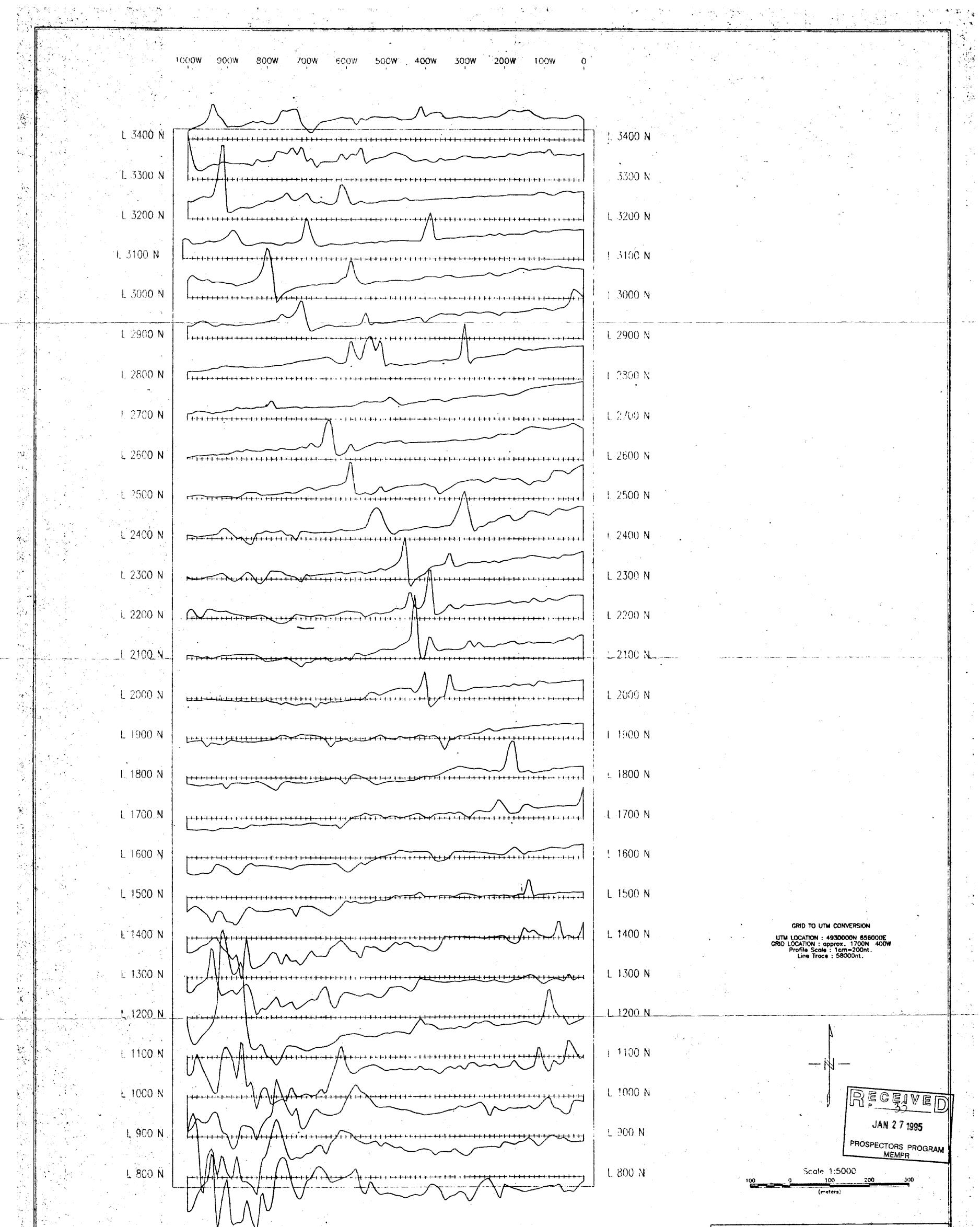
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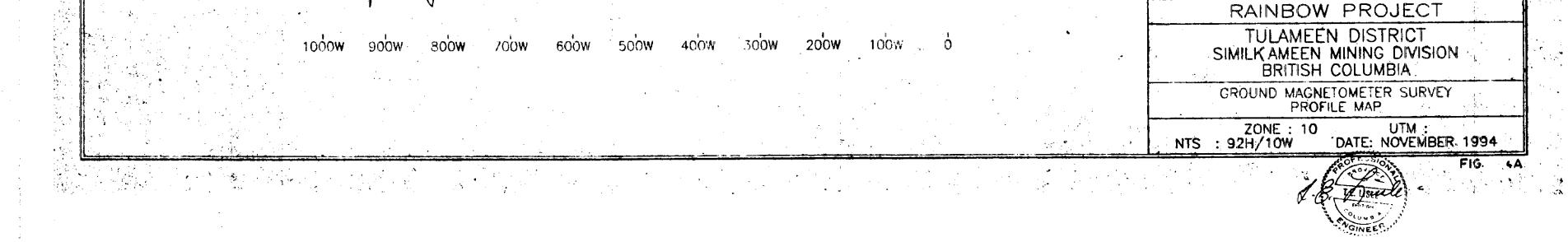
Fig. 1 Example of Field Sheet

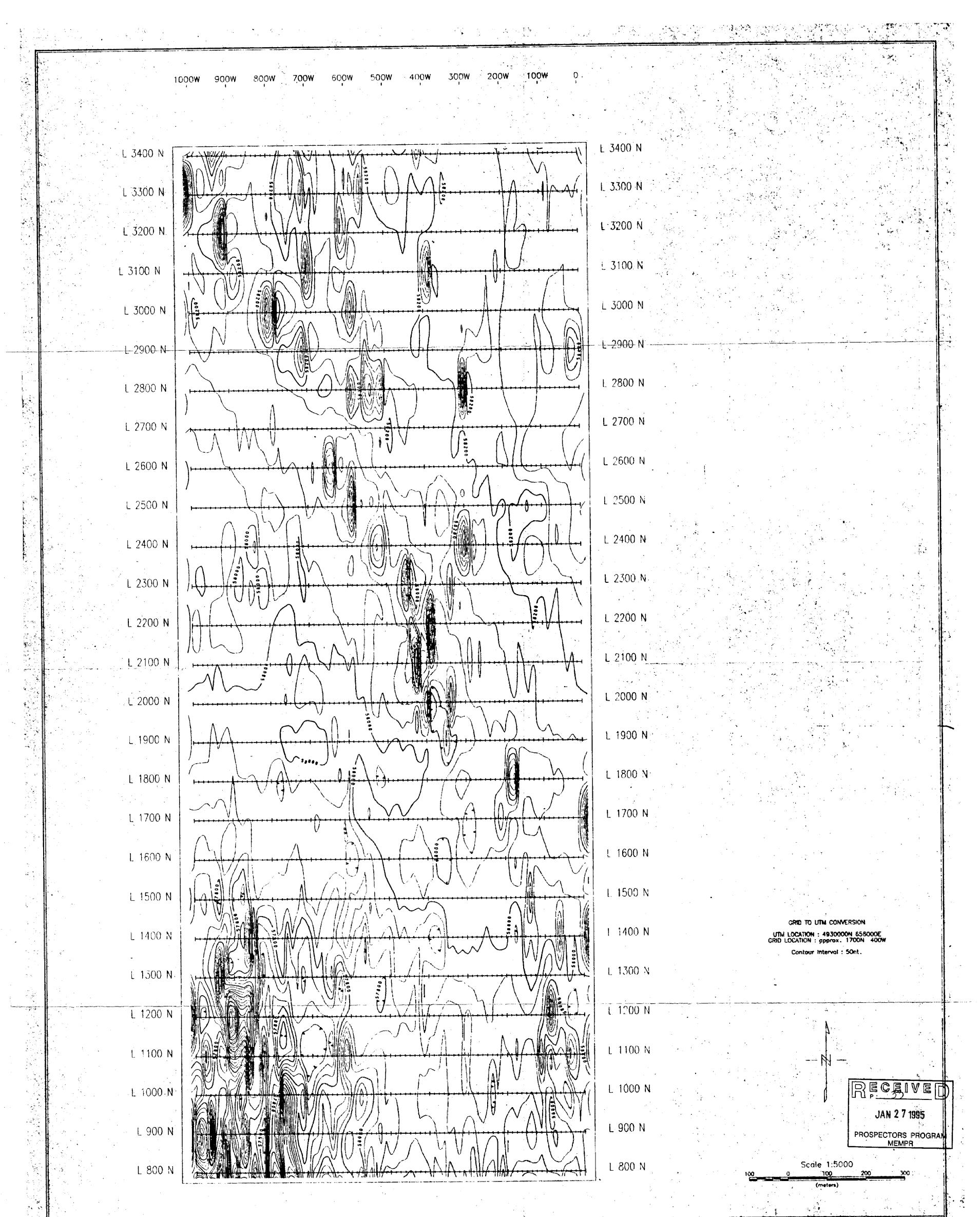
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		+2	-+-32	65
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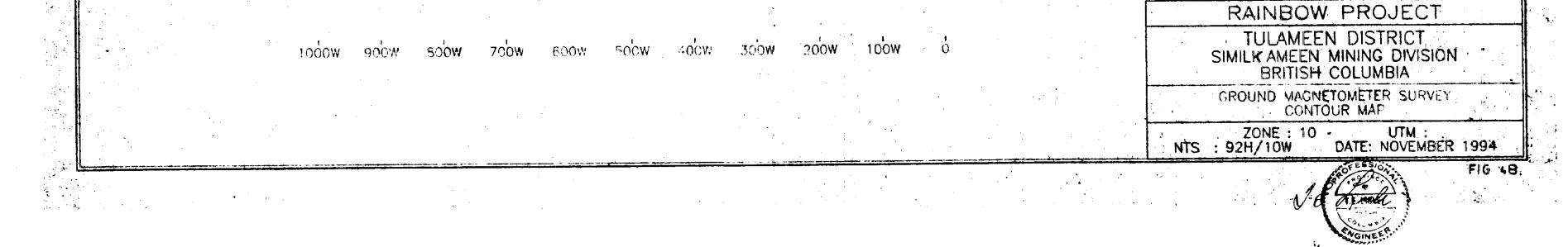


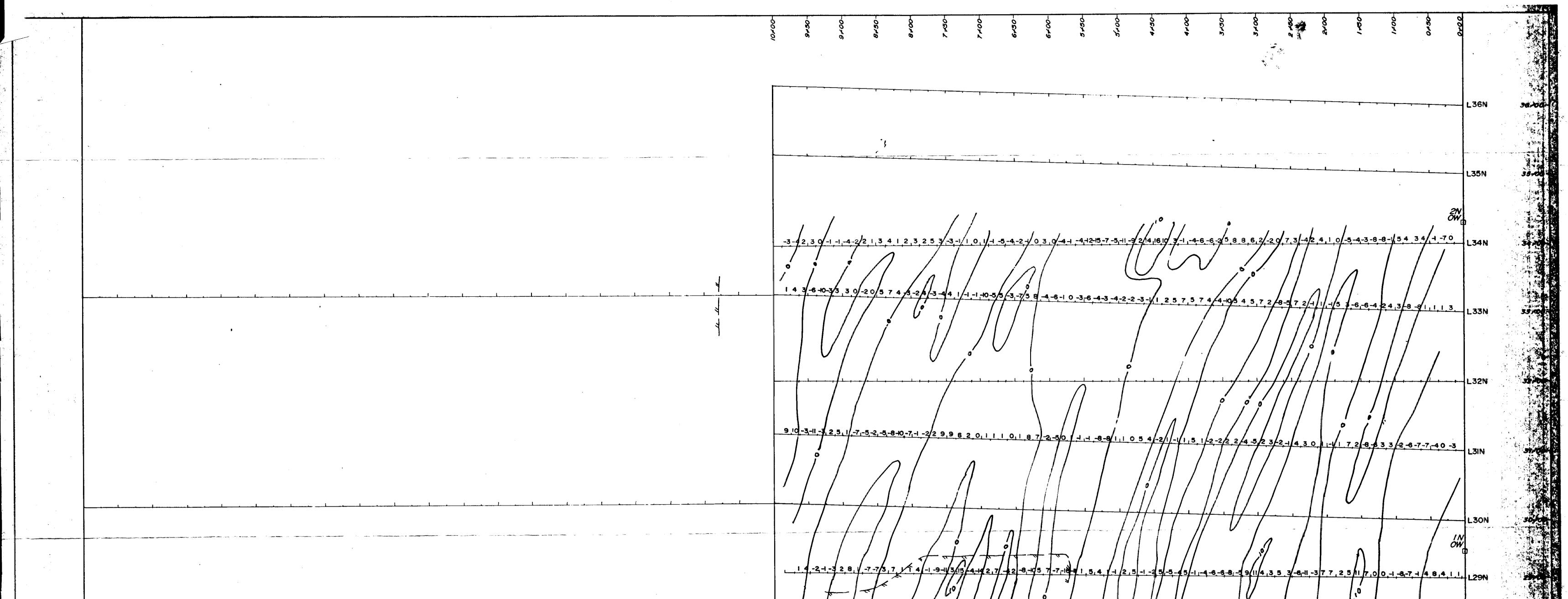
Fig. 2 Field Sheet with Filter Card Overlayed



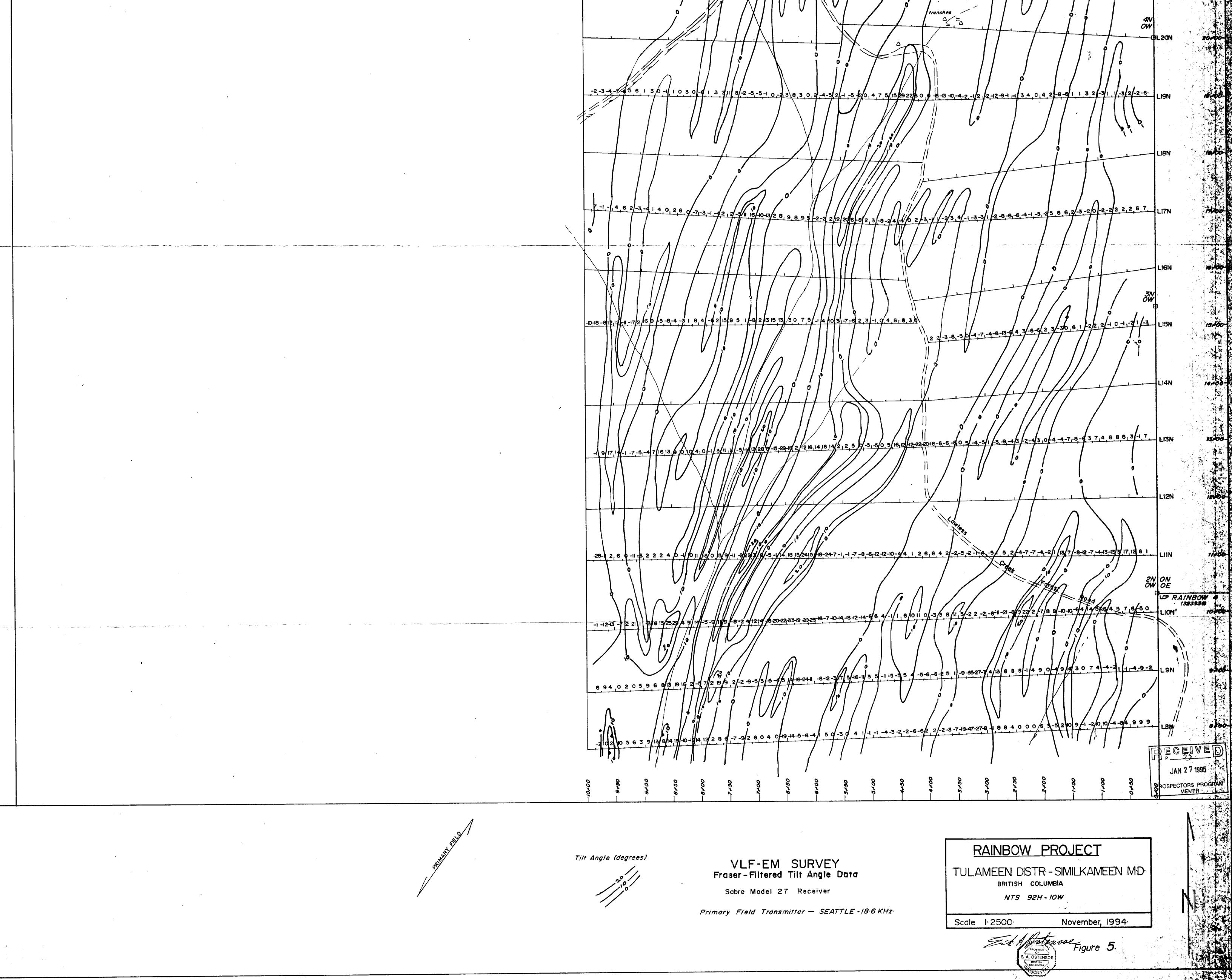








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